

Level-3 Consequence Analysis Part 1 Atmospheric Transport and Dispersion

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27 April – 1 May, 2015
Haiyang, China

Objectives

- Learn the mechanisms that describe
 - Atmospheric transport and dispersion
 - Wet and dry deposition

Processes That Affect a Released Contaminant

Plume transport mechanisms

- Buoyant plume rise
- Dilution and transport
- Dispersion
- Chemical reactions (not usually treated in a PSA)

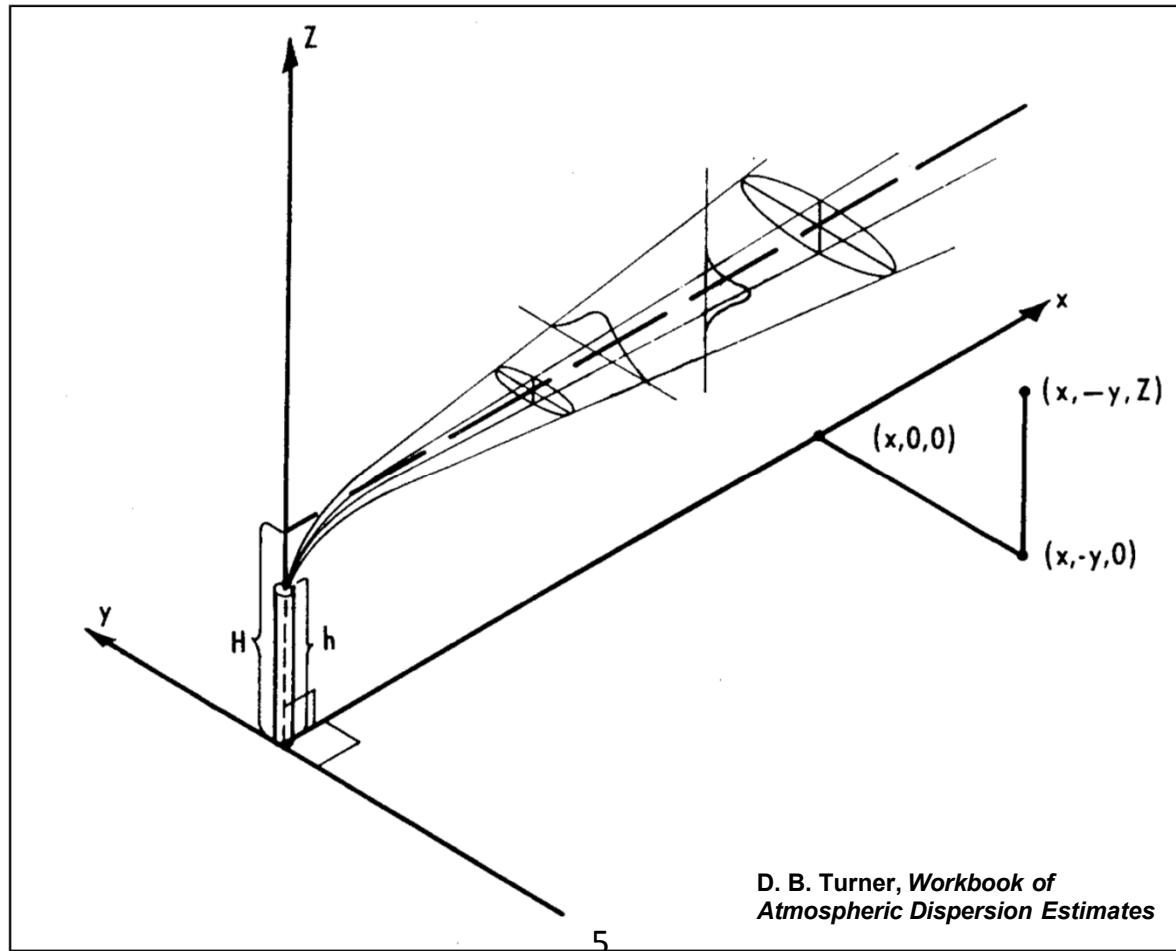
Plume depletion mechanisms

- Radioactive decay
- Wet deposition - rainout by interaction with cloud droplets and washout by falling precipitation
- Dry deposition – gradual loss of reactive vapors and aerosols by deposition onto the surface cover

Atmospheric Transport Inputs and Outputs

- Basic weather inputs
 - Wind speed
 - Wind direction
 - Atmospheric stability
 - Precipitation rate
- Basic outputs
 - Air concentrations
 - Surface deposition

Coordinate System for Atmospheric Transport and Dispersion



Basic Concentration Equation

- **Continuous release**
- **Point source**
- **No boundaries**

$$C = \frac{\dot{Q}}{2\pi\sigma_y\sigma_z u} \exp\left\{-\frac{1}{2}\left[\left(\frac{y}{\sigma_y}\right)^2 + \left(\frac{z}{\sigma_z}\right)^2\right]\right\}$$

C = Plume concentration (Bq/m³)

\dot{Q} = Release rate of contaminant (Bq/s)

y = Cross-wind (lateral) distance from plume centerline (m)

z = Vertical distance from plume centerline (m)

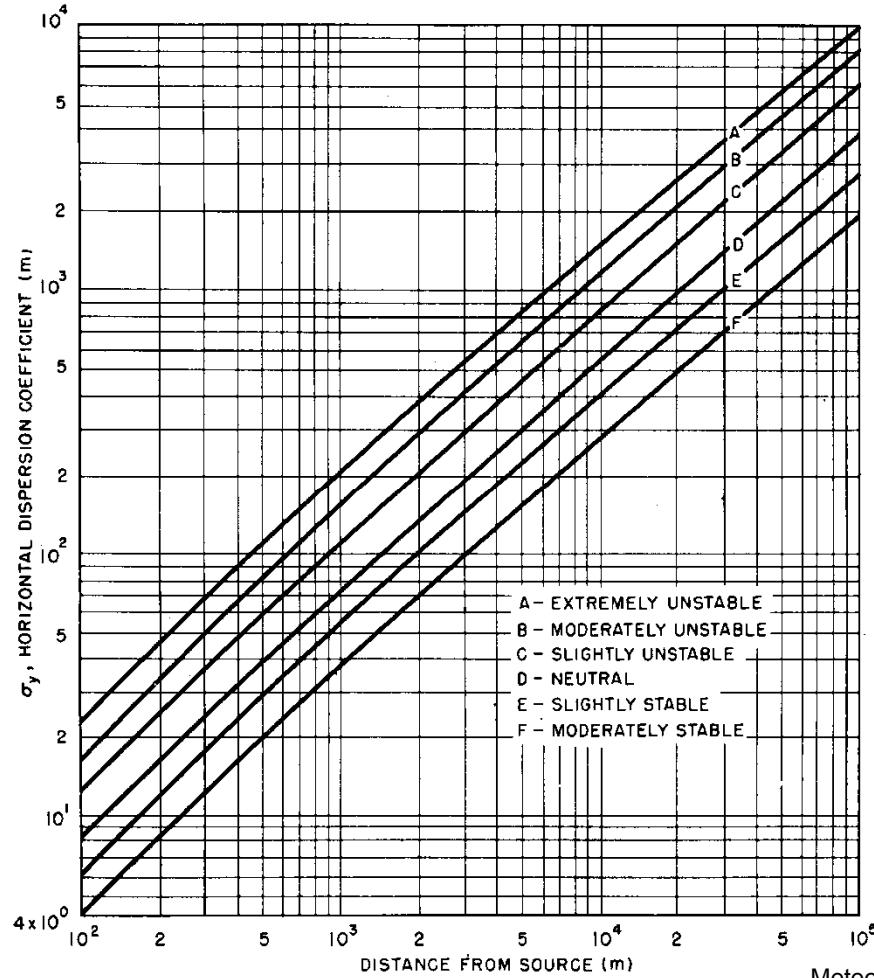
σ_y = Standard deviation of plume in the y direction as a function of x (m)

σ_z = Standard deviation of plume in the z direction as a function of x (m)

u = Average wind speed along plume centerline

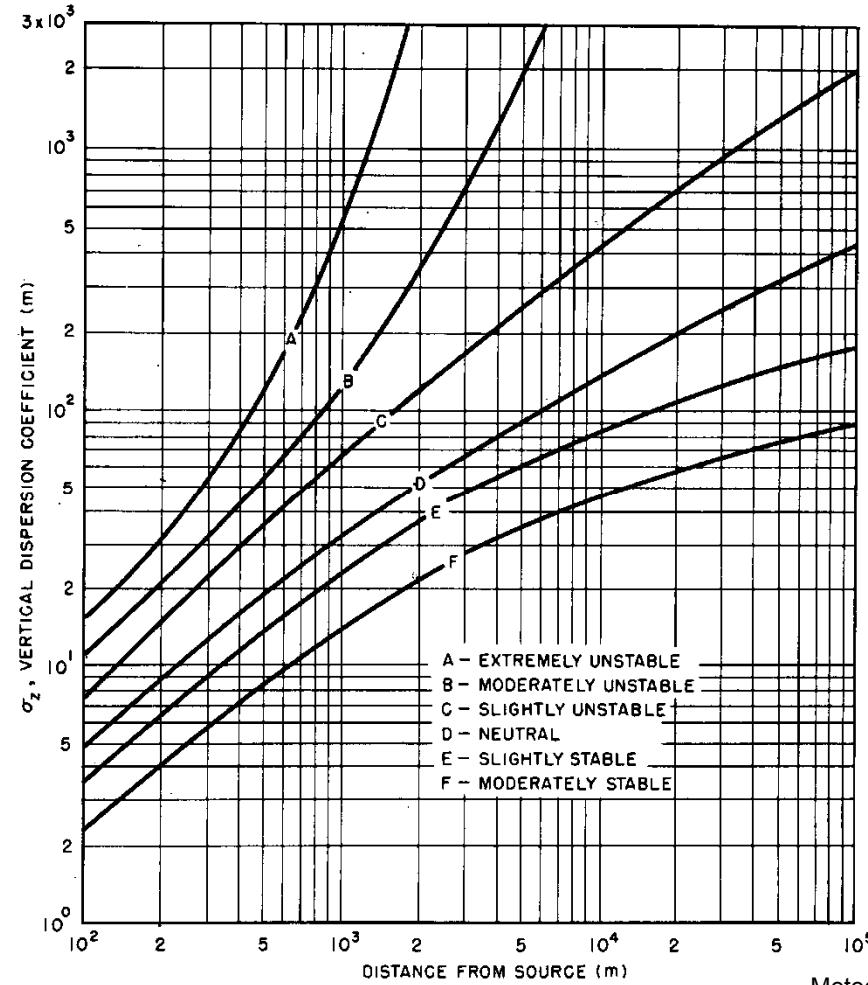
$$\frac{\int C dt}{\int Q dt} = \frac{\chi}{Q}$$

