



Variability in Mechanical Properties of Laser Engineered Net Shaping Material

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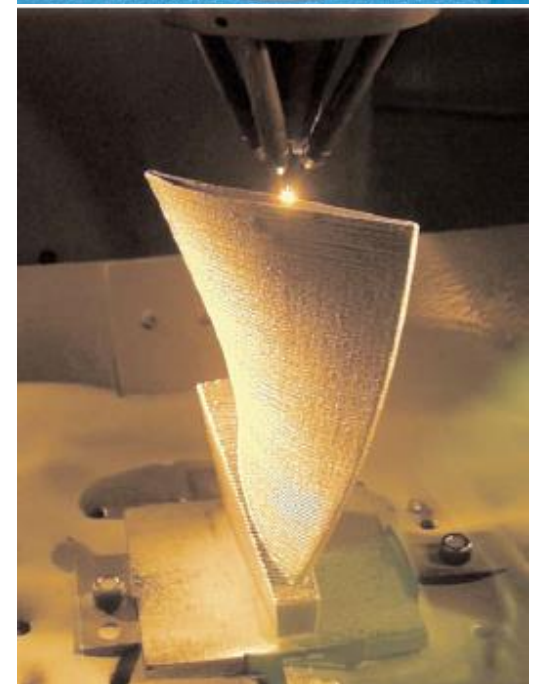
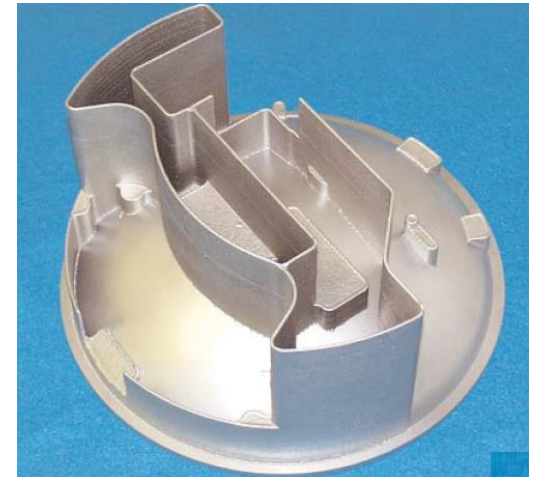
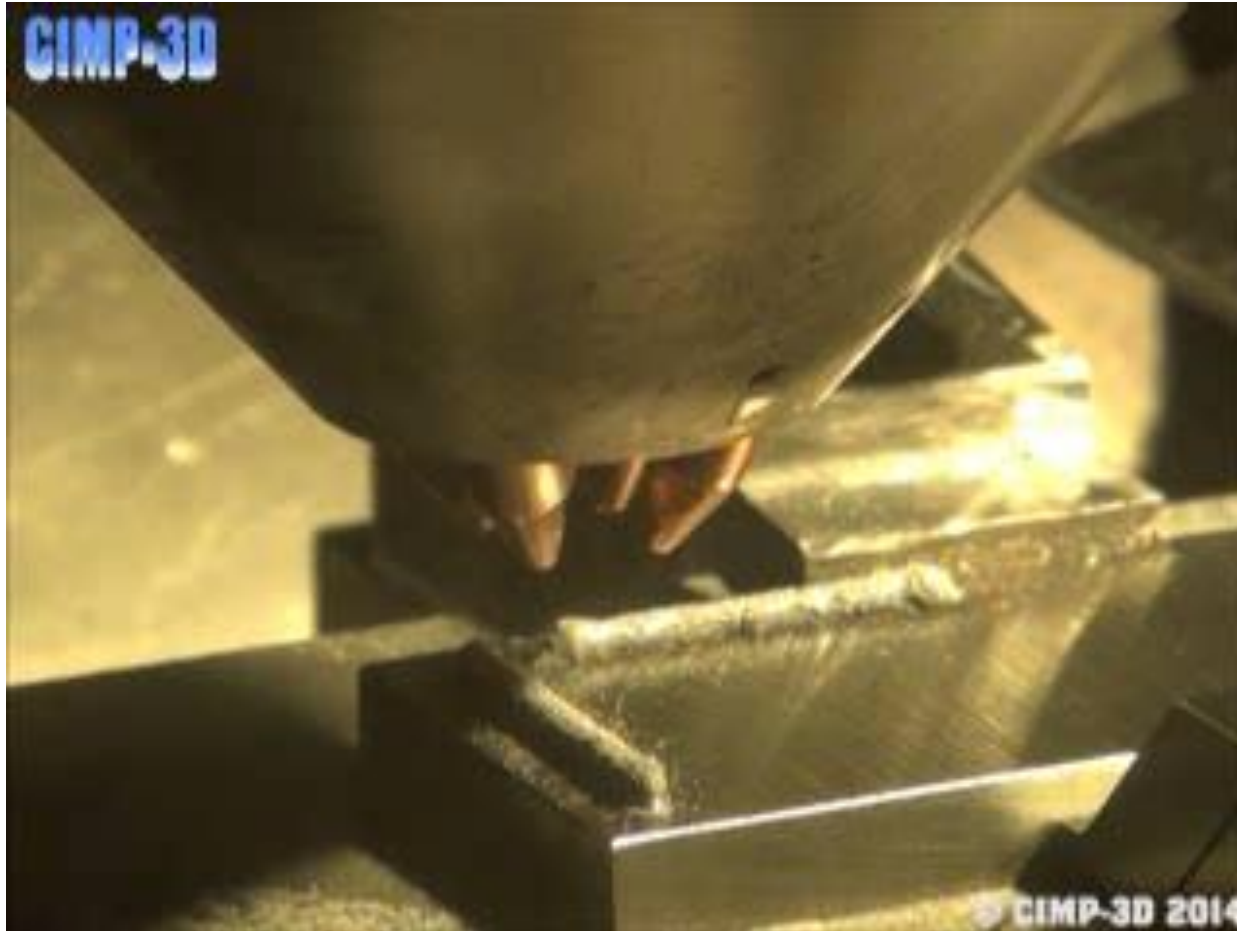


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As opposed to powder-bed technology, the LENS process builds material by injecting powder feedstock with laser heating.

LENS = Laser Engineered Net Shaping



Courtesy of Todd Palmer, Pennsylvania State University

Project: Strain rate effects, variability, and modeling of LENS-like 304L

Quasistatic $10^{-5} - 10^0$



Dynamic $5 \times 10^2 - 3 \times 10^3$

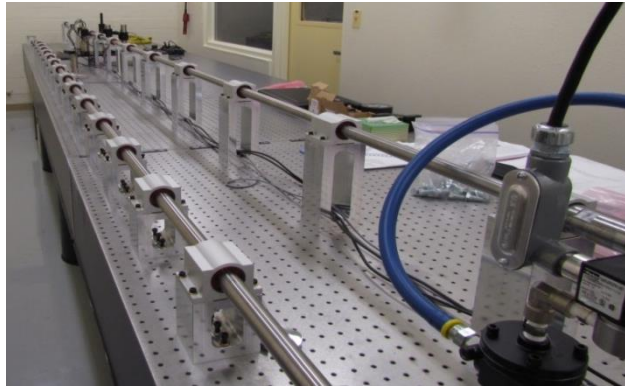


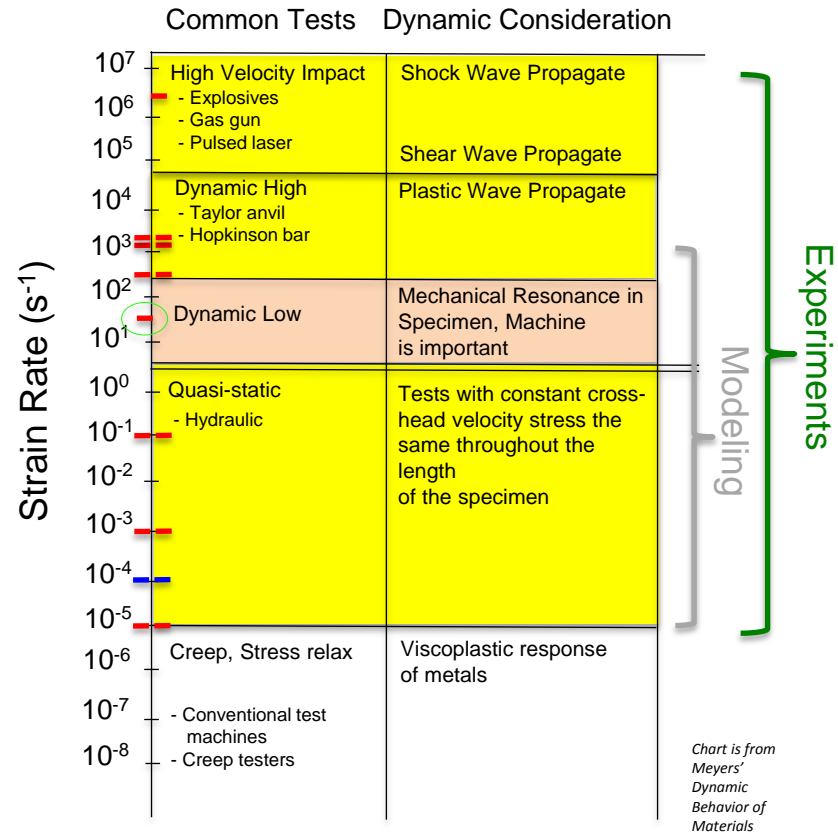
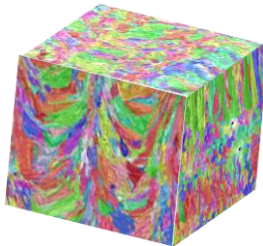
Plate Impact $10^7 - 10^9$



Crystal Plasticity Modeling



Microscopy



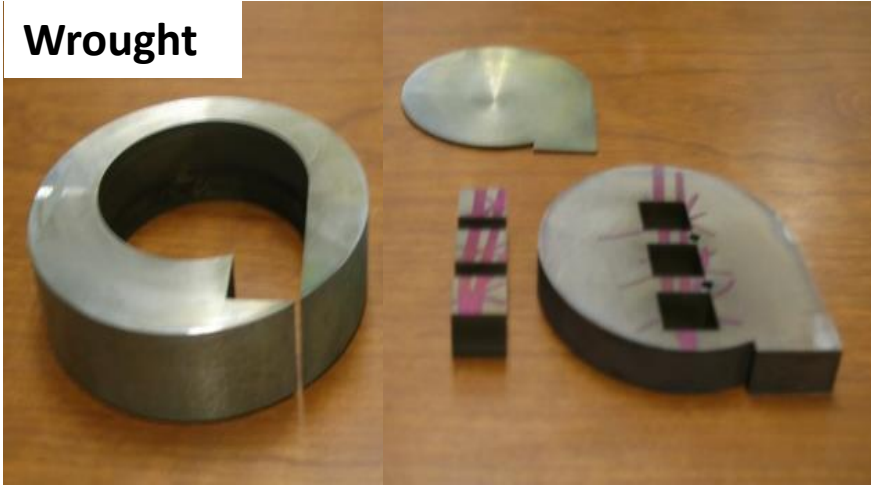
Neutron Diffraction



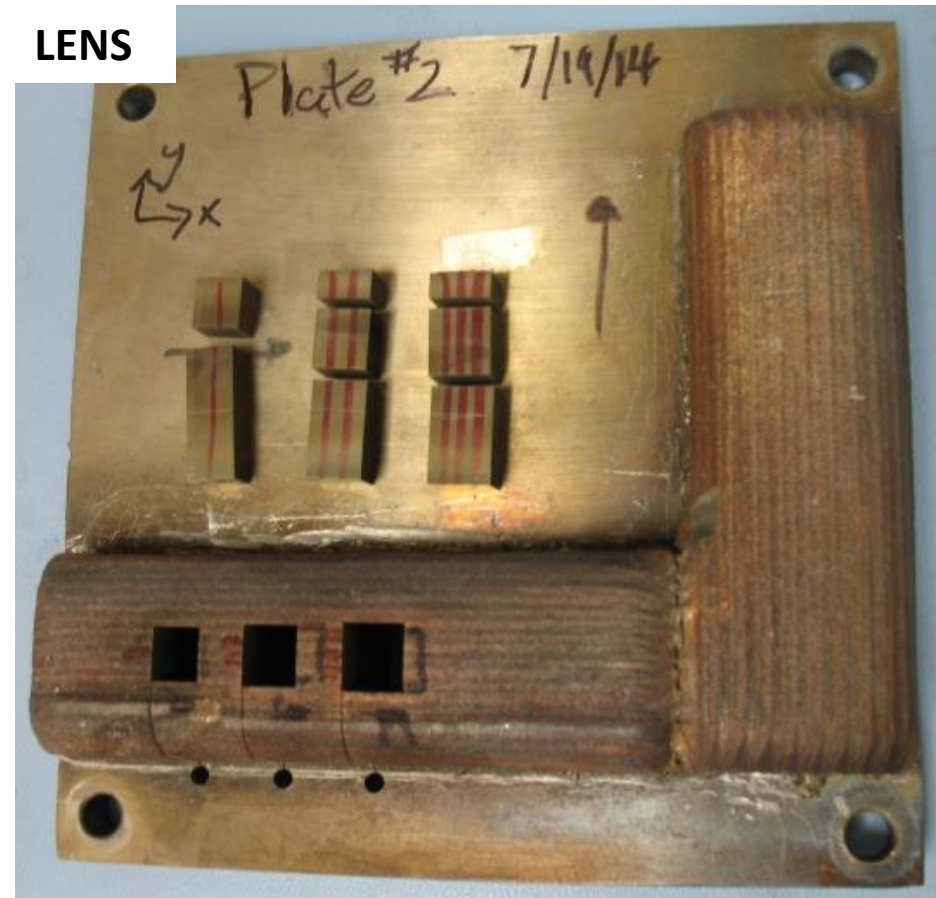
-- Tests at SNL
-- Tests at LANL with neutrons

Specimens cut from wrought and LENS bars for comparison.

