



# Variability in Mechanical Properties of Laser Engineered Net Shaping Material

**Jay D. Carroll<sup>1</sup>, David P. Adams<sup>1</sup>, Michael C. Maguire<sup>1</sup>,  
Joseph E. Bishop<sup>1</sup>, Benjamin Reedlunn<sup>1</sup>, Bo Song<sup>1</sup>,  
Joseph R Michael<sup>1</sup>  
Todd Palmer<sup>2</sup>  
John S. Carpenter<sup>3</sup>, Bjorn Clausen<sup>3</sup>, Donald W. Brown<sup>3</sup>**



**Sandia  
National  
Laboratories**

*Exceptional  
service  
in the  
national  
interest*

<sup>1</sup>Sandia National Laboratories

<sup>2</sup>Pennsylvania State University

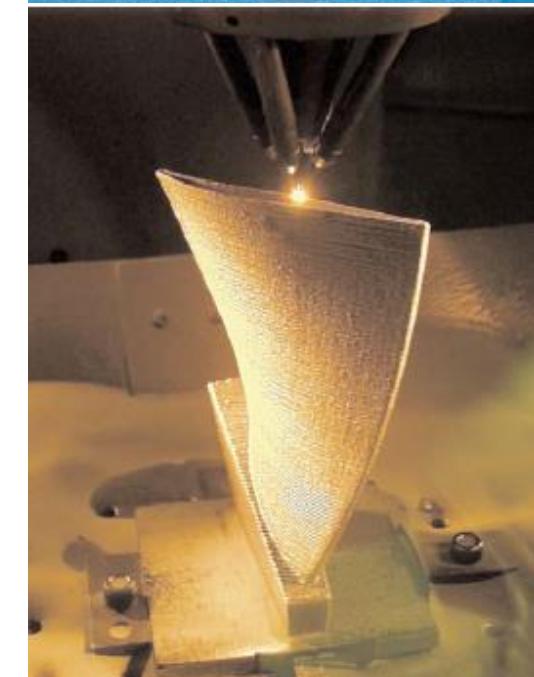
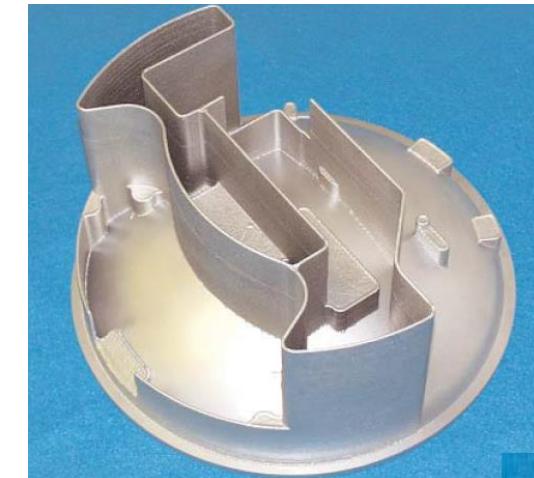
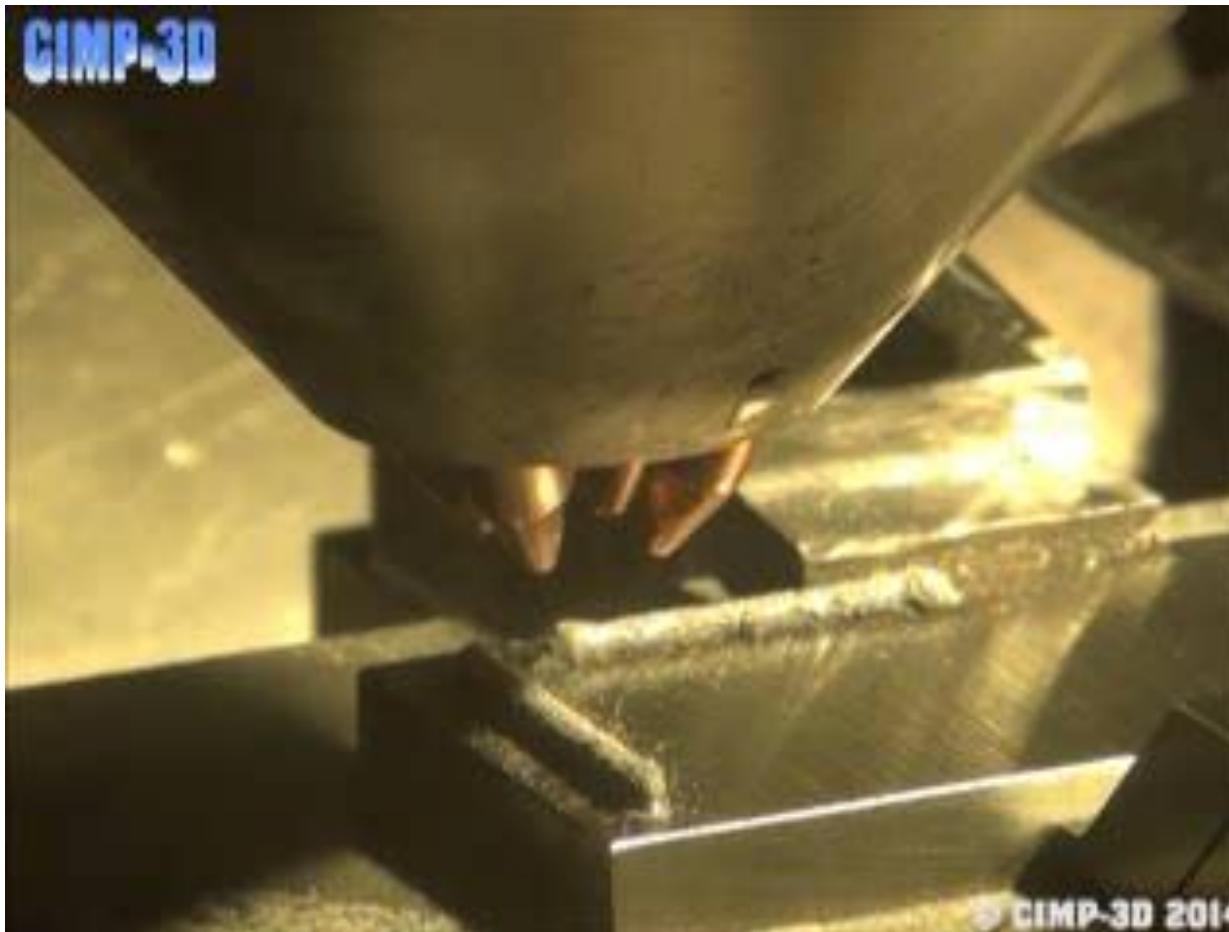
<sup>3</sup>Los Alamos National Laboratory



Sandia National Laboratories is a multi-program laboratory managed and operated by Sandia Corporation, a wholly owned subsidiary of Lockheed Martin Corporation, for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000. SAND NO. 2011-XXXX

As opposed to powder-bed technology, the LENS process builds material by injecting powder feedstock with laser heating.

LENS = Laser Engineered Net Shaping



Courtesy of Todd Palmer, Pennsylvania State University

# Project: Strain rate effects, variability, and modeling of LENS-like 304L

Quasistatic  $10^{-5} - 10^0$



Dynamic  $5 \times 10^2 - 3 \times 10^3$



Plate Impact  $10^7 - 10^9$

**Propellant Gun 89mm**



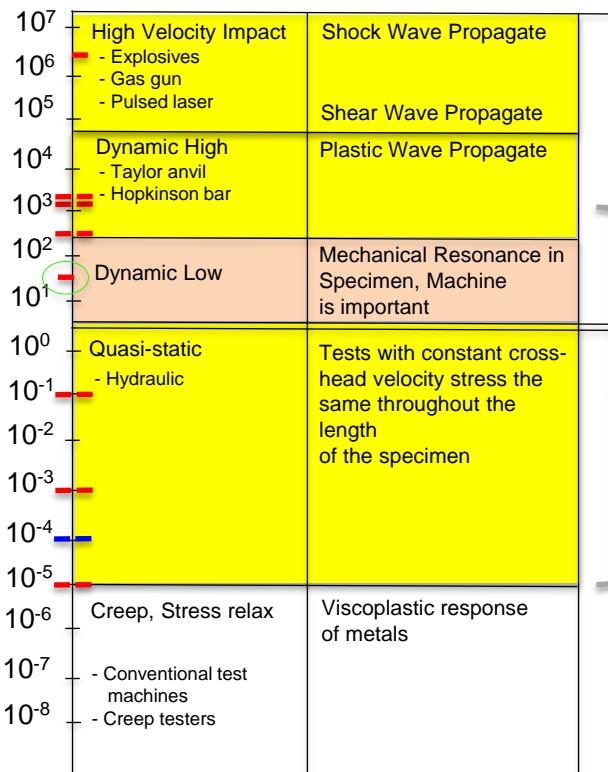
Crystal Plasticity  
Modeling



Microscopy



Common Tests      Dynamic Consideration



Experiments

Chart is from  
Meyers'  
Dynamic  
Behavior of  
Materials

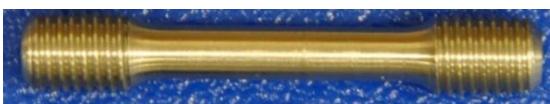
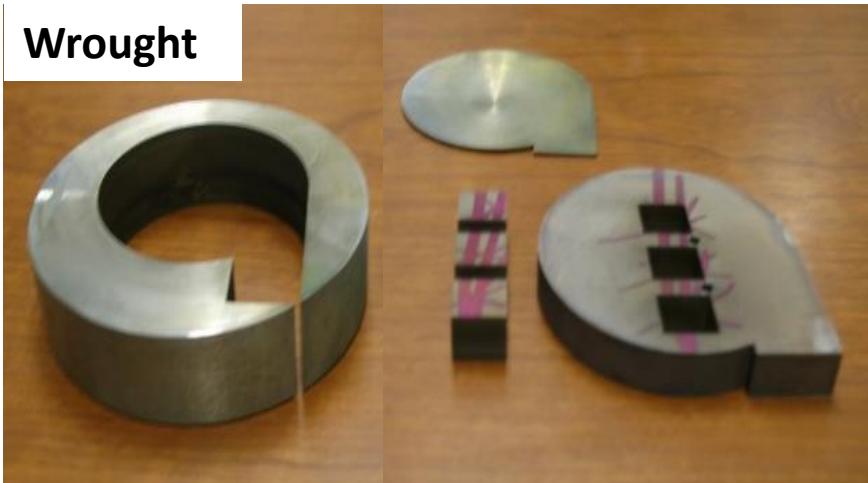
— Tests at SNL  
- - Tests at LANL with neutrons

