

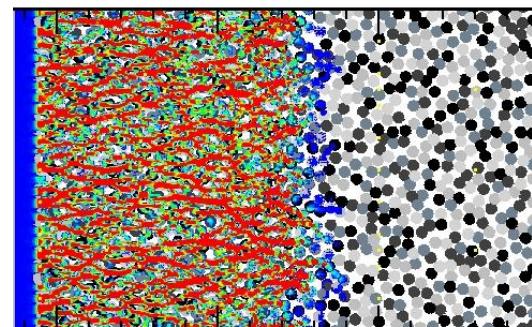
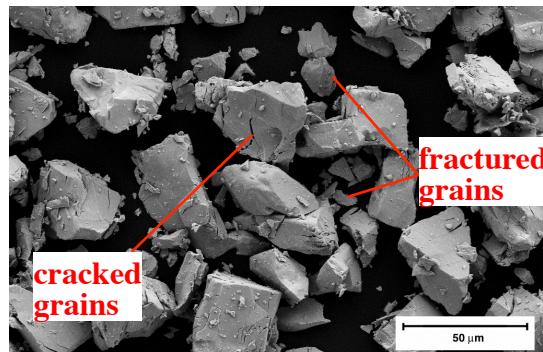
Dynamic Behavior of Granular Materials



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December 9, 2014



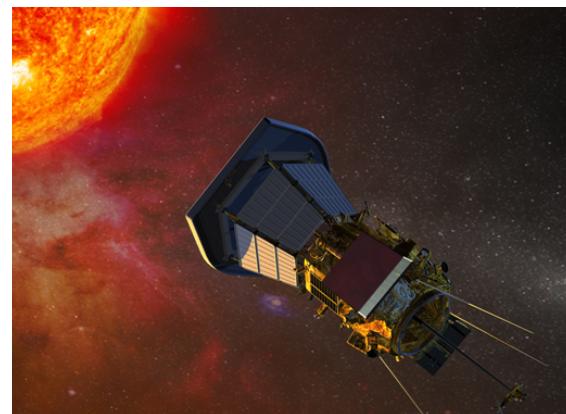


- **Introduction to Shock and High-Pressure Physics**
- **Introduction to Granular Materials**
- **Compaction and Scaling Properties of Waves**
- **High Pressure EOS – Experiments and DFT Modeling**
- **The Intermediate Regime – Porosity Enhanced Densification**
- **Closure and Acknowledgements**

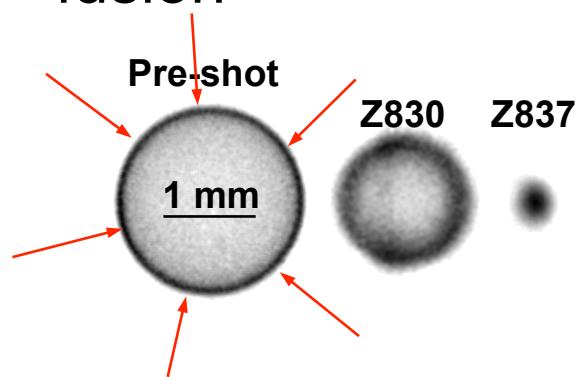


Why Do We Need To Know the Behavior of Materials Under Extreme Conditions?

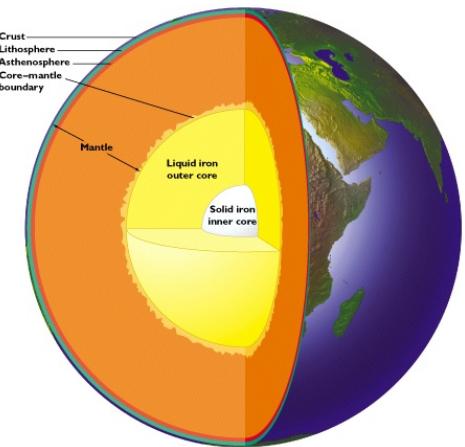
- weapons applications (warheads, armor, etc.)
- explosives behavior and applications



- inertial confinement fusion



- solar probe
 - $100 \mu\text{m}$ particles
 - up to 300 km/s velocities
 - $P_{\max} \sim 100 \text{ TPa}$, $T_{\max} \sim 10^6 \text{ K}$

