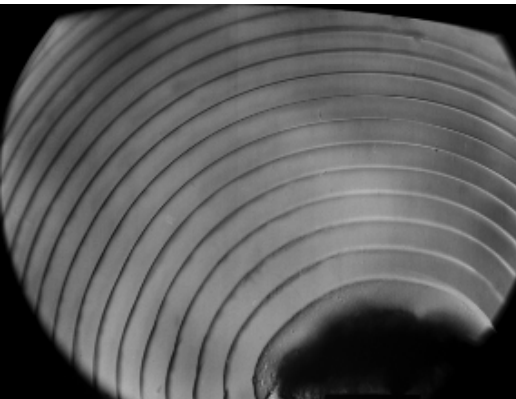
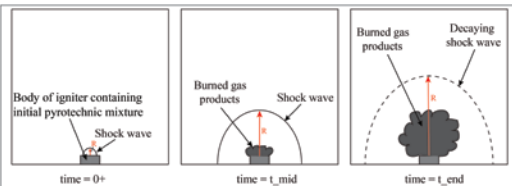
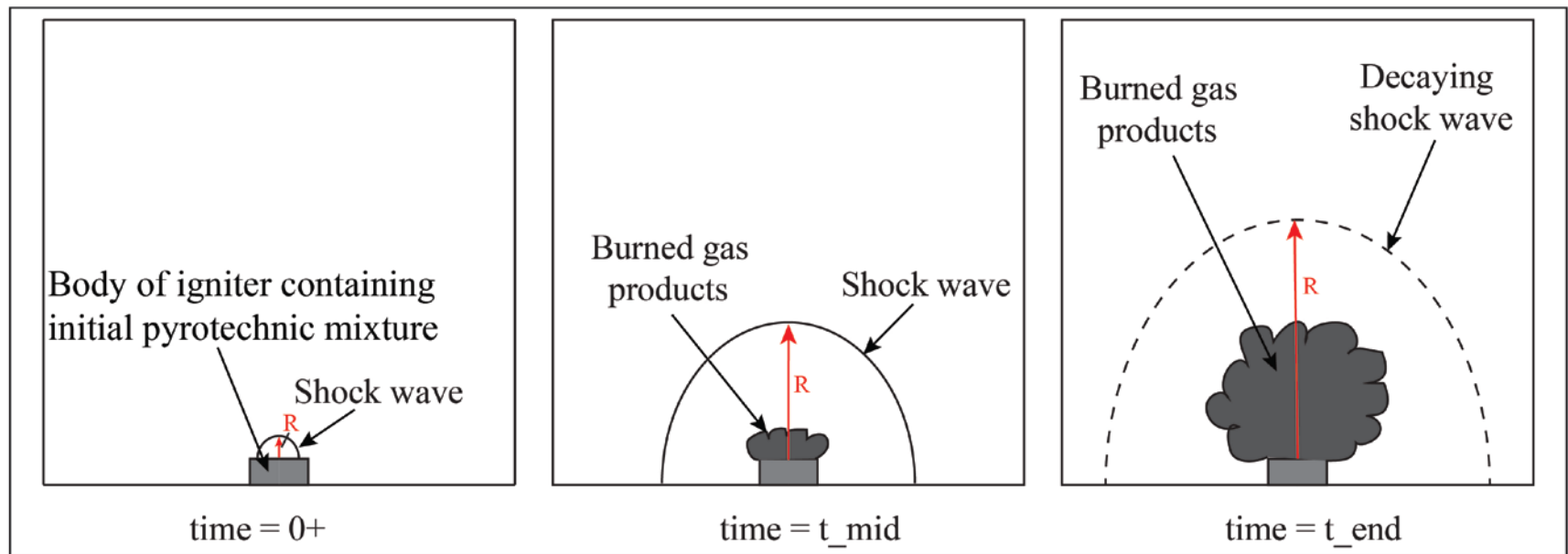


ASSESSING POST-IGNITION PYROTECHNIC BEHAVIOR



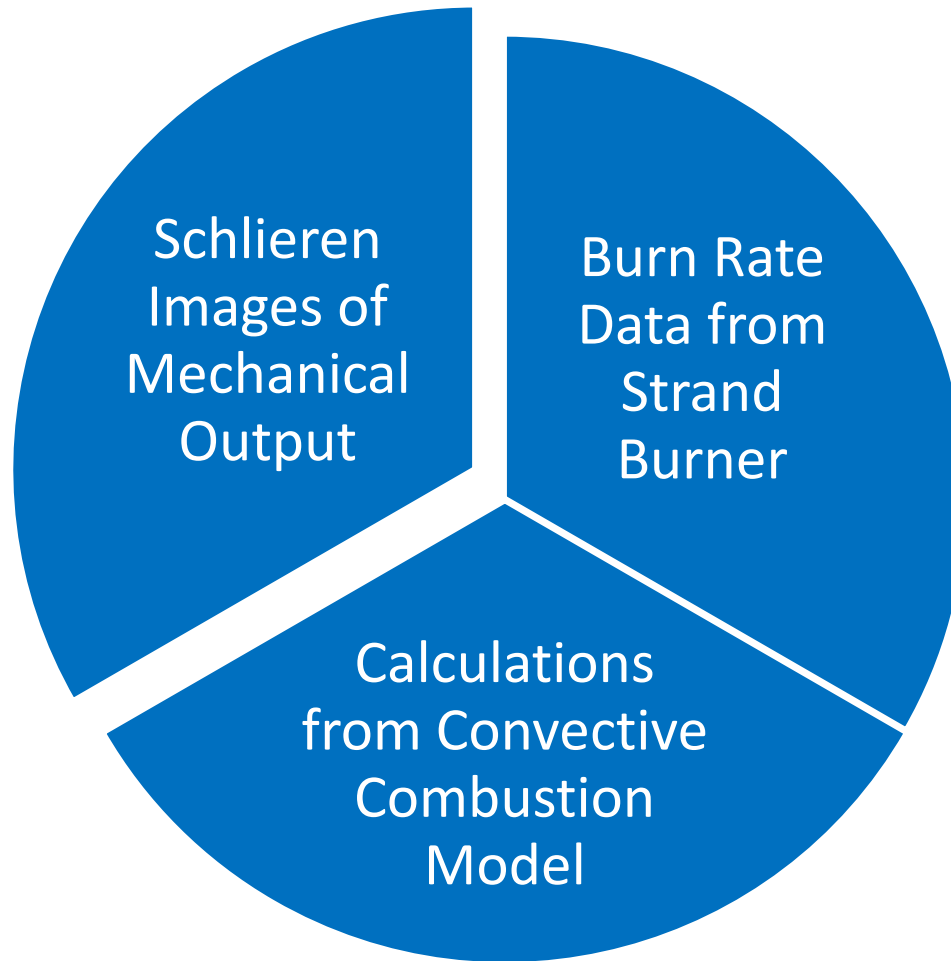
Michelle N. Skaggs, Marcia A. Cooper,
William W. Erikson

