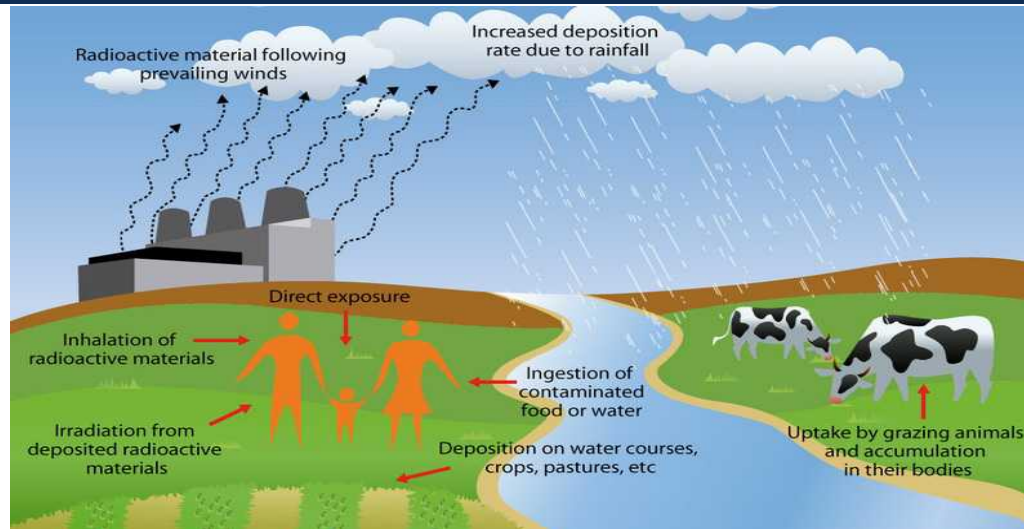


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Level-3 Consequence Analysis Part 1 Atmospheric Transport and Dispersion

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Haiyang, China

Objectives

- Learn the mechanisms that describe
 - Atmospheric transport and dispersion
 - Wet and dry deposition

Processes That Affect a Released Contaminant

Plume transport mechanisms

- Buoyant plume rise
- Dilution and transport
- Dispersion
- Chemical reactions (not usually treated in a PSA)

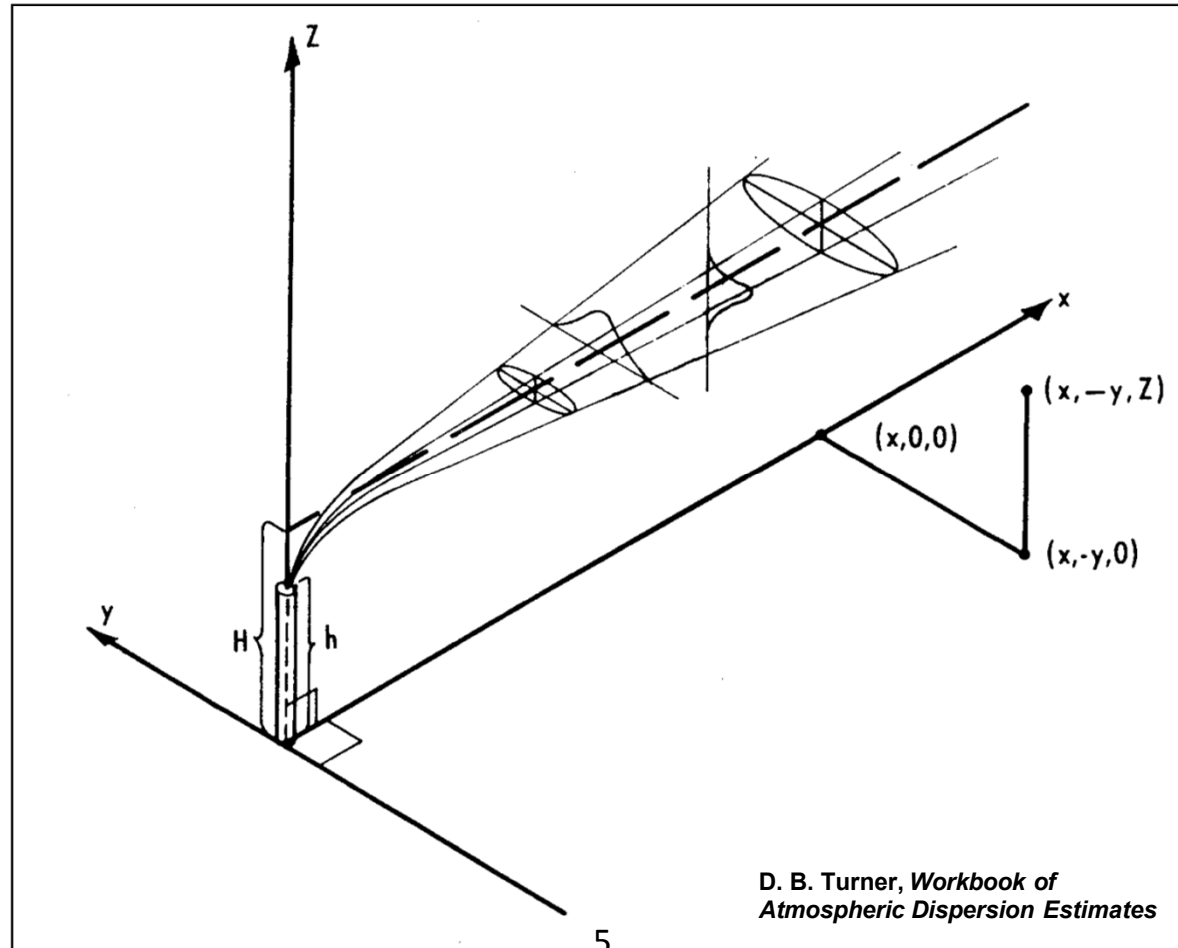
Plume depletion mechanisms

- Radioactive decay
- Wet deposition - rainout by interaction with cloud droplets and washout by falling precipitation
- Dry deposition – gradual loss of reactive vapors and aerosols by deposition onto the surface cover

Atmospheric Transport Inputs and Outputs

- Basic weather inputs
 - Wind speed
 - Wind direction
 - Atmospheric stability
 - Precipitation rate
- Basic outputs
 - Air concentrations
 - Surface deposition

Coordinate System for Atmospheric Transport and Dispersion



Basic Concentration Equation

- Continuous release
- Point source
- No boundaries

$$C = \frac{\dot{Q}}{2\pi\sigma_y\sigma_z u} \exp\left\{-\frac{1}{2}\left[\left(\frac{y}{\sigma_y}\right)^2 + \left(\frac{z}{\sigma_z}\right)^2\right]\right\}$$

C = Plume concentration (Bq/m³)

\dot{Q} = Release rate of contaminant (Bq/s)

y = Cross-wind (lateral) distance from plume centerline (m)

z = Vertical distance from plume centerline (m)

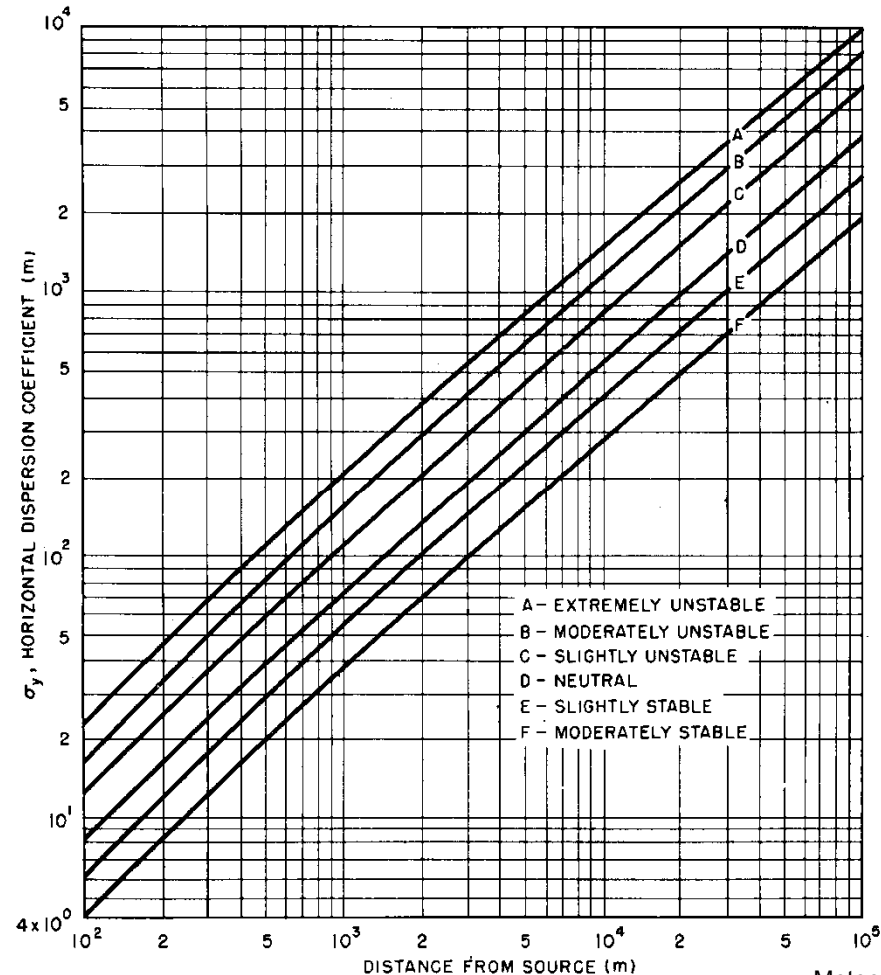
σ_y = Standard deviation of plume in the y direction as a function of x (m)