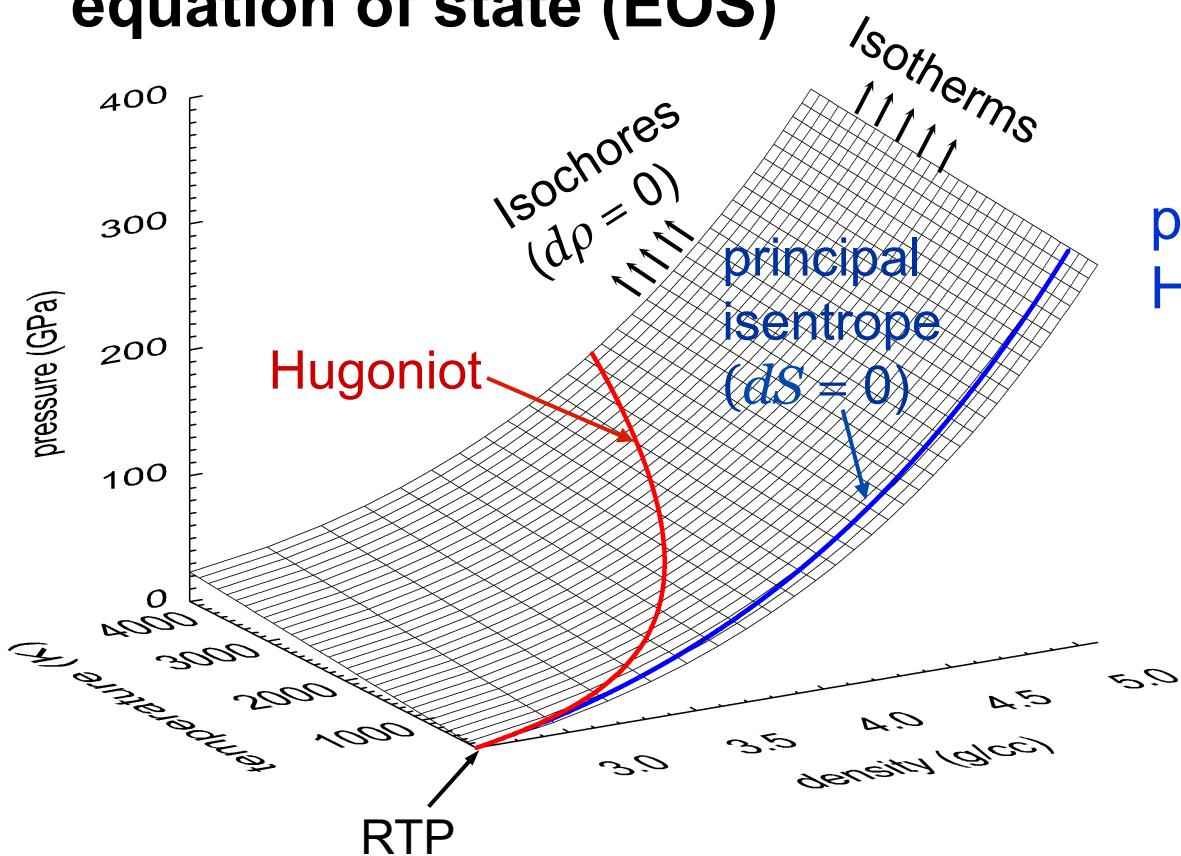


- planetary science ($P \sim 360 \text{ GPa}$, $T \sim 7000 \text{ K}$)



Material Behavior: EOS & Constitutive Aspects

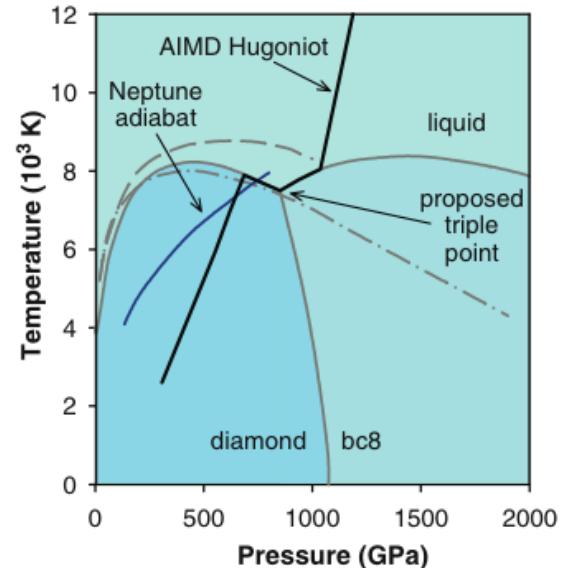
equation of state (EOS)



one thermodynamic state variable as a function of two others:

$$\text{pressure } P = P(\rho, T)$$

$$\text{Helmholtz energy } f = f(v, T)$$



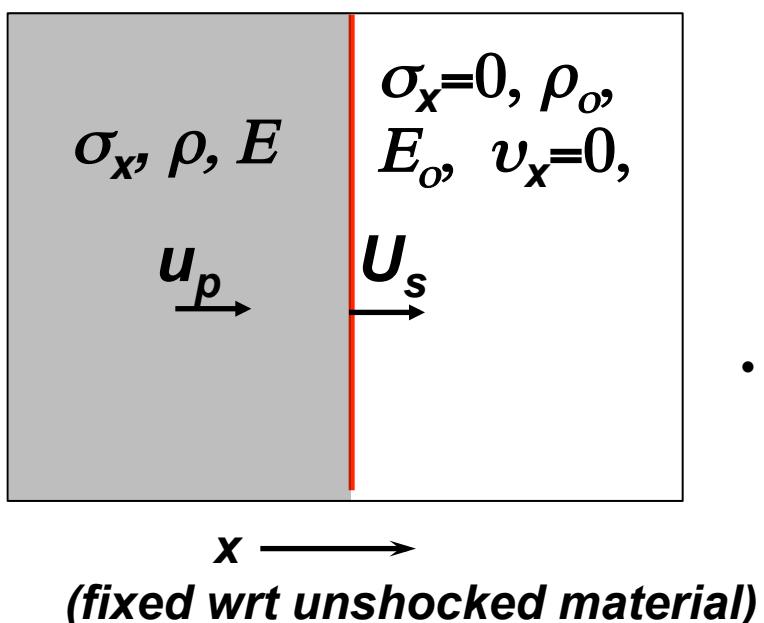
**Also: strength, damage, spall
(tensile failure), compaction**

Knudson, M. D., M. P. Desjarlais and D. H. Dolan (2008). "Shock-wave exploration of the high-pressure phases of carbon." *Science* 322: 1822-1825.



What is a Shock Wave?

- A “discontinuous” wave that moves at a fixed velocity (if steady)
 - wave front moves at speed U_s (*shock velocity*)
 - shocked material moves at speed u_p (*particle or mass velocity*)
 - uniaxial strain condition ($\varepsilon_y = \varepsilon_z = \varepsilon_{xy} = \varepsilon_{yz} = \varepsilon_{xz} = 0$)
- **shocked material** **unshocked material**
 - States ahead and behind shock assumed to be in thermodynamic equilibrium
 - well defined temperature in each state
 - described by equilibrium thermodynamics
 - Shock compression is adiabatic
 - very fast process (< 1 ns)
 - irreversible (i.e. NOT isentropic)
 - temperature *typically* increases





