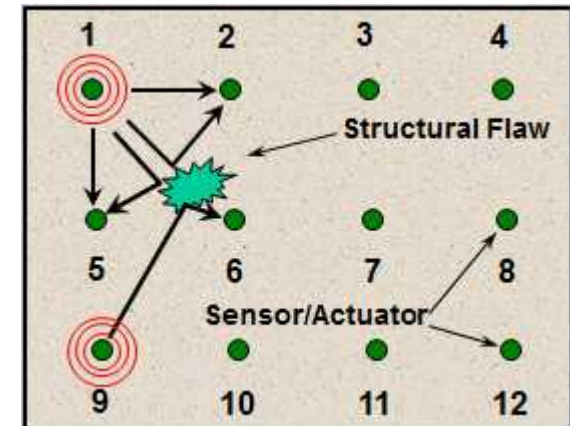
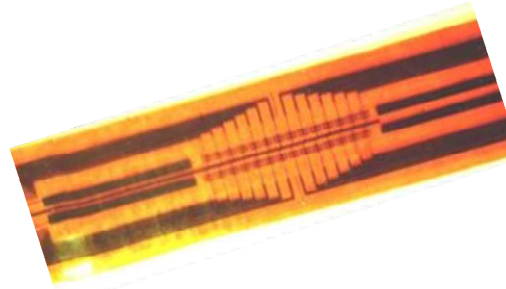


Calculating Probability of Detection for SHM Systems Using One-Sided Tolerance Intervals – Applications & Limitations

SAND2015-3998PE



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Senior Scientist
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Sandia is a multiprogram laboratory operated by Sandia Corporation, a Lockheed Martin Company, for the United States Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000.



Structural Health Monitoring – Integration into Routine Maintenance



Sandia
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STRUCTURAL
MONITORING
SYSTEMS

Toby Chandler, Mike Reveley
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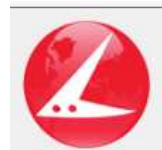
Bernie Adamache,
Joe Zee



John Mitchell, Hin Tsang,
Maurizio Molinari, Marc Lord



Mark Davis, Andrew Brookhart,
Preston Bates, Ray Beale



Acellent

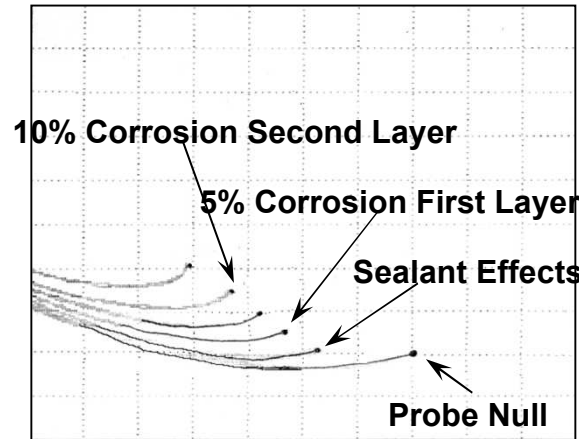
Amrita Kumar, Fu-Kuo Chang,
Howard Chung, Franklin Li



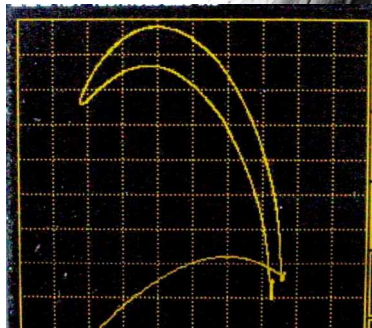
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Typical A-Scan Signals Used for Flaw Detection with Hand-Held Devices

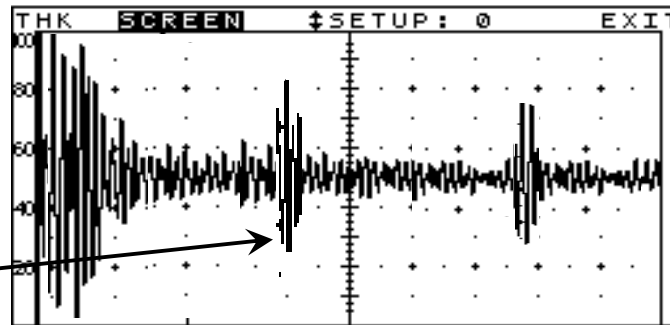


**Corrosion Detection
with Dual Frequency
Eddy Current**



**Eddy Current
Signal at
Crack Site**

Intermediate Echo
Caused by
Delamination



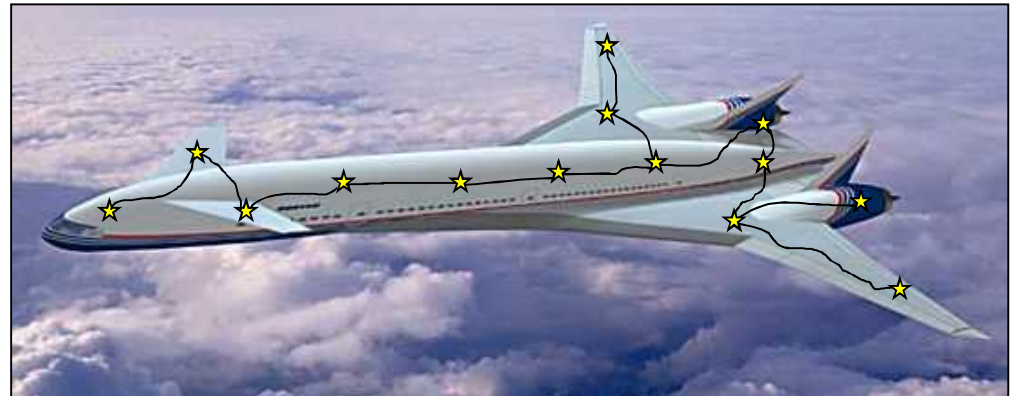
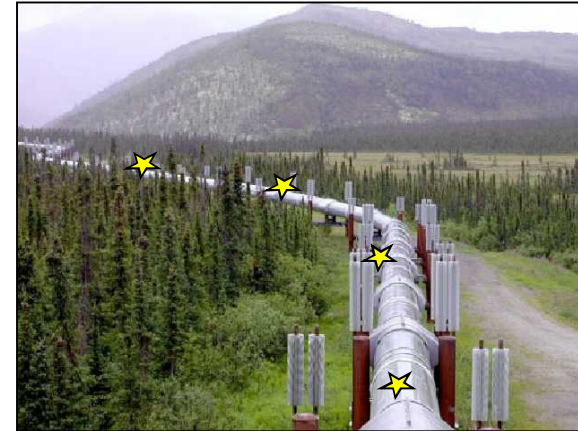
**Ultrasonic Pitch-Catch UT Signals Comparing
Flawed and Unflawed Signatures**



Distributed Sensor Networks for Structural Health Monitoring

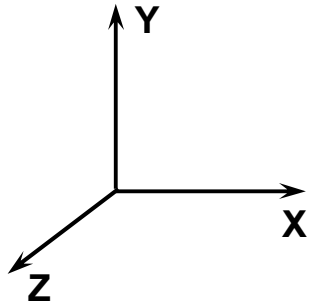
Smart Structures: include in-situ distributed sensors for real-time health monitoring; ensure integrity with minimal need for human intervention

- Remotely monitored sensors allow for condition-based maintenance
- Automatically process data, assess structural condition, & signal need for maintenance actions
- SHM for:
 - Flaw detection
 - Flaw location
 - Flaw characterization
 - Condition Based Maintenance

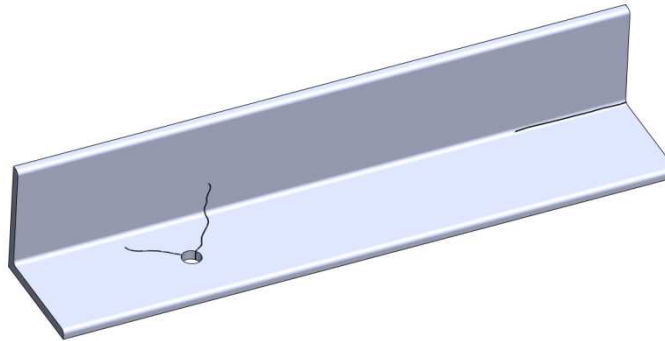


Reliability Assessment for Simple and Complex SHM Solutions

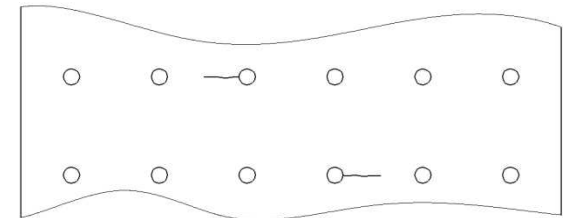
Complex Flaw Orientation



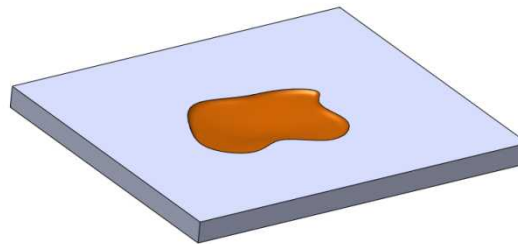
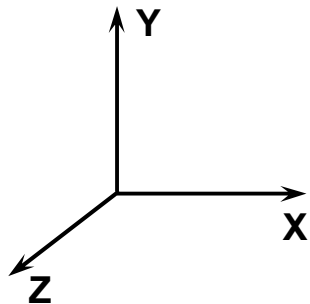
A. Crack with multiple growth paths in complex geometry



B. Crack with single, known crack direction in simple geometry



Complex Flaw Profile

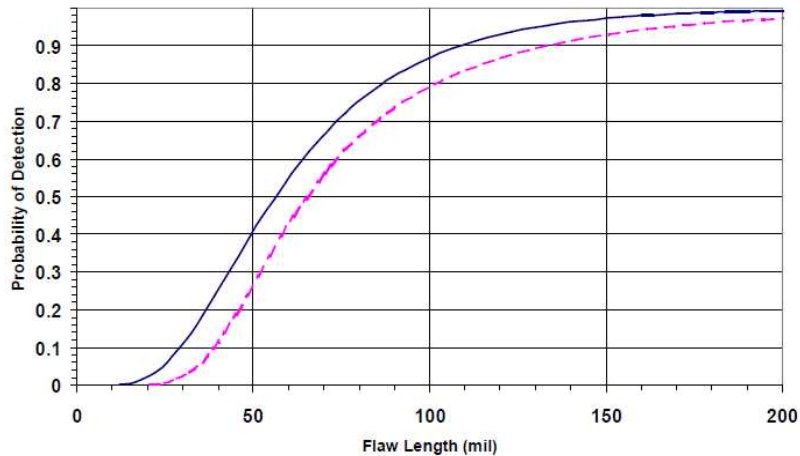


Example: corrosion size, shape and depth variations

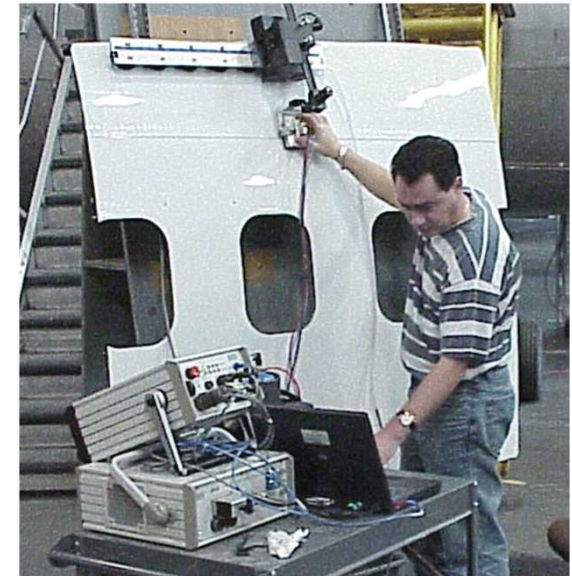
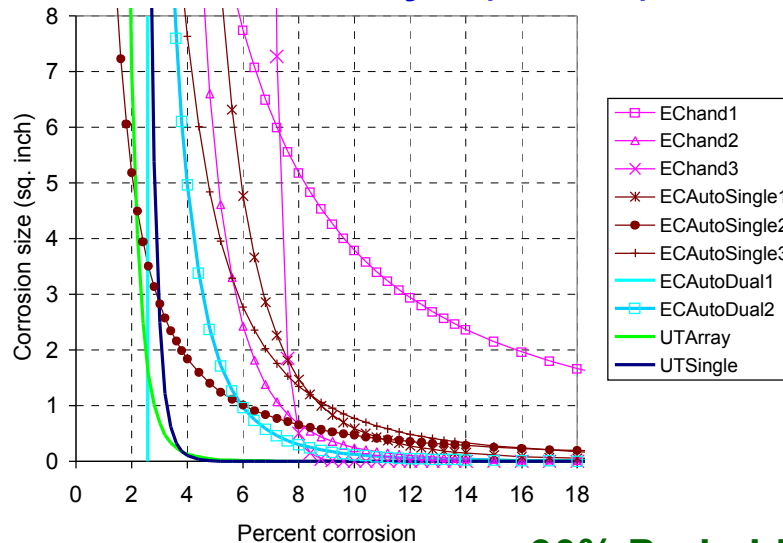
**Analysis for one-dimensional entity
simplifies significantly**