Neutron Diffraction

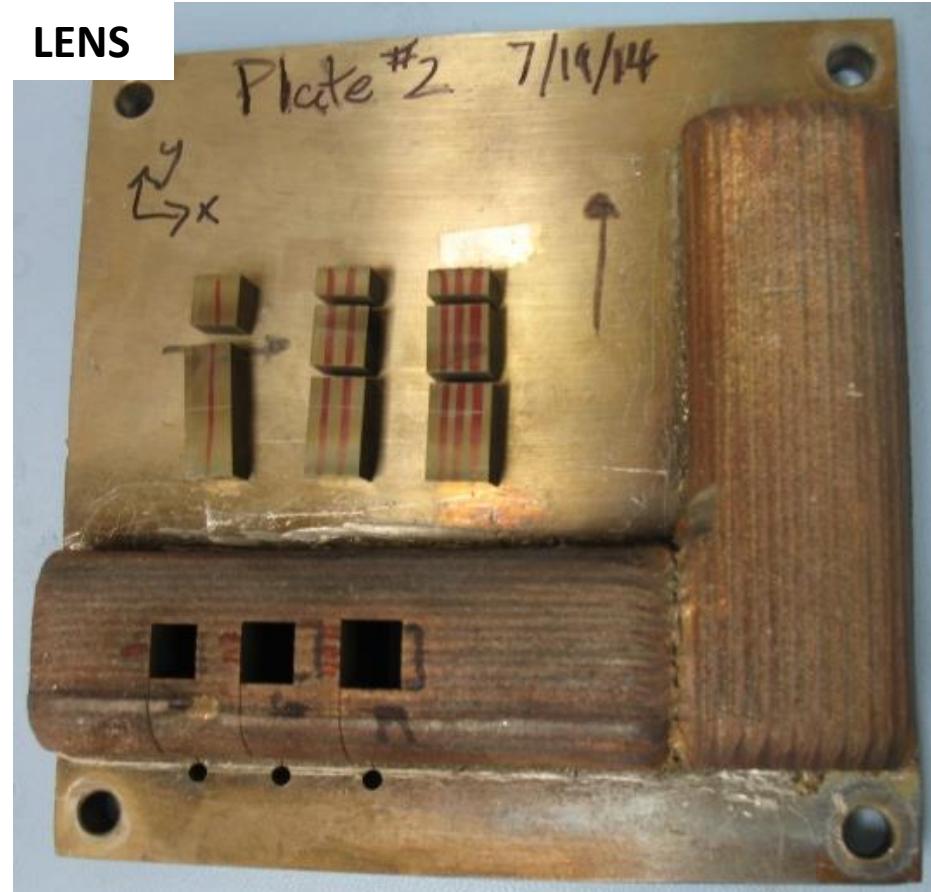


# Specimens cut from wrought and LENS bars for comparison.

Wrought



LENS



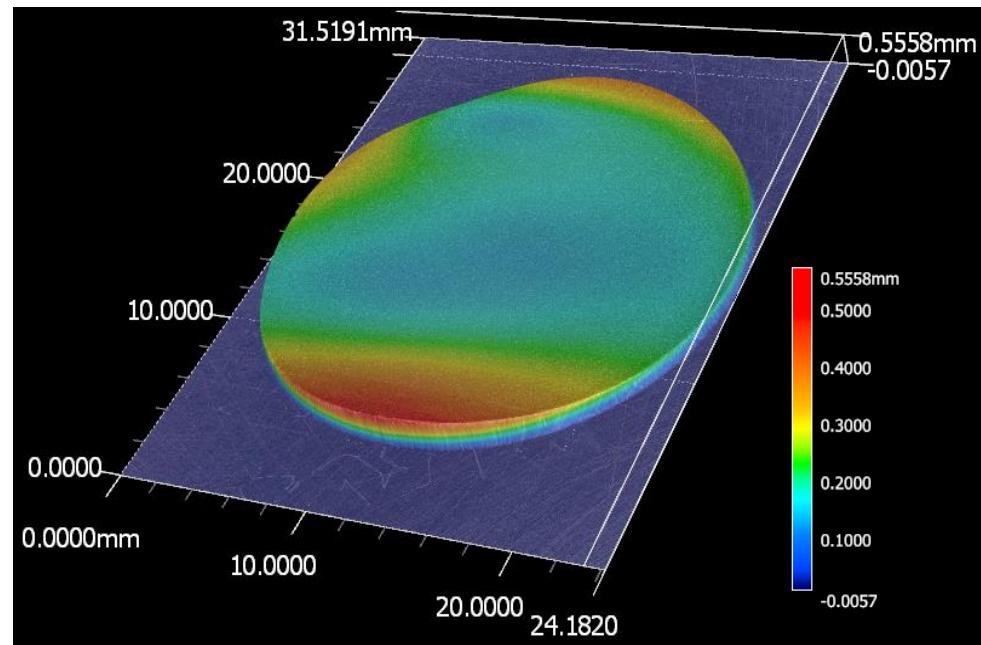
# LENS residual stresses are not as extreme as feared



Lattice parameters in specimens show little difference

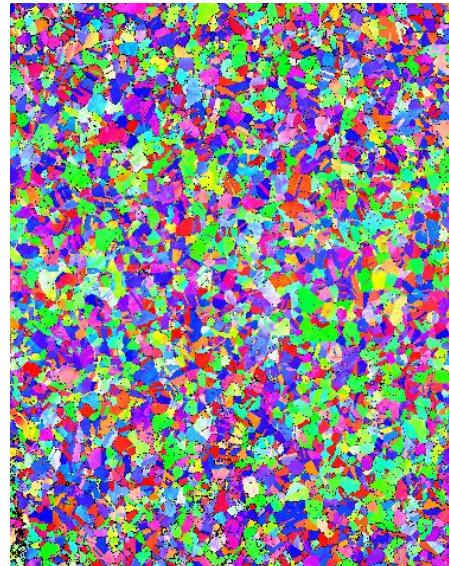
	<i>Austenite parameters</i>	
	$a_l$	$a_t$
Wrought	3.5932 Å	3.5900 Å
LENS 3.8kW //	3.5938 Å	3.5904 Å
LENS 2kW +	3.5941 Å	3.5908 Å

- Base plate warped significantly (12 mm thick).
- Lattice parameters in specimens cut from bars show little difference.
- 100  $\mu\text{m}$  disk cut with very little warping (0.5 mm max over 25 mm).



# LENS grain size is much larger than wrought 304L SS. Same chemistry.

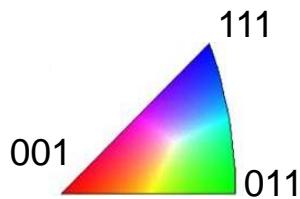
Wrought



LENS



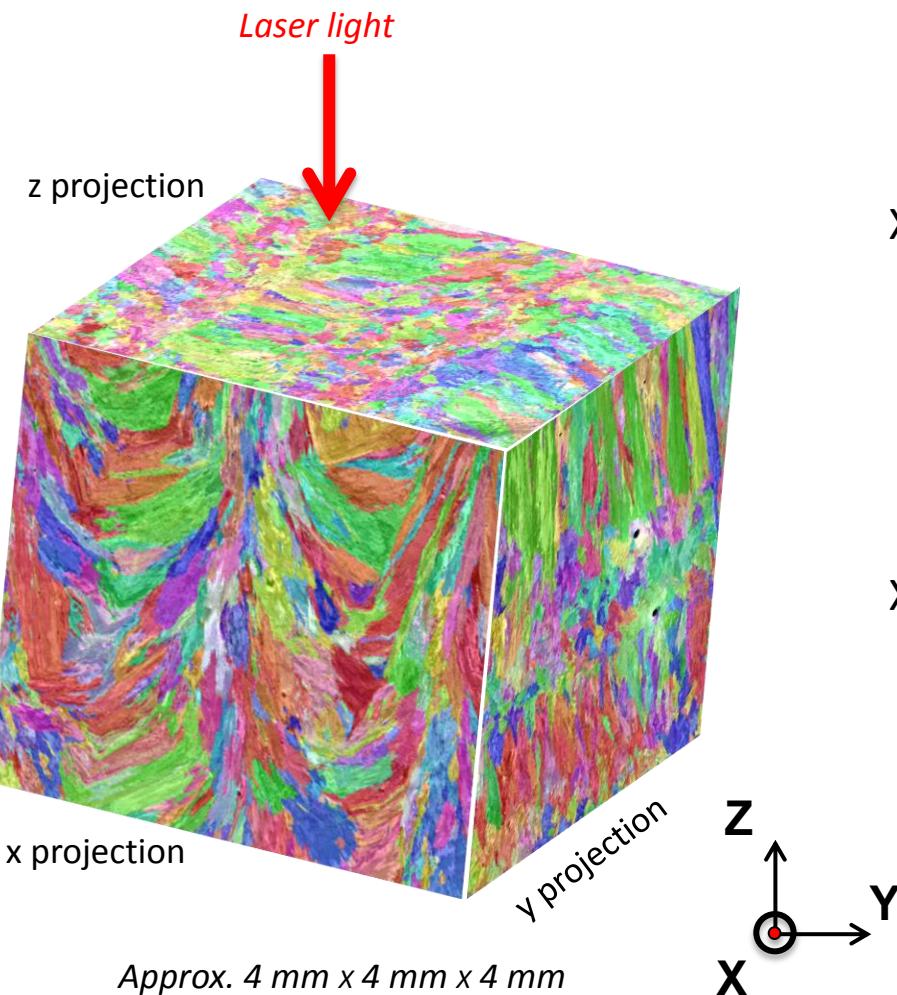
1 mm



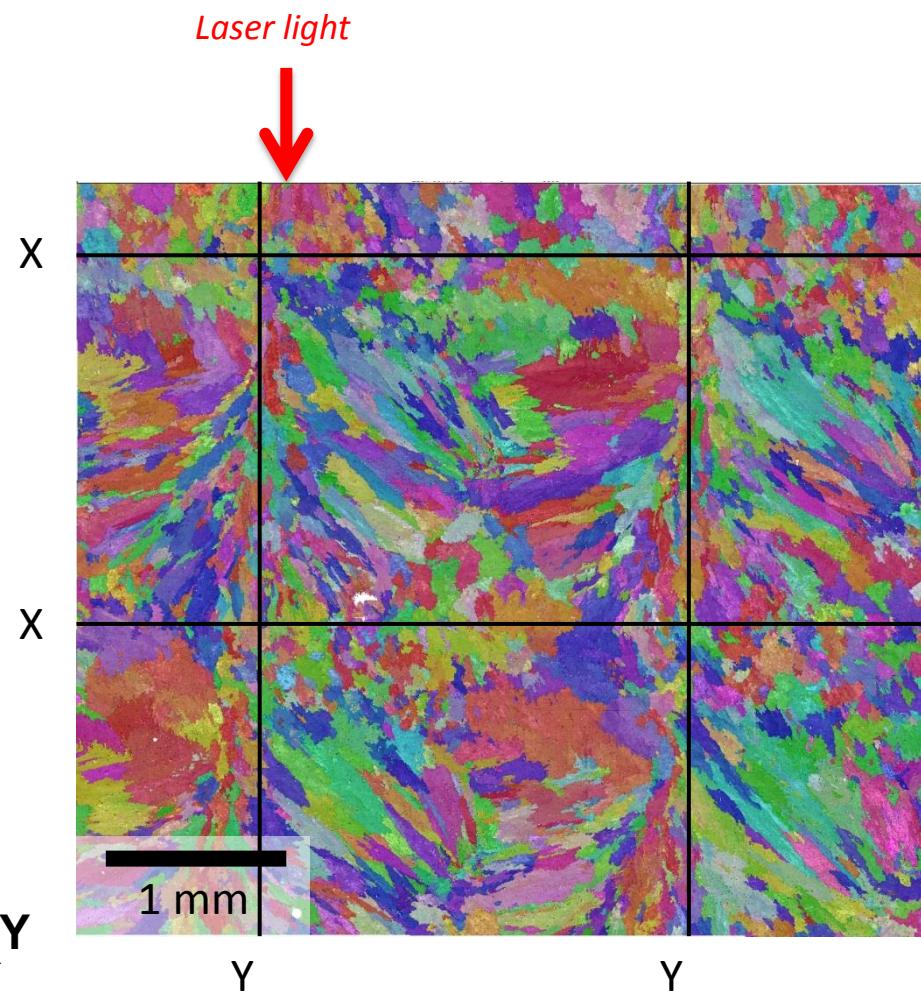
Fe	Cr	Ni	Mn	Si	Mo	Cu	V	C	P	S
bal	19	10.3	1.55	0.55	0.04	0.03	0.02	0.01	0.01	0.01