Lateral Dispersion, σ_y , vs. Downwind Distance From Source



Meteorology and Atomic Energy, 1968

Vertical Dispersion, σ_z , vs. Downwind Distance From Source (Pasquill-Gifford)



Meteorology and Atomic Energy, 1968

Power-Law Representation of Dispersion

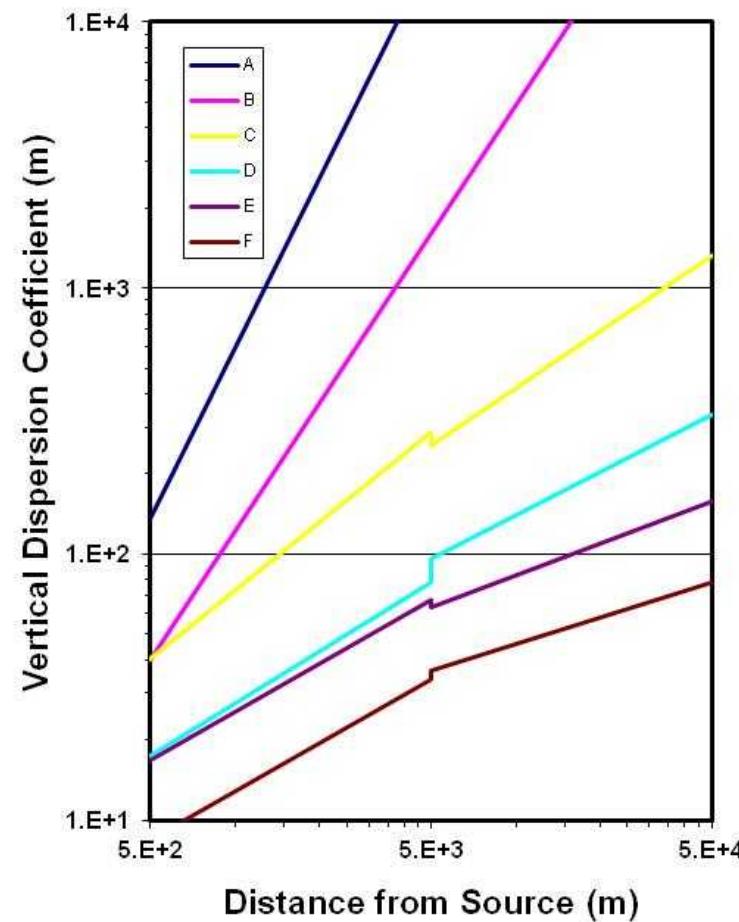
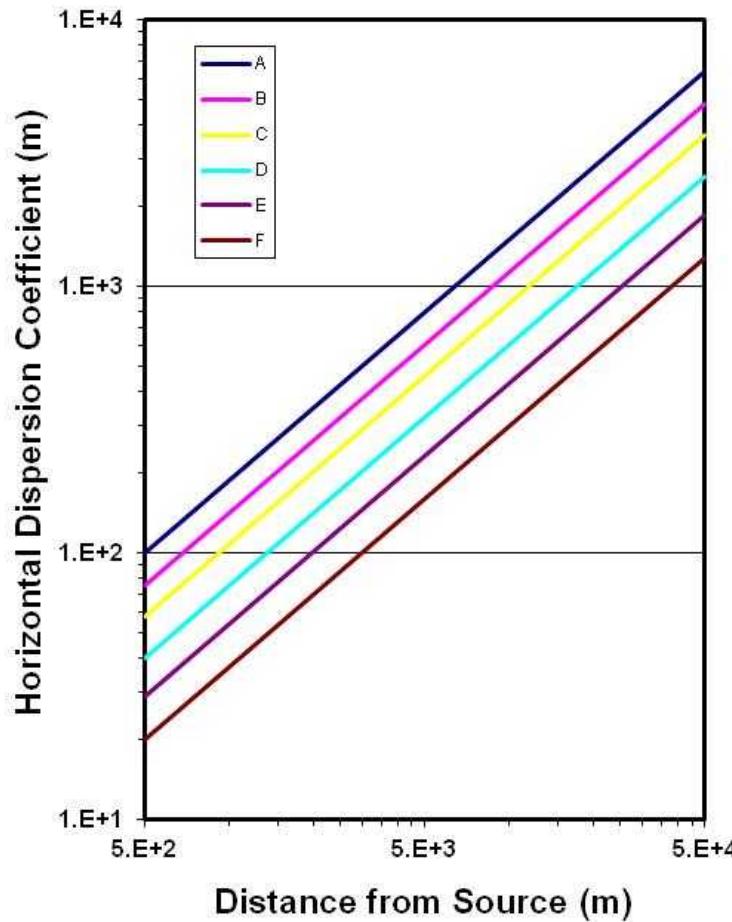
- Power-law representation

$$\sigma_y = a \cdot x^b \quad \sigma_z = c \cdot x^d$$

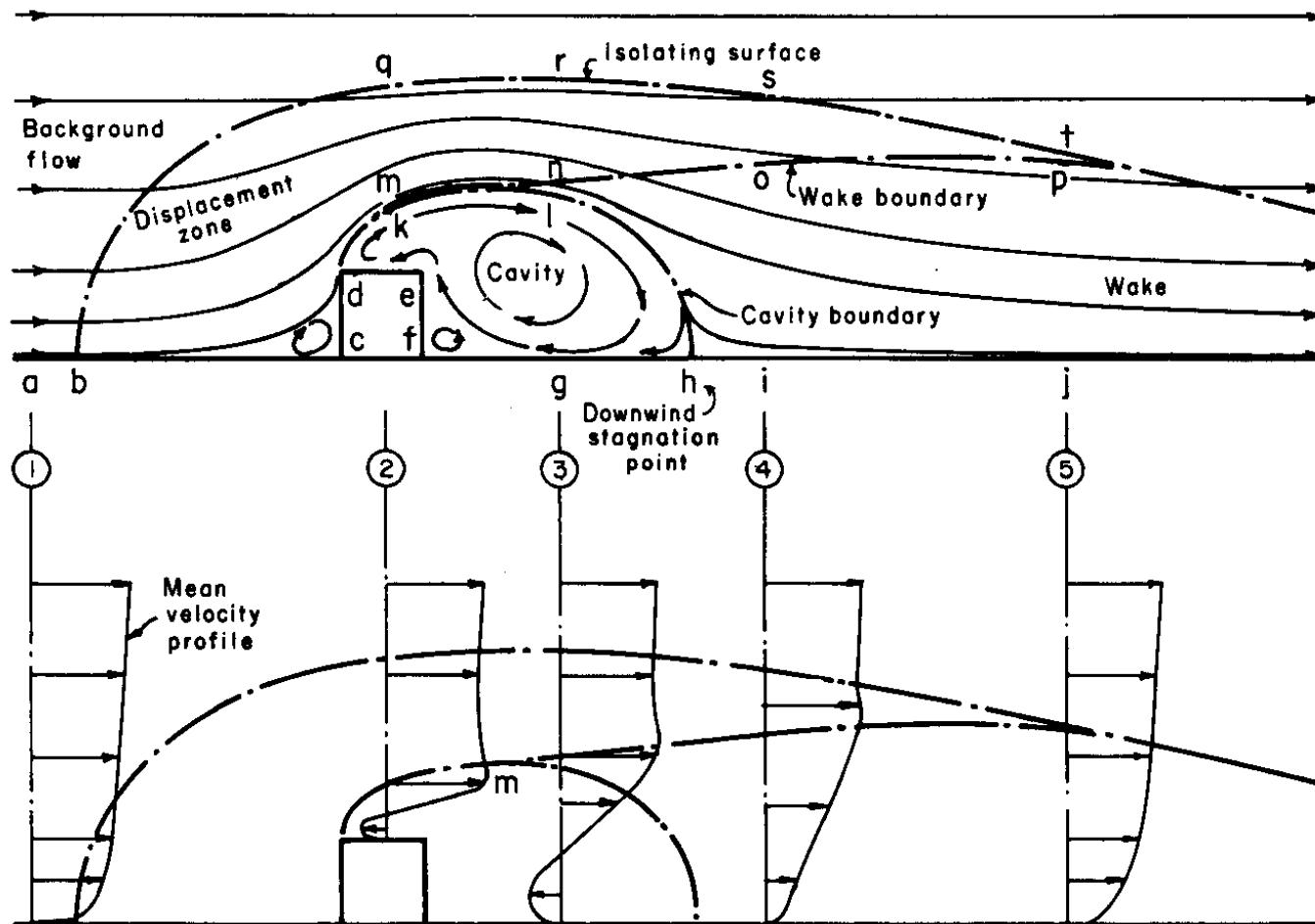
- Excellent representation for σ_y
- Two-piece, less accurate, representation for σ_z

