

# Upscaling Material Properties and Damage in Peridynamics

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and Partial Differential Equations

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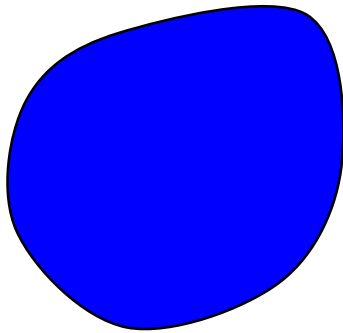
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# Outline

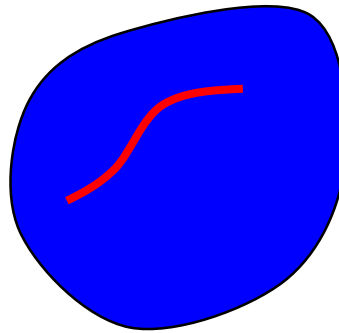
- Peridynamics background
  - Linearized model
- Peridynamics and multiscale
  - Concurrent hierarchical multiscale method
- Upscaling for multiscale material properties
  - Constrained minimization
  - Crack example
  - Time-dependent form
  - Implications for molecular dynamics

# Purpose of peridynamics\*

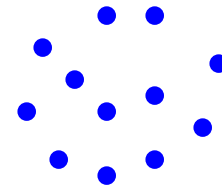
- To unify the mechanics of continuous and discontinuous media within a single, consistent set of equations.



Continuous body



Continuous body  
with a defect



Discrete particles

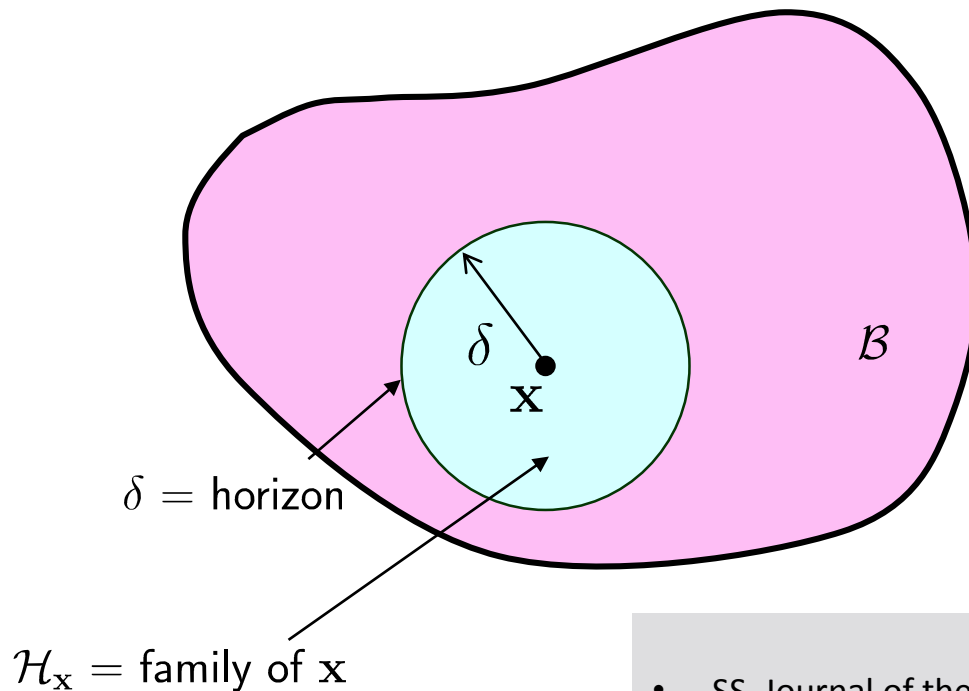
- Why do this?
  - Avoid coupling dissimilar mathematical systems (A to C).
  - Model complex fracture patterns.
  - Communicate across length scales.

\* Peri (near) + dyn (force)

# Peridynamics basics:

## Horizon and family

- Any point  $\mathbf{x}$  interacts directly with other points within a distance  $\delta$  called the “horizon.”
- The material within a distance  $\delta$  of  $\mathbf{x}$  is called the “family” of  $\mathbf{x}$ ,  $\mathcal{H}_{\mathbf{x}}$ .

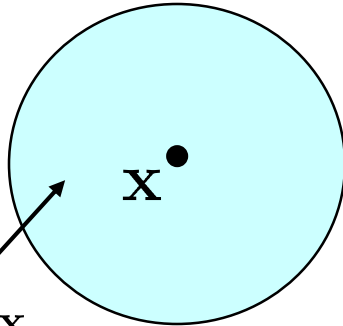


### General references

- SS, Journal of the Mechanics and Physics of Solids (2000)
- SS and R. Lehoucq, Advances in Applied Mechanics (2010)
- Madenci & Oterkus, *Peridynamic Theory & Its Applications* (2014)

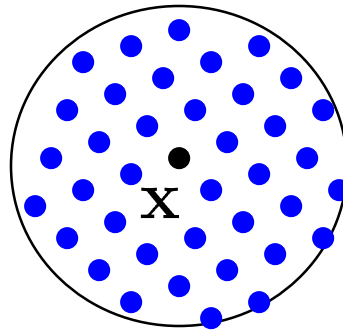
# Point of departure: Strain energy at a point

Continuum

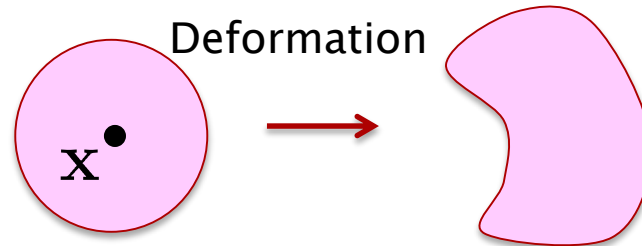
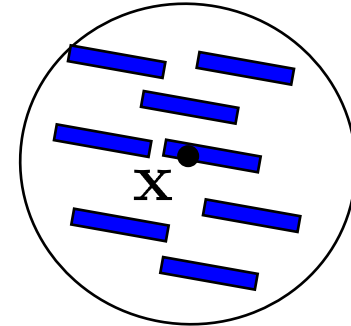


Family of  $x$

Discrete particles



Discrete structures



- Key assumption: the strain energy density at  $x$  is determined by the deformation of its family.

# Potential energy minimization yields the peridynamic equilibrium equation

- Potential energy:

$$\Phi = \int_{\mathcal{B}} (W - \mathbf{b} \cdot \mathbf{y}) dV_{\mathbf{x}}$$

where  $W$  is the strain energy density,  $\mathbf{y}$  is the deformation map,  $\mathbf{b}$  is the applied external force density, and  $\mathcal{B}$  is the body.

- Euler-Lagrange equation is the equilibrium equation:

$$\int_{\mathcal{H}_{\mathbf{x}}} \mathbf{f}(\mathbf{q}, \mathbf{x}) dV_{\mathbf{q}} + \mathbf{b}(\mathbf{x}) = 0$$

for all  $\mathbf{x}$ .  $\mathbf{f}$  is the *pairwise bond force density*.

# Peridynamic vs. local equations

- The structures of the theories are similar, but peridynamics uses nonlocal operators.
  - Notation: State<bond>=vector

<i>Relation</i>	<i>Peridynamic theory</i>	<i>Standard theory</i>
Kinematics	$\underline{\mathbf{Y}}\langle \mathbf{q} - \mathbf{x} \rangle = \mathbf{y}(\mathbf{q}) - \mathbf{y}(\mathbf{x})$	$\mathbf{F}(\mathbf{x}) = \frac{\partial \mathbf{y}}{\partial \mathbf{x}}(\mathbf{x})$
Linear momentum balance	$\rho \ddot{\mathbf{y}}(\mathbf{x}) = \int_{\mathcal{H}} \left( \mathbf{t}(\mathbf{q}, \mathbf{x}) - \mathbf{t}(\mathbf{x}, \mathbf{q}) \right) dV_{\mathbf{q}} + \mathbf{b}(\mathbf{x})$	$\rho \ddot{\mathbf{y}}(\mathbf{x}) = \nabla \cdot \boldsymbol{\sigma}(\mathbf{x}) + \mathbf{b}(\mathbf{x})$
Constitutive model	$\mathbf{t}(\mathbf{q}, \mathbf{x}) = \underline{\mathbf{T}}\langle \mathbf{q} - \mathbf{x} \rangle, \quad \underline{\mathbf{T}} = \hat{\underline{\mathbf{T}}}(\underline{\mathbf{Y}})$	$\boldsymbol{\sigma} = \hat{\boldsymbol{\sigma}}(\mathbf{F})$
Angular momentum balance	$\int_{\mathcal{H}} \underline{\mathbf{Y}}\langle \mathbf{q} - \mathbf{x} \rangle \times \underline{\mathbf{T}}\langle \mathbf{q} - \mathbf{x} \rangle dV_{\mathbf{q}} = \mathbf{0}$	$\boldsymbol{\sigma} = \boldsymbol{\sigma}^T$
Elasticity	$\underline{\mathbf{T}} = W_{\underline{\mathbf{Y}}} \text{ (Fréchet derivative)}$	$\boldsymbol{\sigma} = W_{\mathbf{F}} \text{ (tensor gradient)}$
First law	$\dot{\varepsilon} = \underline{\mathbf{T}} \bullet \dot{\underline{\mathbf{Y}}} + q + r$	$\dot{\varepsilon} = \boldsymbol{\sigma} \cdot \dot{\mathbf{F}} + q + r$

$$\underline{\mathbf{T}} \bullet \dot{\underline{\mathbf{Y}}} := \int_{\mathcal{H}} \underline{\mathbf{T}}\langle \boldsymbol{\xi} \rangle \cdot \dot{\underline{\mathbf{Y}}}\langle \boldsymbol{\xi} \rangle dV_{\boldsymbol{\xi}}$$