Schlieren Images

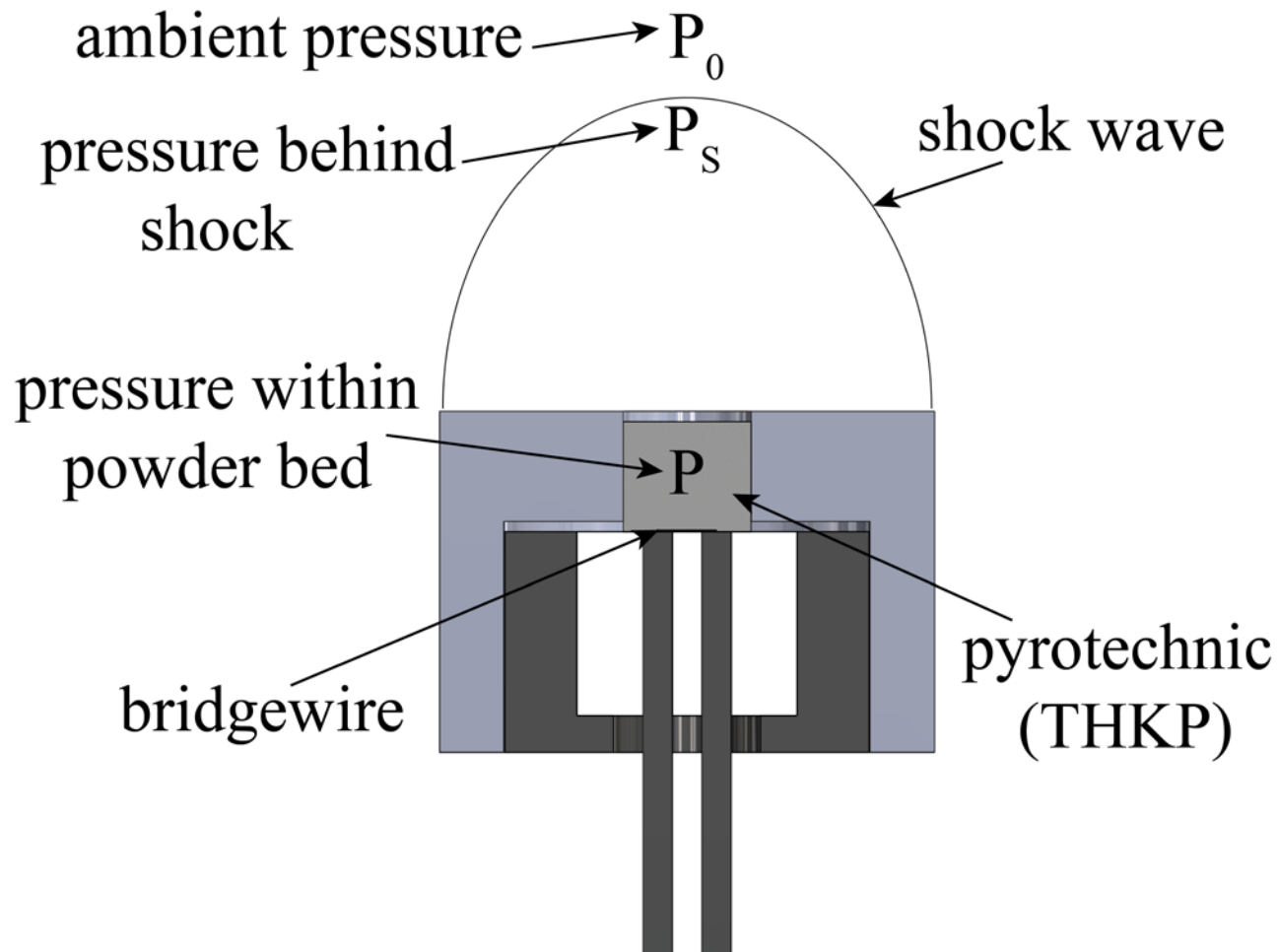


- Pyrotechnic within igniter reacts and releases high pressure into surrounding environment
- High pressure creates an expanding blast wave with radius R
- Images capture expanding blast wave and combustion products as a function of time