Presenting NDI POD Values for Different Flaw Geometries

Lap Splice Fatigue Cracks



Interlayer (Hidden) Corrosion



**90% Probability of Flaw
Detection Contours**



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POD Assessment Using One-Sided Tolerance Interval

- Interval to cover a specified proportion of a population distributed with a given confidence – related to measures of process capability
- One-Sided Tolerance Interval – estimates the upper bound which should contain a certain percentage of all measurements in the population with specified confidence
- Since it is based on a sample of the entire population (n data points), confidence is less than 100%. Thus, it includes two proportions:
 - Degree of confidence (95%)
 - Percent coverage (90%)
- The reliability analysis becomes one of characterizing the distribution of flaw lengths and the cumulative distribution function is analogous to a Probability of Detection (POD) curve.

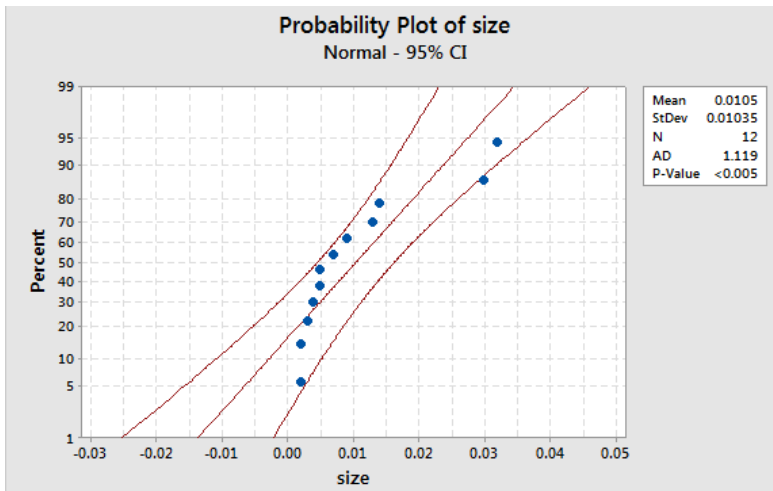
$$TI = \bar{X} \pm (K_{n,Y,\alpha})(S) \quad [\log \text{ scale calculation}]$$

- Interested in a 1-tailed interval (utilize “+” in equation); upper limit of TI;
Uncertainty in knowing the true mean and population variance requires that the estimate of the range of values encompassing a given percentage of the population must increase to compensate

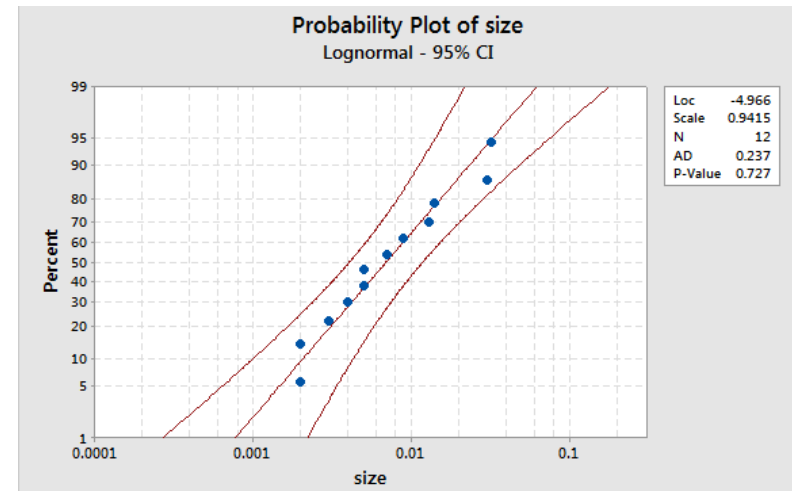


POD Assessment Using One-Sided Tolerance Interval

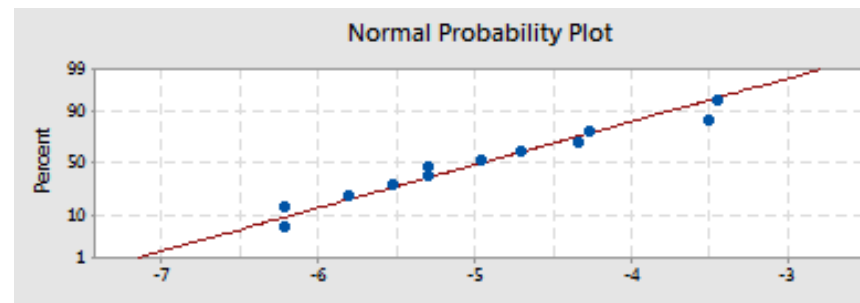
- Assume that the distribution of flaws is such that the logarithm of the lengths (strictly positive sizes) has a Gaussian distribution (log-normal distribution)
- Validity depends on distribution on the flaw lengths at which detection is first made – lognormal distribution plots on straight line with data clustered near 50th percentile
- Anderson-Darling test requires P-value > 0.05



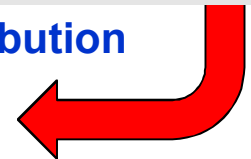
Normal Distribution



Lognormal Distribution

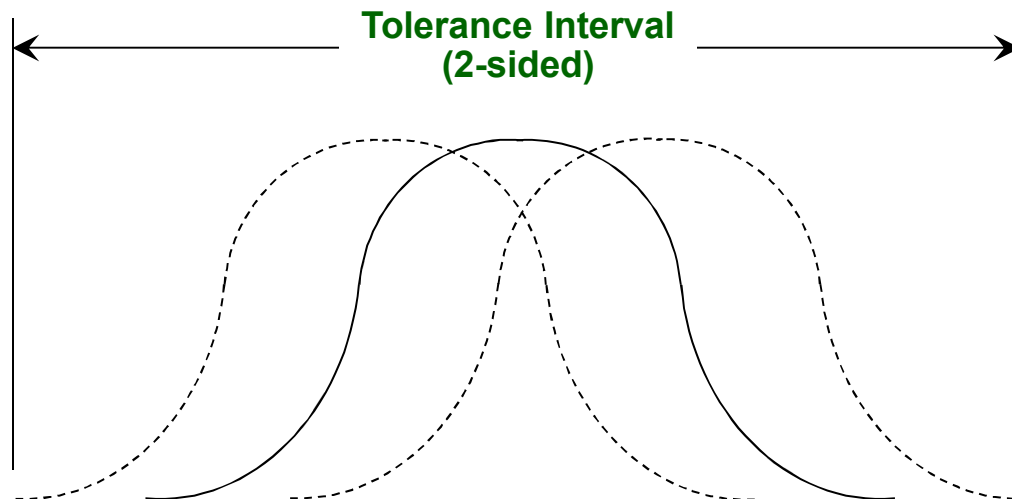


Normal plot of log values of data



POD Assessment Using One-Sided Tolerance Interval

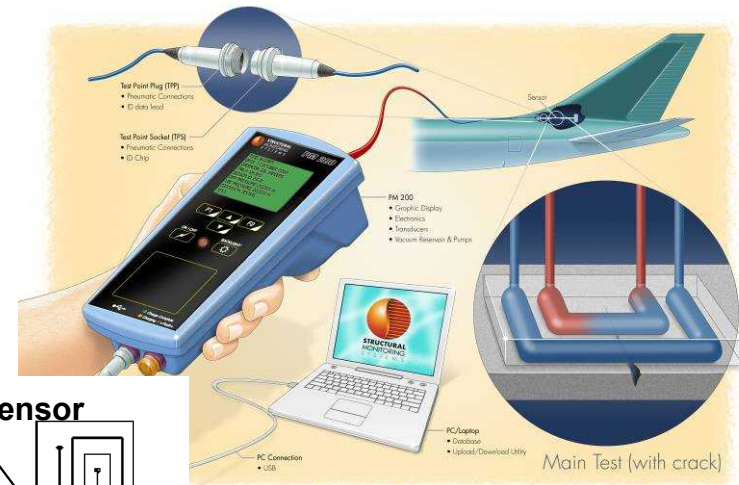
- Used to indicate values at which certain compliance is met
- Capability of the process is determined not only by the location of the sample mean but also by the tail areas of the distribution
- EPA recommends at least 8 points to calculate TI (vs. 51 flaws in a binary data POD) – gage entire population from a small sampling



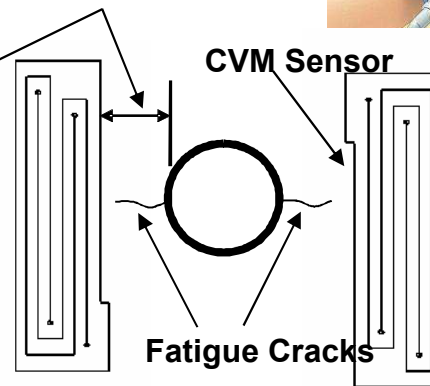
Solid Line = Population Distribution
Dotted Line = Uncertainty of Population Mean

Drivers for Application of CVM Technology

- Overcome accessibility problems; sensors ducted to convenient access point
- Improve crack detection (easier & more often)
- Real-time information or more frequent, remote interrogation
- Initial focus – monitor known fatigue prone areas
- Long term possibilities – distributed systems; remotely monitored sensors allow for condition-based maintenance