Conservation Equations and the Shock Hugoniot

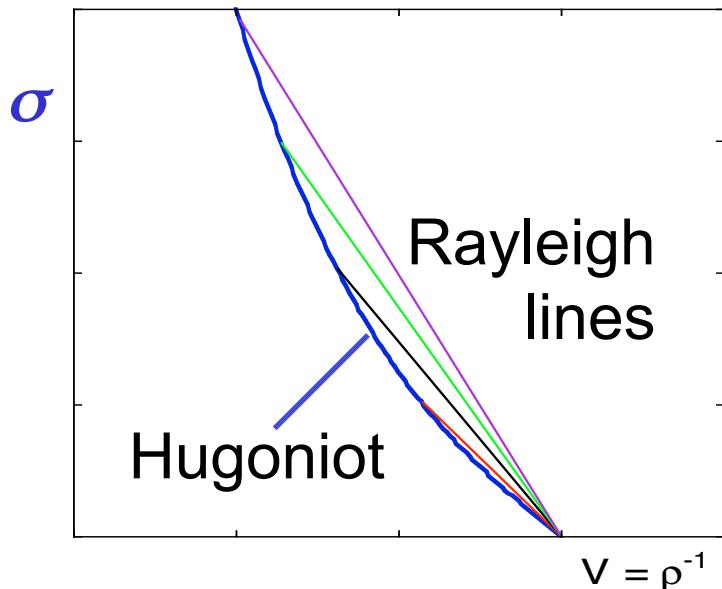
- Five variables: σ_x , u_p , U_s , ρ , and E
- Three conservation relationships (Rankine-Hugoniot jump conditions)
 - By measuring two variables (typically σ_x , u_p , or U_s), the other three can be determined

conservation of

mass: $\rho_0 U_s = \rho (U_s - u_p)$

momentum: $\sigma_x = \rho_0 U_s u_p$

energy: $E - E_0 = 0.5 \sigma_x (V_0 - V)$



material loads along the Rayleigh line, so the Hugoniot is a collection of end states, not a material response curve
the Hugoniot is not a complete equation of state (EOS)!



Gas Guns to Generate Shock Waves



Single Stage Gun 100mm



~1 km/s
~30 GPa

Propellant Gun 89mm



~2 km/s
~100 GPa

Two-Stage Gun 29mm

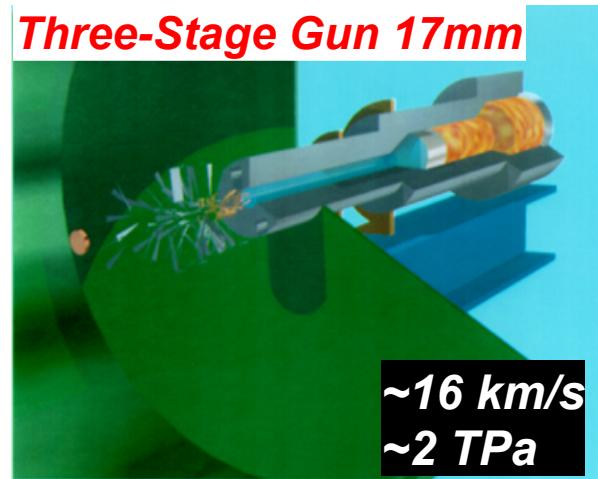


~8 km/s
~700 GPa

gas guns

- launch thin plates (mm's) at high velocities
- well-posed, repeatable initial conditions
- sample is in uniaxial ***strain***
- used to study material behavior at high pressures and strain rates
- usable in laboratory setting

Three-Stage Gun 17mm



~16 km/s
~2 TPa

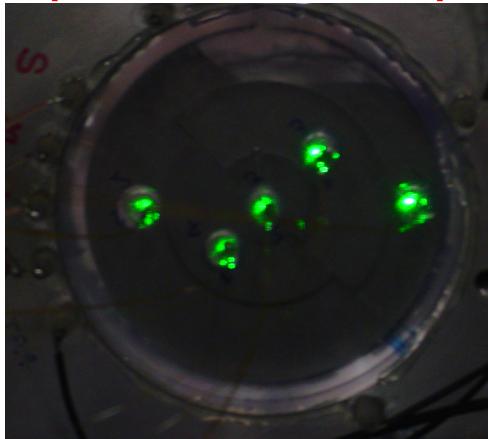
Chhabildas, L. C., Dunn, J. E., Reinhart, W. D., and Miller, J. M. (1993). "An impact technique to accelerate flier plates to velocities over 12 km/s," *Int. J. Impact Eng.* **14**, 121-132.

also: explosives, lasers, magnetic loading (Z)

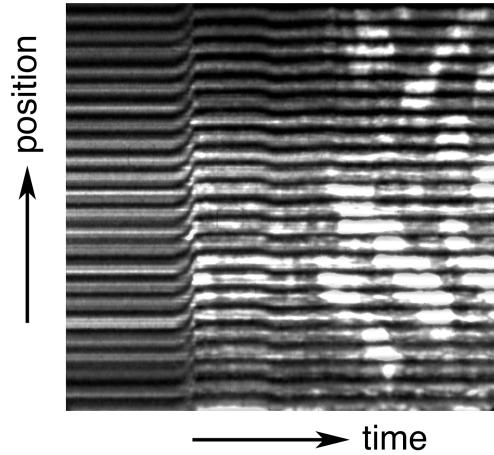


Diagnostics for Dynamic Experiments

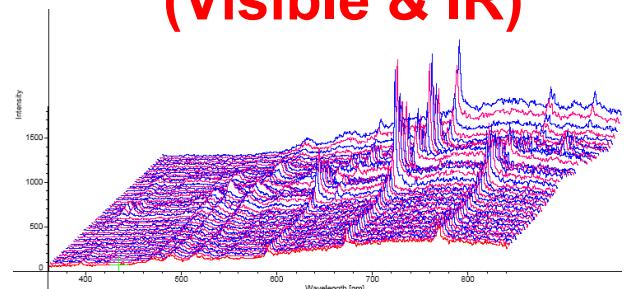
Velocity Interferometry (VISAR & PDV)



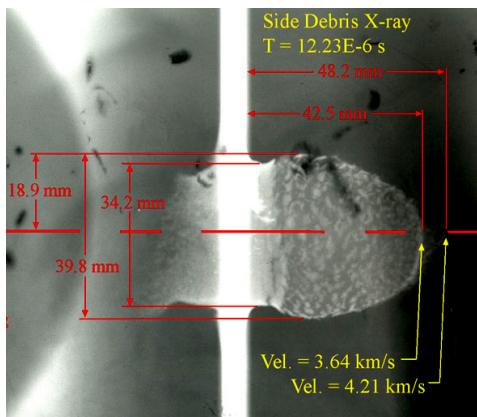
Line-VISAR



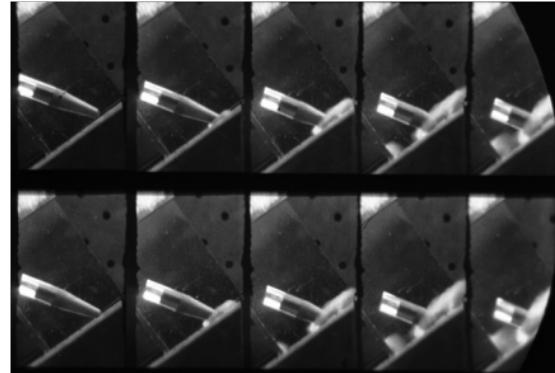
Time-Resolved Spectroscopy (Visible & IR)



Flash X-rays



High-Speed Photography



Pressure Gauges



Advanced Diagnostics: pRad, synchrotron (DCS), etc.