Parameter	Range (km)	Distance						Stability Class					
		A	B	C	D	E	F	G	H	I	J	K	L
a	0.5 - 50	0.36580	0.2751	0.2089	0.1474	0.1046	0.0722	0.0500	0.0350	0.0250	0.0175	0.0125	0.0088
b	0.5 - 50	0.90310	0.9031	0.9031	0.9031	0.9031	0.9031	0.9031	0.9031	0.9031	0.9031	0.9031	0.9031
c	0.5 - 5	0.00025	0.0019	0.2000	0.3000	0.4000	0.2000	0.1474	0.1046	0.0722	0.0500	0.0350	0.0250
	5 - 50			0.5742	0.9605	2.1250	2.1820	1.6021	1.2500	0.9031	0.6021	0.4000	0.2000
d	0.5 - 5	2.12500	1.6021	0.8543	0.6532	0.6021	0.6020	0.7160	0.5409	0.3979	0.3310	0.2500	0.1750
	5 - 50			0.5742	0.9605	2.1250	2.1820	1.2500	1.0000	0.7000	0.5000	0.3000	0.2000

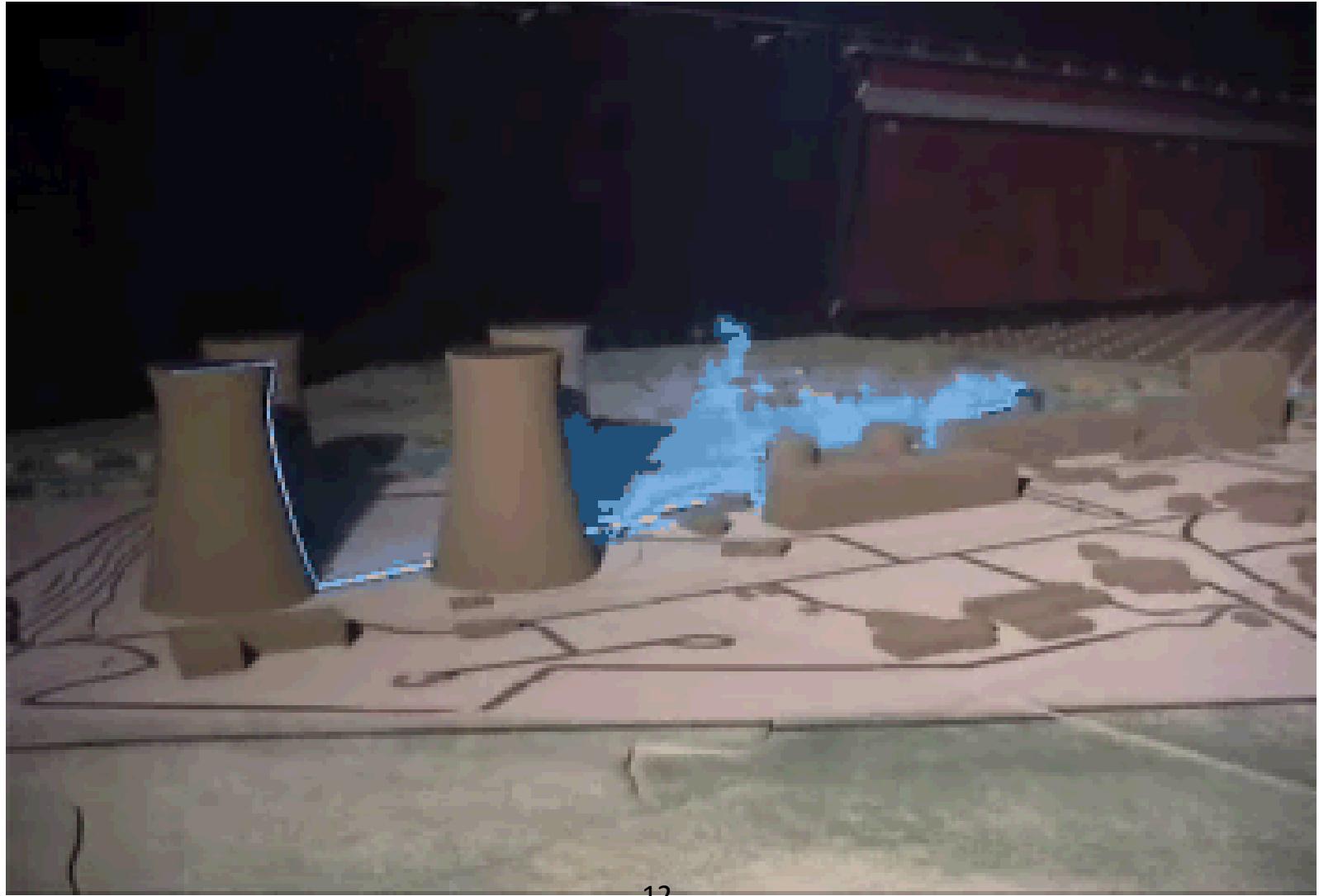
Plots of Power-Law Functions for Tadmor and Gur Parameters



General Arrangement of Flow Zones Near a Sharp-edged Building



Wind-Tunnel Test of Scaled Plant

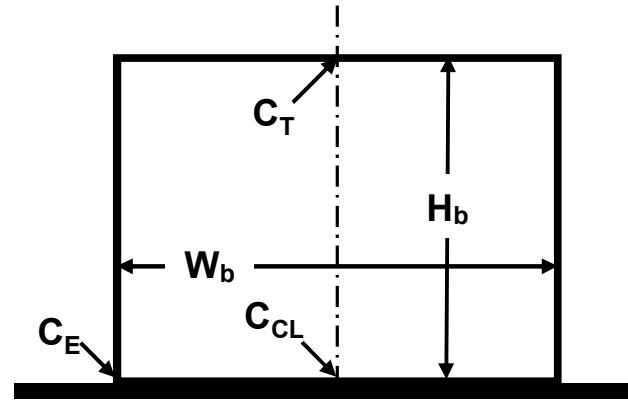


Building Wake - Area Source

- Assume fraction, f , of centerline concentration at building edge and top

$$f = \frac{C_E}{C_{CL}} = \exp\left(\frac{-(W_b/2)^2}{2\sigma_{y_0}^2}\right)$$

$$f = \frac{C_T}{C_{CL}} = \exp\left(\frac{-H_b^2}{2\sigma_{z_0}^2}\right)$$

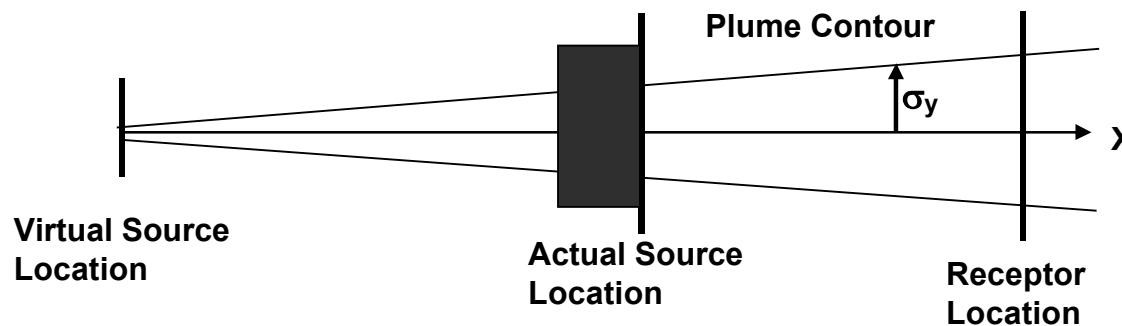


For $f = 0.1$, $\sigma_{y_0} = 0.23 W_b$ and $\sigma_{z_0} = 0.47 H_b$

Where W_b and H_b are the width and height of the building, respectively

Virtual Sources

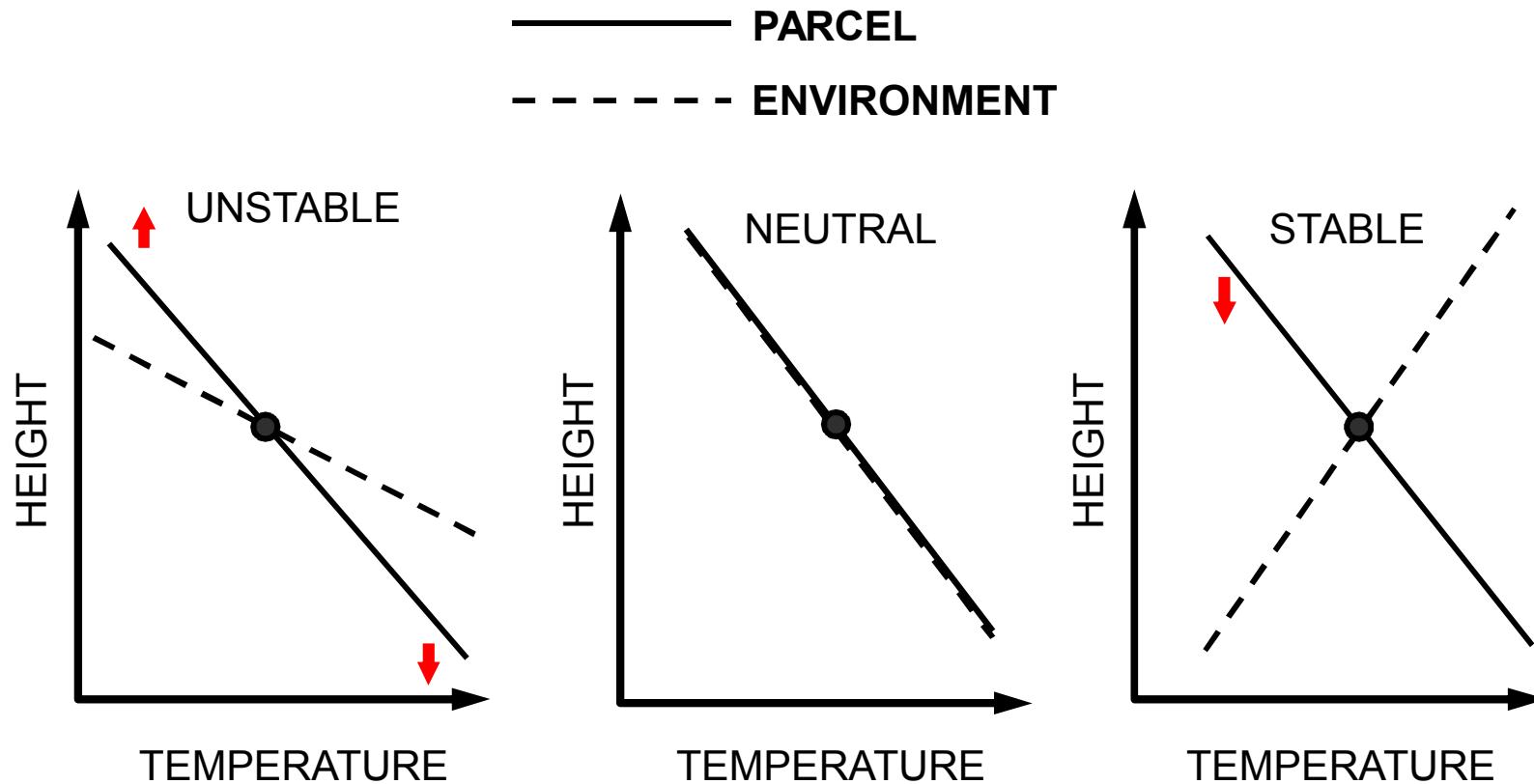
- Virtual source is the location of a “point” source that produces an equivalent plume size
- Actual source location corresponds to a finite distance downwind from the virtual source
 - X_{y0} for crosswind dispersion
 - X_{z0} for vertical dispersion
- Receptor locations are relative to actual source location