# Linearized theory

- For small displacements (possibly superposed on a large deformation):

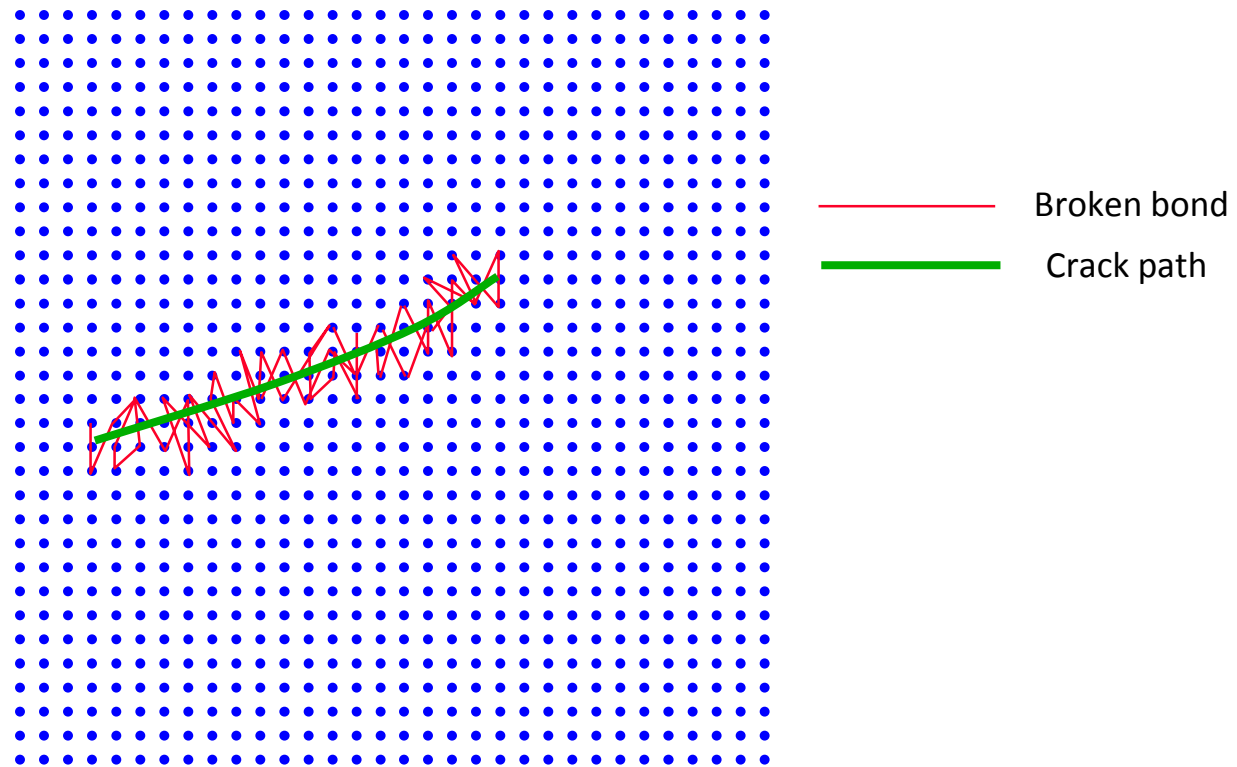
$$\rho \ddot{\mathbf{u}}(\mathbf{x}, t) = \int_{\mathcal{H}} \mathbf{C}(\mathbf{x}, \mathbf{q})(\mathbf{u}(\mathbf{q}, t) - \mathbf{u}(\mathbf{x}, t)) dV_{\mathbf{q}} + \mathbf{b}(\mathbf{x}, t)$$

where  $\mathbf{C}$  is the tensor-valued *micromodulus* field.

- Equation is formally the same as in Kunin's nonlocal theory.
- Can still have bond breakage.
- Most of the following discussion uses the linearized theory.
- Will see how to get  $\mathbf{C}$  by multiscale methods.



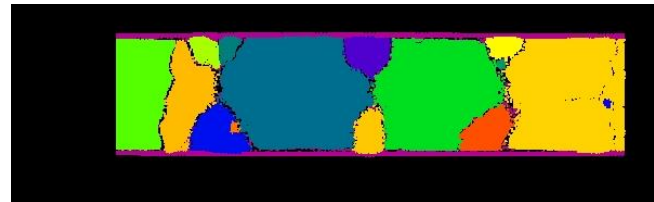
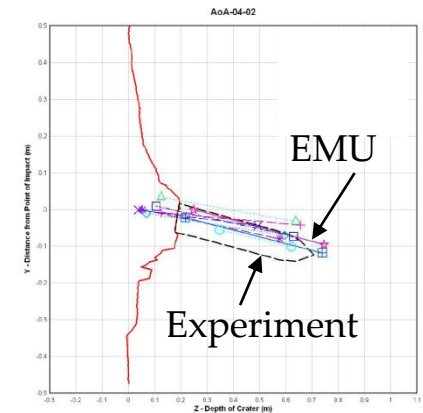
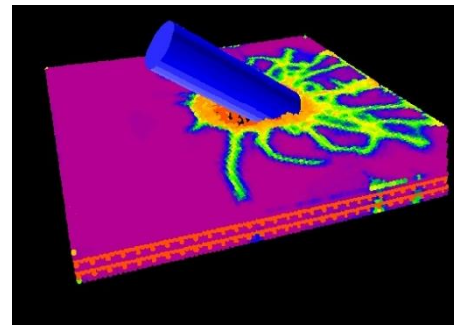
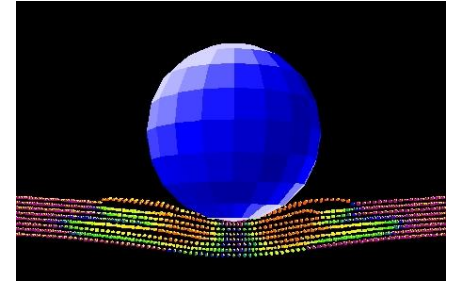
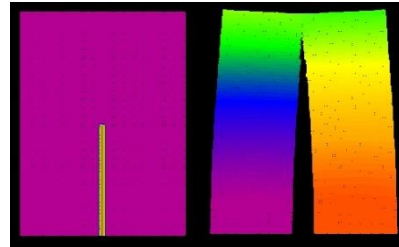
# Bond breakage leads to autonomous crack growth



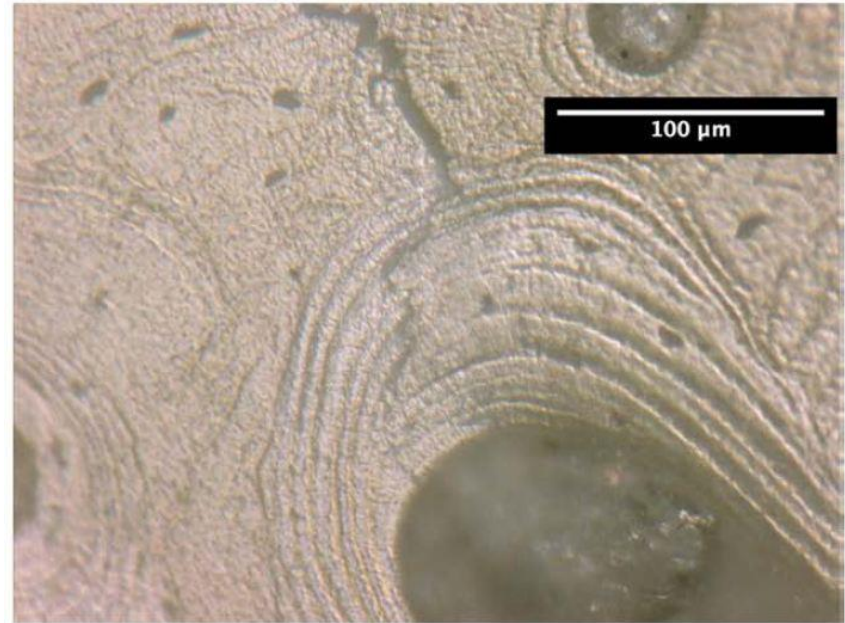
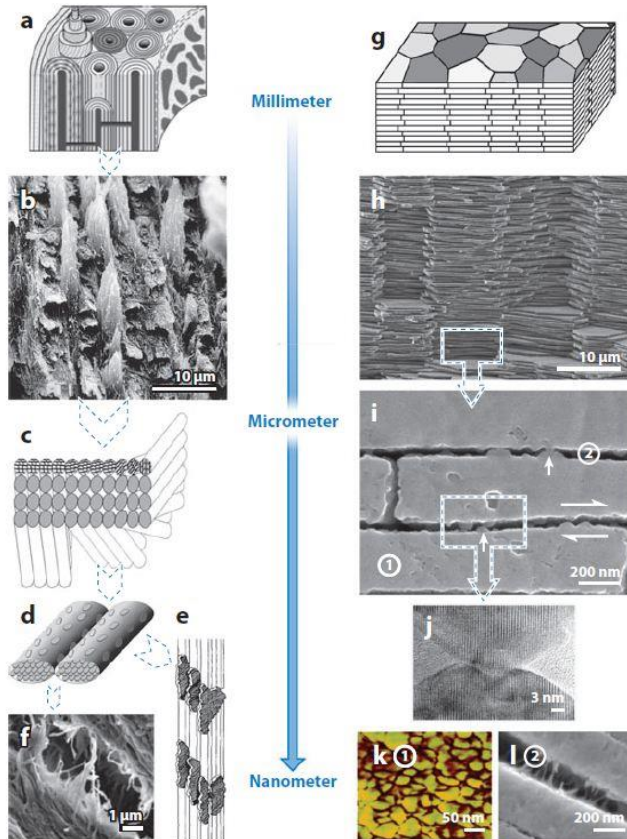
- When a bond breaks, its load is shifted to its neighbors, leading to progressive failure.

