

# Image-Based Correlation of Engine Operating Parameters with Occurrence and Duration of Diesel Fuel Injector Dribble

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**Abstract:** Fuel dribble, defined here as fuel delivery to the combustion chamber outside the intended high-pressure spray event, can negatively affect both fuel efficiency and pollutant emissions. Previously, ensemble-averaged images of dribble have been used to show that dribble exists even for properly functioning fuel injectors and occurred in discrete events, immediately following injection, during expansion, and during exhaust blowdown. Ensemble-averaged dribble exhibit changes to some parametric variations, however the mechanism(s) controlling fuel dribble remain unknown. This study looks for statistical correlations in instantaneous images for the occurrence and duration of single-cycle resolved dribble events with parameter variations that cover fuel type, fuel rail pressure, combustion effects, injector body manufacturer (all mini-sac type), orifice size, and injection schedule – including a post-injection. Our results are consistent with X-ray measurements in which ingested gasses entered the needle sac during dribble. Several possibilities for the transient behavior of this ingested gas and its impact on the other observed dribble features are discussed. For the various timing of dribble events recorded here, we estimate bounds for the contribution of dribble to losses in single cycle fuel efficiency and increases in emissions. As final note on boundary conditions for spray modeling, we recommend that the needle sac volume is proscribed to be mostly gas at the start of needle motion.



# Acknowledgements

## Mentors:

Supervisor: Dr. Mark Musculus,

Engine Department Manager: Dr. Paul Miles

## Hardware support:

Dave Cicone, Ken St. Hilaire, Keith Penny, Chris Carlen

## Injectors:

Cummins (XPI) Bosch (Lyle Pickett, spray B, ECN) Delphi

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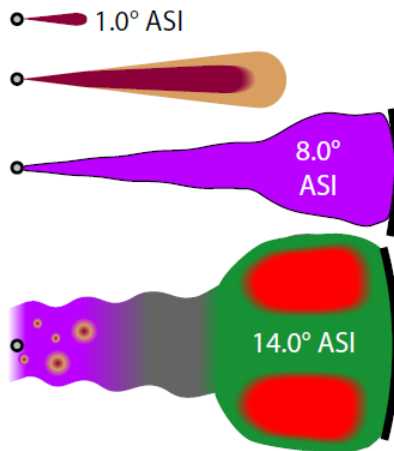
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# Building a conceptual understanding of dribble

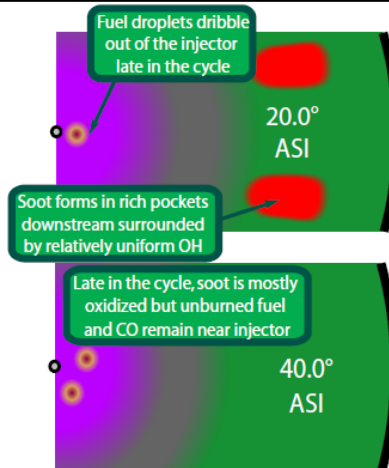
## Long-Term Objective

**Develop the science base of in-cylinder spray, combustion, and pollutant-formation processes for both conventional diesel and LTC that industry needs to design and build cleaner, more efficient engines**

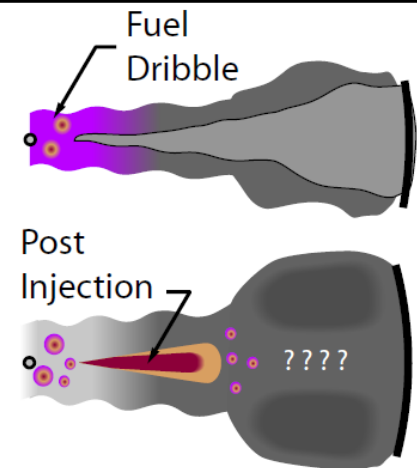
2012: LTC Diesel  
(Single Injection)








2013: Conventional and LTC  
(UHC + Soot Formation)





2014: Injector Dynamics  
(Multiple Injections)



 Liquid Fuel  
 Pre-ignition Vapor Fuel  
 First-Stage Ignition ( $\text{H}_2\text{CO}$ ,  $\text{H}_2\text{O}_2$ , CO, UHC)

 Intermediate Ignition (CO, UHC)  
 Second-Stage Ignition of Intermediate Stoichiometry or Diffusion Flame (OH)

 Second-Stage Ignition of fuel-rich mixtures  
 Soot or Soot Precursors (PAH)

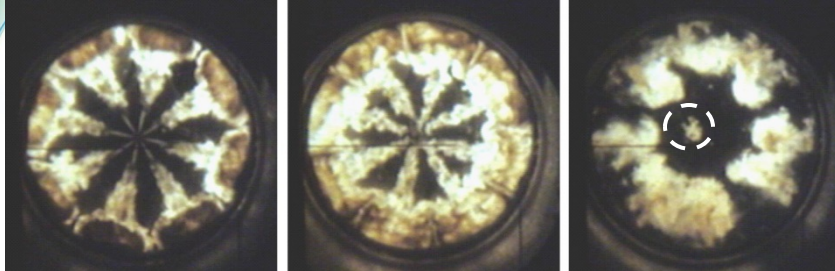


# Goals of this presentation

- Define dribble (and explain why we desire a definition)
- Describe some physical processes that affect dribble
- Examine how bad the problem is or could be

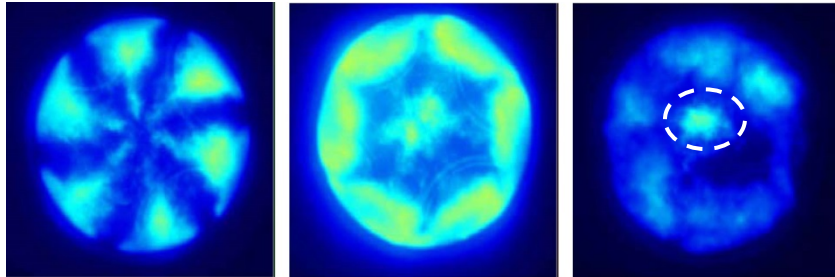


# Previous studies indicate dribble events at a wide range of conditions



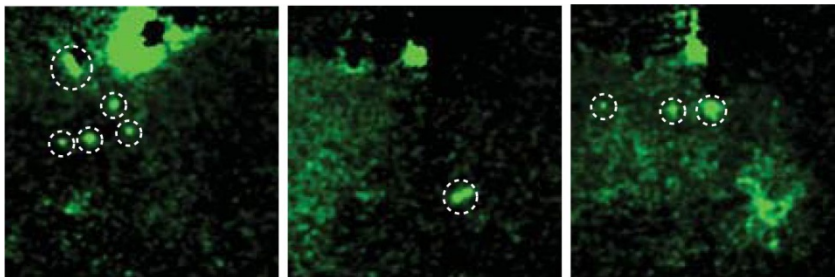
SAE 930971 (Dec, Sandia)

- Heavy-duty, diesel reference fuel
- Cam-driven, mini-sac injector
- Late soot at center



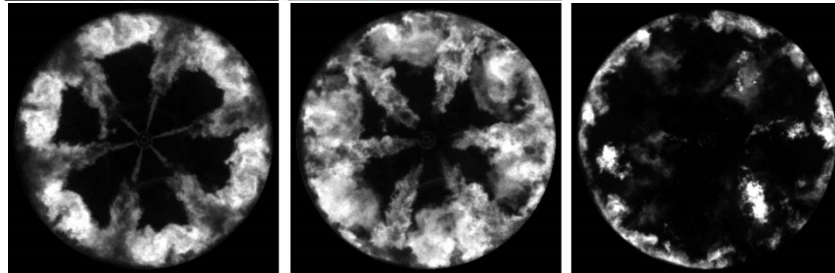
SAE 2005-01-3845 (Taschek et al., Aachen)

- Light-duty, diesel fuel
- Common-rail, mini-sac injector
- Conceptual model: Inj. sac vapor → soot



SAE 2009-01-1446 (Ekoto et al., Sandia)

- Light-duty, diesel fuel
- Common-rail, mini-sac injector
- Side-view PLIF, bright fuel droplets late



SAE 2001-01-2004 (Mueller et al., Sandia)

- Heavy-duty, diesel reference fuel
- HEUI, VCO injector
- No late soot at center (but sometimes yes)