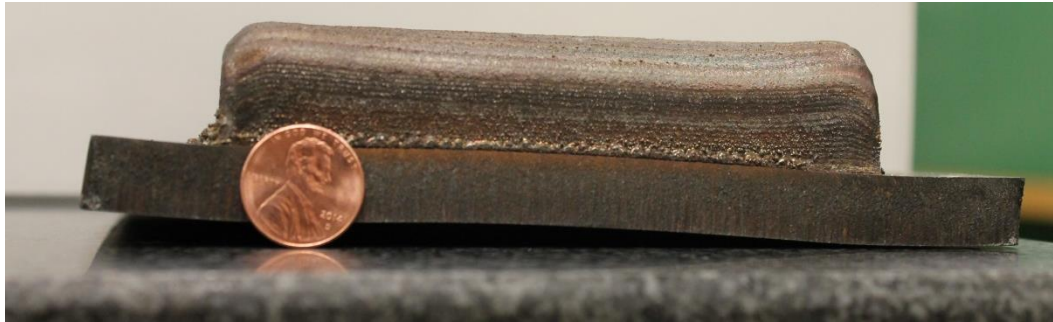
Wrought



LENS



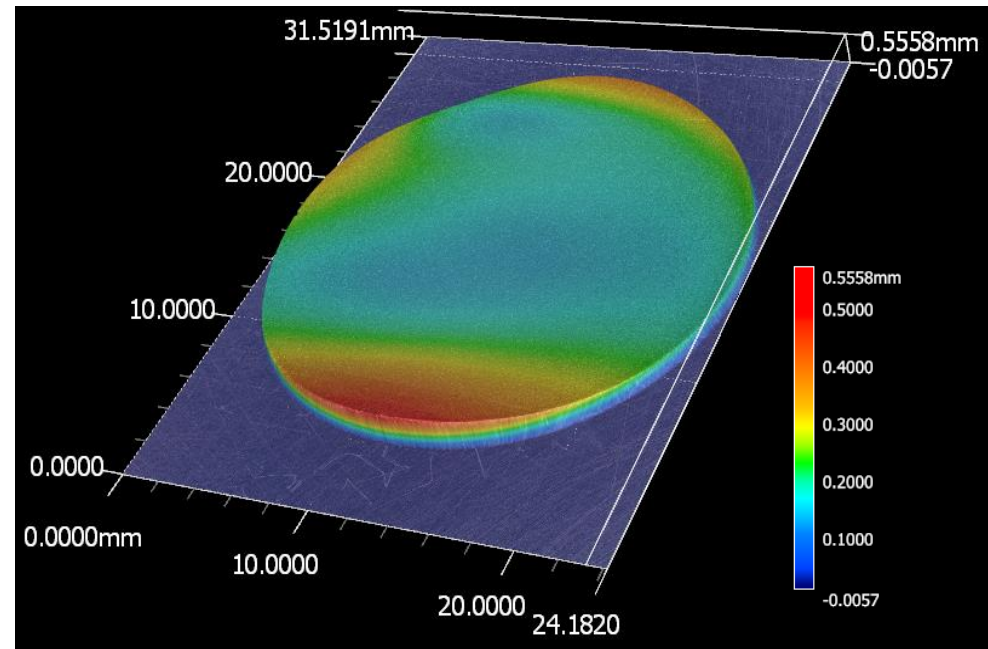
LENS residual stresses are not as extreme as feared



- Base plate warped significantly (12 mm thick).
- Lattice parameters in specimens cut from bars show little difference.
- 100 μm disk cut with very little warping (0.5 mm max over 25 mm).

Lattice parameters in specimens show little difference

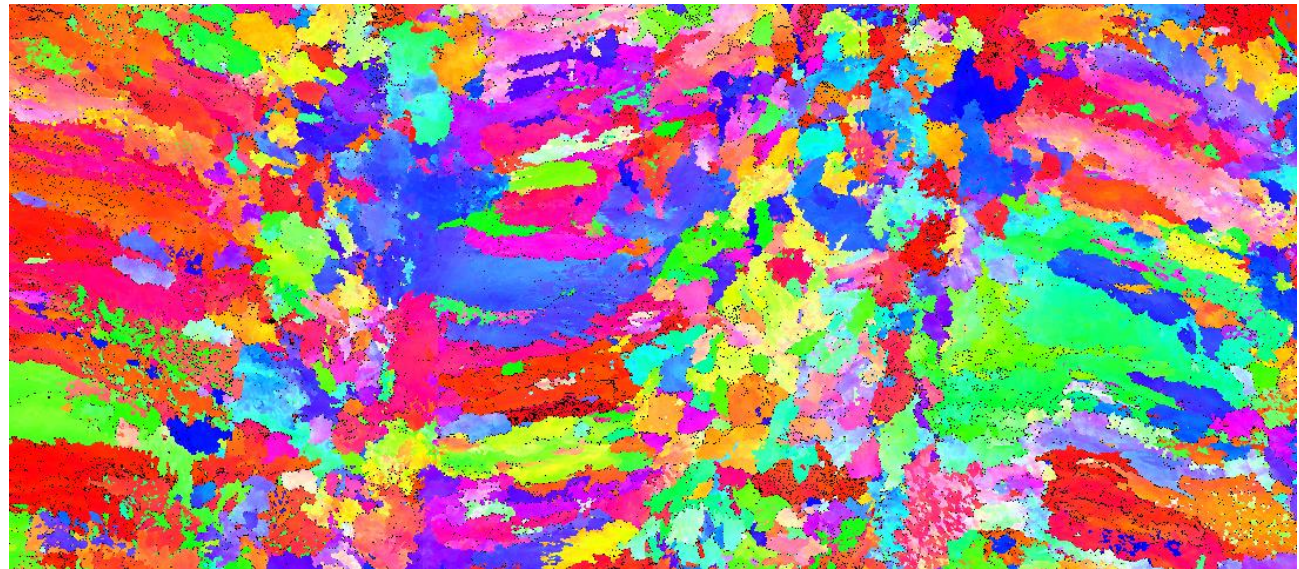
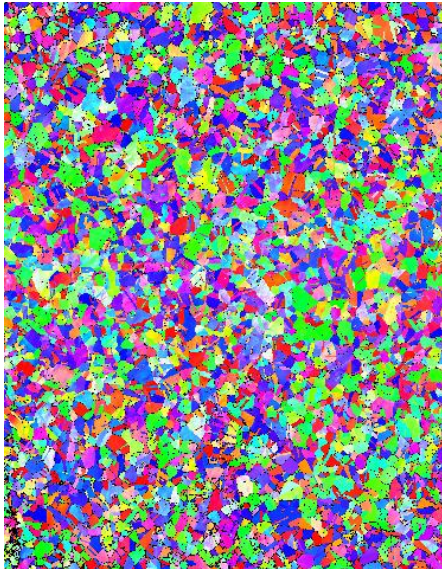
	<i>Austenite parameters</i>	
	a_l	a_t
Wrought	3.5932 Å	3.5900 Å
LENS 3.8kW //	3.5938 Å	3.5904 Å
LENS 2kW +	3.5941 Å	3.5908 Å



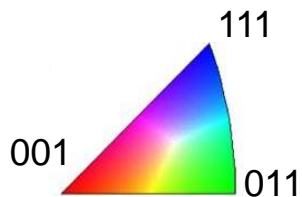
LENS grain size is much larger than wrought 304L SS. Same chemistry.

Wrought

LENS



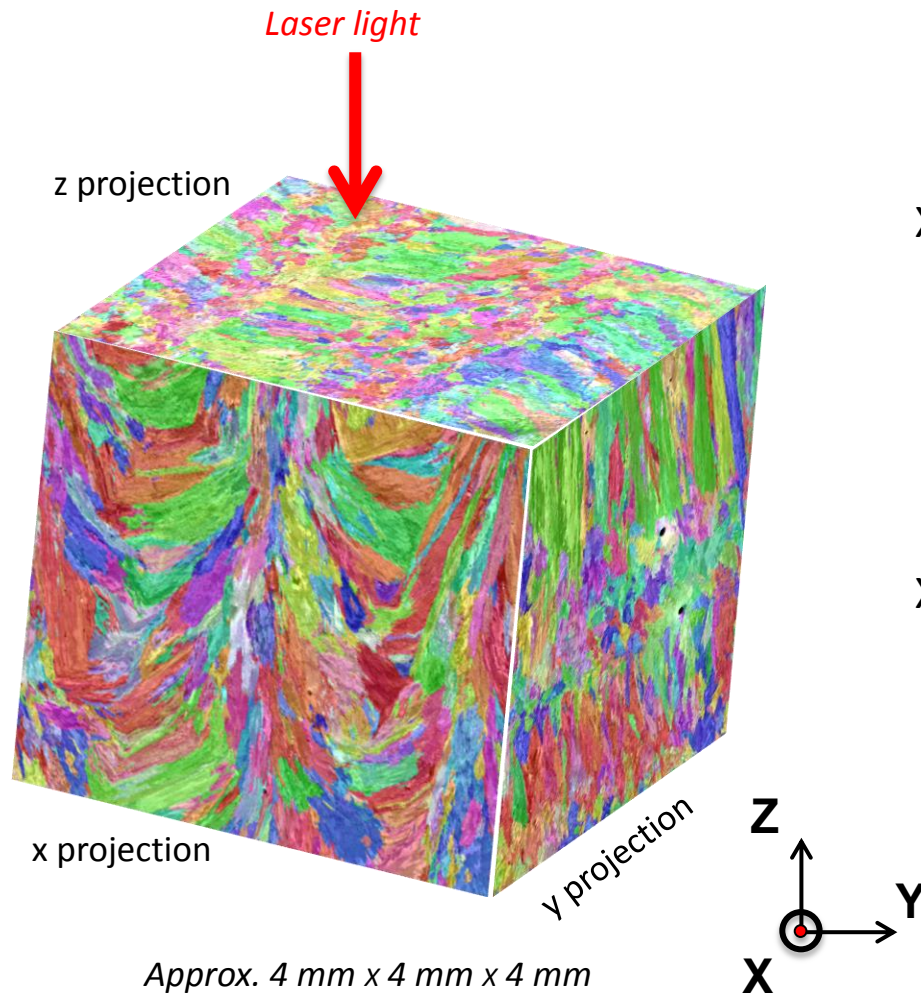
1 mm



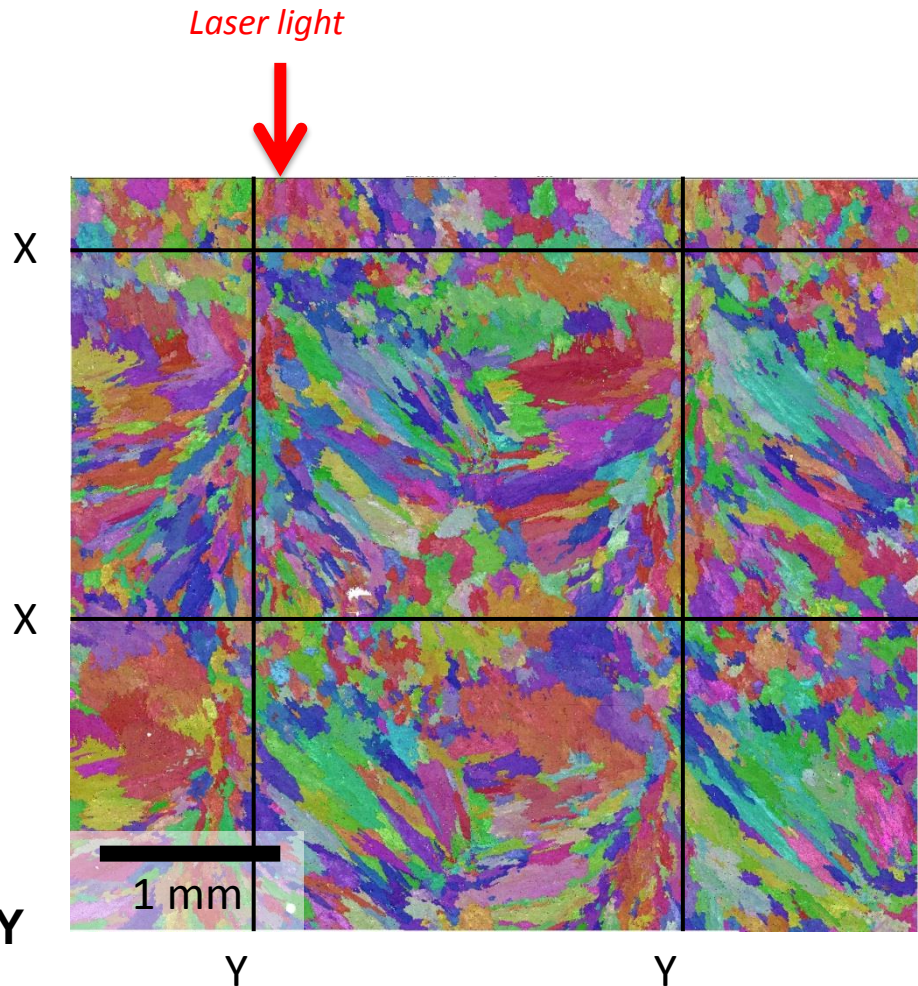
Fe	Cr	Ni	Mn	Si	Mo	Cu	V	C	P	S
bal	19	10.3	1.55	0.55	0.04	0.03	0.02	0.01	0.01	0.01

3D grain structure of AM material is a mixture of small and large grains.