# Examples of application of peridynamics

- Single crack brittle energy balance
- 3-point bend test
- Dynamic fracture
  - Crack growth velocity
  - Trajectory
  - Branching
- Impact into concrete and aluminum
  - Residual velocity
  - Penetration depth
  - Crater size
- Fatigue
  - S-N curves for aluminum and epoxy
  - Paris law curves for aluminum
- Composite impact, damage, and fracture
  - Delaminations (compare NDE)
  - Residual strength in OHC, OHT
  - Stress concentration profile in OHT
  - Bird strike loading
  - Lamina tensile fracture



# Bone: A composite material with many length scales



Bone structure helps delay, deflect crack growth. Image: Chan, Chan, and Nicolella, *Bone* 45 (2009) 427–434

Bone contains a hierarchy of structures at many length scales. Image: Wang and Gupta, *Ann. Rev. Mat. Sci.* 41 (2011) 41-73

# Peridynamics as a multiscale method

- The basic equations have a fundamental length scale (the horizon).
- Changing the horizon in a consistent way could provide a way to connect length scales.

## Some previous work on multiscale peridynamics

- Derivation of peridynamic equations from statistical mechanics (Lehoucq & Sears, 2011).
- Higher order gradients to connect MD to peridynamic (Seleson, Parks, Gunzburger, & Lehoucq, 2005).
- Adaptive mesh refinement (Bobaru & Hu, 2011).
- Two-scale evolution equation for composites (Alali & Lipton, 2012).
- PFHMM method for atomistic-to-continuum coupling (Rahman, Foster, & Haque, 2014).

# Scalable multiscale methods

- How to couple multiple physics across wide variations in length/time scales when many length scales are naturally present in the problem?
- Idea:
  - Hierarchy of levels  $m$  each with length scale  $L_m = L_0 2^m$
  - $L_0$  is the smallest physically operative length scale.
  - Each level is coupled to the adjacent levels by the same equations:

$$\dot{y}_m = f(y_{m-1}, y_m, y_{m+1})$$

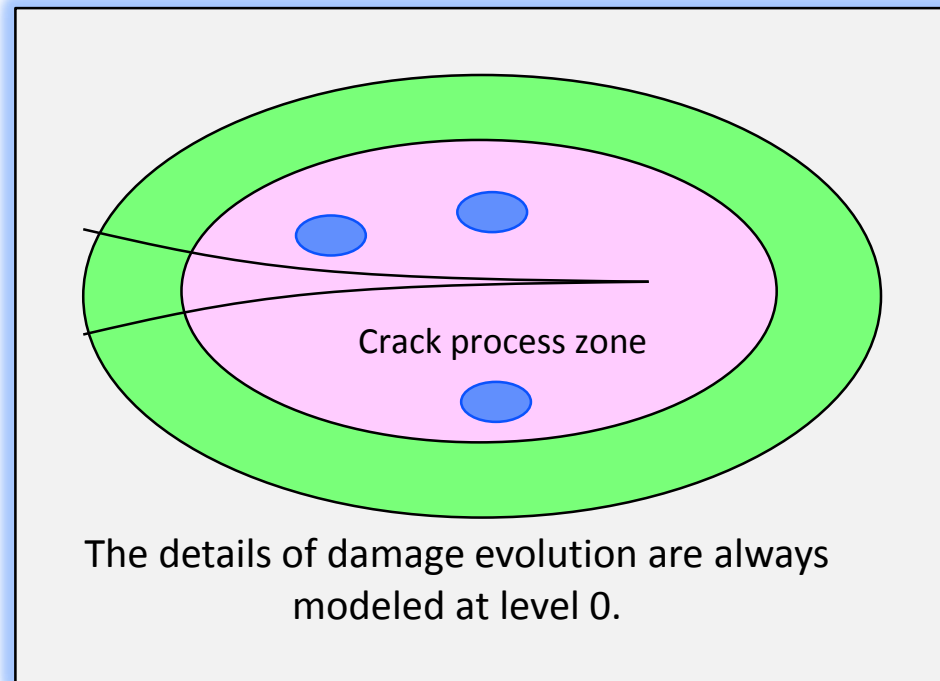
where  $f$  is independent of  $m$ .



- Avoids reinventing the wheel at each level.

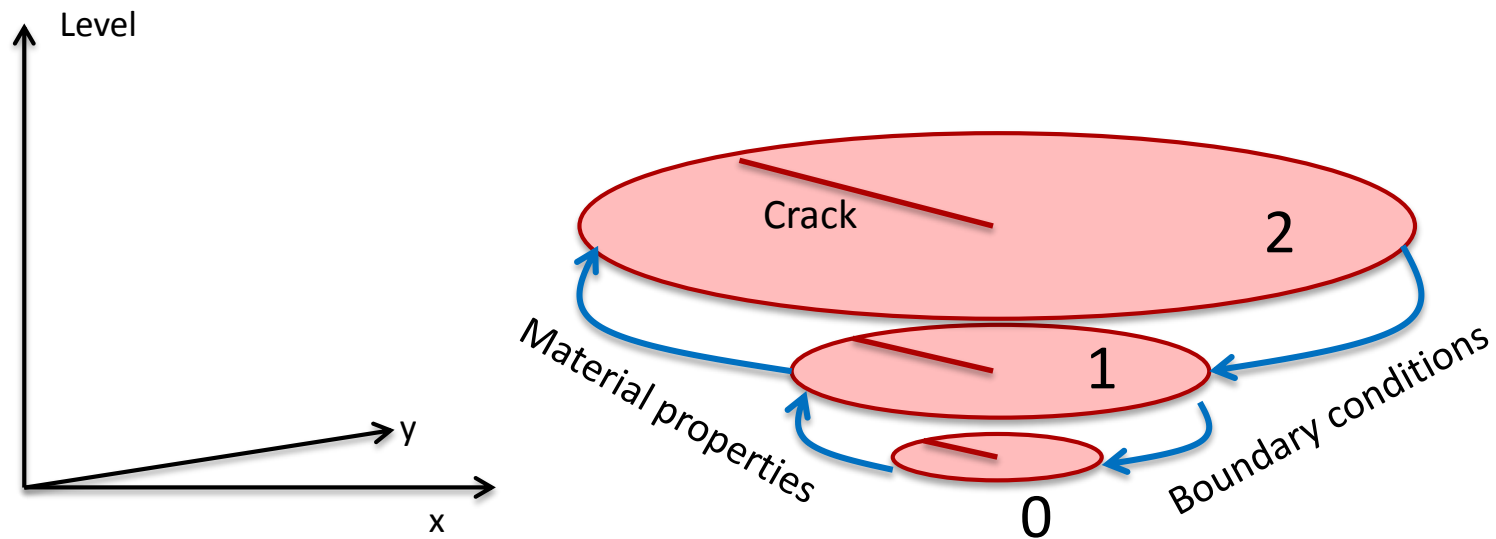
# Concurrent multiscale method for defects

- Apply the best practical physics at the smallest length scale (near a crack tip).
- Scale up hierarchically to larger length scales.
- Each level is related to the one below it by the same equations.
  - Any number of levels can be used.
- Adaptively follow the crack tip.