# 3D grain structure of AM material is a mixture of small and large grains.

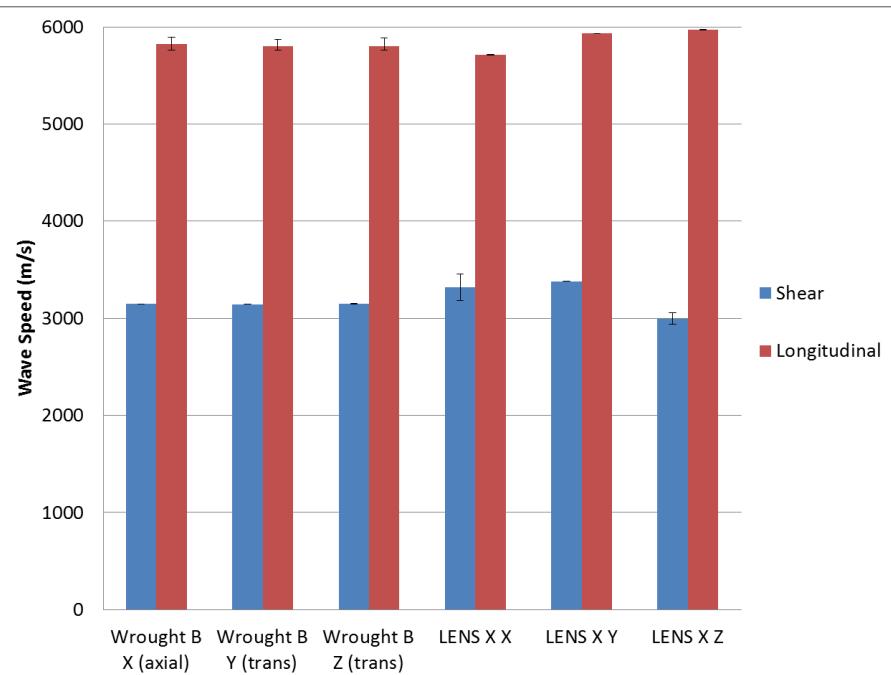
Parallel Hatch



Cross Hatch



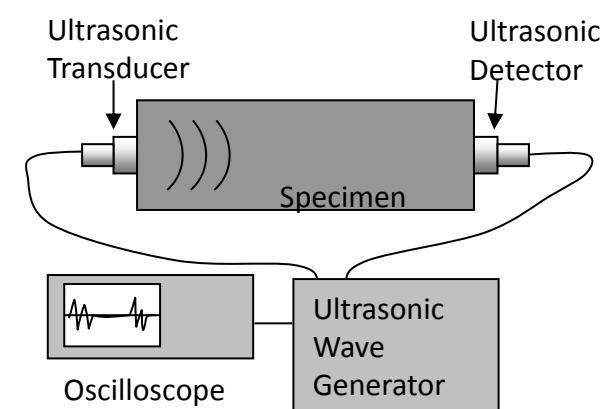
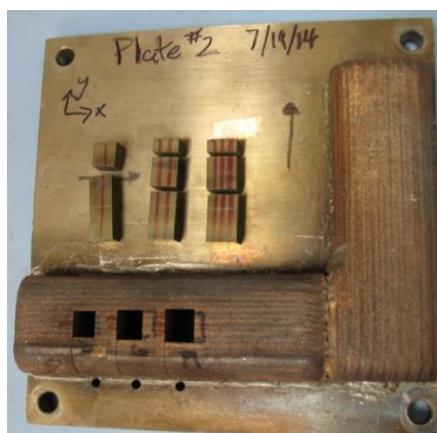
# Wave speeds in wrought and LENS cubes indicate anisotropy in LENS material.



- Measure shear wave speed,  $C_s$
- Measure dilatational wave speed,  $C_d$
- Measure density,  $\rho$

Material	Direction	Density (kg/m <sup>3</sup> )	Shearmod (GPa)	Poisson's Ratio	Elastic Modulus (GPa)
Wrought B	X (axial)	7854.5	<b>77.8</b>	<b>0.29</b>	<b>201.3</b>
Wrought B	Y (trans)		<b>77.6</b>	<b>0.29</b>	<b>200.5</b>
Wrought B	Z (trans)		<b>77.8</b>	<b>0.29</b>	<b>201.0</b>
LENS X	X	7842.9	<b>86.6</b>	<b>0.24</b>	<b>215.5</b>
LENS X	Y		<b>89.6</b>	<b>0.26</b>	<b>225.7</b>
LENS X	Z		<b>70.5</b>	<b>0.33</b>	<b>187.6</b>

99.85 % dense



$$C_s = \sqrt{\frac{\mu}{\rho}}$$

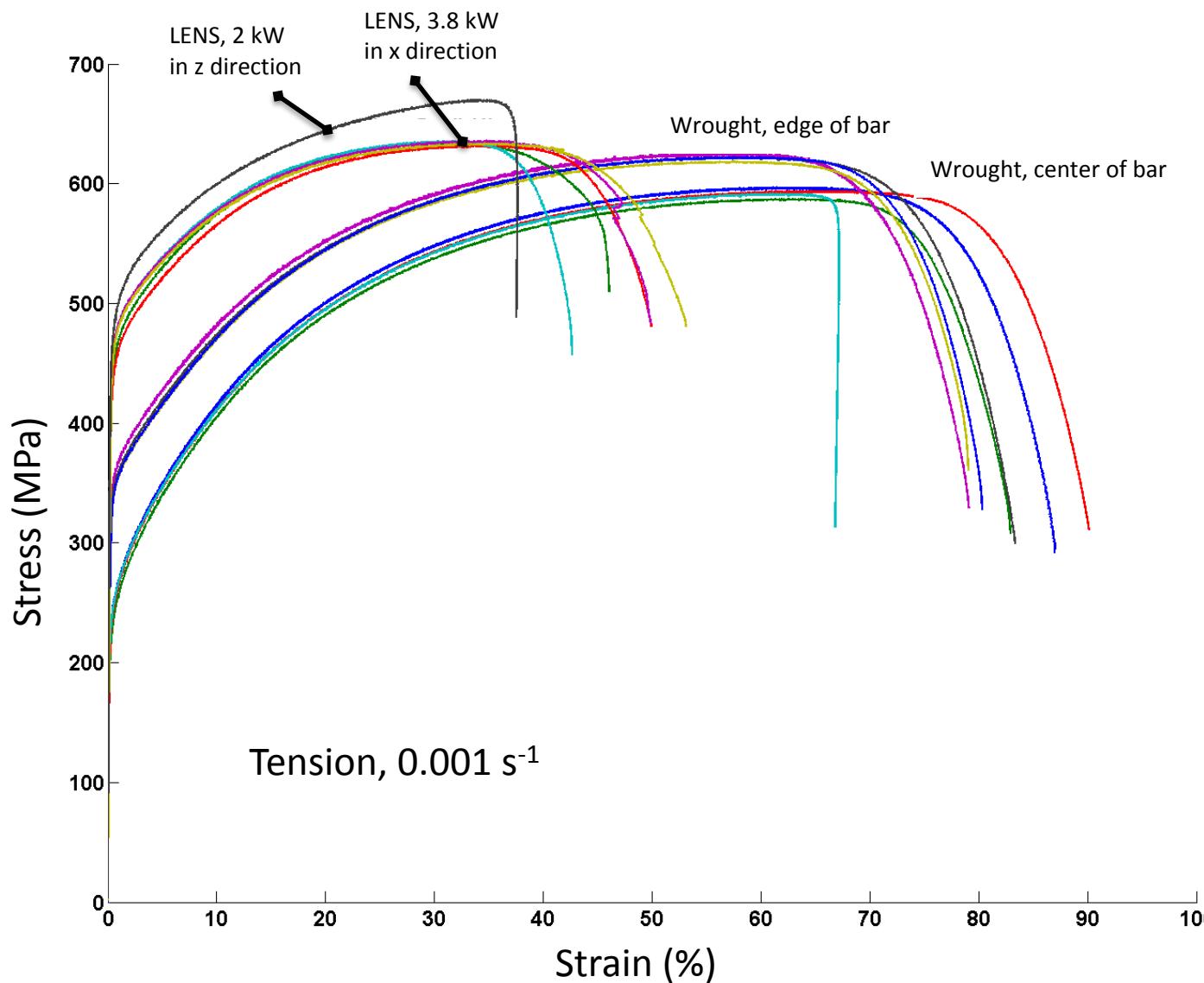
$$\mu = C_s^2 \rho$$

$$C_d^{pl-\varepsilon} = \sqrt{\frac{2(1-\nu)\mu}{(1-2\nu)\rho}}$$

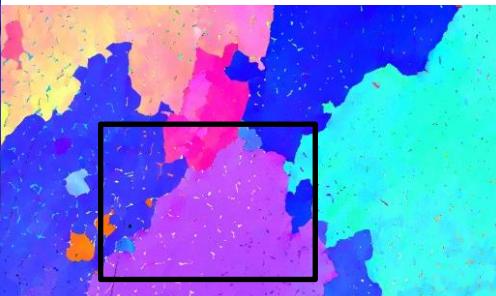
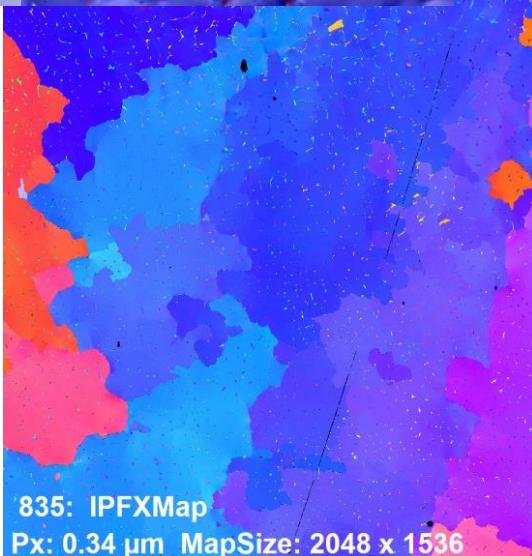
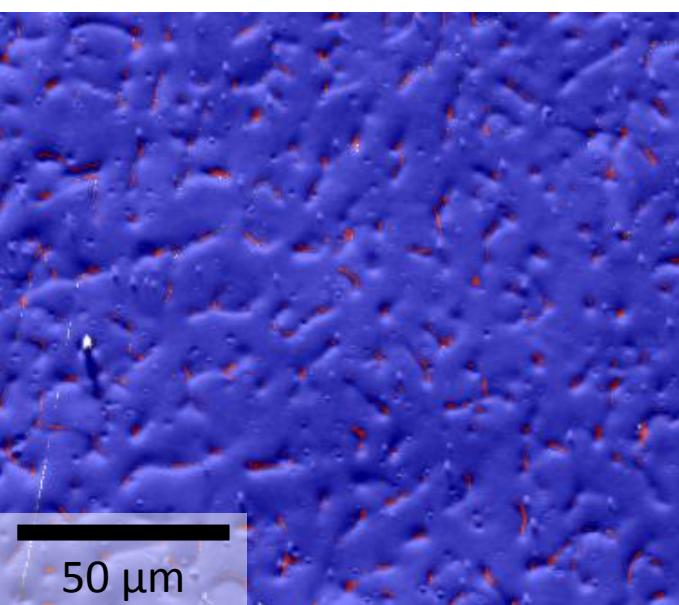
$$\nu = \frac{\frac{1}{2} \left( \frac{C_d}{C_s} \right)^2 - 1}{\left( \frac{C_d}{C_s} \right)^2 - 1}$$