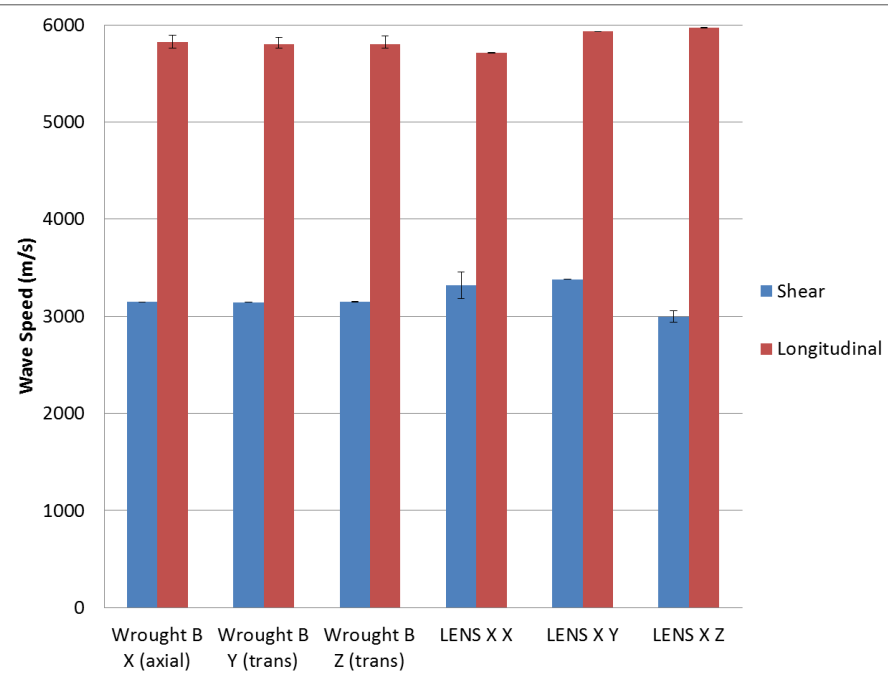
Parallel Hatch



Cross Hatch



Wave speeds in wrought and LENS cubes indicate anisotropy in LENS material.



- Measure shear wave speed, C_s
- Measure dilatational wave speed, C_d
- Measure density, ρ

Material	Direction	Density (kg/m ³)	Shear mod (GPa)	Poisson's Ratio	Elastic Modulus (GPa)
Wrought B	X (axial)	7854.5	77.8	0.29	201.3
Wrought B	Y (trans)		77.6	0.29	200.5
Wrought B	Z (trans)		77.8	0.29	201.0
LENS X	X	7842.9	86.6	0.24	215.5
LENS X	Y		89.6	0.26	225.7
LENS X	Z		70.5	0.33	187.6
		99.85 % dense			

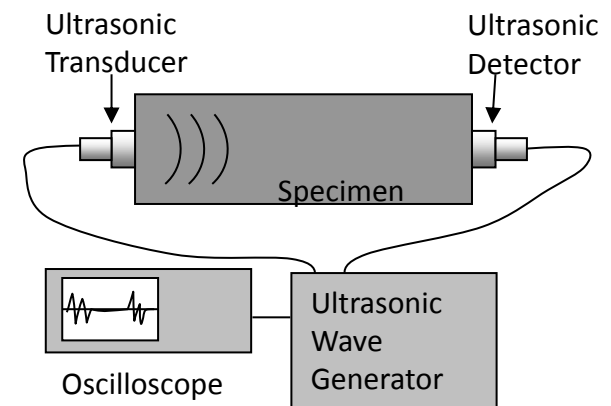
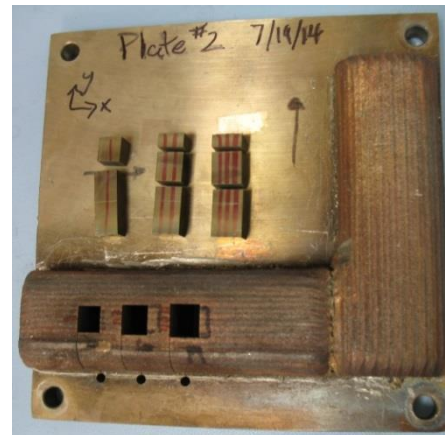
$$C_s = \sqrt{\frac{\mu}{\rho}}$$

$$\mu = C_s^2 \rho$$

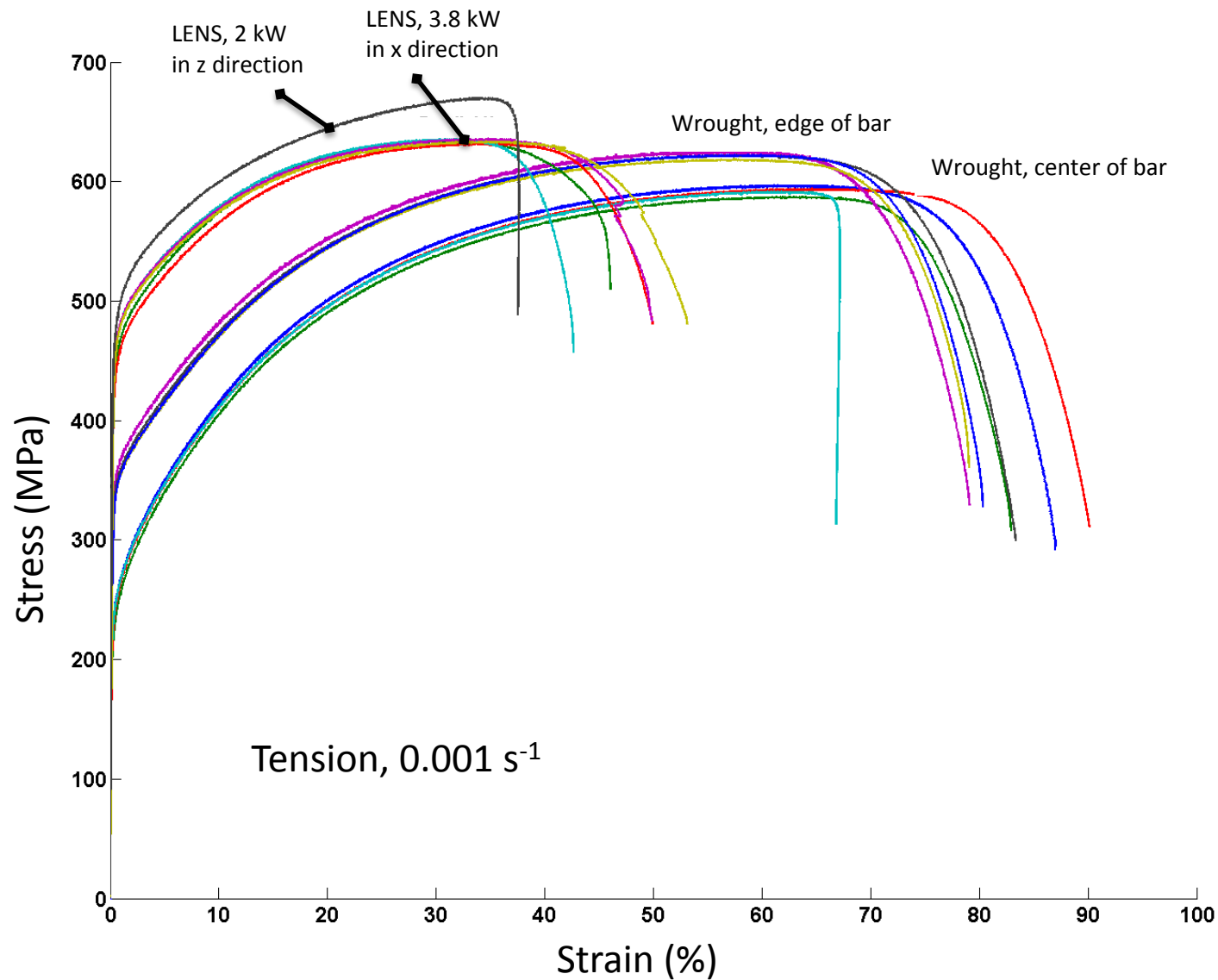
$$C_d^{pl-\varepsilon} = \sqrt{\frac{2(1-\nu)\mu}{(1-2\nu)\rho}}$$

$$\nu = \frac{\frac{1}{2}\left(\frac{C_d}{C_s}\right)^2 - 1}{\left(\frac{C_d}{C_s}\right)^2 - 1}$$

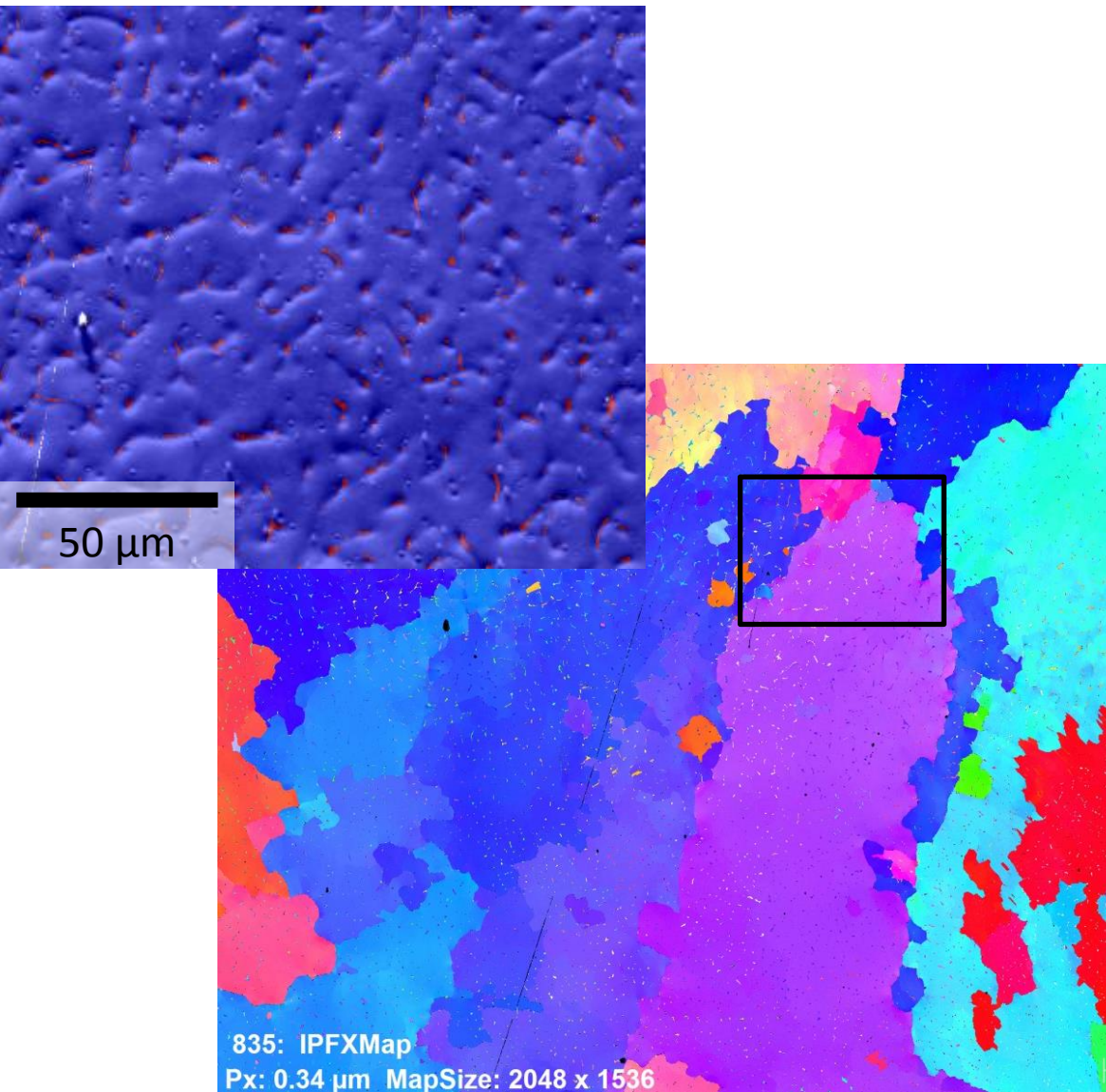
$$E = 2\mu(1+\nu)$$



LENS material is significantly stronger than wrought, contrary to the Hall-Petch expectation based on grain size.