# Concurrent solution strategy

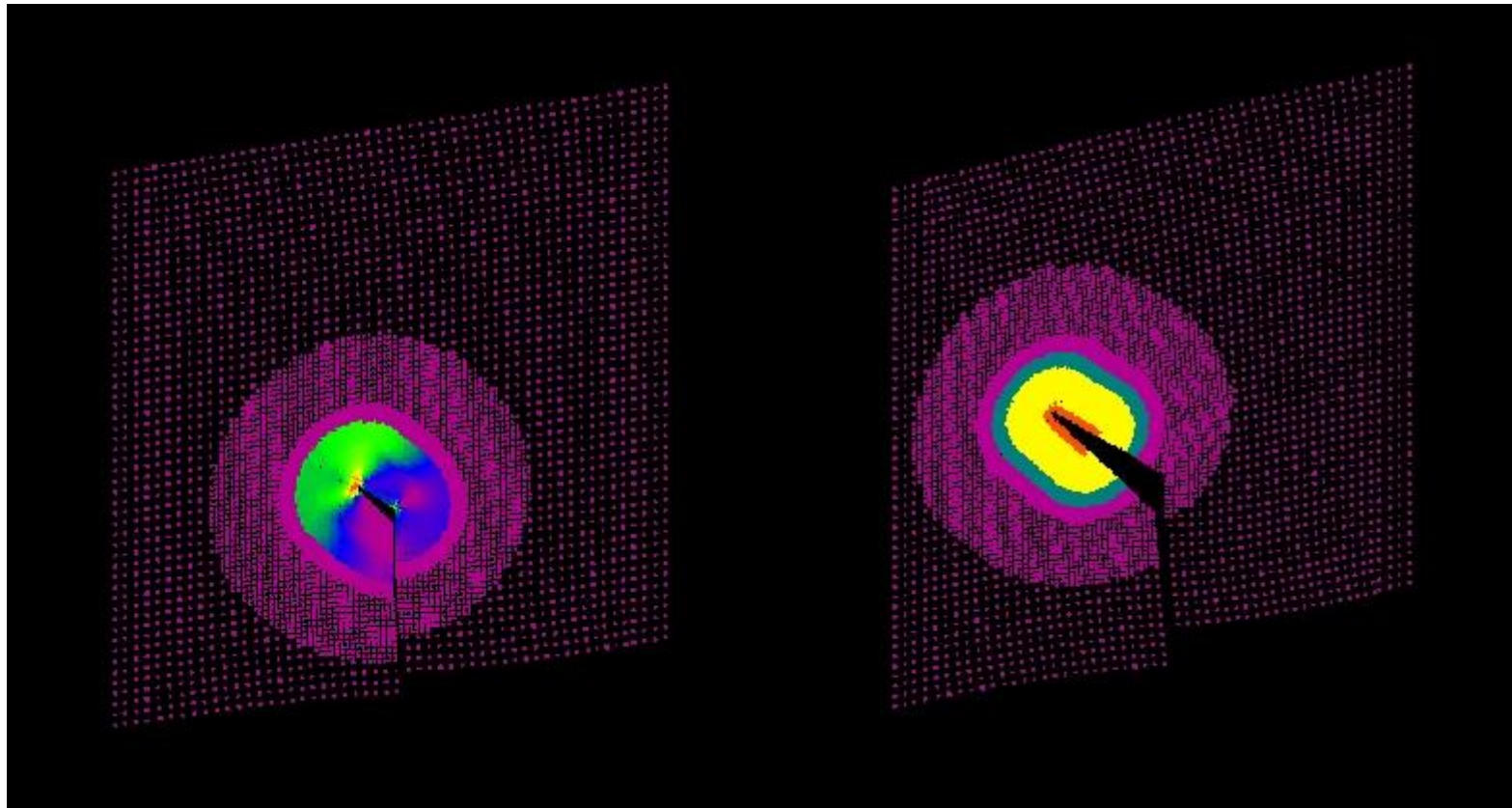
- The equation of motion is applied only within each level.
- Higher levels provide boundary conditions on lower levels.
- Lower levels provide coarsened material properties (including damage) to higher levels.



Schematic of communication between levels in a 2D body



# Concurrent multiscale example: shear loading of a crack



Bond strain

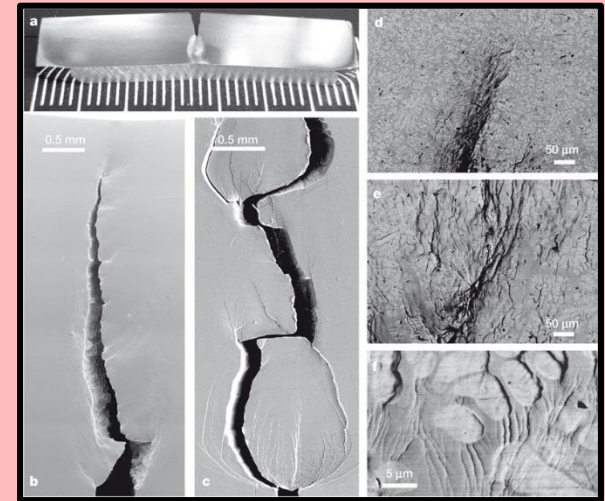
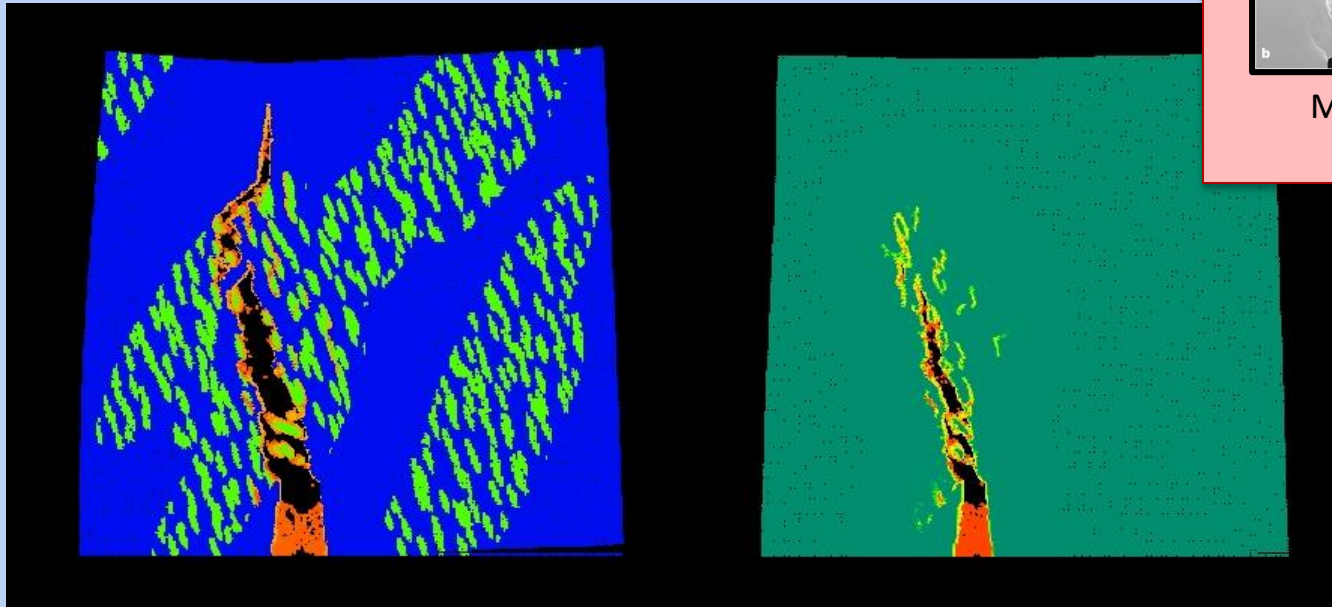
Damage process zone



# Multiscale modeling reveals the structure of brittle cracks

- Material design requires understanding of how morphology at multiple length scales affects strength.
- This is a key to material reliability.

Multiscale model of crack growth through a brittle material with distributed defects



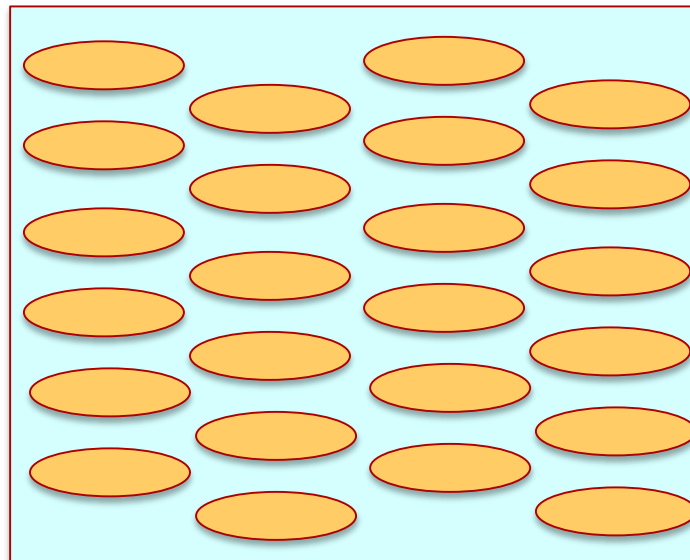
Metallic glass fracture (Hofmann et al, Nature 2008)

# Upscaling of material properties

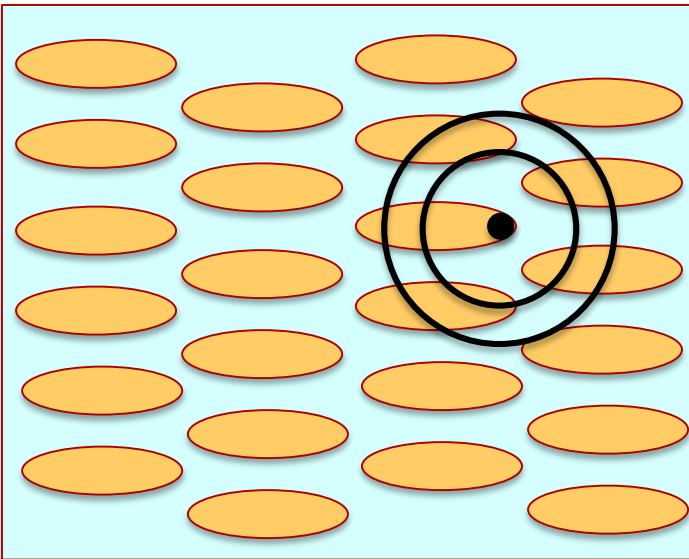
- Suppose we have an accurate model in level 0.
  - How can we obtain material properties in level 1?
  - This is called “upscaling” or “coarse-graining”.
  - Will next describe a method for doing this based on constrained optimization.

