

# **Comparison of Shielding Effectiveness of High Q Canonical Cavities with Thin Slots in a Mode-Stirred and Anechoic Chamber**

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# Outline

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- **Why is this important?**
- **Current Gain Correction Methods**
- **Measurement techniques**
- **Test Objects**
- **Results**
  - 1, 2, and 8 slot cylindrical, high Q cavity ( $Q \approx 4000$ )
  - 1 slot cylindrical lower Q cavity ( $Q \approx 800$ )
- **Conclusions**



# Why is this important?

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- **A gain correction is needed to go from mode-stirred chamber shielding effectiveness data to free-space data**
  - **For transfer functions**
  - **For susceptibility testing**



# Gain Corrections

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Gain correction for a single slot (from Warne, et. al at Sandia)

$$D \approx \frac{4\ell}{\lambda} \qquad D_m \approx \begin{cases} 0, & D < 1 \\ D, & D \geq 1, \end{cases}$$

Gain correction for an intentional emitter [1]

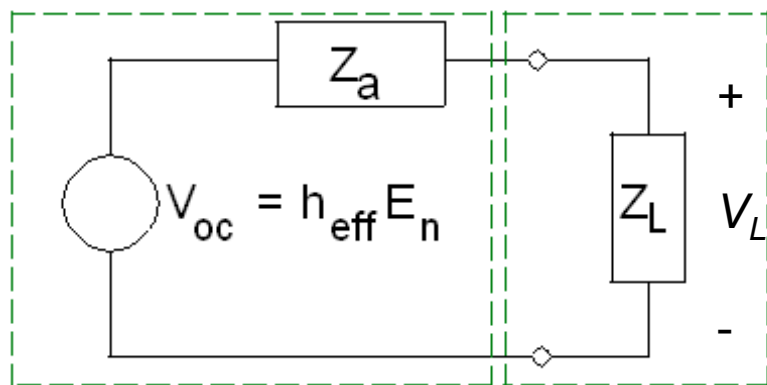
$$D_m \approx \begin{cases} 3, & ka \leq 1 \\ (ka)^2 + 2ka, & ka > 1, \end{cases}$$

Gain correction for an unintentional emitter for a planar cut [2]

$$D_m \approx \begin{cases} 2.45, & ka \leq 1 \\ 0.577 + \ln(2(2ka + 1)) + \frac{1}{4(2ka + 1)}, & ka > 1, \end{cases}$$

# Calculating chamber and test object interior fields

Monopole Sensor



The load voltage,  $V_L$ , is measured. Use the following values to calculate the normal electric field picked up by the monopole.

$Z_L = 50 \Omega$  load

$Z_a$  = monopole radiation impedance

$V_{oc}$  = monopole open circuit voltage

$h_{eff}$  = monopole effective height

**$E_n$  = normal electric field  
(quantity of interest)**

## Calculation derivation

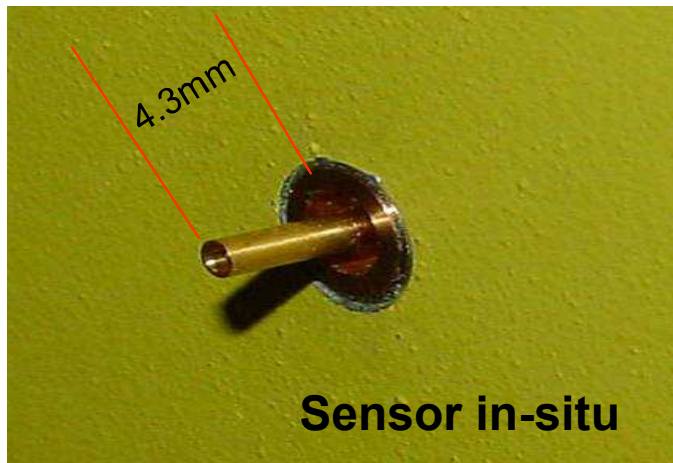
$$V_L = V_{oc} \frac{Z_L}{Z_a + Z_L} \quad \text{from circuit theory}$$