σ_z = Standard deviation of plume in the z direction as a function of x (m)

u = Average wind speed along plume centerline

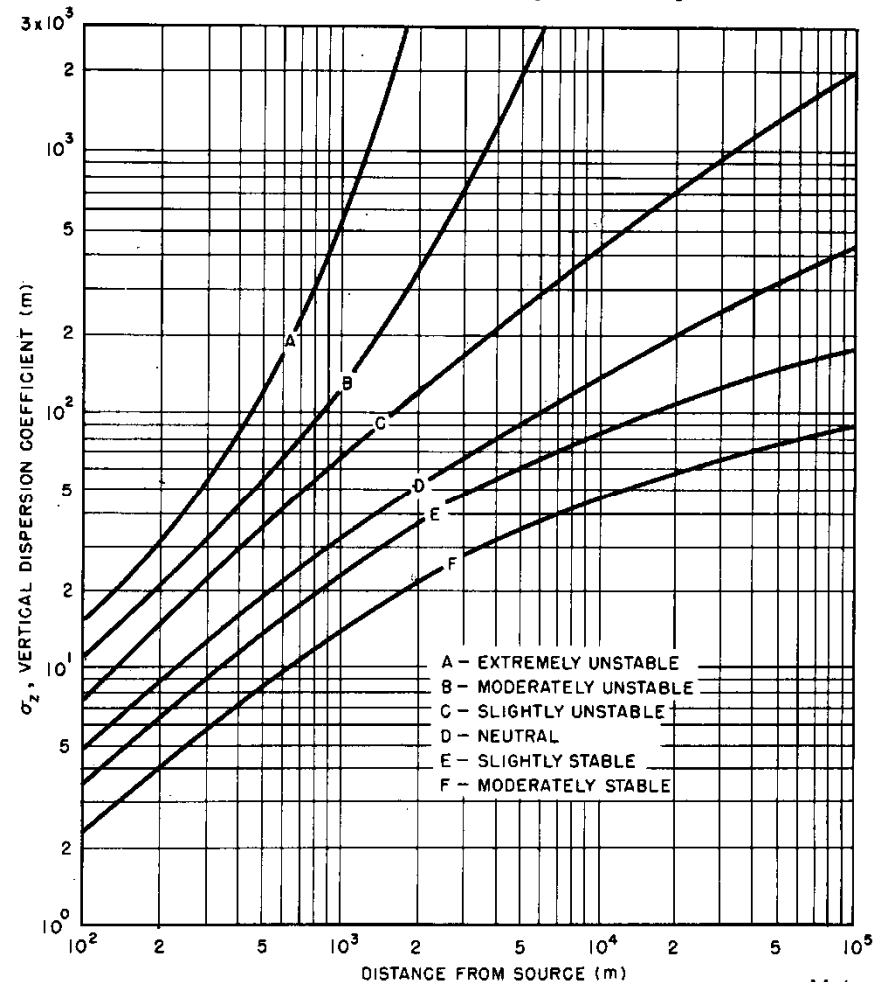
$$\frac{\int C dt}{\int \dot{Q} dt} = \frac{\chi}{Q}$$

Lateral Dispersion, σ_y , vs. Downwind Distance From Source



Meteorology and Atomic Energy, 1968

Vertical Dispersion, σ_z , vs. Downwind Distance From Source (Pasquill-Gifford)



Meteorology and Atomic Energy, 1968

Power-Law Representation of Dispersion

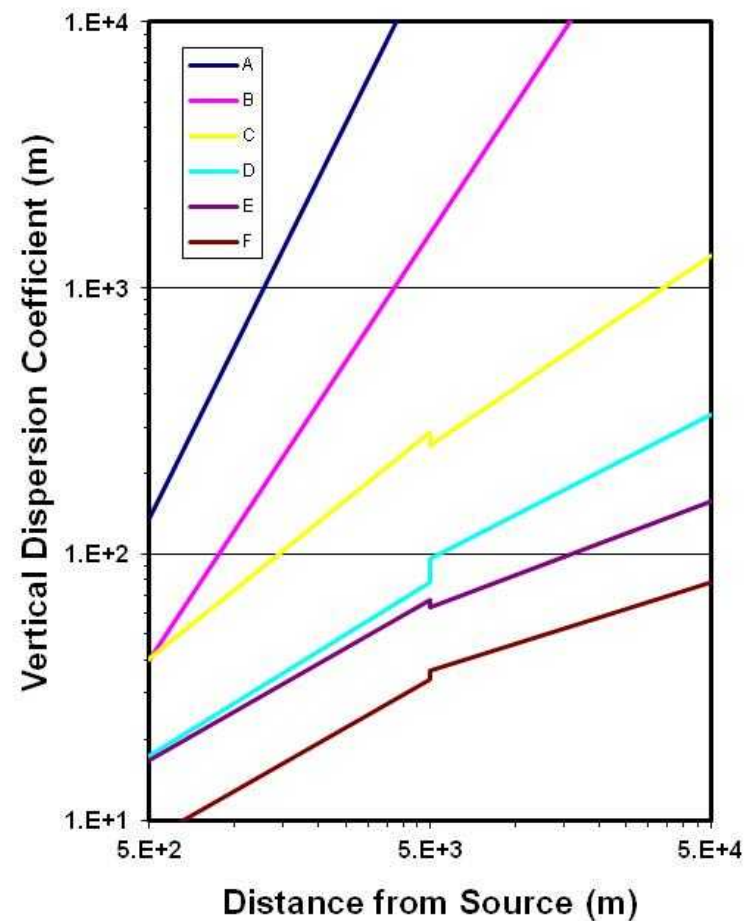
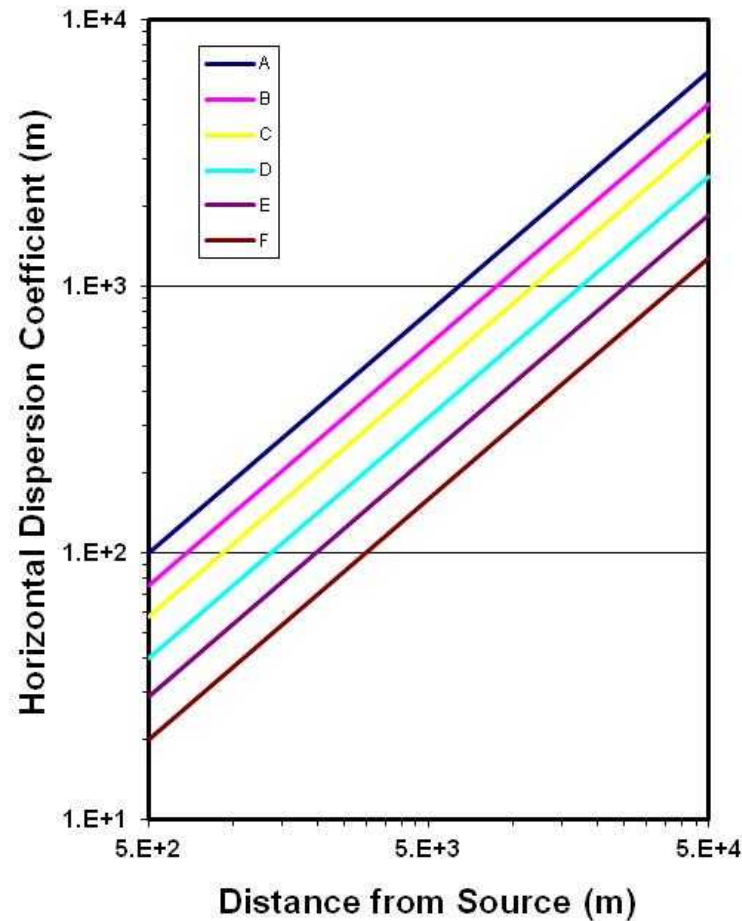
- Power-law representation

$$\sigma_y = a \cdot x^b \qquad \sigma_z = c \cdot x^d$$

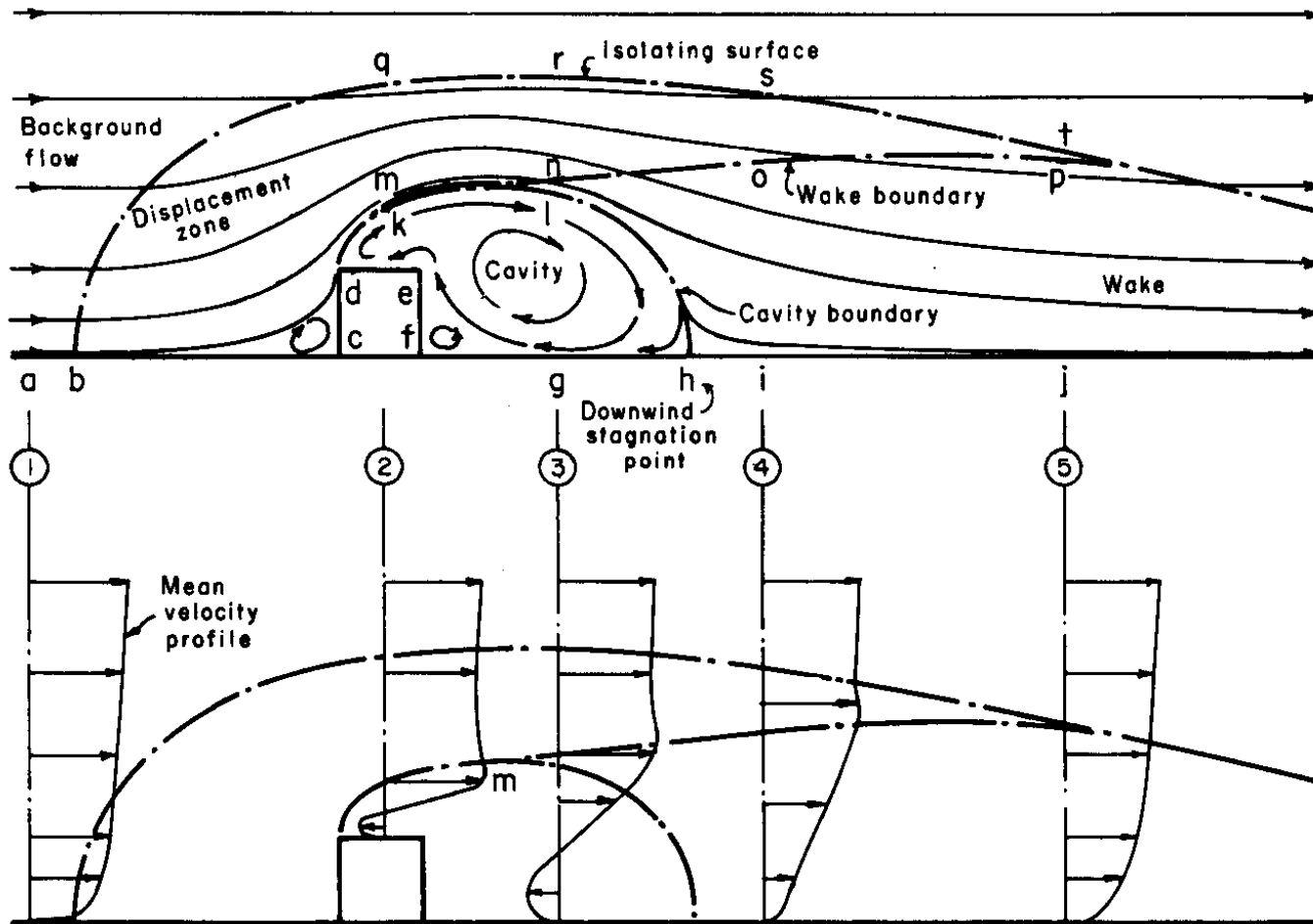
- Excellent representation for σ_y
- Two-piece, less accurate, representation for σ_z