# What are the elastic moduli of a heterogeneous material?

- This is an imprecise question in the classical (local) theory.
- Only becomes meaningful in the limit of a very large volume.
- Try to find a peridynamic approach to upscaling that does not assume this.



# We will try to find the micromodulus for different multiscale levels



- Level 0:

$$\int_{\mathcal{H}^0} C^0(q, x)(u^0(q) - u^0(x)) dV_q + b(x) = 0$$

- Level 1:

$$\int_{\mathcal{H}^1} C^1(q, x)(u^1(q) - u^1(x)) dV_q + b(x) = 0$$

- Level m:

$$\int_{\mathcal{H}^m} C^m(q, x)(u^m(q) - u^m(x)) dV_q + b(x) = 0$$

- Upscaling: Find  $C^1$  from  $C^0$ ,  $C^2$  from  $C^1$ , ....

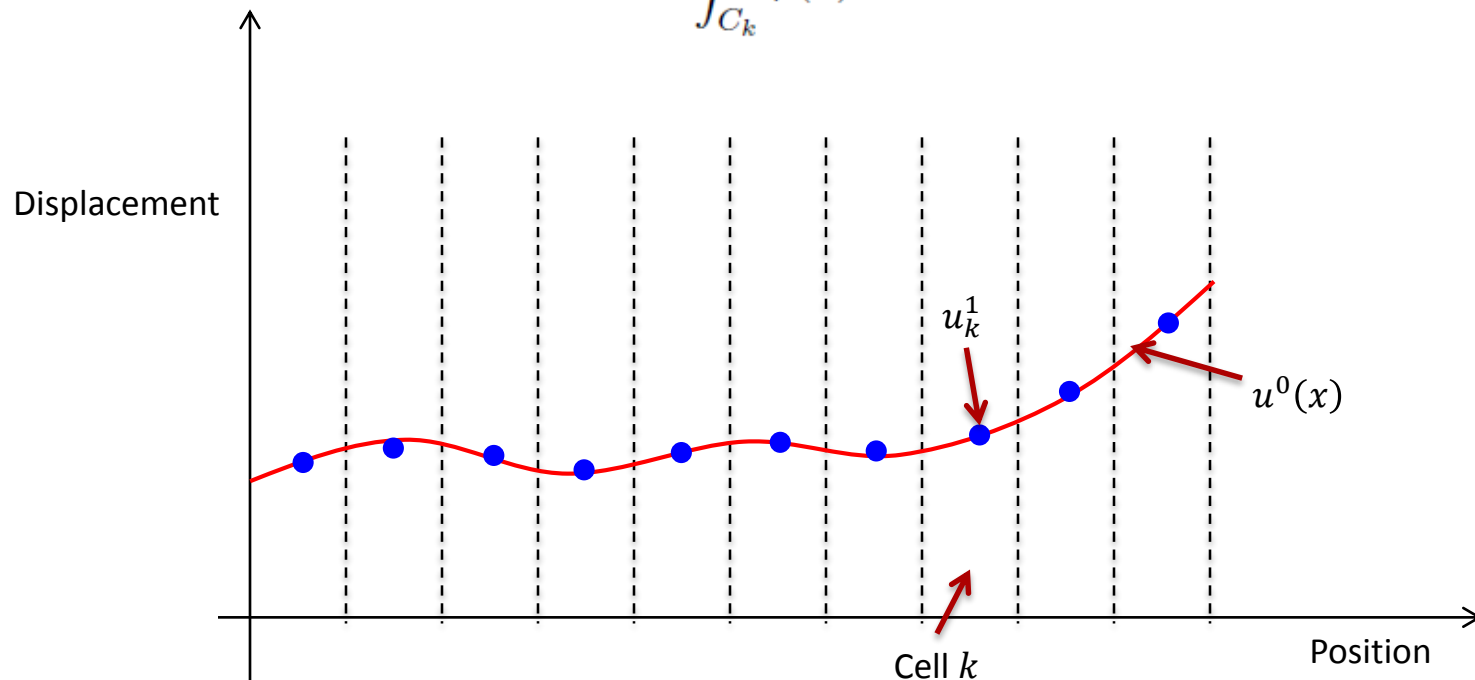
# Level 1 DOFs

- Divide the region into  $K$  "cells"  $C_k$ .
- The mean level 0 displacement within each cell is the level 1 DOF:

$$u_k^1 = \int_{C_k} \varphi(x) u^0(x) dx$$

where

$$\int_{C_k} \varphi(x) = 1.$$



# Level 1 DOF as a constraint

- Pretend all the  $u_k^1$  values are given.
- In effect, this places a constraint on the  $u^0$  function.
- Constrained potential energy functional:

$$\Phi = \int_{\mathcal{B}} (W^0(x) - u^0(x)b(x)) \, dx - \sum_{k=1}^K \lambda_k \left( \int_{C_k} \varphi(x)u^0(x) \, dx - u_k^1 \right)$$

where  $\lambda_1, \lambda_2, \dots, \lambda_K$  are Lagrange multipliers.

# Force balance on cell $k$

- Resulting constrained equilibrium equation:

$$L^0(x) + b(x) + \lambda_k \varphi(x) = 0$$

where  $k$  is whichever cell contains  $x$  and  $L^0$  is the level 0 internal force operator:

$$L^0(x) = \int_{\mathcal{H}_x} \left( \underline{T}[x] \langle q - x \rangle - \underline{T}[q] \langle x - q \rangle \right) dq.$$

- Observe that the constraint acts like a body force distributed over cell  $k$ .
- Integrate the equilibrium equation over cell  $k$ , recall  $\int \varphi = 1$ , set  $b \equiv 0$ :

$$\int_{C_k} L^0(x) dx + \lambda_k = 0.$$

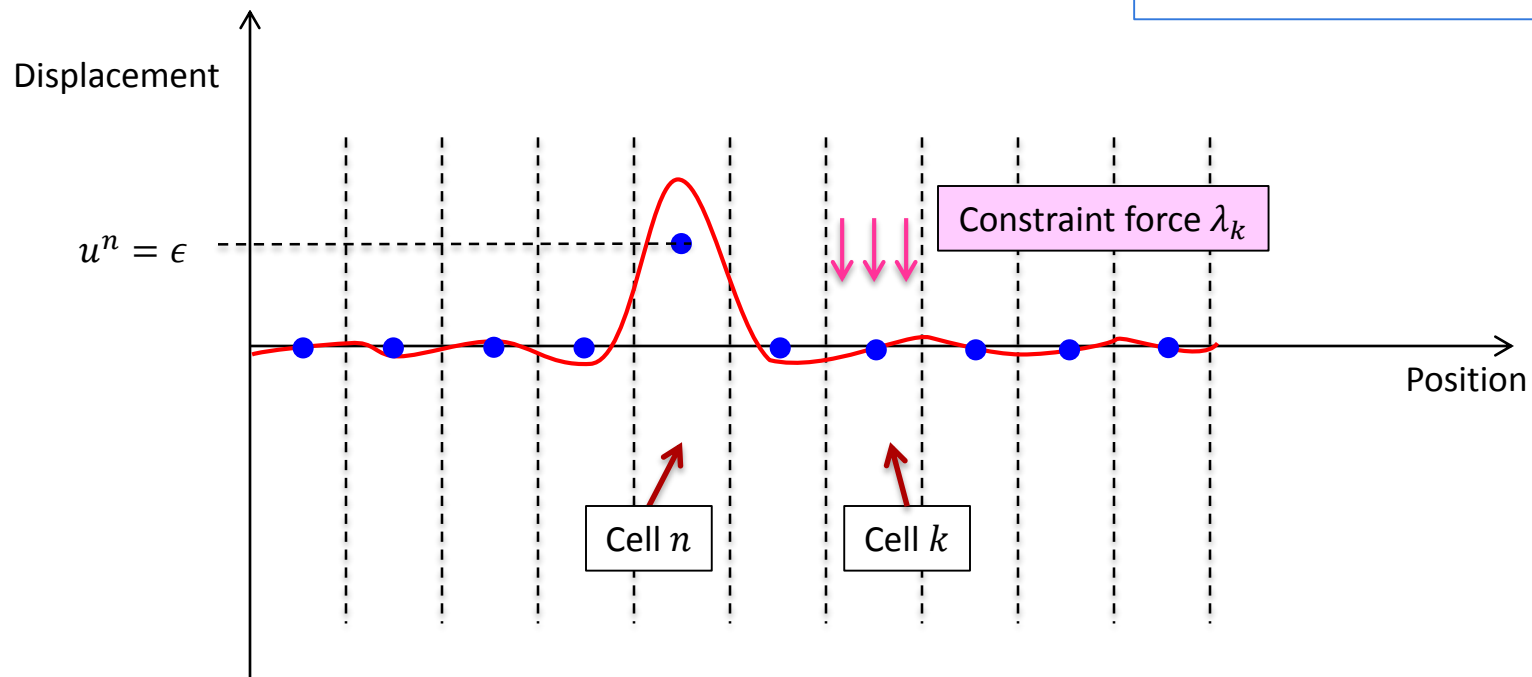
Interaction forces from other cells + constraint force = 0