Minimize distance from rivet head to produce smallest crack detection

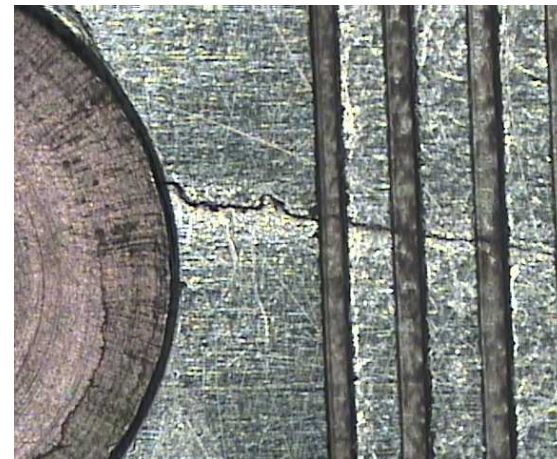
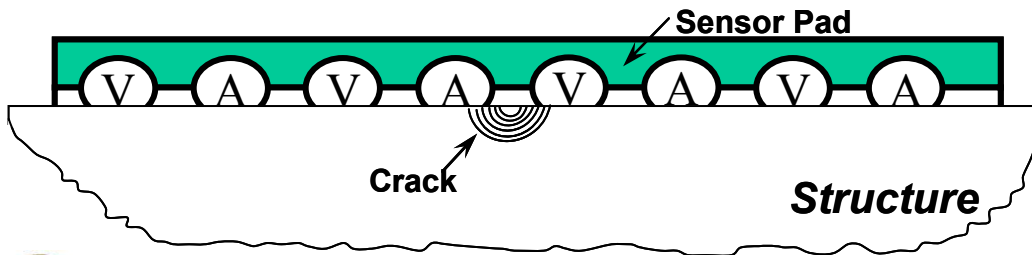
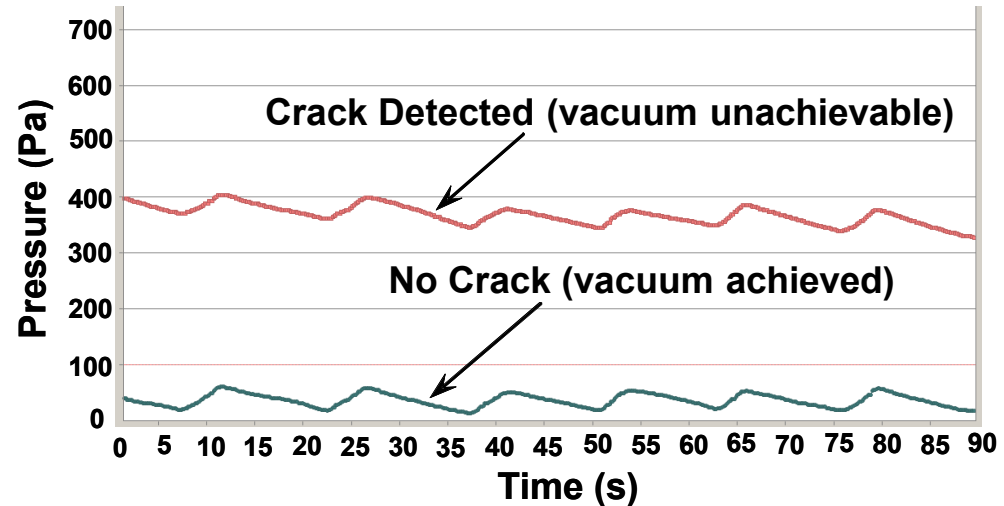


Comparative Vacuum Monitoring System

- Sensors contain fine channels - vacuum is applied to embedded galleries (**crack detection ~ 0.1" to 0.5" L for thick steel**)
- Leakage path produces a measurable change in the vacuum level
- Doesn't require electrical excitation or couplant/contact



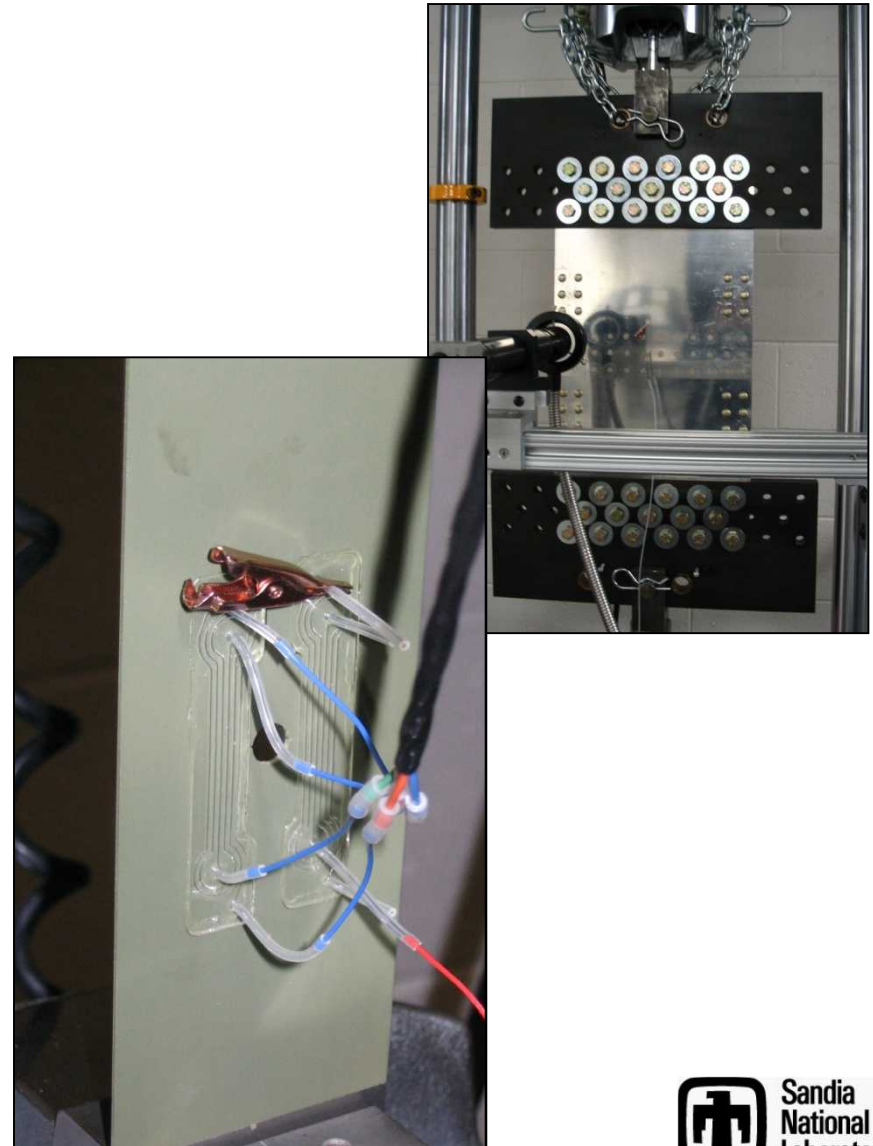
CVM Sensor Adjacent to Crack Initiation Site



Test Matrix to Quantify Probability of Crack Detection

Test Scenarios:

<u>Material</u>	<u>Thickness</u>	<u>Coating</u>
2024-T3	0.040"	bare
2024-T3	0.040"	primer
2024-T3	0.071"	primer
2024-T3	0.100"	bare
2024-T3	0.100"	primer
7075-T6	0.040"	primer
7075-T6	0.071"	primer
7075-T6	0.100"	primer



CVM Validation – Data Analysis Using One-Sided Tolerance Intervals

- Crack detection based on PM-200 “Green Light” – “Red Light” results
- Data captured is the crack length at the time when CVM provided permanent (unloaded) detection
- Reliability analysis – cumulative distribution function provides maximum likelihood estimation (POD)
- One-sided tolerance bound for various flaw sizes:

$$\text{POD}_{95\% \text{ Confidence}} = \bar{X} + (K_{n, 0.95, \alpha}) (S)$$

\bar{X} = Mean of detection lengths

K = Probability factor (\sim sample size, confidence level)

S = Standard deviation of detection lengths

n = Sample size

α = Detection level

γ = Confidence level



POD Calculations - One-Sided Tolerance Interval

POD Determined from CVM Response Data

CVM Crack Detection Data (0.040" th)

Bare Metal		Over Primer	
Flaw size (inch)	Log (flaw size)	Flaw size (inch)	Log (flaw size)
0.003	-2.52	0.002	-2.70
0.007	-2.15	0.007	-2.15
0.002	-2.70	0.010	-2.00
0.030	-1.52	0.009	-2.05
0.009	-2.05	0.004	-2.40
0.005	-2.30	0.006	-2.22
0.004	-2.40	0.010	-2.00
0.002	-2.70	0.009	-2.05
0.014	-1.85	0.011	-1.96
0.005	-2.30	0.007	-2.15
0.013	-1.89		
0.032	-1.49		

Statistic Estimates on Log Scale

Statistic	Over Bare metal	Over Primer
Mean	-2.1566	-2.1679
Std deviation	0.40889	0.22809

POD Detection Levels

($\gamma = 95\%$, $n = 12$ for bare, $n=10$ for primer)

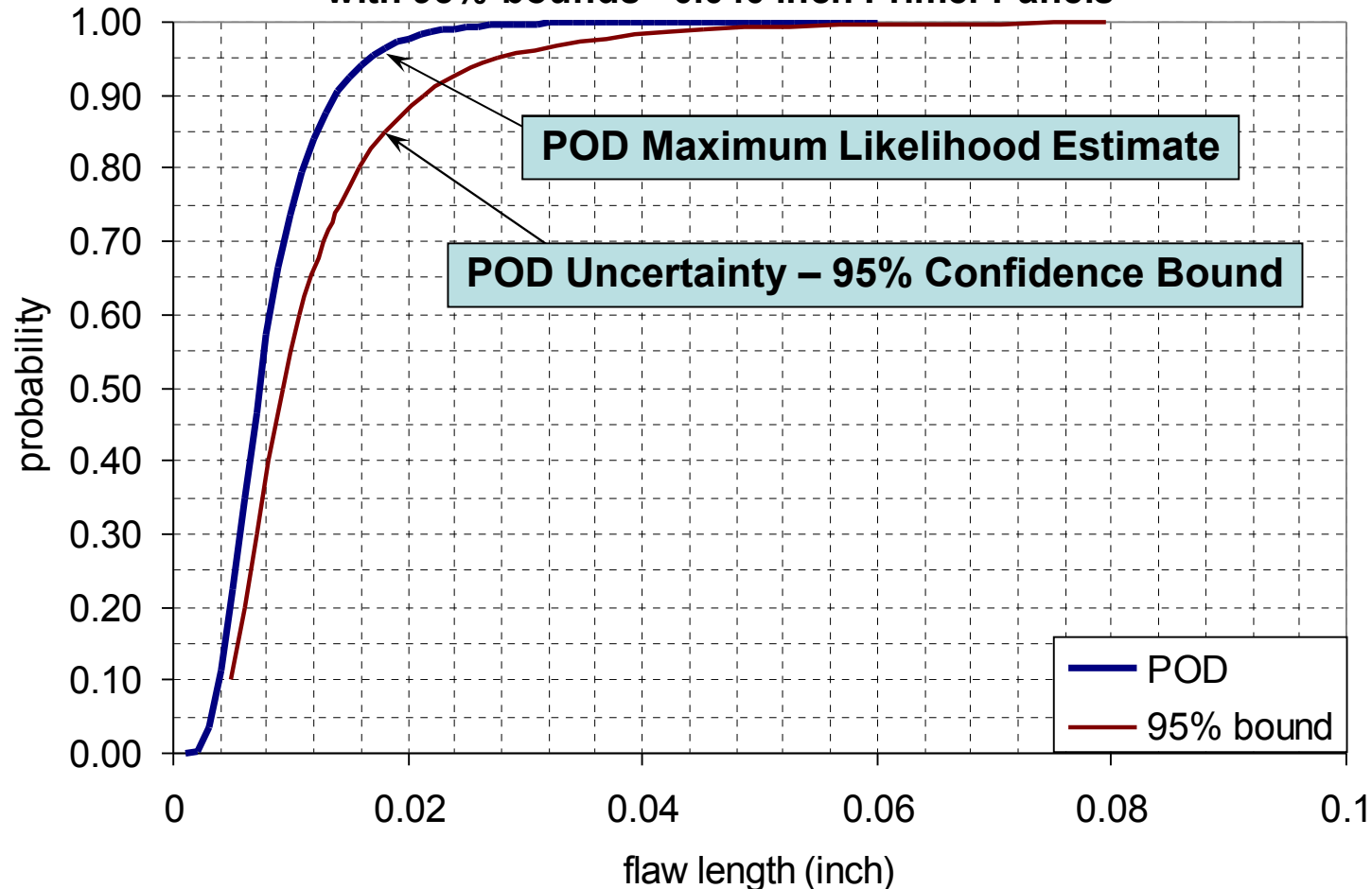
Detection level ($1 - \alpha$)	$K_{n,0.95,\alpha}$		$\bar{X} + K_{n,0.95,\alpha} \cdot S$ (log scale)		Flaw size in inches	
	bare	primer	bare	primer	bare	primer
0.75	1.366	1.465	-1.598	-1.834	0.025	0.015
0.90	2.210	2.355	-1.253	-1.631	0.056	0.023
0.95	2.736	2.911	-1.038	-1.504	0.092	0.031
0.99	3.747	3.981	-0.624	-1.260	0.237	0.055
0.999	4.900	5.203	-0.153	-0.981	0.703	0.104

$$\text{POD}_{(\text{Max Likelihood Est})} = \frac{1}{xS\sqrt{2\pi}} \text{EXP} \left(\frac{-(\ln(x) - \bar{X})^2}{2S^2} \right)$$