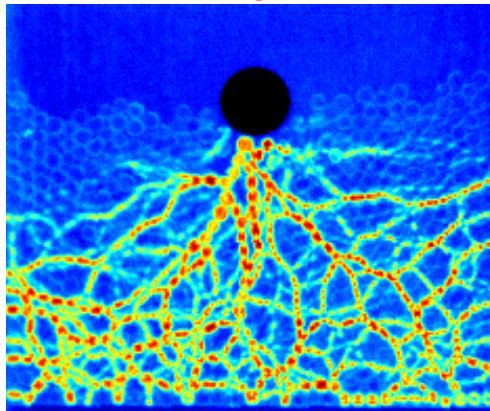


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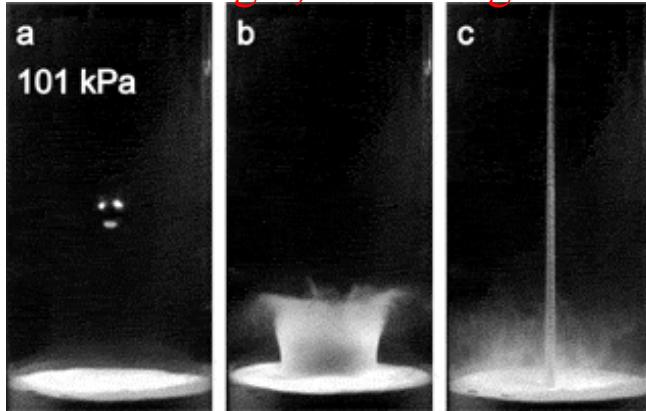


Background on Dynamic Behavior of Granular Materials

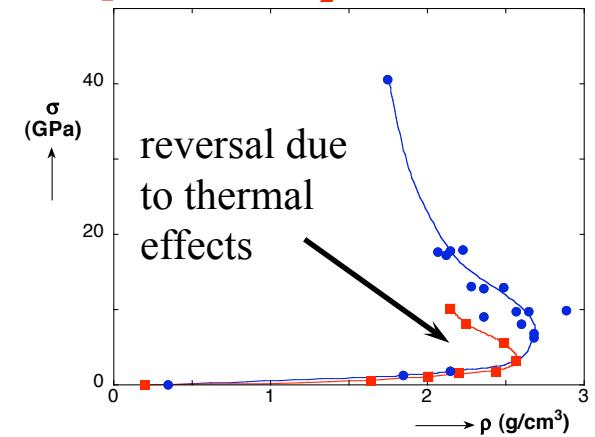
B. Behringer, Duke



H. Jaeger, U. Chicago



porous SiO_2 , Trunin et al.



- granular materials display a rich variety of behaviors
- significant experimental and modeling challenges
- extensive quasi-static and low-velocity impact work
- determine thermal behavior through P-V work (Trunin, 2004)
- consolidation studied extensively to optimize loading, etc.
- partial compaction region seldom addressed
- applications: dynamic consolidation, energetic / reactive materials, planetary science, energy/blast absorption, ceramic armor



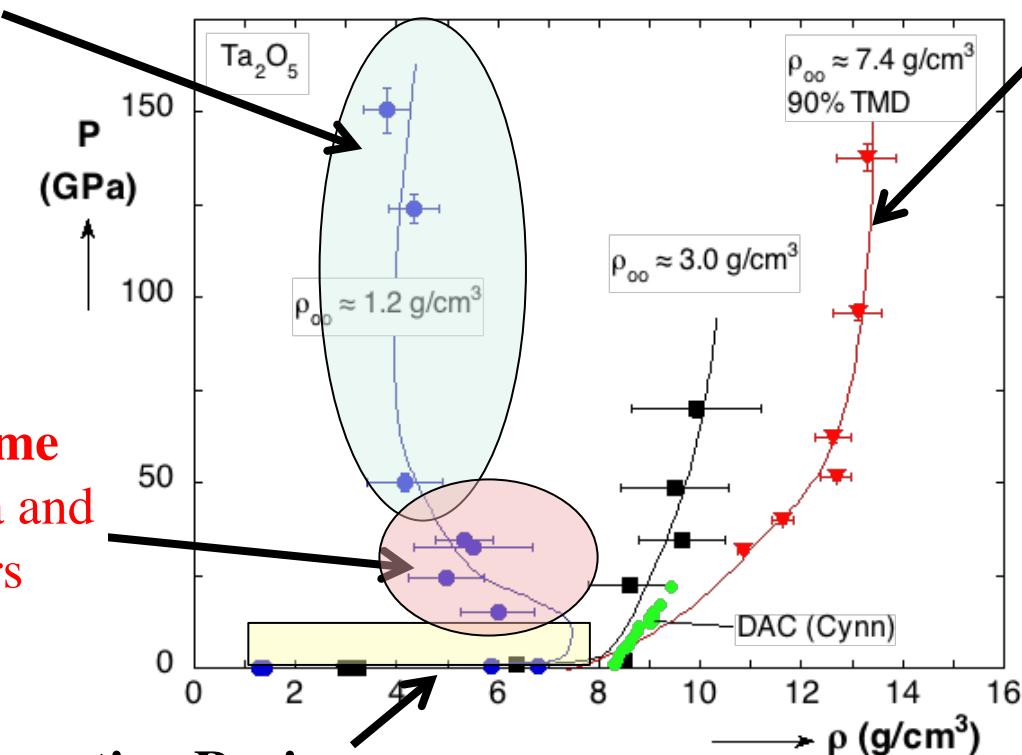
Regimes of Behavior for Granular Ceramics

High Pressure
Expanded Regime
warm dense matter
regime, thermal EOS
melting, ionization,
disassociation, etc.