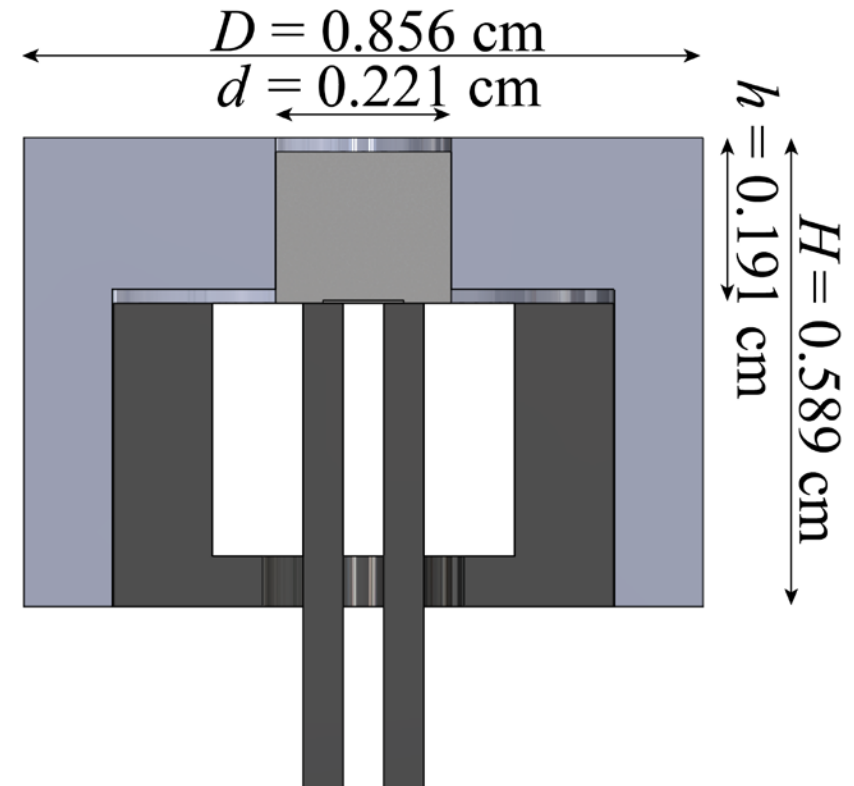
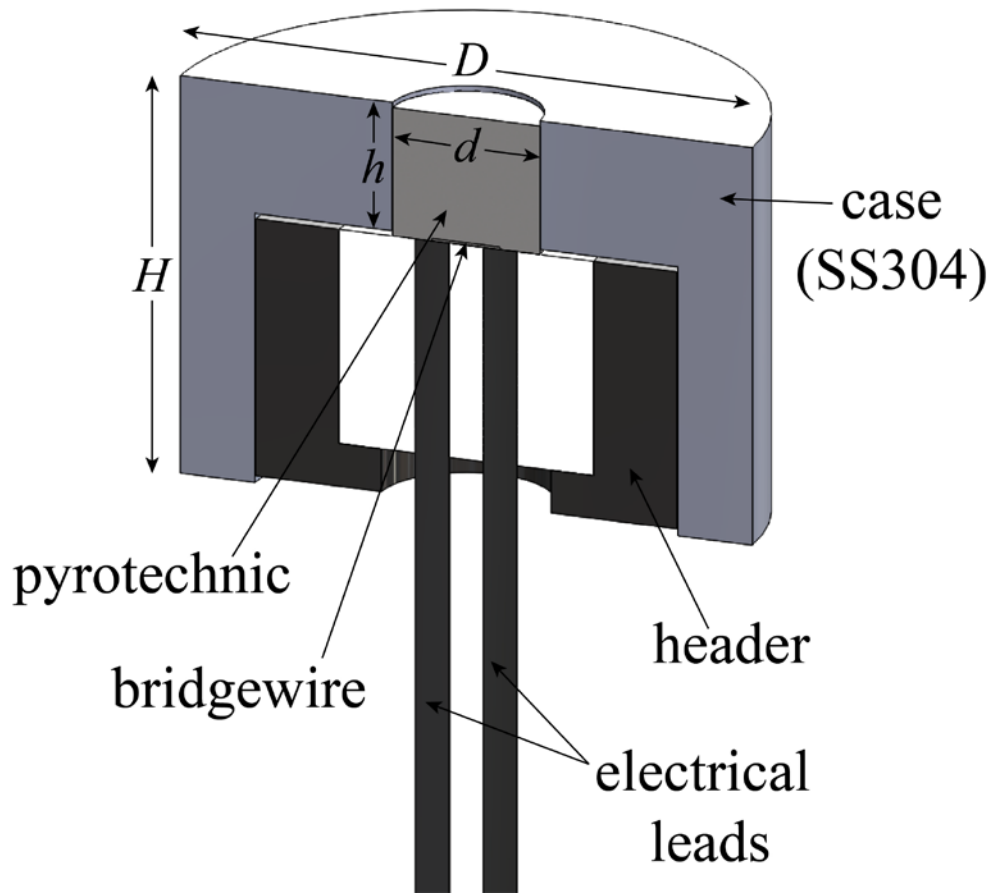
Combined Research Effort