It is possible to calculate a one sided tolerance bound for various percentile flaw sizes - find factors $K_{n,\gamma,\alpha}$ to determine the confidence γ such that at least a proportion (α) of the distribution will be less than $X + (K_{n,\gamma,\alpha})S$ where X and S are estimators of the mean and the standard deviation computed from a random sample of size n

Sample Probability of Detection Curves for CVM

Cumulative Distribution Function Detectable Flaw Lengths -
with 95% bounds - 0.040 inch Primer Panels



CVM Validation - Crack Detection Results

All POD levels listed are for 95% confidence

Description: 0.040 inch thick panel (primer surface)

2024-T3 Alum.

PHASE 2 TESTS						
Panel	Fastener Crack Site	Distance from Fastener (inches)	Crack Length at CVM Detection (growth after install in inches)	SIM-8 Reading ΔPa (Pasm)	PM-4 Read-out	PM-4 Indicate Crack (Y or N)
4018	5R	0.040	0.002	400-500	1607	Y
4018	6R	0.014	0.007	1700-1800	2847	Y
4018	7R	0.040	0.010	400-500	1704	Y
4018	5R(2)	0.050	0.009	1700-1800	2768	Y
4018	6L	0.052	0.004	1000-1100	2161	Y
407	7L	0.118	0.006	3758-3786	4790	Y
407	5L	0.125	0.010	654-695	1769	Y
407	7R	0.147	0.009	345-375	1426	Y
407	5R	0.139	0.011	374-409	1391	Y
4018	6L	0.194	0.007	530-560	1628	Y
4018	5L	0.253	0.006	380-430	1553	Y
4018	8R	0.262	0.011	320-360	1452	Y
407	6R	0.189	0.012	450-510	1661	Y

90% POD Level	False Calls
0.021"	0

No false calls experienced in over 150 fatigue crack detection tests

[all panels are 2024-T3 alum. (AMS-4040, 41, QQ-A-250/5) with 0.0005" th. clad]



CVM Validation - Crack Detection Results (cont.)

All POD levels listed are for 95% confidence

Description: 0.100 inch thick panel (primer surface)

2024-T3 Alum.

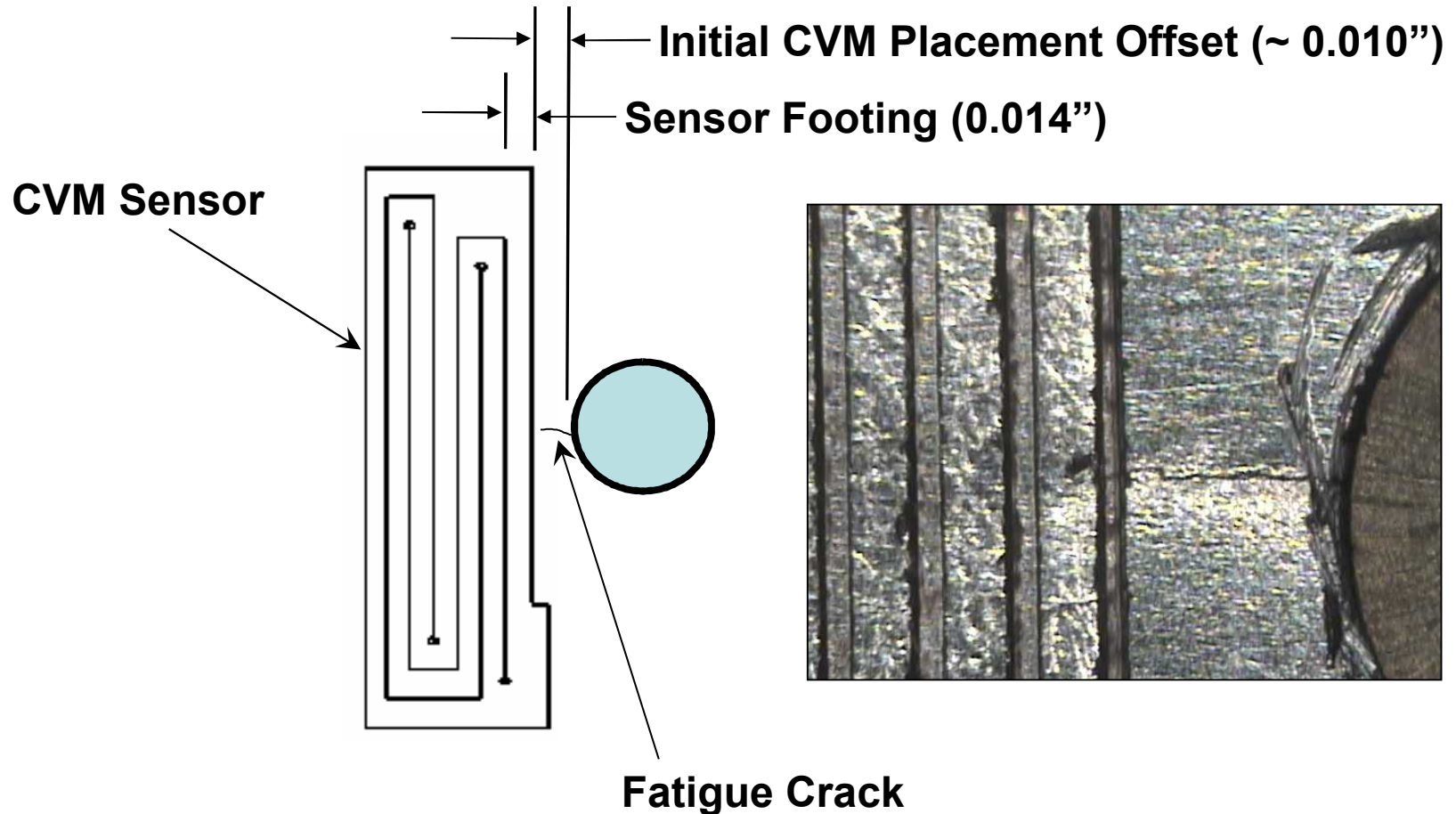
PHASE 2 TESTS						
Panel	Fastener Crack Site	Distance from Fastener (inches)	Crack Length at CVM Detection (growth after install in inches)	SIM-8 Reading ΔPa (Pasm)	PM-4 Read-out	PM-4 Indicate Crack (Y or N)
1001	5L	0.350	0.065	773-825	1713	Y
1001	7R	0.206	0.054	697-722	1768	Y
1001	8R	0.115	0.060	560-600	1609	Y
1003	8L	0.044	0.068	297-320	1410	Y
1003	7L	0.086	0.058	342-386	1411	Y
1003	8L	0.187	0.069	~1800	3391	Y
1003	6L	0.061	0.065	476-500	1846	Y
1003	6L	0.131	0.076	800-946	2117	Y
1003	8R	0.160	0.045	380-420	1508	Y

90% POD Level	False Calls
0.090"	0

[all panels are 2024-T3 alum. (AMS-4040, 41, QQ-A-250/5) with 0.0005" th. clad]