$$E = 2\mu(1+\nu)$$

# LENS material is significantly stronger than wrought, contrary to the Hall-Petch expectation based on grain size.

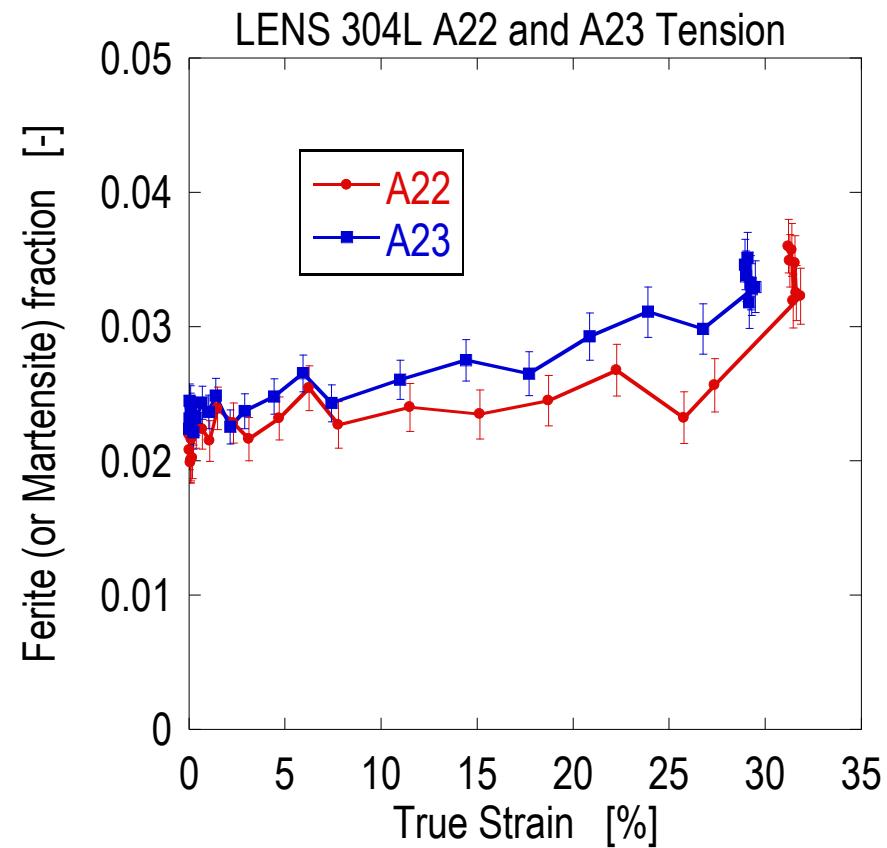
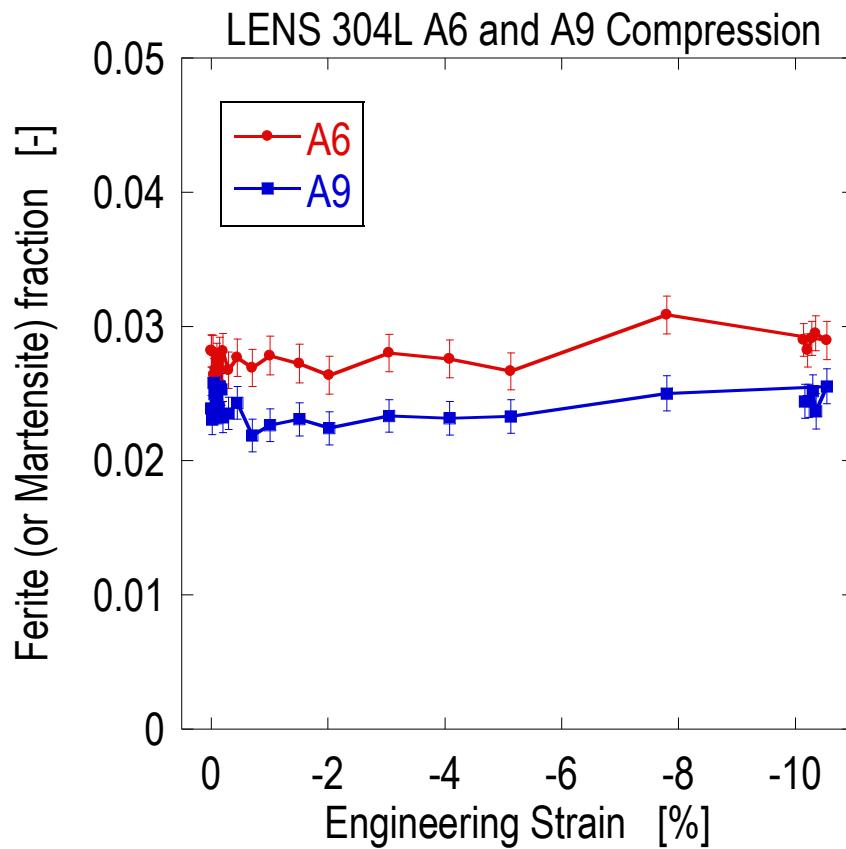


# Hall-Petch is not limited to grain size. Small ferrite islands could be responsible for hardening.

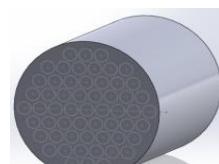
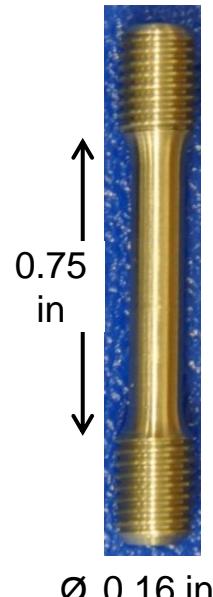


- Small ferrite islands
- Subgrains and grain substructure associated with geometrically necessary dislocations.
- Initial BCC phase: 1.2% for Wrought and 2.3% for LENS (ferritescope)
- Ferrite content appears to increase slightly with loading (~3%)

# Ferrite content in LENS samples may increase slightly with tensile loading (Neutron Diffraction at LANL)



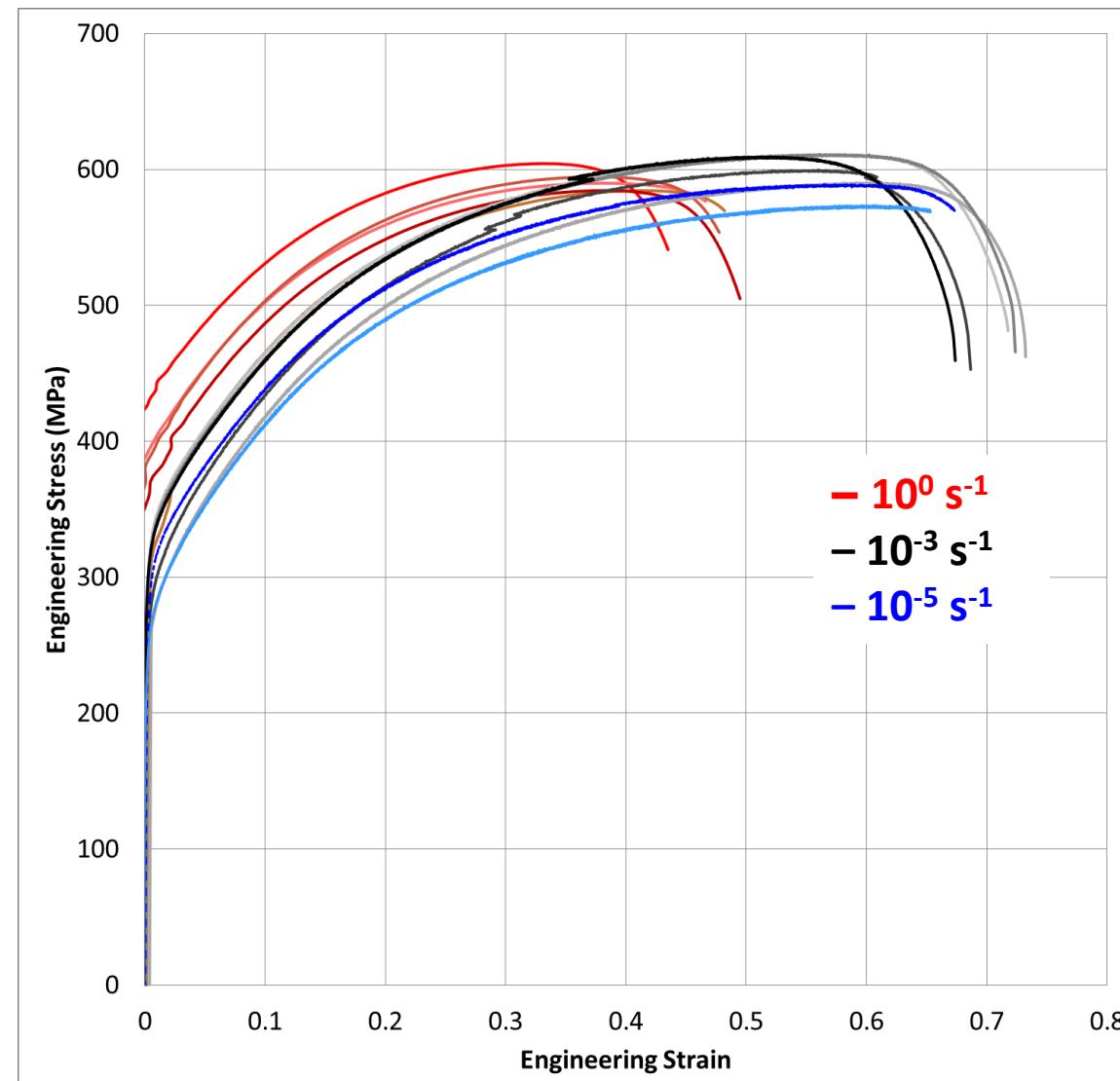
# Quasistatic tension on wrought SS304L exhibit some moderate strain rate dependence.