# An incomplete list of candidate mechanisms affecting dribble

## Geometry

- Uncontrolled Volume
- Number of orifices

## Injector dynamics

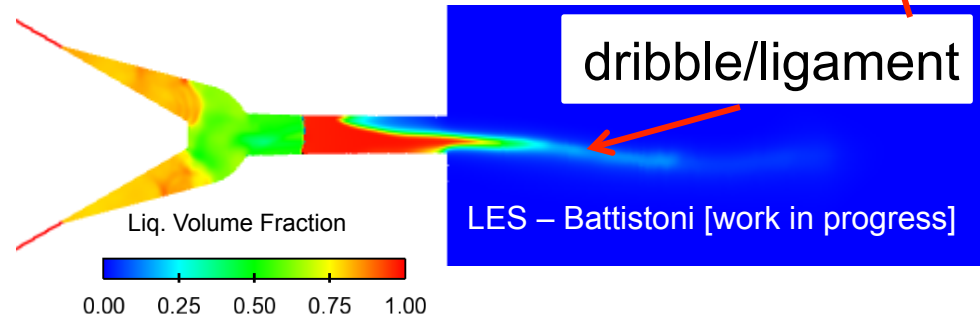
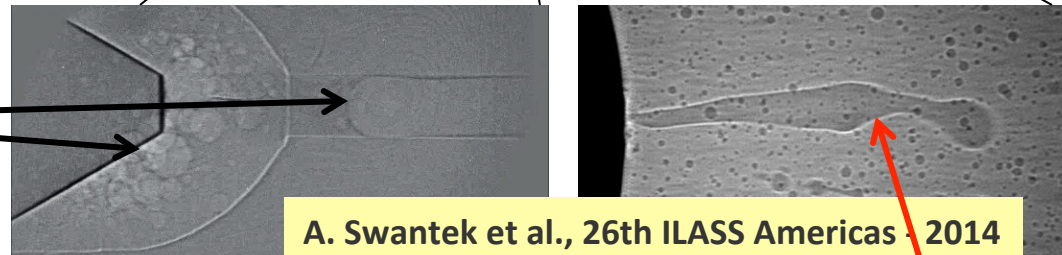
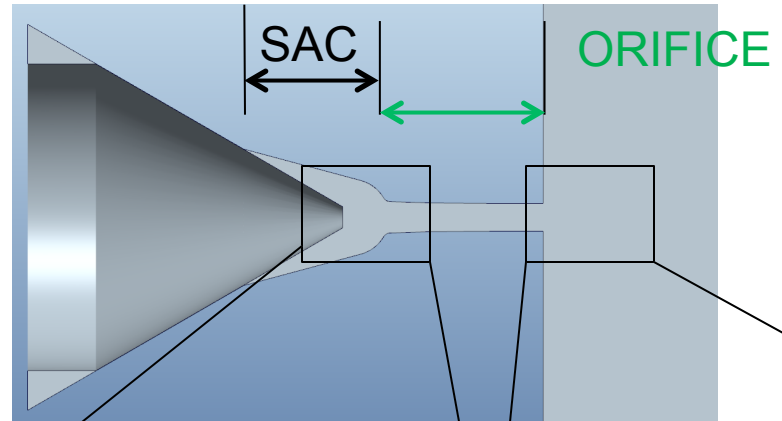
- Needle seal
- Needle bounce

## Ingested Gasses

## Fuel Compressibility

## Dissolved Gasses

## Multi-component mixture speed of sound



# Fate and transport of dribble

## Heavy Duty

~12mg/injection per 1bar [IMEP]

## Light Duty

~2mg/injection per 1bar [IMEP]

Mini-sac volumes (holes + sac)

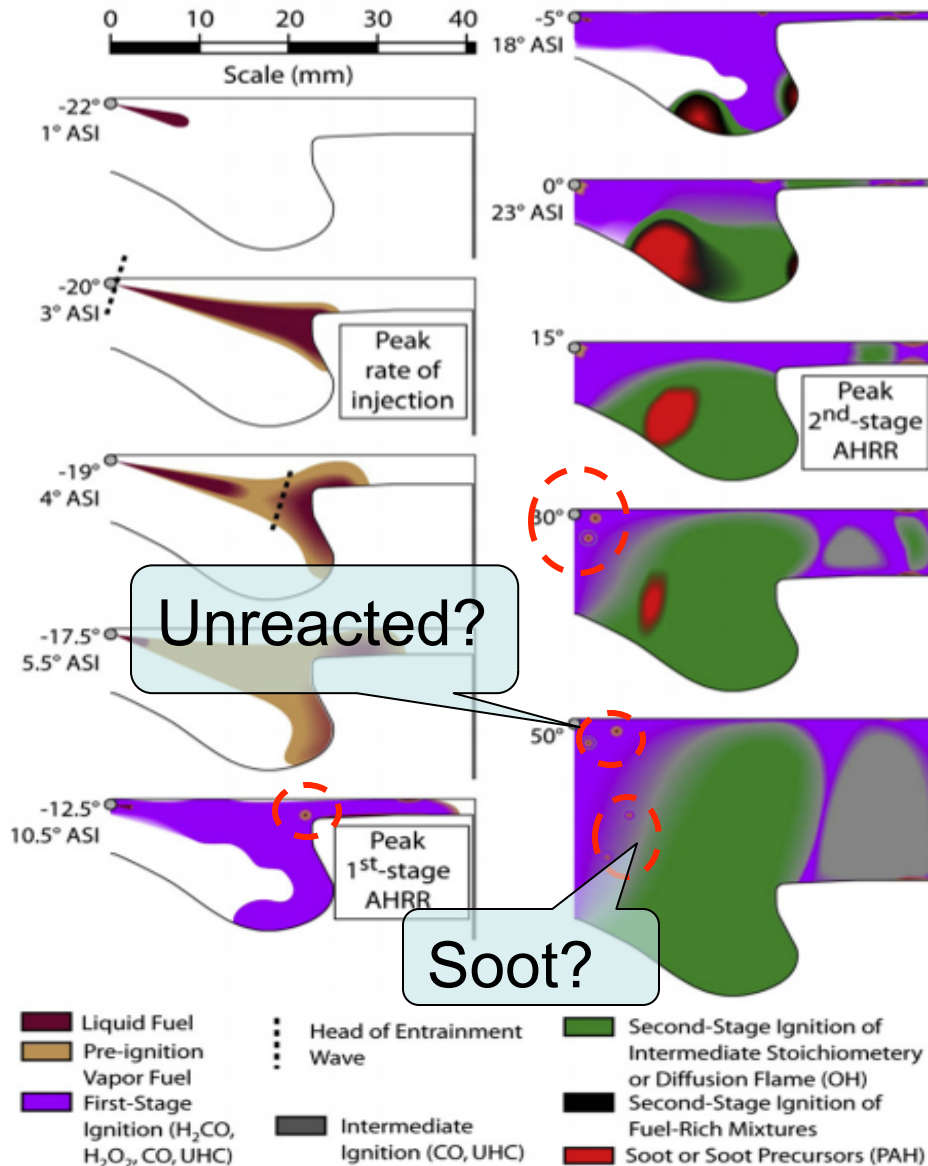
0.2-0.3mm<sup>3</sup> ~ 0.3mg/injection

## Sandia Heavy Duty Optical Engine

| IMEP                | 1 bar | 3 bar | 5 bar |
|---------------------|-------|-------|-------|
| Injections /kg-fuel | 4200  | 2100  | 1400  |
| Dribble [g/kg-fuel] | 1.49  | 0.73  | 0.49  |

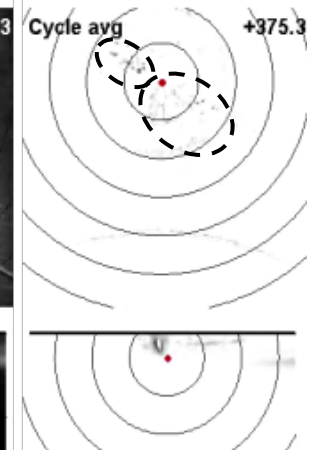
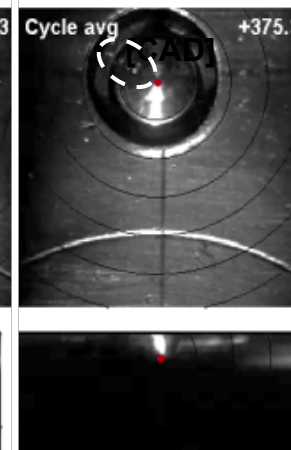
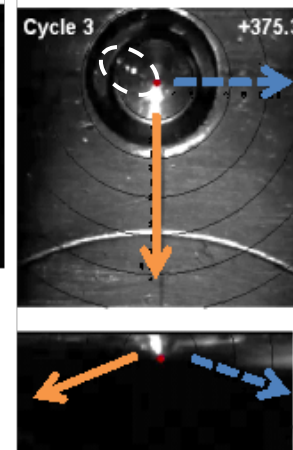
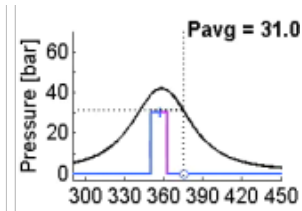
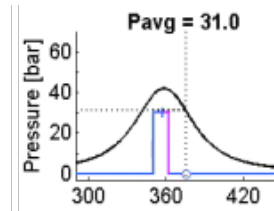
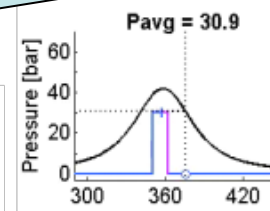
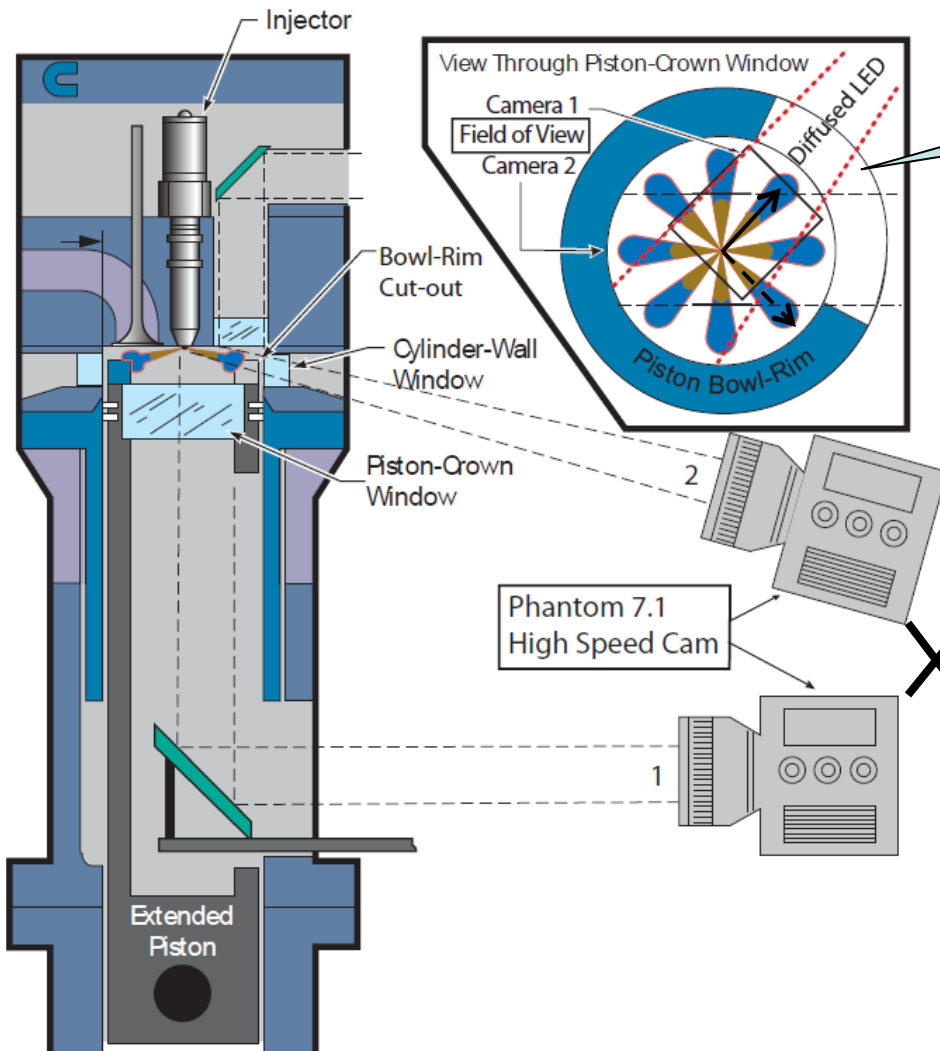
## Sandia Light Duty Optical Engine