$$V_{oc} = \frac{V_L}{Z_L} (Z_a + Z_L) = h_{eff} E_n$$

$$E_n = \frac{V_L}{Z_L h_{eff}} (Z_a + Z_L)$$

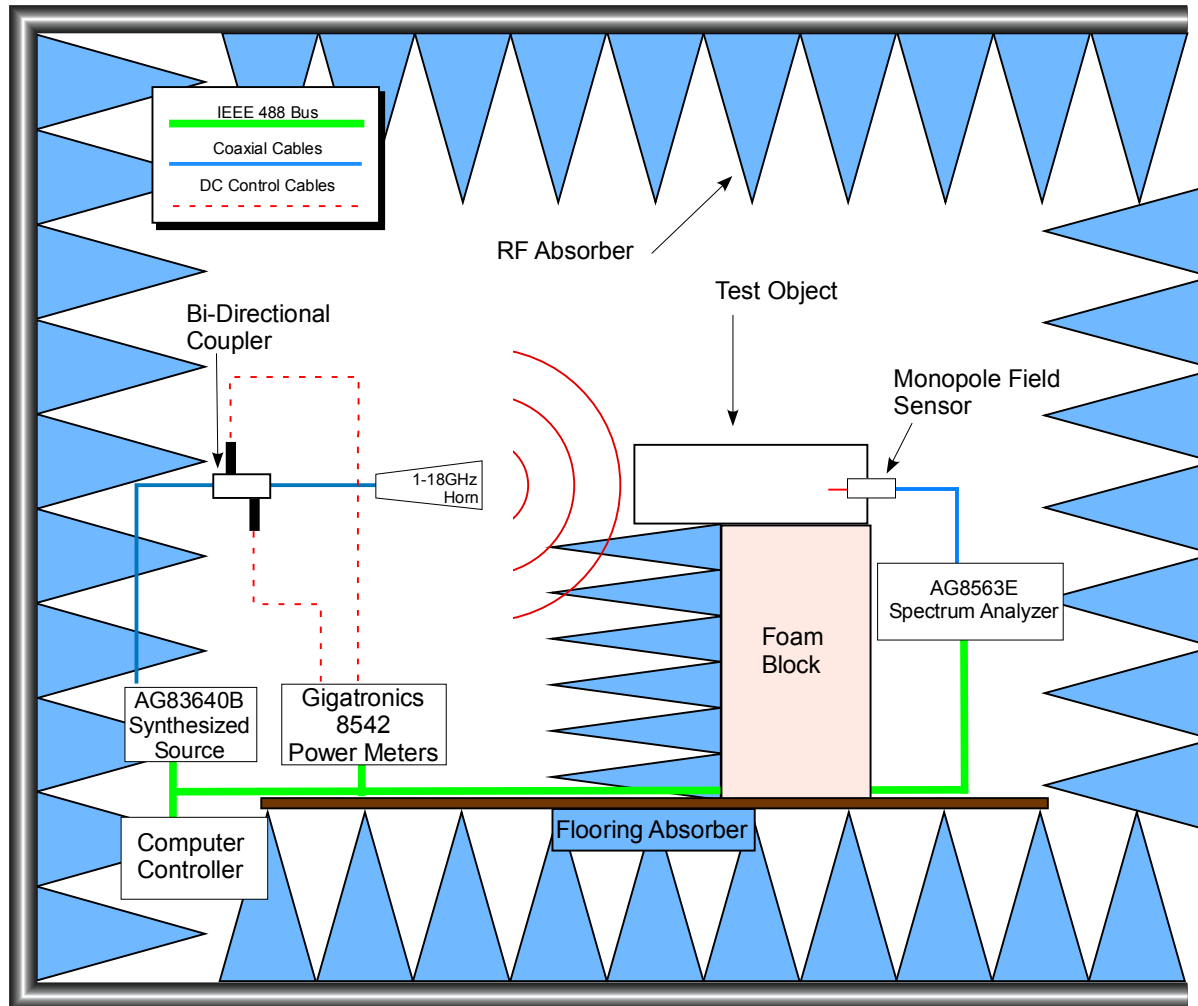
# Monopole Sensors

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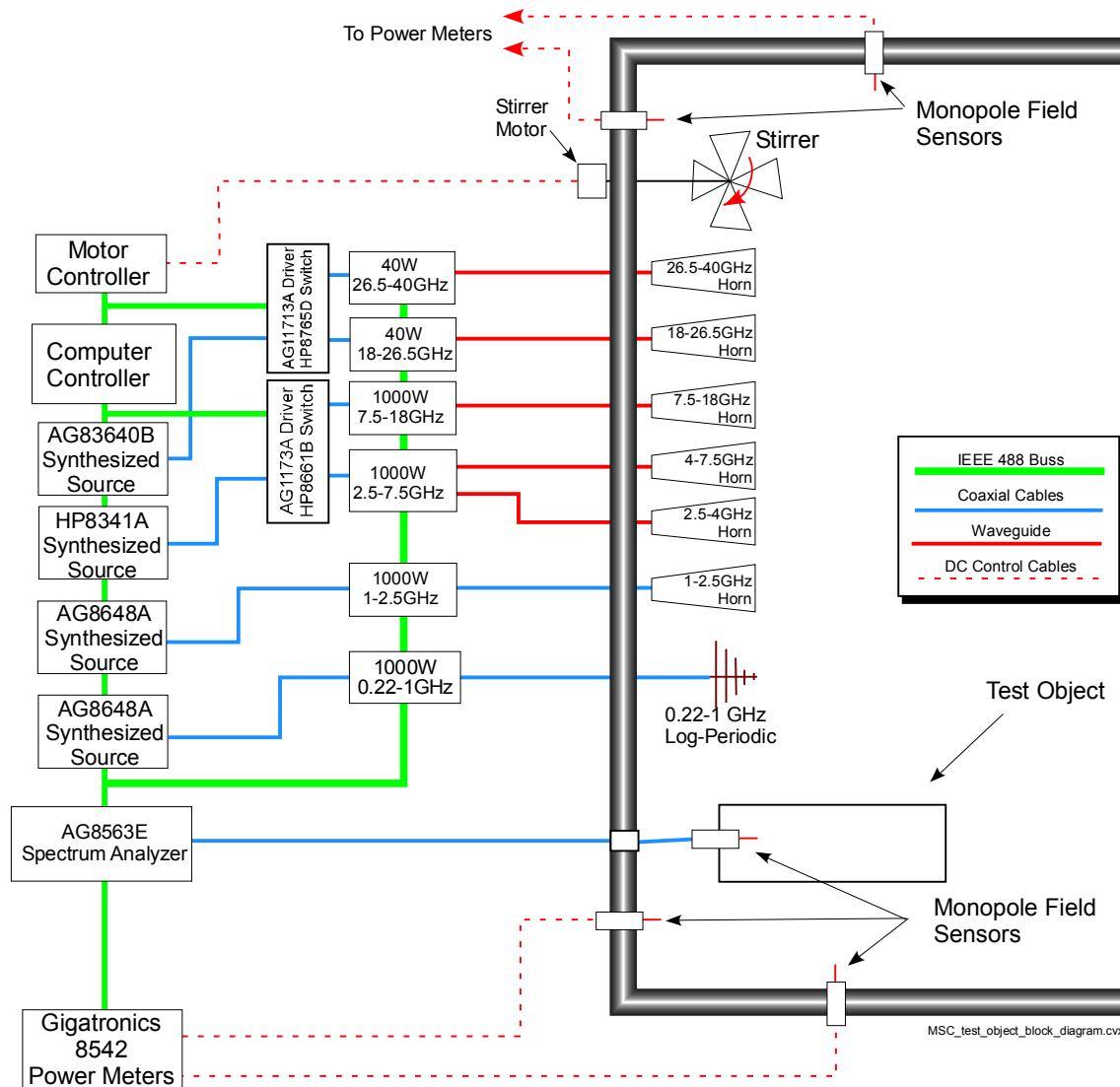
**220 MHz – 18 GHz  
Monopole sensor**

# Anechoic Chamber Diagram



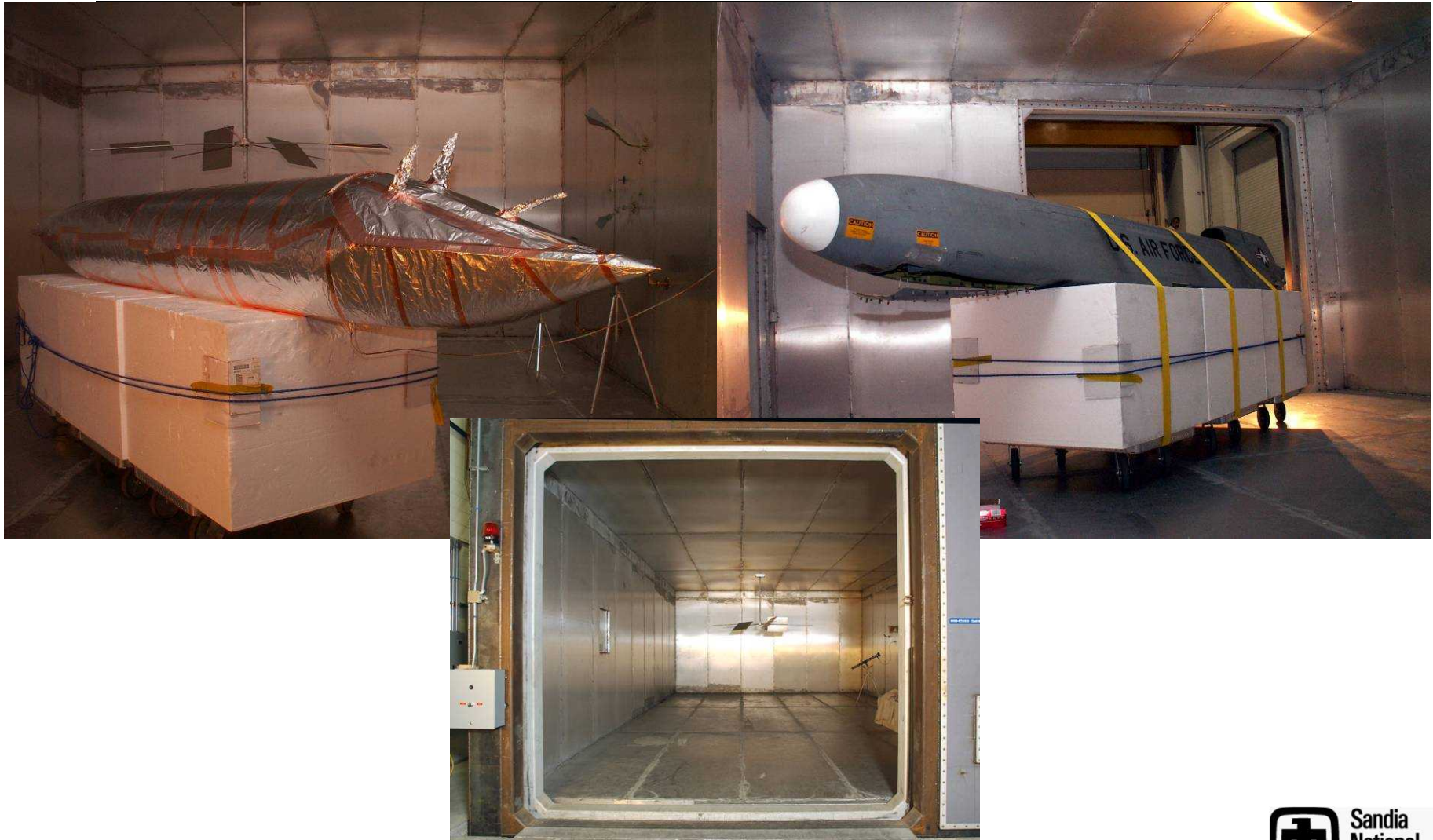
Anechoic\_test\_object\_block\_diagram.cvx