Intermediate Regime
all EOS phenomena and
particulate behaviors
may be active

Compaction Regime
 $P, \sigma < Y$ (10-20 GPa)
particle crushing, fracture,
strength of granular compact

Principal Hugoniot
EOS, strength, phase
transformations, melt





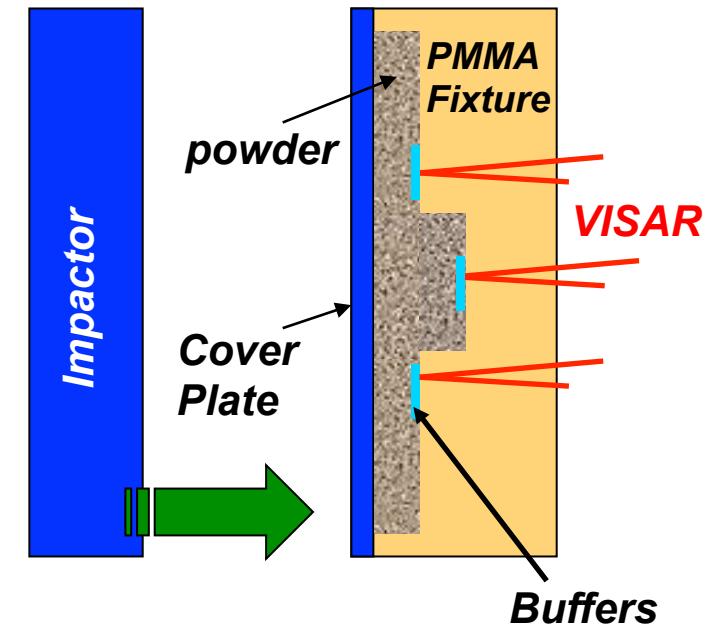
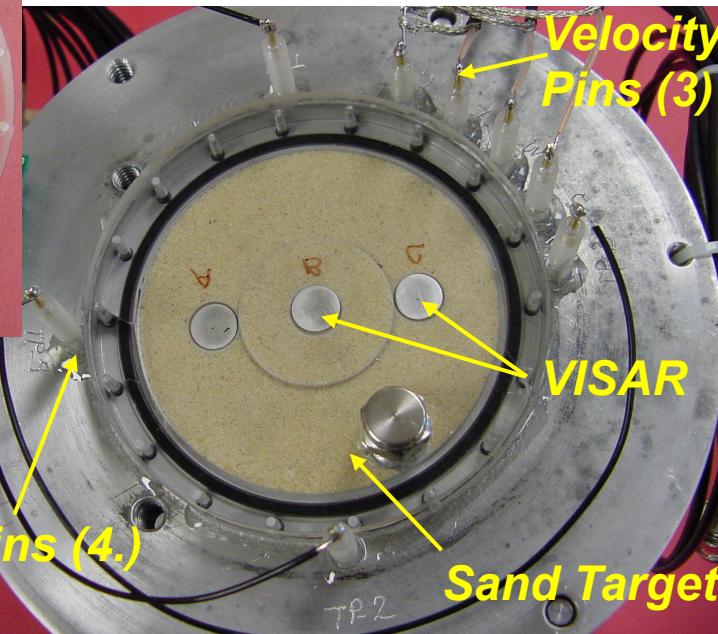
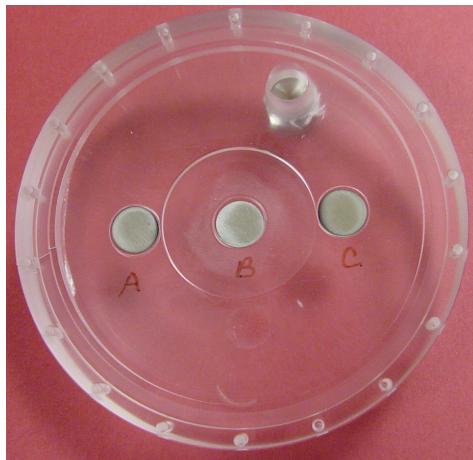
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Planar Impact Experiments on Granular Materials



~1 km/s
~30 GPa



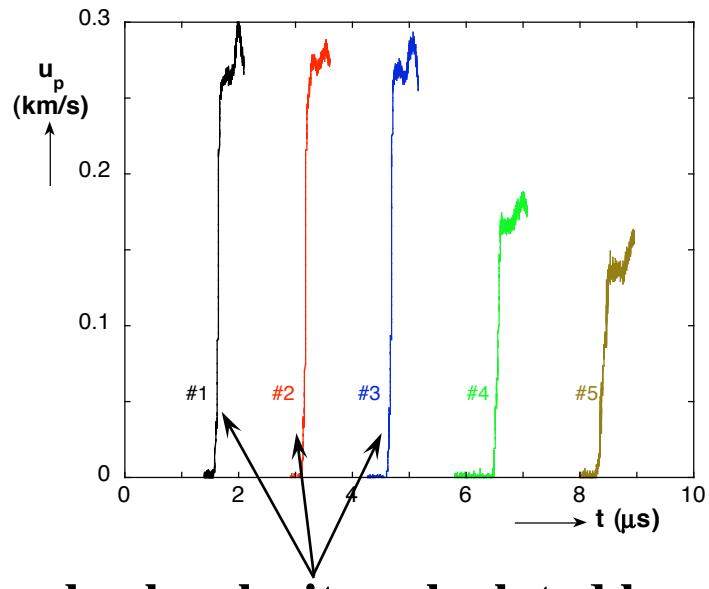
stepped sample for accurate shock velocity and uniform powder density; sealed capsule allows fluid / powder mixtures

Vogler, T.J., Lee, M.Y., Grady, D.E., 2007. "Static and dynamic compaction of ceramic powders." *International Journal of Solids and Structures* **44**, 636-658.