# Level 1 micromodulus

- Set all  $u_k^1 = 0$  except for cell  $n$ :  $u_n^1 = \epsilon \ll 1$ .
- Solve the constrained equilibrium equation for  $u^0(x)$  and the  $\lambda_1, \lambda_2, \dots, \lambda_K$ .
- The upscaled micromodulus is

$$c_{kn}^1 = \lambda_k / \epsilon. \rightarrow$$

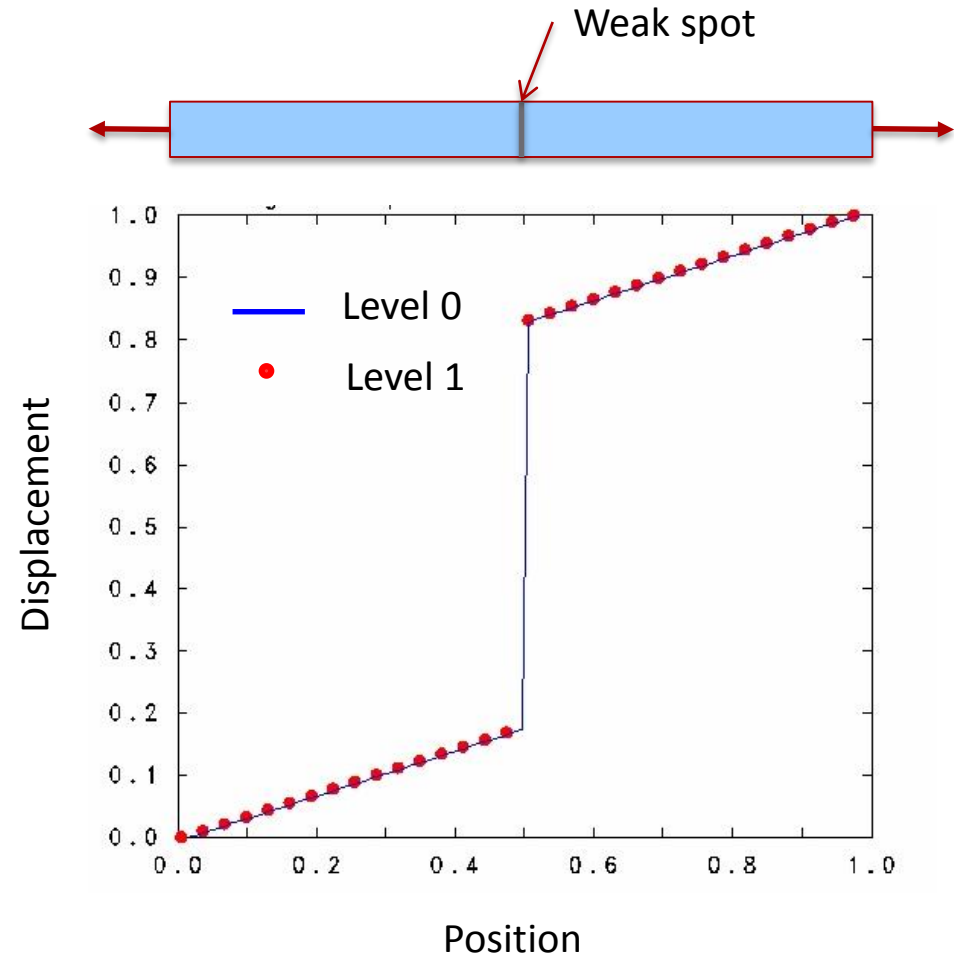
$$\rho \ddot{u}_i^1 = \sum_{j \in H_i} c_{ij}^1 (u_j^1 - u_i^1)$$





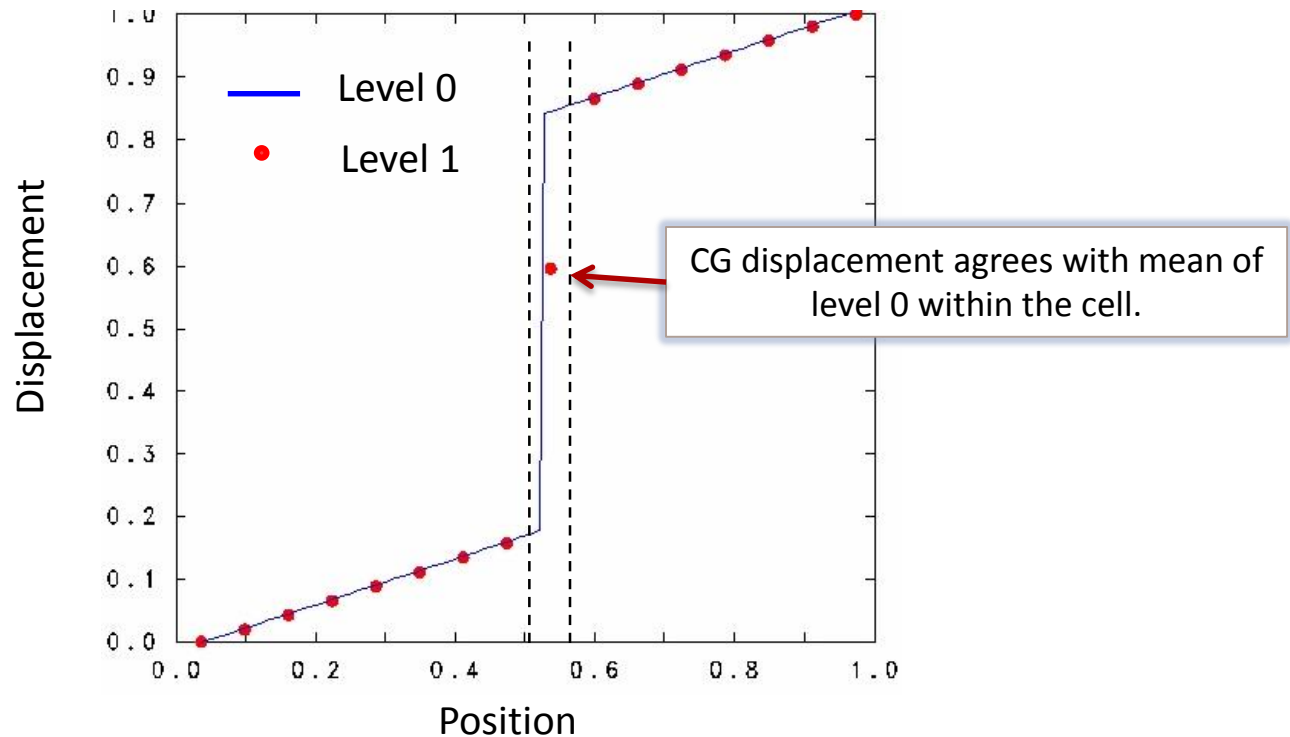
# Example: Rod with a defect

- Upscaling method preserves the effect of a defect embedded within a cell.



# Coarser level 1

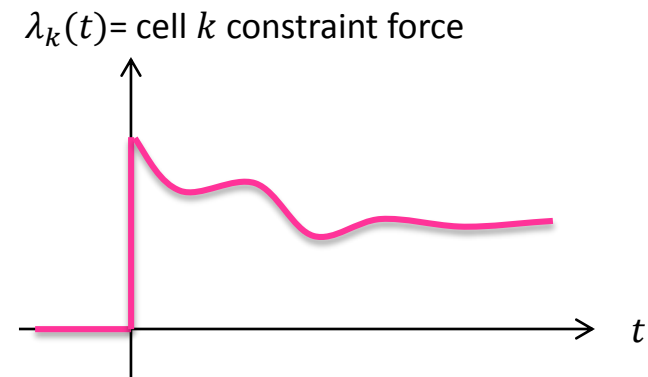
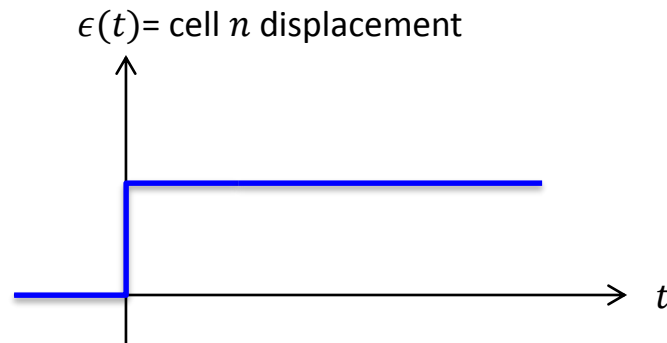
- If the defect is not exactly at a cell boundary, the method still produces the mean of the level 0 displacements within each cell.