# Mode-Stirred Chamber Diagram





# Mode-Stirred Chamber (MSC)





# Mode-Stirred Chamber (MSC)

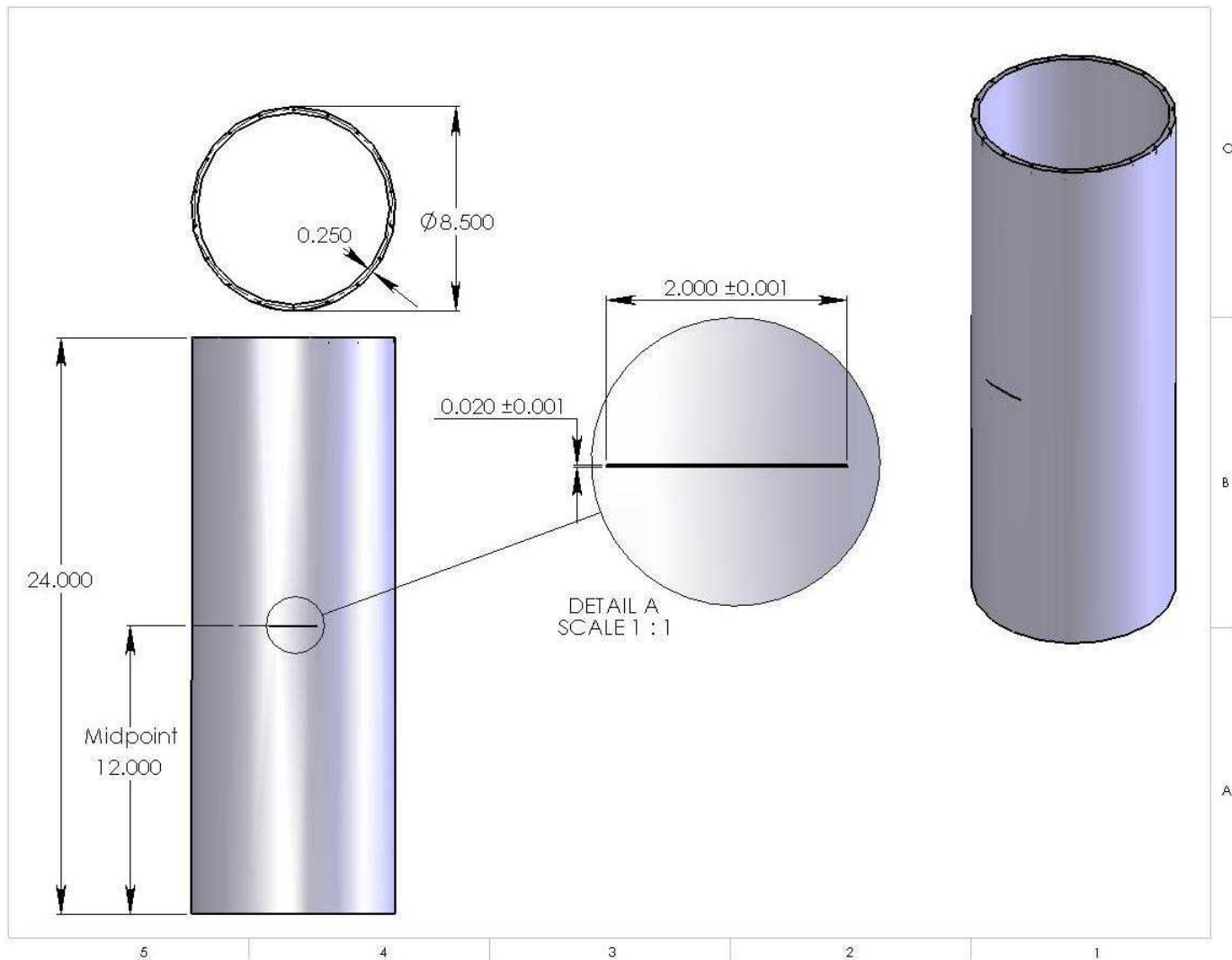
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- **MSC provides statistically uniform incident electromagnetic field**
- **A superposition of plane waves**
- **Bathes test object in electromagnetic field, which ensures leaks are found**
- **Cables do not need to be in a specific orientation**

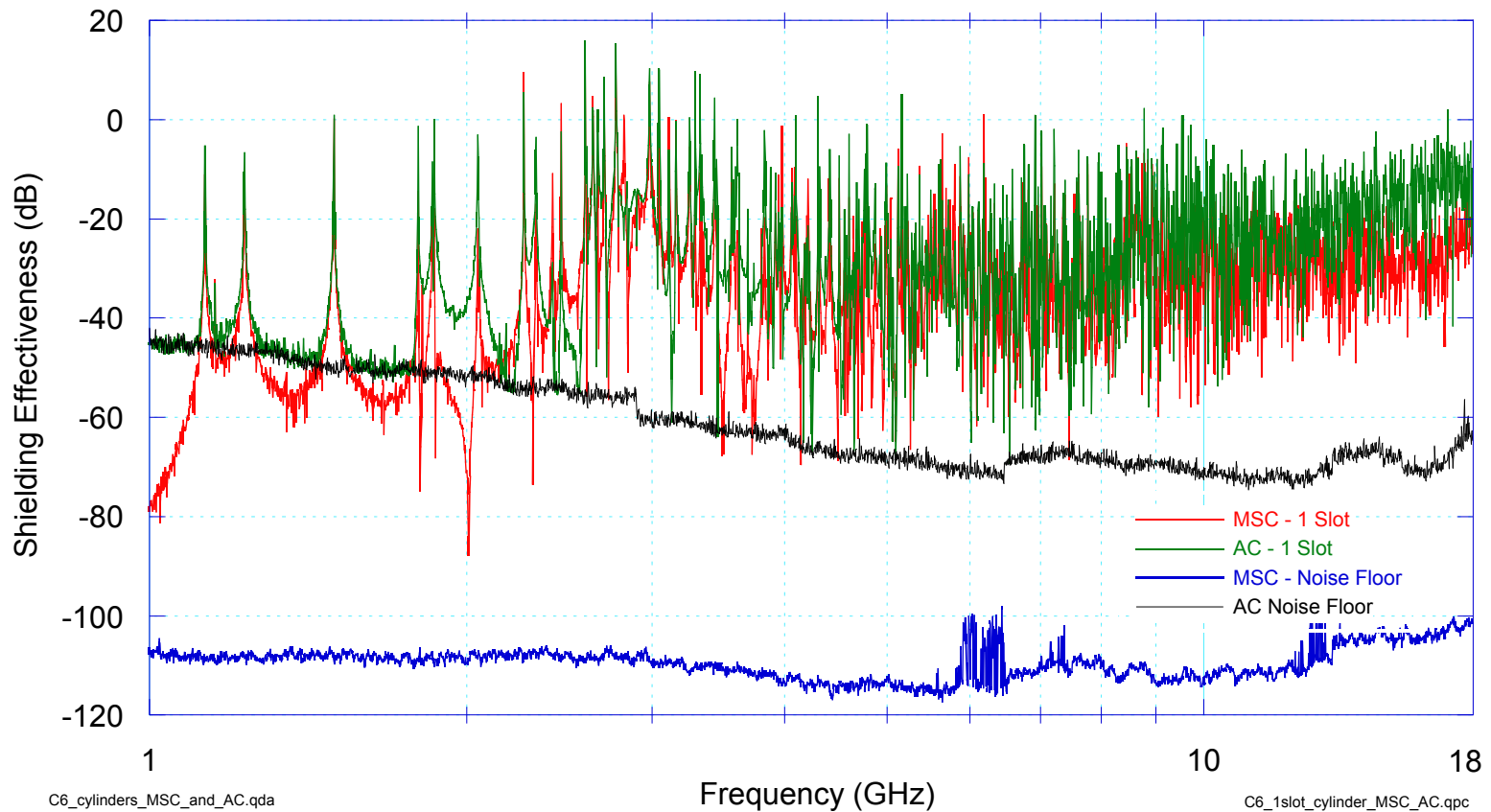
Performance Characteristics of Mode-Stirred Chamber Test Facility

|                     |                                     |
|---------------------|-------------------------------------|
| Dimension           | 4 x 7 x 11 m (HxWxL)                |
| Design              | Welded Aluminum                     |
| Entrance Dimensions | 3.7 x 3.7 m                         |
| Frequency           | 0.22 – 40 GHz                       |
| Input Power         | Solid State and TWT amplifiers      |
|                     | 1000 W,<br>220 MHz – 18 GHz         |
|                     | 40 W,<br>18 GHz – 40 GHz            |
| Field Strength      | ~3000 V/m peak,<br>220 MHz – 18 GHz |
|                     | ~600 V/m peak,<br>18 – 40 GHz       |