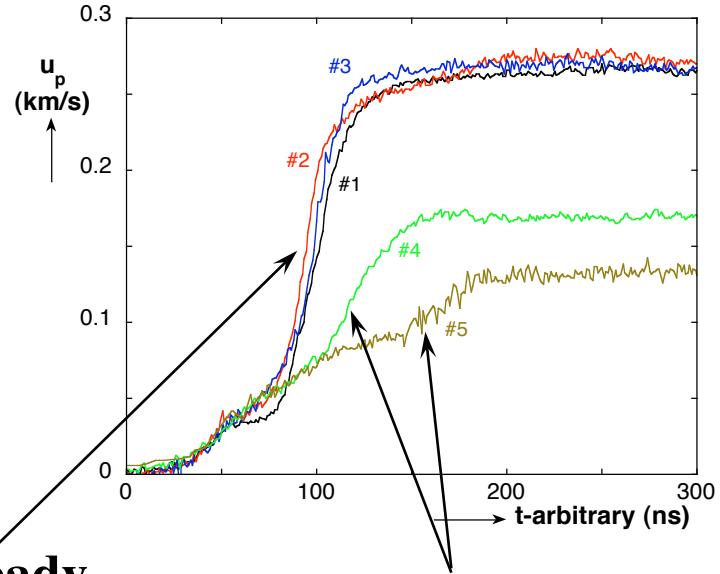
Brown, J.L., Thornhill, T.F., Reinhart, W.D., Chhabildas, L.C., Vogler, T.J., 2007. "Shock response of dry sand." in Shock Compression of Condensed Matter – 2007, American Institute of Physics, 1363-1366.



Measured Steady Waves in WC



shock velocity calculated based on powder thicknesses and arrival times



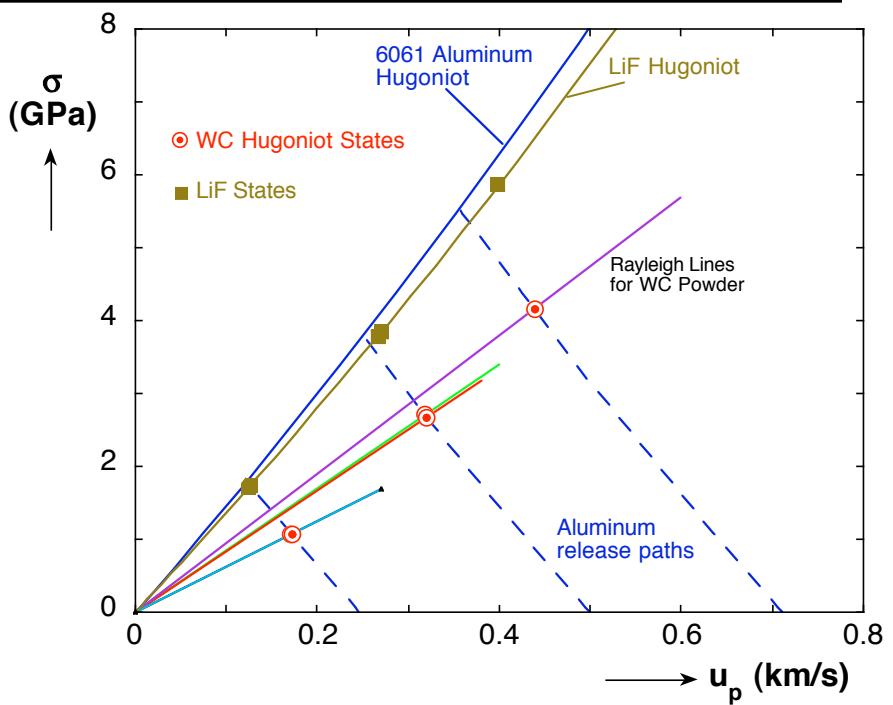
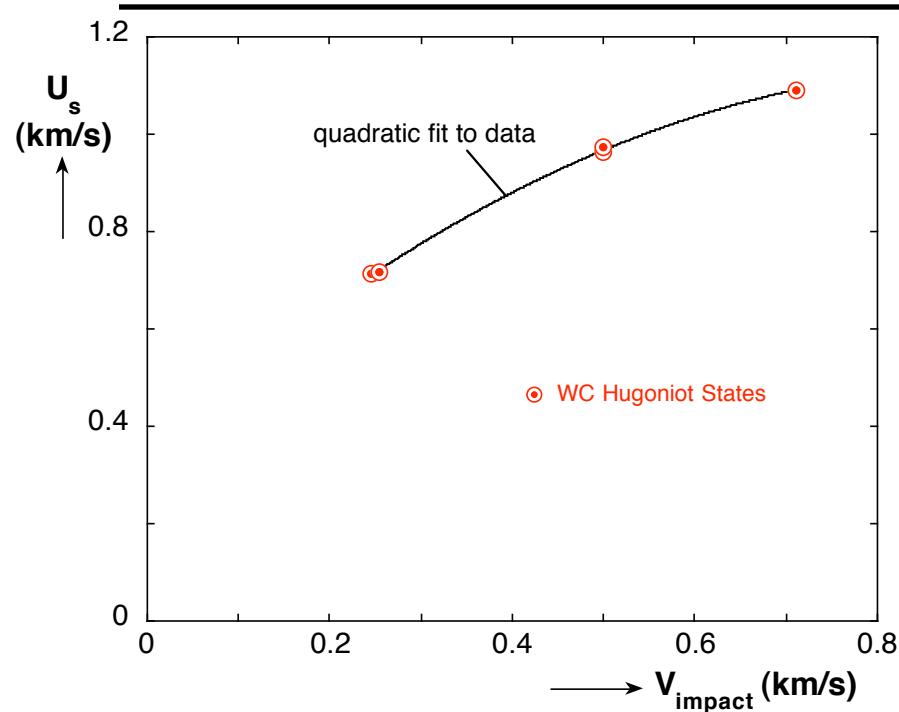
steady, structured waves

attenuated waves

- seem to be first time-resolved measurements of steady waves in granular materials
- since waves are steady, Rankine-Hugoniot jump conditions can be used even though waves have finite rise times