Study within *and* external to device



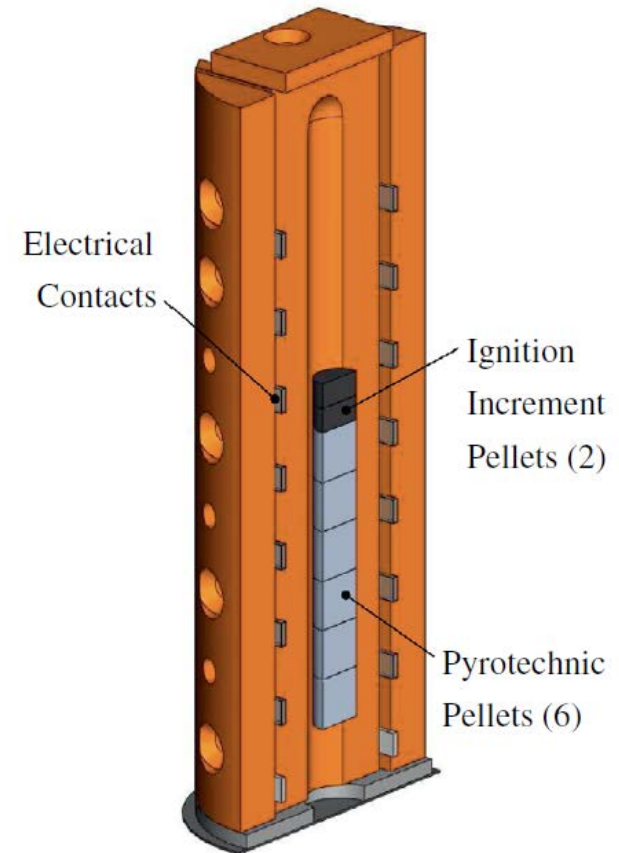
Research igniter



- $\text{TiH}_{1.65}/\text{KClO}_4$ (THKP)
 - 33% $\text{TiH}_{1.65}$: 67% KClO_4 by weight
 - $\text{TiH}_{1.65}$ particles are nominally 13 μm
 - KClO_4 particles are nominally 22 μm
 - TMD = 2.845 g/cm³
 - THKP density studied for this work is nominally 80% TMD

Relating strand burner burn rate data to device scale

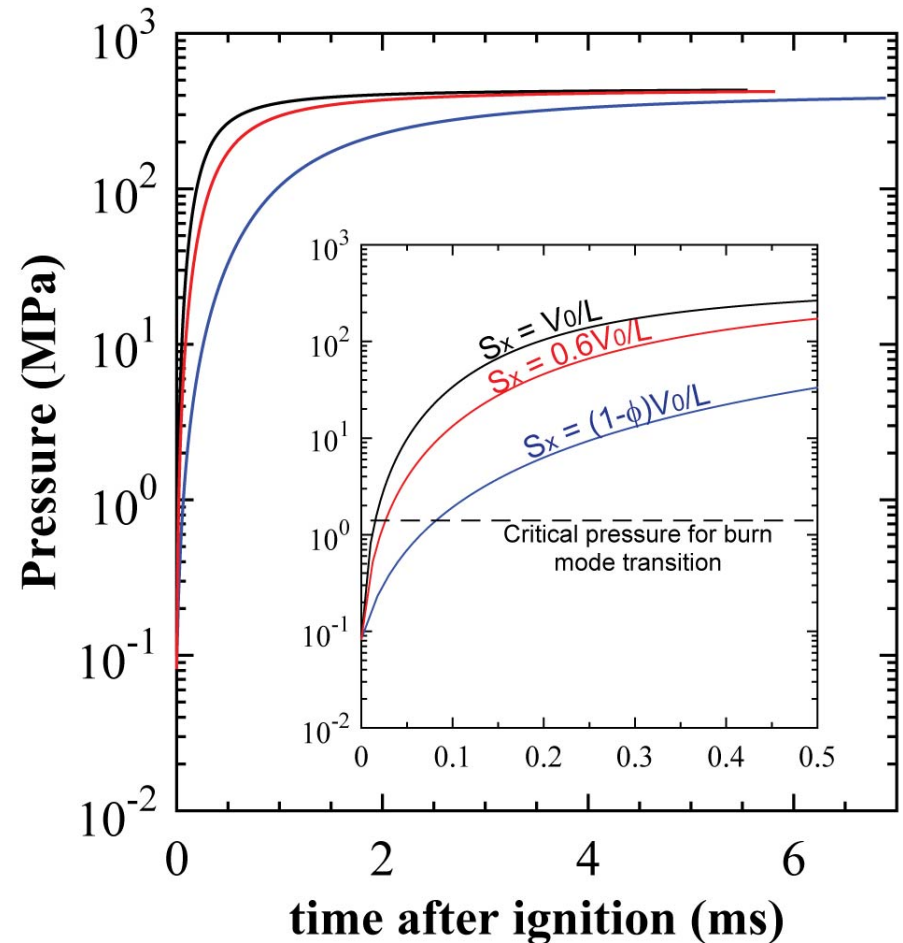
- Steady conductive burn rates previously measured in hybrid closed-bomb strand burner
- Data fitted to Vieille's equation $r = BP^n$ ($B = 1.5054 \text{ cm/s}$ and $n = 0.5239$)
- Relate these burn rates to much smaller device scale through derived universal relationship
- Pressure rise in free volume dependent on gas phase products generated by combustion of initial solid material with burn surface area (S_x)



Source: M.A. Cooper and
M.S. Oliver (2013)
Combustion and Flame.

Burn rate pressure prediction

- Predictions vary with assumption of S_x
- Previous studies have shown that red curve best represents strand burner experiments
- Predicted pressure is >100 MPa at 500 μ s after ignition
- Predicted pressure is >200 MPa at 2 ms after ignition
- Evidence of transition to unsteady (deconsolidated) burning mode