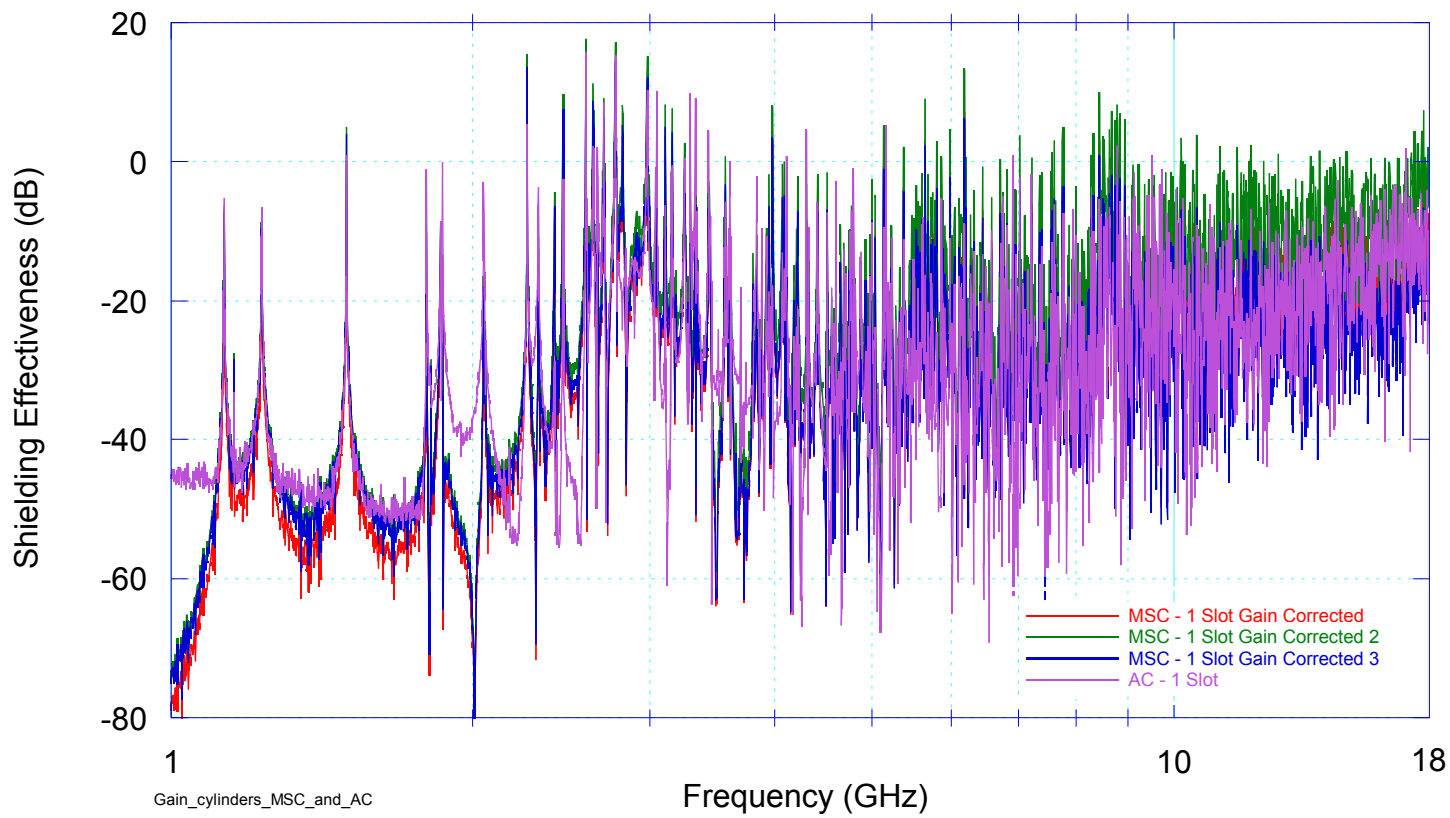
# Cylindrical Test Object



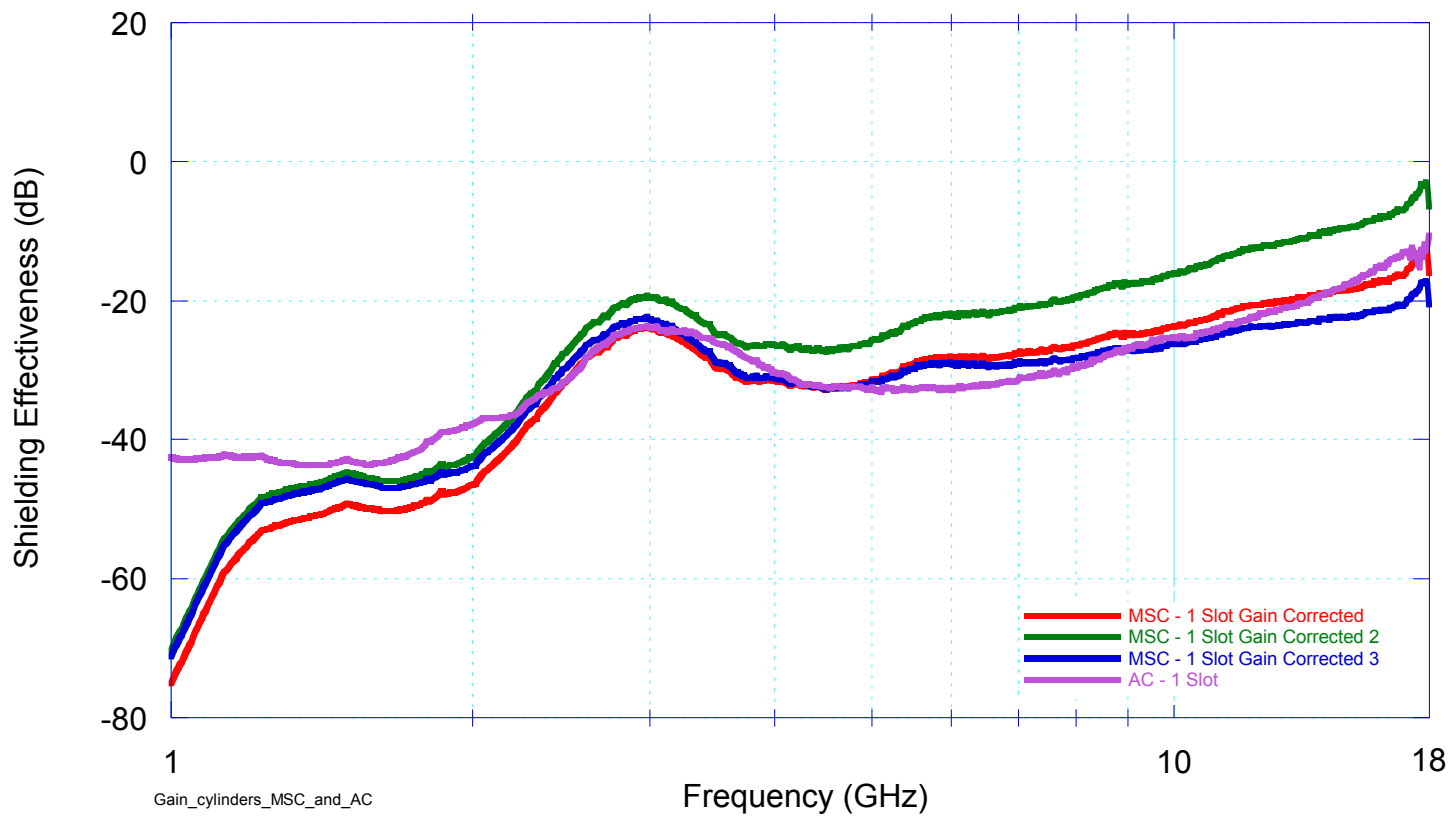
# Single Slot Cylinder



# Single Slot Cylinder with Gain