

Comparison of Shielding Effectiveness of High Q Canonical Cavities with Thin Slots in a Mode-Stirred and Anechoic Chamber

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Outline

- **Why is this important?**
- **Current Gain Correction Methods**
- **Measurement techniques**
- **Test Objects**
- **Results**
 - **1, 2, and 8 slot cylindrical, high Q cavity ($Q \approx 4000$)**
 - **1 slot cylindrical lower Q cavity ($Q \approx 800$)**
- **Conclusions**



Why is this important?

- A gain correction is needed to go from mode-stirred chamber shielding effectiveness data to free-space data
 - For transfer functions
 - For susceptibility testing



Gain Corrections

Gain correction for a single slot (from Warne, et. al at Sandia)

$$D \approx \frac{4\ell}{\lambda} \quad D_m \approx \begin{cases} 0, & D < 1 \\ D, & D \geq 1, \end{cases}$$

Gain correction for an intentional emitter [1]

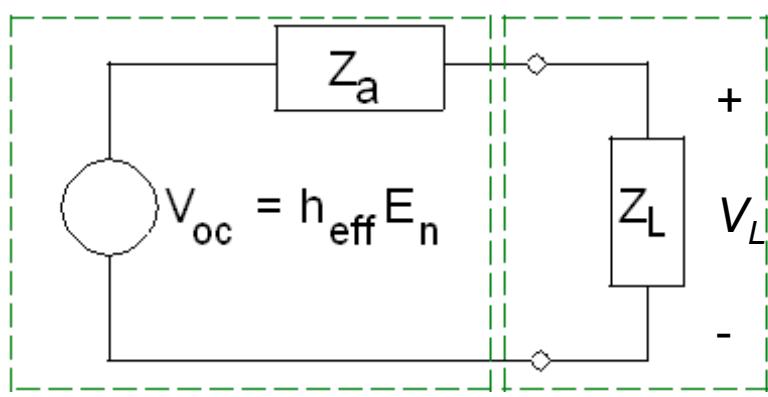
$$D_m \approx \begin{cases} 3, & ka \leq 1 \\ (ka)^2 + 2ka, & ka > 1, \end{cases}$$

Gain correction for an unintentional emitter for a planar cut [2]

$$D_m \approx \begin{cases} 2.45, & ka \leq 1 \\ 0.577 + \ln(2(2ka + 1)) + \frac{1}{4(2ka + 1)}, & ka > 1, \end{cases}$$

Calculating chamber and test object interior fields

Monopole Sensor



The load voltage, V_L , is measured. Use the following values to calculate the normal electric field picked up by the monopole.

$Z_L = 50 \Omega$ load

Z_a = monopole radiation impedance

V_{oc} = monopole open circuit voltage

h_{eff} = monopole effective height

E_n = **normal electric field**
(quantity of interest)

Calculation derivation

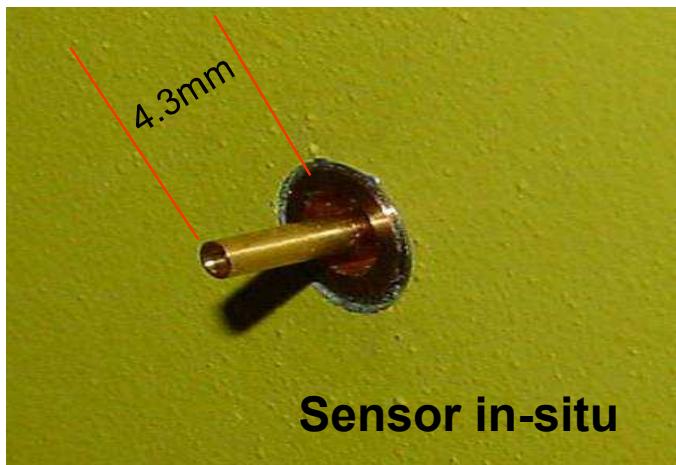
$$V_L = V_{oc} \frac{Z_L}{Z_a + Z_L} \quad \text{from circuit theory}$$