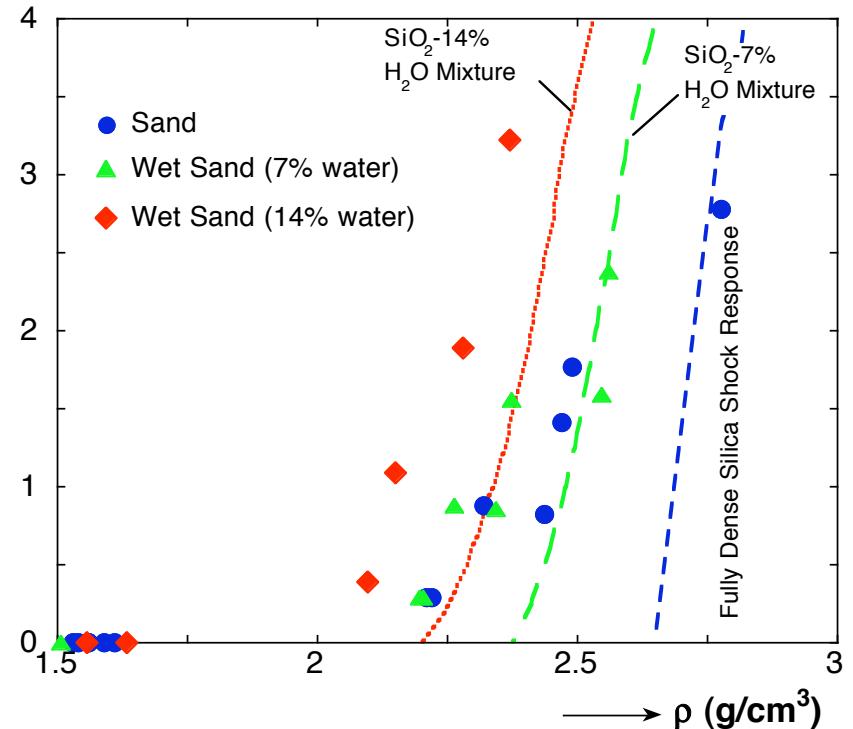
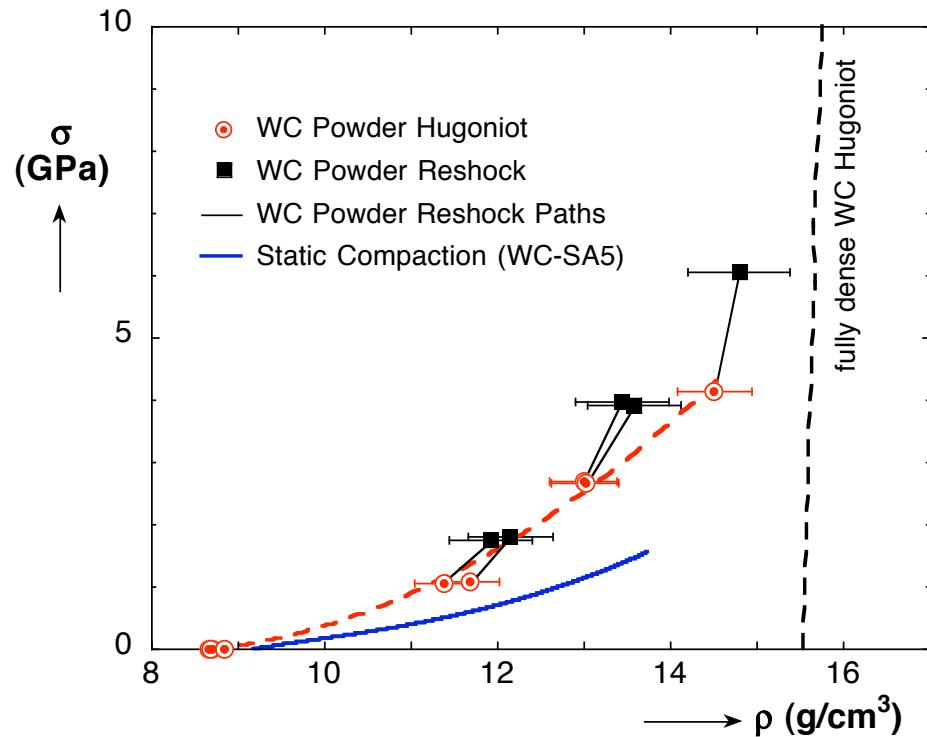
Shock Velocities and Hugoniot States



- impedance matching to aluminum impactor used to determine Hugoniot stress and particle velocity ($\sigma = \rho_{oo} U_s u_p$)
- density then calculated from $\rho = \rho_{oo} U_s / (U_s - u_p)$



Compaction Response for WC and Wet/Dry Sand

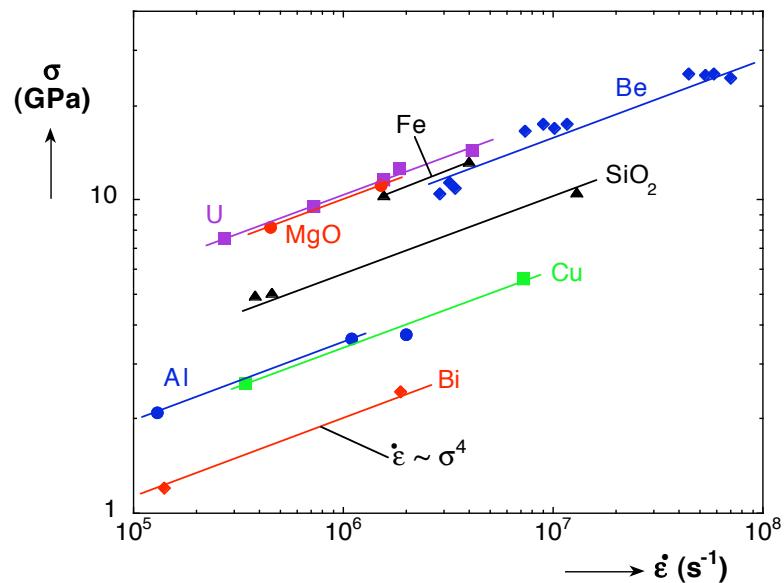


- first reshock state lies above Hugoniot suggesting elastic response of compacted material
- dynamic response is stiffer than static response for WC, about the same for sand