Parameter	Distance Range (km)	Stability Class					
		A	B	C	D	E	F
a	0.5 - 50	0.36580	0.2751	0.2089	0.1474	0.1046	0.0722
b	0.5 - 50	0.90310	0.9031	0.9031	0.9031	0.9031	0.9031
c	0.5 - 5	0.00025	0.0019	0.2000	0.3000	0.4000	0.2000
	5 - 50			0.5742	0.9605	2.1250	2.1820
d	0.5 - 5	2.12500	1.6021	0.8543	0.6532	0.6021	0.6020
	5 - 50			0.7160	0.5409	0.3979	0.3310

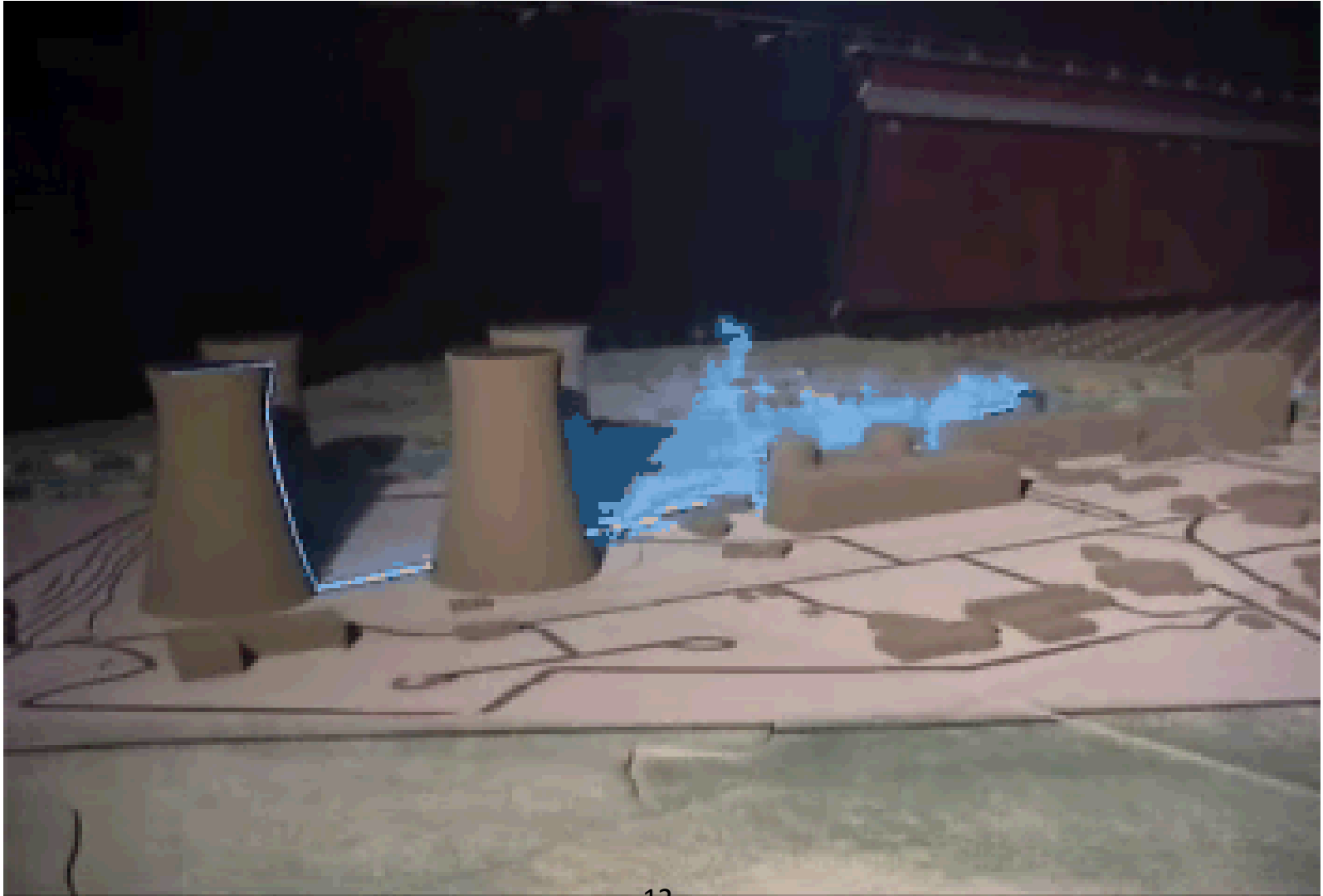
Plots of Power-Law Functions for Tadmor and Gur Parameters



General Arrangement of Flow Zones Near a Sharp-edged Building



Wind-Tunnel Test of Scaled Plant

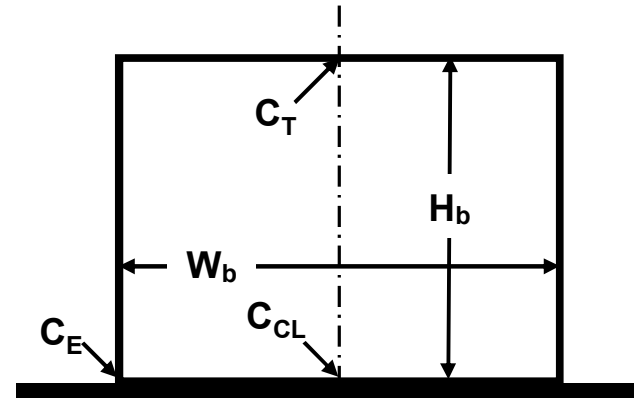


Building Wake - Area Source

- Assume fraction, f , of centerline concentration at building edge and top

$$f = \frac{C_E}{C_{CL}} = \exp\left(\frac{-(W_b/2)^2}{2\sigma_{y_0}^2}\right)$$

$$f = \frac{C_T}{C_{CL}} = \exp\left(\frac{-H_b^2}{2\sigma_{z_0}^2}\right)$$

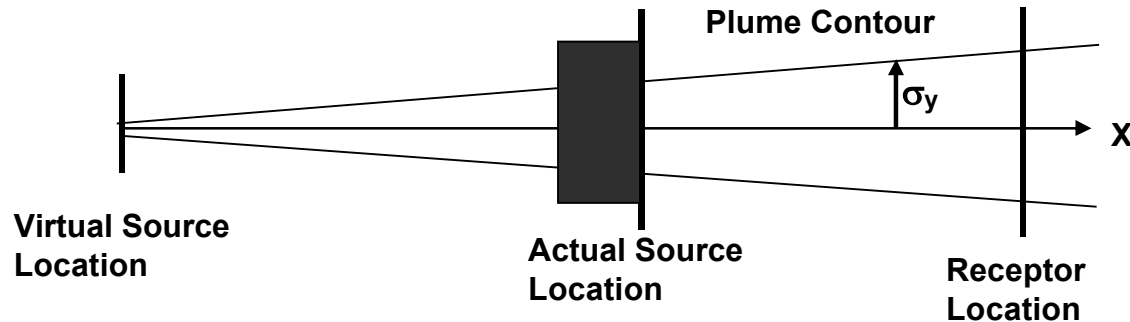


For $f = 0.1$, $\sigma_{y_0} = 0.23 W_b$ and $\sigma_{z_0} = 0.47 H_b$

Where W_b and H_b are the width and height of the building, respectively

Virtual Sources

- Virtual source is the location of a “point” source that produces an equivalent plume size
- Actual source location corresponds to a finite distance downwind from the virtual source
 - X_{y0} for crosswind dispersion
 - X_{z0} for vertical dispersion
- Receptor locations are relative to actual source location