$$V_{oc} = \frac{V_L}{Z_L} (Z_a + Z_L) = h_{eff} E_n$$

$$E_n = \frac{V_L}{Z_L h_{eff}} (Z_a + Z_L)$$

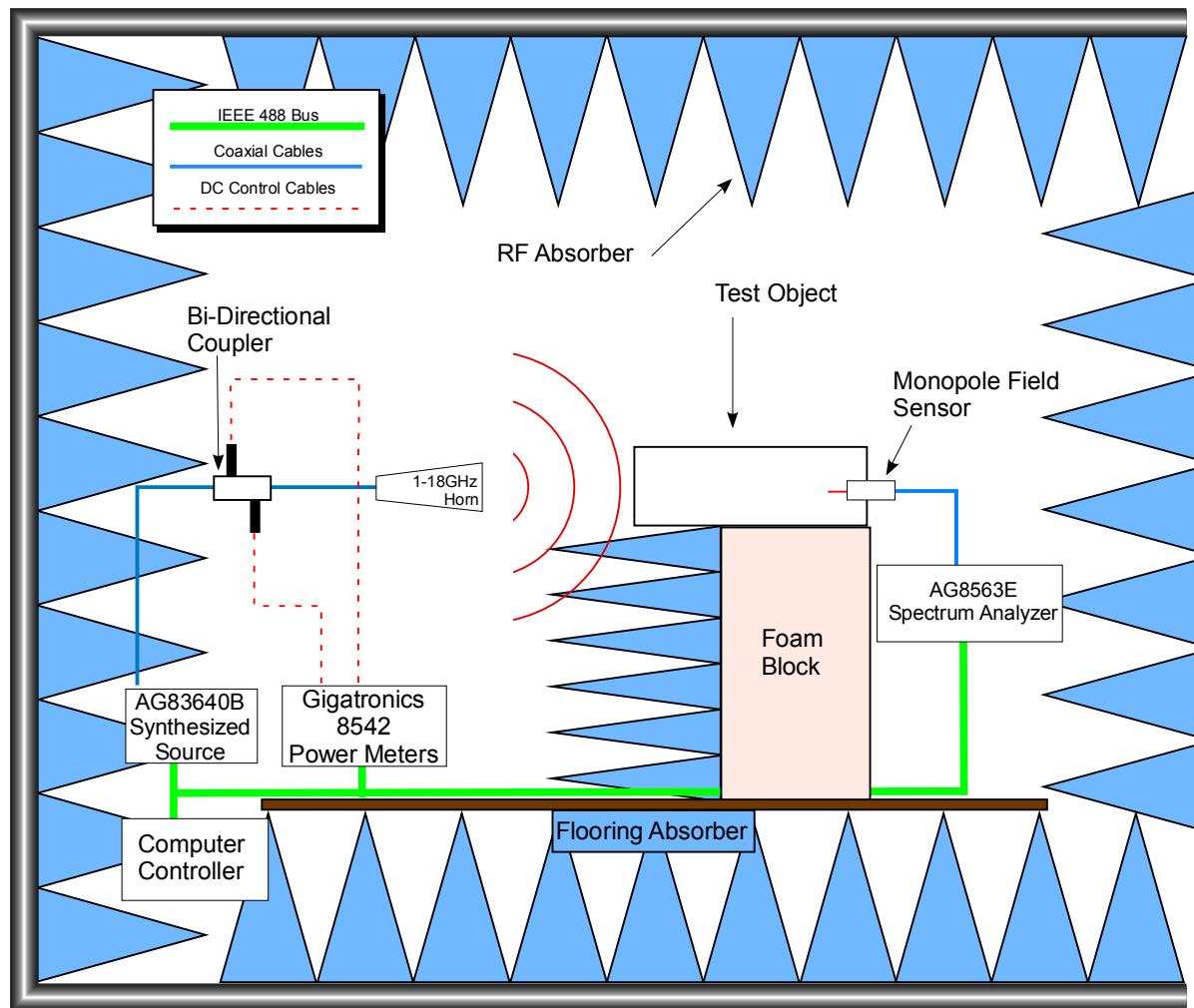


Monopole Sensors

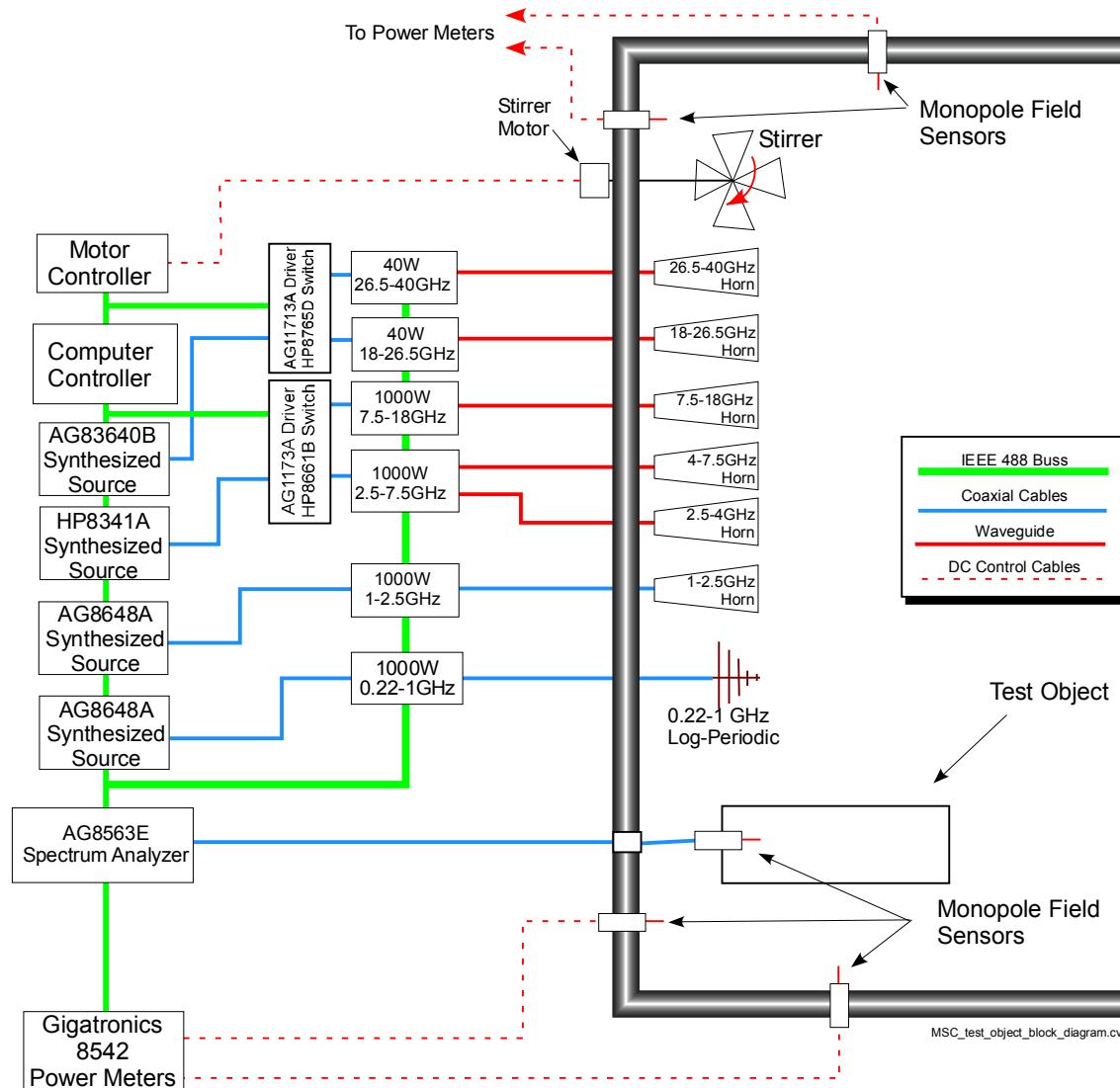


**220 MHz – 18 GHz
Monopole sensor**

Anechoic Chamber Diagram

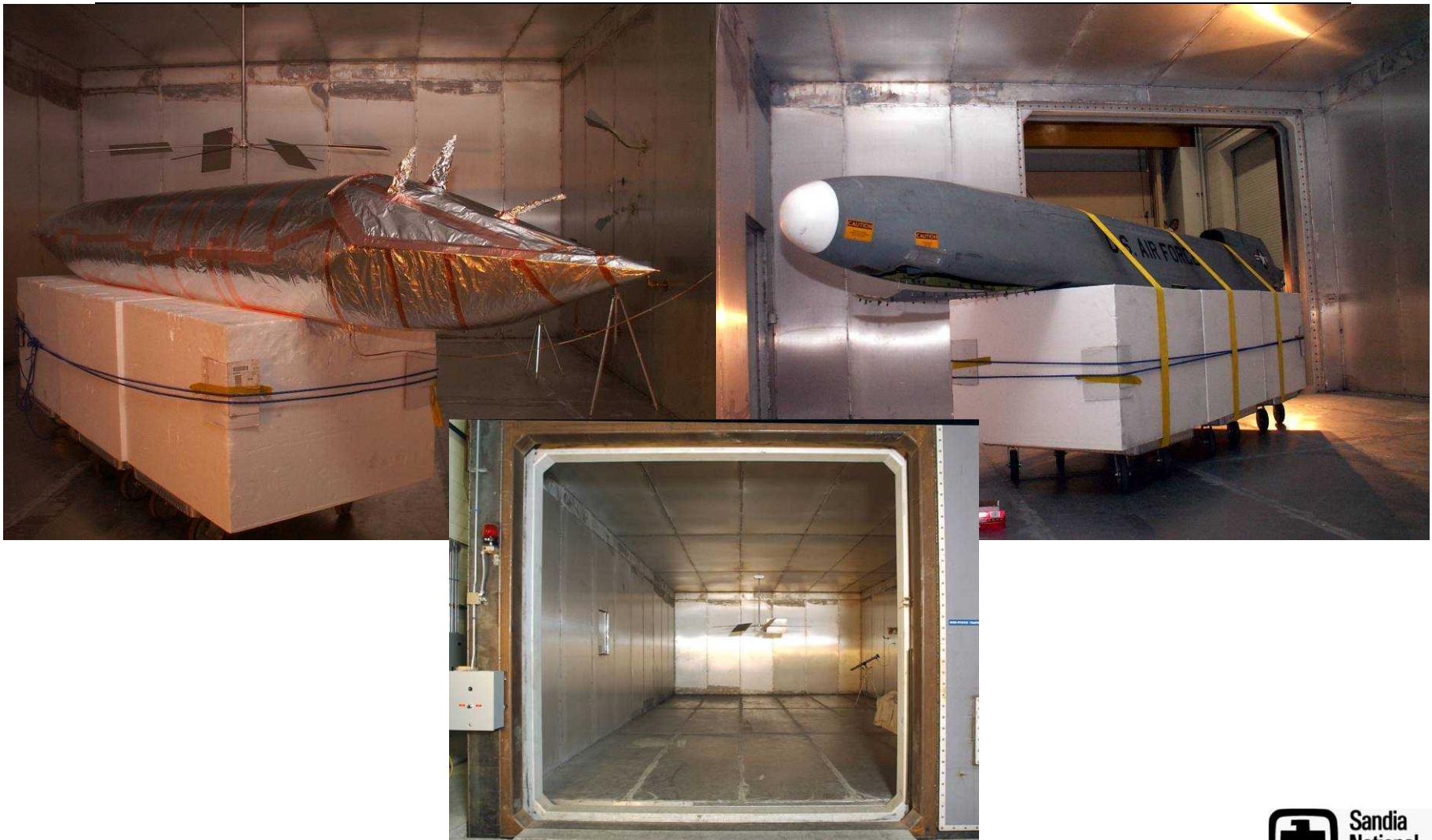


Mode-Stirred Chamber Diagram





Mode-Stirred Chamber (MSC)