Correction

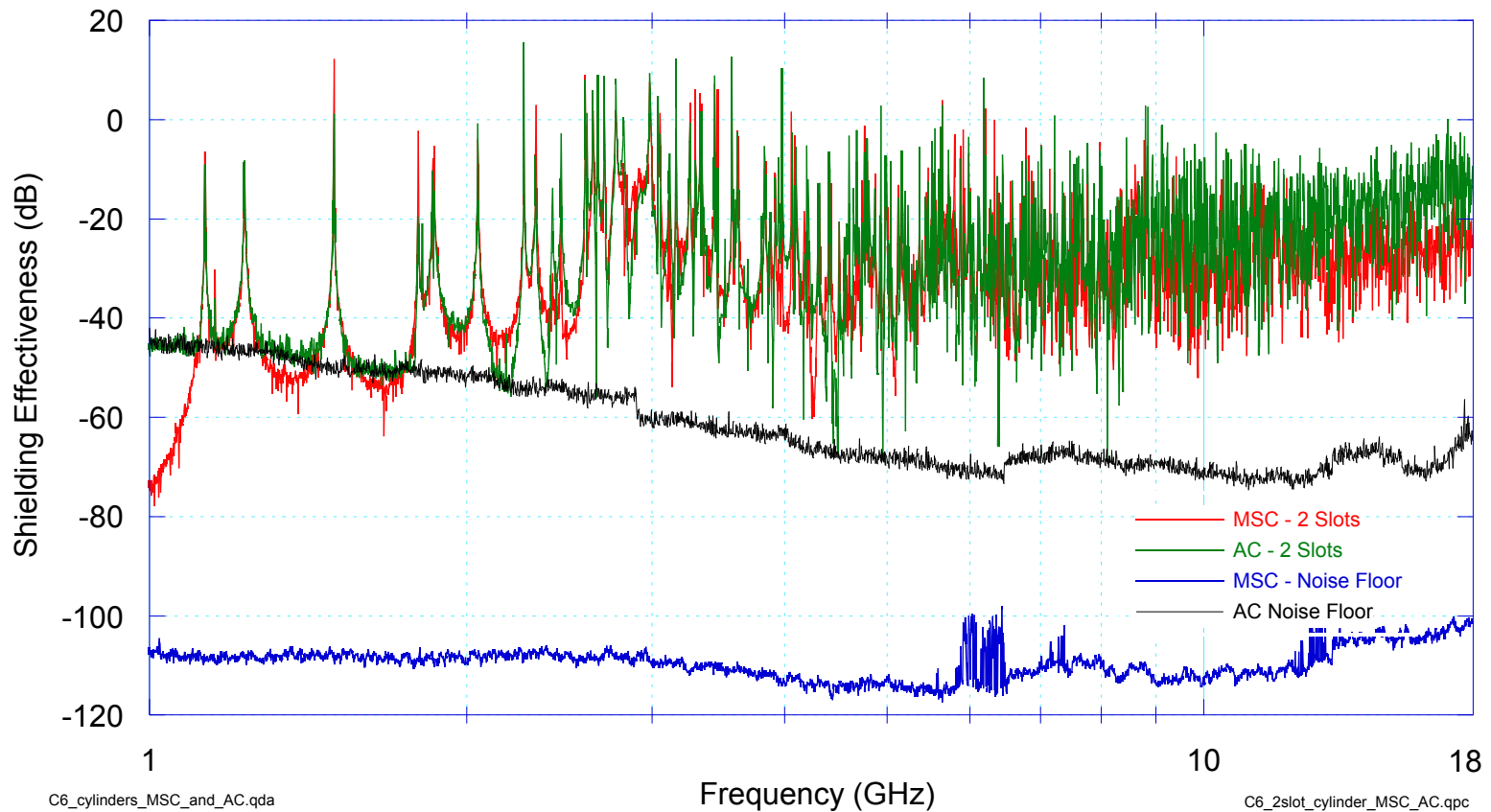


# Gain Corrected and Smoothed

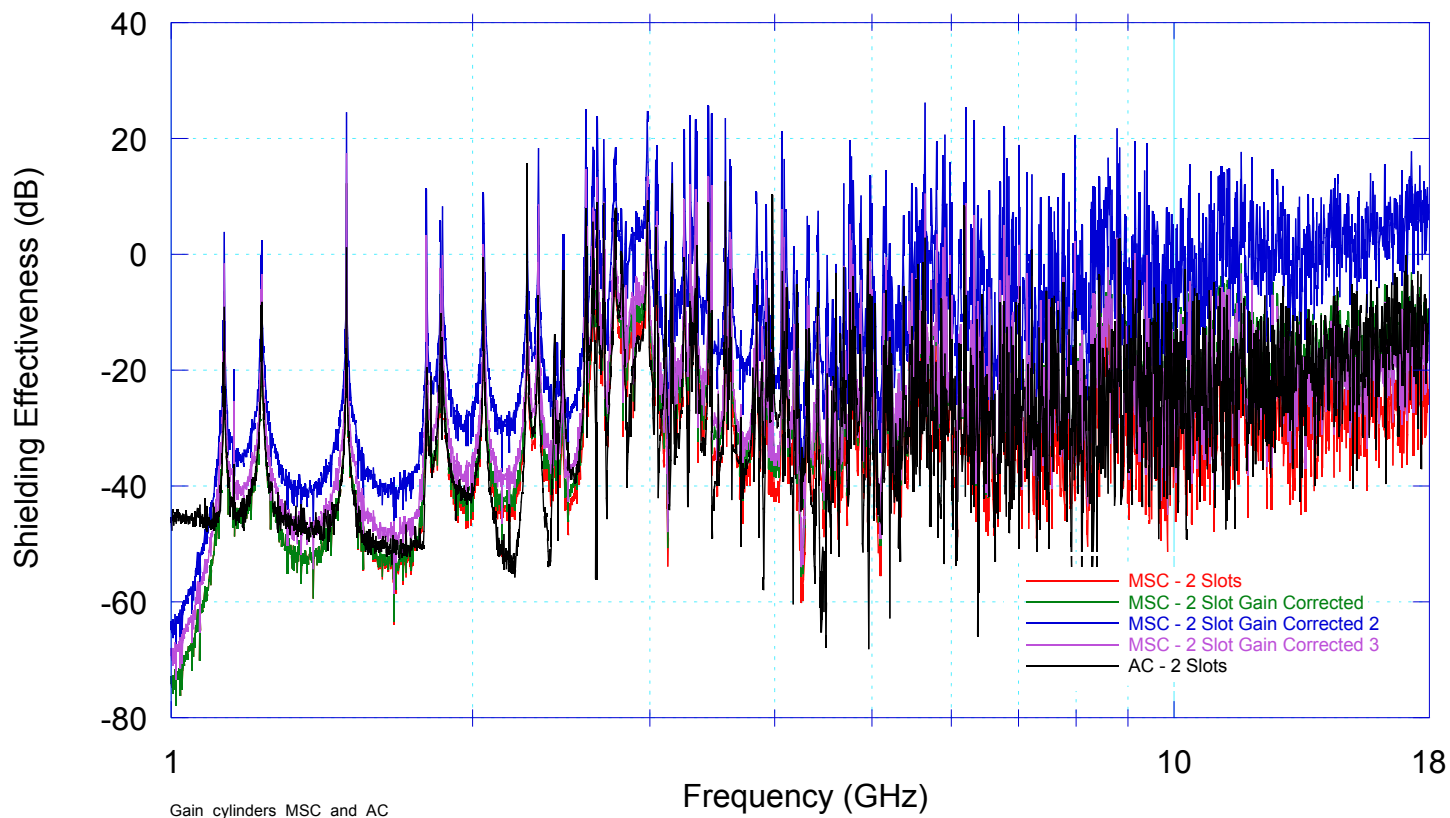




# Two Slot Cylinder