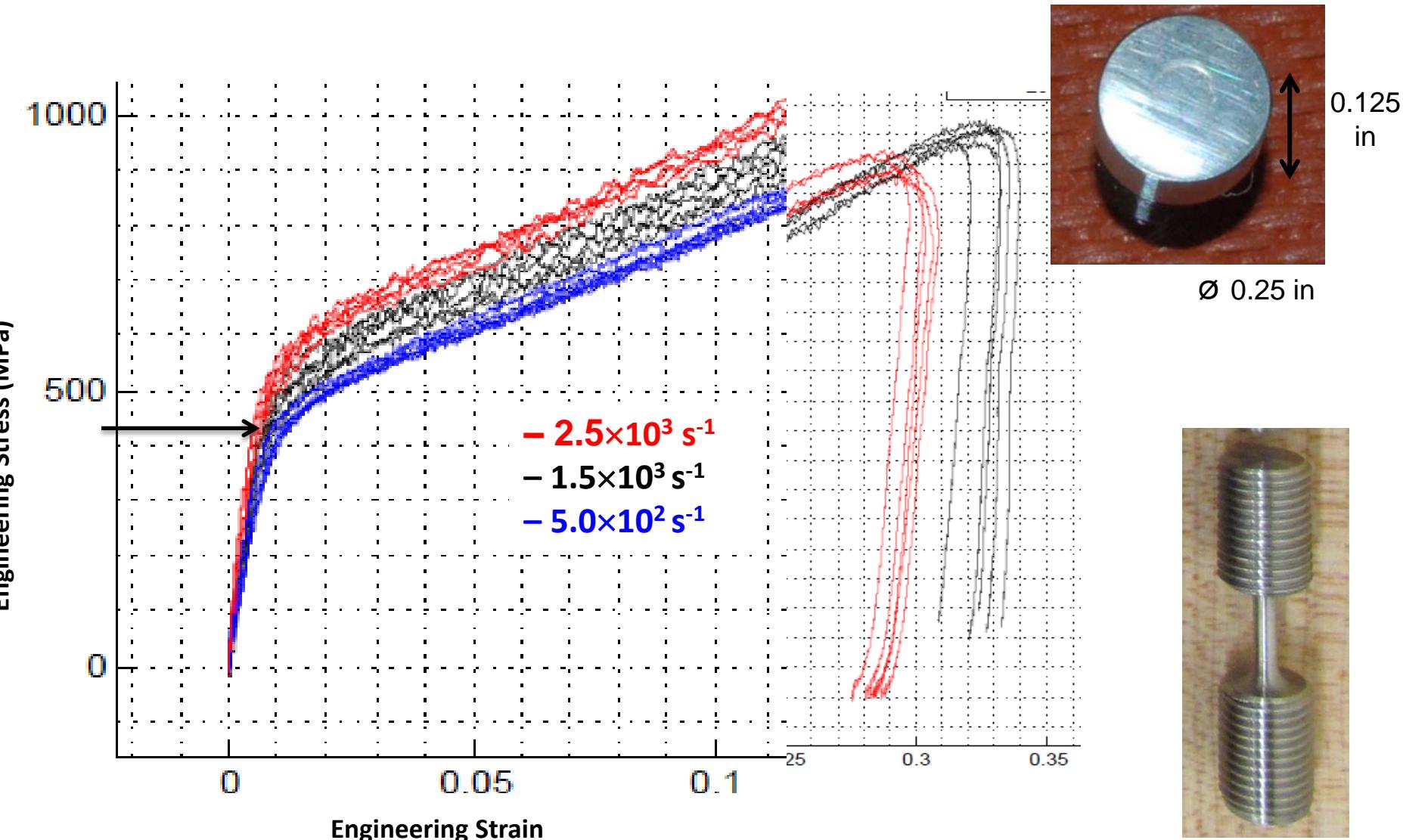
Longitudinal



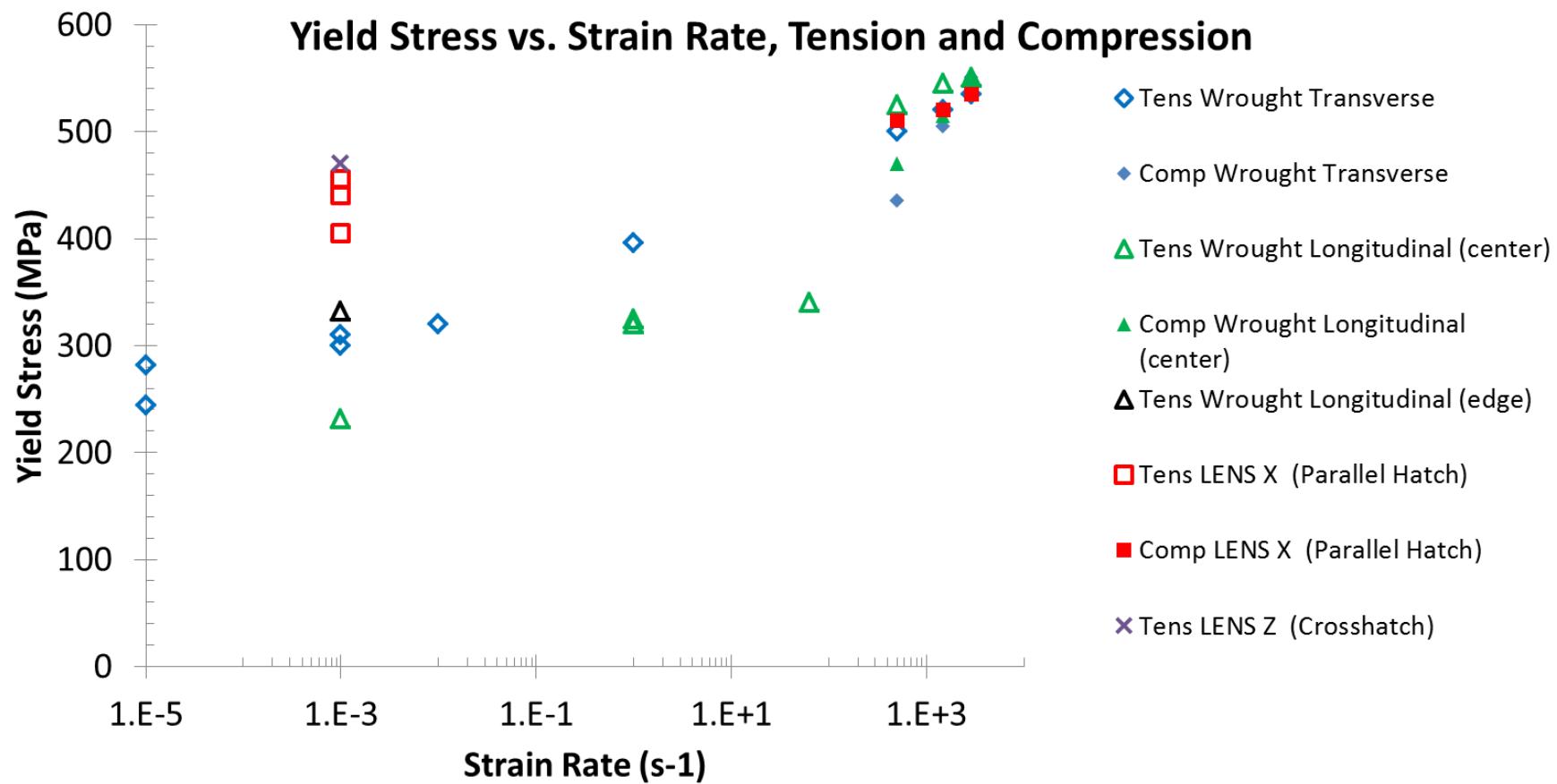
Transverse



# Dynamic compression on conventional SS304L exhibit some moderate strain rate dependence.



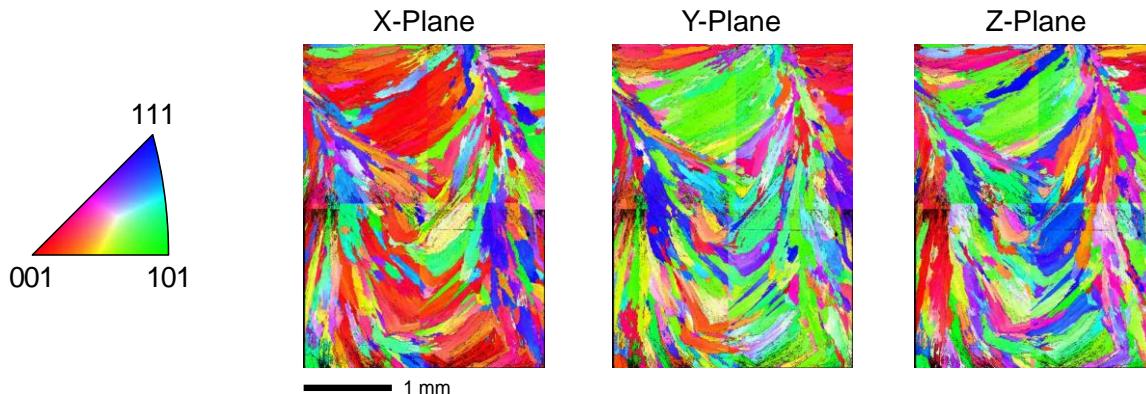
# Strain rate effects of wrought and AM 304L in tension.



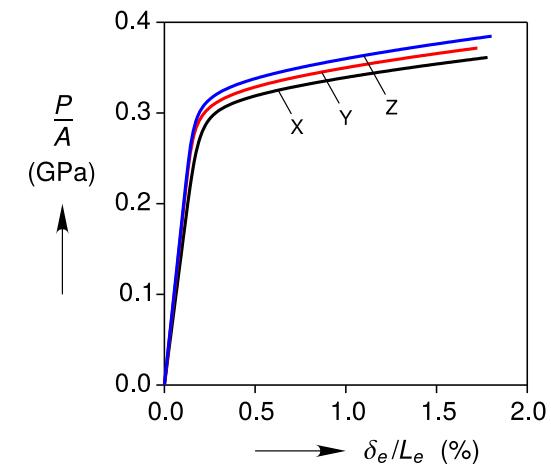
- LENS material appears to be less strain rate dependent.

# Preliminary Texture Study

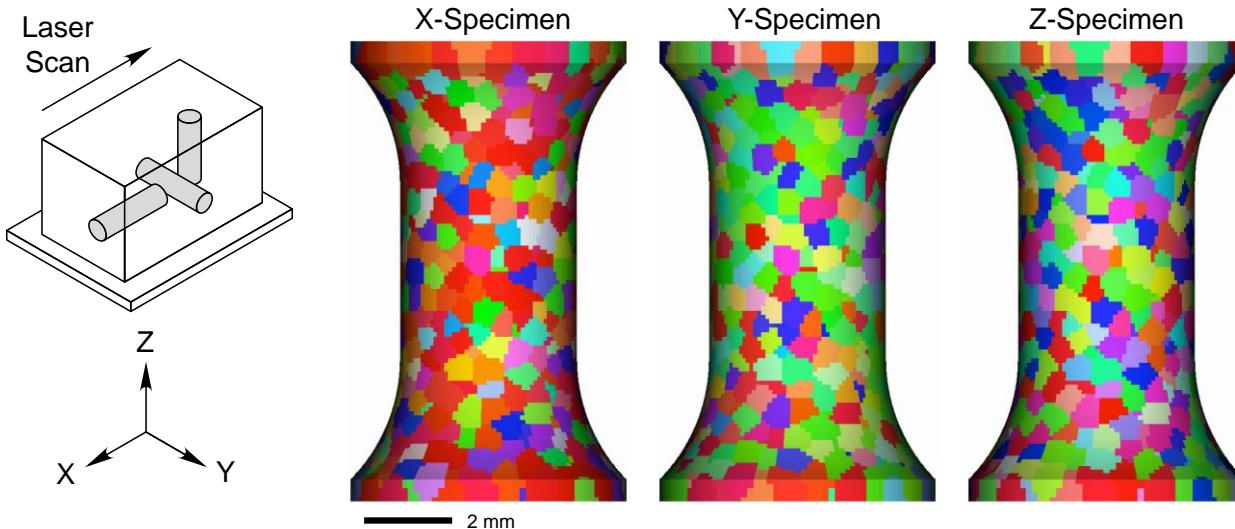
## EBSD Orientation Maps



## Mechanical Responses

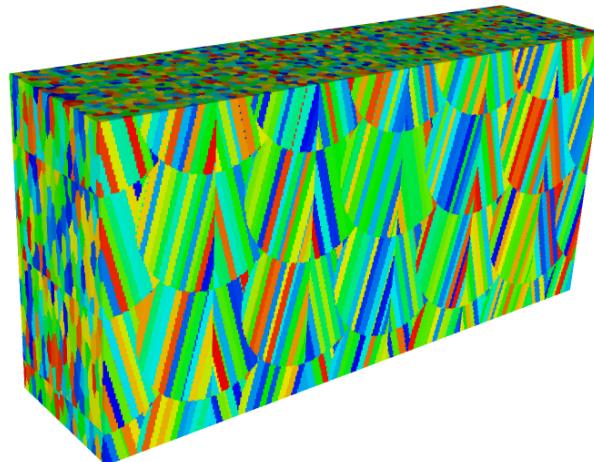


## Tensile Specimens

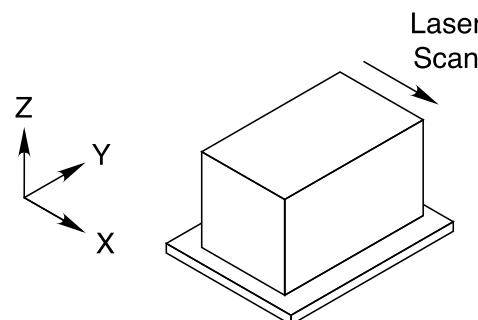


# Modeling effects of grain morphology and orientation on mechanical behavior.

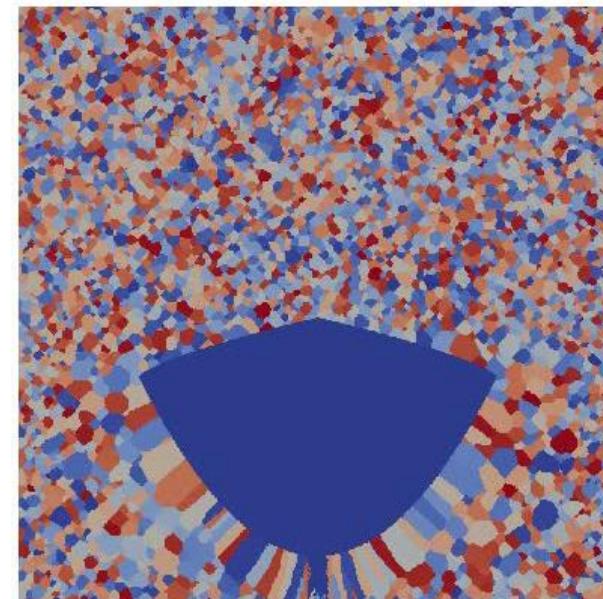
Initial Attempt:  
Voronoi Tessellation



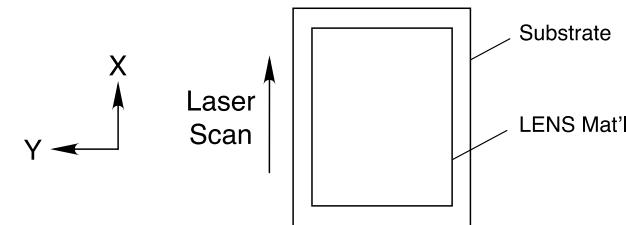
bead size = 1 mm  
grain size = 40 microns



Future Direction:  
Grain Growth

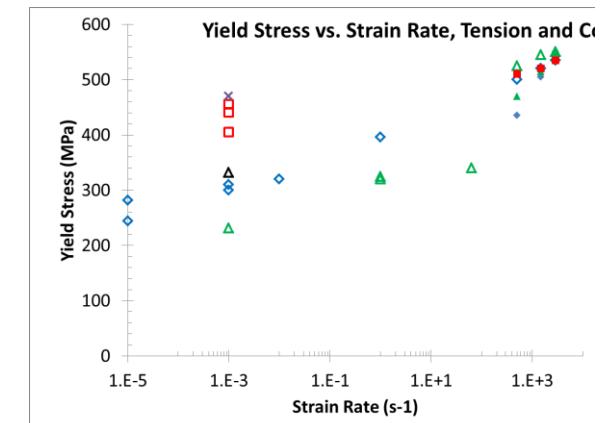
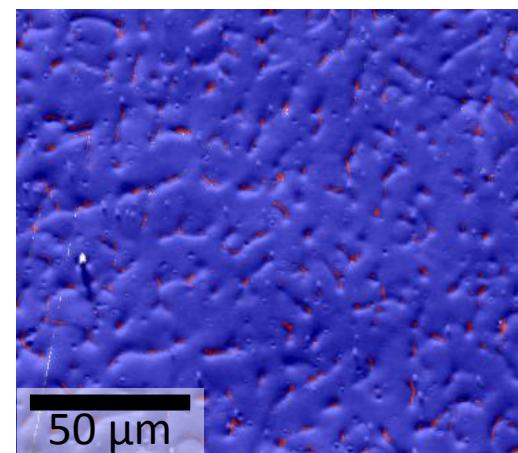
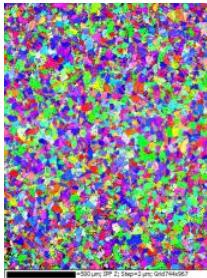