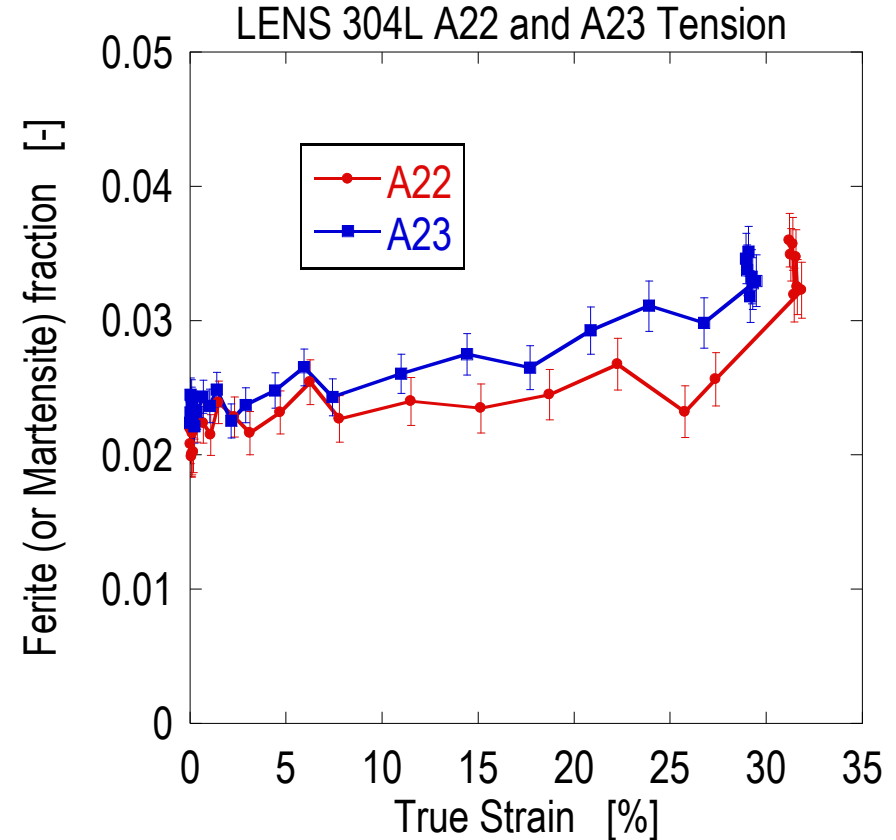
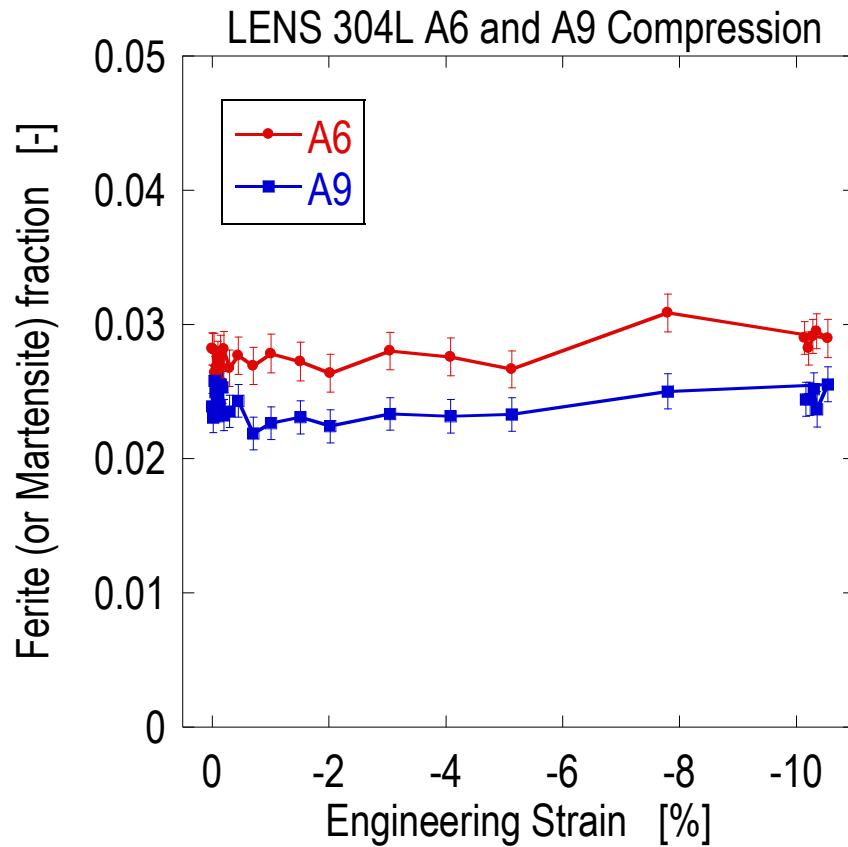


Hall-Petch is not limited to grain size. Small ferrite islands could be responsible for hardening.

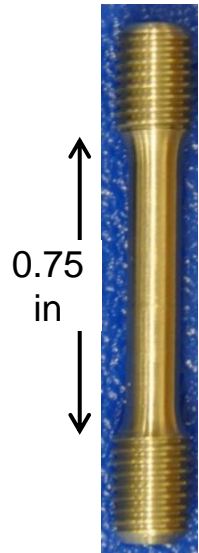


- Small ferrite islands
- Subgrains and grain substructure associated with geometrically necessary dislocations.
- Initial BCC phase: 1.2% for Wrought and 2.3% for LENS (ferritescope)
- Ferrite content appears to increase slightly with loading ($\sim 3\%$)

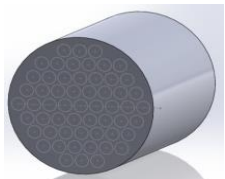
Ferrite content in LENS samples may increase slightly with tensile loading (Neutron Diffraction at LANL)



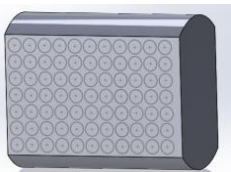
Quasistatic tension on wrought SS304L exhibit some moderate strain rate dependence.



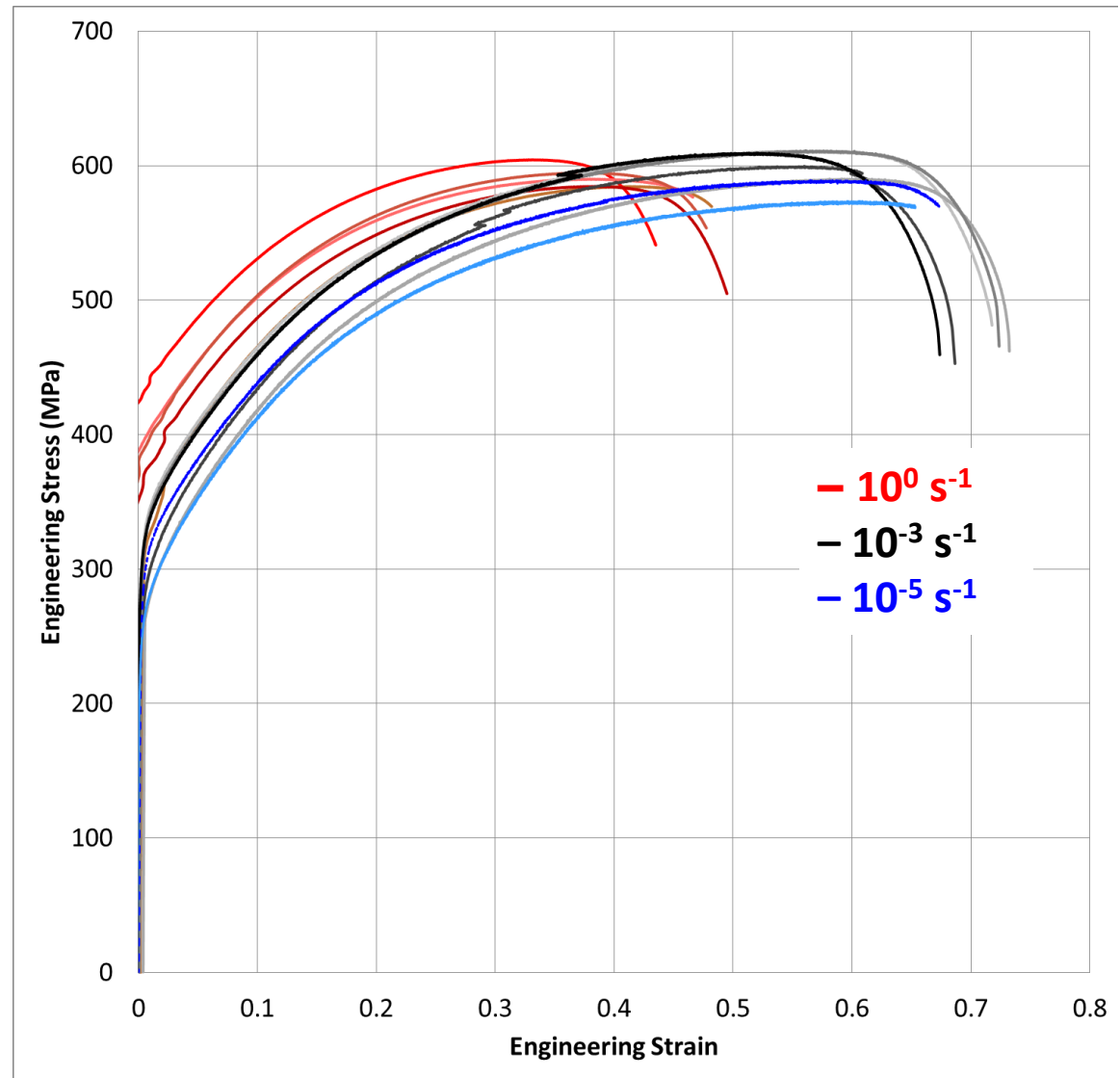
Ø 0.16 in



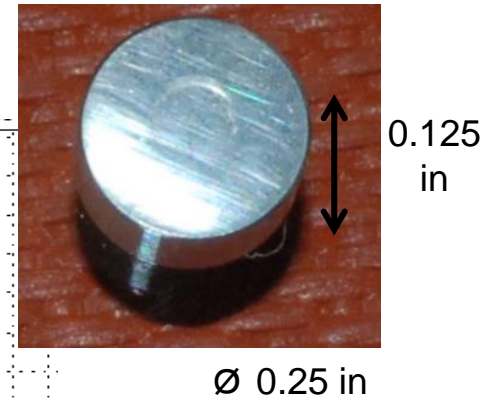
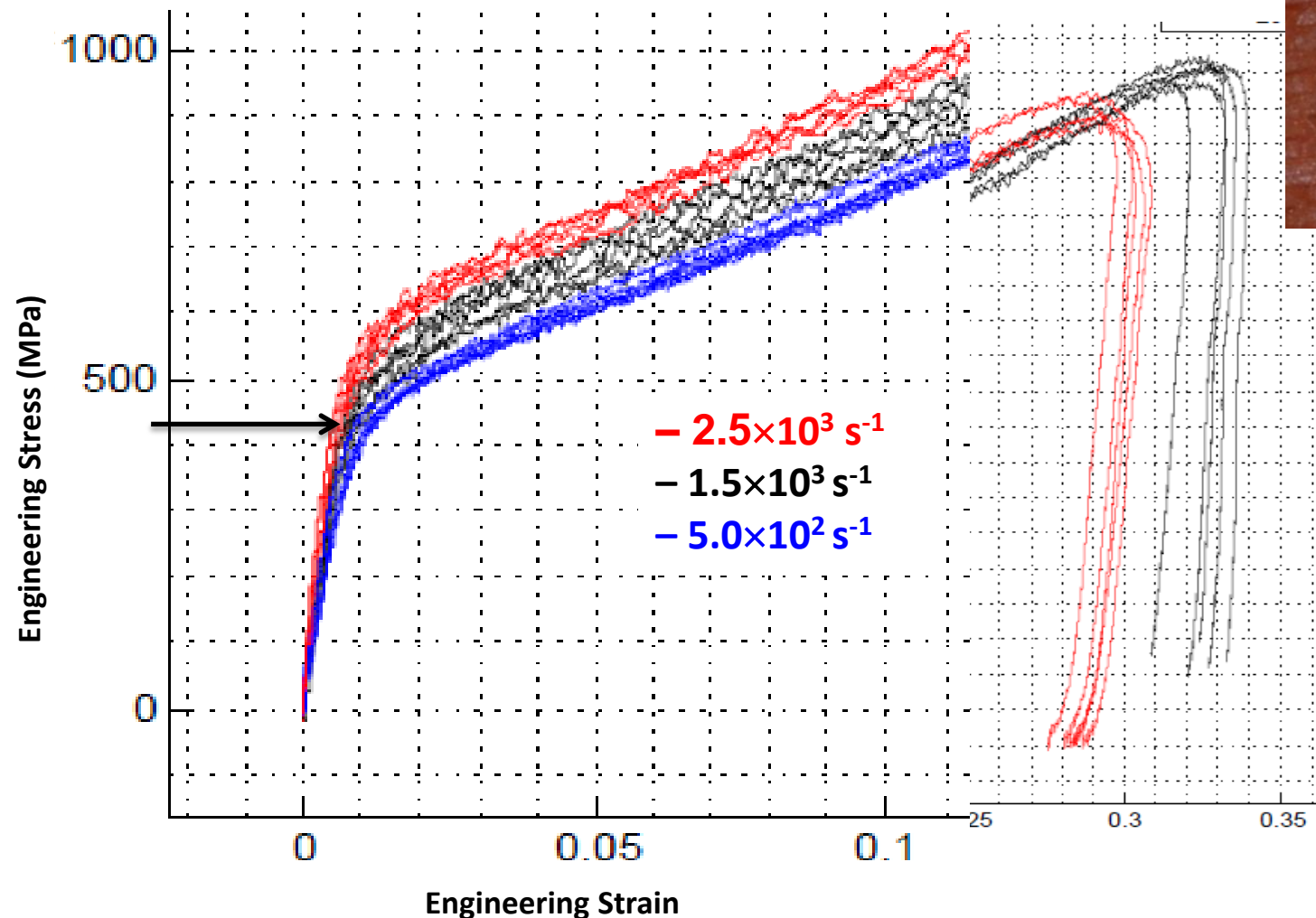
Longitudinal