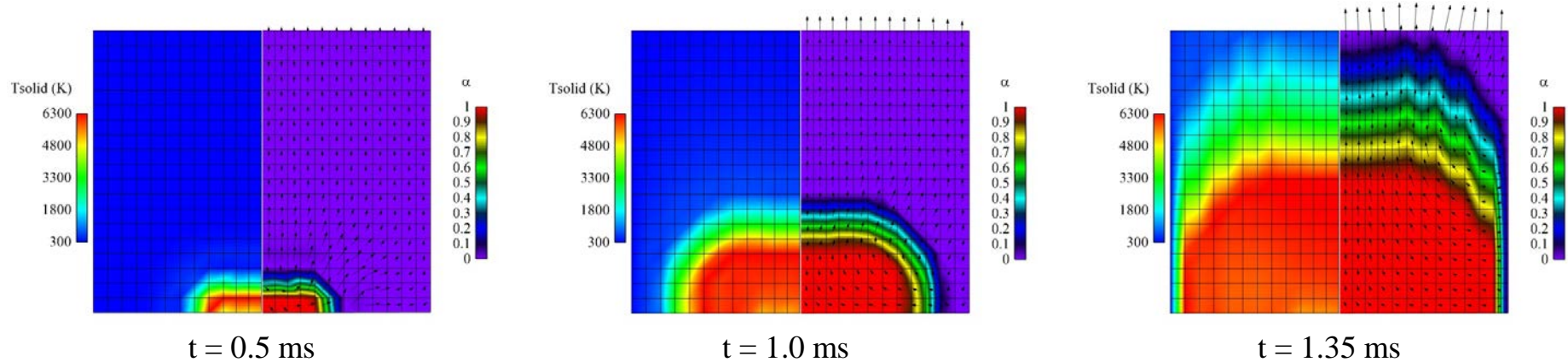


Convective Combustion Model

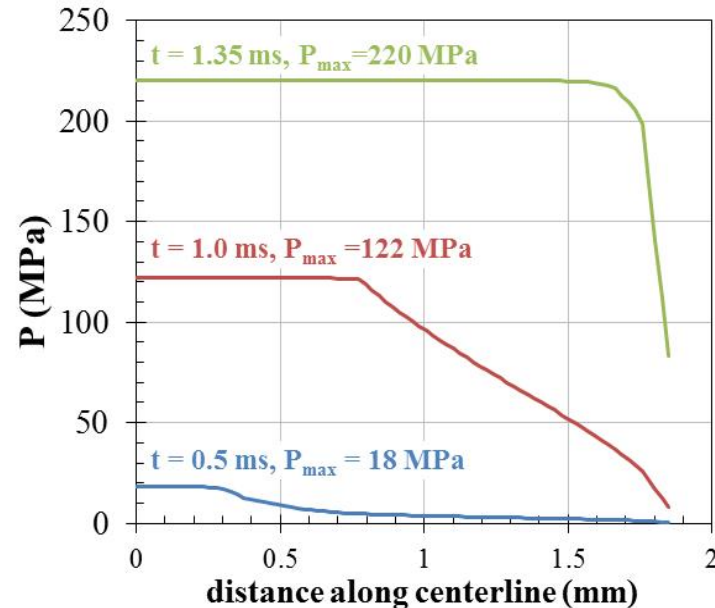
- Simple convective combustion model = solid particle combustion coupled with porous flow model for gas transport
 - Particles treated as shrinking spheres
 - Gas transport via Forchheimer-corrected Darcy's law
 - Ideal gas or Noble-Abel equations of state are used
 - Neglect particle bed compaction and certain flow effects (turbulence, supersonic flow, etc.)
- THKP initial values:
 $C_p = 850 \text{ J/kg-K}$, $W = 39 \text{ g/mol}$, $\Delta H_{\text{rxn}} = -3.8\text{e}7 \text{ J/kg}$, $F_g = 0.5$

Combustion Model pressure predictions

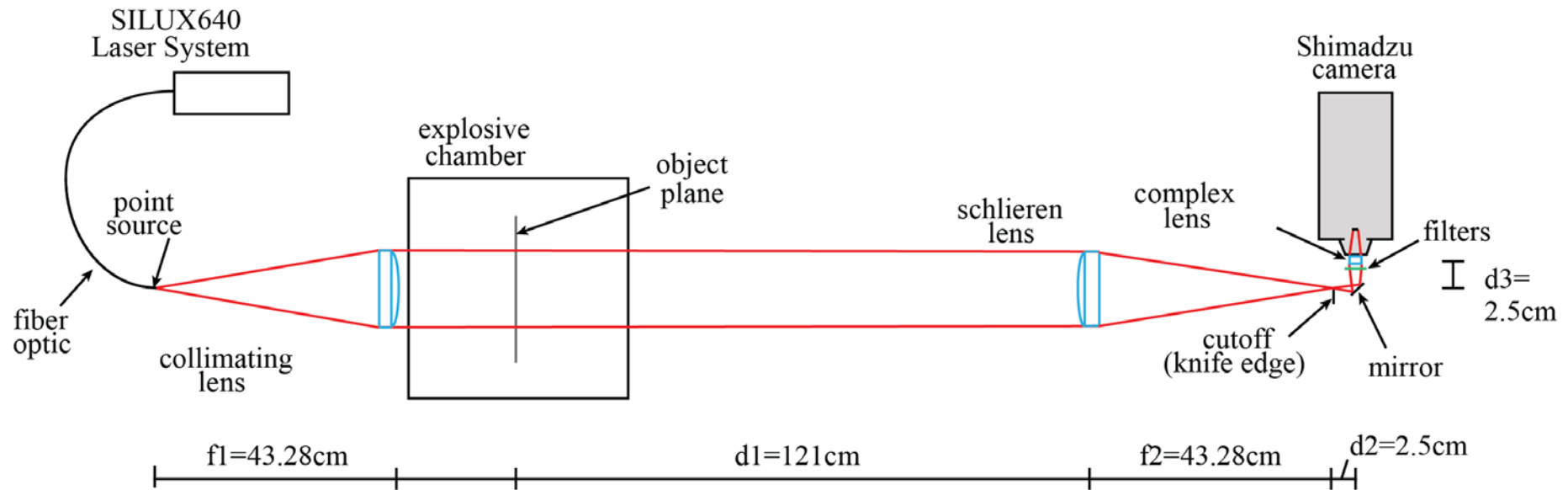
(Left) solid temperature and (right) extent of reaction with velocity vectors