Planetary Boundary Layer

- Region of atmosphere between earth's surface and an upper region of nonturbulent, geostrophic flow
- Ranges in height from 50 m – height of troposphere (10 to 18 km)
- Consists of three parts
 - Surface layer (first 10%, turbulence is created)
 - Core (up to 70% of PBL, turbulence is dissipated)
 - Top (remainder)
- Principal types are convective and stably stratified
- Wind speed and direction tend to vary with height in surface layer
- Stability of atmosphere within PBL determines turbulence intensity (dispersion effects)
- Radioactive materials are assumed to be trapped in this layer
- Here we assume it is the same as the mixing layer

Illustrations of PBL Stability Conditions



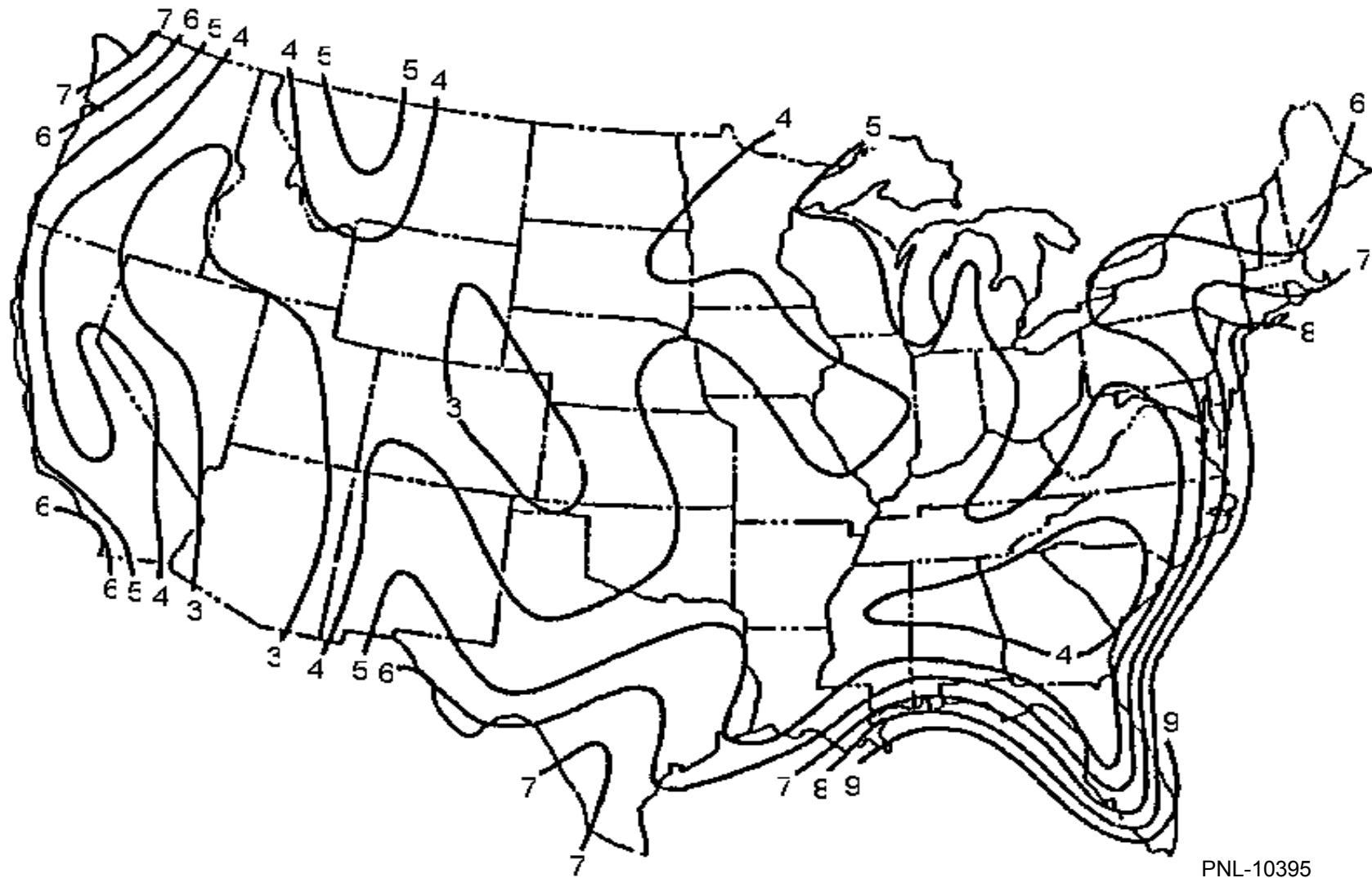
Atmospheric Stability Classifications by Vertical Temperature Gradient (Lapse Rate)

Stability classification	Pasquill categories	Temperature change with height ($^{\circ}\text{C}/100 \text{ m}$)
Extremely unstable	<i>A</i>	$\Delta T/\Delta z \leq -1.9$
Moderately unstable	<i>B</i>	$-1.9 < \Delta T/\Delta z \leq -1.7$
Slightly unstable	<i>C</i>	$-1.7 < \Delta T/\Delta z \leq -1.5$
Neutral	<i>D</i>	$-1.5 < \Delta T/\Delta z \leq -0.5$
Slightly stable	<i>E</i>	$-0.5 < \Delta T/\Delta z \leq 1.5$
Moderately stable	<i>F</i>	$1.5 < \Delta T/\Delta z \leq 4.0$
Extremely stable	<i>G</i>	$4.0 < \Delta T/\Delta z$