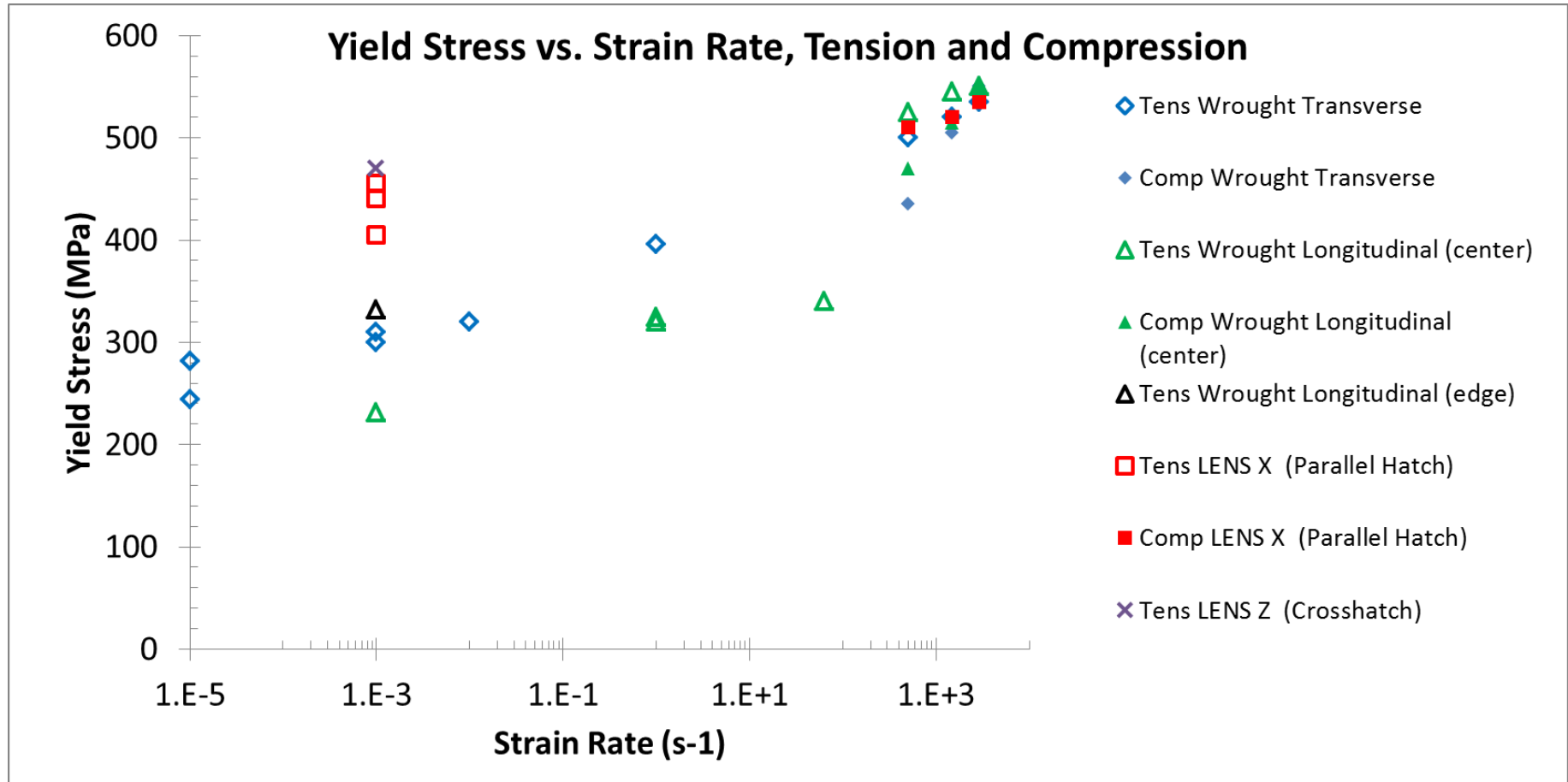
Transverse



Dynamic compression on conventional SS304L exhibit some moderate strain rate dependence.

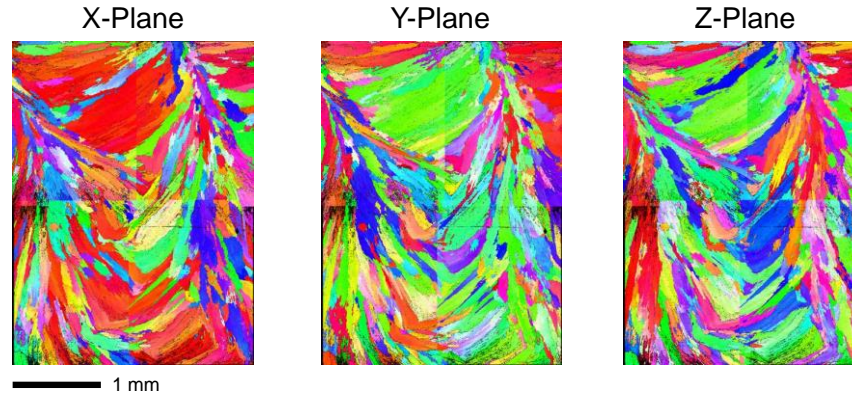
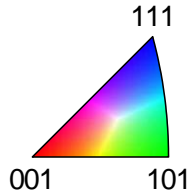


Strain rate effects of wrought and AM 304L in tension.

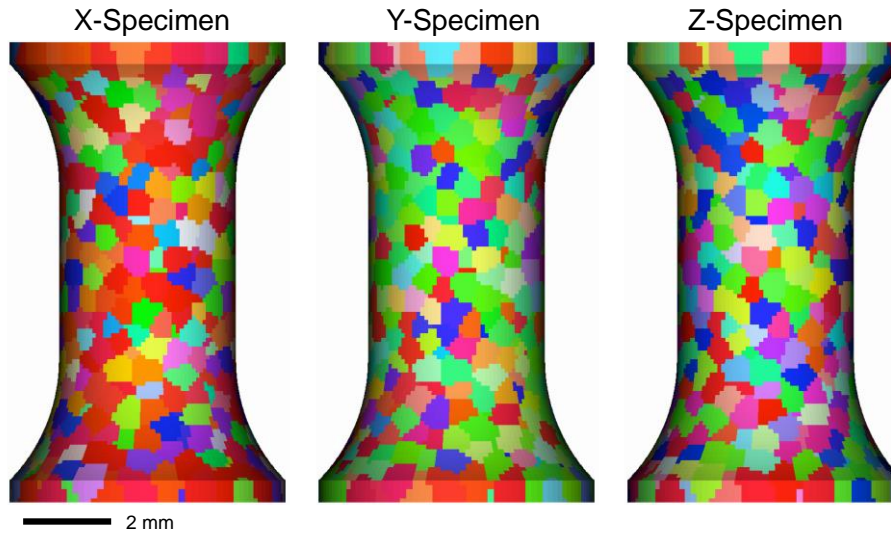
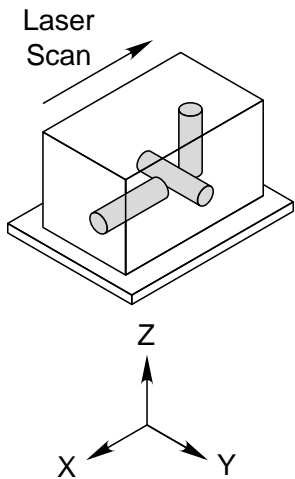


- LENS material appears to be less strain rate dependent.

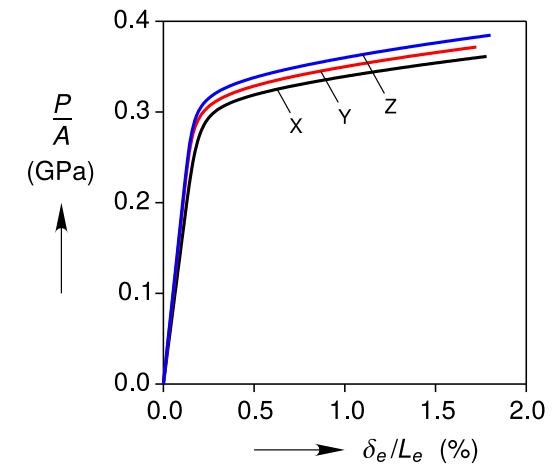
EBSD Orientation Maps



Tensile Specimens

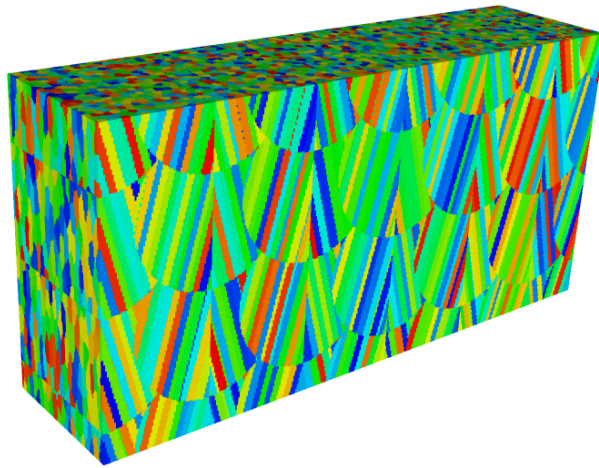


Mechanical Responses

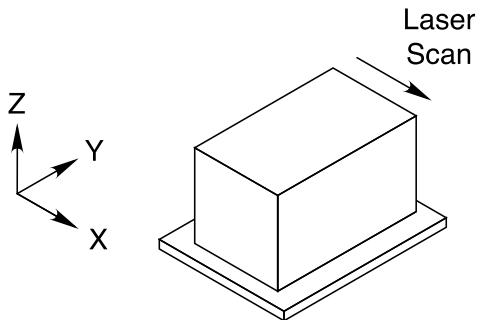


Modeling effects of grain morphology and orientation on mechanical behavior.