| IMEP                | 6 bar | 9 bar | 12 bar |
|---------------------|-------|-------|--------|
| Injections /kg-fuel | 7100  | 5000  | 3800   |
| Dribble [g/kg-fuel] | 2.48  | 1.75  | 1.35   |



# Side-view dribble visualization at TDC requires bowl modifications

Large bowl-rim wall cut-out



Instantaneous

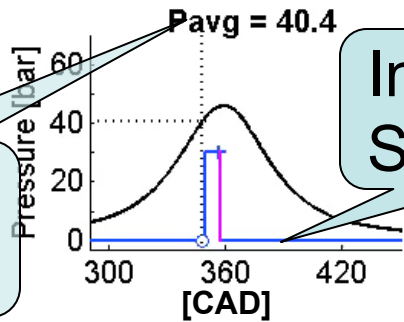
Cycle Averaged

Processed





cylinder  
pressure

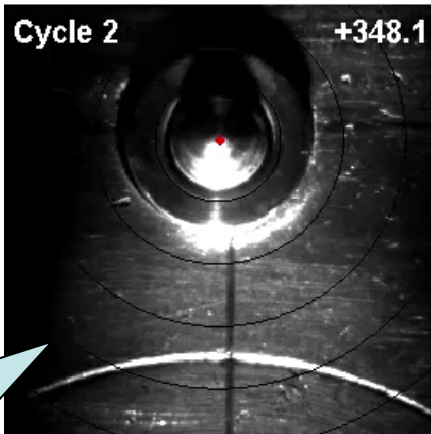


Injector  
SOI,DSE

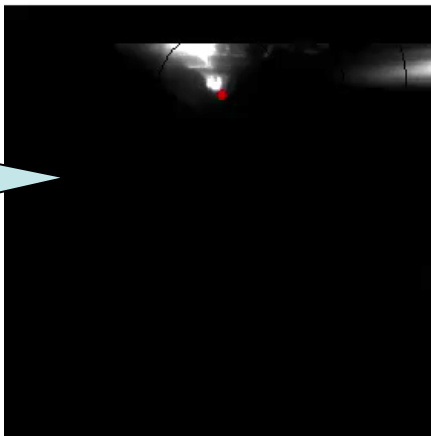
## Important concepts

A definition of dribble includes:

- **Liquid** and/or **vapor** fuel
- Dribble occurs in *multiple events*
- Dribble is *not due to malfunction*
- Dribble can contribute unburned hydrocarbons *directly to the exhaust*



Piston  
View  
35mm



Liner  
View

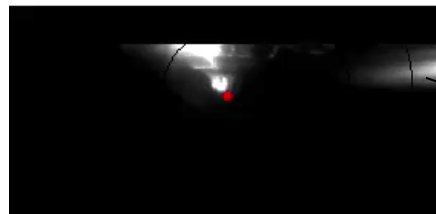
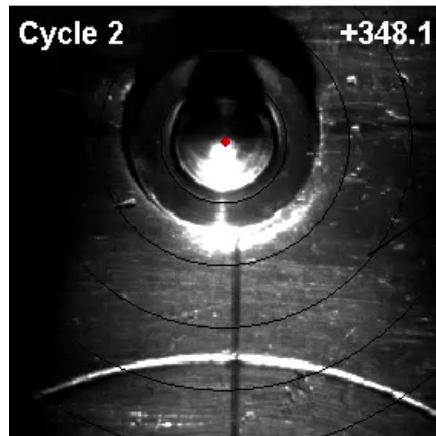
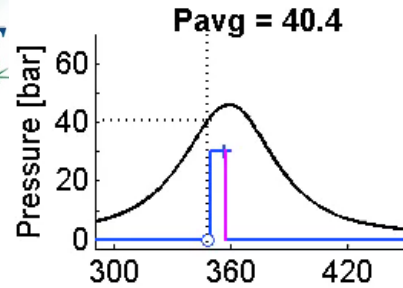
Full Cycle

|                       |                            |
|-----------------------|----------------------------|
| Fuel                  | Diesel #2, nC <sub>7</sub> |
| Intake                | 0%, 18% O <sub>2</sub>     |
| DSE                   | 1ms                        |
| T <sub>TDC</sub>      | 930 K                      |
| $\rho_{TDC}$          | 16.6 kg/m <sup>3</sup>     |
| Intake T              | 156 C                      |
| Intake P              | 2.14 bar                   |
| CR SOI                | 350° (TDC 360)             |
| Speed                 | 1200 rpm                   |
| Engine r <sub>c</sub> | 9.93                       |
| View                  | ~35 mm square              |
| Framing               | 25000 fps                  |
| Filter                | None                       |

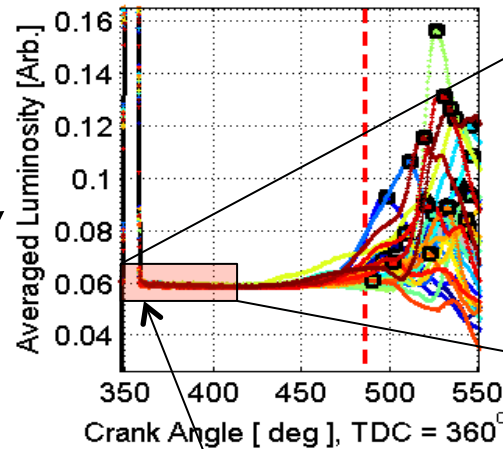
Boosted  
intake

Low  
compression

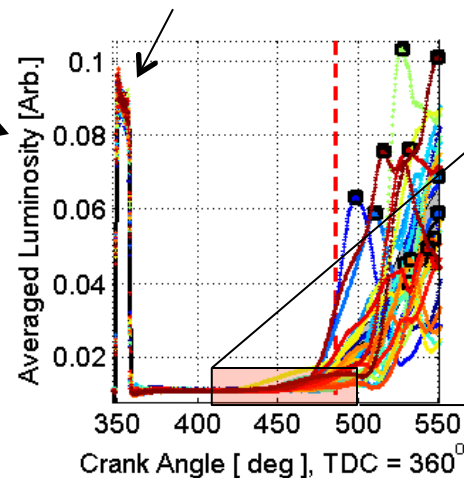
# Processing Dribble Movies



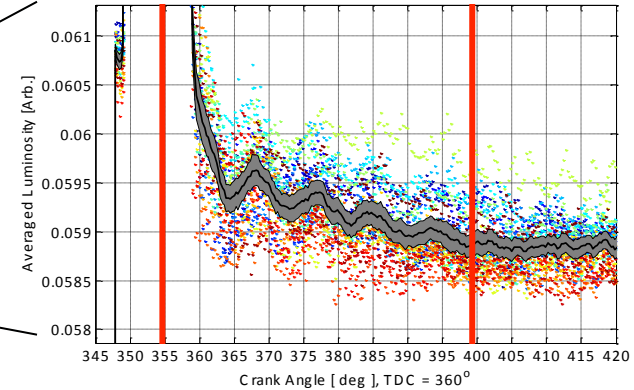
Dribble amount difficult to quantify from luminosity. But timing of different dribble events is possible.