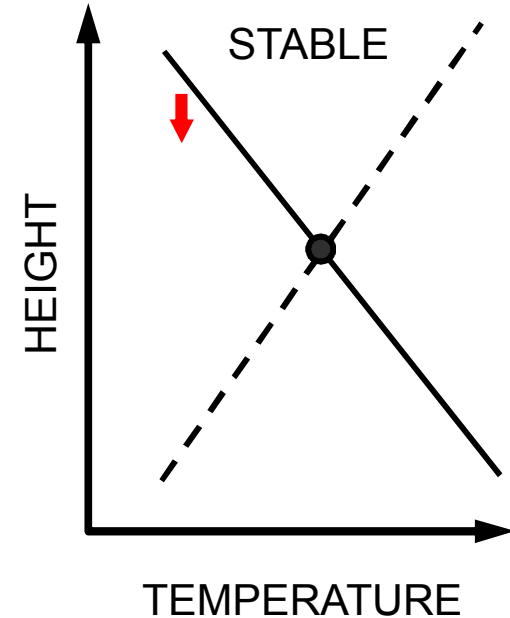
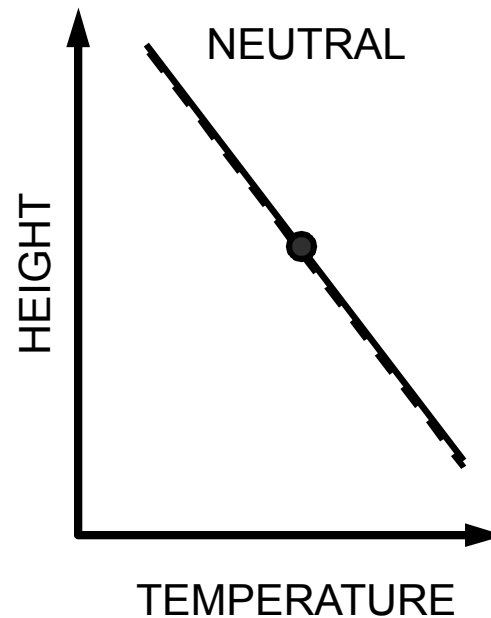
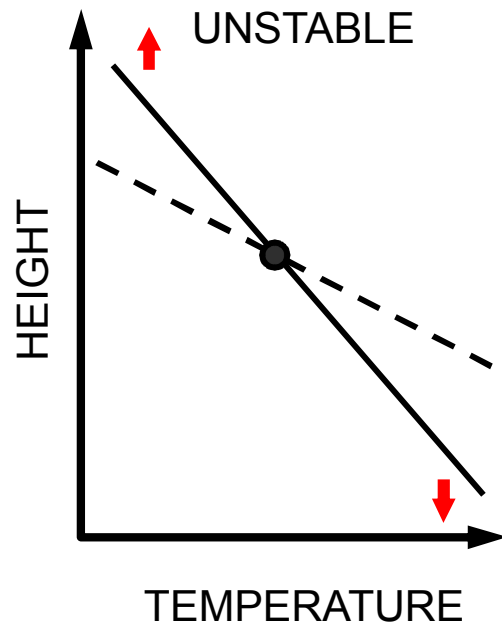


Planetary Boundary Layer

- Region of atmosphere between earth's surface and an upper region of nonturbulent, geostrophic flow
- Ranges in height from 50 m – height of troposphere (10 to 18 km)
- Consists of three parts
 - Surface layer (first 10%, turbulence is created)
 - Core (up to 70% of PBL, turbulence is dissipated)
 - Top (remainder)
- Principal types are convective and stably stratified
- Wind speed and direction tend to vary with height in surface layer
- Stability of atmosphere within PBL determines turbulence intensity (dispersion effects)
- Radioactive materials are assumed to be trapped in this layer
- Here we assume it is the same as the mixing layer

Illustrations of PBL Stability Conditions

————— PARCEL
----- ENVIRONMENT



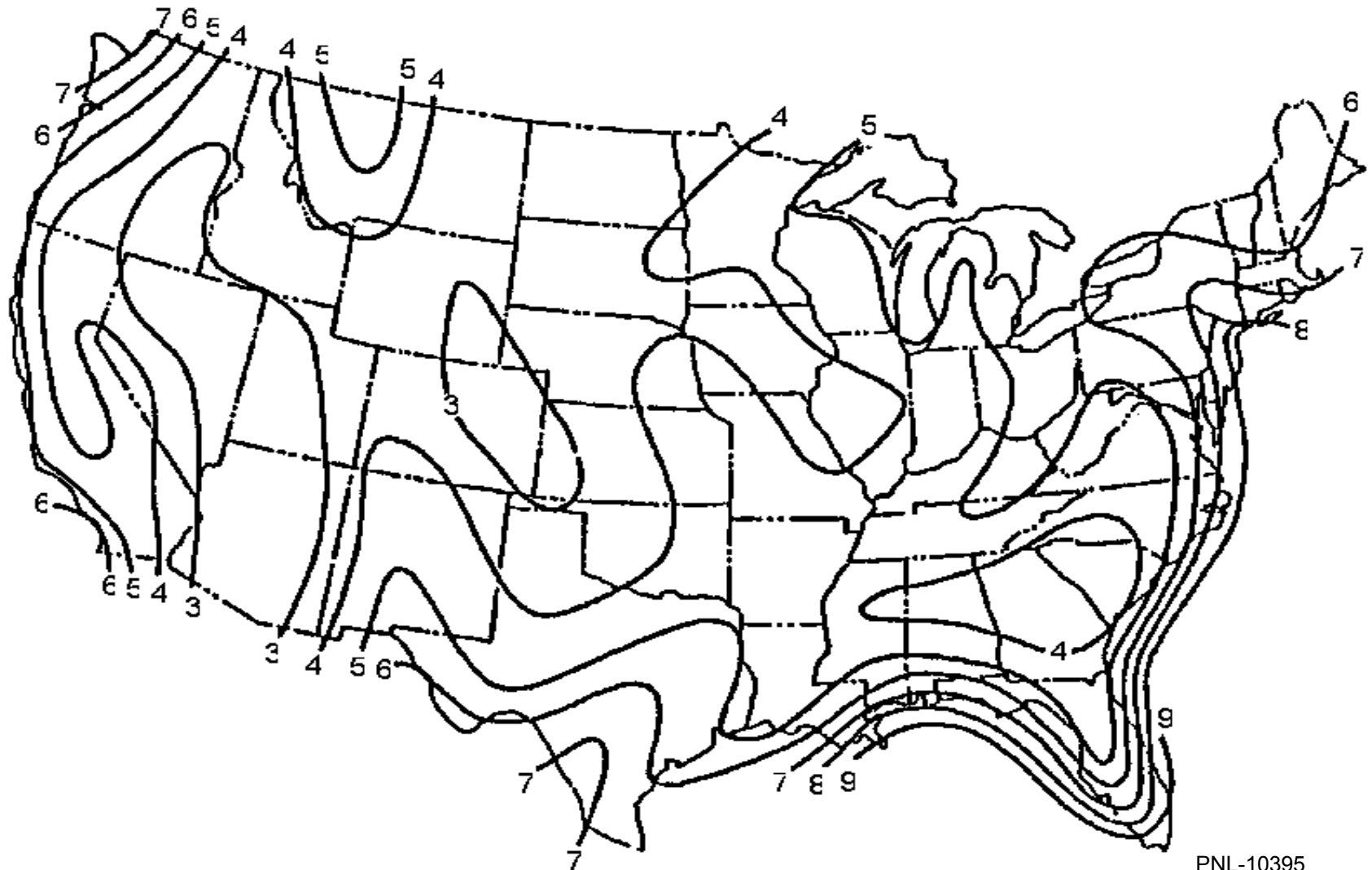
Atmospheric Stability Classifications by Vertical Temperature Gradient (Lapse Rate)

Stability classification	Pasquill categories	Temperature change with height (°C/100 m)
Extremely unstable	<i>A</i>	$\Delta T/\Delta z \leq -1.9$
Moderately unstable	<i>B</i>	$-1.9 < \Delta T/\Delta z \leq -1.7$
Slightly unstable	<i>C</i>	$-1.7 < \Delta T/\Delta z \leq -1.5$
Neutral	<i>D</i>	$-1.5 < \Delta T/\Delta z \leq -0.5$
Slightly stable	<i>E</i>	$-0.5 < \Delta T/\Delta z \leq 1.5$
Moderately stable	<i>F</i>	$1.5 < \Delta T/\Delta z \leq 4.0$
Extremely stable	<i>G</i>	$4.0 < \Delta T/\Delta z$

Mixing Height

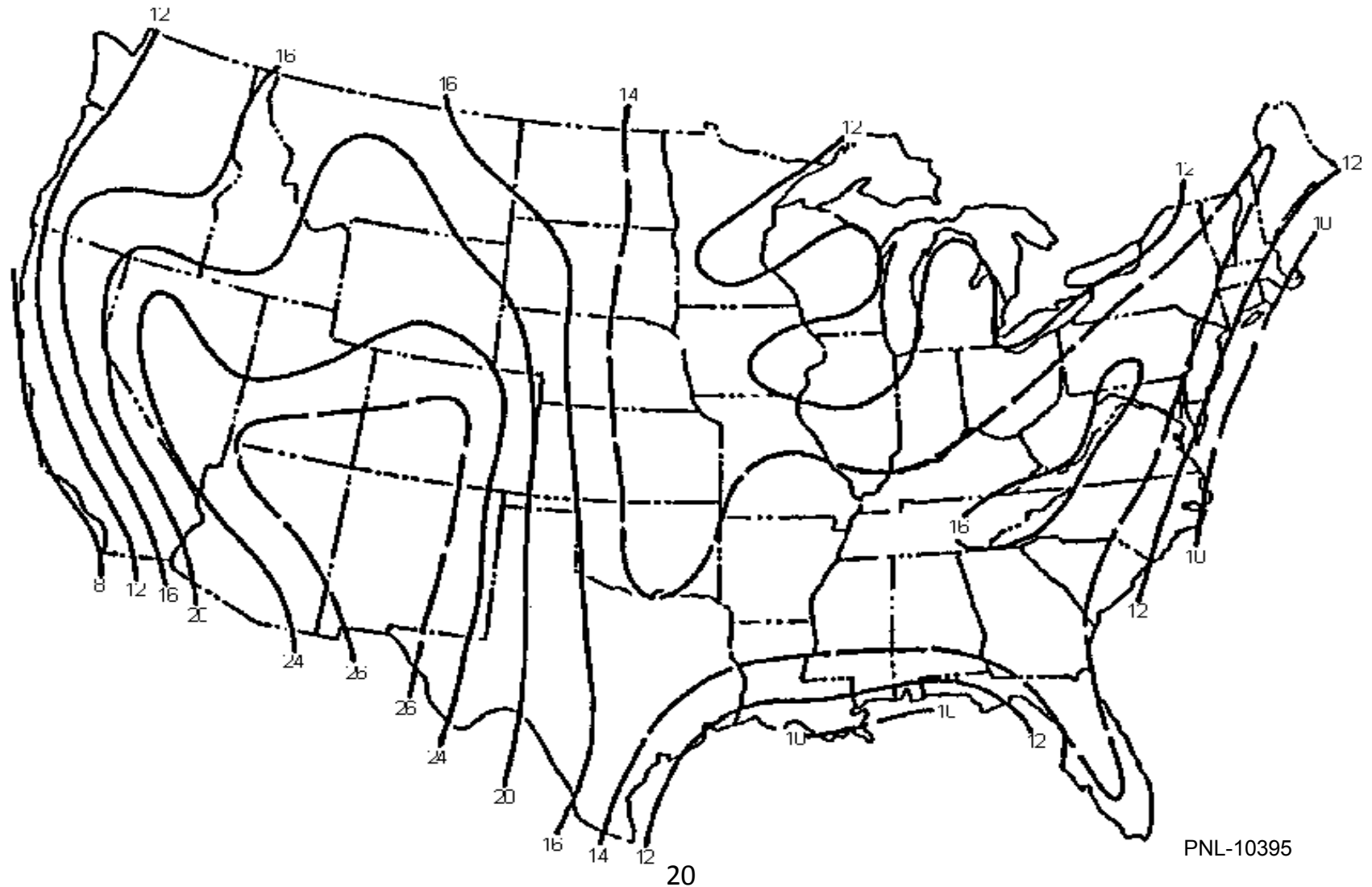
- Mixing height is usually determined by
 - Thermal mixing (convection) during daytime
 - Mechanical mixing during nighttime
- Varies continuously (hour to hour, day to day, season to season)
- Usually lowest at night and early morning
- Usually highest in afternoon
- Inhibits plume rise (we assume that it is an absolute barrier)