# Time-dependent response

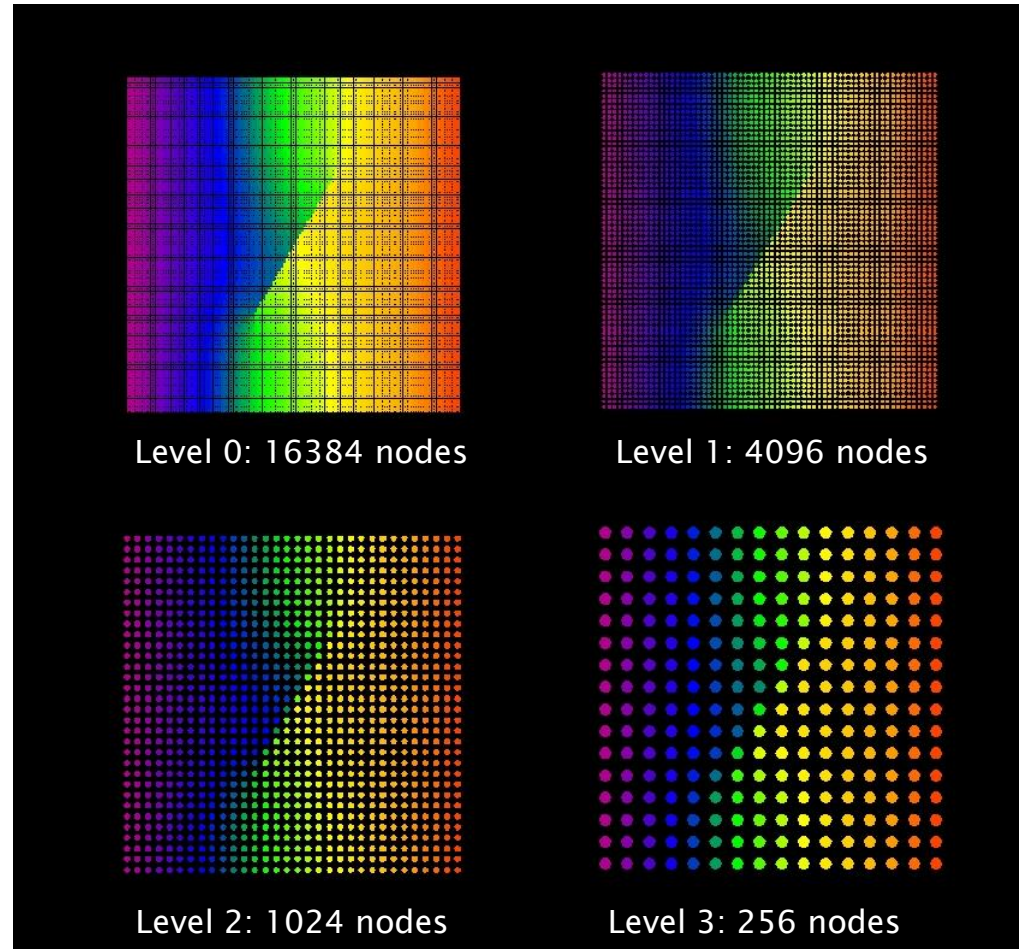
- Time-dependent bond force model for level 1:

$$f(x_n, x_k) = \int_0^t \lambda_k(t - \tau) (\dot{u}(x_k, \tau) - \dot{u}(x_n, \tau)) d\tau$$



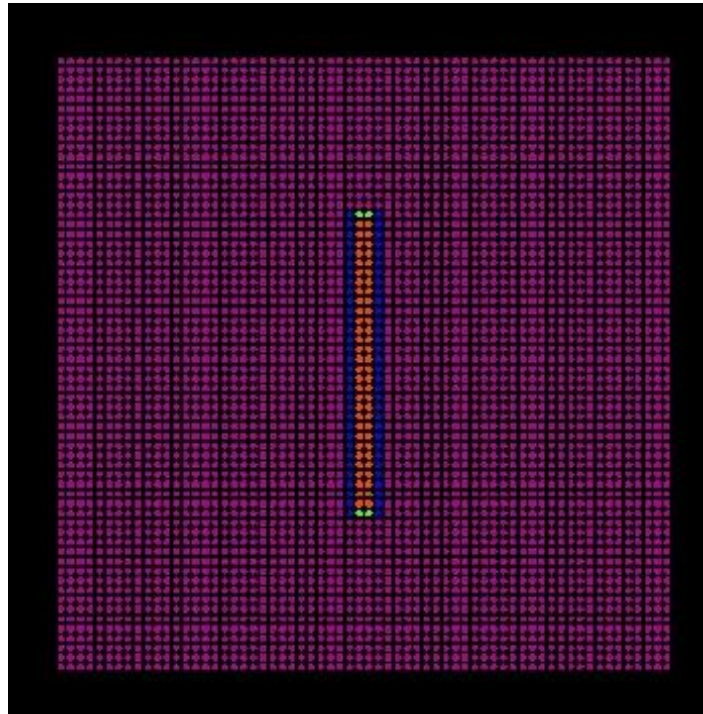
# Coarse graining verification: crack in a plate

- Example: Solve the same problem in four different levels using the successively upscaled material properties – results are the same.



# Defining damage from coarse-grained material properties

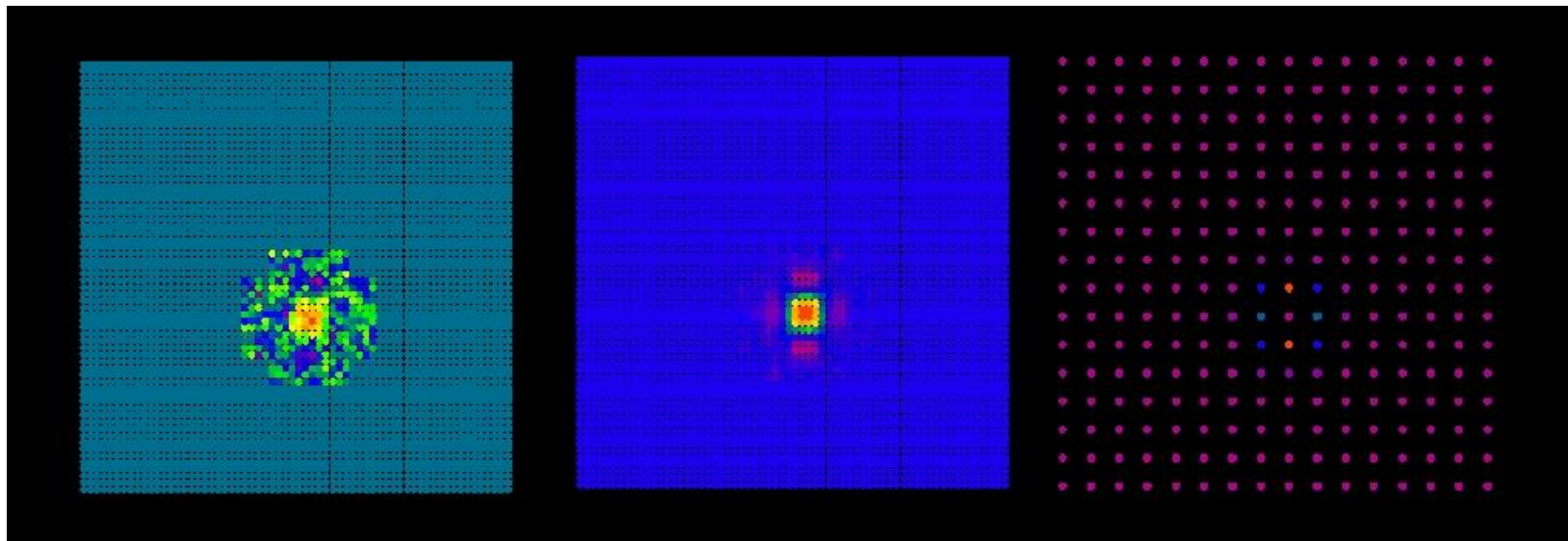
- Define bonds to be damaged if their coarse-grained micromodulus is less than a tolerance.
- This allows damage to be determined without deforming the MD grid.



Level 1 damage contours deduced from coarse-grained properties

# Coarse graining MD directly into peridynamics

- The level 0 physics can be anything: PD, standard continuum, MD, MC(?), DFT(?)



Level 0: MD showing  
thermal oscillations

MD time-averaged  
displacements

Level 1: Coarse grained  
micromodulus

# Summary

- Concurrent multiscale:
  - Adaptively follow crack tips.
  - Apply the best practical physics in level 0.
  - Also multiscale in time because of time step increase for higher levels.
- Coarse-graining:
  - Derives incremental elastic properties at higher levels.
  - Does not rely on a representative volume element (RVE).
- Methods are “scalable:” can be applied any number of times to obtain any desired increase in length scale.



## Extra slides

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# Reconstruction

- The constrained minimization problem is:

$$\int_{\mathcal{H}_x} C^m(x, q)(u^m(q) - u^m(x)) dq + b + \lambda_k \phi_k = 0, \quad \int_{\mathcal{B}_k} u^m \phi = u_k^{m+1}$$

- To get level  $m + 1$  from level  $m$ :

$$\begin{bmatrix} [C^m] & [\phi^m] \\ [\phi^m]^T & [0] \end{bmatrix} \begin{Bmatrix} \{u^m\} \\ \{\lambda^m\} \end{Bmatrix} = \begin{Bmatrix} \{0\} \\ \{u^{m+1}\} \end{Bmatrix}.$$

- Invert the matrix:

$$\begin{bmatrix} [\dots] & [R^m] \\ [R^m]^T & [\dots] \end{bmatrix} \begin{Bmatrix} \{0\} \\ \{u^{m+1}\} \end{Bmatrix} = \begin{Bmatrix} \{u^m\} \\ \{\lambda^m\} \end{Bmatrix}.$$

- $[R^m]$  is the *reconstruction matrix*.