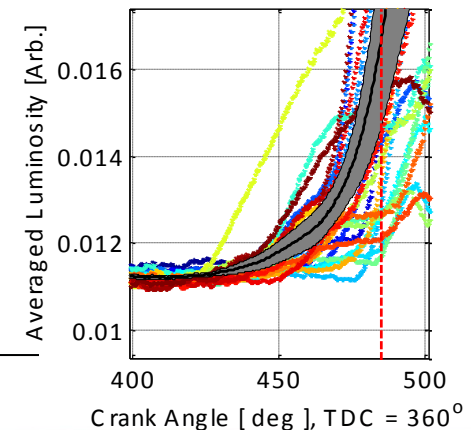
Injection



Immediate dribble



Late Dribble, condensation

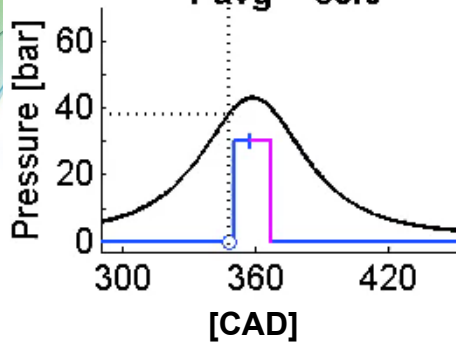




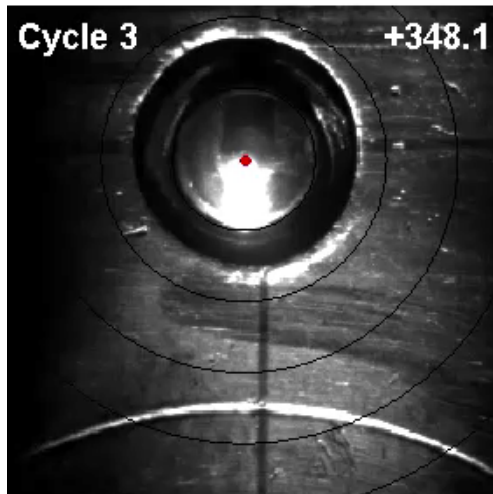
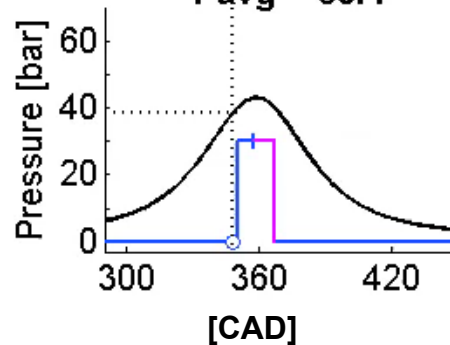


# Dribble is not a single event, but distribution among events is sensitive to fuel type

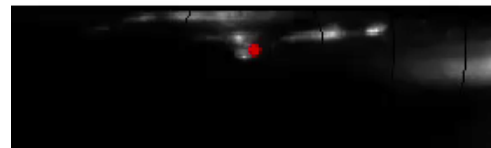
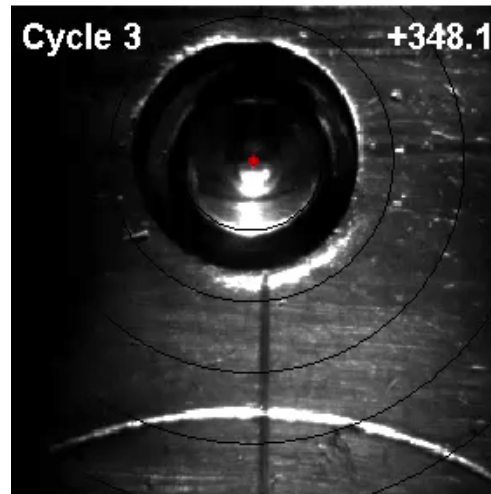
$P_{avg} = 38.0$



$P_{avg} = 38.4$



0.09mm XPI  
D2 1000bar



0.13mm XPI  
nC<sub>7</sub> 1000bar

- **Immediate Dribble**

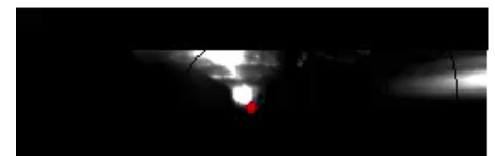
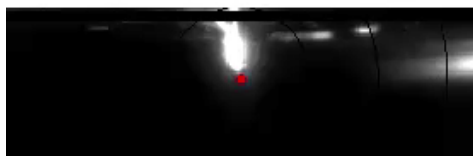
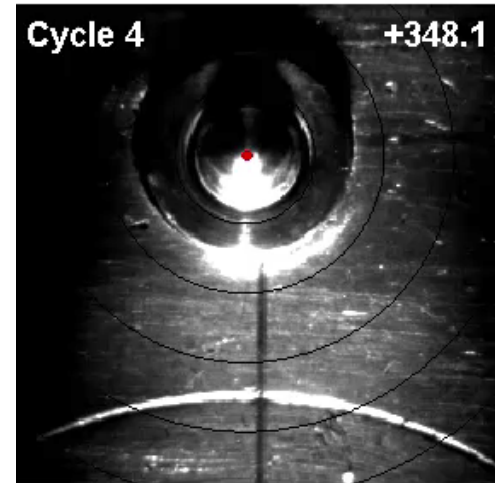
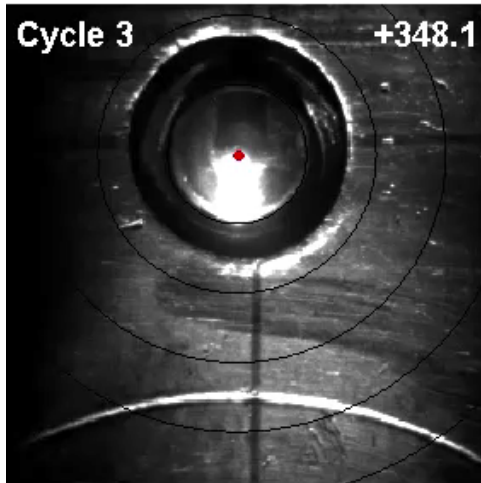
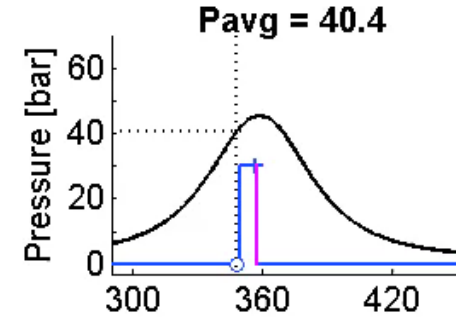
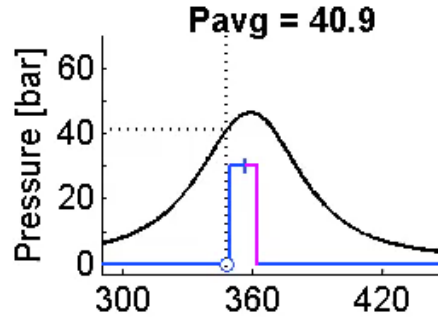
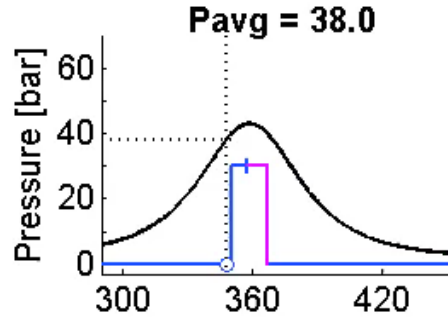
- Liquid droplets
- Hole-to-hole variation

- **Late Dribble**

- Cylinder pressure actuation
- Liquid or vapor which may condense back to liquid
- Dribble exiting directly to exhaust (during blowdown)

|              |                   |
|--------------|-------------------|
| Intake       | 0% O <sub>2</sub> |
| DSE          | 1ms               |
| Intake T     | 156 C             |
| Intake P     | 2.14 bar          |
| CA SOI       | 350° (TDC 360)    |
| Speed        | 1200 rpm          |
| Engine $r_c$ | 9.93              |
| View         | ~35 mm square     |
| Framing      | 25000 fps         |
| Filter       | None              |