Mean Annual Morning Mixing Heights ($\text{m} \times 10^2$)



PNL-10395

Mean Annual Afternoon Mixing Heights ($\text{m} \times 10^2$)

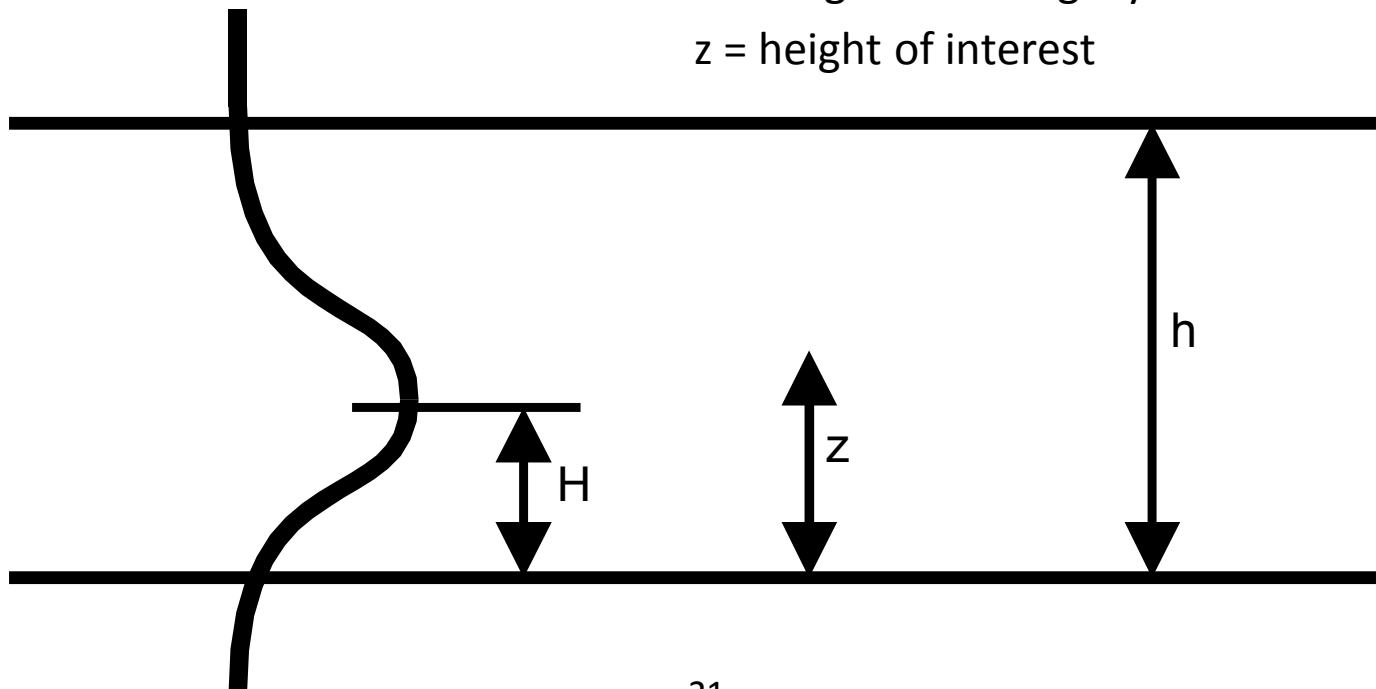


Vertical Boundaries Ground and Mixing Layer

H = release height (or lofting
height) above ground

h = height of mixing layer

z = height of interest



General Gaussian Plume Equation With Reflective Boundaries

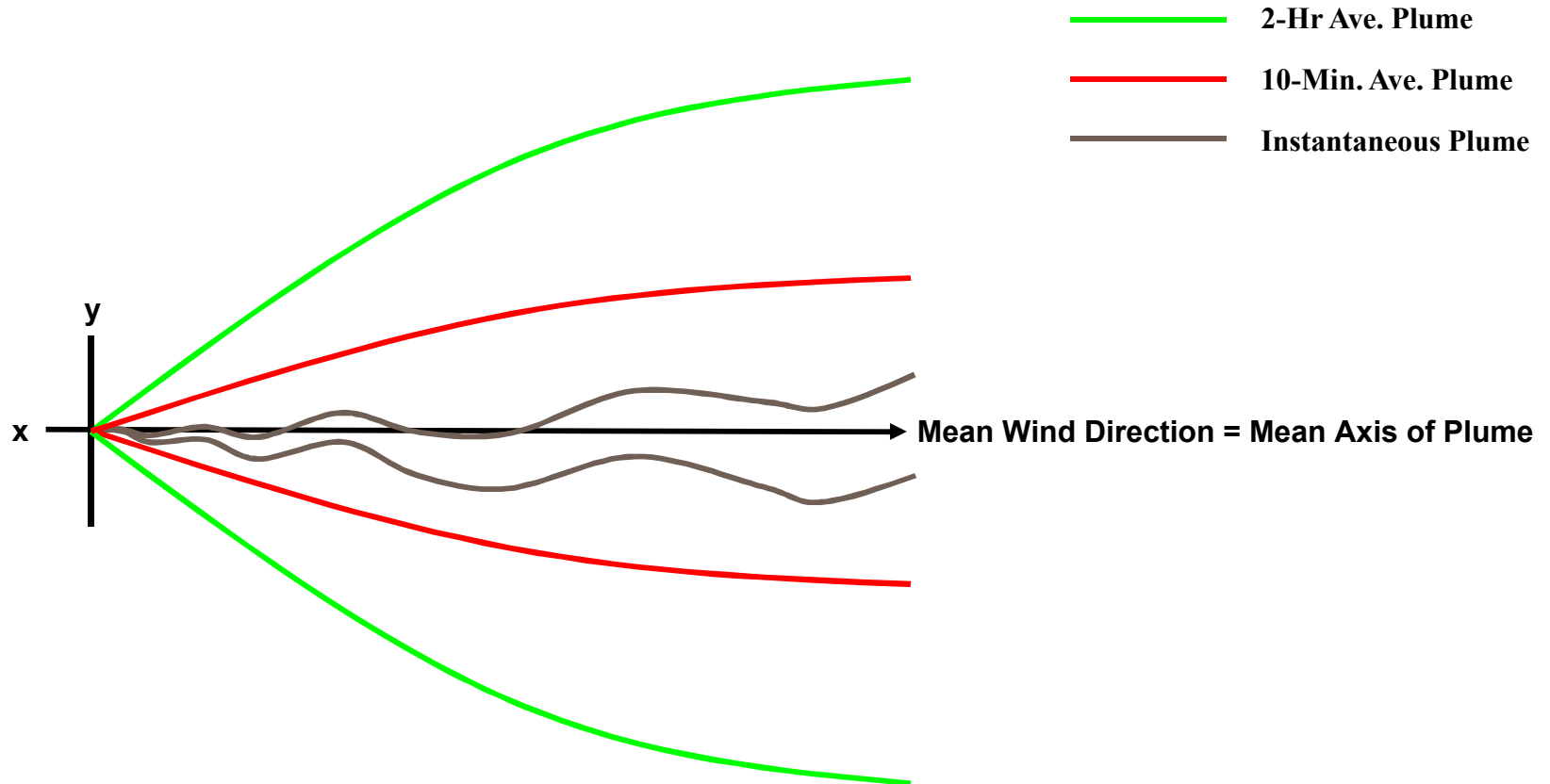
- Account for material that would have been lost through boundaries

$$C = \frac{\dot{Q}}{2\pi\sigma_y\sigma_z u} \exp\left(\frac{-y^2}{2\sigma_y^2}\right) \sum_{n=-\infty}^{\infty} \left\{ \exp\left[-\frac{1}{2}\left(\frac{2nh - H - z}{\sigma_z}\right)^2\right] + \exp\left[-\frac{1}{2}\left(\frac{2nh + H - z}{\sigma_z}\right)^2\right] \right\}$$

- Simplified equation when release is at ground level and observation point is on plume centerline ($H = y = z = 0$)

$$C = \frac{\dot{Q}}{2\pi\sigma_y\sigma_z u} \sum_{n=-\infty}^{\infty} 2 \exp\left[-2\left(\frac{nh}{\sigma_z}\right)^2\right]$$

Effect of Diffusion Times – Plume Meander



Original MACCS2 Plume Meander

- Increases effective plume spread in y direction
- Effect of plume meander continues downwind indefinitely

$$\sigma_{y, m} = \sigma_y \left(\frac{\Delta t}{\Delta t_{\text{ref}}} \right)^m$$