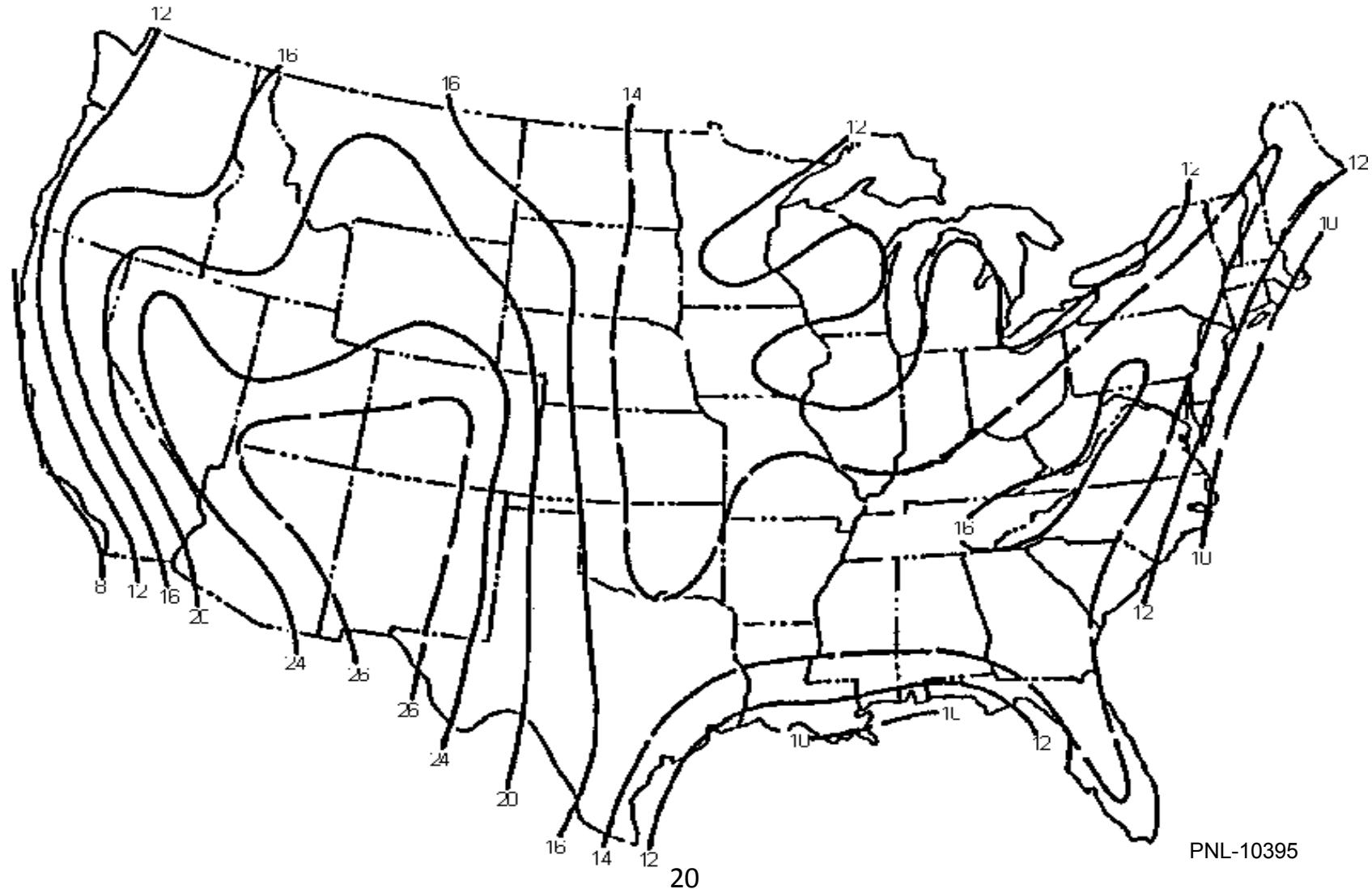
Mixing Height

- Mixing height is usually determined by
 - Thermal mixing (convection) during daytime
 - Mechanical mixing during nighttime
- Varies continuously (hour to hour, day to day, season to season)
- Usually lowest at night and early morning
- Usually highest in afternoon
- Inhibits plume rise (we assume that it is an absolute barrier)

Mean Annual Morning Mixing Heights (m x 10²)



Mean Annual Afternoon Mixing Heights (m x 10²)



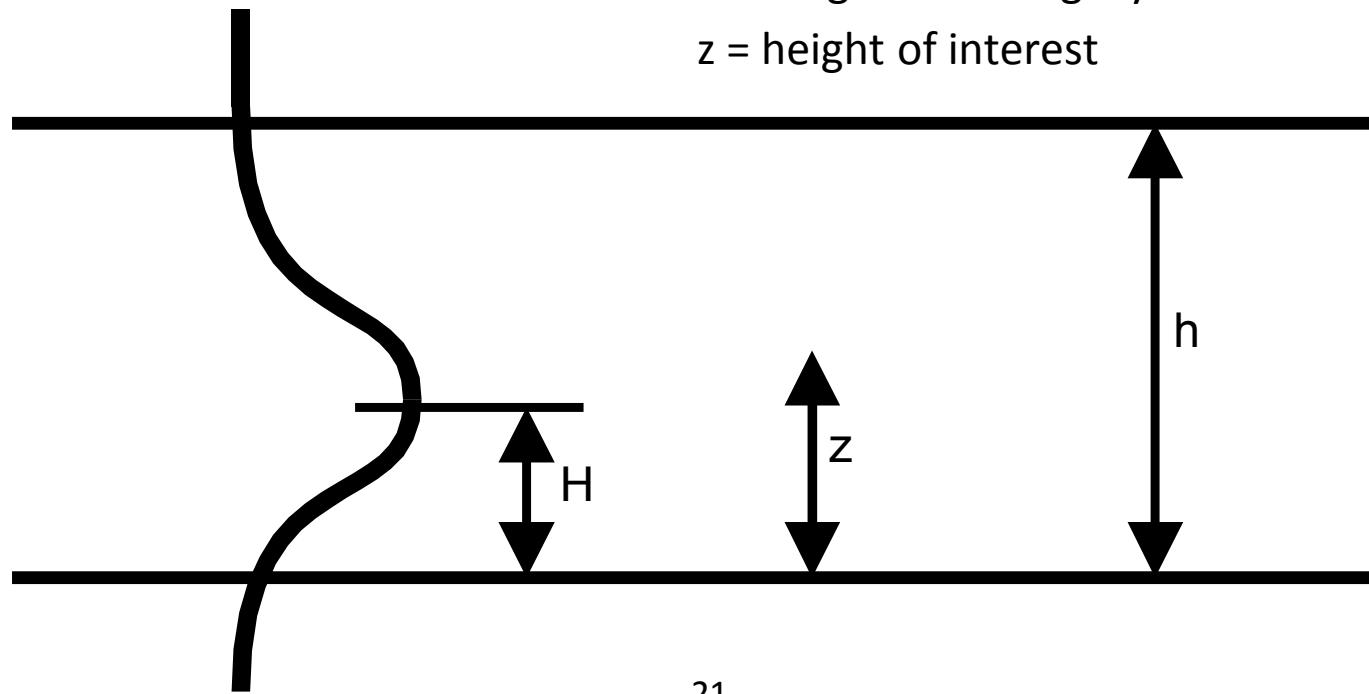
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Vertical Boundaries Ground and Mixing Layer

H = release height (or lofting height) above ground

h = height of mixing layer

z = height of interest



General Gaussian Plume Equation With Reflective Boundaries

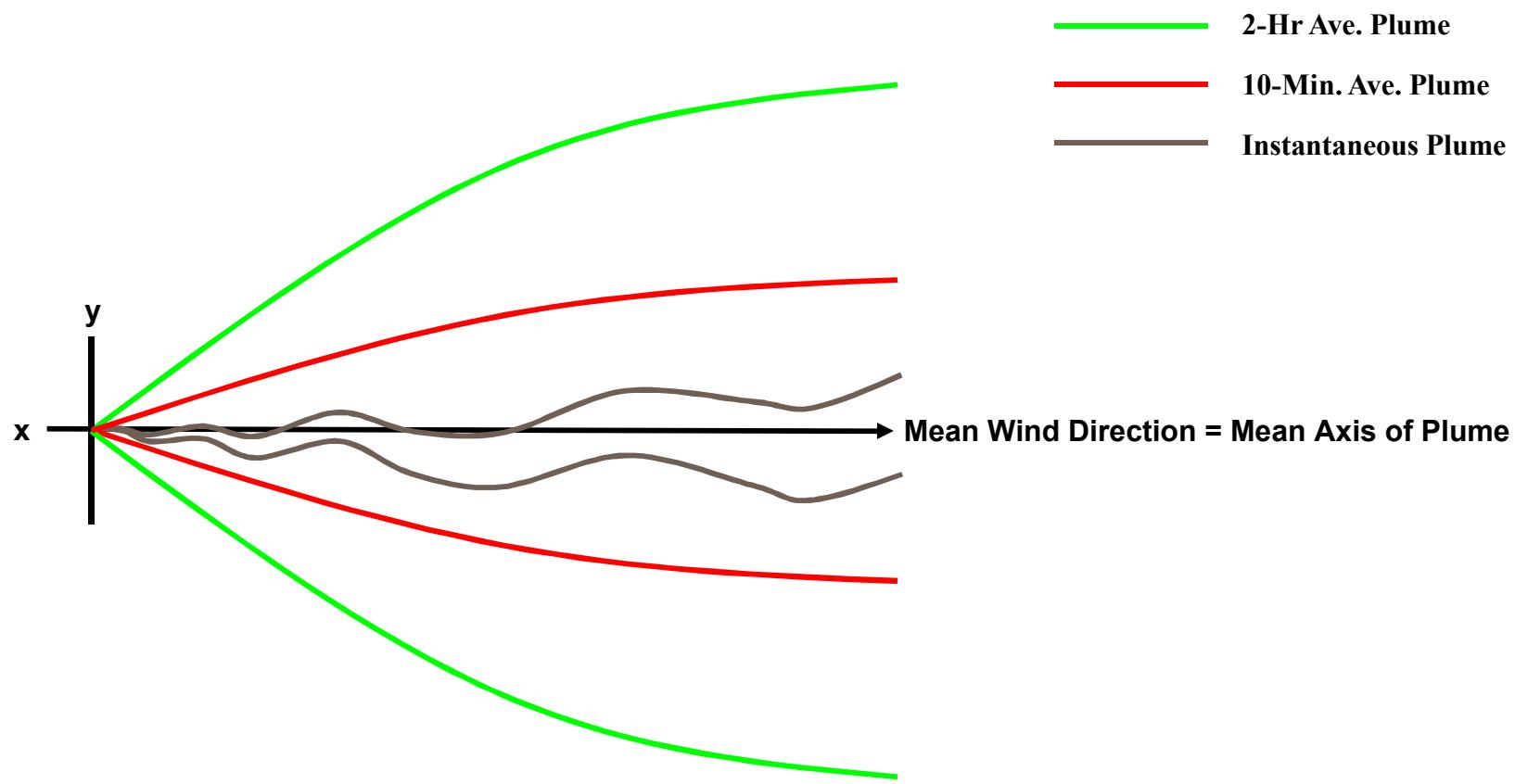
- Account for material that would have been lost through boundaries

$$C = \frac{\dot{Q}}{2\pi\sigma_y\sigma_z u} \exp\left(\frac{-y^2}{2\sigma_y^2}\right) \sum_{n=-\infty}^{\infty} \left\{ \exp\left[-\frac{1}{2}\left(\frac{2nh - H - z}{\sigma_z}\right)^2\right] + \exp\left[-\frac{1}{2}\left(\frac{2nh + H - z}{\sigma_z}\right)^2\right] \right\}$$

- Simplified equation when release is at ground level and observation point is on plume centerline ($H = y = z = 0$)

$$C = \frac{\dot{Q}}{2\pi\sigma_y\sigma_z u} \sum_{n=-\infty}^{\infty} 2 \exp\left[-2\left(\frac{nh}{\sigma_z}\right)^2\right]$$

Effect of Diffusion Times – Plume Meander



Original MACCS2 Plume Meander

- Increases effective plume spread in y direction
- Effect of plume meander continues downwind indefinitely

$$\sigma_{y, m} = \sigma_y \left(\frac{\Delta t}{\Delta t_{ref}} \right)^m$$

Δt = Release duration (s)