# Dribble is not a malfunction, and exists for a range of orifice sizes and injector manufacturers

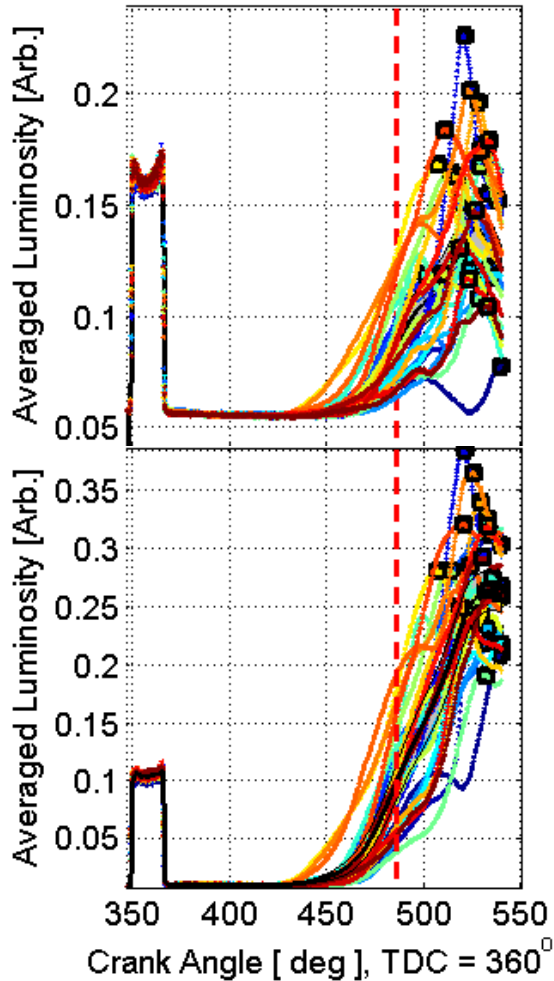


0.09mm XPI  
D2, 1000bar

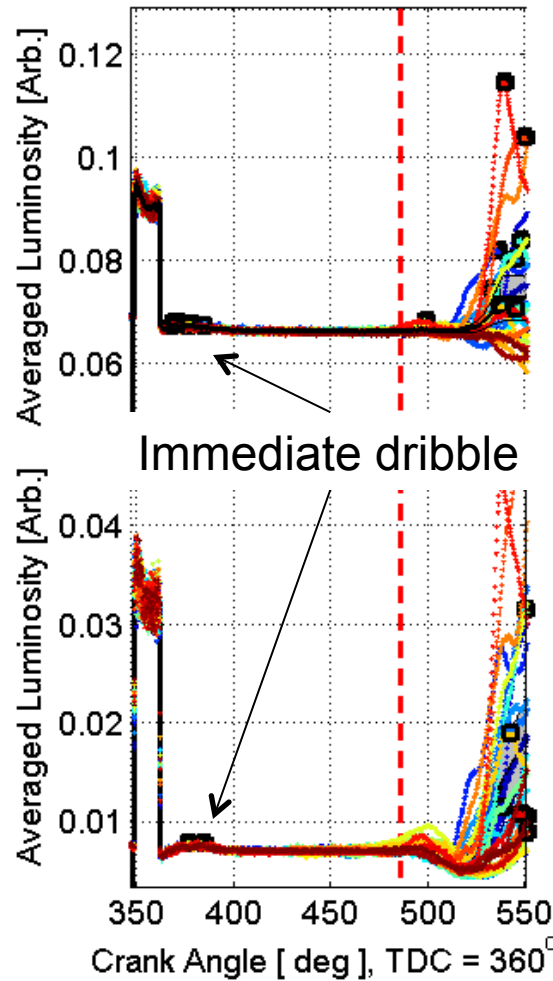
0.09mm Bosch  
D2, 1000bar

0.13mm Delphi  
D2, 1000bar

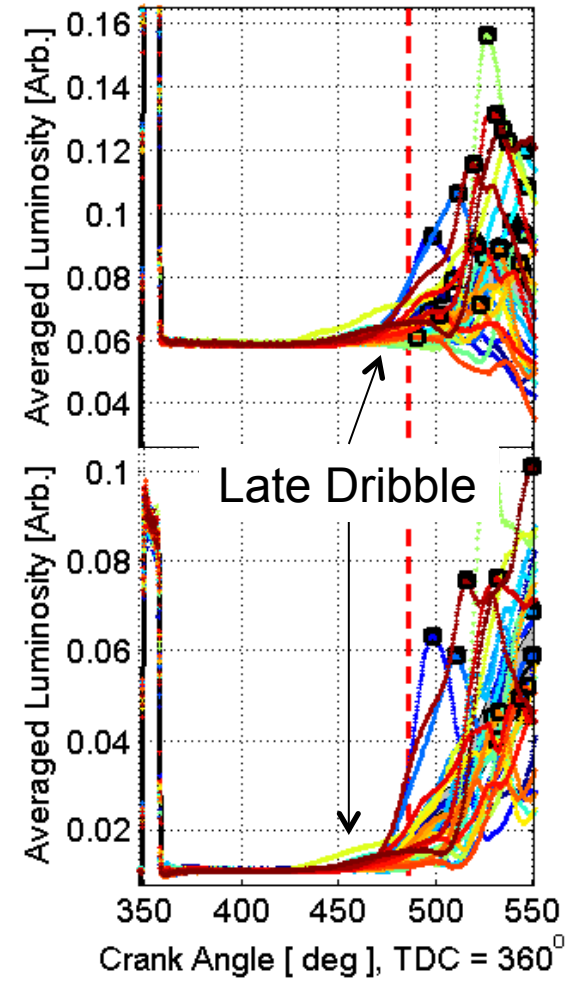
# Instantaneous Dribble from motored injections at 0% $O_2$



0.09mm XPI  
D2, 1000bar

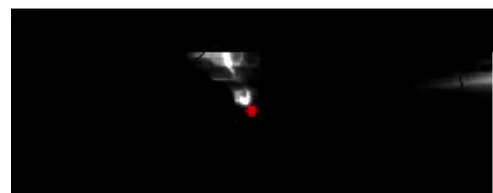
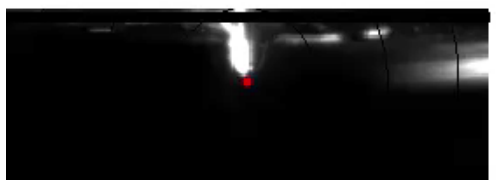
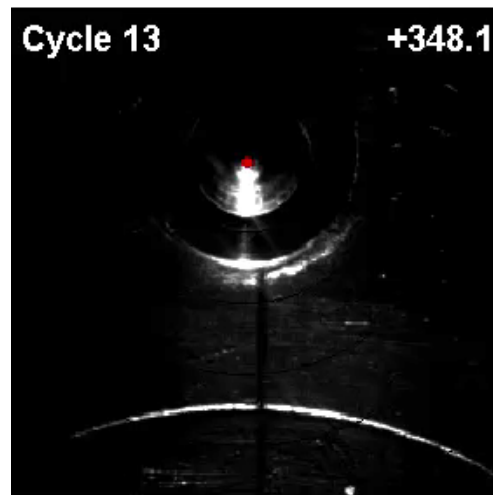
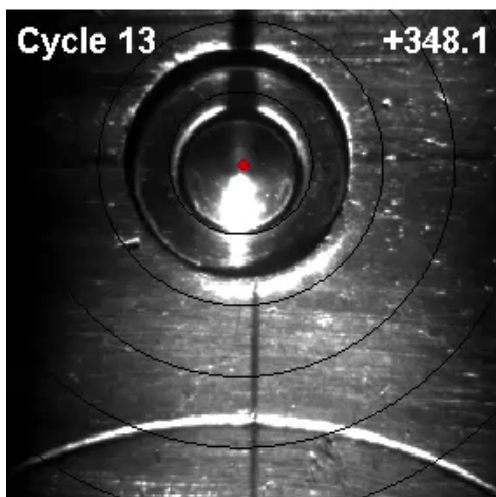
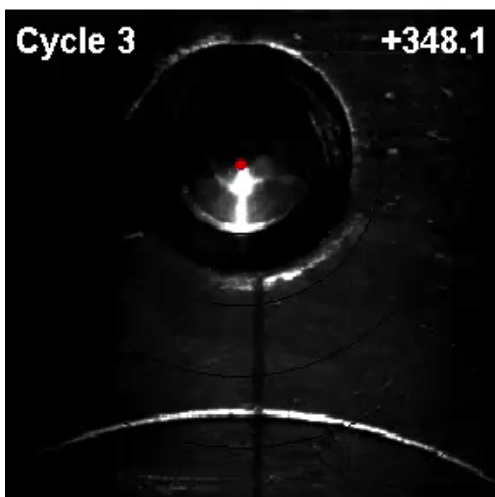
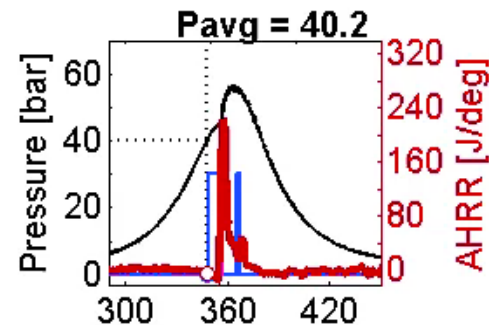
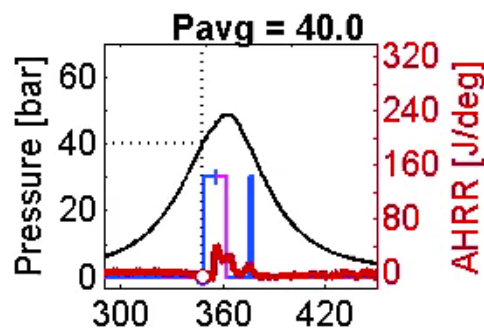
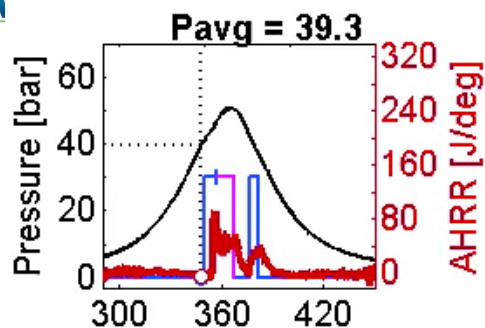


0.09mm Bosch  
D2, 1000bar



0.13mm Delphi  
D2, 1000bar

# Dribble occurs after both main and post injection



0.09mm XPI  
nC<sub>7</sub>, 1000bar

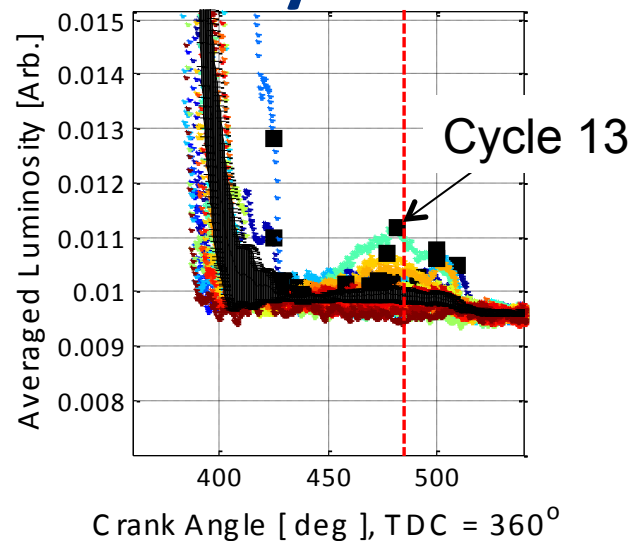
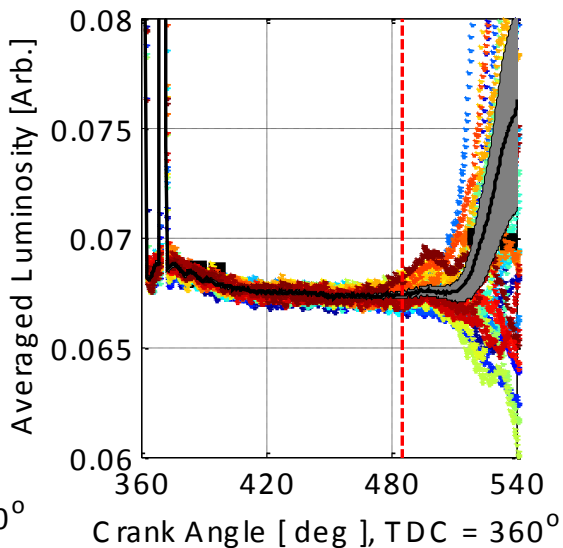
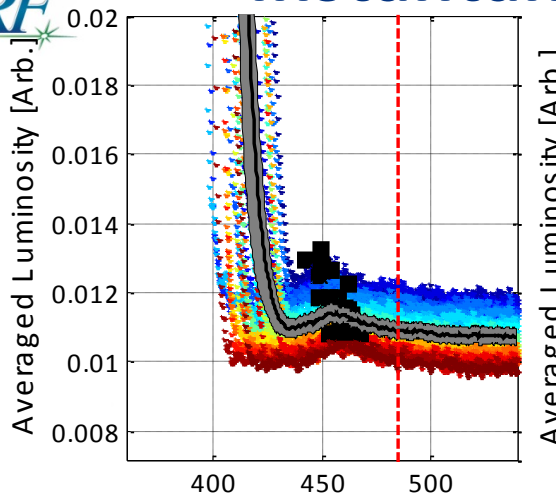
0.09mm Bosch  
D2, 1000bar