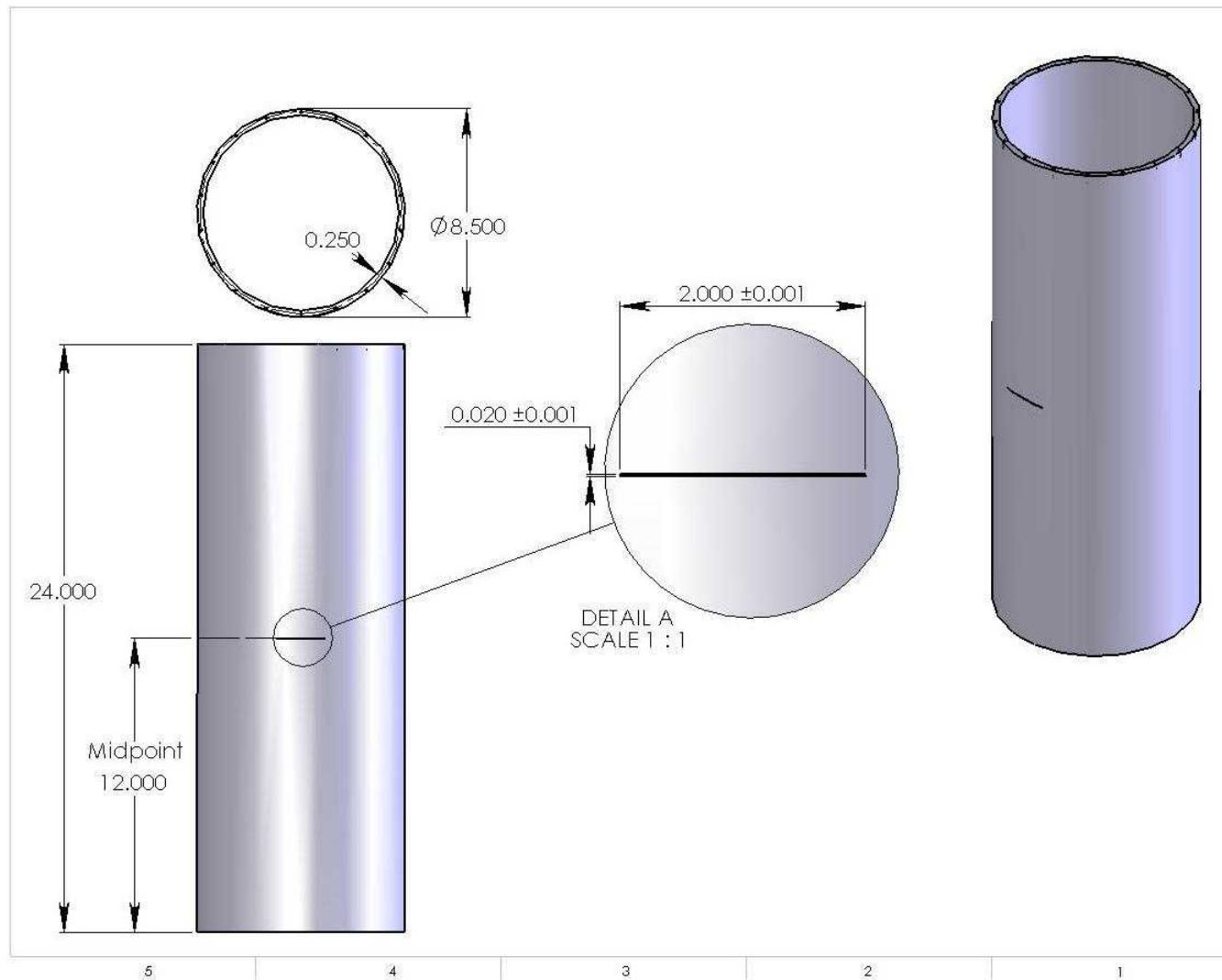
Mode-Stirred Chamber (MSC)

- **MSC provides statistically uniform incident electromagnetic field**
- **A superposition of plane waves**
- **Bathes test object in electromagnetic field, which ensures leaks are found**
- **Cables do not need to be in a specific orientation**

Performance Characteristics of Mode-Stirred Chamber Test Facility

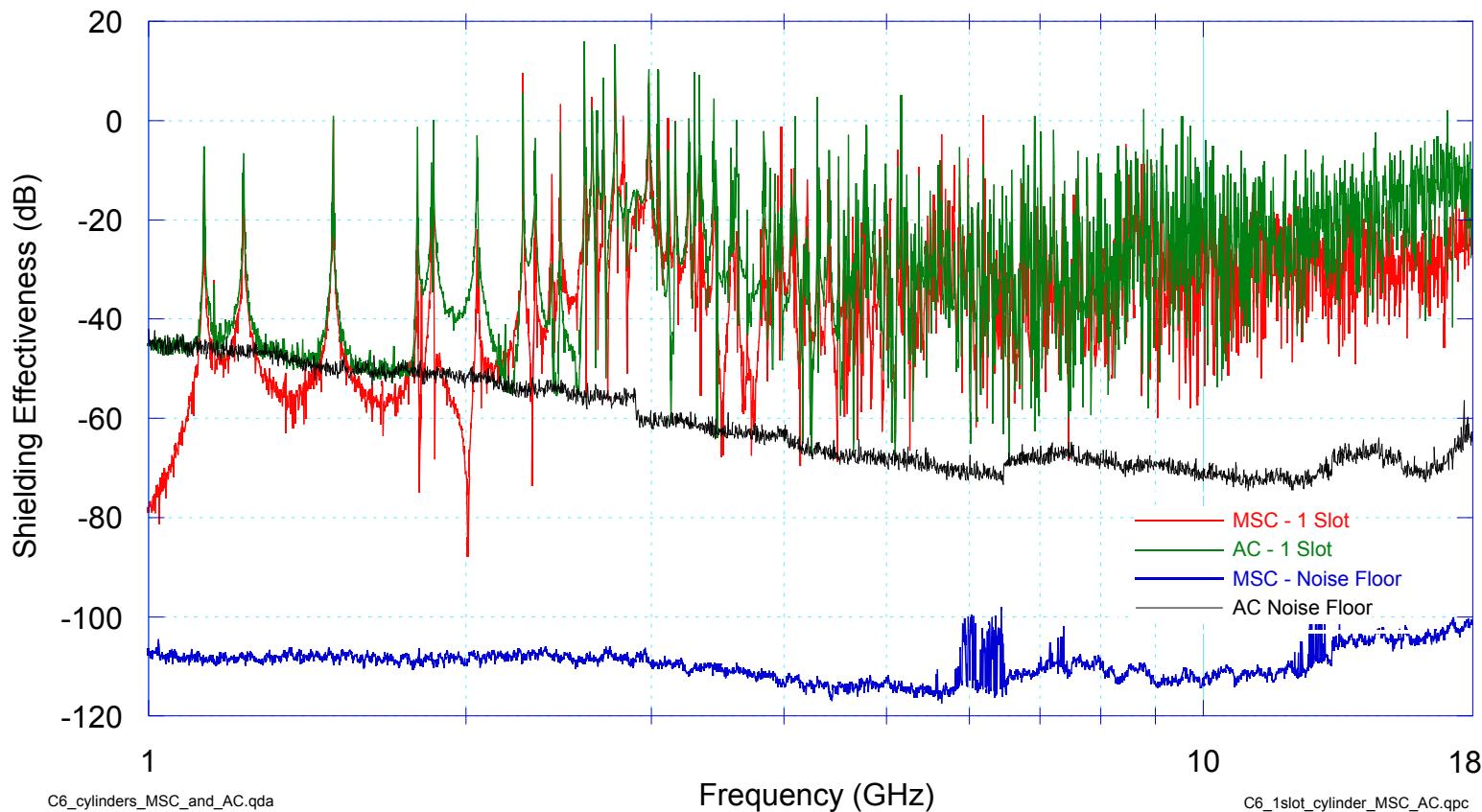
Dimension	4 x 7 x 11 m (HxWxL)
Design	Welded Aluminum
Entrance Dimensions	3.7 x 3.7 m
Frequency	0.22 – 40 GHz
Input Power	Solid State and TWT amplifiers
	1000 W, 220 MHz – 18 GHz
	40 W, 18 GHz – 40 GHz
Field Strength	~3000 V/m peak, 220 MHz – 18 GHz
	~600 V/m peak, 18 – 40 GHz