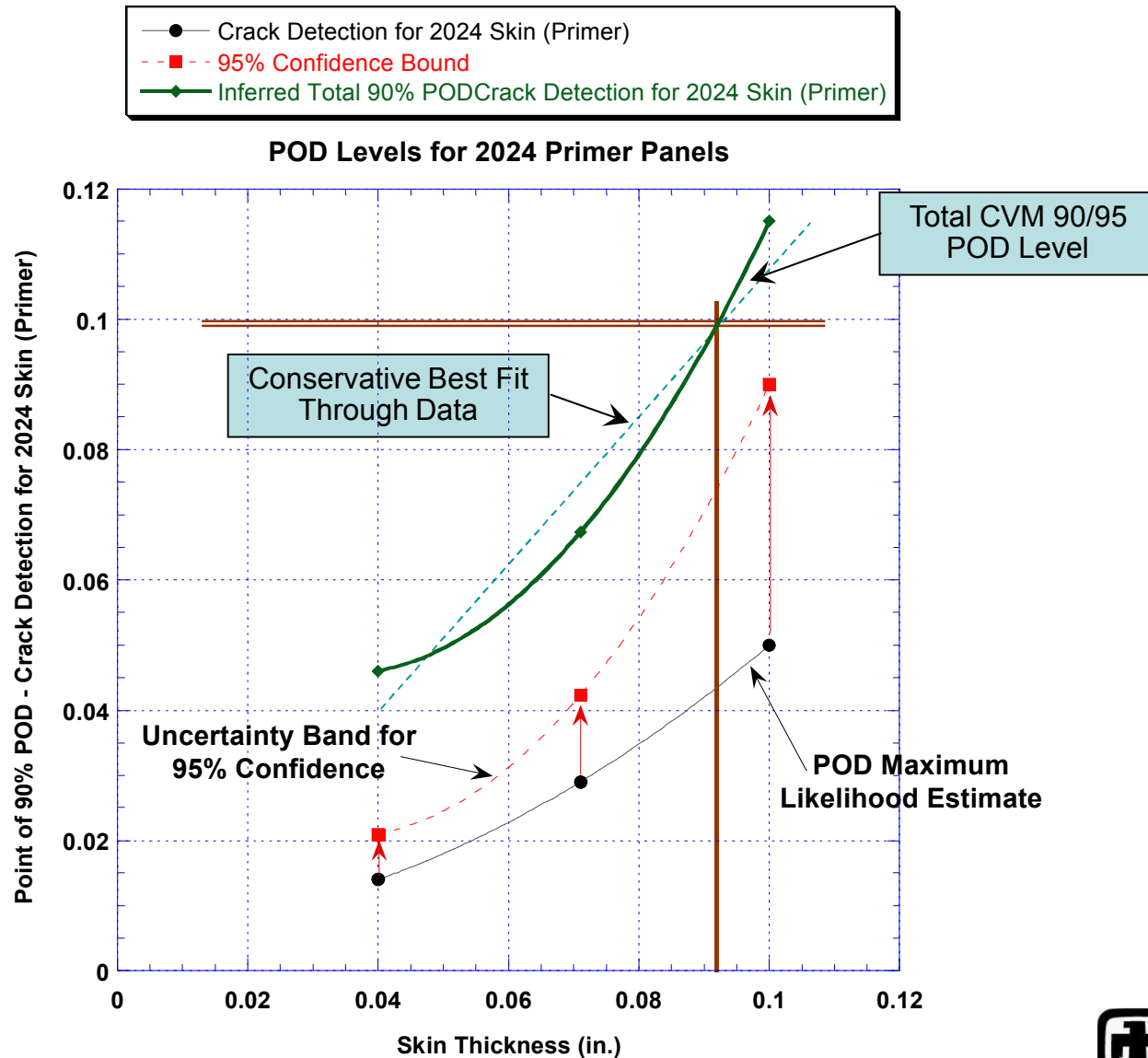


Determining Final CVM Crack Detection Level from Crack “Lag” Values



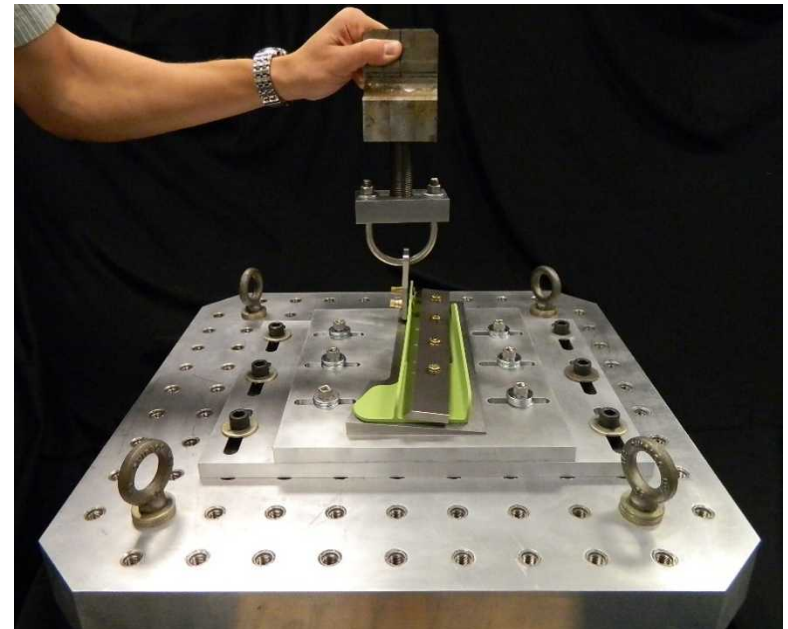
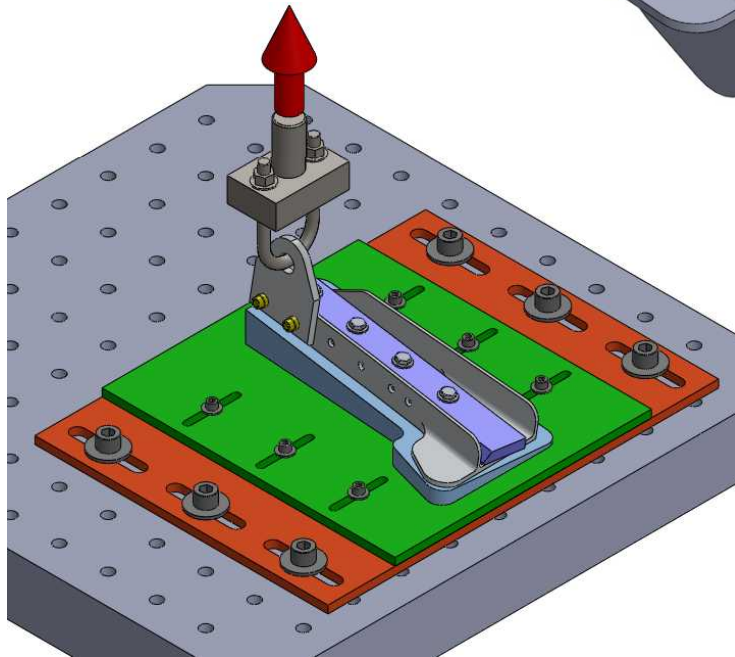
Total Crack Length at Detection = CVM Lag Detection + 0.014" + 0.010"

Overall Probability of Detection Values as a Function of Material Thickness



737NG Center Wing Box – CVM Performance Tests

Wing Box Fitting
Tension-Bending
Fatigue Loading



737NG Center Wing Box – CVM Performance Tests



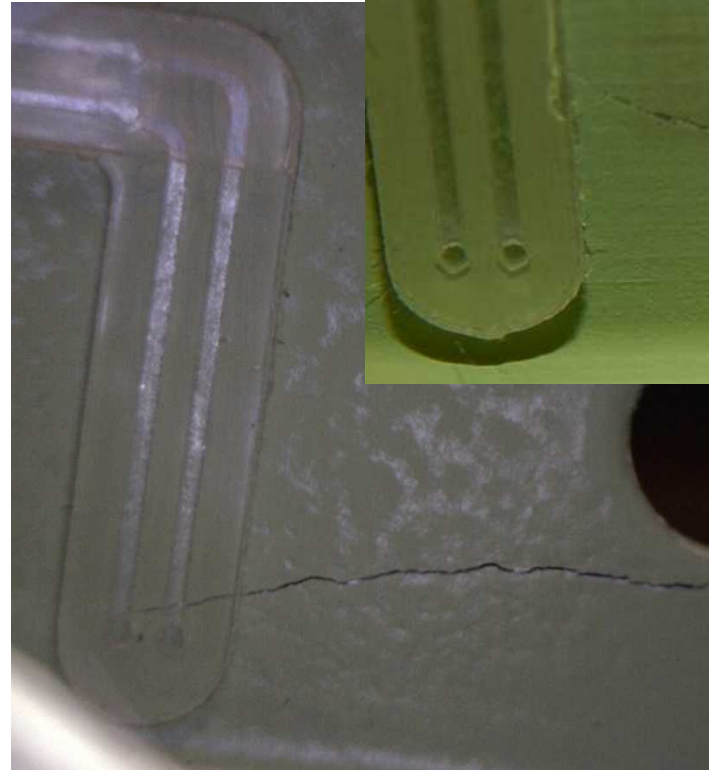
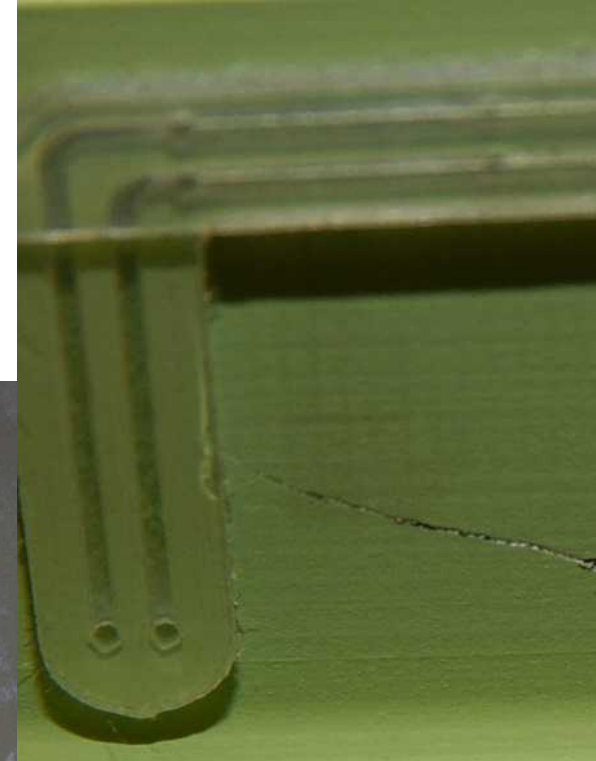
Sim-8 for real-time monitoring and PM-200 for final confirmation of CVM crack detection



737NG Center Wing Box – CVM Performance Tests



Fatigue crack
intercepting
dual gallery
arrangement



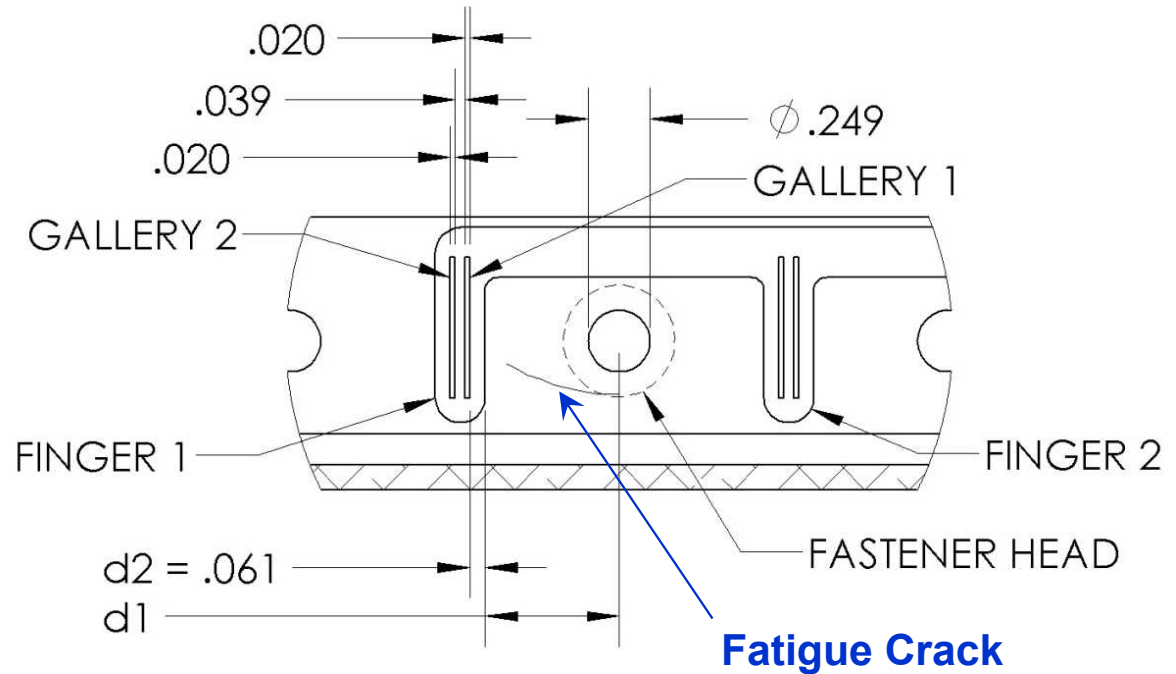
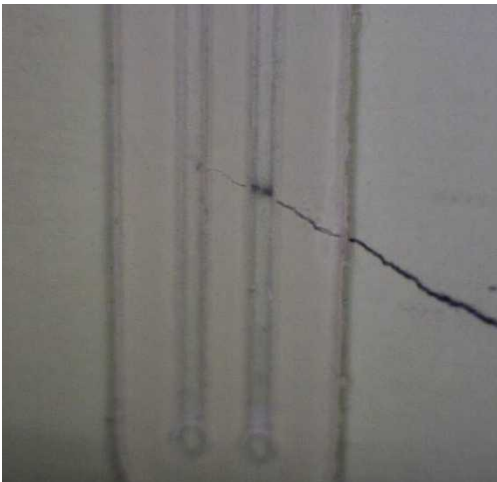
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National
Laboratories

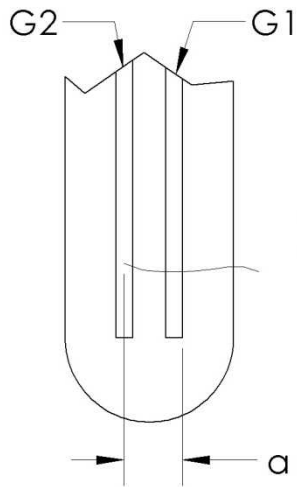
737NG Center Wing Box – CVM Performance Tests

- Bending crack has increased closure loads
- Monitoring for permanent crack detection – unloaded, unfastened and multiple day lag in readings
- Sealant (FVB) applied to determine crack detection when entire surface is sealed
- POD_[90/95] for 1st & 2nd gallery; S/N > 10