0.13mm Delphi  
D2, 1000bar

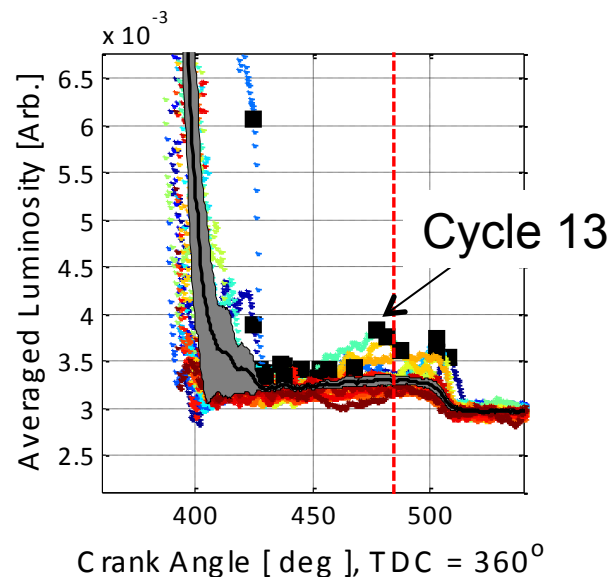
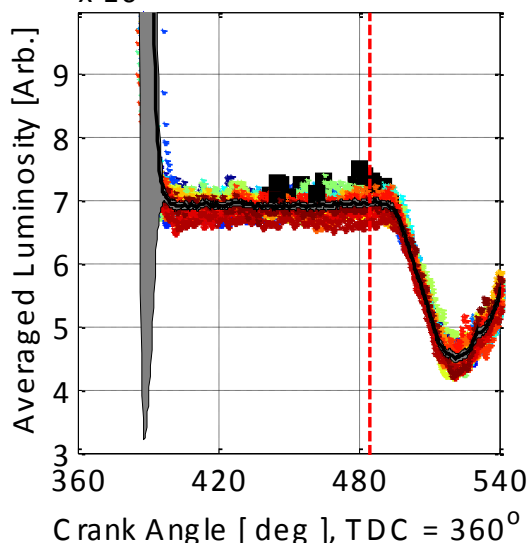
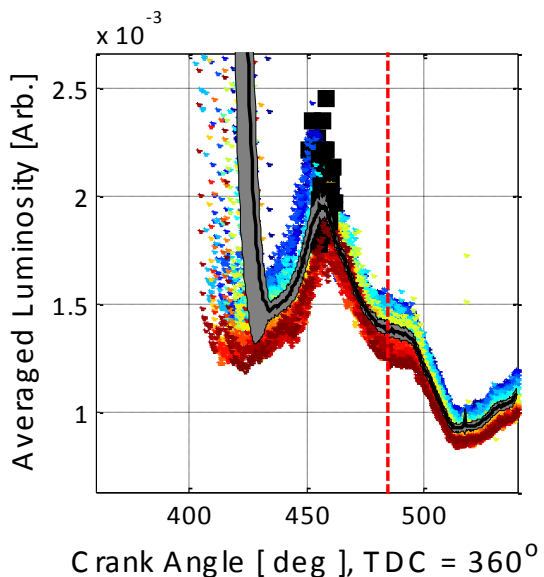


# Instantaneous Dribble from fired cycles

Bottom View



Side View

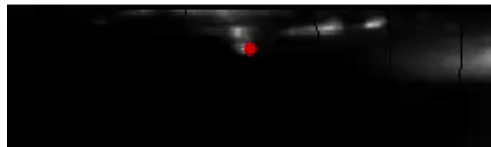
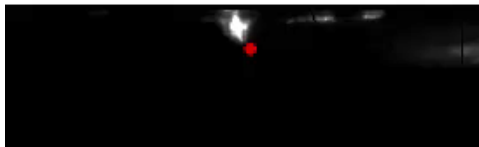
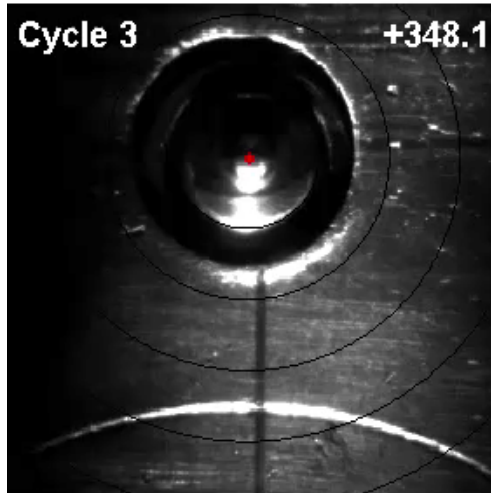
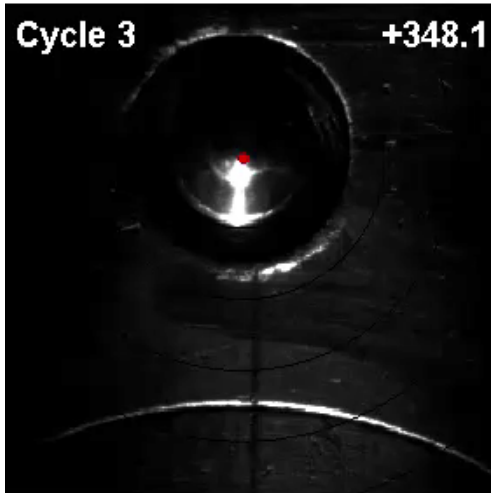
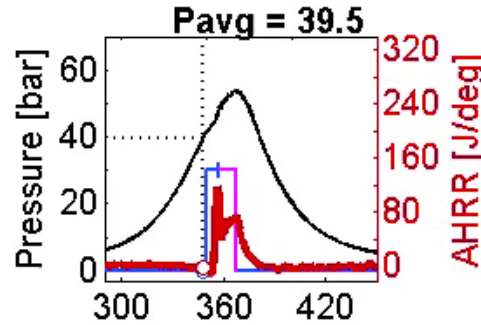
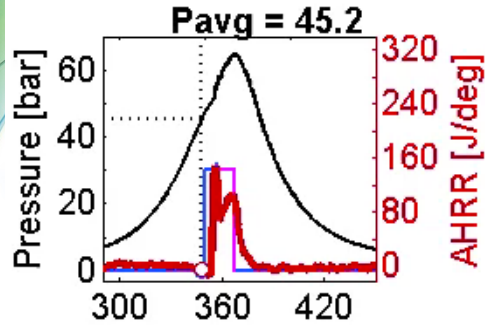