Cylindrical Test Object



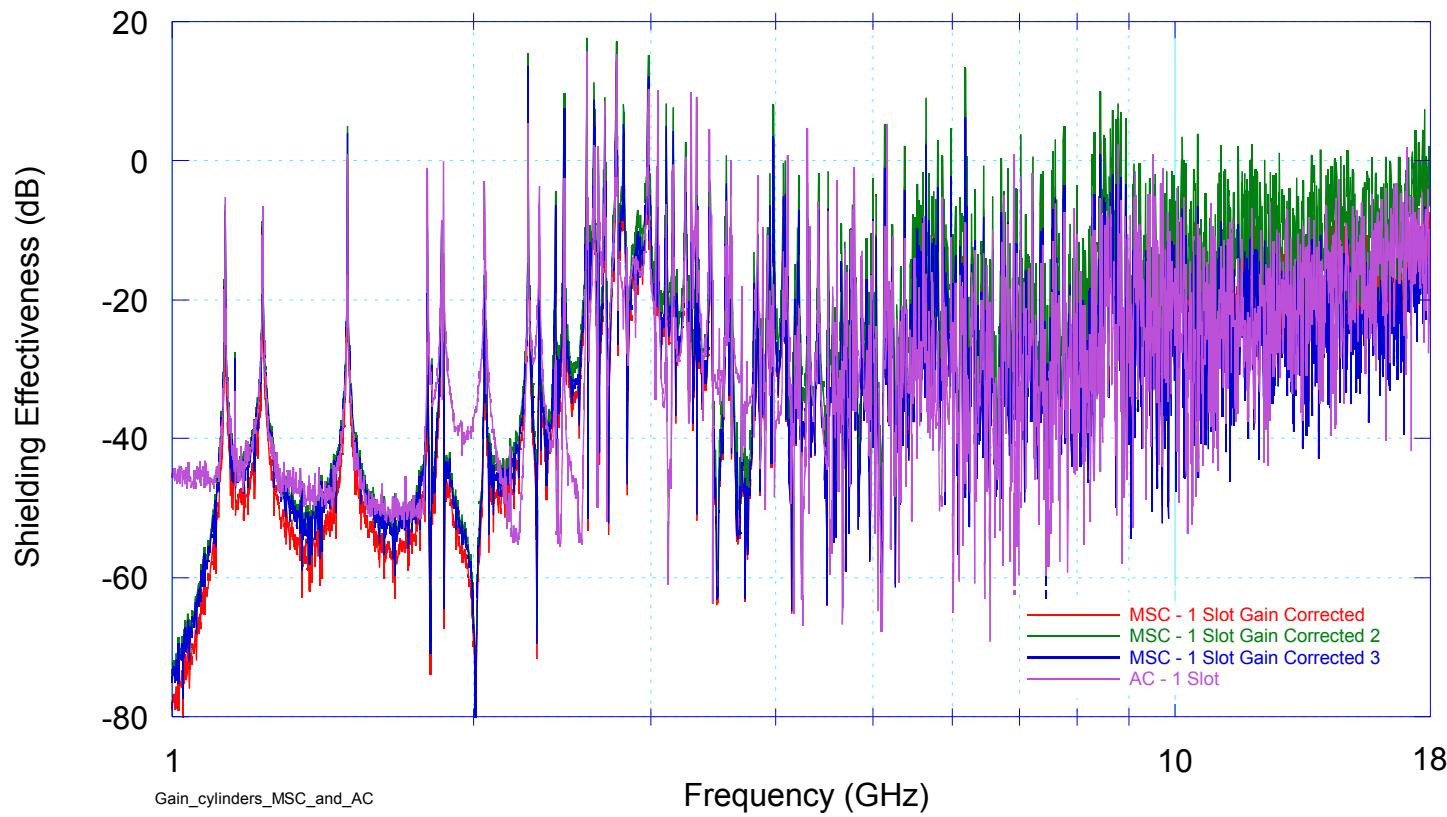


Single Slot Cylinder



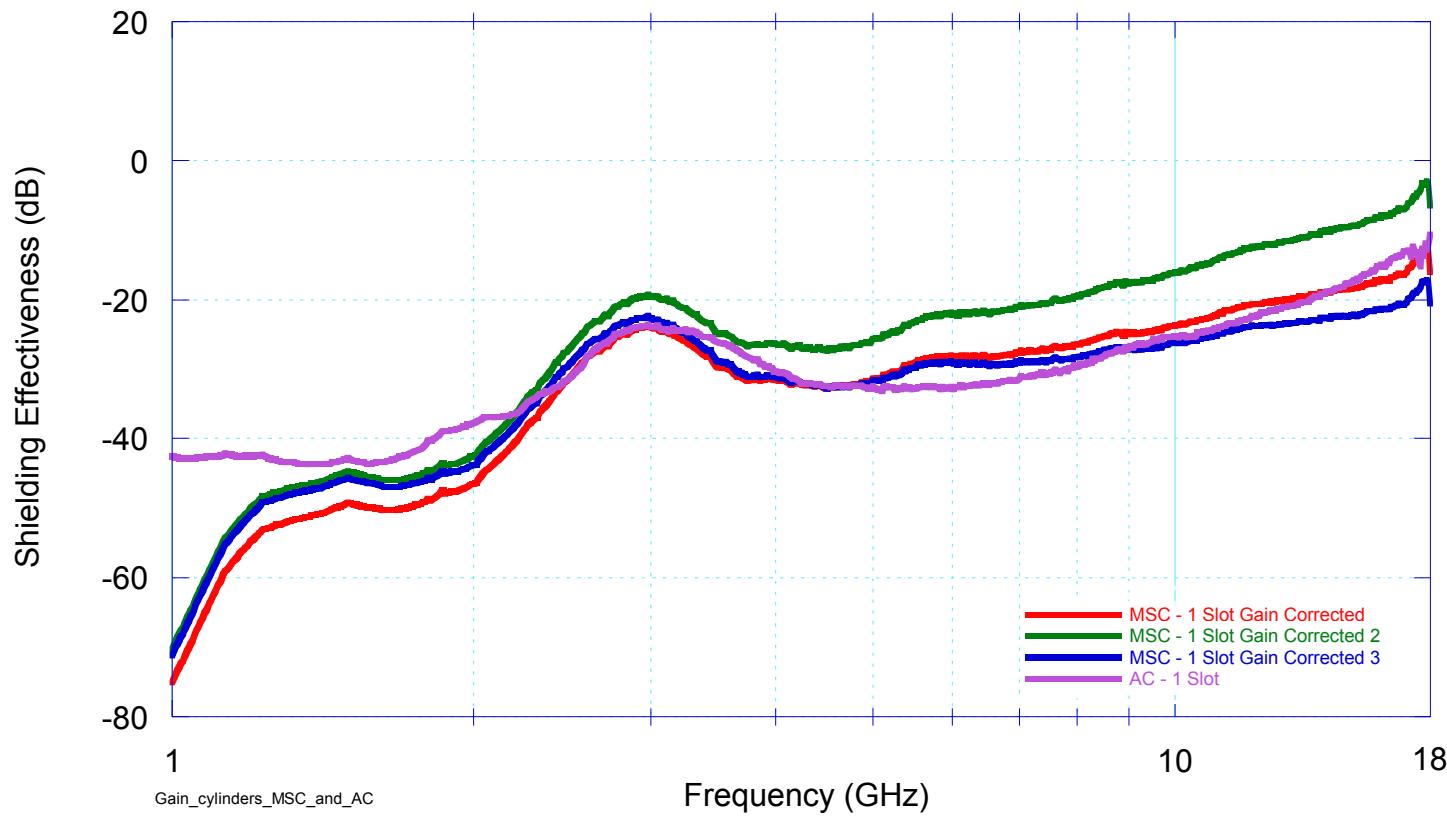


Single Slot Cylinder with Gain Correction

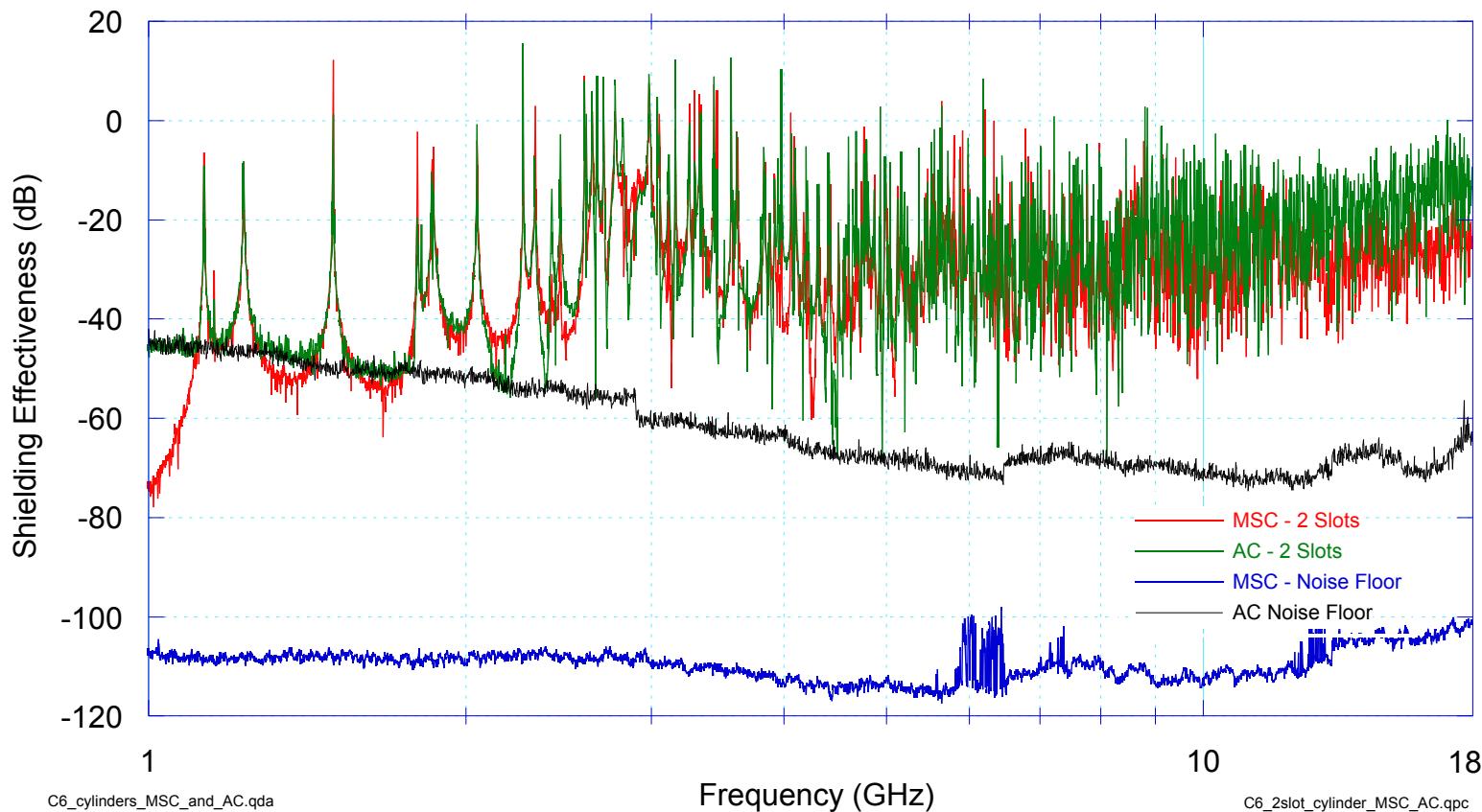




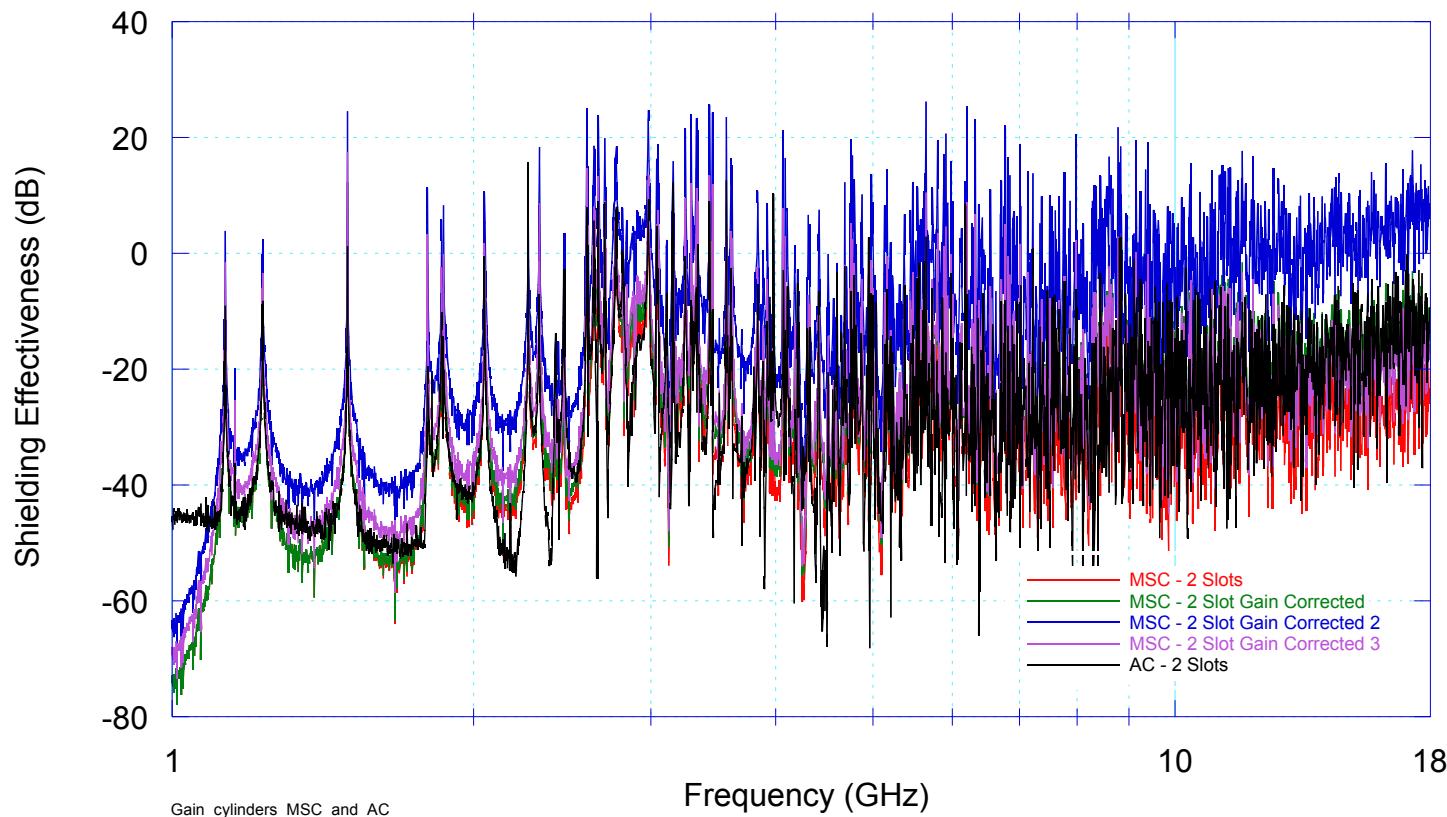
Gain Corrected and Smoothed

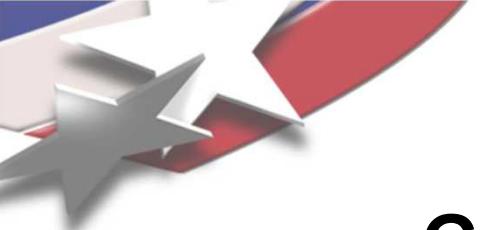


Two Slot Cylinder

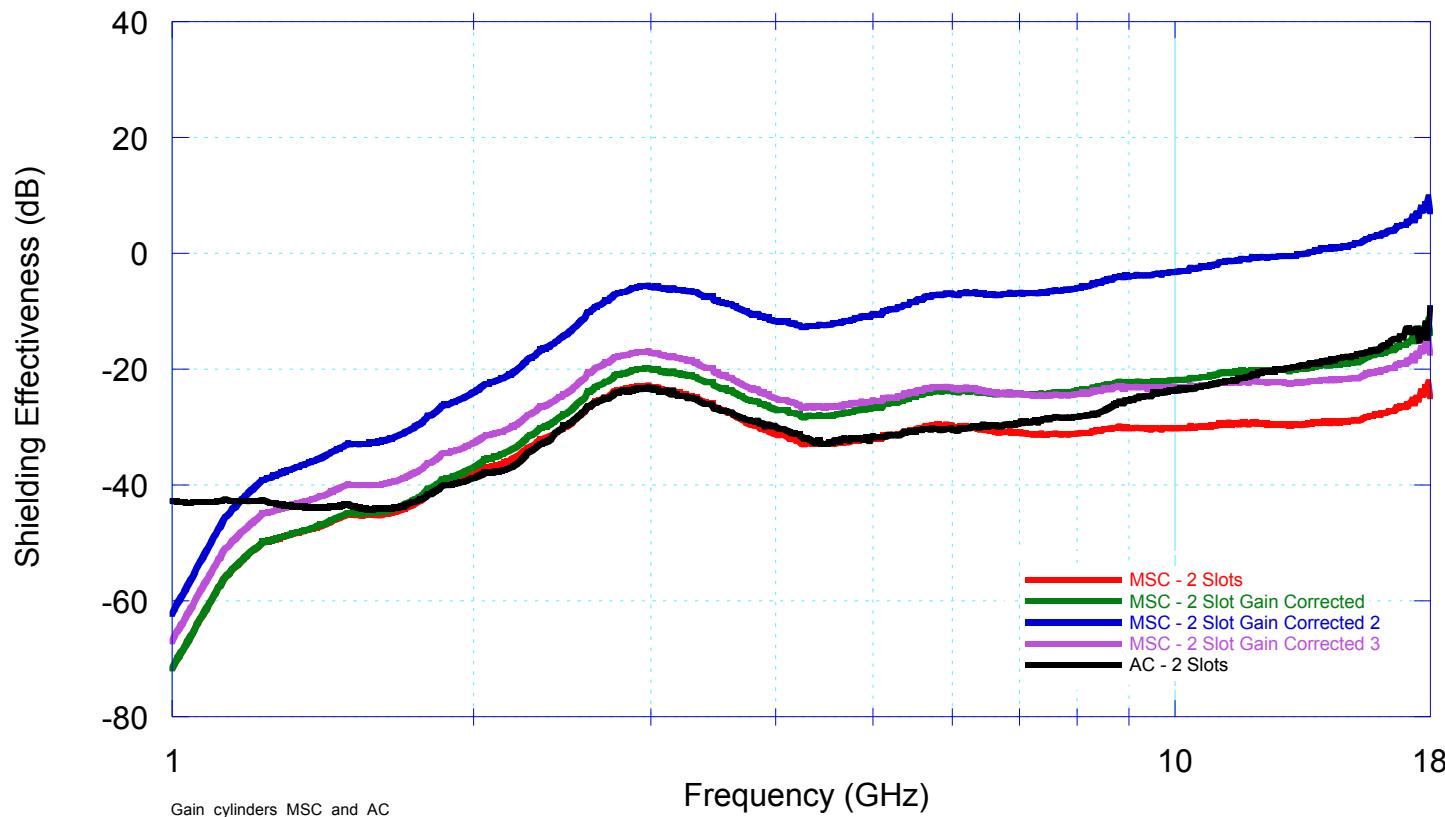


Two Slot Cylinder with Gain Correction