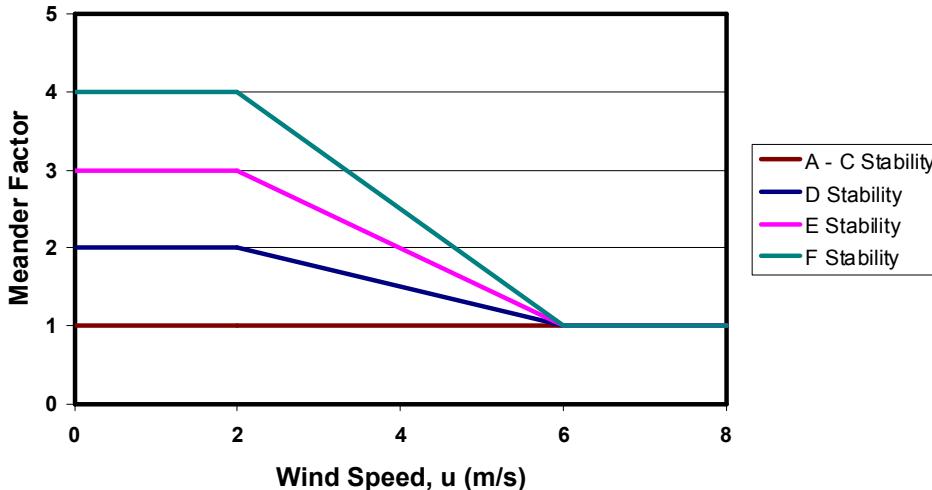
Δt_{ref} = 600, the experimental duration of the Prairie Grass tests (s)

m = an empirical exponent

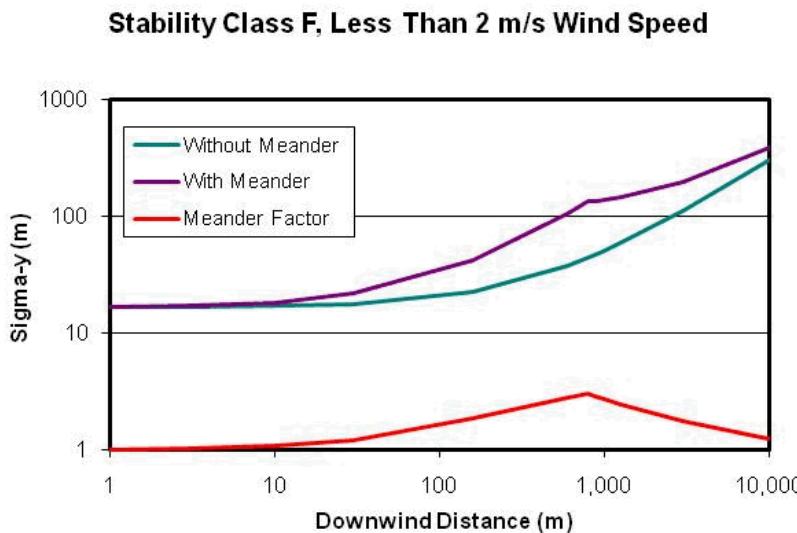
= 0.2 when $\Delta t < 1$ hr

= 0.25 when $\Delta t > 1$ hr

Regulatory Guide 1.145 Plume Meander Model



- Meander factor depends on stability class and wind speed
- Model is based on a 1-hr plume duration
- Effect of plume meander diminishes beyond 800 m from source
- Plot shows
 - Dispersion not accounting for plume meander
 - Dispersion accounting for plume meander (<2 m/s and F stability)
 - Effective meander factor



Plume Rise

- Earlier Briggs' model is used to estimate plume rise
 - Near-field trajectory (used for stability classes A – D)

$$\Delta H(x) = \frac{1.6(Fx)^2}{\bar{u}}^{1/3}$$

- Final rise for stability classes A – D

$$\Delta H_f = 38.7 \frac{F}{\bar{u}}^{0.60} \quad \text{when } F \geq 55$$

$$\Delta H_f = 21.4 \frac{F}{\bar{u}}^{0.75} \quad \text{when } F < 55$$

- Final rise for stability classes E – F

$$\Delta H_f = 2.4 \left(\frac{F}{\bar{u} s} \right)^{1/3}$$

Plume Trapping in Building Wake

- Plume is trapped in building wake when

$$u > \left(\frac{9.09F}{H_b} \right)^{1/3}$$

Where H_b is the building height (m)

F is the buoyancy flux defined previously (m^4/s^3)

u is wind speed (m/s)

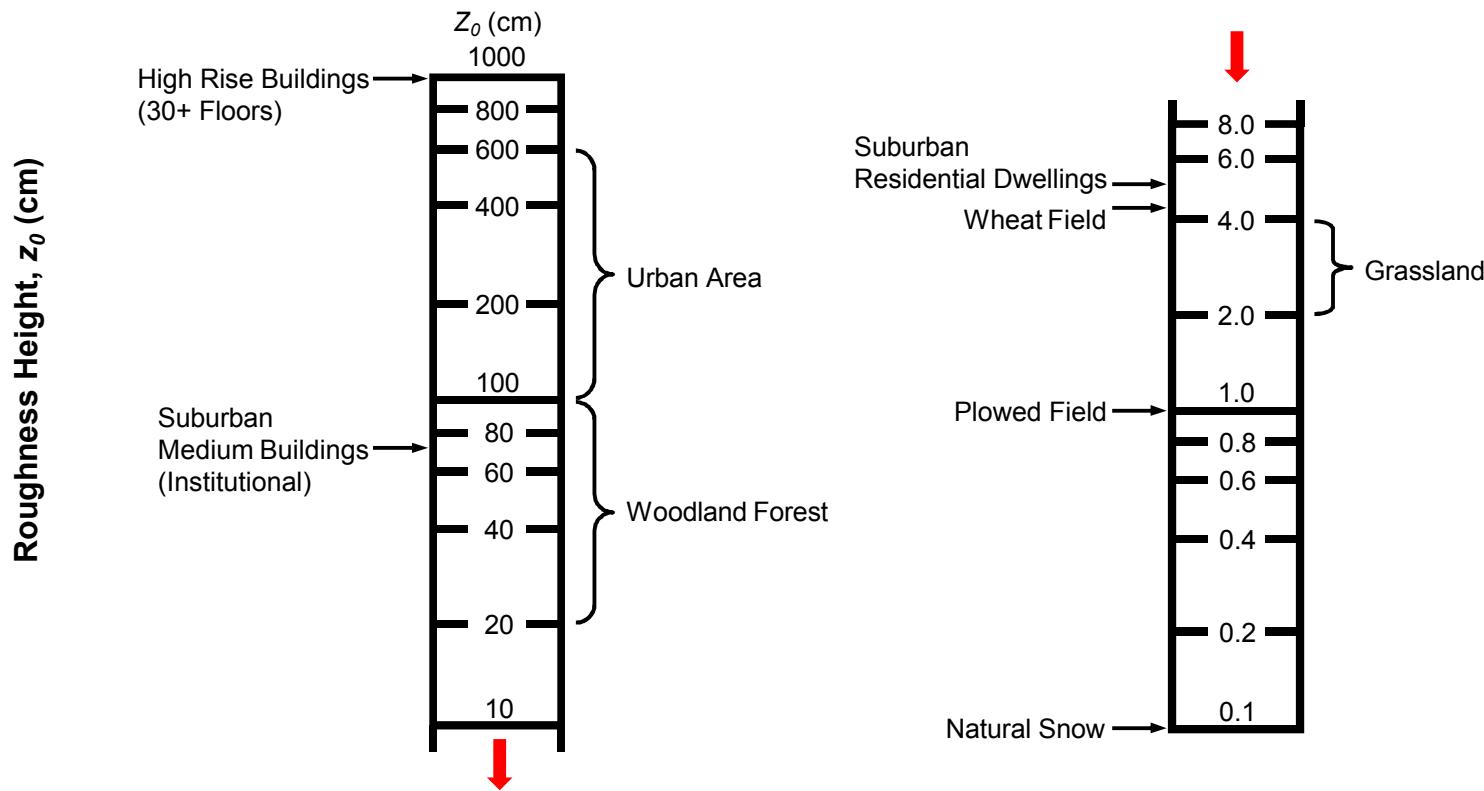
- A trapped plume is
 - Released at the level of the initial release point

Roughness Length, z_0

- Function of size and spacing of roughness elements
- Dependent on the frontal area of the average element (facing the wind) divided by the ground width it occupies
- A lower roughness length implies less momentum exchange between the surface and the atmosphere
- σ_z measured over flat terrain during Prairie Grass tests ($z_0 = 3$ cm)

$$\sigma_z = \sigma_{z, PG} \left(\frac{z_0}{3} \right)^{0.2}$$

Roughness Lengths for Various Surfaces



Workshop Example 1 – Pasquill-Gifford Chart

For a 30 minute release from this building (assume dimensions of 200 ft. high by 120 ft. wide) of 1 Ci of ^{137}Cs , what is the maximum ground concentration 1/2 mile downwind and at the mall (8 miles downwind). Assume worst case conditions.

Assumptions:

Worst Case - Wind blowing directly towards mall

Concentration at plume centerline ($y = z = H = 0$)

Low wind speed ($u = 1 \text{ m/s}$; may not be worst case for short half lives)

Minimize atmospheric dispersion; stability = F

Heat low enough so that no plume rise

Other - Converting dimensions of interest:

1/2 mi \sim 800m

8 mi \sim 13000m

Building height = 200ft \sim 60m

Building width = 120ft \sim 37m

Roughness length (z_0) = 100cm (suburban/urban)

WORKSHOP EXAMPLE 1 (cont.)