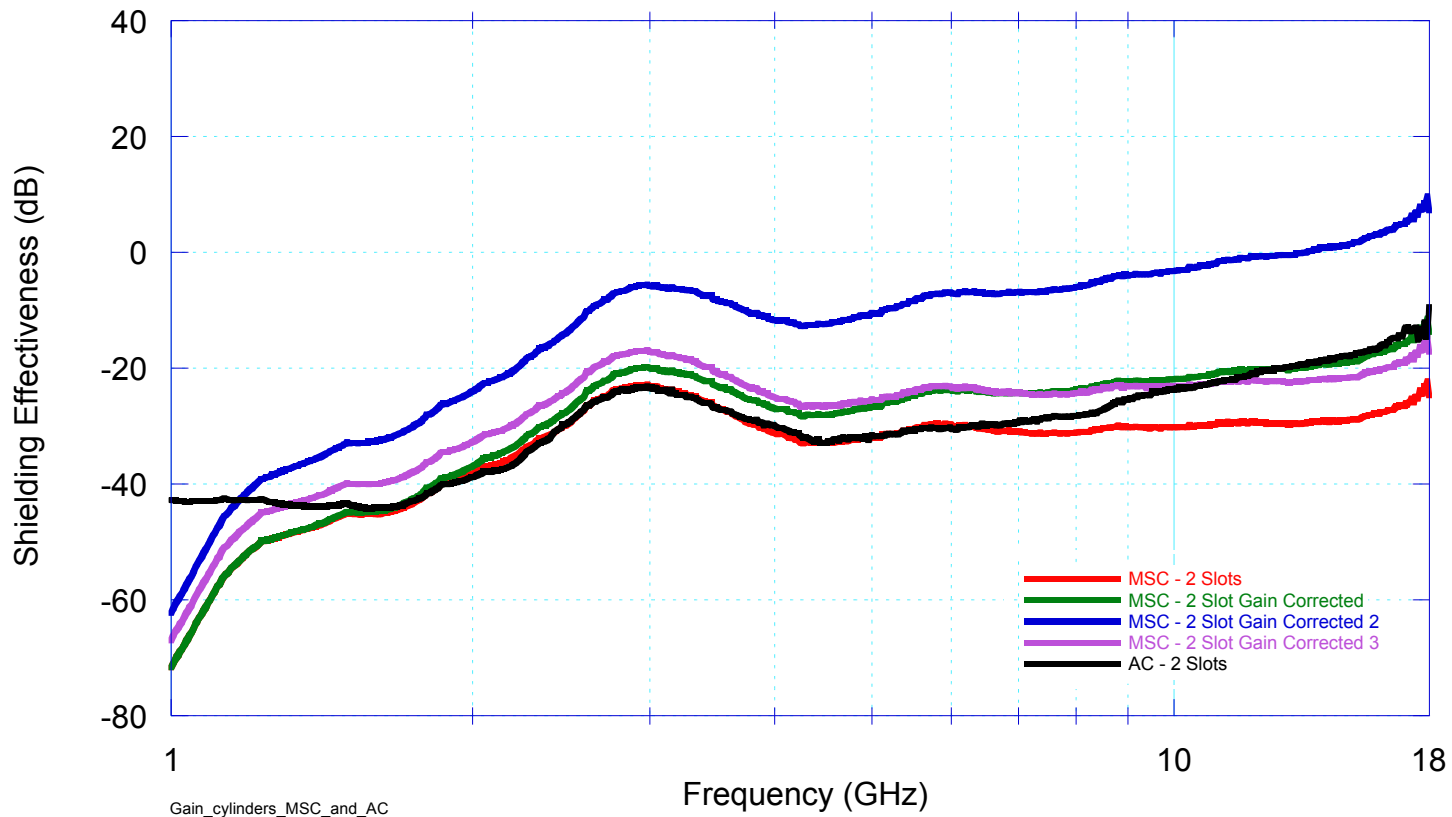


# Two Slot Cylinder with Gain Correction

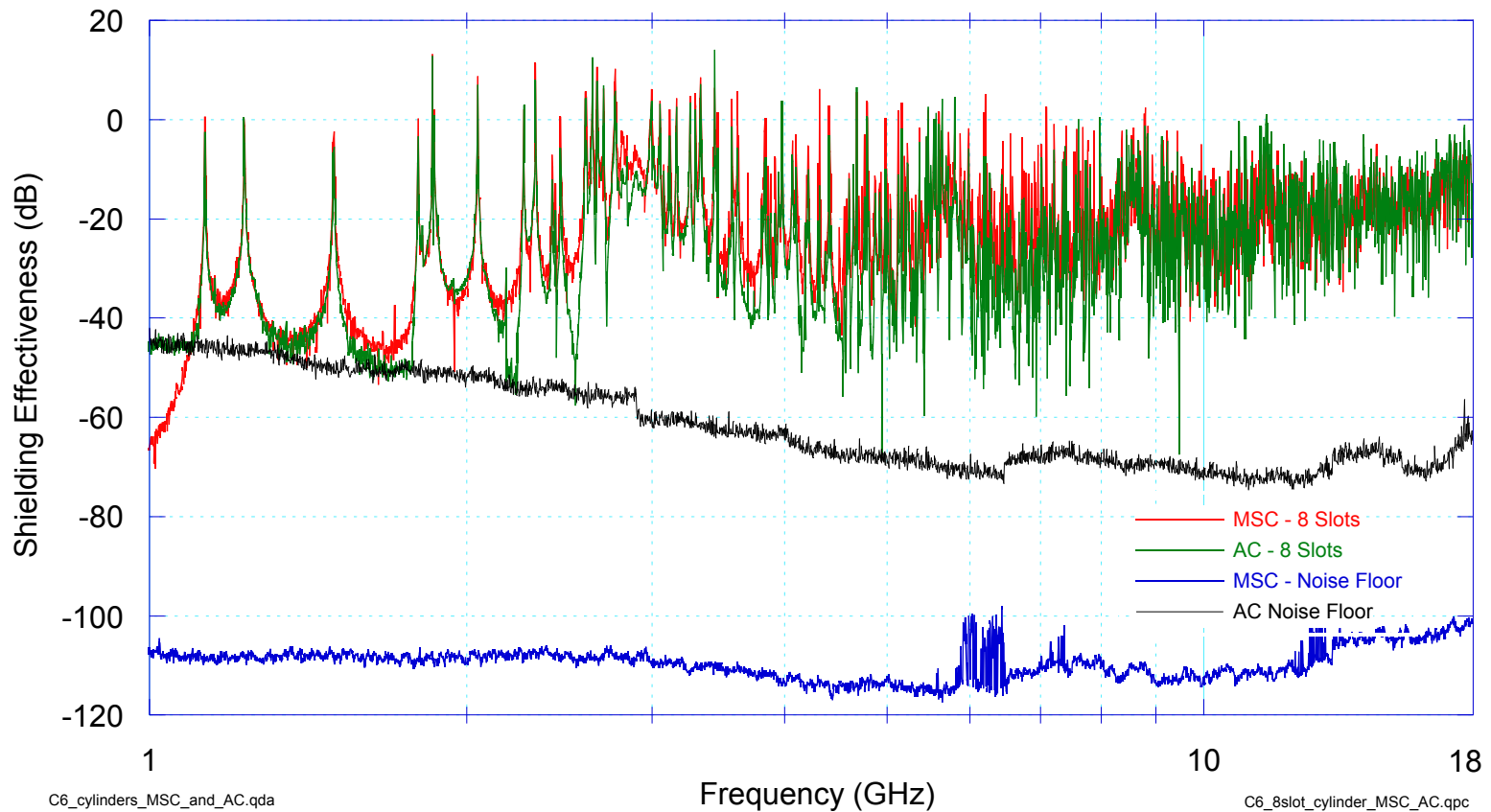




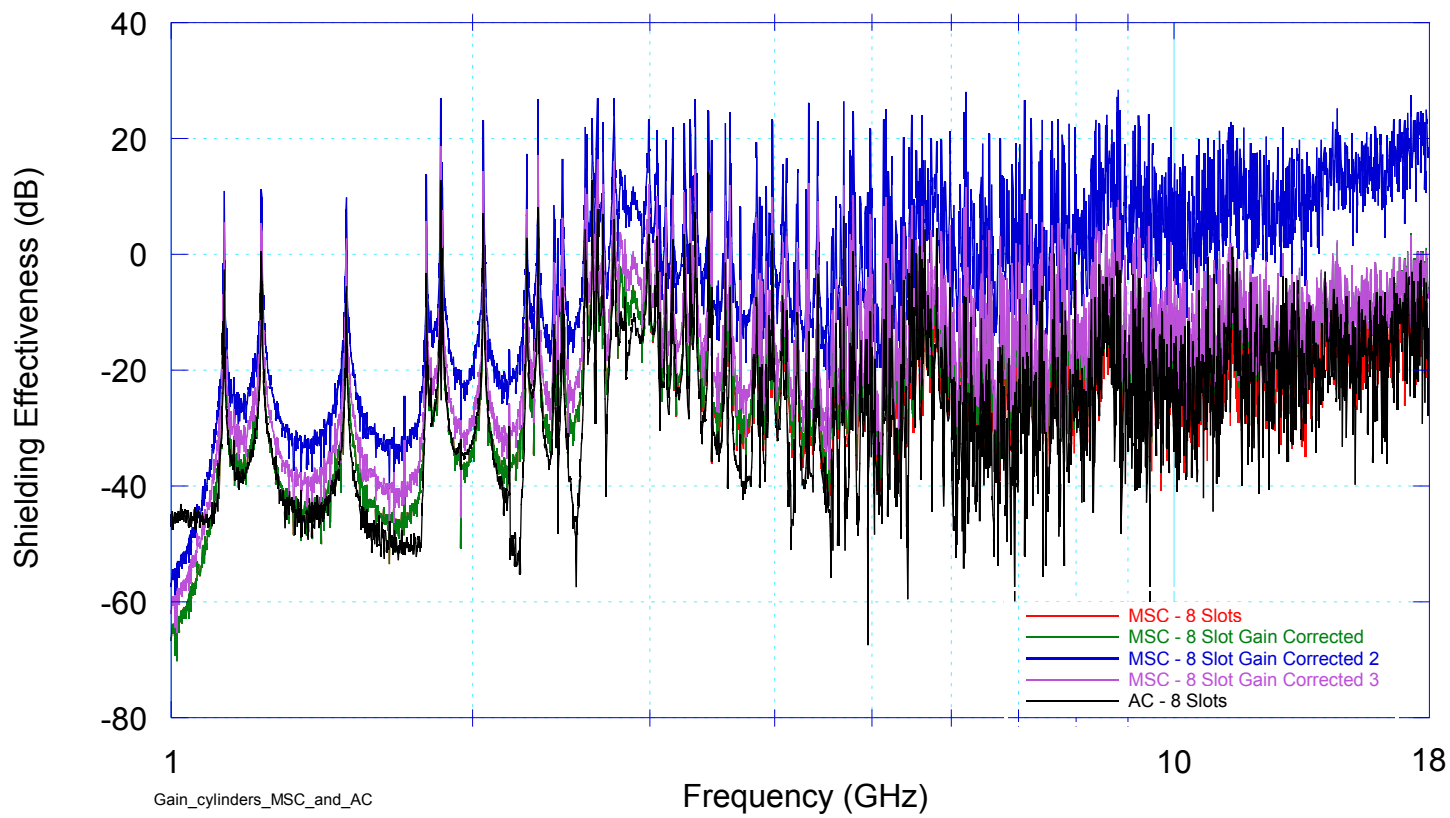