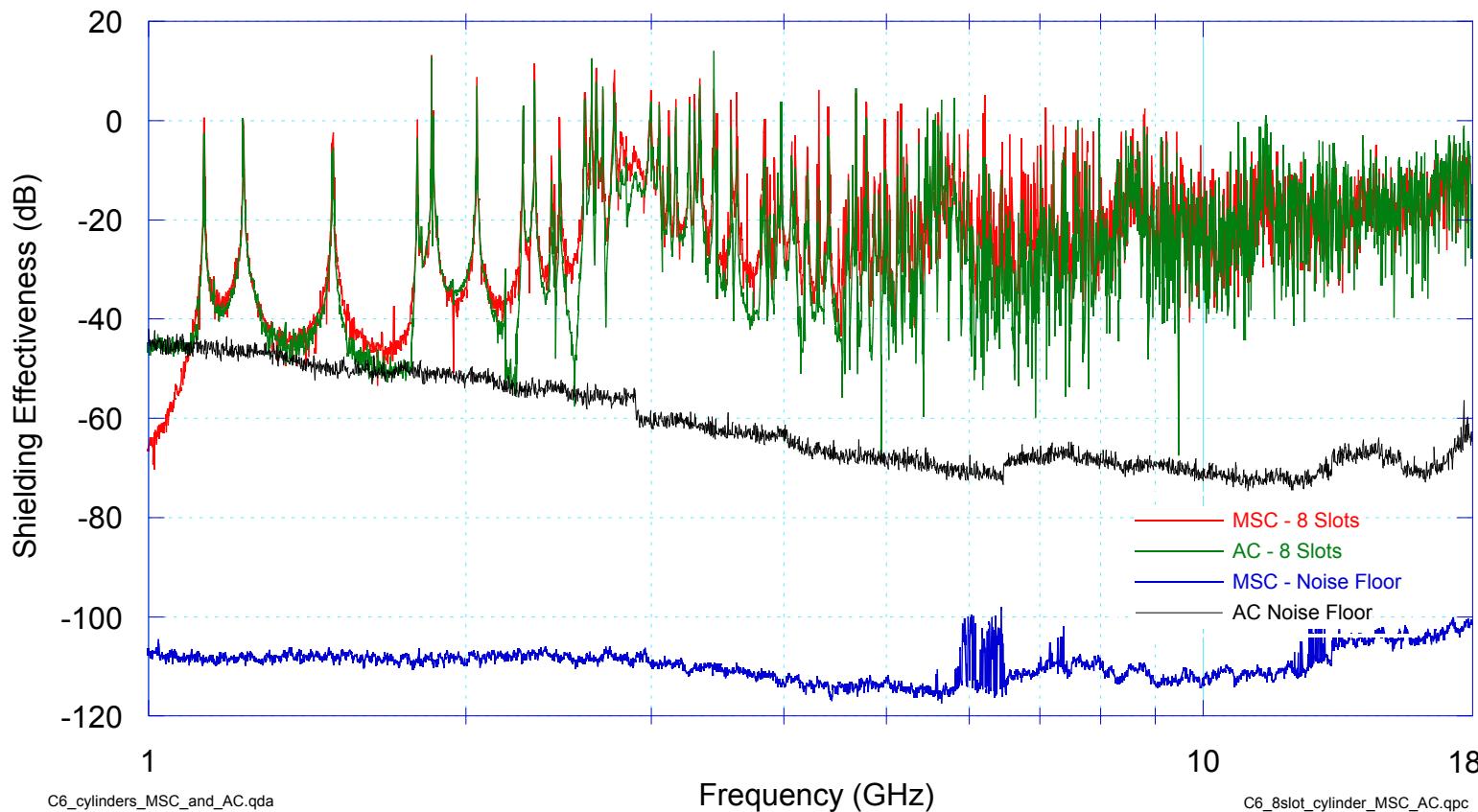


Gain Corrected and Smoothed





Eight Slot Cylinder

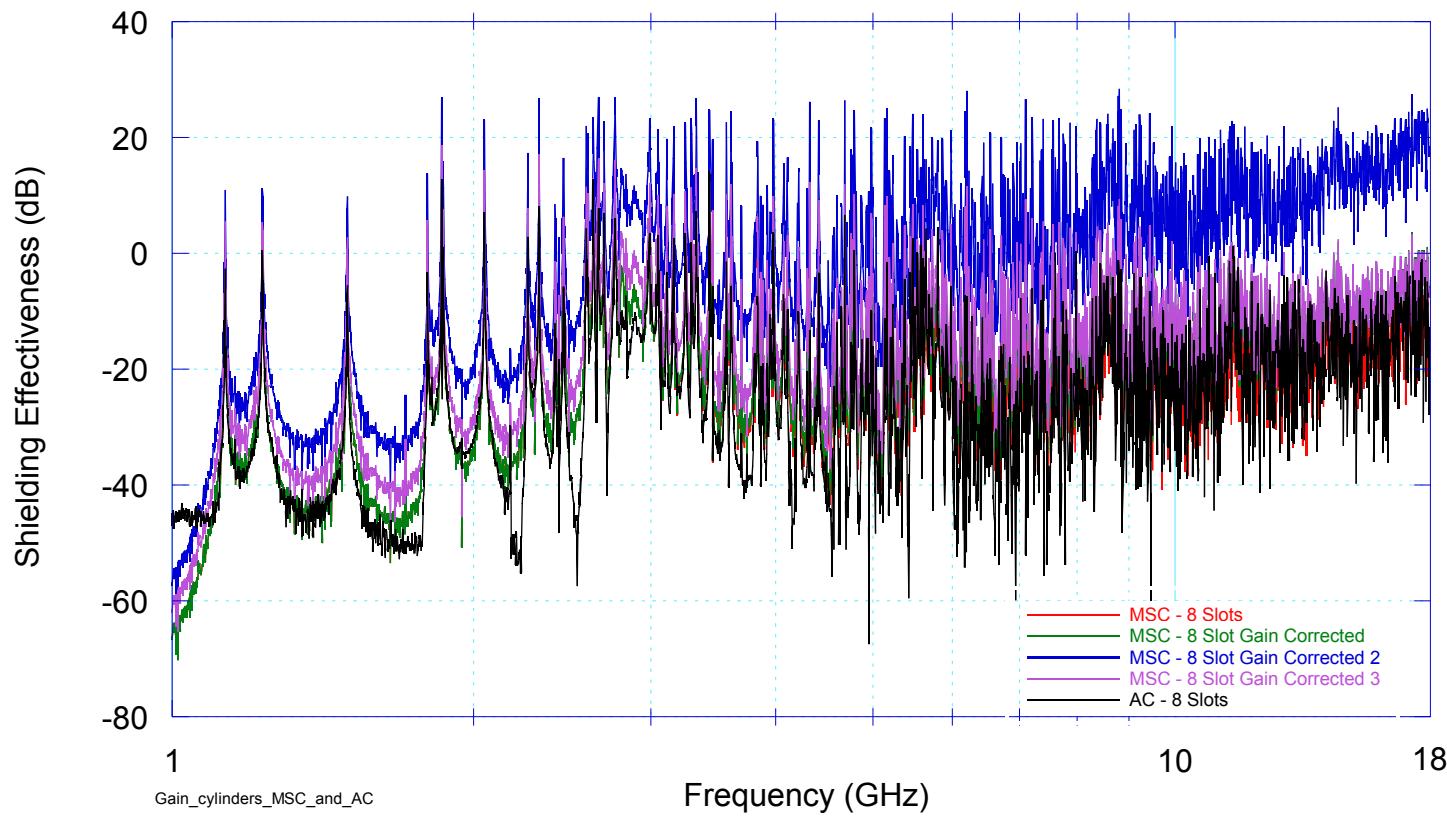


C6_cylinders_MSC_and_AC.qda

C6_8slot_cylinder_MSC_AC.qpc

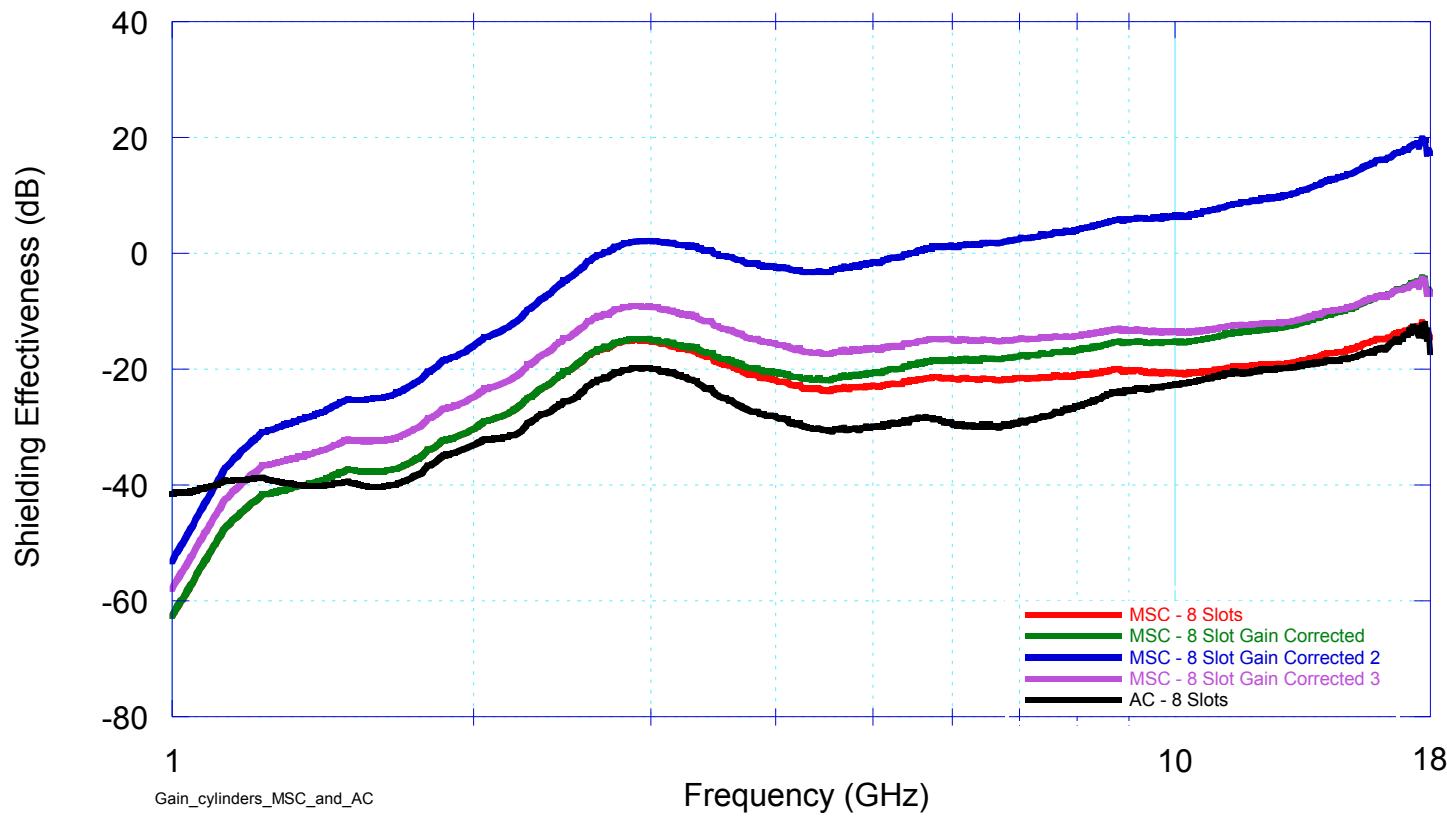


Eight Slot Cylinder with Gain Correction



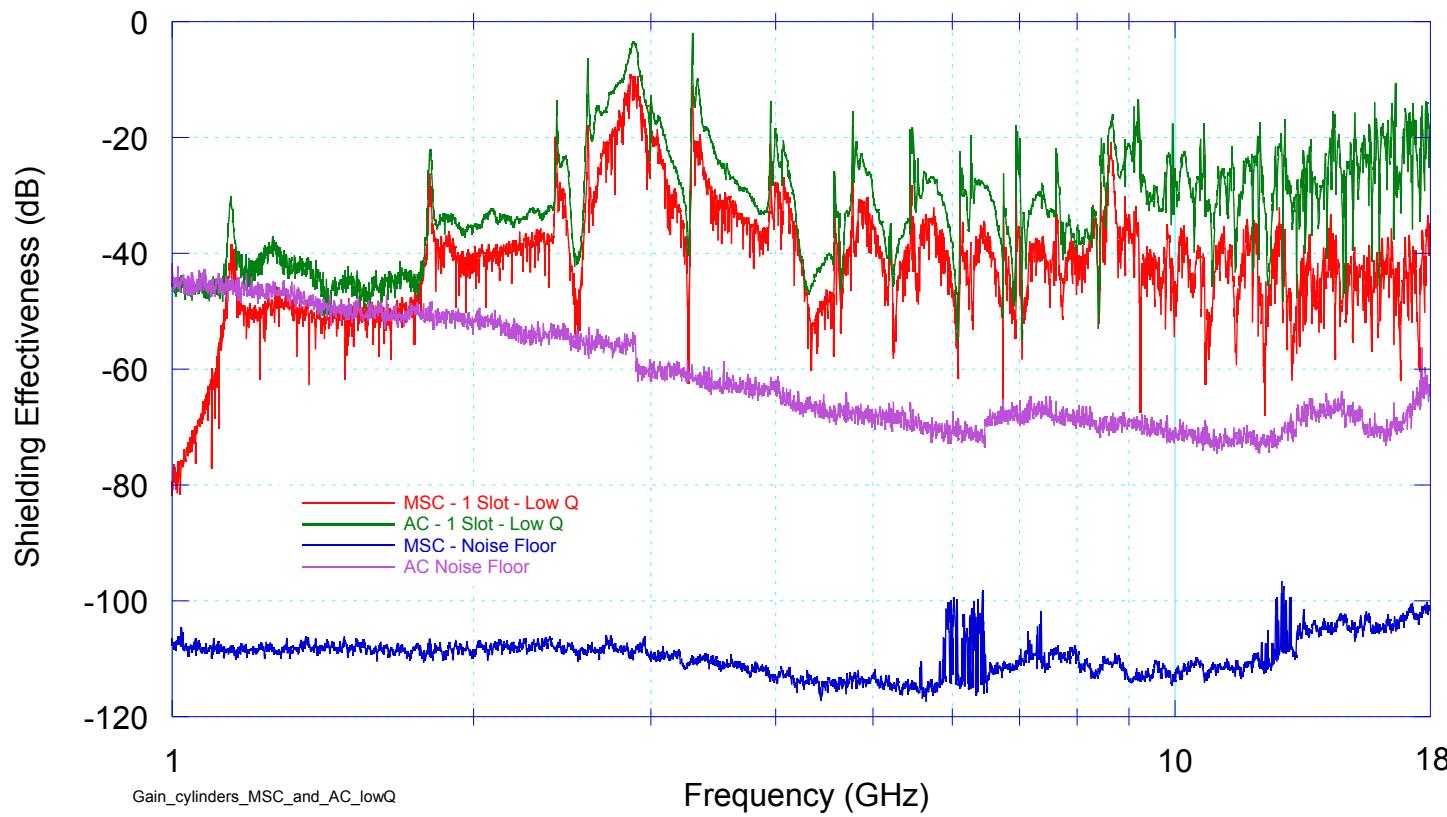


Gain Corrected and Smoothed



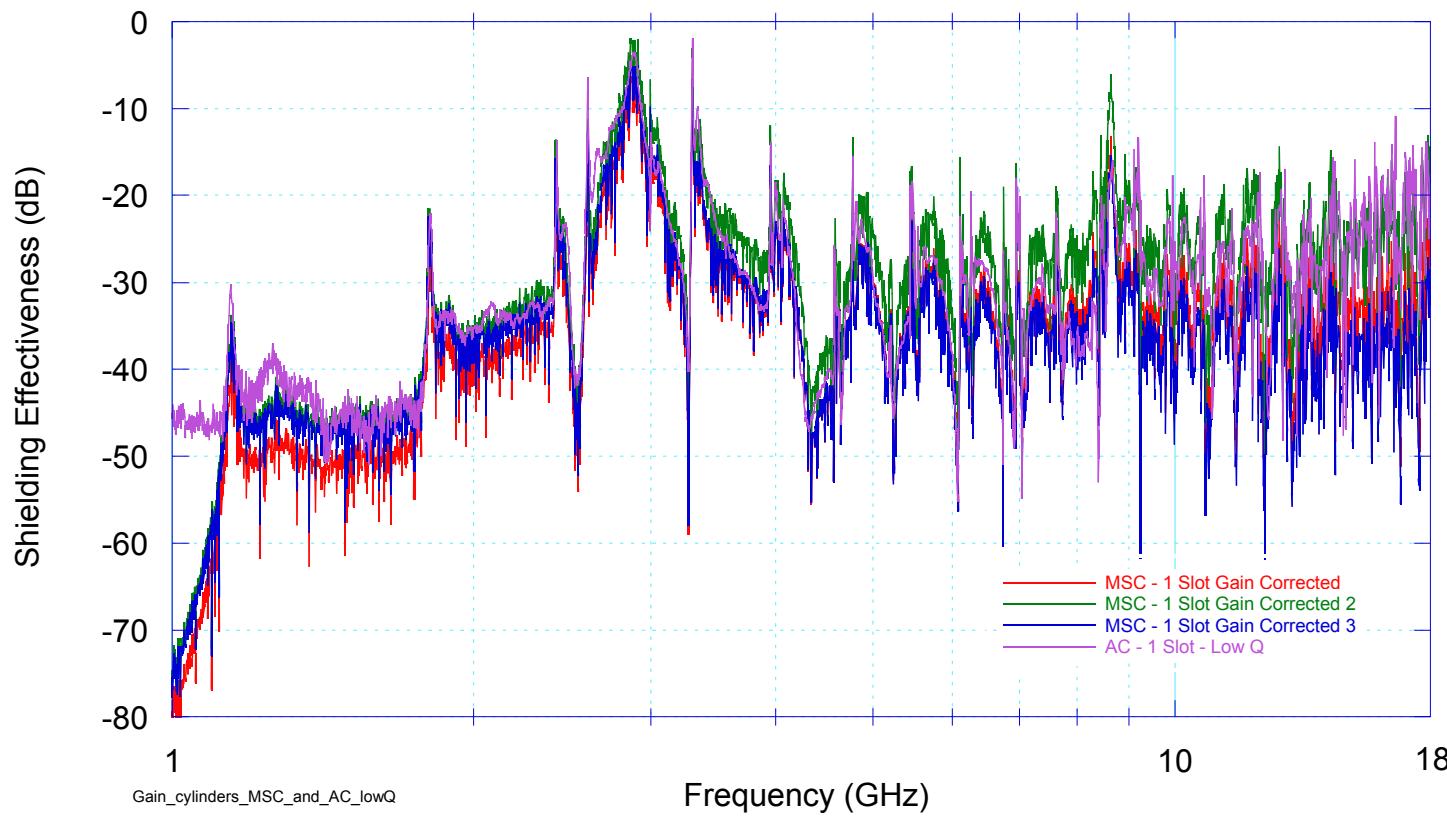


Single Slot Cylinder – Low Q



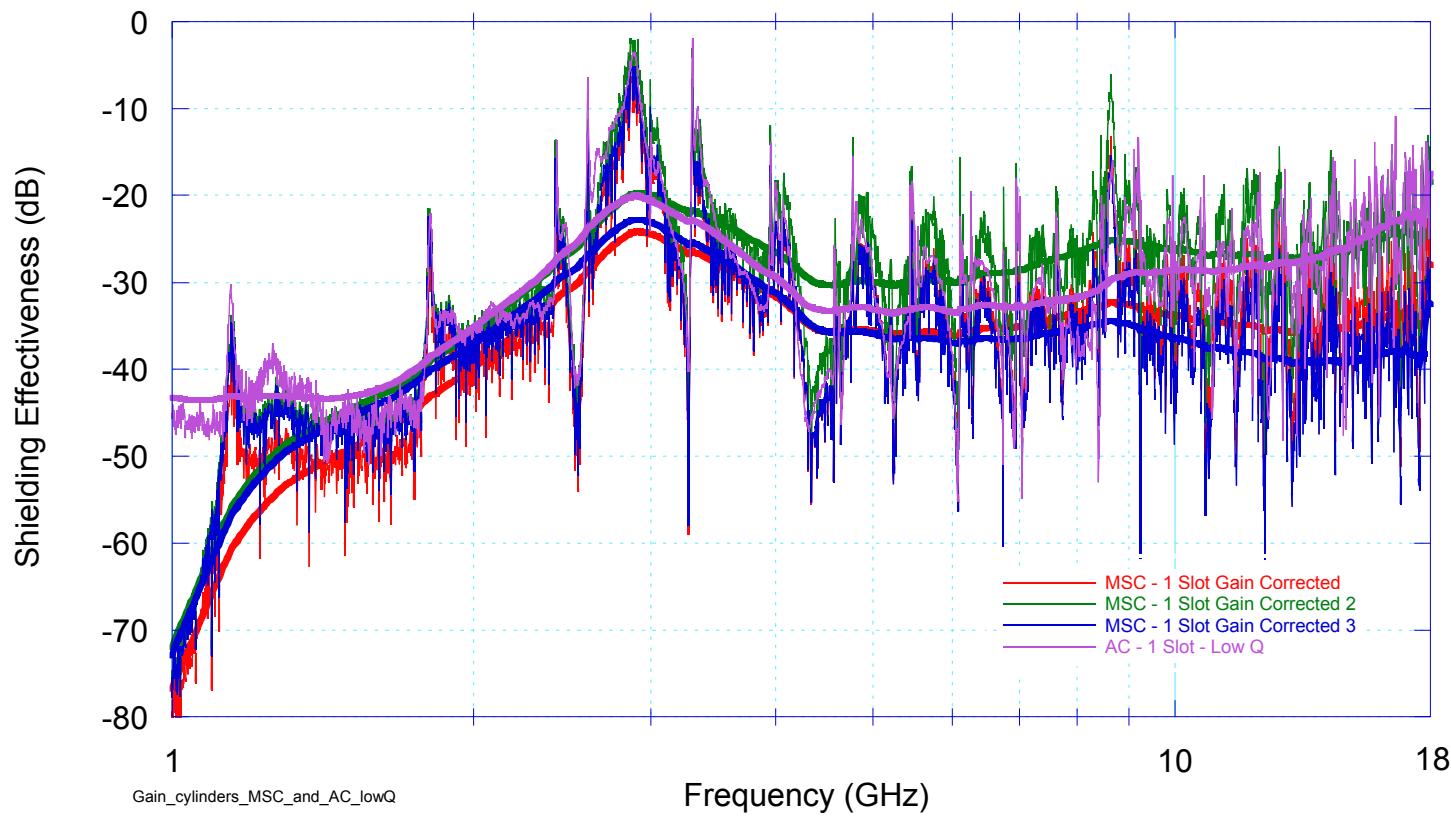