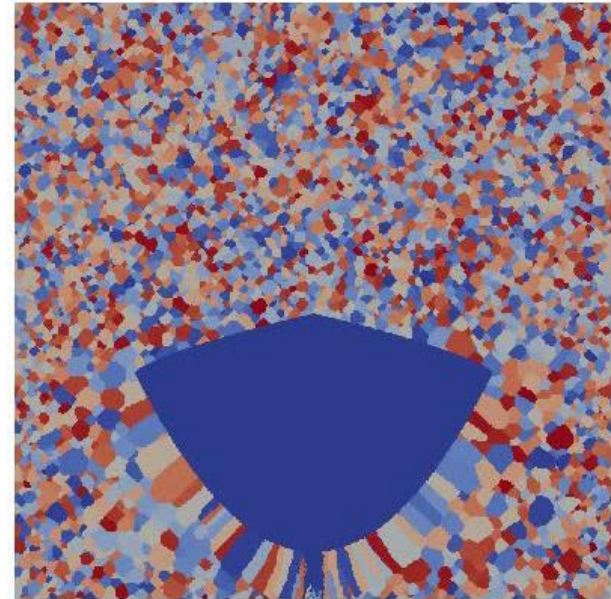
Initial Attempt:
Voronoi Tessellation



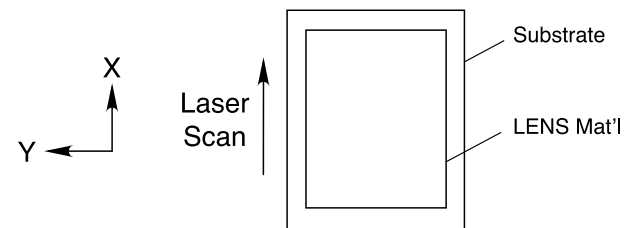
bead size = 1 mm
grain size = 40 microns



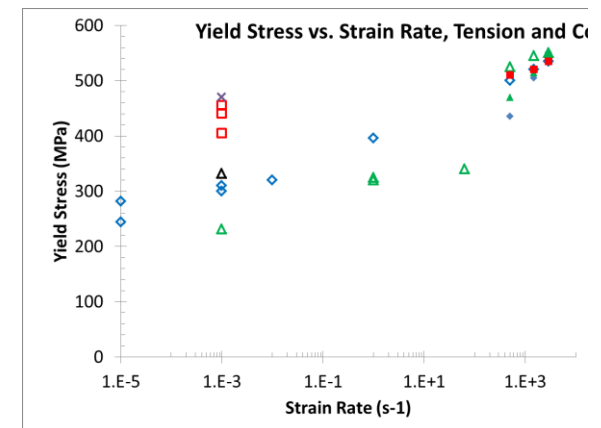
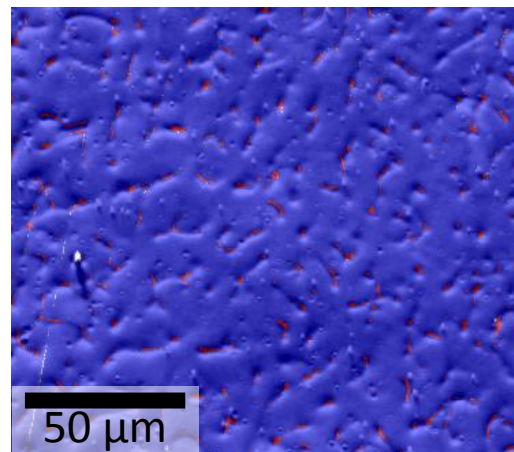
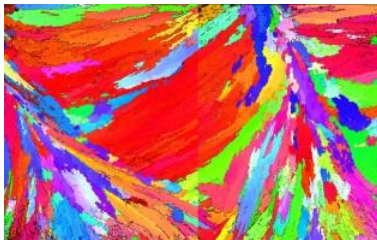
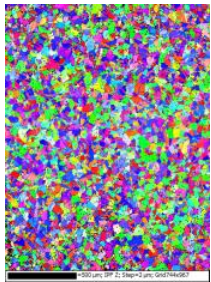
Future Direction:
Grain Growth



Video courtesy of Veena Tikare (Org. 1444)
and John Madison (Org. 1814)

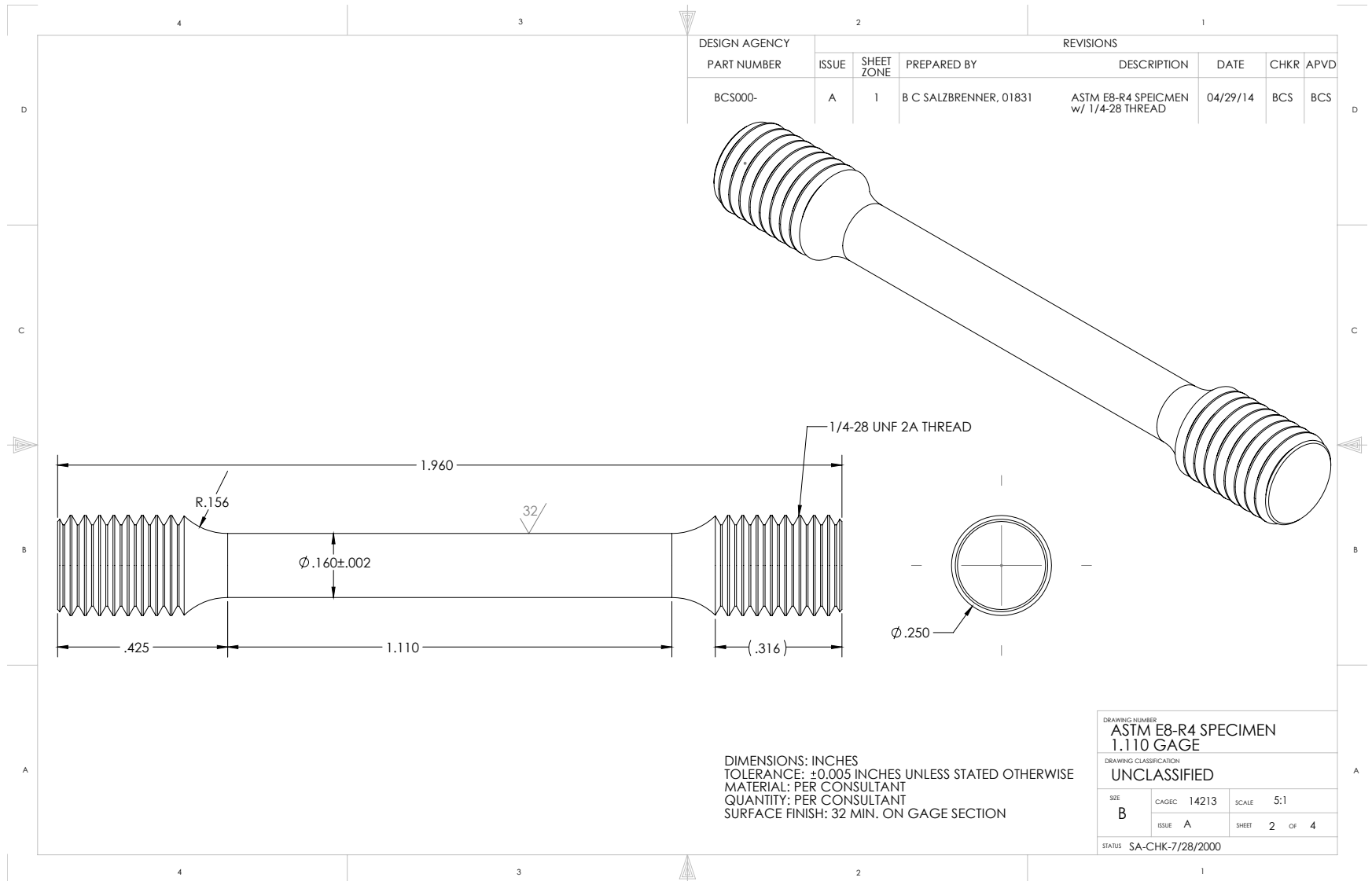


1. Microstructure in LENS-like 304L is considerably different from conventional 304L.
2. LENS 304L is stronger despite larger grain size.
 - Ferrite islands at micron scale are likely responsible.
3. Strain rate dependence observed.

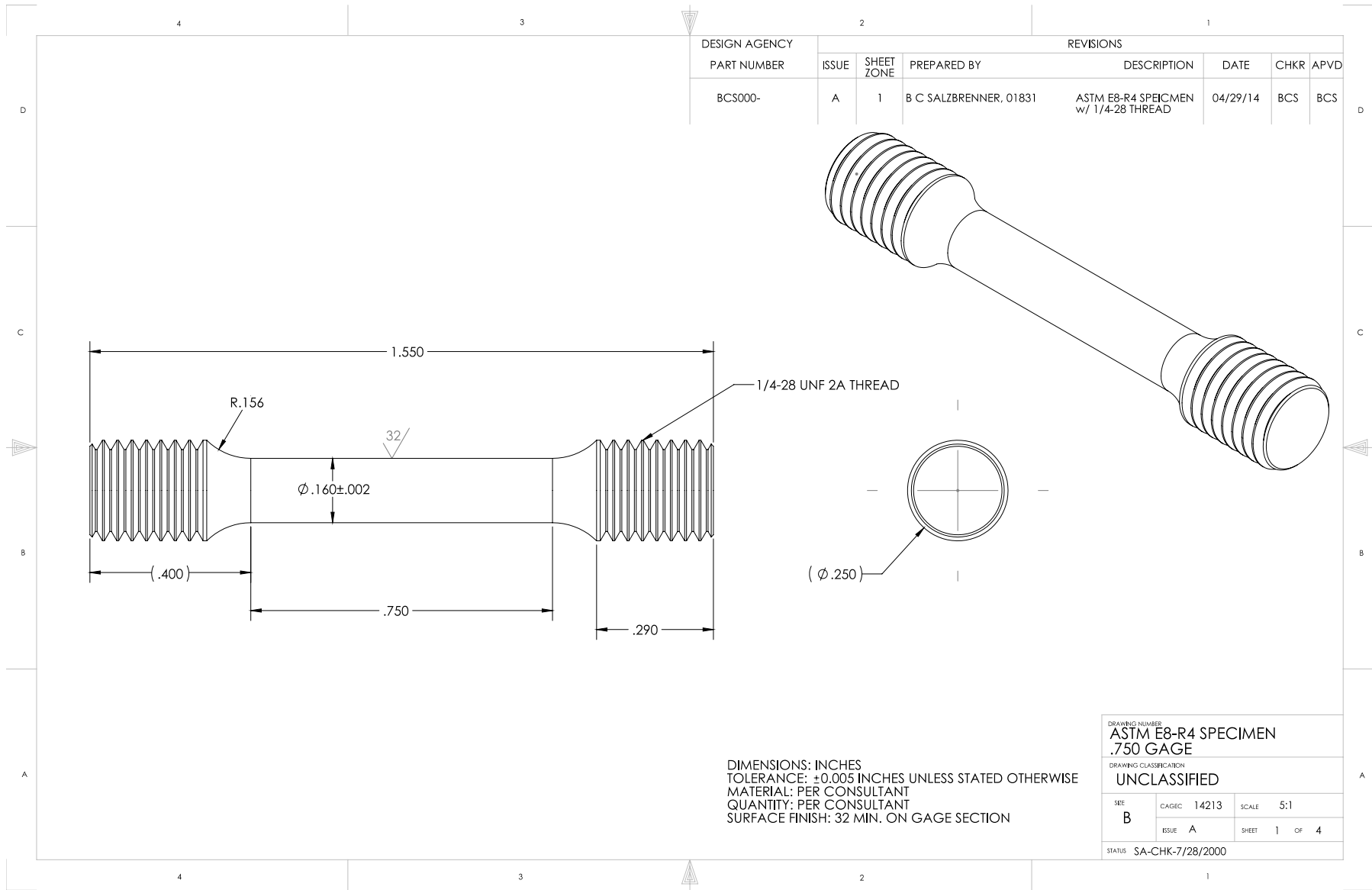


Extra Slides

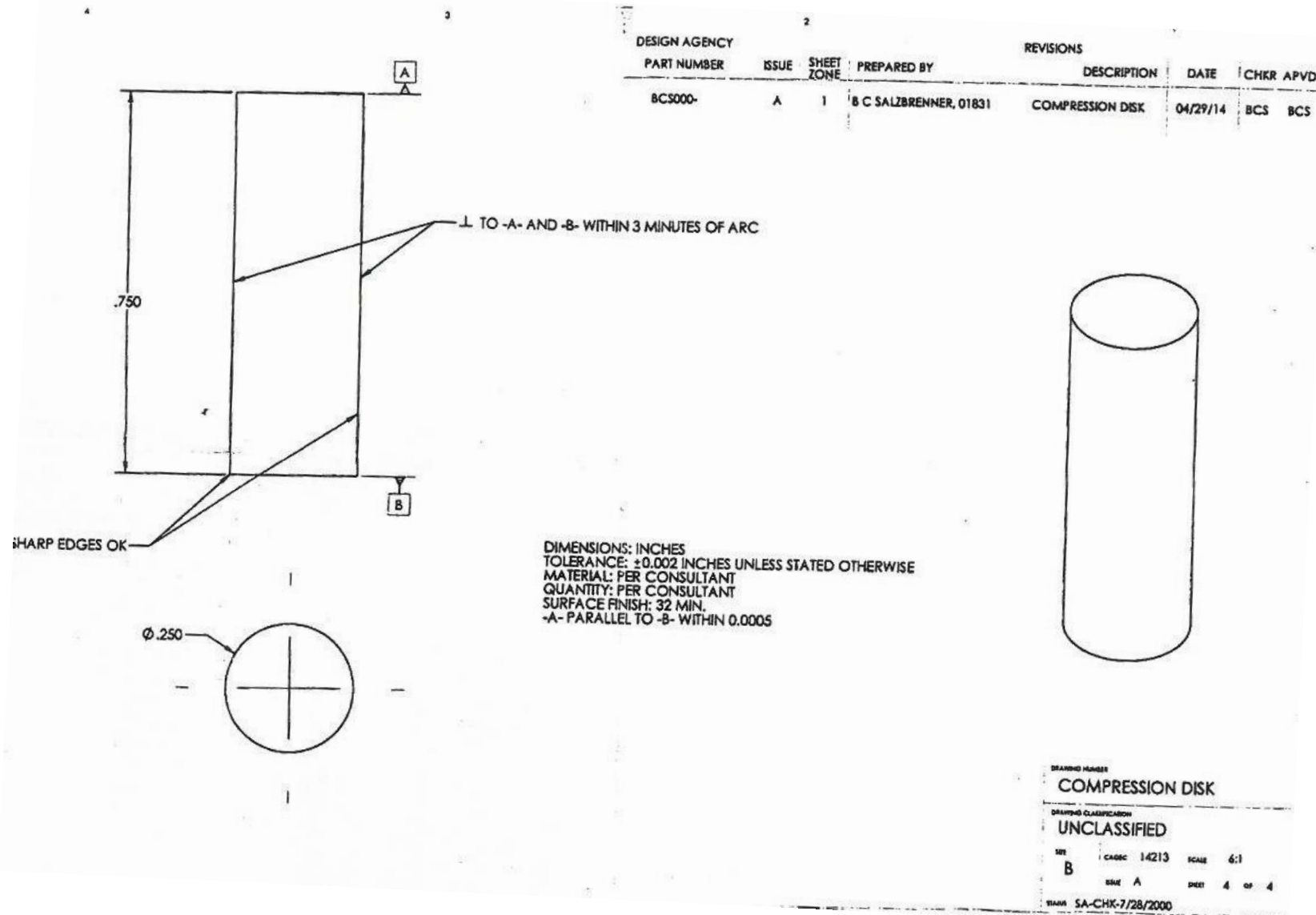
Tensile samples for testing (quasi-static)