Δt = Release duration (s)

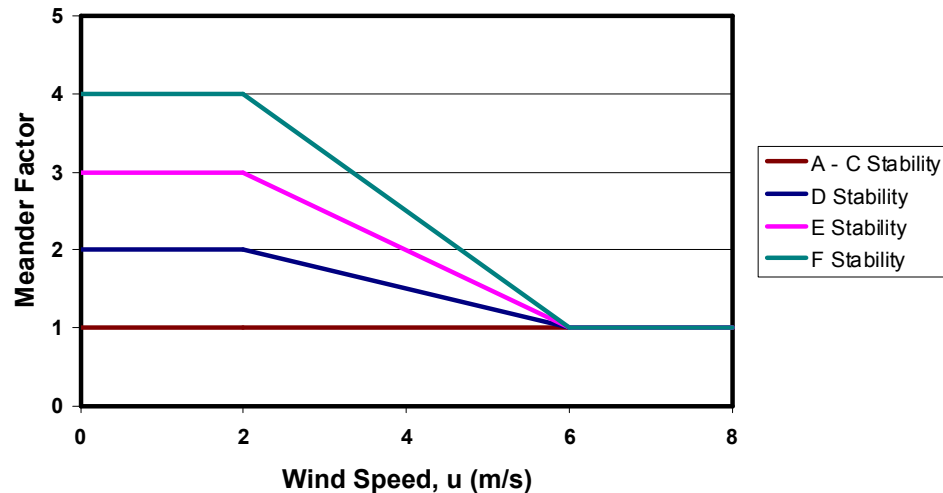
Δt_{ref} = 600, the experimental duration of the Prairie Grass tests (s)

m = an empirical exponent

= 0.2 when $\Delta t < 1$ hr

= 0.25 when $\Delta t > 1$ hr

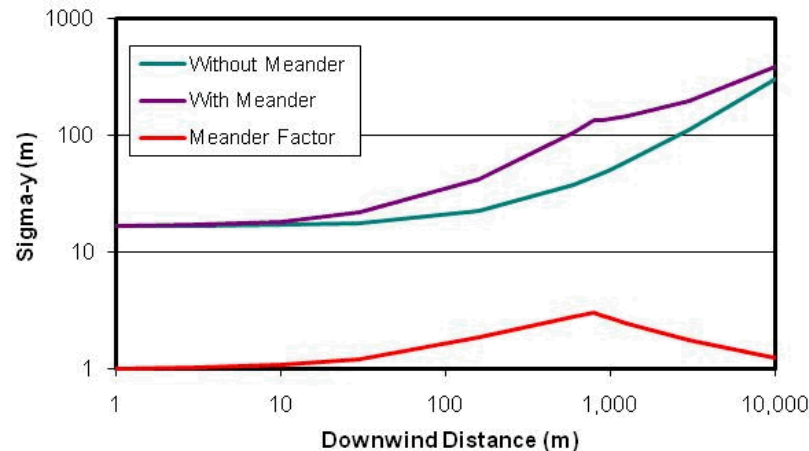
Regulatory Guide 1.145 Plume Meander Model



- Meander factor depends on stability class and wind speed
- Model is based on a 1-hr plume duration
- Effect of plume meander diminishes beyond 800 m from source
- Plot shows

- Dispersion not accounting for plume meander
- Dispersion accounting for plume meander (<2 m/s and F stability)
- Effective meander factor

Stability Class F, Less Than 2 m/s Wind Speed



Plume Rise

- Earlier Briggs' model is used to estimate plume rise
 - Near-field trajectory (used for stability classes A – D)

$$\Delta H(x) = \frac{1.6(Fx^2)^{1/3}}{\bar{u}}$$

- Final rise for stability classes A – D

$$\Delta H_f = 38.7 \frac{F^{0.60}}{\bar{u}} \quad \text{when } F \geq 55$$

$$\Delta H_f = 21.4 \frac{F^{0.75}}{\bar{u}} \quad \text{when } F < 55$$

- Final rise for stability classes E – F

$$\Delta H_f = 2.4 \left(\frac{F}{\bar{u}s} \right)^{1/3}$$

Plume Trapping in Building Wake

- Plume is trapped in building wake when

$$u > \left(\frac{9.09F}{H_b} \right)^{1/3}$$

Where H_b is the building height (m)

F is the buoyancy flux defined previously (m^4/s^3)

u is wind speed (m/s)

- A trapped plume is
 - Released at the level of the initial release point

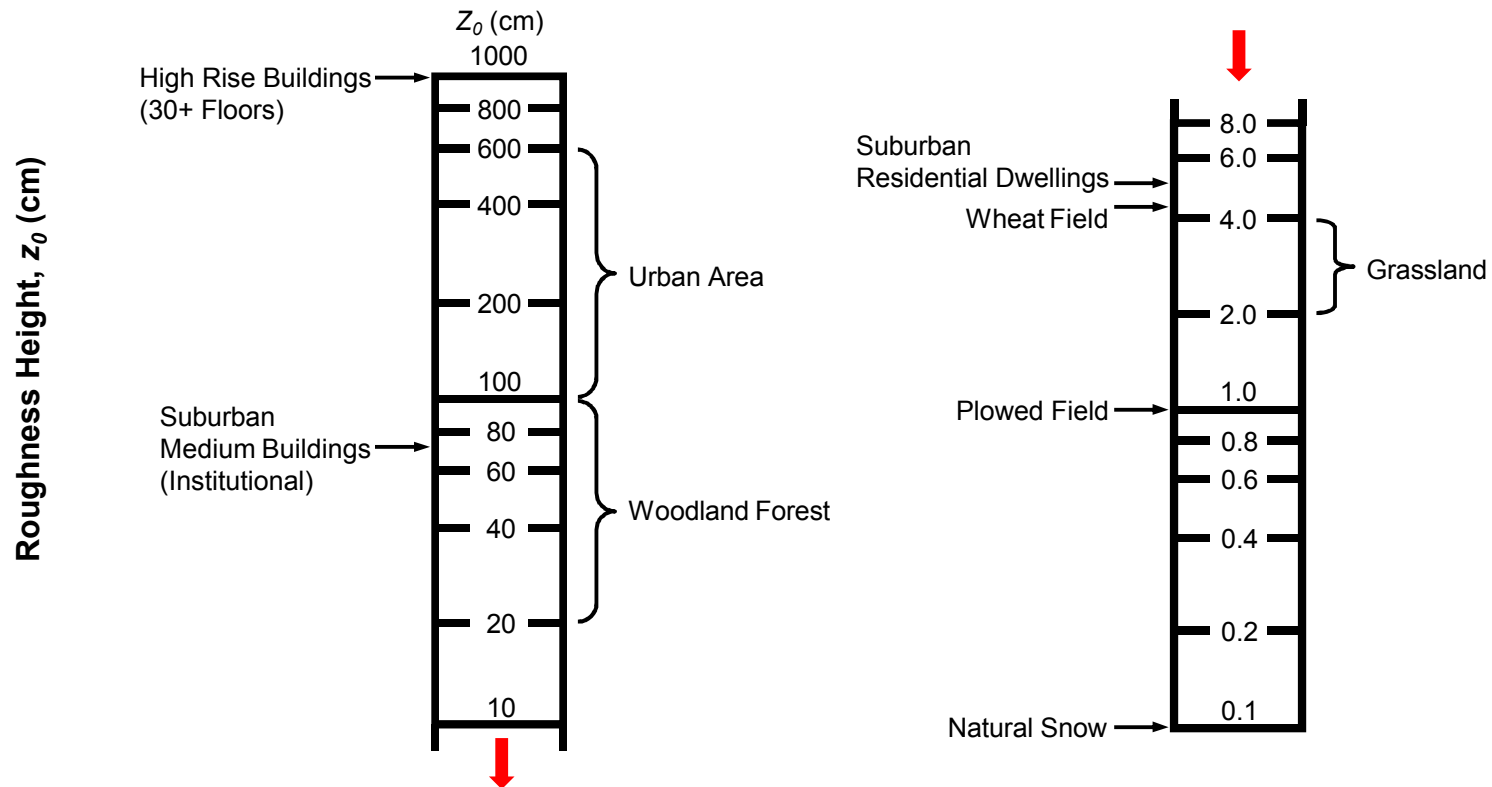
Roughness Length, z_0

- Function of size and spacing of roughness elements
- Dependent on the frontal area of the average element (facing the wind) divided by the ground width it occupies
- A lower roughness length implies less momentum exchange between the surface and the atmosphere
- σ_z measured over flat terrain during Prairie Grass tests ($z_0 = 3$ cm)

$$\sigma_z = \sigma_{z, PG} \left(\frac{z_0}{3} \right)^{0.2}$$

28

Roughness Lengths for Various Surfaces



Workshop Example 1 – Pasquill-Gifford Chart

For a 30 minute release from this building (assume dimensions of 200 ft. high by 120 ft. wide) of 1 Ci of ^{137}Cs , what is the maximum ground concentration 1/2 mile downwind and at the mall (8 miles downwind). Assume worst case conditions.

Assumptions:

Worst Case - Wind blowing directly towards mall

Concentration at plume centerline ($y = z = H = 0$)

Low wind speed ($u = 1$ m/s; may not be worst case for short half lives)

Minimize atmospheric dispersion; stability = F

Heat low enough so that no plume rise

Other - Converting dimensions of interest:

1/2 mi ~ 800m

8 mi ~ 13000m

Building height = 200ft ~ 60m

Building width = 120ft ~ 37m

Roughness length (z_0) = 100cm (suburban/urban)

WORKSHOP EXAMPLE 1 (cont.)