737NG Center Wing Box – CVM Performance Tests

CVM Sensor Wing Box Fitting Performance Tests					
Test No.	CVM Finger Location	Sensor Distance from Fastener d_1 (In)	Crack Length at CVM Detection a (In)	SIM-8 Reading (Pa)	PM200 Reading (dCVM)
T1	2	0.488	0.084	282	7.4
T2	1	0.524	0.109	496	35.5
T3	1	0.550	0.089	2017	157.5
T4	1	0.570	0.094	330	14.4
T5	1	0.574	0.084	285	8.9
T6	1	0.580	0.079	2901	264.8
T7	2	0.546	0.124	318	22.5
* Final values being confirmed					
** Detection for unloaded state with sealed crack and sensor					

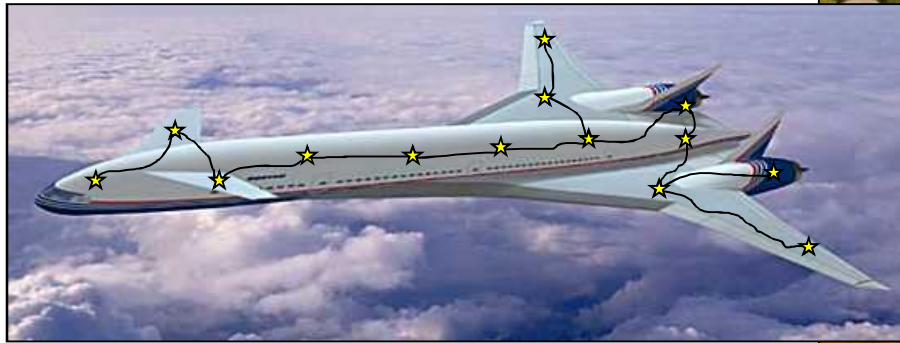


Crack Length: a = excursion into CVM galleries

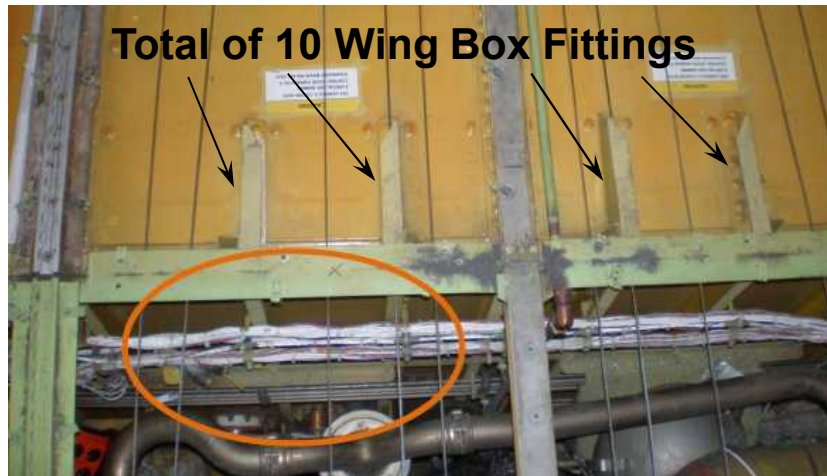


Field Evaluation of Sensor Networks for Structural Health Monitoring

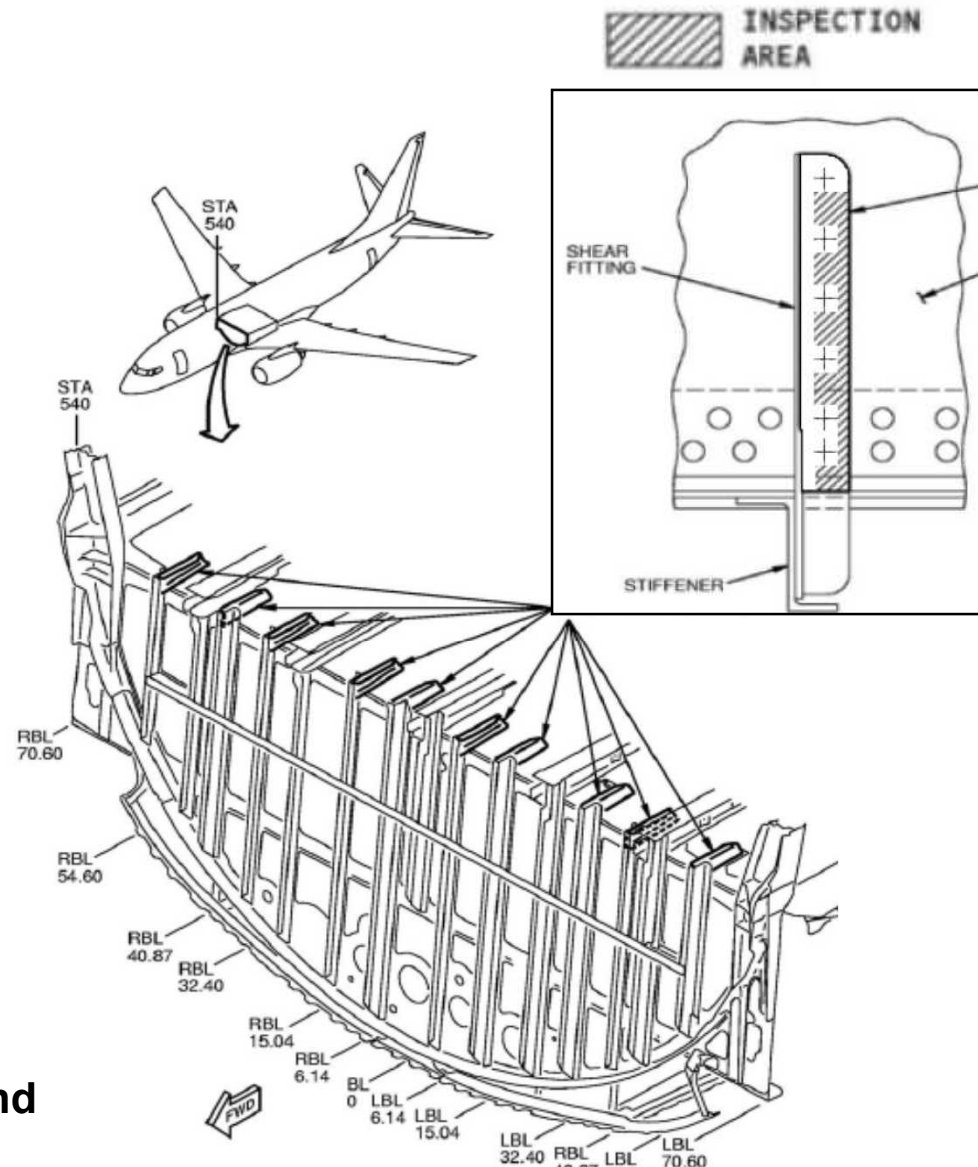
Automatically assess structural condition, & signal need for maintenance actions



737NG Center Wing Box – CVM Flight Tests



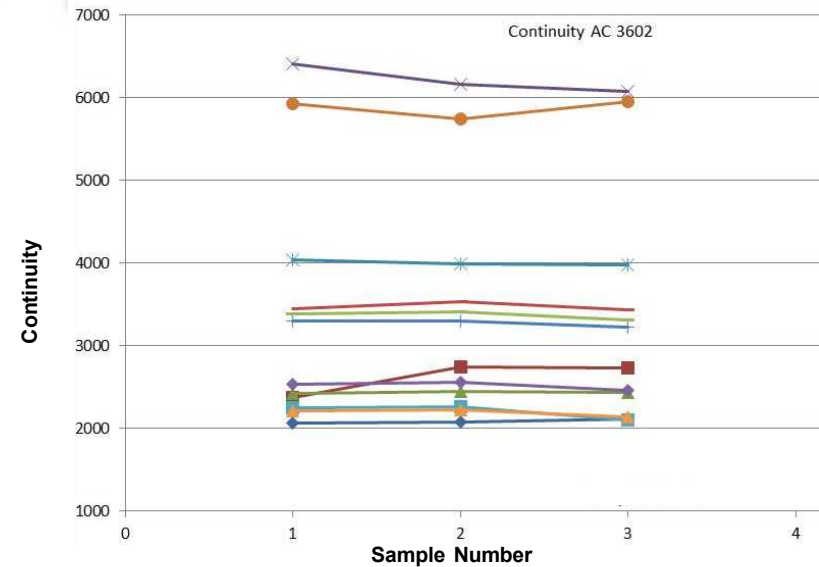
**CVM Sensor on 737NG Wing Box Fitting and
Top View of SLS Mount Location**



Sample CVM Flight Test Data

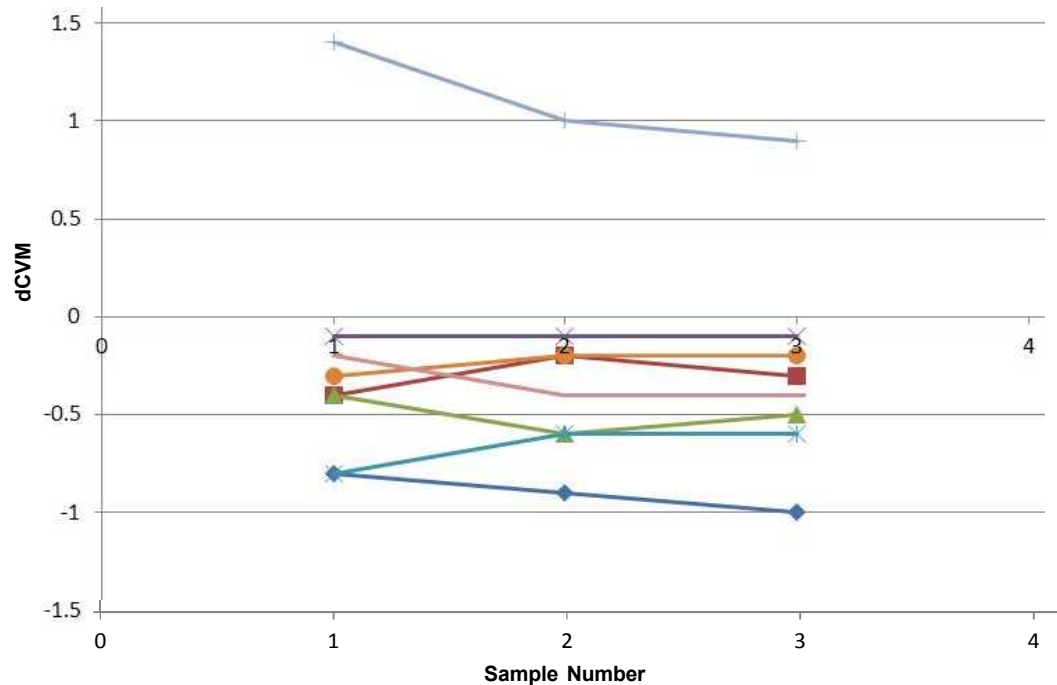
AC3602 Continuity Check

- Fail-safe check – want continuity (flow) high
- Crack detection – dCVM (vacuum) low = no crack
- Conductivity Index = flow