- Predicted pressure is 18 MPa at 500 μ s after ignition
- Predicted pressure is >220 MPa at 2 ms after ignition (only half of research igniter column height)



Schlieren Imaging System



- SILUX640 Laser system = non-coherent illumination at 640nm
- Shimadzu HPV-2 high-speed camera records 102-frame image sequences at 500 kHz with 312×260 pixels
- FOV is $8\text{ cm} \times 8\text{ cm}$

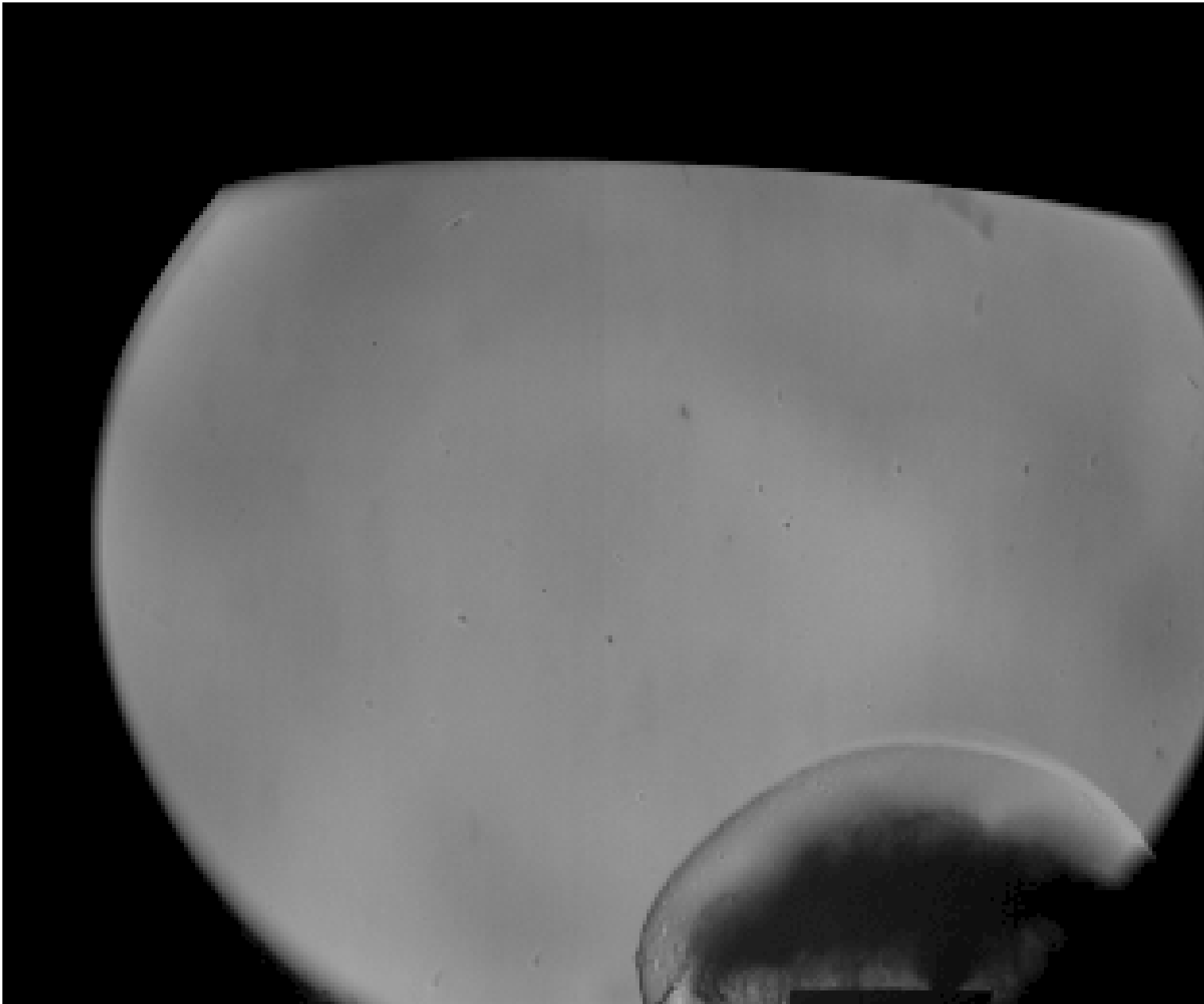


Image Results – blast wave

- Igniter located in bottom right corner
- a) Composite frame showing blast wave shape evolution every $10\ \mu\text{s}$
- b-d) Shows gas volume expansion and particle motion every $20\ \mu\text{s}$
- $t=0\ \mu\text{s}$ corresponds to trigger time required to synchronize laser pulses, camera frames, and firing signal ($t=0\ \mu\text{s} \approx t = 2\ \text{ms}$ after ignition)