Video courtesy of Veena Tikare (Org. 1444)  
and John Madison (Org. 1814)



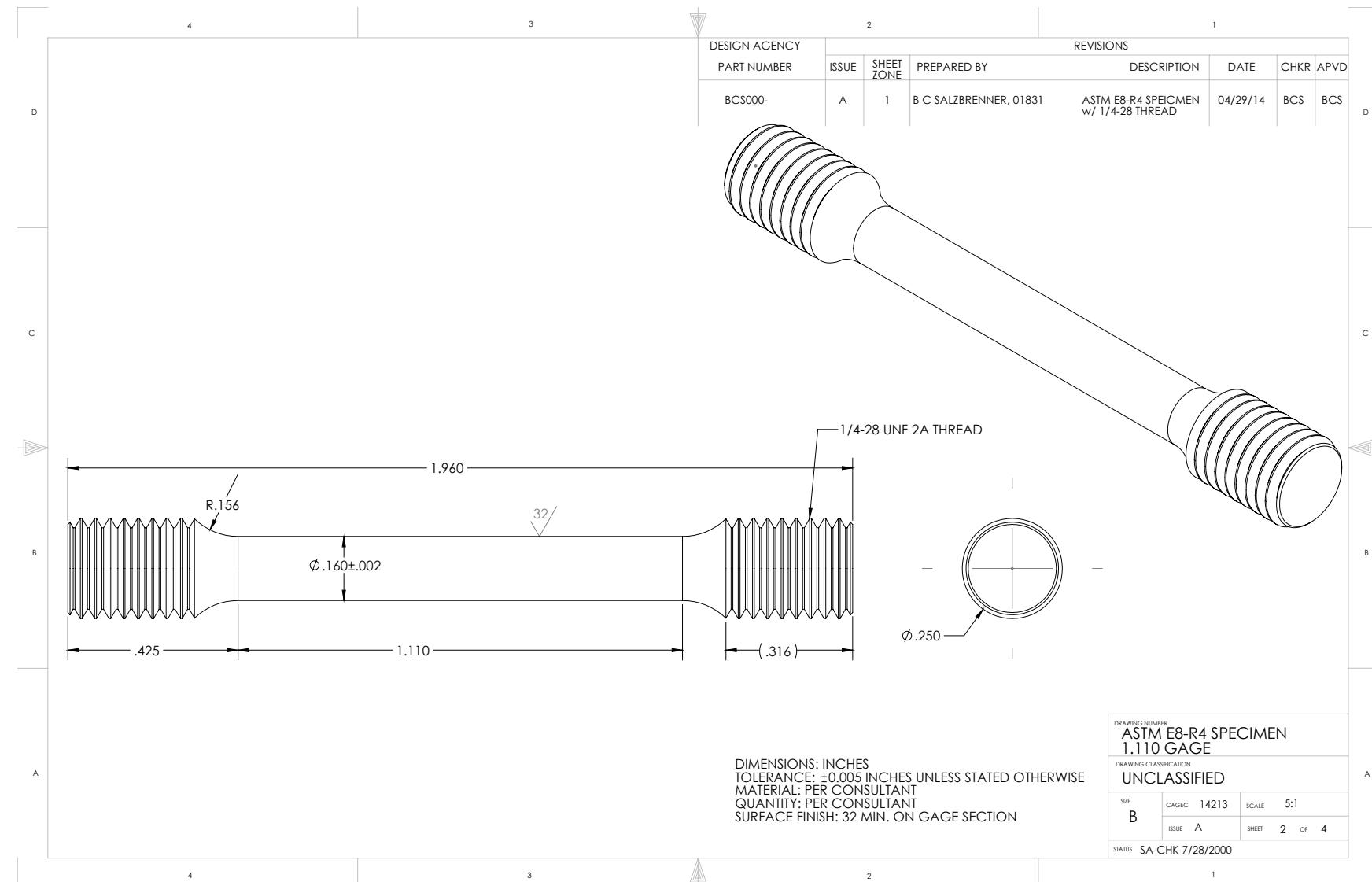
# Conclusions

1. Microstructure in LENS-like 304L is considerably different from conventional 304L.
2. LENS 304L is stronger despite larger grain size.
  - Ferrite islands at micron scale are likely responsible.
3. Strain rate dependence observed.

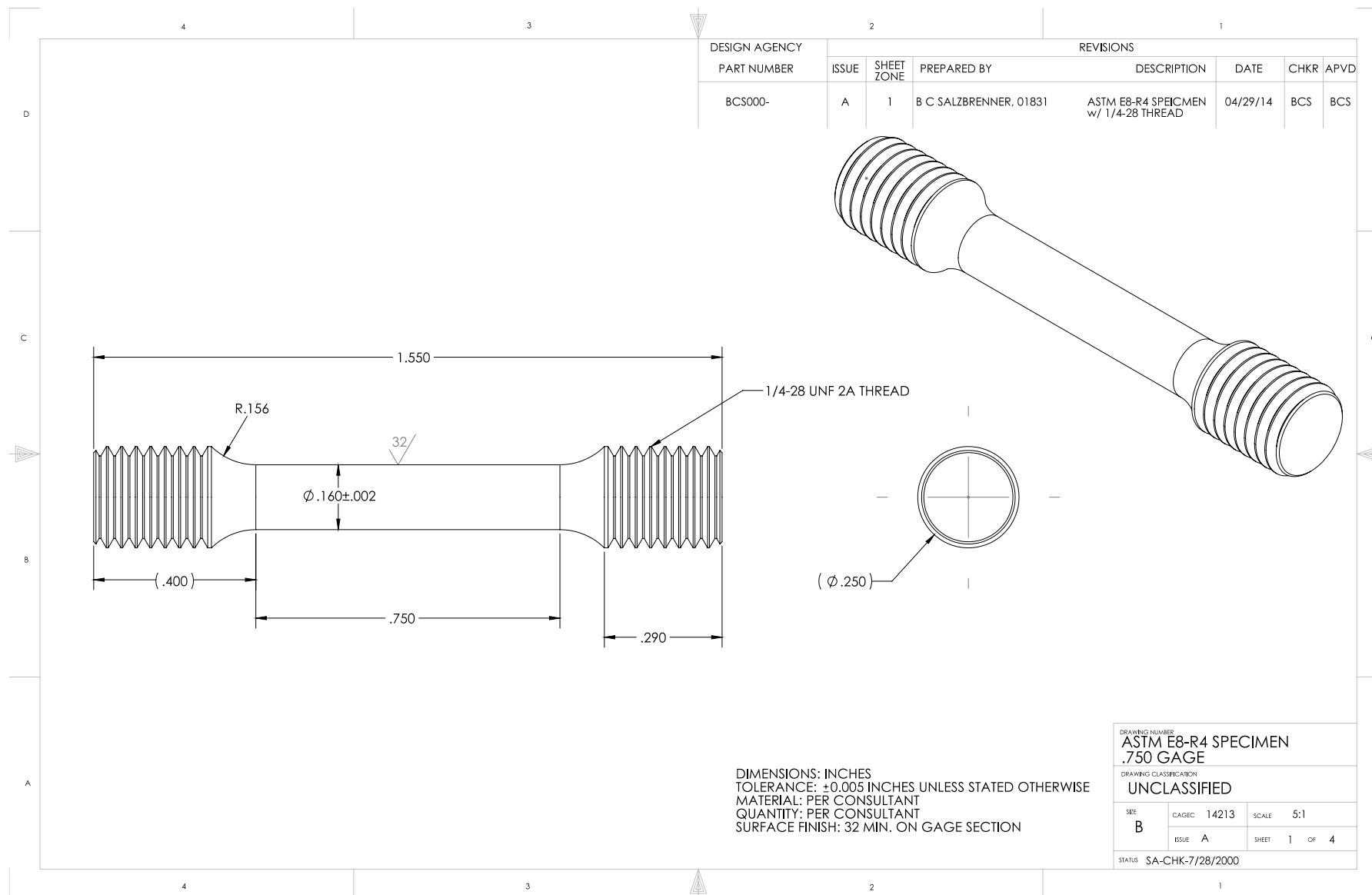


# Extra Slides

# Tensile samples for testing (quasi-static)

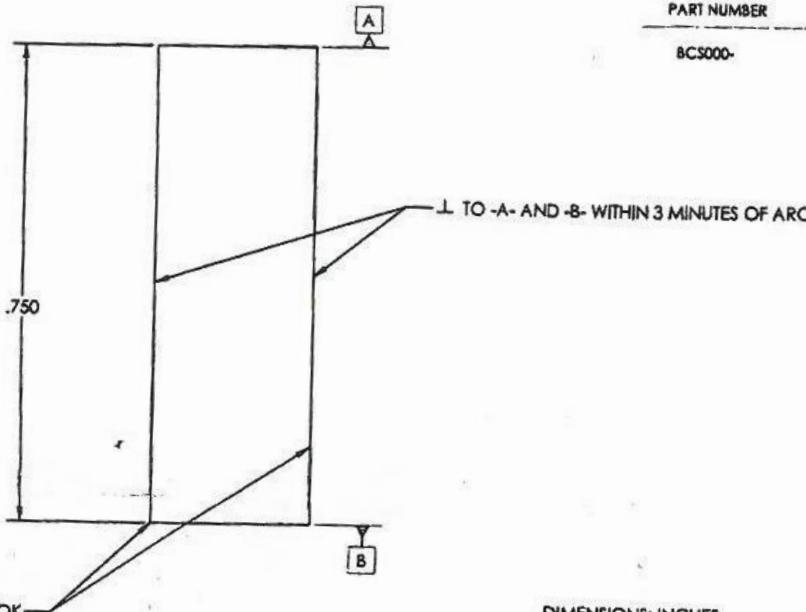


# Tensile samples for testing (quasi-static)

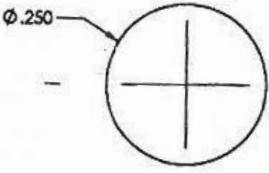


# Tensile samples for testing (quasi-static, compression)

DESIGN AGENCY			REVISIONS				
PART NUMBER	ISSUE	SHEET ZONE	PREPARED BY	DESCRIPTION	DATE	CHKR	APVD
BCS000-	A	1	B C SALZBRENNER, 01831	COMPRESSION DISK	04/29/14	BCS	BCS



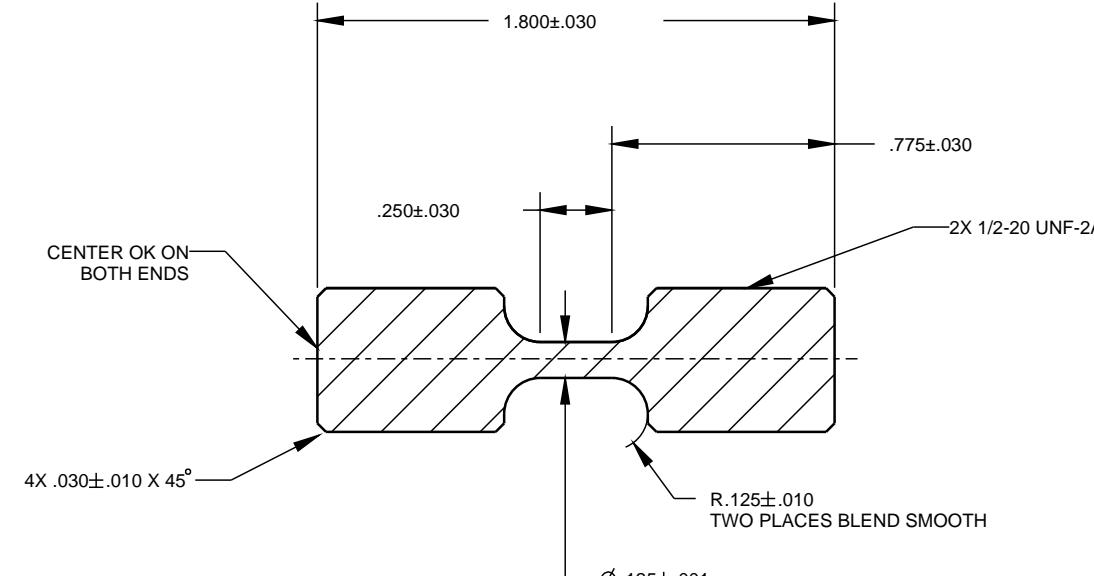
**DIMENSIONS: INCHES**  
**TOLERANCE:  $\pm 0.002$  INCHES UNLESS STATED OTHERWISE**  
**MATERIAL: PER CONSULTANT**  
**QUANTITY: PER CONSULTANT**  
**SURFACE FINISH: 32 MIN.**  
**-A- PARALLEL TO -B- WITHIN 0.0005**