Meander (5-26): $\sigma_{y,m} = \sigma_y \left(\frac{30}{10} \right)^{0.2} = 1.25\sigma_y$

Roughness (5-32): $\sigma_{z,z_0} = \sigma_z \left(\frac{100}{3} \right)^{0.2} = 2.0\sigma_z$

Building Wake (5-15): $\sigma_{y_0} = .23(37) = 8.6m$
 $\sigma_{z_0} = .47(60) = 28m$

Mixing Height: Morning = 550m (worst case meteorologically)
(5- 21, 5-22) Afternoon = 1500m (worst case because most people at mall)

WORKSHOP EXAMPLE 1 (cont.)

from (5-9) and (5-10)

Receptor Distance (m)	σ_y (m)	σ_z (m)
	$8.6/1.25 = 6.9 \Rightarrow X_{y_0} = 180$	$28/2.0 = 14 \Rightarrow X_{z_0} = 1100$
800	$39 (@ X = 800 + 180) * 1.25 = 49$	$21 (@ X = 800 + 1100) * 2 = 42$
13000	$390 (@ X = 13000 + 180) * 1.25 = 490$	$53 (@ X = 13000 + 1100) * 2 = 106$

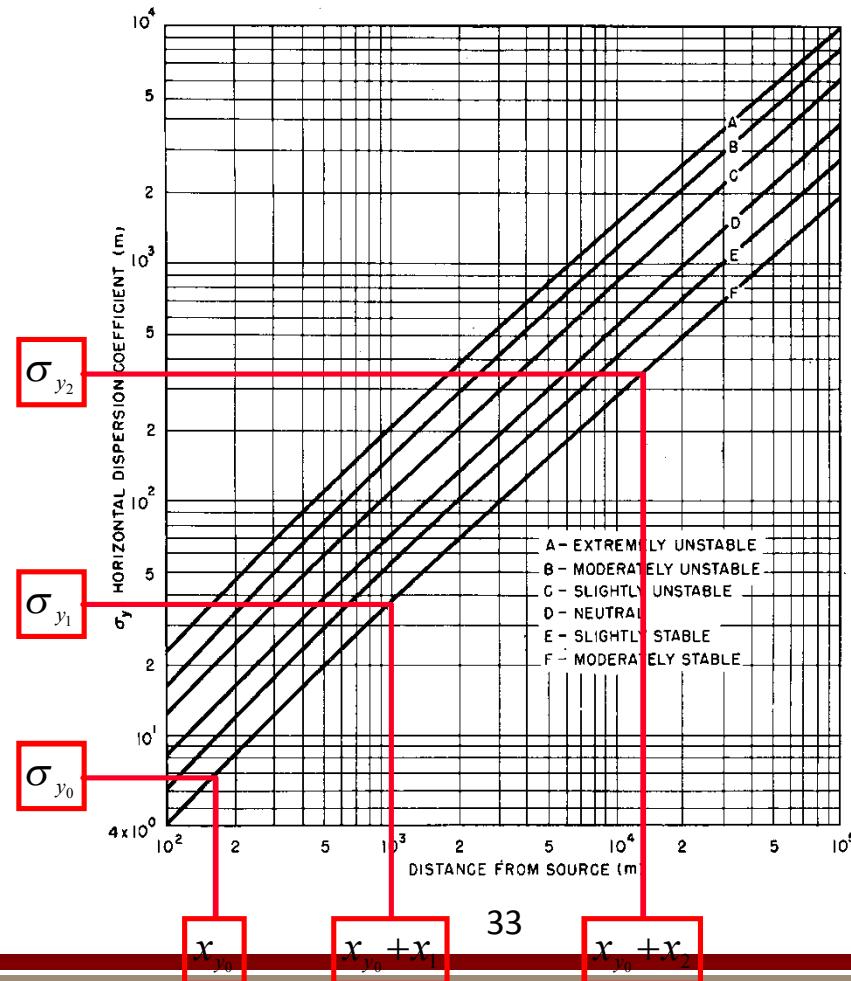
Series Terms (5-24):

$$\sum_{n=-\infty}^{\infty} 2e^{\left[-2\left(\frac{n1500}{\sigma_z}\right)^2\right]} \quad \begin{matrix} Z=0 \\ H=0 \end{matrix}$$

$\sigma_z \backslash n$	0	-1	+1
42	2	0	0
106	2	0	0

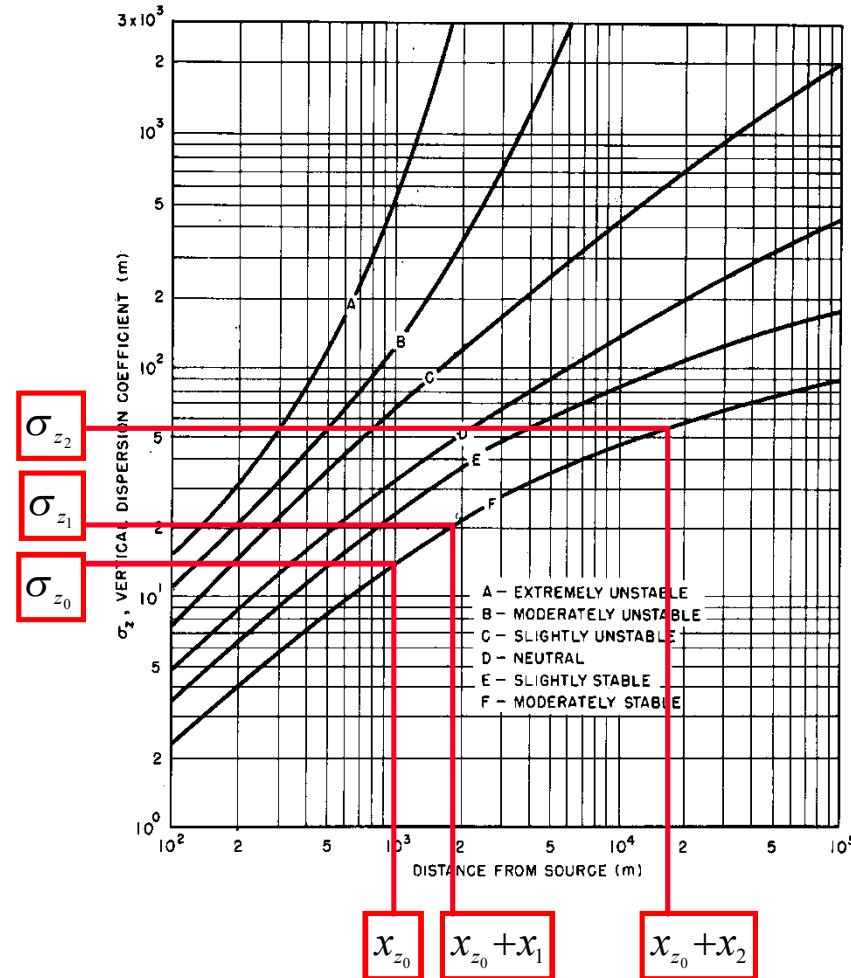
WORKSHOP EXAMPLE 1 (cont.)

Lateral Dispersion (5-9), σ_y , vs. Downwind Distance From Source for Pasquill's Stability Classes



WORKSHOP EXAMPLE 1 (cont.)

Vertical Dispersion (5-10), σ_z , vs. Downwind Distance From Source for Pasquill's Stability Classes



WORKSHOP EXAMPLE 1 (cont.)

(5-24)

1/2 mile

$$\frac{C}{Q} = \frac{1}{2\pi(49)(42)(1)}(2) = 1.6 \times 10^{-4} \frac{\text{sec}}{\text{m}^3}$$

8 miles

$$= \frac{1}{2\pi(490)(106)(1)}(2) = 6.1 \times 10^{-6} \frac{\text{sec}}{\text{m}^3}$$

$$C = 1.6 \times 10^{-4} \frac{\text{sec}}{\text{m}^3} \times \frac{1 \text{ curie}}{1800 \text{ sec}} = 8.9 \times 10^{-8} \frac{\text{curie}}{\text{m}^3}$$

$$= 6.1 \times 10^{-6} \frac{\text{sec}}{\text{m}^3} \times \frac{1 \text{ curie}}{1800 \text{ sec}} = 3.4 \times 10^{-9} \frac{\text{curie}}{\text{m}^3}$$

C = Inversely proportional to $\sigma_y \cdot \sigma_z$ (plume centerline, no reflections, no decay)

dist	$\sigma_y \cdot \sigma_z$	$C/C_{0.5 \text{ mi}}$
0.5 mi	(39) (21)	1
8 mi	(390) (53)	1/25
50 mi	(1700) (87)	1/180

Workshop Example 1 – Tadmor and Gur Parameters

For a 30 minute release from this building (assume dimensions of 200 ft. high by 120 ft. wide) of 1 Ci of ^{137}Cs , what is the maximum ground concentration 1/2 mile downwind and at the mall (8 miles downwind). Assume worst case conditions.

Assumptions:

Worst Case - Wind blowing directly towards mall

Concentration at plume centerline ($y = z = H = 0$)

Low wind speed ($u = 1\text{m/s}$; may not be worst case for short half lives)

Minimize atmospheric dispersion; stability = F

Heat low enough so that no plume rise

Other - Converting dimensions of interest:

$1/2\text{ mi} \sim \underline{800\text{m}}$

$8\text{ mi} \sim \underline{13000\text{m}}$

Building height = 200ft $\sim \underline{60\text{m}}$

Building width = 120ft $\sim \underline{37\text{m}}$

Roughness length (z_0) = 100cm (suburban/urban)

WORKSHOP EXAMPLE 1 – T&G (cont.)