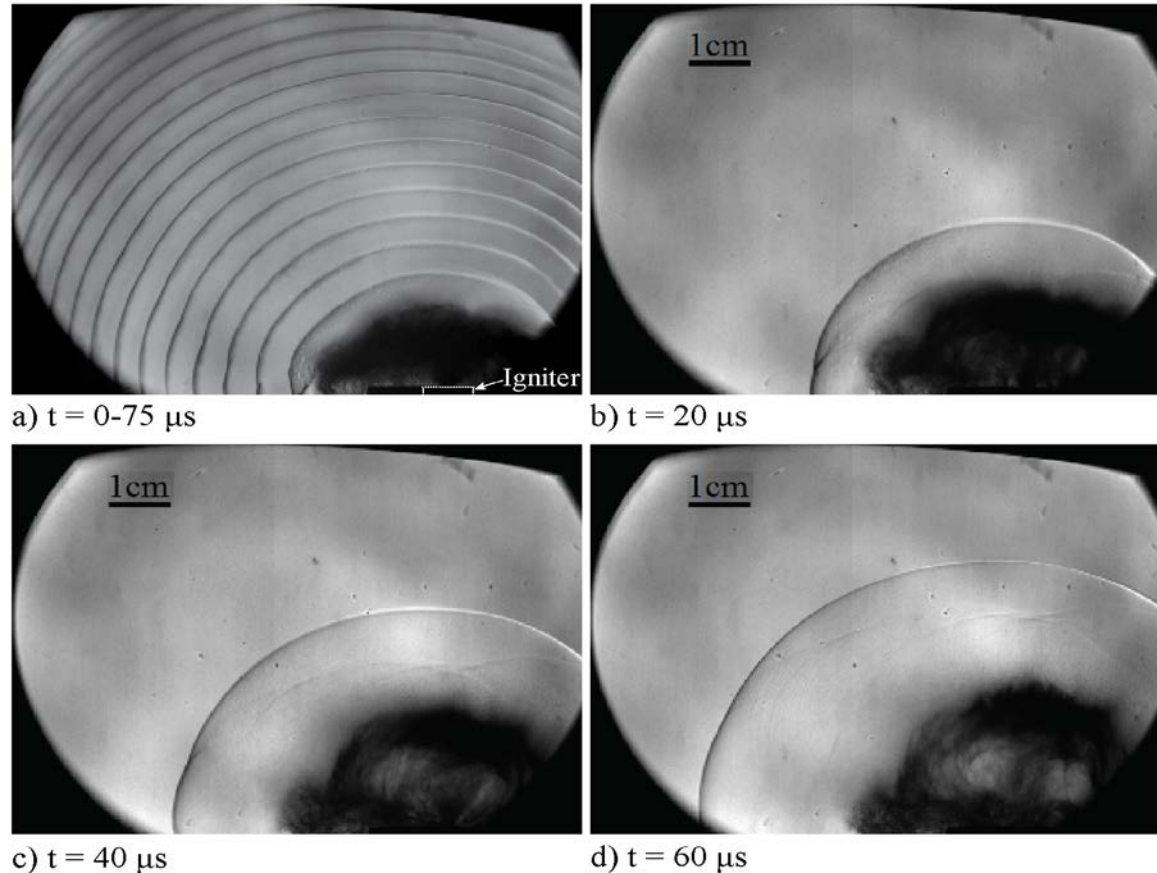
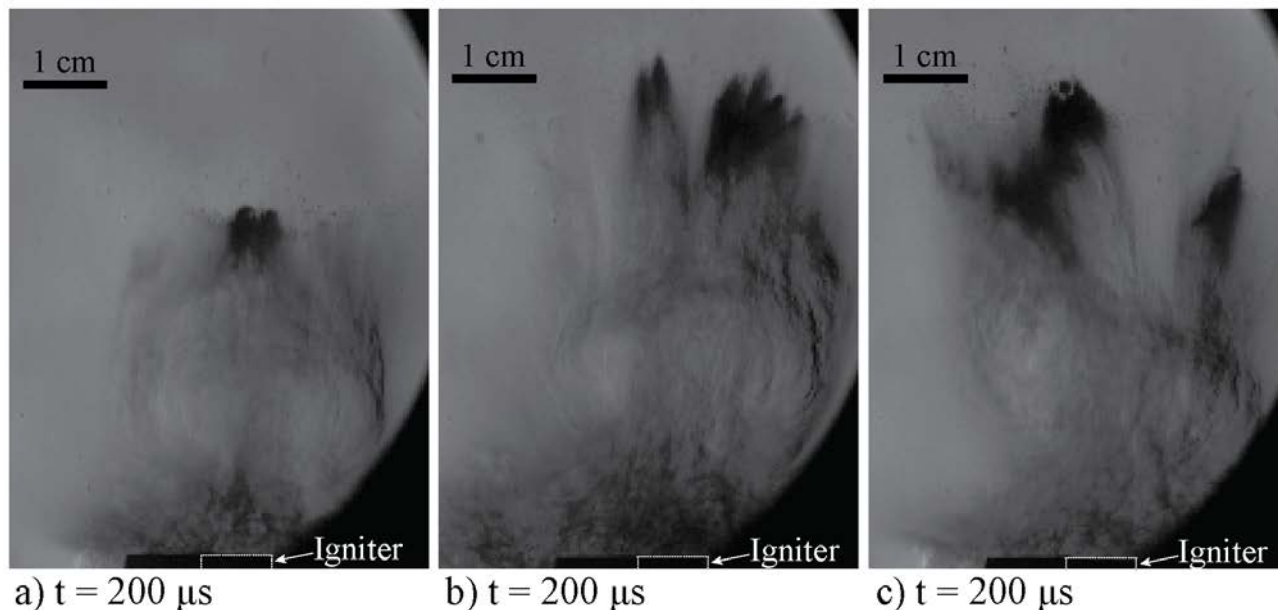