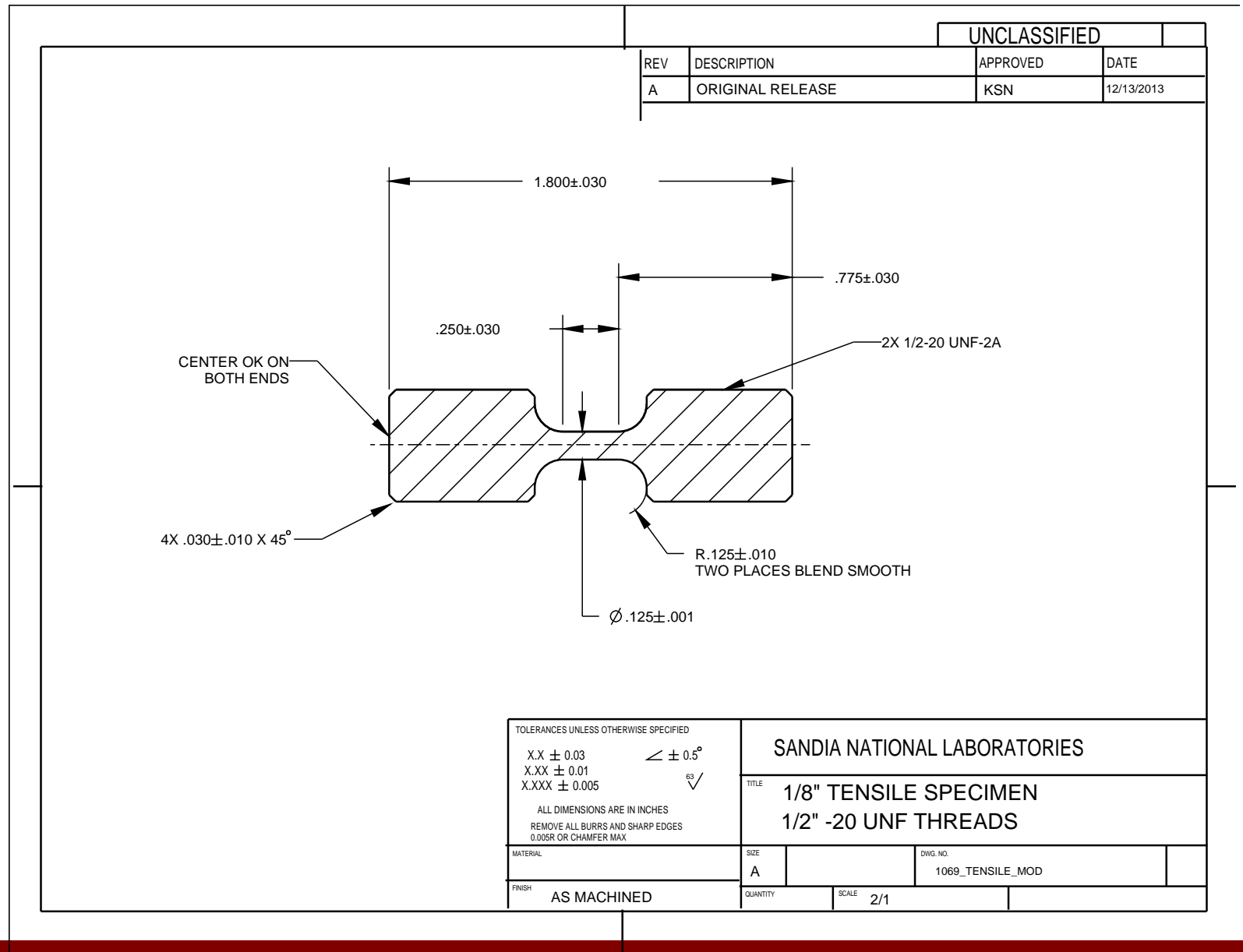
Tensile samples for testing (quasi-static)



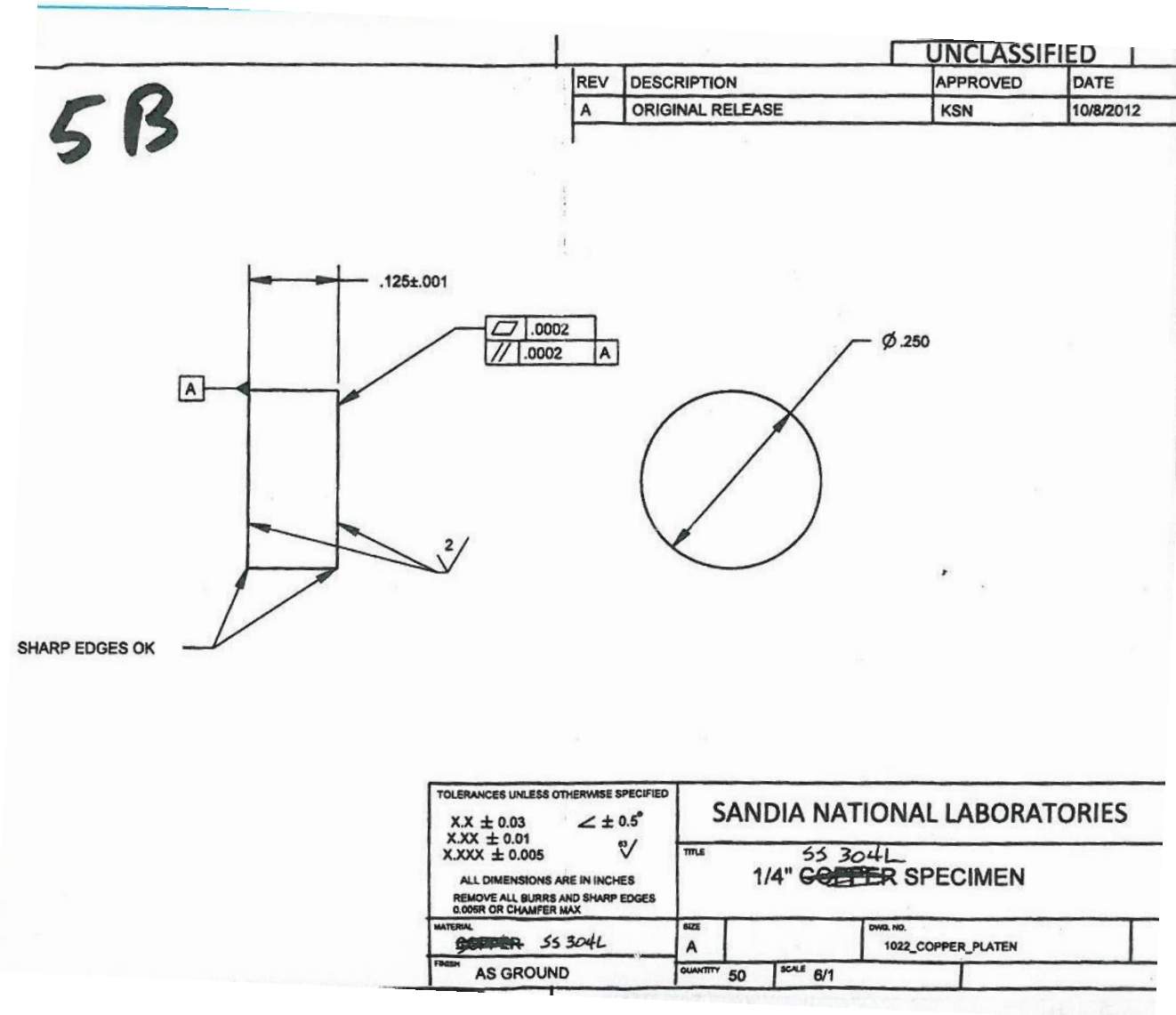
Tensile samples for testing (quasi-static, compression)



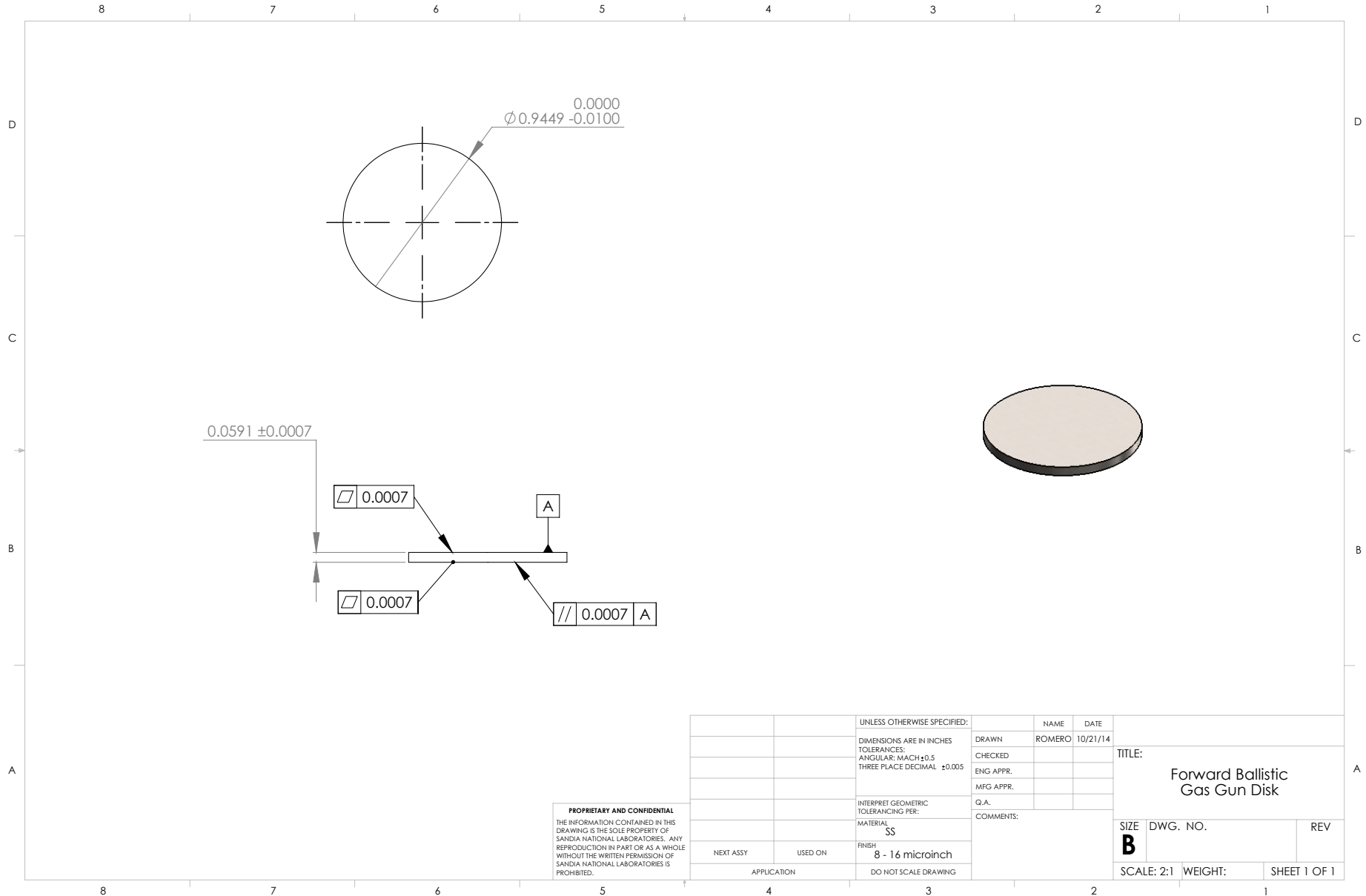
Tensile samples for testing (Hopkinson)