0.09mm XPI  
nC<sub>7</sub>, 1000bar

0.09mm Bosch  
nC<sub>7</sub>, 1000bar

0.13mm Delphi  
D2, 1000bar

# Heat release has minimal effect on dribble, demonstrates UHC can go directly to exhaust



0.09mm XPI  
D2 1000bar

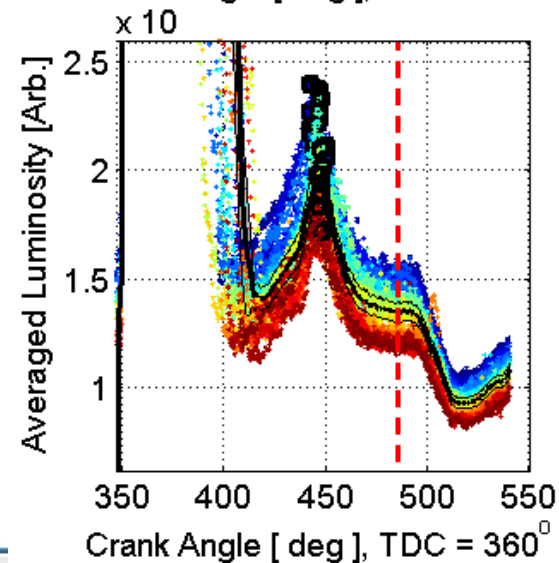
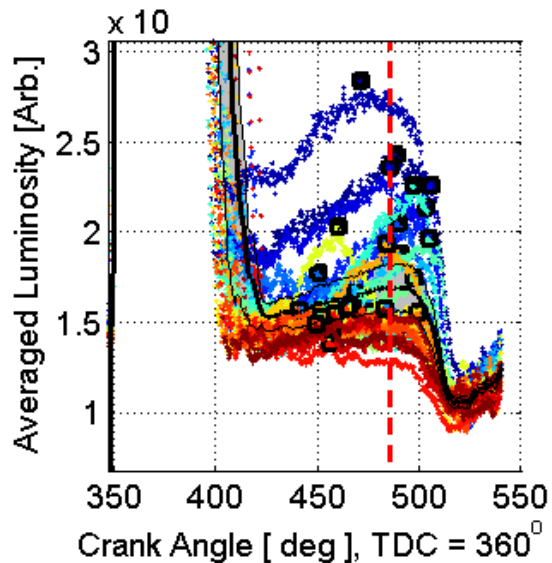
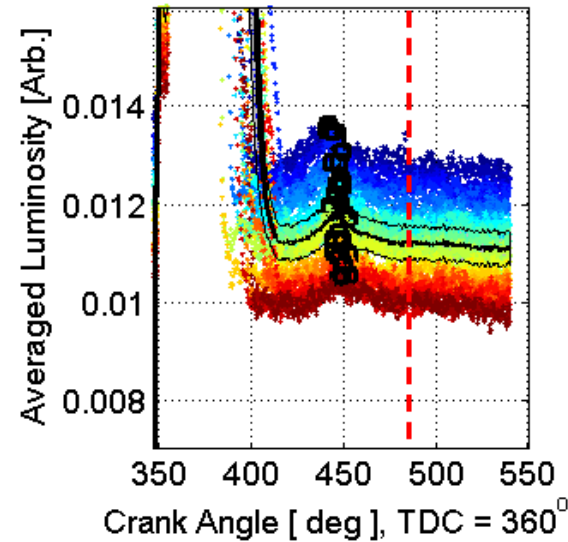
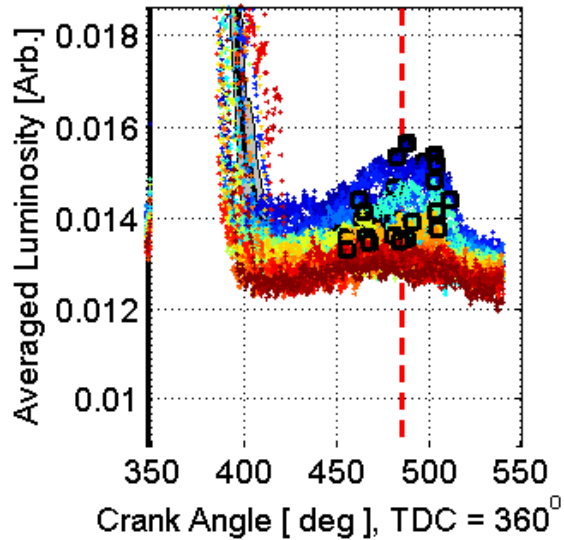
0.09mm XPI  
nC<sub>7</sub> 1000bar

- Immediate Dribble
  - Liquid droplets (soot)
- Late Dribble
  - Pressure driven
  - Vapor or liquid (UHC)

|                       |                    |
|-----------------------|--------------------|
| Intake                | 18% O <sub>2</sub> |
| DSE                   | 1ms                |
| Intake T              | 156 ± 2C           |
| Intake P              | 2.06 bar           |
| CA SOI                | 350° (TDC 360)     |
| Speed                 | 1200 rpm           |
| Engine r <sub>c</sub> | 9.93               |
| View                  | ~35 mm square      |
| Framing               | 25000 fps          |
| Filter                | None               |

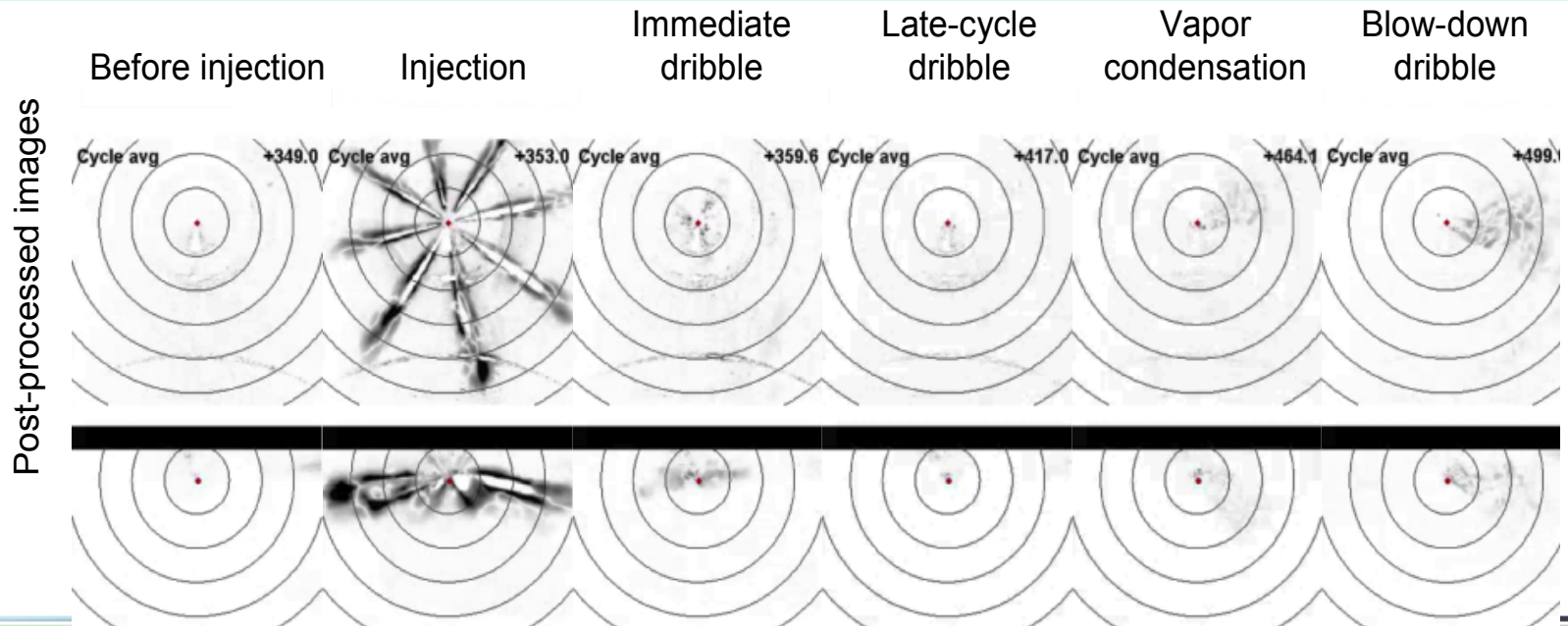


# Diesel fuel dribble condensation shows greater stochasticity than n-heptane

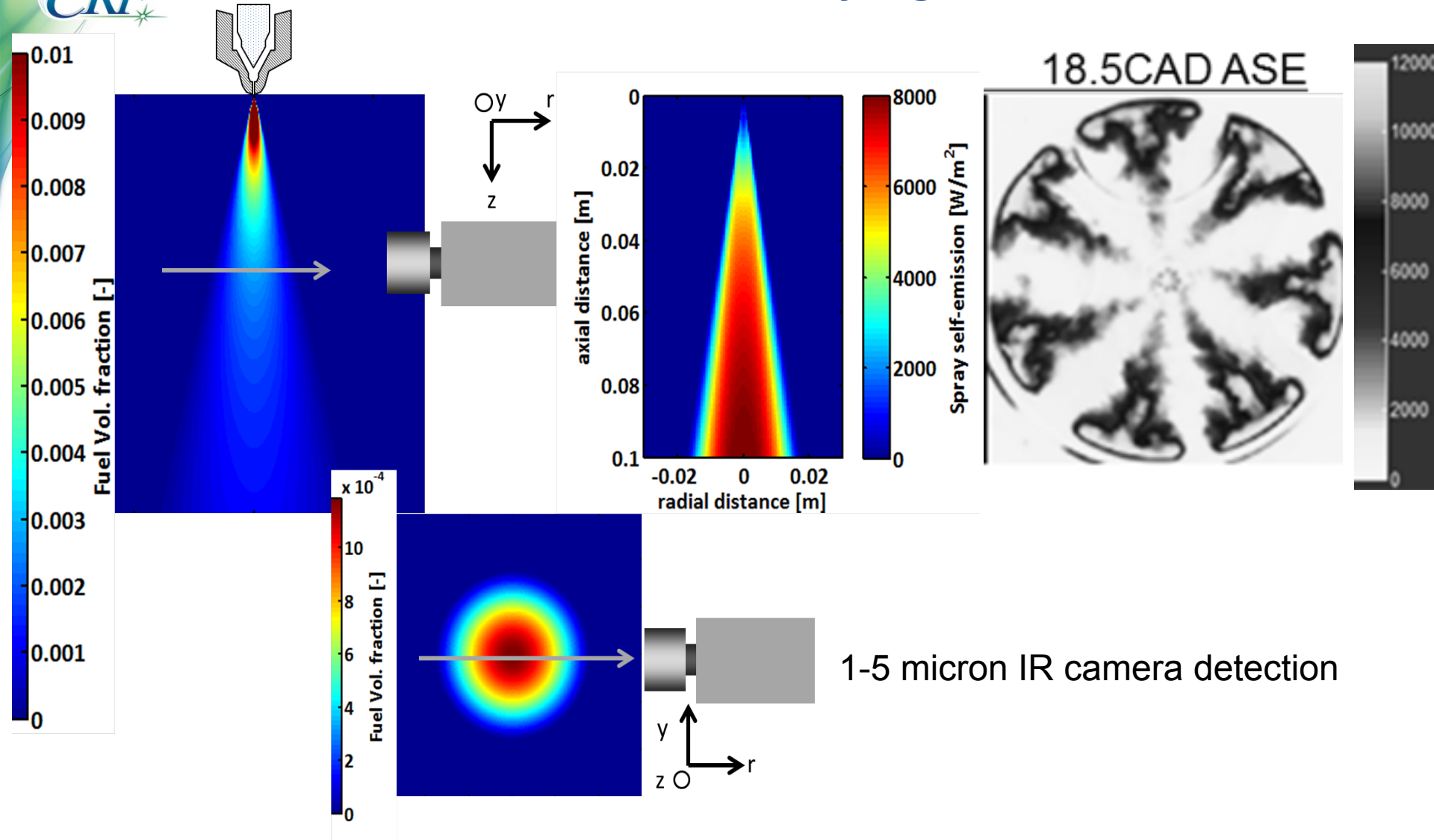


# Summary

- Dribble, as defined here, is ***not due to malfunction***  
(the term 'leaking injector' is preferable in such cases)
- Dribble occurs in ***multiple events***
- Dribbled fuel may emerge as either ***liquid droplets or fuel vapors***
- Dribble contributes some unburned hydrocarbons ***directly to the exhaust***
- ***Stochastic behavior of dribble between different types***