Single Slot Cylinder (Low Q) with Gain Correction





Gain Corrected and Smoothed





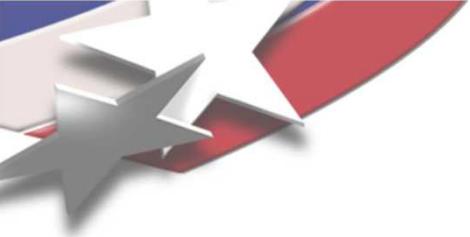
Conclusions

- **High Q Cavities**
 - **Single slot**
 - Good correlation on average was seen with gain correction at slot resonance and above with the Sandia equation and the equation from Ref #2.
 - **2 slot**
 - MSC data appears to not need gain correction below 7 GHz.
 - Above 9 GHz, Sandia equation and Ref #2 equation perform well.
 - **8 slot**
 - MSC data appears to not need gain correction.
 - Full pattern of test object needed in Anechoic chamber.



Conclusions (cont.)

- **Low Q Cavities**
 - **Single slot**
 - Good correlation on average was seen with gain correction below 3.5 GHz and above 10 GHz using the equation from Ref #1. Between 3.5 and 10 GHz the gain was over compensated by less than 5 dB.
 - Below 10 GHz Sandia equation and Ref #2 equation under compensated by 2 – 3 dB.



References

1. Hill, D.A.; Camell, D.G.; Cavcye, K.H.; and Koepke, G.H., “Radiated emissions and immunity of microstrip transmission lines: theory and reverberation chamber measurements,” *IEEE Trans. Electromag. Compat.*, vol. 38, pp. 165-172, 1996.
2. Koepke, G.H.; Hill, D.A.; and Ladbury, J., “Directivity of the Test Device in EMC Measurements,” *IEEE International Symposium on Electromagnetic Compatibility*, vol. 2, pp. 535-539, Aug. 2000.