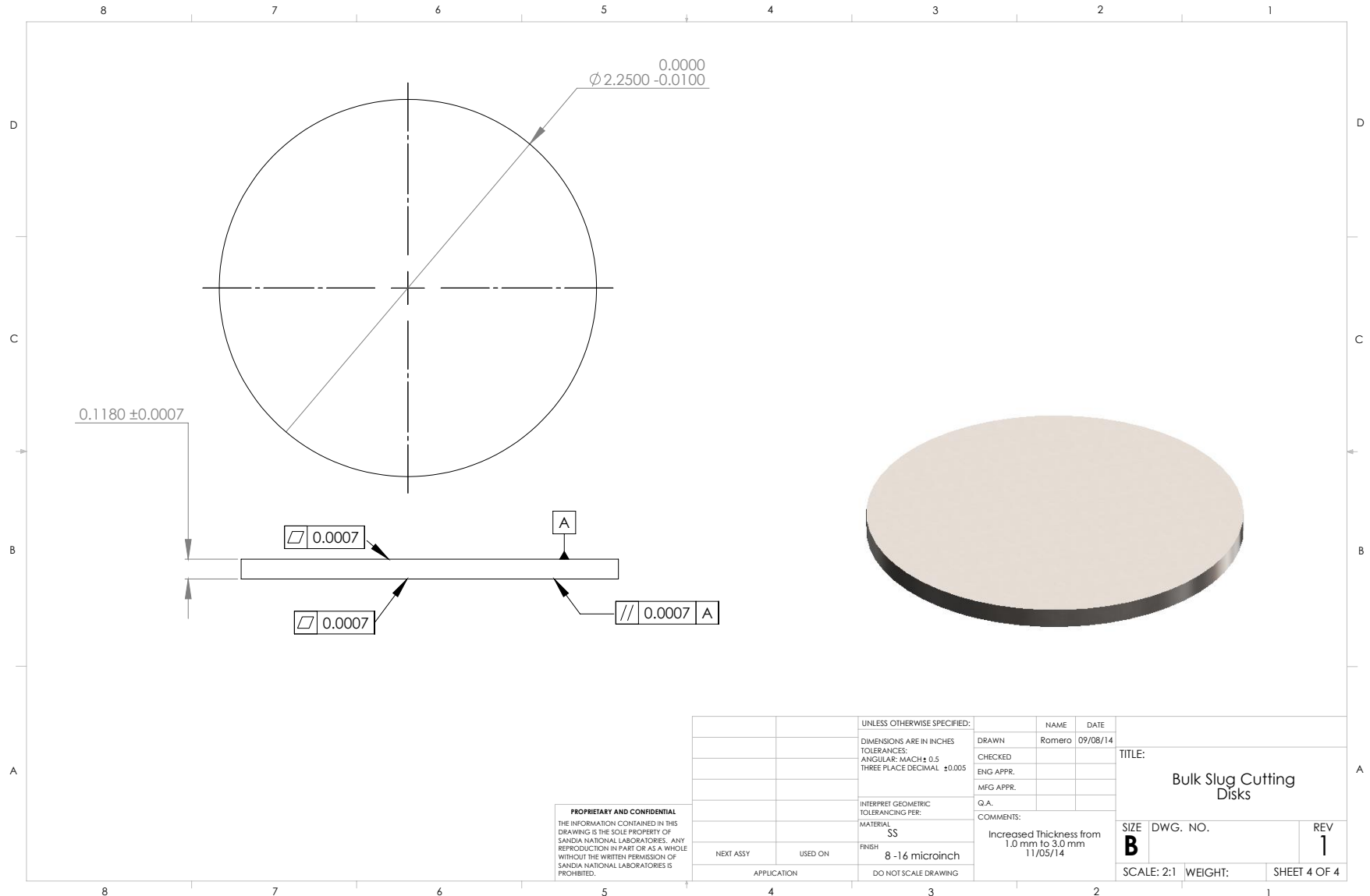
Tensile samples for testing (Hopkinson, compression)



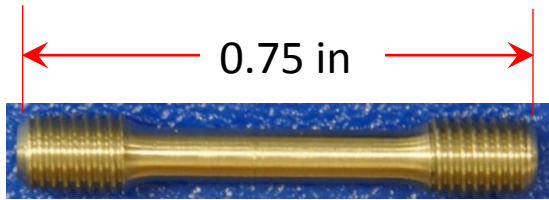
Tensile samples for gas gun testing (forward ballistic)



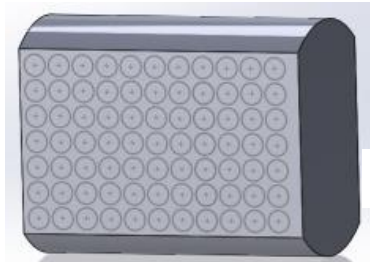
Tensile samples for gas gun testing (reverse ballistic)



Quasistatic mechanical tests on wrought 304L SS

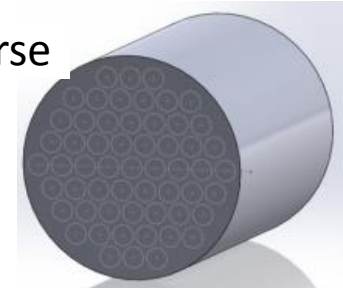


$\varnothing 0.16$ in

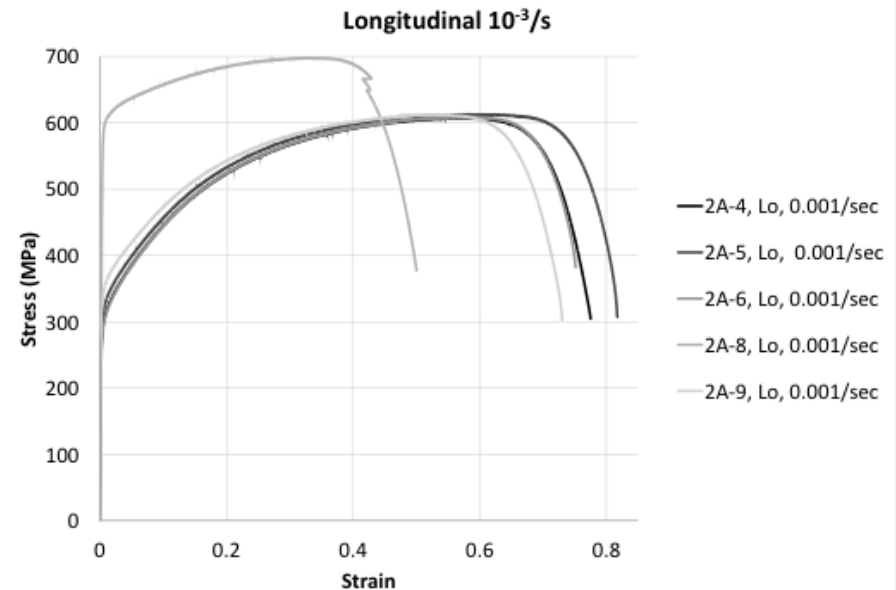
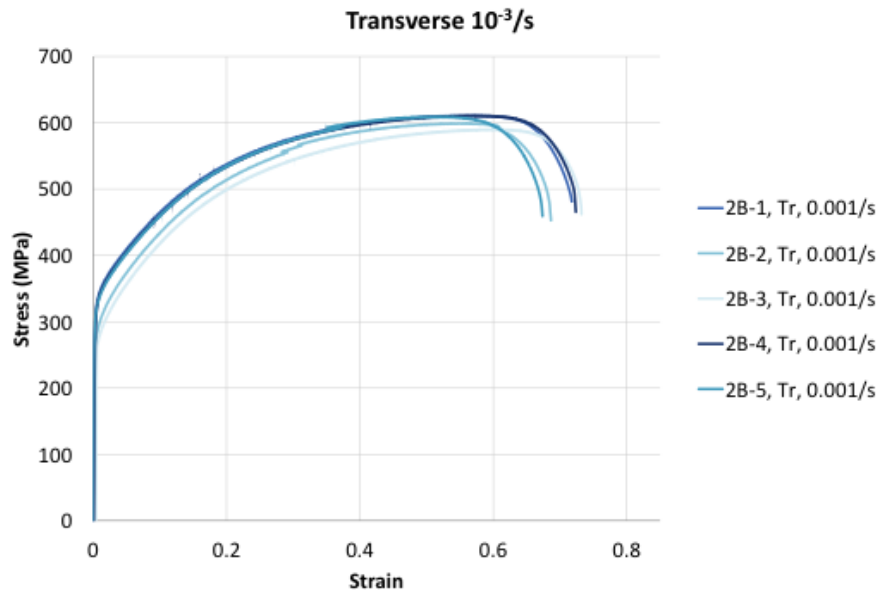


longitudinal

transverse



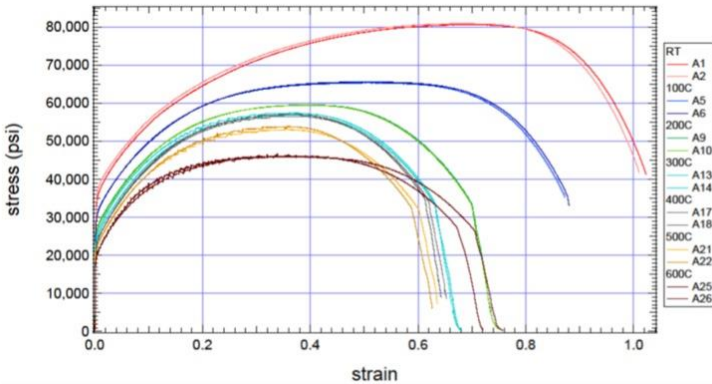
Stress-strain curves



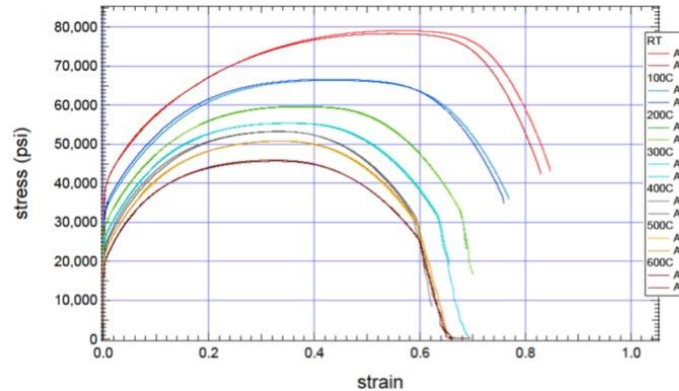
Temperature and strain rate dependence of 304L

Antoun (Sandia)

Axial Orientation - Effect of Temperature on 9800314 304L VAR
strain rate = 0.001/s



Axial Orientation - Effect of Temperature on 9800314 304L VAR
strain rate = 0.1/s



Lichtenfield et al. 2006

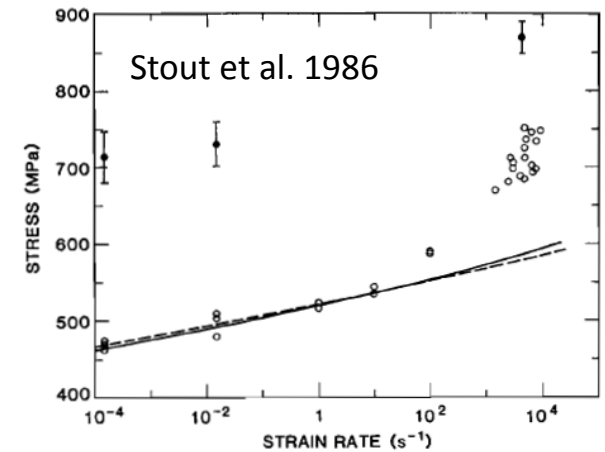
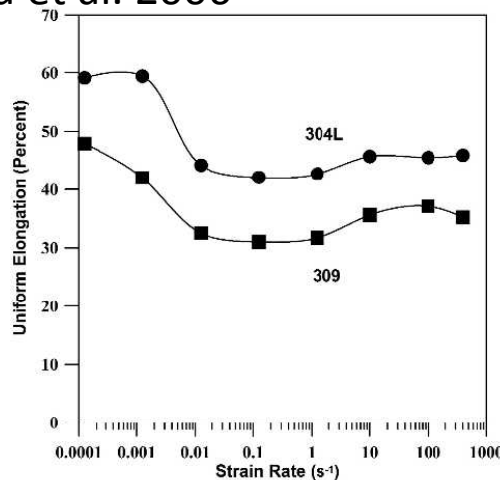
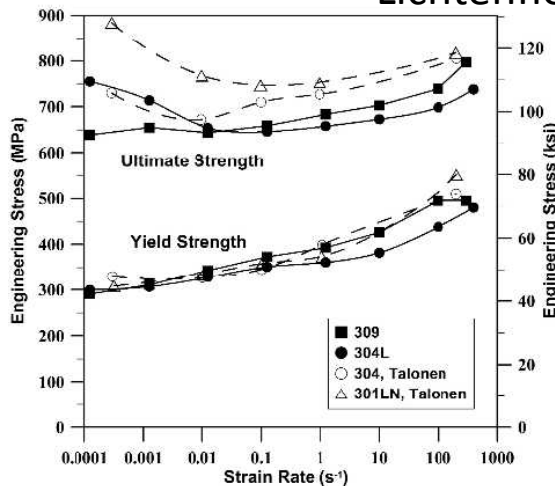


Fig. 13 Comparison of the flow stress values (circles) with equation (14) (solid line) and the power law, equation (7) (dashed line), with $Q = 522$ MPa and $m = 0.0123$. Also included in this plot are the measured mechanical threshold stress values (solid circles with error bars).

Fig. 5—Var
for 309 and

- Temperature has a significant effect on strength and ductility.
- Higher strain rate has little effect on strength, but a noticeable effect on ductility.