# Future work – Quantifying Dribbled Fuel



Infrared Emission/Absorption from fuel at the injector tip (3.4 micron bandpass filter)

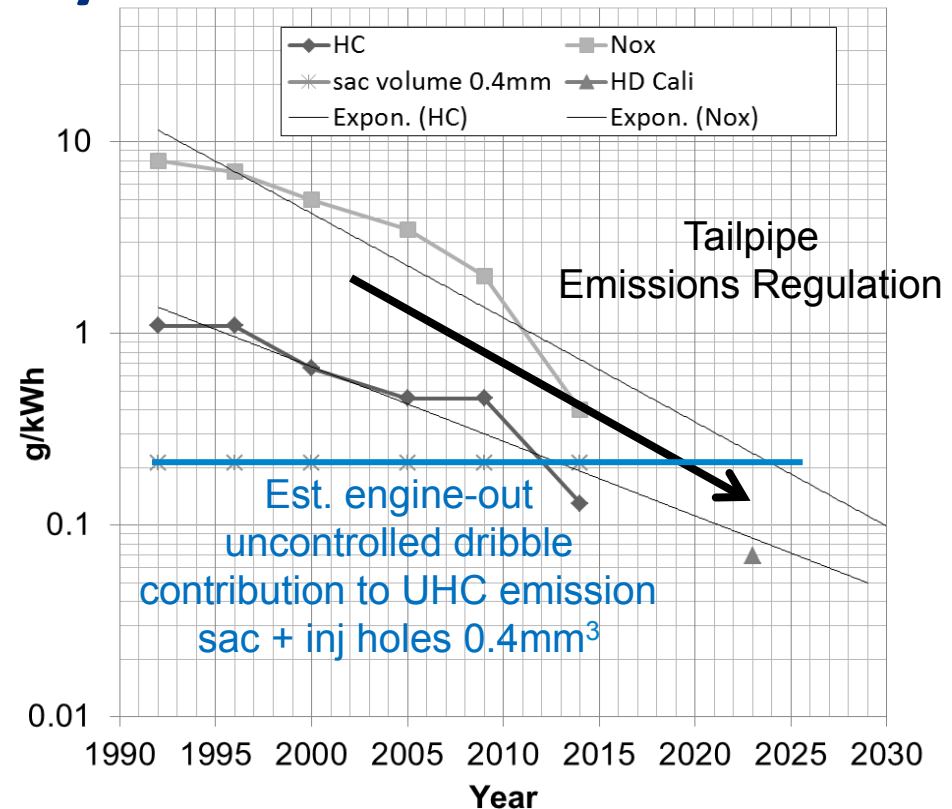


# Impact on industry and the environment

$$m_{\downarrow dribble} / inj = 0.2 \cdot m_{\downarrow fuel\_sac}$$

## Sandia Heavy Duty Optical Engine

| IMEP                        | 1 bar | 3 bar | 5 bar |
|-----------------------------|-------|-------|-------|
| Injections/<br>kg-fuel      | 42000 | 21000 | 14000 |
| Est. Dribble<br>[g/kg-fuel] | 2.8   | 1.4   | 0.94  |



- The emission factor g/kg\_fuel allows us to estimate the total impact of dribble wrt HC emission and total fuel use.
- Los Angeles on-road diesel fuel usage of  $2.9 \times 10^9$  L fuel/yr  
Fleet-average tailpipe emission of 2.1g/kg\_fuel\*

**Diesel fleet exhausts roughly 14,000 kg of fuel per day!**

‡Greeves, G., Khan, I.M., Wang, C.H.T., Fenne, I.: Origins of Hydrocarbon Emissions from Diesel Engines. SAE Tech. Pap. (1977).

\* Bishop, G.A., Stedman, D.H.: Remote Measurements of On-Road Emissions from Heavy-Duty Diesel Vehicles in California; Year 5, 2012. 1–35 (2013).

# Conclusions

- Significant impacts on dribble by further reductions in sac+orifice volumes is unlikely, and so **requires mechanistic understanding to further mitigate.**
- Because **dribble is a per-injection event**, contributions from dribble are expected to increase with decreasing load. (i.e. lowest for heavy-duty full-load and highest for light-duty, low-load)
  - Worst case presented:  $(2.48 \text{ g/kgf}) * (1\text{kgf}/48\text{MJ}) * (3.6\text{MJ}/0.4\text{kWh}) = \mathbf{0.465 \text{ g/kWh}}$ 
    - As a baseline, Euro VI UHC emissions targets are **0.55g/kWhr**
    - but note: the problem gets relatively 'worse' with better fuel economy!
- **Fuel type** had the most significant (visual) impact on dribble, and other fuels should be investigated
  - Drastic difference in amount and character of dribble events
  - Opposite trends in dribble distribution between immediate and late with rail pressure
- Still, **other sources of UHC's exist.** Crevices and/or wall wetting may contribute as much or more depending on operating condition



# Back-up Slides





# Engine Operating Parameters

|                     | SSE/DSE<br>[CAD/ms] ‡ | SSE/DSE2<br>[CAD/ms] ‡ | P <sub>rail</sub><br>[bar] ‡ | Motored Speed<br>[RPM] ‡ | Cylinder Gas‡      |
|---------------------|-----------------------|------------------------|------------------------------|--------------------------|--------------------|
| Spray Start         | -/1.0                 | -/-                    | 1000                         | 0                        | 100% N2            |
| TDC timing          | 347/1.0               | *                      | *                            | 1200                     | *                  |
| Early timing        | 327/1.0               | *                      | *                            | *                        | *                  |
| Late timing         | 357/1.0               | *                      | *                            | *                        | *                  |
| w/post              | 347/1.0               | 371/0.350 <sup>†</sup> | *                            | *                        | *                  |
| High P TDC          | *                     | -/-                    | 1600 <sup>††</sup>           | *                        | *                  |
| Low P TDC           | *                     | *                      | 800                          | *                        | *                  |
| Fired TDC           | *                     | *                      | 1000                         | Skip Fired 10Hz          | 18% O <sub>2</sub> |
| Fired TDC<br>w/post | *                     | 363/0.350              | *                            | *                        | *                  |
| Spray End           | -/1.0                 | -/-                    | *                            | 0                        | 100% N2            |

|                 | Diesel Certification<br>Fuel (2007) | n-Heptane               |
|-----------------|-------------------------------------|-------------------------|
| Density         | 841.7 kg/m <sup>3</sup>             | 687.3 kg/m <sup>3</sup> |
| Viscosity (STP) | 2.35 cs                             | 0.6285 cs               |
| Cetane Number   | 45.7                                | 56                      |

| Engine Variable         | Operating Condition          | Cameras            | Phantom 7.1             |
|-------------------------|------------------------------|--------------------|-------------------------|
| Engine Speed            | 1200 ±10 RPM*                | Frame Rate         | 25kHz (40μs)            |
| Engine Load Range       | 1-6 bar gIMEP <sup>†</sup>   | Exposure Time      | 25 μs                   |
| Intake O <sub>2</sub>   | 0%, 18.0% ± 0.2              | LED delay/duration | 7 μs / 15 μs            |
| Intake Pressure         | 206 ± 10 kPa                 | Lens               | Nikon 55mm, 85mm        |
| Intake Temperature      | 156 ± 2°C                    | f/#                | 1.8, 2.0 (respectively) |
| Intake Mass Flow        | 41.4 ±0.5g/s                 | Fuel Rail Pressure | 800, 1000, 1600 ±20 bar |
| TDC Motored Density     | 16.6 ± 0.4 kg/m <sup>3</sup> | BDC Pressure       | 164 ± 10 kPa            |
| TDC Motored Temperature | 936 K                        | BDC Temperature    | 78 ±4°C                 |



# Injector Operating Parameters

| Fuel injector build(# tested)  | Cummins XPI (3)   | Bosch 'ECN Spray B' (1) | Delphi DFI-1.5 (1) |
|--|-------------------|-------------------------|--------------------|
| Number of holes & arrangement  | 8, equally-spaced | 3                       | 8, equally spaced  |
| Pull-in / Hold Current [amps]  | 21 / 12           | 18 / 12                 | 16.5 / 7           |
| Nozzle Tip   | 0.090mm, 152°     |                         |                    |
| [orifice diameter, spray incl. angle]  | 0.131mm, 152°     |                         |                    |
|  | 0.200mm, 152°     | 0.090mm, 145°           | 0.200mm, 156°      |
|  | 0.200mm, 160°     |                         |                    |
| Start of injection (SOI)   | 0.400ms [2.9CAD]  |                         |                    |
| delay from start of solenoid energizing (SSE) at 1000bar rail pressure*  | 0.400ms [2.9CAD]  | 0.320ms [2.3 CAD]       | 0.320ms [2.3 CAD]  |
|  | 0.480ms [3.4 CAD] |                         |                    |
|  | 0.360ms [2.6 CAD] |                         |                    |
| Extra duration of injection (EDOI) for a duration of solenoid energizing (DSE) of 1ms at 1000bar rail pressure | 1.400ms           |                         |                    |
|  | 0.700ms           | 0.840ms [6.0 CAD]       | 0.160ms[1.2 CAD]   |
|  | 0.000ms           |                         |                    |
|  | 0.400ms           |                         |                    |

\*SOI and EOI determined from optical imaging,  $\pm 0.04$ ms