Meander (5-26): $\sigma_{y,m} = \sigma_y \left(\frac{30}{10} \right)^{0.2} = 1.25\sigma_y$

Roughness (5-32): $\sigma_{z,z_0} = \sigma_z \left(\frac{100}{3} \right)^{0.2} = 2.0\sigma_z$

Building Wake (5-15): $\sigma_{y_0} = .23(37) = 8.6m$
 $\sigma_{z_0} = .47(60) = 28m$

Mixing Height: Morning = 550m (worst case meteorologically)
(5- 21, 5-22) Afternoon = 1500m (worst case because most people at mall)

WORKSHOP EXAMPLE 1 (cont.)

from (5-9) and (5-10)

Receptor Distance (m)	σ_y (m)	σ_z (m)
	$8.6/1.25 = 6.9 \Rightarrow X_{y_0} = 180$	$28/2.0 = 14 \Rightarrow X_{z_0} = 1100$
800	$39 (@ X = 800 + 180) * 1.25 = 49$	$21 (@ X = 800 + 1100) * 2 = 42$
13000	$390 (@ X = 13000 + 180) * 1.25 = 490$	$53 (@ X = 13000 + 1100) * 2 = 106$

Series Terms (5-24):

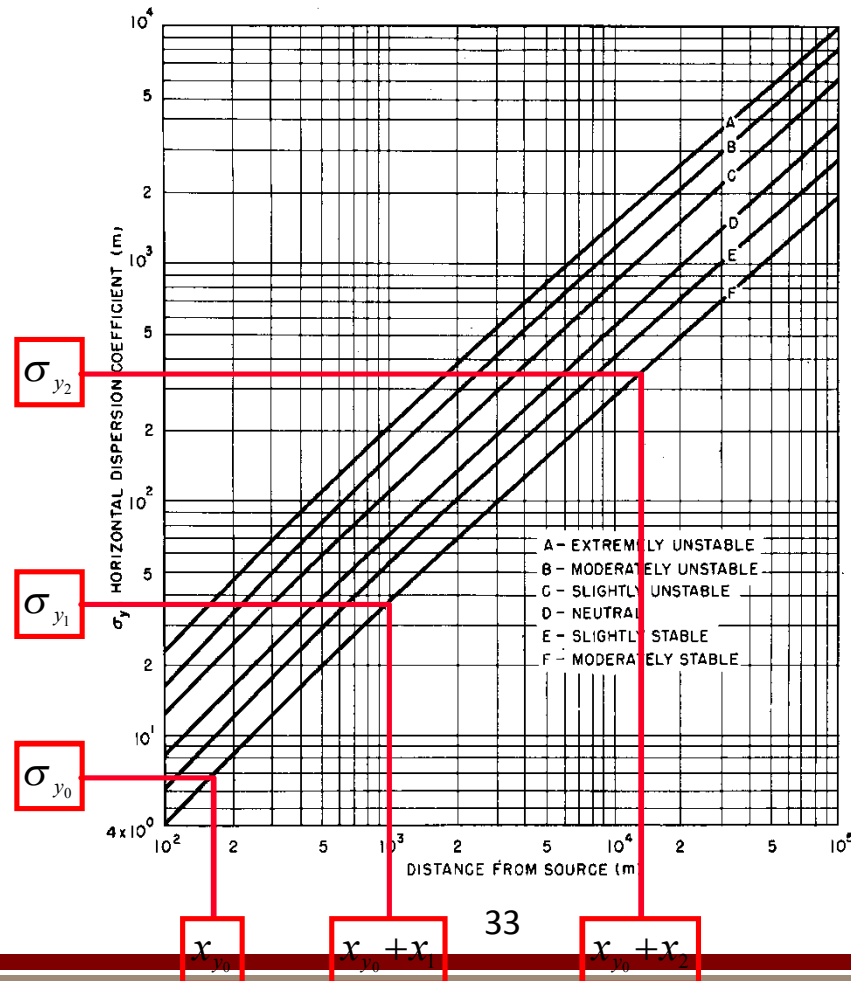
$$\sum_{n=-\infty}^{\infty} 2e^{\left[-2\left(\frac{n1500}{\sigma_z}\right)^2\right]}$$

$$\begin{aligned} Z &= 0 \\ H &= 0 \end{aligned}$$

$\sigma_z \backslash n$	0	-1	+1
42	2	0	0
106	2	0	0

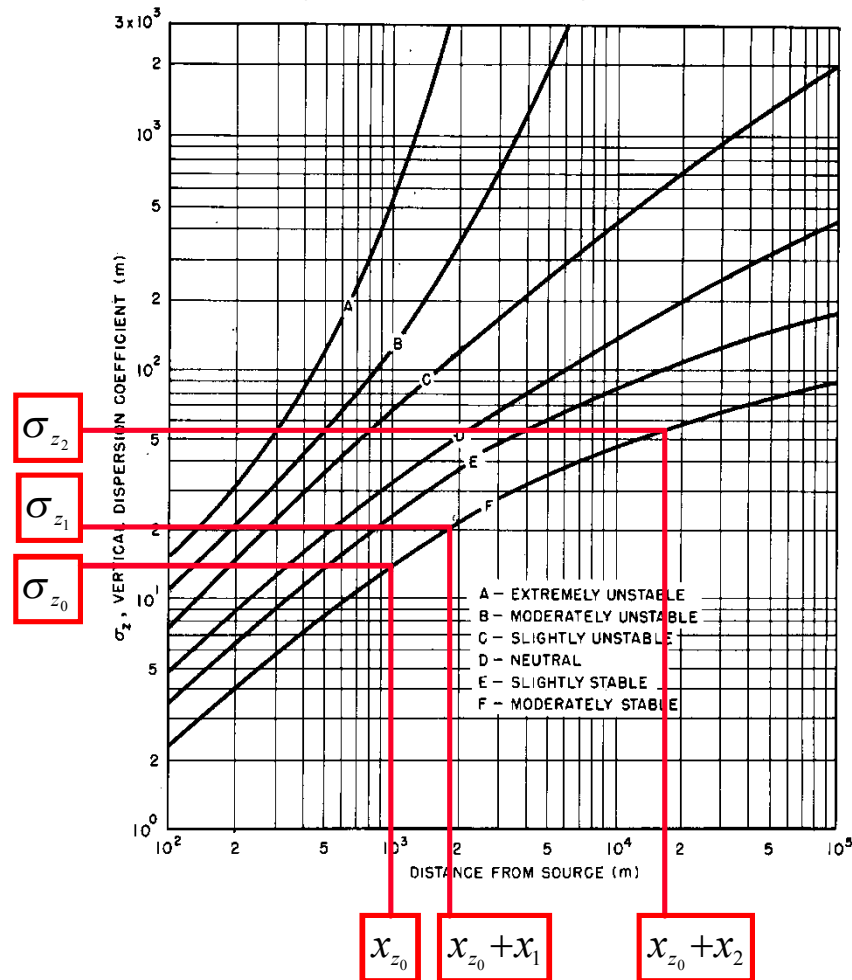
WORKSHOP EXAMPLE 1 (cont.)

Lateral Dispersion (5-9), σ_y , vs. Downwind Distance From Source for Pasquill's Stability Classes



WORKSHOP EXAMPLE 1 (cont.)

Vertical Dispersion (5-10), σ_z , vs. Downwind Distance From Source for Pasquill's Stability Classes



WORKSHOP EXAMPLE 1 (cont.)

(5-24)

1/2 mile

8 miles

$$\frac{C}{Q} = \frac{1}{2\pi(49)(42)(1)}(2) = 1.6 \times 10^{-4} \frac{\text{sec}}{\text{m}^3}$$

$$= \frac{1}{2\pi(490)(106)(1)}(2) = 6.1 \times 10^{-6} \frac{\text{sec}}{\text{m}^3}$$

$$C = 1.6 \times 10^{-4} \frac{\text{sec}}{\text{m}^3} \times \frac{1 \text{ curie}}{1800 \text{ sec}} = 8.9 \times 10^{-8} \frac{\text{curie}}{\text{m}^3}$$

$$= 6.1 \times 10^{-6} \frac{\text{sec}}{\text{m}^3} \times \frac{1 \text{ curie}}{1800 \text{ sec}} = 3.4 \times 10^{-9} \frac{\text{curie}}{\text{m}^3}$$

C = Inversely proportional to $\sigma_y \cdot \sigma_z$ (plume centerline, no reflections, no decay)

dist	$\sigma_y \cdot \sigma_z$	$C/C_{0.5 \text{ mi}}$
0.5 mi	(39) (21)	1
8 mi	(390) (53)	1/25
50 mi	(1700) (87)	1/180

Workshop Example 1 – Tadmor and Gur Parameters

For a 30 minute release from this building (assume dimensions of 200 ft. high by 120 ft. wide) of 1 Ci of ^{137}Cs , what is the maximum ground concentration 1/2 mile downwind and at the mall (8 miles downwind). Assume worst case conditions.

Assumptions:

Worst Case - Wind blowing directly towards mall

Concentration at plume centerline ($y = z = H = 0$)

Low wind speed ($u = 1\text{m/s}$; may not be worst case for short half lives)

Minimize atmospheric dispersion; stability = F

Heat low enough so that no plume rise

Other - Converting dimensions of interest:

1/2 mi ~ 800m

8 mi ~ 13000m

Building height = 200ft ~ 60m

Building width = 120ft ~ 37m

Roughness length (z_0) = 100cm (suburban/urban)

WORKSHOP EXAMPLE 1 – T&G (cont.)