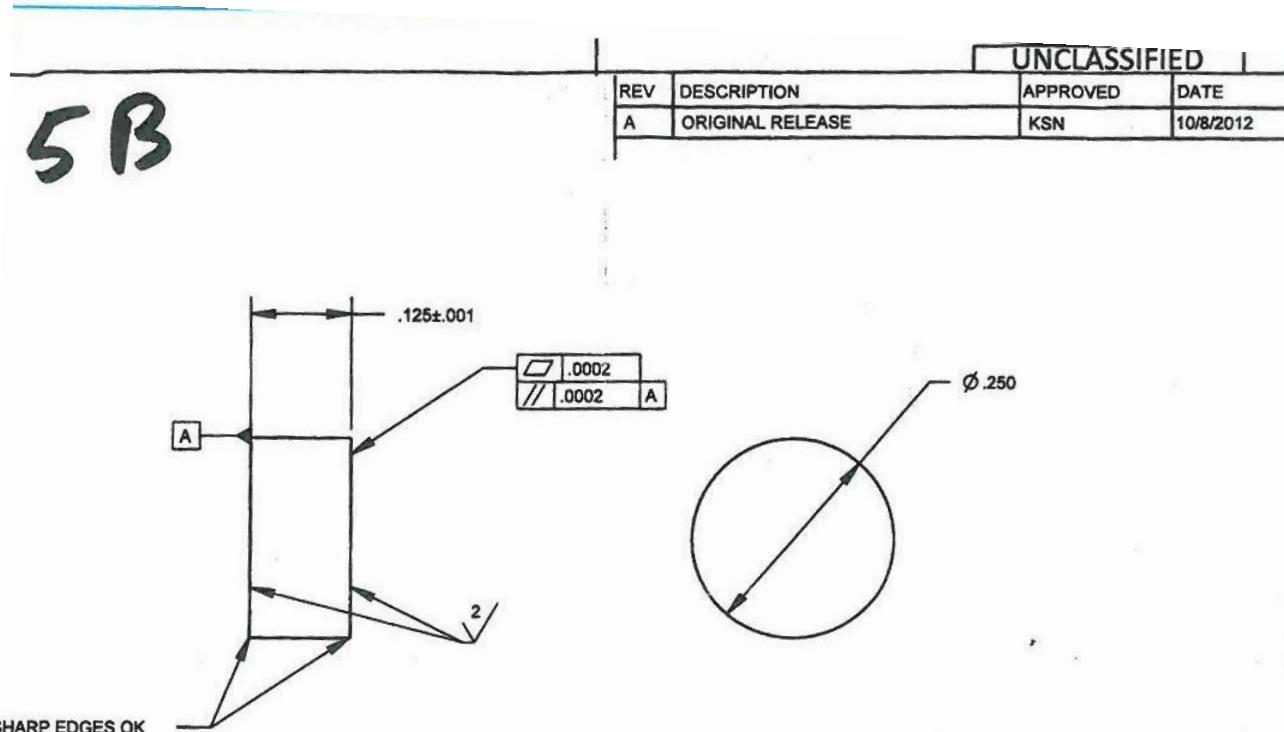
DRAWING NUMBER: **COMPRESSION DISK**  
 DRAWING CLASSIFICATION: **UNCLASSIFIED**  
 DATE: **SA-CHX-7/28/2000**

IN CAD/CAM 14213 SCALE 6:1  
 B SIZE A SHEET 4 OF 4

# Tensile samples for testing (Hopkinson)

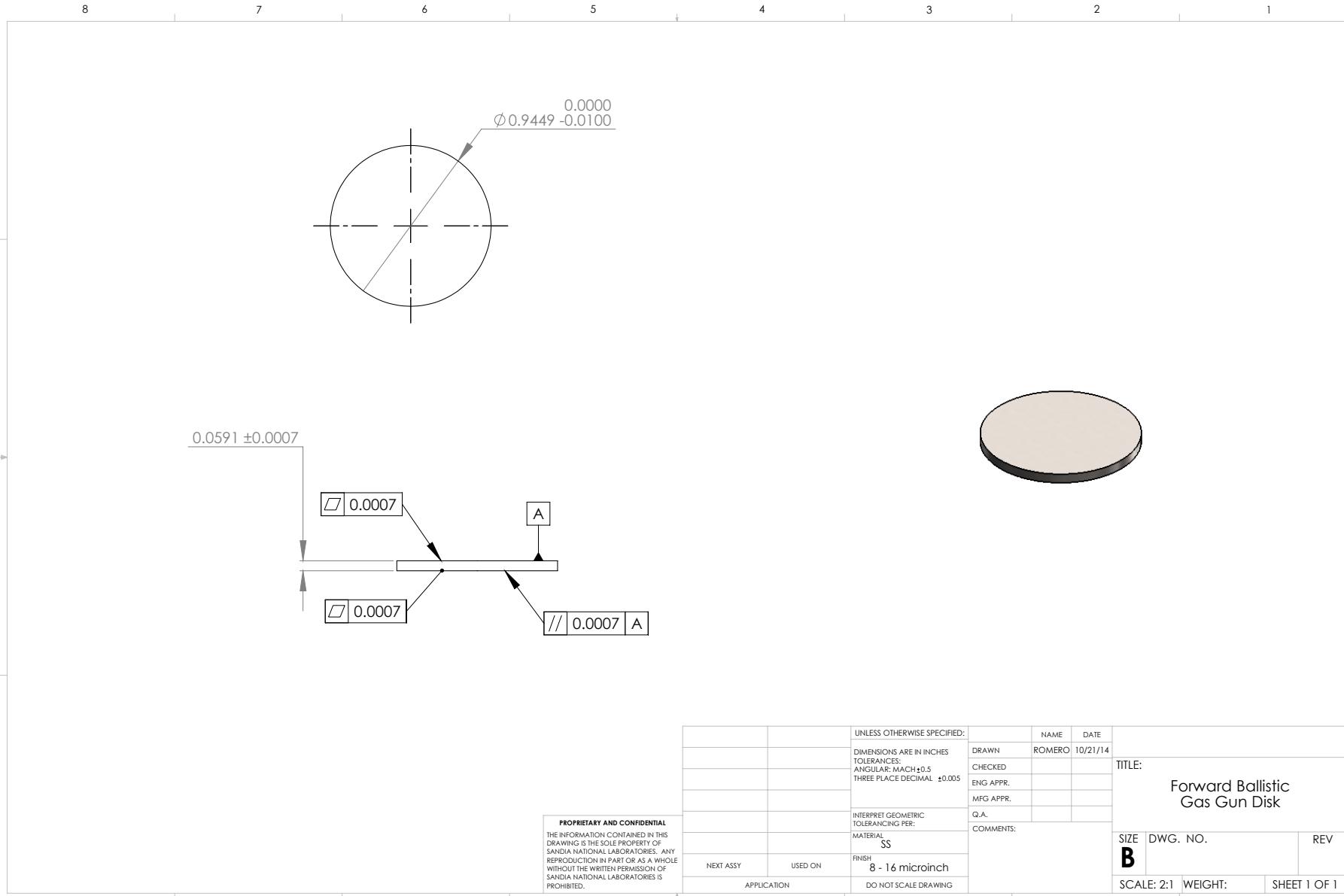
UNCLASSIFIED											
REV	DESCRIPTION	APPROVED	DATE								
A	ORIGINAL RELEASE	KSN	12/13/2013								
											
<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 50%; padding: 5px;">TOLERANCES UNLESS OTHERWISE SPECIFIED  X.X ± 0.03      <math>\angle \pm 0.5^\circ</math> X.XX ± 0.01 X.XXX ± 0.005  ALL DIMENSIONS ARE IN INCHES REMOVE ALL BURRS AND SHARP EDGES 0.005R OR CHAMFER MAX</td> <td style="width: 50%; padding: 5px; text-align: center;">63 ✓  SANDIA NATIONAL LABORATORIES  TITLE 1/8" TENSILE SPECIMEN 1/2" -20 UNF THREADS</td> </tr> <tr> <td style="width: 50%; padding: 5px;">MATERIAL</td> <td style="width: 50%; padding: 5px; text-align: center;">SIZE A</td> </tr> <tr> <td style="width: 50%; padding: 5px;">FINISH</td> <td style="width: 50%; padding: 5px; text-align: center;">Dwg. No. 1069_TENSILE_MOD</td> </tr> <tr> <td style="width: 50%; padding: 5px;">AS MACHINED</td> <td style="width: 50%; padding: 5px; text-align: center;">QUANTITY SCALE 2/1</td> </tr> </table>				TOLERANCES UNLESS OTHERWISE SPECIFIED  X.X ± 0.03 $\angle \pm 0.5^\circ$ X.XX ± 0.01 X.XXX ± 0.005  ALL DIMENSIONS ARE IN INCHES REMOVE ALL BURRS AND SHARP EDGES 0.005R OR CHAMFER MAX	63 ✓  SANDIA NATIONAL LABORATORIES  TITLE 1/8" TENSILE SPECIMEN 1/2" -20 UNF THREADS	MATERIAL	SIZE A	FINISH	Dwg. No. 1069_TENSILE_MOD	AS MACHINED	QUANTITY SCALE 2/1
TOLERANCES UNLESS OTHERWISE SPECIFIED  X.X ± 0.03 $\angle \pm 0.5^\circ$ X.XX ± 0.01 X.XXX ± 0.005  ALL DIMENSIONS ARE IN INCHES REMOVE ALL BURRS AND SHARP EDGES 0.005R OR CHAMFER MAX	63 ✓  SANDIA NATIONAL LABORATORIES  TITLE 1/8" TENSILE SPECIMEN 1/2" -20 UNF THREADS										
MATERIAL	SIZE A										
FINISH	Dwg. No. 1069_TENSILE_MOD										
AS MACHINED	QUANTITY SCALE 2/1										