Meander:
$$\sigma_{y,m} = \sigma_y \left(\frac{30}{10} \right)^{0.2} = 1.25\sigma_y$$

Roughness:
$$\sigma_{z,z_0} = \sigma_z \left(\frac{100}{3} \right)^{0.2} = 2.0\sigma_z$$

Building Wake:
$$\sigma_{y_0} = .23(37) = 8.6m$$

$$\sigma_{z_0} = .47(60) = 28m$$

Mixing Height: Morning = 550m (worst case meteorologically)
Afternoon = 1500m (worst case because most people at mall)

WORKSHOP EXAMPLE 1 – T&G (cont.)

from (5-11)

Parameter	Distance Range (km)	Stability Class					
		A	B	C	D	E	F
a	0.5 - 50	0.36580	0.2751	0.2089	0.1474	0.1046	0.0722
b	0.5 - 50	0.90310	0.9031	0.9031	0.9031	0.9031	0.9031
c	0.5 - 5	0.00025	0.0019	0.2000	0.3000	0.4000	0.2000
	5 - 50			0.5742	0.9605	2.1250	2.1820
d	0.5 - 5	2.12500	1.6021	0.8543	0.6532	0.6021	0.6020
	5 - 50			0.7160	0.5409	0.3979	0.3310

Receptor Distance (m)	$\sigma_y(m)$	$\sigma_z(m)$
Initial Virtual Source Distance	$8.6 = 1.25 \cdot 0.0722 \cdot x^{0.9031}$ $x = 155$	$28 = 2.0 \cdot 0.2000 \cdot x^{0.6020}$ $x = 1160$
800 m	$1.25 \cdot 0.0722 \cdot (155 + 800)^{0.9031}$ $= 44$	$2.0 \cdot 0.2000 \cdot (1160 + 800)^{0.6020}$ $= 38$
5000 m	$1.25 \cdot 0.0722 \cdot (155 + 5000)^{0.9031}$ $= 203$	$2.0 \cdot 0.2000 \cdot (1160 + 5000)^{0.6020}$ $= 76$

WORKSHOP EXAMPLE 1 – T&G (cont.)

Distance (m)	σ_y (m)	σ_z (m)
Virtual Source Distance @ 5000 m	$203 = 1.25 \cdot 0.0722 \cdot x^{0.9031}$ $x = 5155 - 5000 = 155$	$76 = 2.0 \cdot 2.1820 \cdot x^{0.3310}$ $x = 5712 - 5000 = 712$
13,000	$1.25 \cdot 0.0722 \cdot (155 + 13000)^{0.9031}$ $= 474$	$2.0 \cdot 2.1820 \cdot (712 + 13000)^{0.3310}$ $= 102$

Reflections:

$$\sum_{n=-\infty}^{\infty} 2e^{-2\left(\frac{n \times 1500}{\sigma_z}\right)^2} \quad Z=0 \quad H=0$$

		n		
		0	-1	+1
σ_z	38	2	0	0
	124	2	0	0

WORKSHOP EXAMPLE 1 – T&G (cont.)

1/2 mile

$$C/\dot{Q} = \frac{2}{2\pi(44\text{ m})(38\text{ m})(1\frac{\text{m}}{\text{s}})} = 1.8 \times 10^{-4} \text{ s/m}^3$$

8 miles

$$C/\dot{Q} = \frac{2}{2\pi(474\text{ m})(102\text{ m})(1\frac{\text{m}}{\text{s}})} = 6.6 \times 10^{-6} \text{ s/m}^3$$

$$C = 1.8 \times 10^{-4} \frac{\text{s}}{\text{m}^3} \times \frac{1\text{ Ci}}{1800\text{ s}} = 1.0 \times 10^{-7} \frac{\text{Ci}}{\text{m}^3}$$

$$C = 6.6 \times 10^{-6} \frac{\text{s}}{\text{m}^3} \times \frac{1\text{ Ci}}{1800\text{ s}} = 3.7 \times 10^{-9} \frac{\text{Ci}}{\text{m}^3}$$

Workshop Exercise 1

- For a two hour ground level release in the morning of 10 curies of ^{132}I (half-life = 2.3 hours) containing one-half million Btu (147 KW-hr) heat content from a building which is 38.3 meters high and 56.5 meters wide located in a rural area of central Kentucky, what is the concentration of iodine that would be inhaled by a farmer standing in his plowed field 5.67 miles (9100 meters) downwind? Measurements on a met tower near the release indicate a typical day of 4 m/sec wind speed; the temperature at the 10-meter (height) sensor is 0.6 deg F (0.33 deg C) higher than that at the 30-meter sensor.
- Part 2: What concentration would the farmer see if the PBL were moderately stable?
- Part 3: Moderately stable with a wind speed of 1 m/sec?

Deposition Processes

- Dry Deposition
 - Impaction
 - Diffusion (Brownian motion)
 - Gravitational settling
- Wet Deposition
 - Scavenging by precipitation (washout)
 - Scavenging by cloud droplets (rainout)

Dry Deposition

- **Continuous and slow**

$$D = CV_d \Delta t$$

D = dry deposition (ground concentration) (Bq/m²)

C = near-surface air concentration (Bq/m³)

V_d = deposition velocity (m/s)

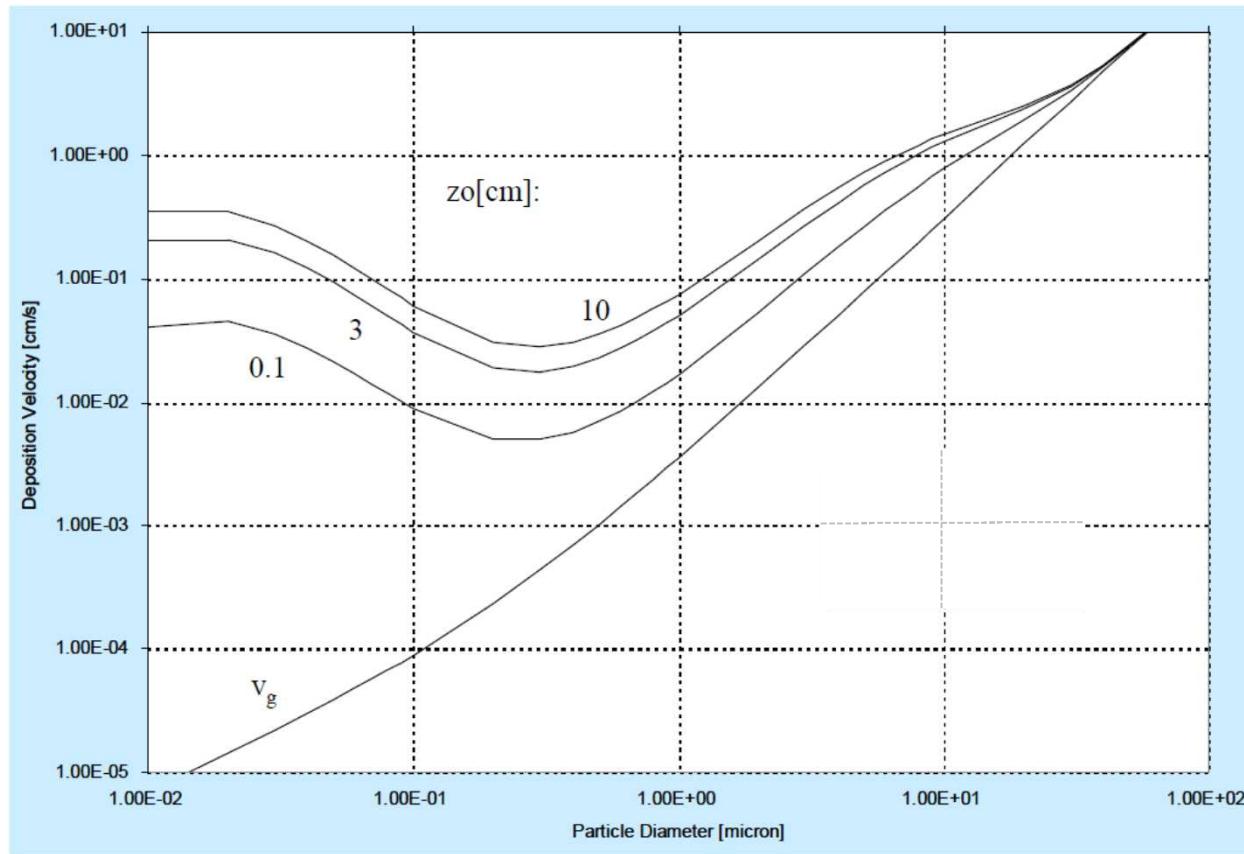
Δt = plume residence time (s)

- **Approximate formula for deposition losses**

$$\frac{Q}{Q_0} = \exp\left(-\frac{V_d \Delta t}{\bar{z}}\right) \quad \bar{z} = \sqrt{\frac{\pi}{2}} \left(\frac{\sigma_z}{\Sigma}\right)$$

Where Q is the material suspended in the plume (Bq) and Σ represents the summation term in the expression for σ_z (p. 5-24).

Average Deposition Velocities (cm/s)



Wet Deposition

- Discontinuous (precipitation events)
- Rapid (relative to dry)
 - Λ = scavenging or washout rate (1/s)
 - Λ = function of precipitation type and rate, saturation conditions, contaminant characteristics

$$\frac{dQ}{dt} = -\Lambda Q \quad ; \quad \frac{Q}{Q_0} = e^{-\Lambda \cdot \Delta t} \quad \Delta t = \text{duration of precipitation (s)}$$

$$\Lambda = aI^b$$

Λ = scavenging rate (1/s)

I = precipitation rate (mm/hr)

$$a = 9.5 \times 10^{-5}$$

$$b = 0.8$$

Workshop Exercise 2 (Deposition)

- For the release of ^{137}Cs analyzed in the workshop example, what is the deposition (Ci/m^2) one-half mile downwind and at the mall?
- Assumptions (same as workshop example):
 - No rain
 - $V_d = 1 \text{ cm/sec}$
- How much of the plume would have deposited prior to the mall if it had been raining steadily throughout the plume's path at a rate of 1 inch/hour?

References

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- E. D. Gorham, et al., “Evaluation of Severe Accident Risks: Methodology for the Containment, Source Term, Consequence, and Risk Integration Analyses,” NUREG/CR-4551, Vol.. 1, Rev. 1, Dec. 1993.
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