Meander:
$$\sigma_{y,m} = \sigma_y \left(\frac{30}{10} \right)^{0.2} = 1.25\sigma_y$$

Roughness:
$$\sigma_{z,z_0} = \sigma_z \left(\frac{100}{3} \right)^{0.2} = 2.0\sigma_z$$

Building Wake:
$$\begin{aligned}\sigma_{y_0} &= .23(37) = 8.6m \\ \sigma_{z_0} &= .47(60) = 28m\end{aligned}$$

Mixing Height: Morning = 550m (worst case meteorologically)
Afternoon = 1500m (worst case because most people at mall)

WORKSHOP EXAMPLE 1 – T&G (cont.)

from (5-11)

Parameter	Distance Range (km)	Stability Class					
		A	B	C	D	E	F
a	0.5 - 50	0.36580	0.2751	0.2089	0.1474	0.1046	0.0722
b	0.5 - 50	0.90310	0.9031	0.9031	0.9031	0.9031	0.9031
c	0.5 - 5	0.00025	0.0019	0.2000	0.3000	0.4000	0.2000
	5 - 50			0.5742	0.9605	2.1250	2.1820
d	0.5 - 5	2.12500	1.6021	0.8543	0.6532	0.6021	0.6020
	5 - 50			0.7160	0.5409	0.3979	0.3310

Receptor Distance (m)	$\sigma_y(m)$	$\sigma_z(m)$
Initial Virtual Source Distance	$8.6 = 1.25 \cdot 0.0722 \cdot x^{0.9031}$ $x = 155$	$28 = 2.0 \cdot 0.2000 \cdot x^{0.6020}$ $x = 1160$
800 m	$1.25 \cdot 0.0722 \cdot (155 + 800)^{0.9031}$ $= 44$	$2.0 \cdot 0.2000 \cdot (1160 + 800)^{0.6020}$ $= 38$
5000 m	$1.25 \cdot 0.0722 \cdot (155 + 5000)^{0.9031}$ $= 203$	$2.0 \cdot 0.2000 \cdot (1160 + 5000)^{0.6020}$ $= 76$

WORKSHOP EXAMPLE 1 – T&G (cont.)

Distance (m)	σ_y (m)	σ_z (m)
Virtual Source Distance @ 5000 m	$203 = 1.25 \cdot 0.0722 \cdot x^{0.9031}$ $x = 5155 - 5000 = 155$	$76 = 2.0 \cdot 2.1820 \cdot x^{0.3310}$ $x = 5712 - 5000 = 712$
13,000	$1.25 \cdot 0.0722 \cdot (155 + 13000)^{0.9031}$ $= 474$	$2.0 \cdot 2.1820 \cdot (712 + 13000)^{0.3310}$ $= 102$

Reflections:

$$\sum_{n=-\infty}^{\infty} 2e^{\left[-2\left(\frac{n \times 1500}{\sigma_z}\right)^2\right]} \quad \begin{matrix} Z=0 \\ H=0 \end{matrix}$$

	n		
σ_z	0	-1	+1
38	2	0	0
124	2	0	0

WORKSHOP EXAMPLE 1 – T&G (cont.)

1/2 mile

$$C/\dot{Q} = \frac{2}{2\pi(44\text{ m})(38\text{ m})(1\frac{\text{m}}{\text{s}})} = 1.8 \times 10^{-4} \text{ s/m}^3$$

8 miles

$$C/\dot{Q} = \frac{2}{2\pi(474\text{ m})(102\text{ m})(1\frac{\text{m}}{\text{s}})} = 6.6 \times 10^{-6} \text{ s/m}^3$$

$$C = 1.8 \times 10^{-4} \frac{\text{s}}{\text{m}^3} \times \frac{1\text{ Ci}}{1800\text{ s}} = 1.0 \times 10^{-7} \frac{\text{Ci}}{\text{m}^3}$$

$$C = 6.6 \times 10^{-6} \frac{\text{s}}{\text{m}^3} \times \frac{1\text{ Ci}}{1800\text{ s}} = 3.7 \times 10^{-9} \frac{\text{Ci}}{\text{m}^3}$$

Workshop Exercise 1

- For a two hour ground level release in the morning of 10 curies of ^{132}I (half-life = 2.3 hours) containing one-half million Btu (147 KW-hr) heat content from a building which is 38.3 meters high and 56.5 meters wide located in a rural area of central Kentucky, what is the concentration of iodine that would be inhaled by a farmer standing in his plowed field 5.67 miles (9100 meters) downwind? Measurements on a met tower near the release indicate a typical day of 4 m/sec wind speed; the temperature at the 10-meter (height) sensor is 0.6 deg F (0.33 deg C) higher than that at the 30-meter sensor.
- Part 2: What concentration would the farmer see if the PBL were moderately stable?
- Part 3: Moderately stable with a wind speed of 1 m/sec?

Deposition Processes

- Dry Deposition
 - Impaction
 - Diffusion (Brownian motion)
 - Gravitational settling
- Wet Deposition
 - Scavenging by precipitation (washout)
 - Scavenging by cloud droplets (rainout)

Dry Deposition

■ Continuous and slow

$$D = CV_d\Delta t$$

D = dry deposition (ground concentration) (Bq/m²)

C = near-surface air concentration (Bq/m³)

V_d = deposition velocity (m/s)

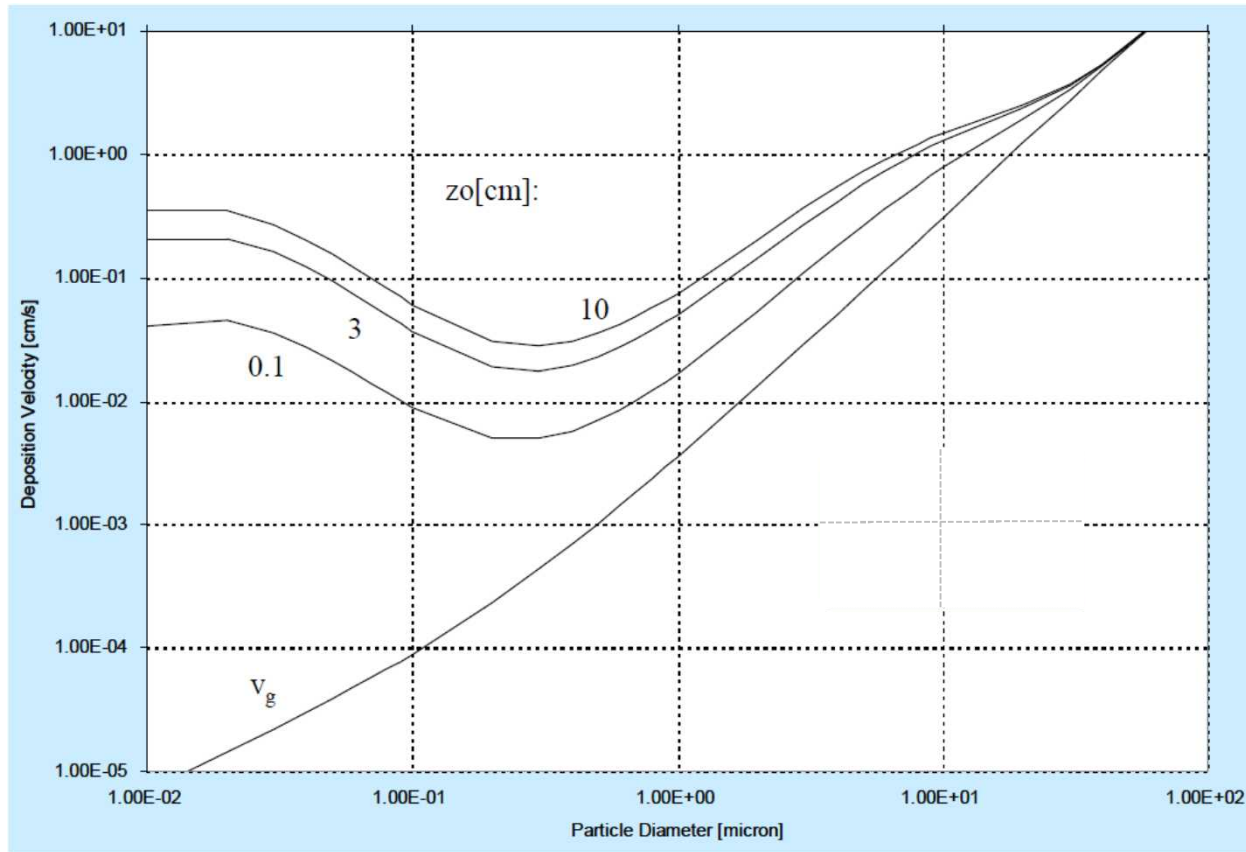
Δt = plume residence time (s)

■ Approximate formula for deposition losses

$$\frac{Q}{Q_0} = \exp\left(-\frac{V_d\Delta t}{\bar{z}}\right) \quad \bar{z} = \sqrt{\frac{\pi}{2}} \left(\frac{\sigma_z}{\bar{\Sigma}}\right)$$

Where Q is the material suspended in the plume (Bq) and Σ represents the summation term in the expression for σ_z (p. 5-24).

Average Deposition Velocities (cm/s)



Wet Deposition

- Discontinuous (precipitation events)
- Rapid (relative to dry)
 - Λ = scavenging or washout rate (1/s)
 - Λ = function of precipitation type and rate, saturation conditions, contaminant characteristics

$$\frac{dQ}{dt} = -\Lambda Q \quad ; \quad \frac{Q}{Q_0} = e^{-\Lambda \Delta t} \quad \Delta t = \text{duration of precipitation (s)}$$

$$\Lambda = aI^b$$

Λ = scavenging rate (1/s)

I = precipitation rate (mm/hr)

$$a = 9.5 \times 10^{-5}$$

$$b = 0.8$$

Workshop Exercise 2 (Deposition)

- For the release of ^{137}Cs analyzed in the workshop example, what is the deposition (Ci/m^2) one-half mile downwind and at the mall?
- Assumptions (same as workshop example):
 - No rain
 - $V_d = 1 \text{ cm/sec}$
- How much of the plume would have deposited prior to the mall if it had been raining steadily throughout the plume's path at a rate of 1 inch/hour?

References

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- E. D. Gorham, et al., “Evaluation of Severe Accident Risks: Methodology for the Containment, Source Term, Consequence, and Risk Integration Analyses,” NUREG/CR-4551, Vol.. 1, Rev. 1, Dec. 1993.
- Severe Accident Risks: An Assessment for Five U.S. Nuclear Power Plants, NUREG/CR-1150
- State-of-the-Art Reactor Consequence Analysis (SOARCA) Report, NUREG-1935
- Sandia National Laboratories, “State-of-the-Art Reactor Consequence Analysis Project, Vol. 1: Peach Bottom Integrated Analysis,” NUREG/CR-7110
- Sandia National Laboratories, “State-of-the-Art Reactor Consequence Analysis Project, Vol. 2: Surry Integrated Analysis,” NUREG/CR-7110