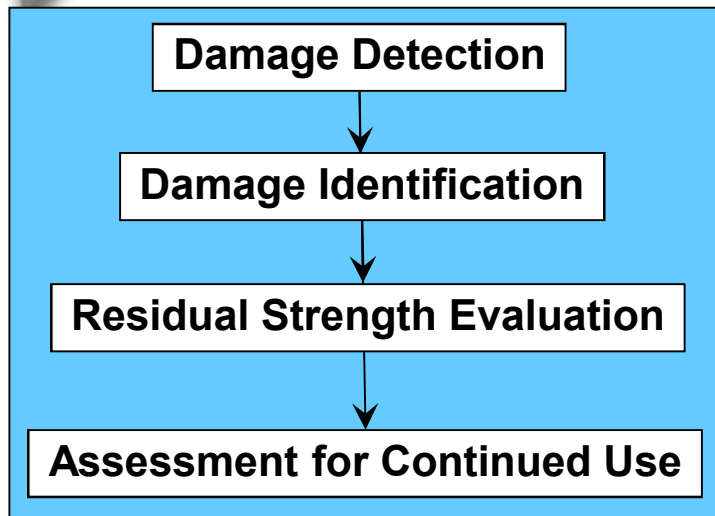


- ◆ 1CVM Pos 1 (1,2,3)
- 2CVM Pos 1 (1,2,3)
- ▲ 1CVM Pos 2 (4,5)
- ✕ 2CVM Pos 2 (4,5)
- ✱ 1CVM Pos 3 (6,7)
- 2CVM Pos 3 (6,7)
- + 1CVM Pos 4 (8,9,10)
- 2CVM Pos 4 (8,9,10)

AC3602 CVM Readings

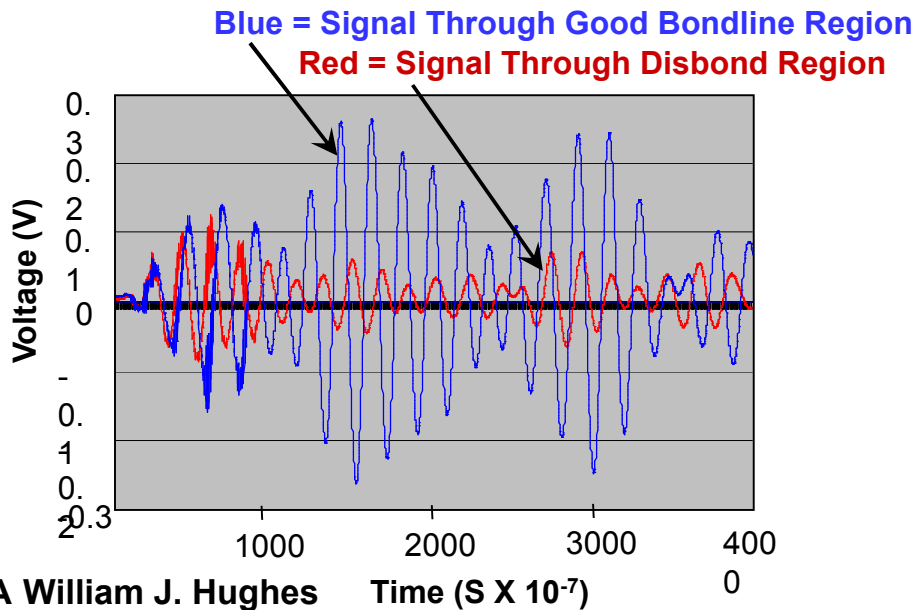
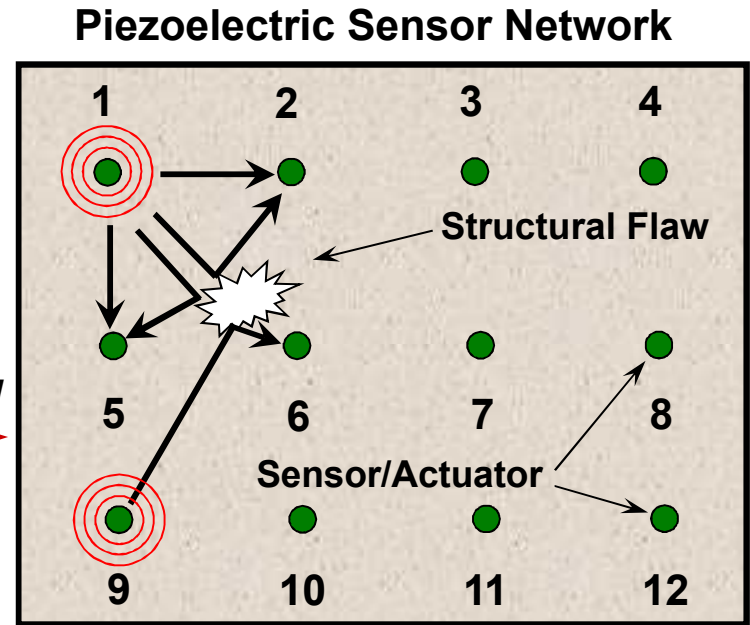


Global SHM - Disbond Detection & Growth Monitoring with Piezoelectric Sensors

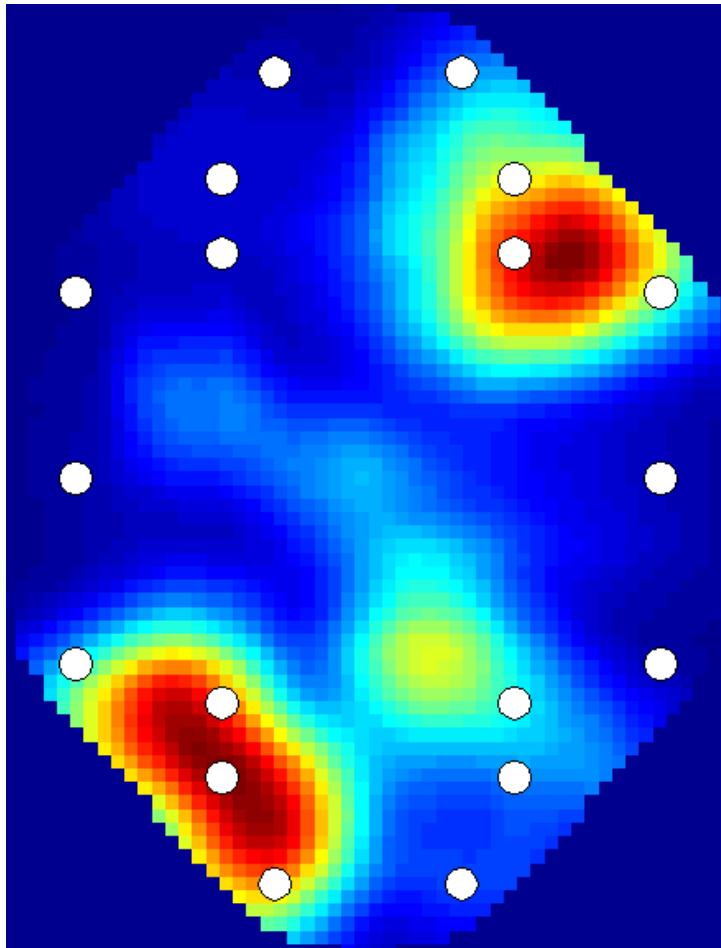


Sensor Data
←

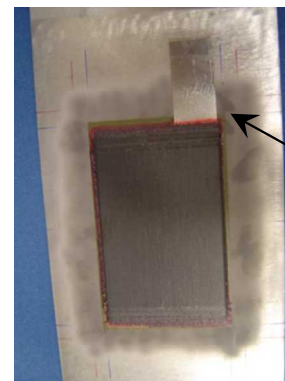
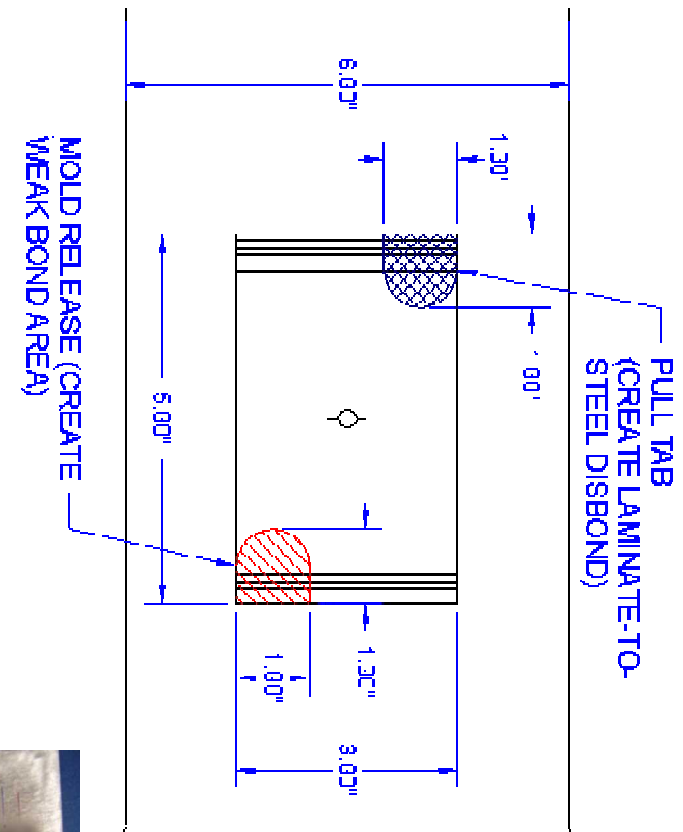
Actuation Signal
→



Disbond Detection & Growth Monitoring with Piezoelectric Sensors

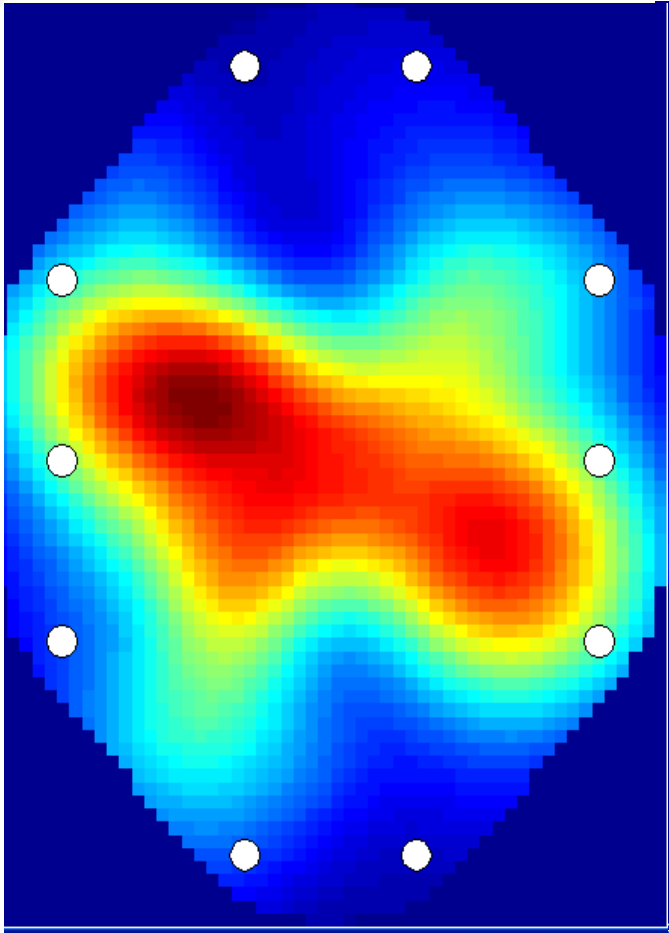


After mold release flaw growth
(50 KHz inspection)