# Coarse graining a damage criterion

- Can we model level 1 damage processes without modeling level 0 explicitly?
- Suppose the level 0 damage depends only on the bond displacements

$$\underline{U}^0[x] \langle q - x \rangle := u^0(q) - u^0(x).$$

- Recall

$$\{u^0\} = [R^0]\{u^1\}.$$

- Can use this to find a *bond reconstruction state*  $\underline{R}^0$  such that

$$\underline{U}^0[x] = \underline{R}^0[x] \bullet \underline{U}^1[x]$$

where  $\underline{U}^1[x]$  is the level 1 displacement state at  $x$ .

- We can then compute level 0 bond damage without solving for the level 0 displacements.

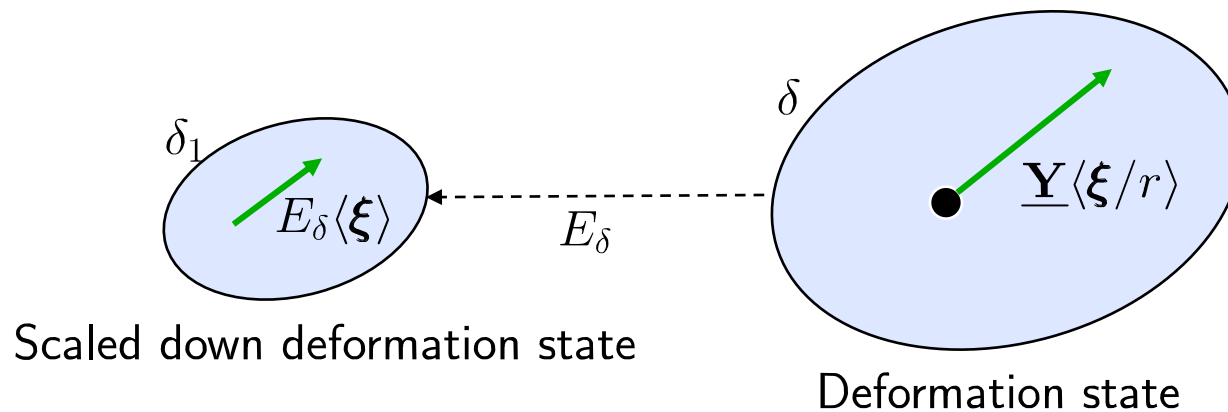
# Rescaling an elastic material model

- Start with a material model  $W_1$  which has some fixed horizon  $\delta_1$ .
- Define a mapping that takes a new, larger horizon  $\delta$  into the original:

$$(E_\delta(\underline{\mathbf{Y}}))\langle \underline{\boldsymbol{\xi}} \rangle = r \underline{\mathbf{Y}} \langle \underline{\boldsymbol{\xi}}/r \rangle, \quad r = \frac{\delta_1}{\delta} \leq 1$$

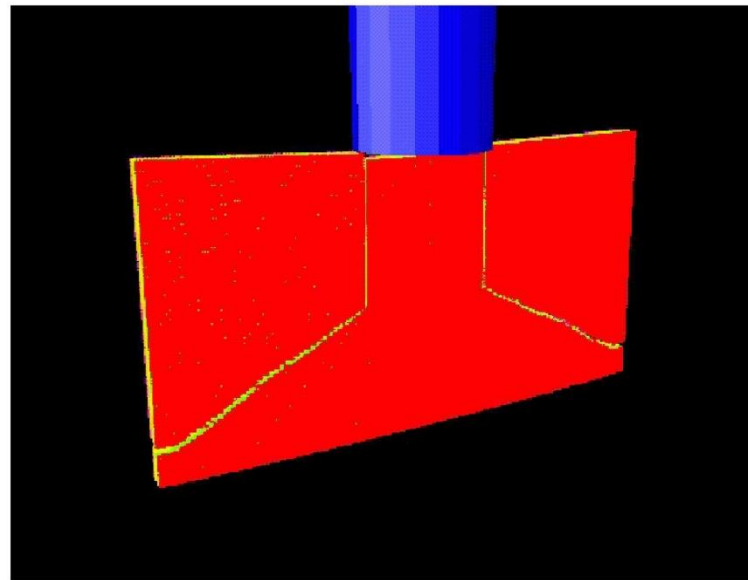
- Then set

$$W_\delta(\underline{\mathbf{Y}}) = W_1(E_\delta(\underline{\mathbf{Y}}))$$

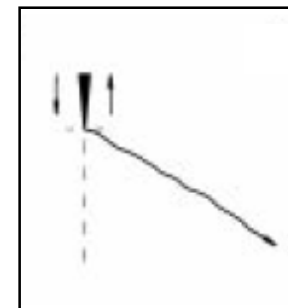


# Example: Dynamic fracture

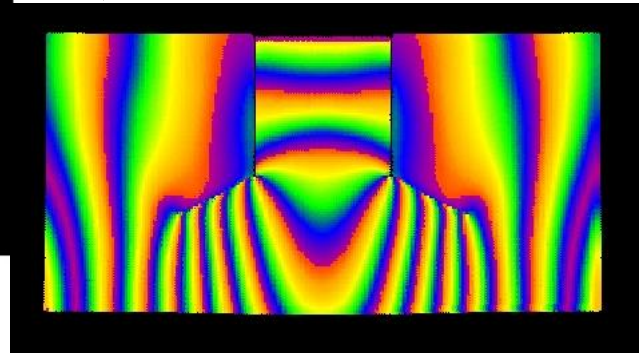
- Dynamic fracture in maraging steel (Kalthoff & Winkler, 1988)
- Mode-II loading at notch tips results in mode-I cracks at 70deg angle.
- 3D EMU model reproduces the crack angle.



EMU\*



Experiment



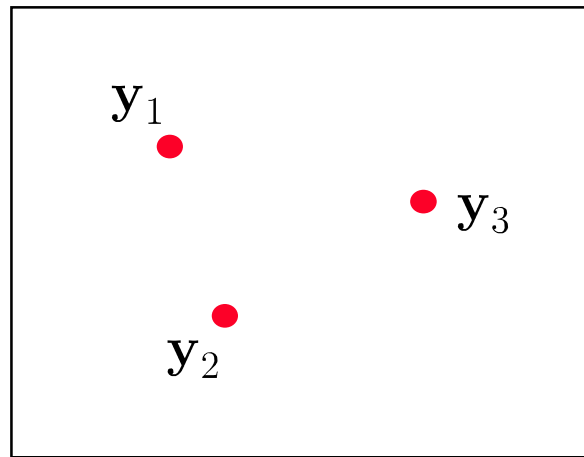
# Discrete particles and PD states

- Consider a set of atoms that interact through an  $N$ -body potential:

$$U(\mathbf{y}_1, \mathbf{y}_2, \dots, \mathbf{y}_N),$$

$\mathbf{y}_1, \dots, \mathbf{y}_N$  = deformed positions,  $\mathbf{x}_1, \dots, \mathbf{x}_N$  = reference positions.

- This can be represented exactly as a peridynamic body.

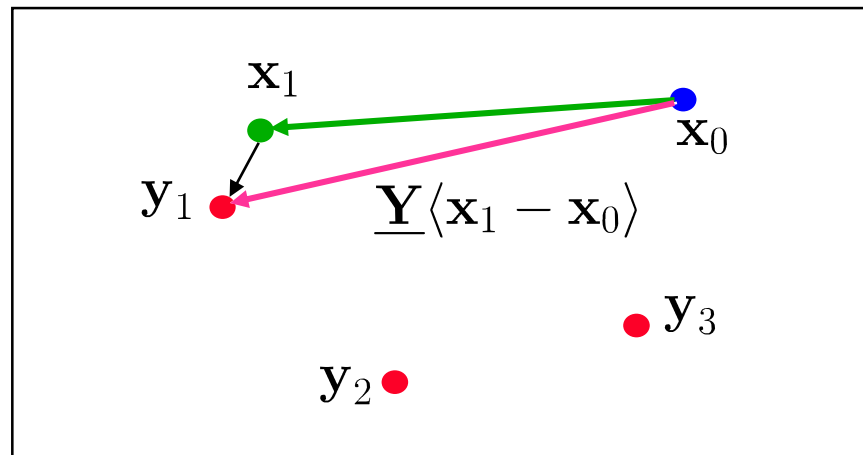


## Discrete particles and PD states, ctd.

Define a peridynamic body by:

$$\hat{W}(\underline{\mathbf{Y}}, \mathbf{x}) = \Delta(\mathbf{x} - \mathbf{x}_0) U(\underline{\mathbf{Y}}\langle \mathbf{x}_1 - \mathbf{x}_0 \rangle, \underline{\mathbf{Y}}\langle \mathbf{x}_2 - \mathbf{x}_0 \rangle, \dots, \underline{\mathbf{Y}}\langle \mathbf{x}_N - \mathbf{x}_0 \rangle),$$

$$\rho(\mathbf{x}) = \sum_i \Delta(\mathbf{x} - \mathbf{x}_i) M_i$$



## Discrete particles and PD states, ctd.

After evaluating the Frechet derivative  $\underline{\mathbf{T}}$ , find

$$\rho(\mathbf{x})\ddot{\mathbf{y}}(\mathbf{x}, t) = \int \mathbf{f}(\mathbf{x}', \mathbf{x}, t) dV_{\mathbf{x}'}$$

implies

$$M_i\ddot{\mathbf{y}}(\mathbf{x}_i, t) = -\frac{\partial U}{\partial \mathbf{y}_i}, \quad i = 1, \dots, N$$

In other words, the PD equation of motion reduces to Newton's second law.