# Tensile samples for testing (Hopkinson, compression)

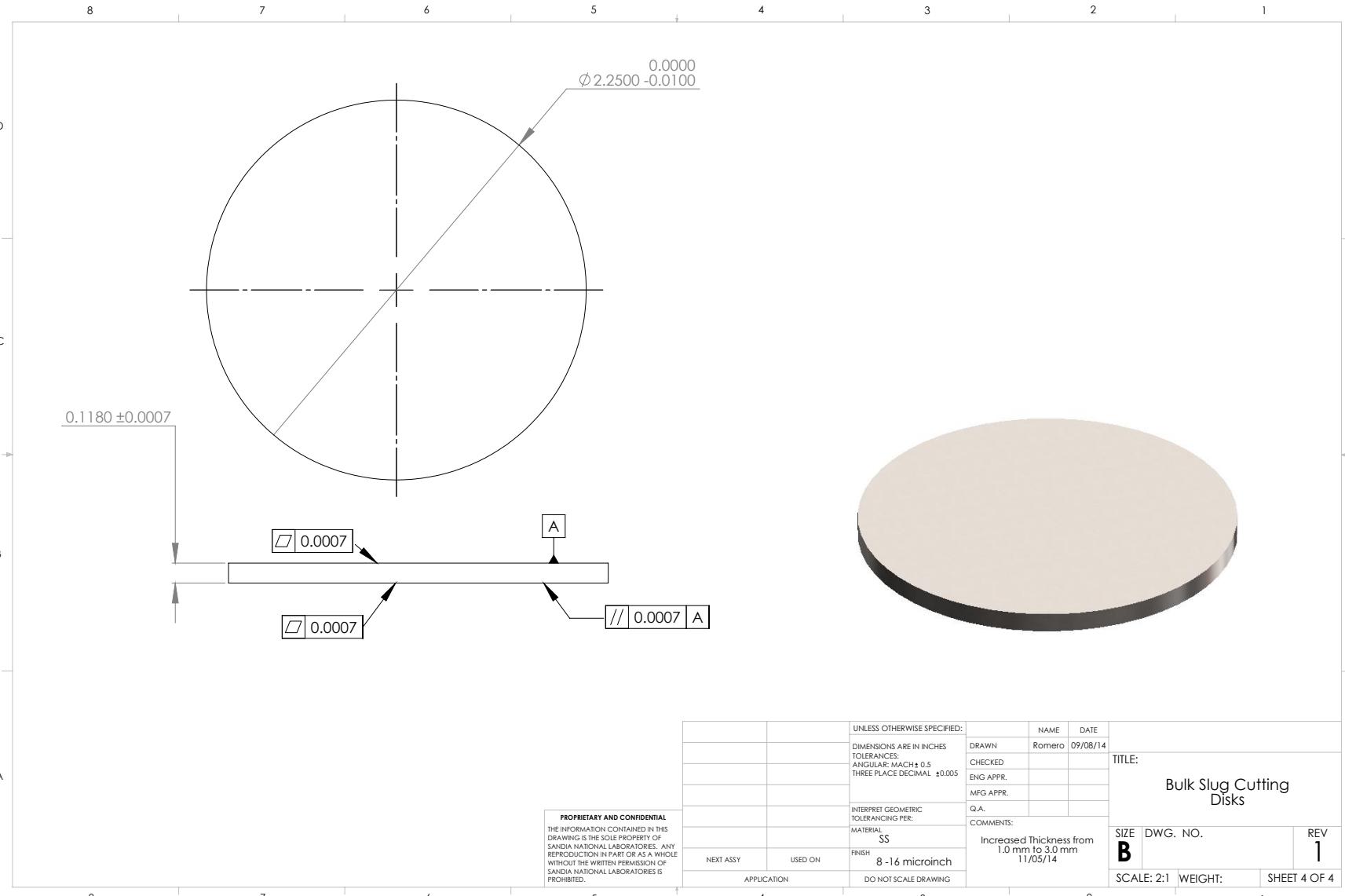


TOLERANCES UNLESS OTHERWISE SPECIFIED		SANDIA NATIONAL LABORATORIES	
XX ± 0.03      < ± 0.5° XXX ± 0.01      ✓ XXXX ± 0.005		TITLE SS 304L 1/4" COPPER SPECIMEN	
ALL DIMENSIONS ARE IN INCHES REMOVE ALL BURRS AND SHARP EDGES 0.005R OR CHAMFER MAX		MATERIAL COPPER SS 304L	
FINISH AS GROUND		SIZE A	DWG. NO. 1022_COPPER_PLATEN
		QUANTITY 50	SCALE 6/1

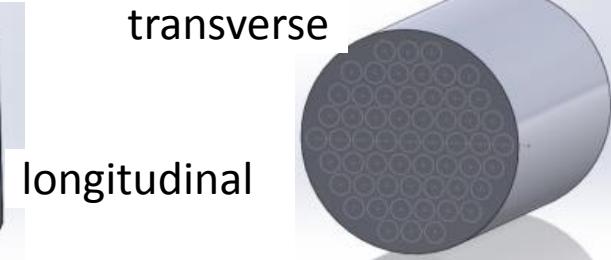
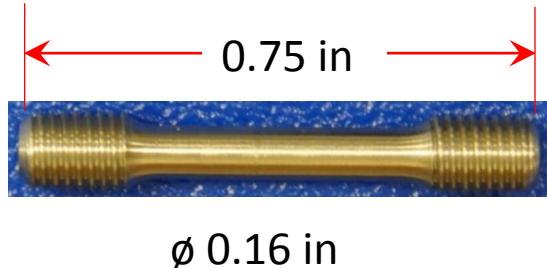
# Tensile samples for gas gun testing (forward ballistic)



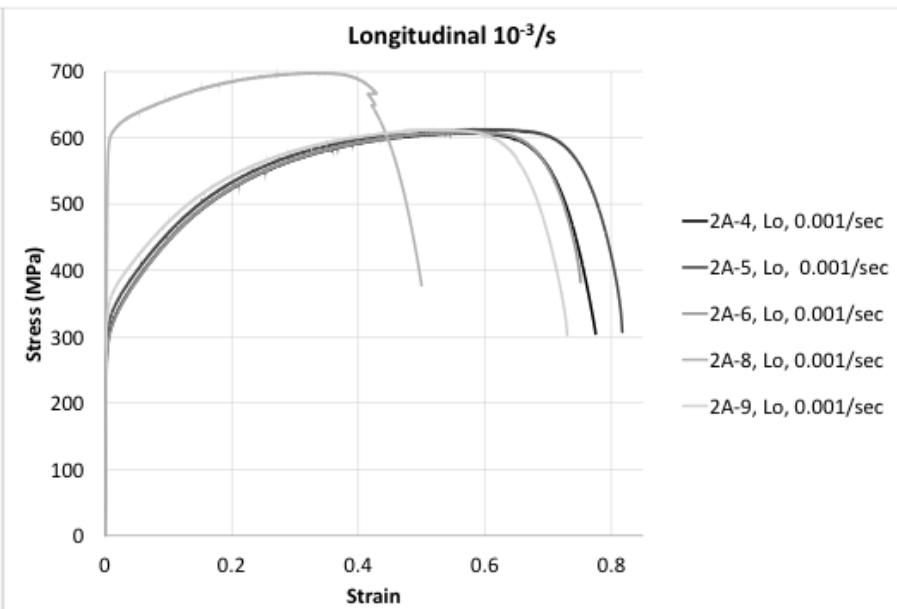
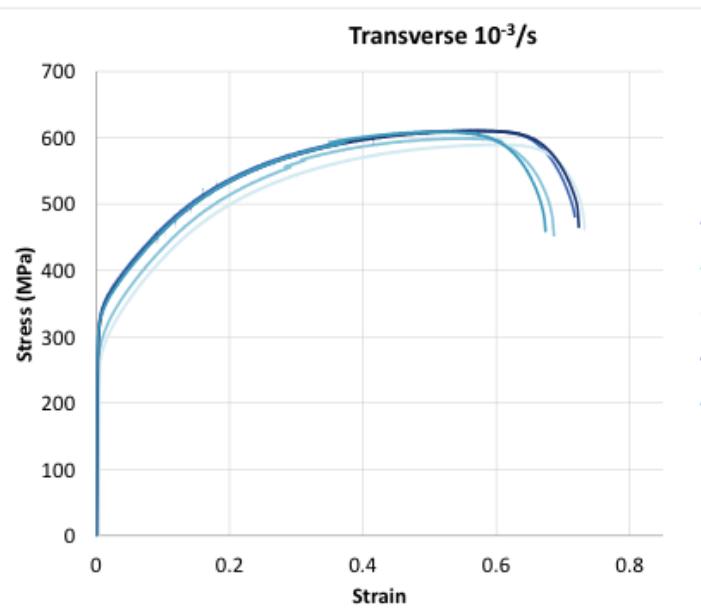
# Tensile samples for gas gun testing (reverse ballistic)



## Quasistatic mechanical tests on wrought 304L SS

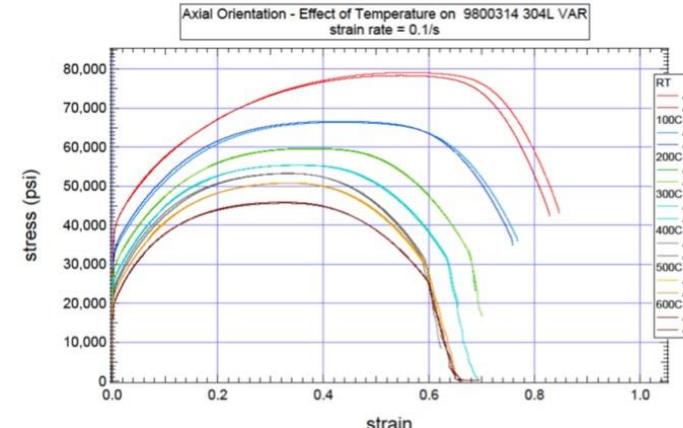
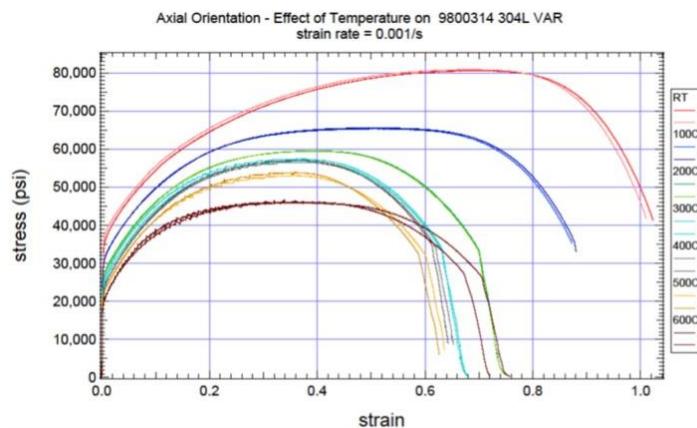


### Stress-strain curves



# Temperature and strain rate dependence of 304L

Antoun (Sandia)



Lichtenfield et al. 2006

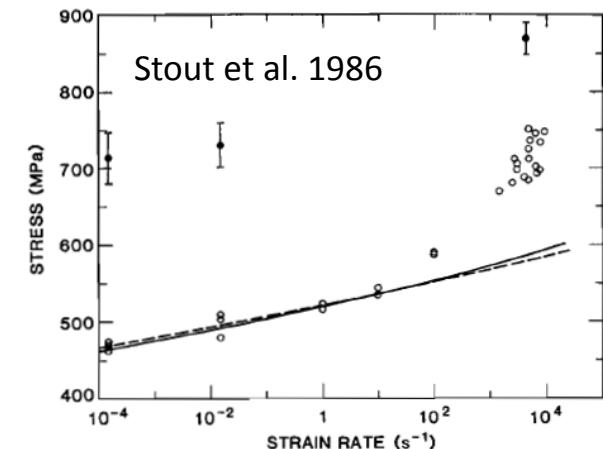
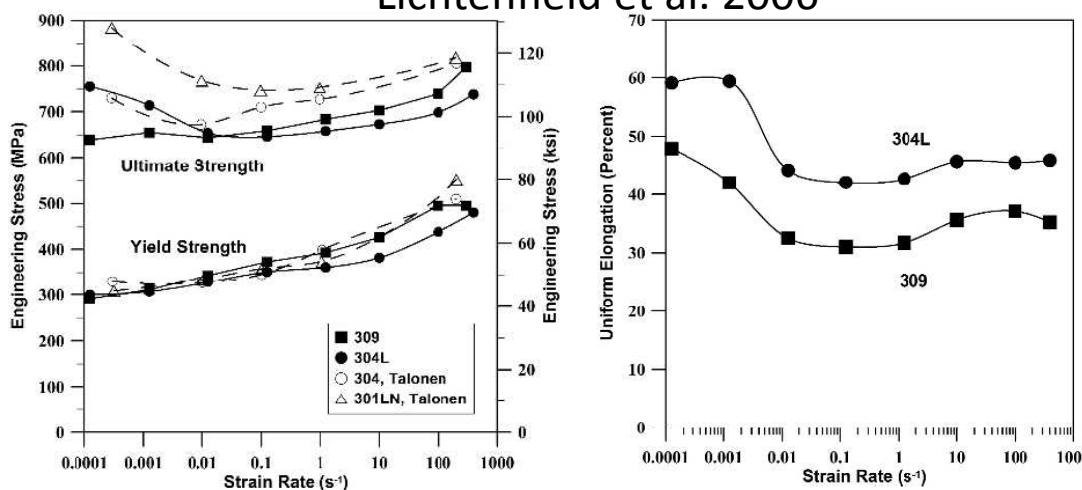


Fig. 13 Comparison of the flow stress values (circles) with equation (14) (solid line) and the power law, equation (7) (dashed line), with  $Q = 522$  MPa and  $m = 0.0123$ . Also included in this plot are the measured mechanical threshold stress values (solid circles with error bars).

Fig. 5—Var  
for 309 and

- Temperature has a significant effect on strength and ductility.
- Higher strain rate has little effect on strength, but a noticeable effect on ductility.