# Gain Corrected and Smoothed



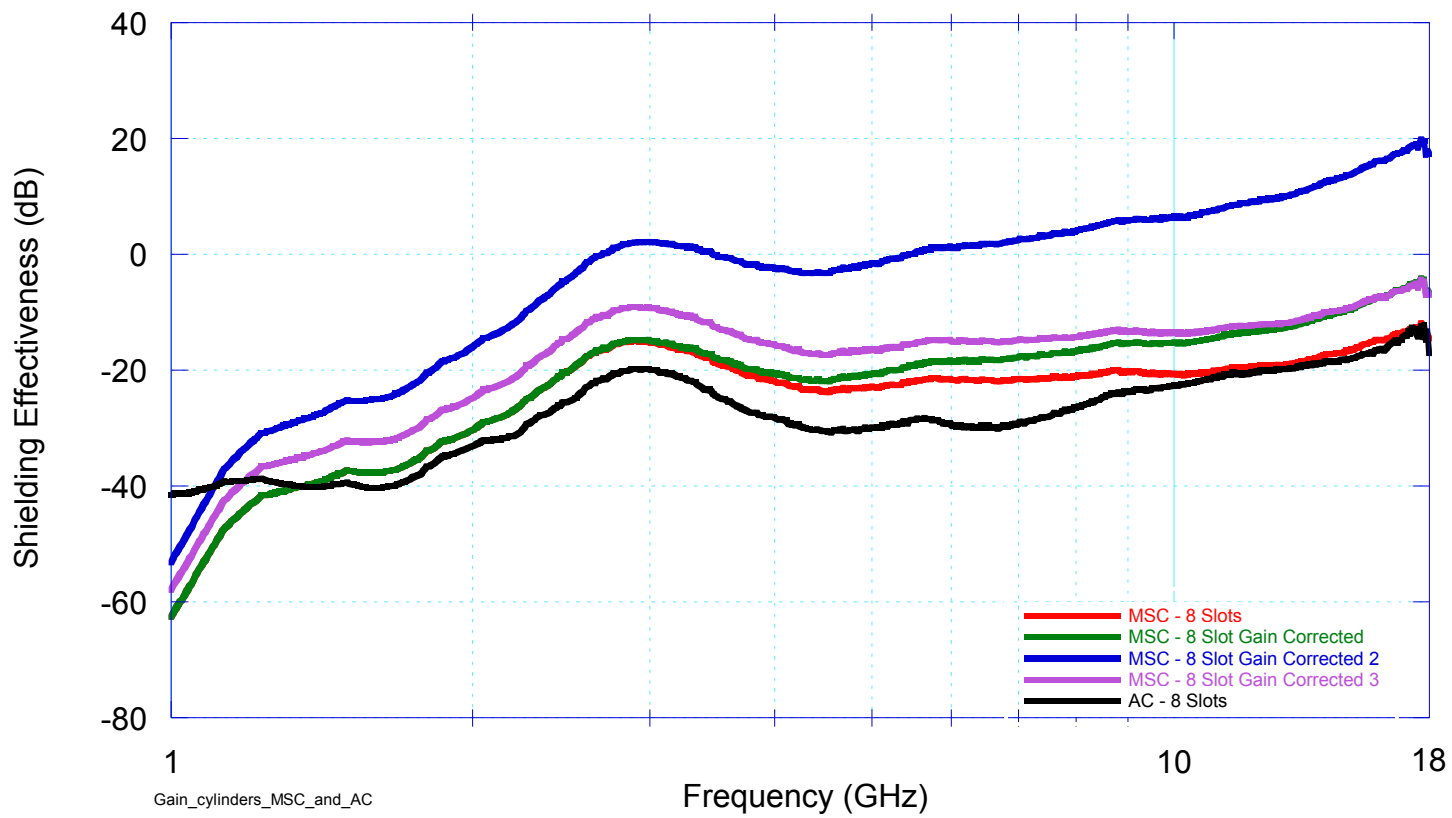
# Eight Slot Cylinder



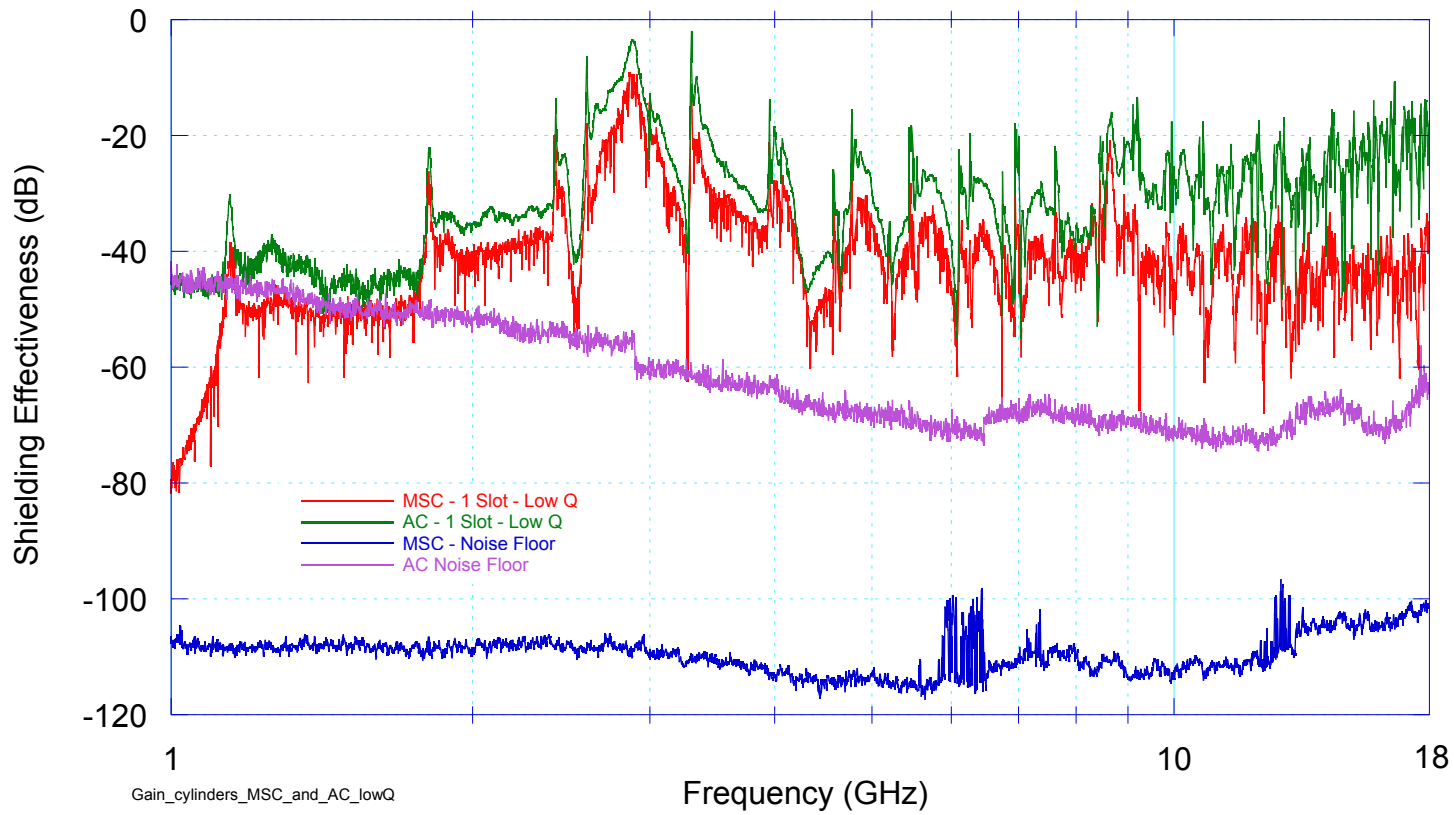
# Eight Slot Cylinder with Gain Correction