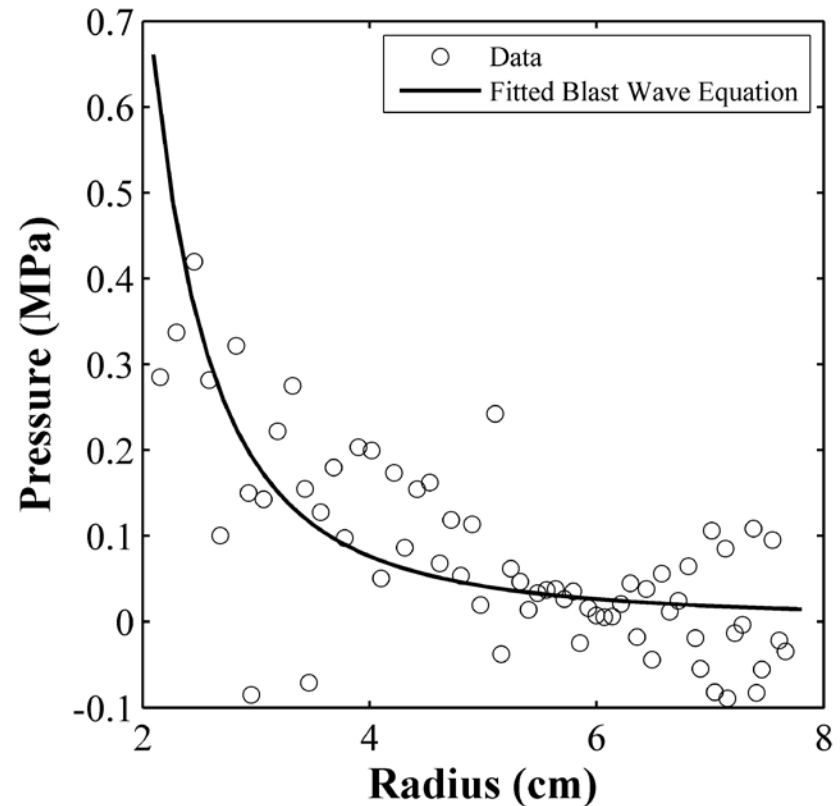
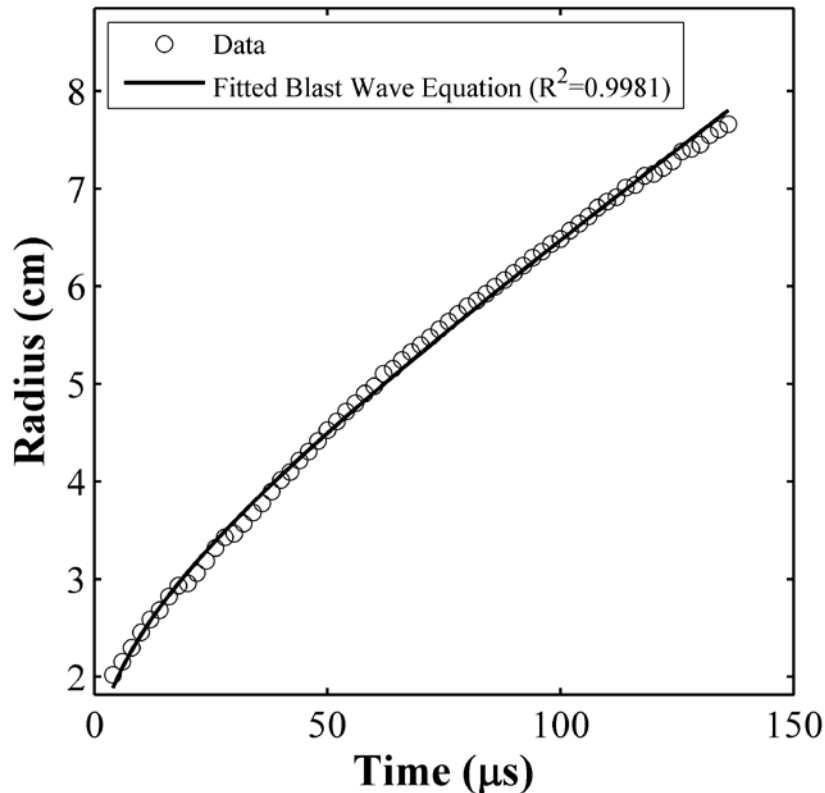
Image Results – particle motion

- Evidence of presumably unburned solid particles for several THKP tests repeating same conditions
- Lead to qualitative assessment of extent of reaction



Pressure results

$$\text{Dewey Blast Wave Eq.: } R = A + Ba_0t + C \ln(1 + a_0t) + D\sqrt{\ln(1 + a_0t)}$$



- Blast pressure is approximately 0.4 MPa at 2-3 cm radius

$t=0 \mu\text{s}$ corresponds to trigger time ($t=0 \mu\text{s} \approx t = 2 \text{ ms}$ after ignition)

- Pressures within device agree well
 - Burn rate data predicts $P > 200$ MPa at 2 ms
 - Combustion model predicts $P > 220$ MPa at 2 ms
- Pressure measured within device and external to device ($P = 0.4$ MPa) do not agree well
 - Lack of near-field, early-time data hinders direct comparison
 - Future work will pursue different triggering algorithm
- Strong correlation across all research efforts that pyrotechnic material is not completely consumed by combustion reaction
 - Unburned particles in images
 - Evidence of transition to unsteady burning mode in both other studies

Conclusions

- Presented data from three efforts aimed at improving understanding of pyrotechnic device behavior from within the device to the resulting multiphase flow output
- Consistent phenomena are suggested:
 - Generation of large pressures suitable for production of strong shock waves
 - Likelihood of steady-to-unsteady combustion mode transition within charge cavity of device leading to ejection of solid particles

Acknowledgments

The authors would like to thank the following individuals for their assistance with various aspects of these efforts:

- Mike Oliver
- Ian Kohl
- Ryan Marinis
- Duane Richardson
- Cody Love
- David Glaze
- Steve Kennon
- Mario Martinez
- Sam Subia
- Lindsey Erickson

Sandia is a multi-program laboratory operated by Sandia Corporation, a Lockheed Martin company, for the United States Department of Energy's National Nuclear Security Administration under contract No. DE-AC04-94AL85000. Approved for public release, SAND2015-2816C.