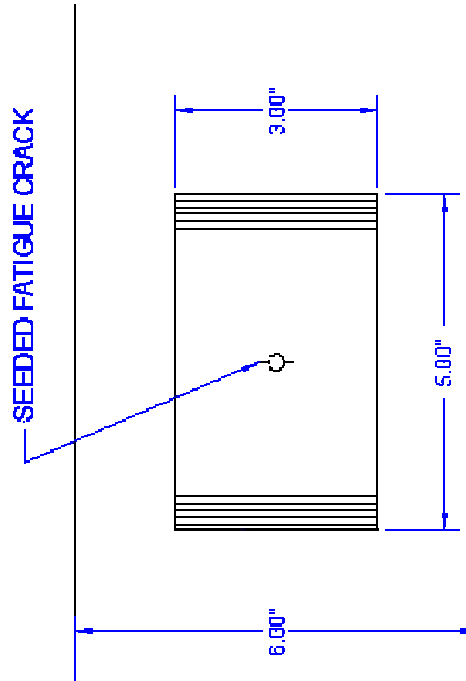


Pull tab flaw

Crack Detection & Growth Monitoring with Piezoelectric Sensors



87K Cycles



***PZT crack length estimates
within 5% of measured***



FAA William J. Hughes
Technical Center





Conclusions on Use of SHM Reliability

- Recent advances in health monitoring methods have produced viable systems for on-board aircraft inspections
- Sensors must be low-profile, easily mountable, durable, reliable & fail-safe
- Calibration for flaw identification (damage signatures) is key
- General lab performance (sensitivity/POD) & flight test data is needed
- **Reliability/POD assessments will depend on sensor system, flaw type/orientation and application**
- CVM sensor detects cracks in the component it is adhered to - inspection process and diagnosis is automated & remote
- **One-sided tolerance interval can be used to calculate POD for certain circumstances (known flaw location and flaw direction)**
- Can monitoring process & diagnosis be fully automated (green or red light)?
- Status –
 - Successful integration of SHM in NDT Standard Practices Manuals
 - AMOC for SBs and ADs or STCs – safety driven use is achieved in concert with OEMS & regulatory agencies; Certification & regulatory framework is being addressed (need for formal POD)





SHM Environmental Durability Performance Assessment



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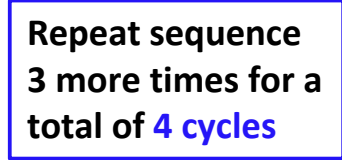




Environmental Durability Performance Assessment

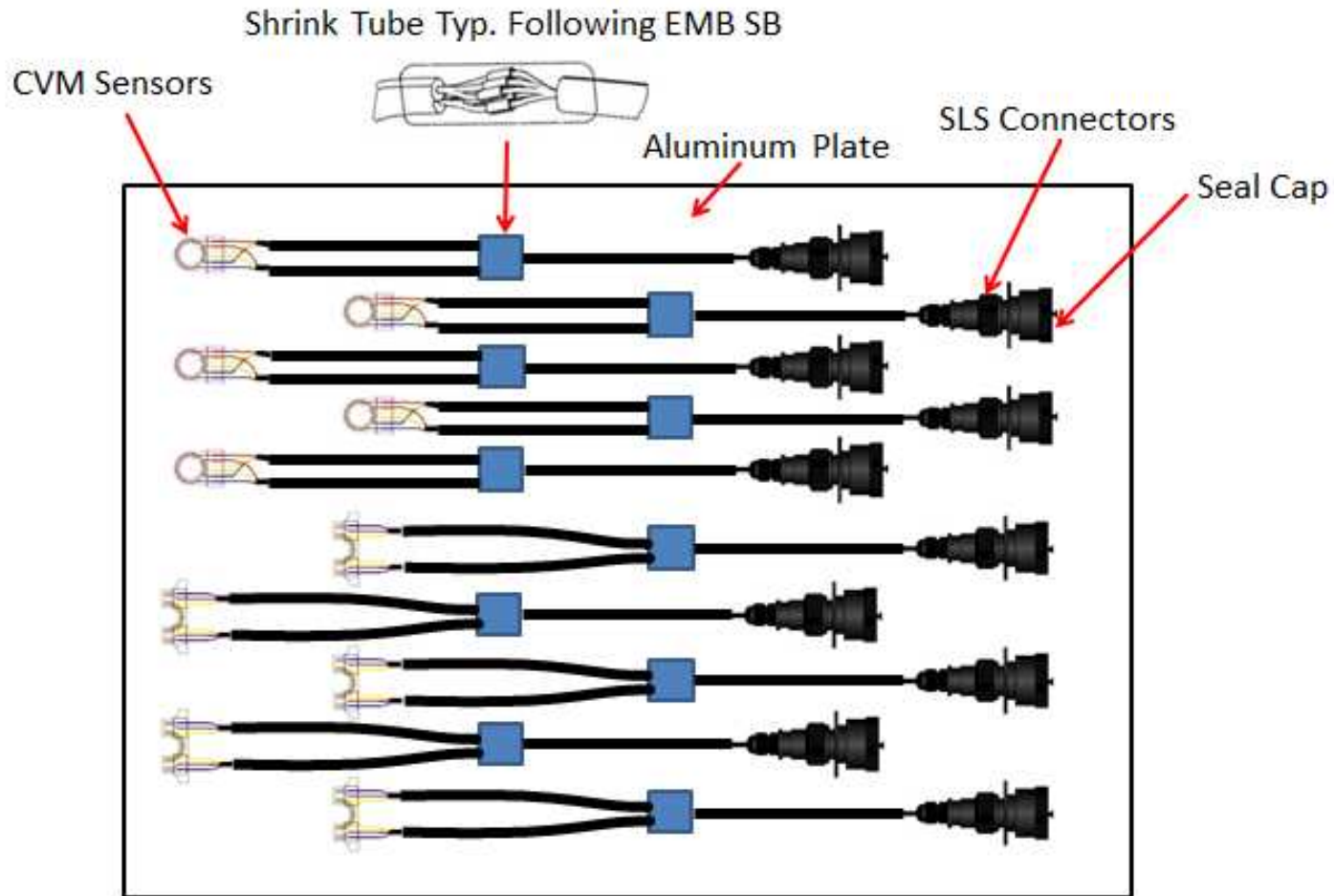
- Part of overall performance testing - meant to establish durability of sensor systems
- Utilize same approach as previous FAA certification effort with Boeing-Delta
- Sensor fail-safe feature is critical item – will be proven
- Environmental elements:
 - Hot-wet (55°C and 95% +% RH)
 - Freeze (-18°C)
 - Heat (93°C)
 - 7 day cycle – repeated 4 times (28 days)
- Sensor function measurements will be acquired at each environment change
- Test specimens include all hardware that remains on the aircraft during operation





Environmental Test Configuration for CVM Sensors

CVM will be coated with Polysulfide sealant AMS 3281
(2007B002AM654SK, Manuf. PRC Desoto Int'l Inc.)



Study to Assess the Effects of Corrosion Inhibiting Compounds on the Performance of CVM

Objective: Provide confidence in the performance of CVM in the presence of CICs during crack growth

CIC Selected:

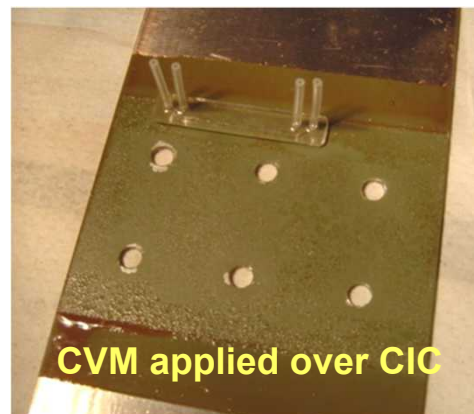
- BMS 3-35 which is Ardrox AV15 or Corban-35 (Zip Chem)
- BMS 3-23 which is LPS-3 or Ardrox AV-8 or Dinitrol



Crack Detection:

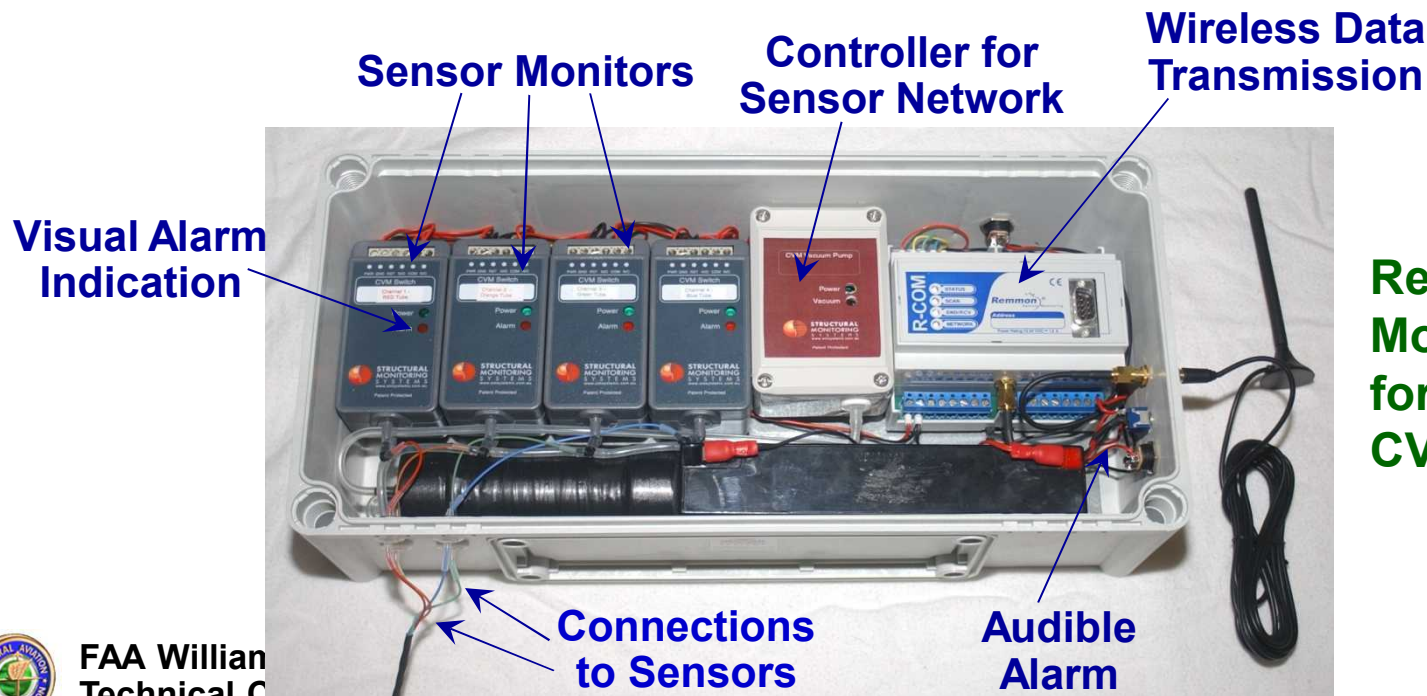
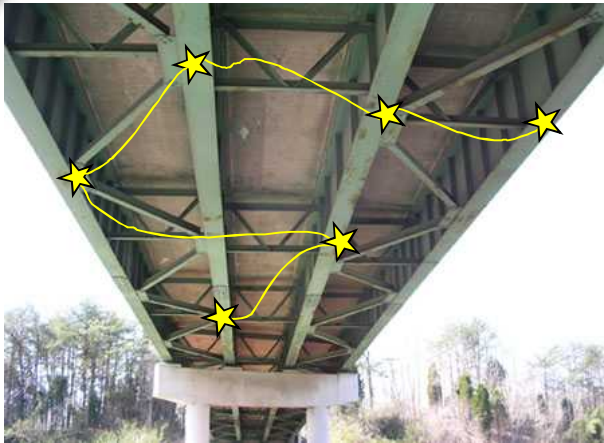
$a_{90} = 0.011''$ w/o CIC

$a_{90} = 0.013''$ w/ CIC



No CIC drawn into galleries

Real-Time Structural Health Monitoring of Bridges Using CVM Sensors



Real-Time, Remote Monitoring System for a Network of CVM Sensors