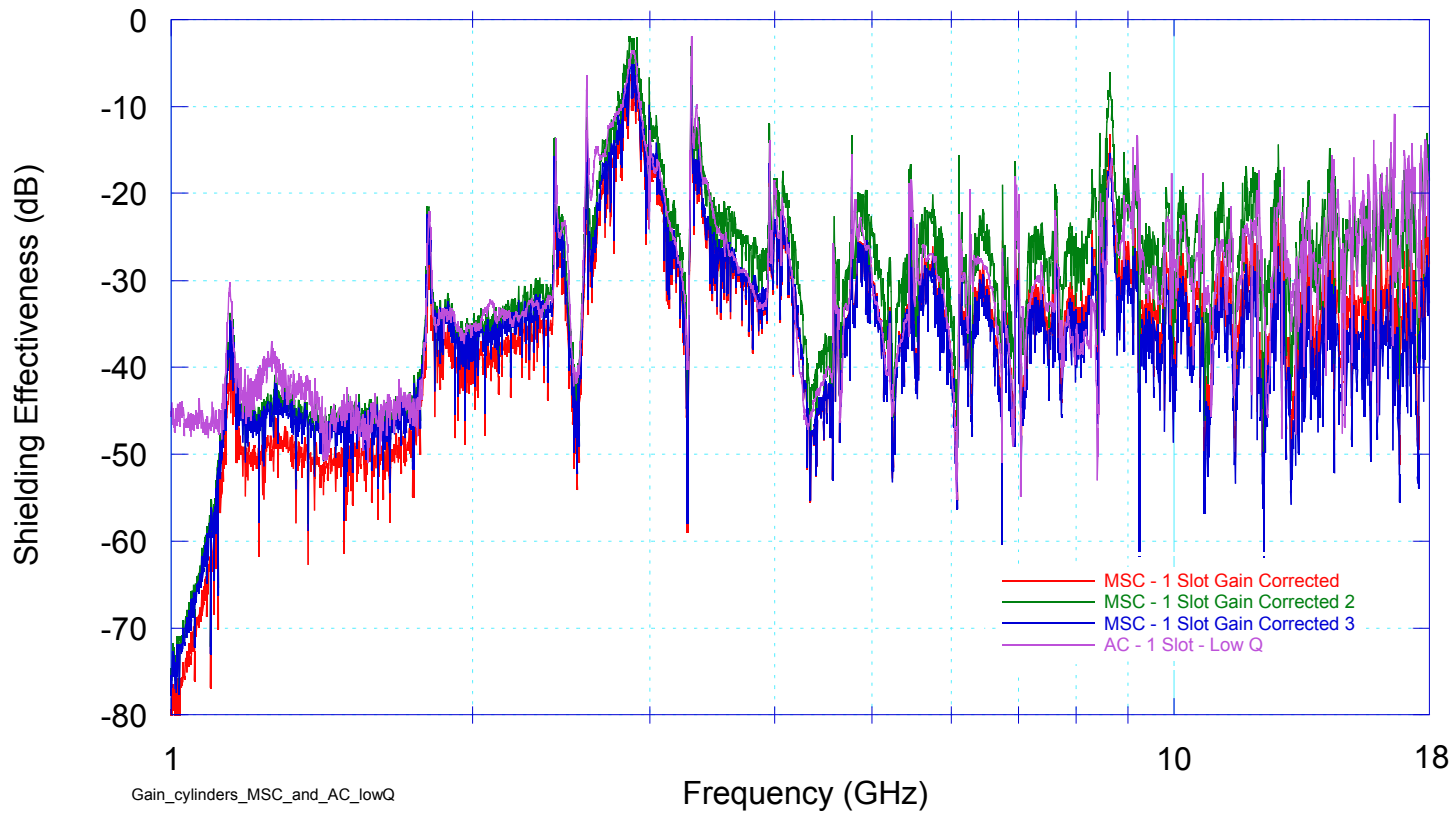
# Gain Corrected and Smoothed



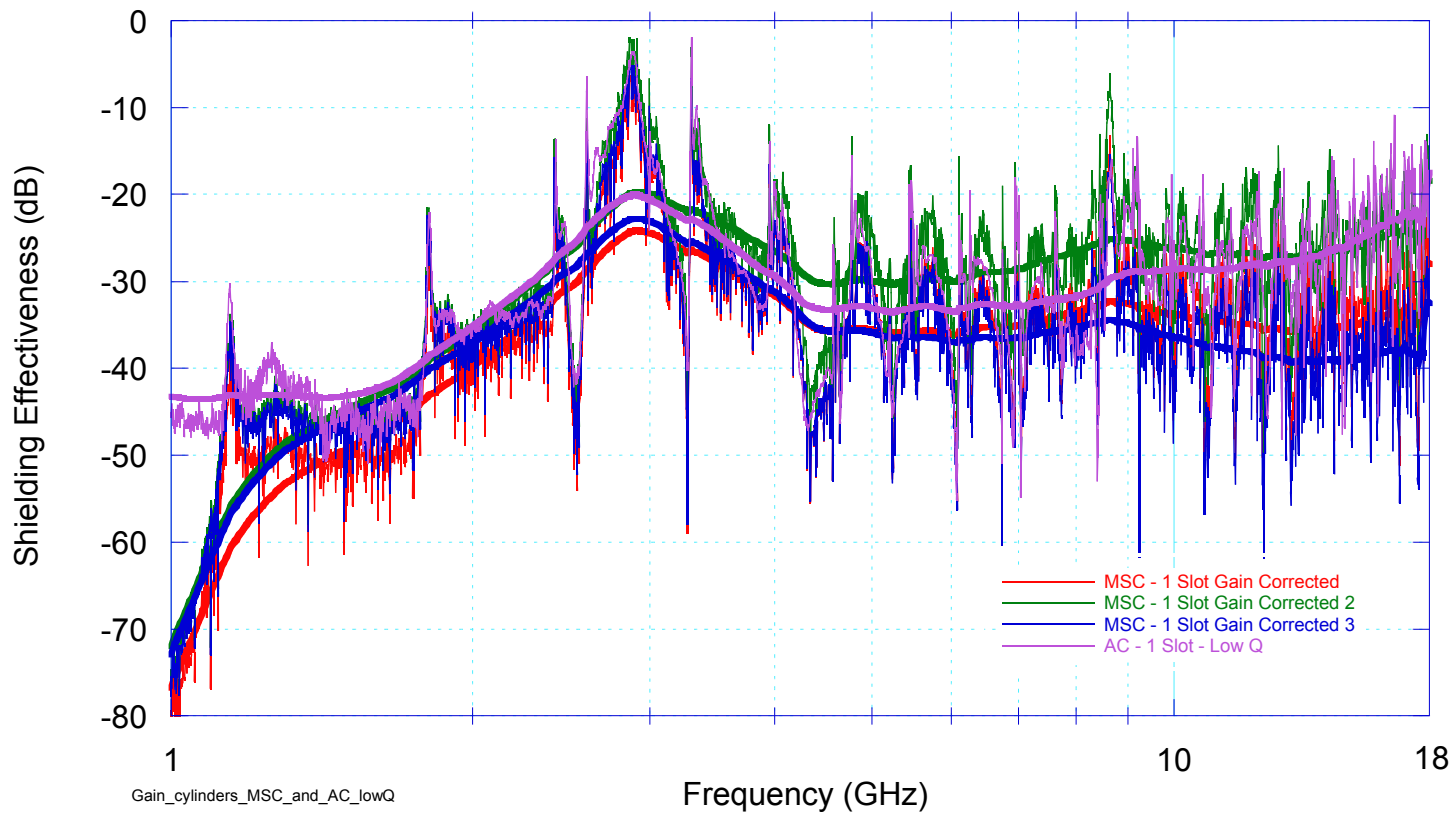
# Single Slot Cylinder – Low Q



# Single Slot Cylinder (Low Q) with Gain Correction



# Gain Corrected and Smoothed





# Conclusions

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- **High Q Cavities**
  - **Single slot**
    - **Good correlation on average was seen with gain correction at slot resonance and above with the Sandia equation and the equation from Ref #2.**
  - **2 slot**
    - **MSC data appears to not need gain correction below 7 GHz.**
    - **Above 9 GHz, Sandia equation and Ref #2 equation perform well.**
  - **8 slot**
    - **MSC data appears to not need gain correction.**
    - **Full pattern of test object needed in Anechoic chamber.**





## Conclusions (cont.)

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- **Low Q Cavities**

- **Single slot**

- **Good correlation on average was seen with gain correction below 3.5 GHz and above 10 GHz using the equation from Ref #1. Between 3.5 and 10 GHz the gain was over compensated by less than 5 dB.**
    - **Below 10 GHz Sandia equation and Ref #2 equation under compensated by 2 – 3 dB.**



# References

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1. Hill, D.A.; Camell, D.G.; Cavcey, K.H.; and Koepke, G.H., “Radiated emissions and immunity of microstrip transmission lines: theory and reverberation chamber measurements,” *IEEE Trans. Electromag. Compat.*, vol. 38, pp. 165-172, 1996.
2. Koepke, G.H.; Hill, D.A.; and Ladbury, J., “Directivity of the Test Device in EMC Measurements,” *IEEE International Symposium on Electromagnetic Compatibility*, vol. 2, pp. 535-539, Aug. 2000.