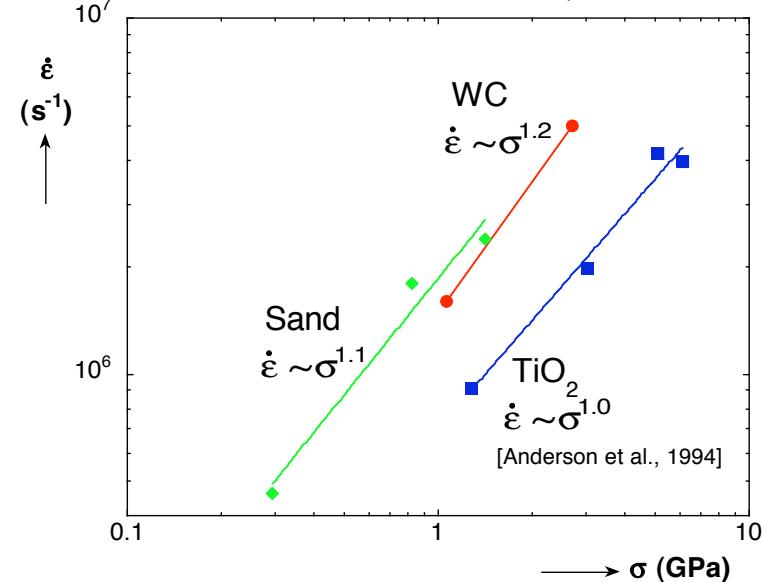
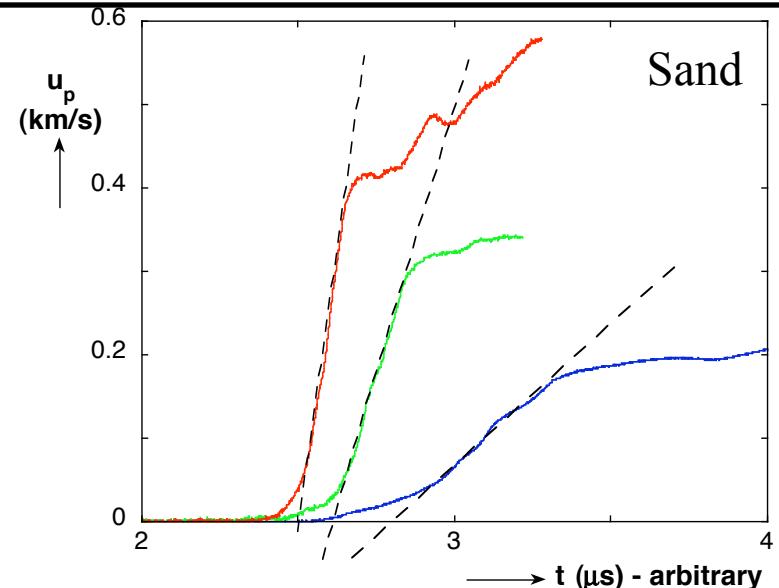


Scaling Between Rise Time of Wave and Stress

for many fully dense materials (Al, Be, Bi, Cu, Fe, MgO, SiO₂, U),
rise times of steady waves scale as
• $\dot{\varepsilon} \sim \sigma^4$ (Swegle & Grady, 1985)



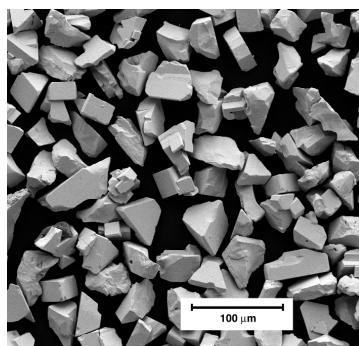
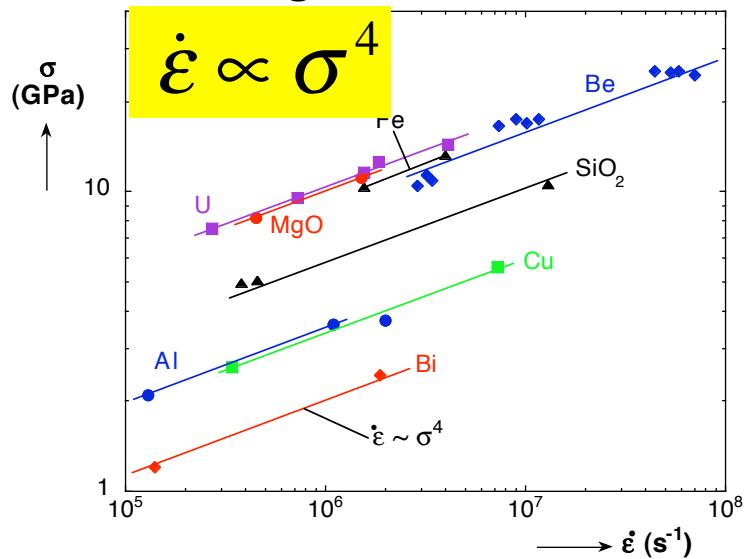
data on three granular ceramics
and sugar suggest a linear scaling
between stress and strain rate



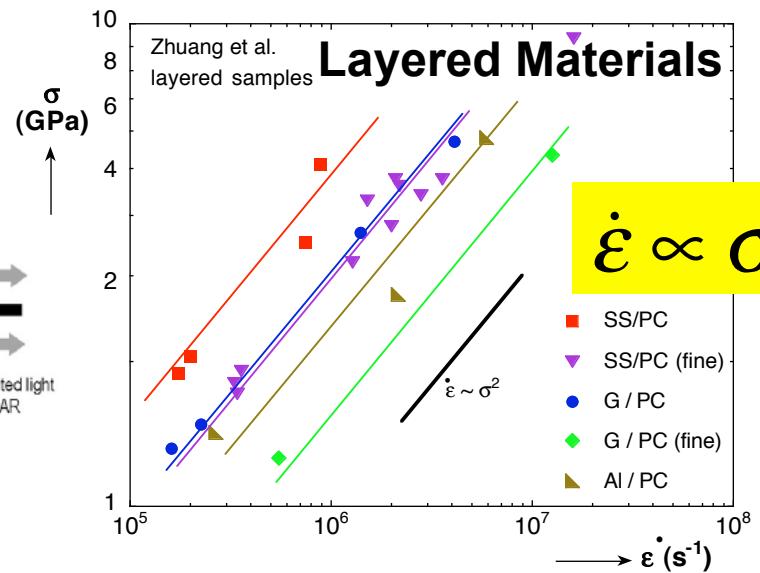
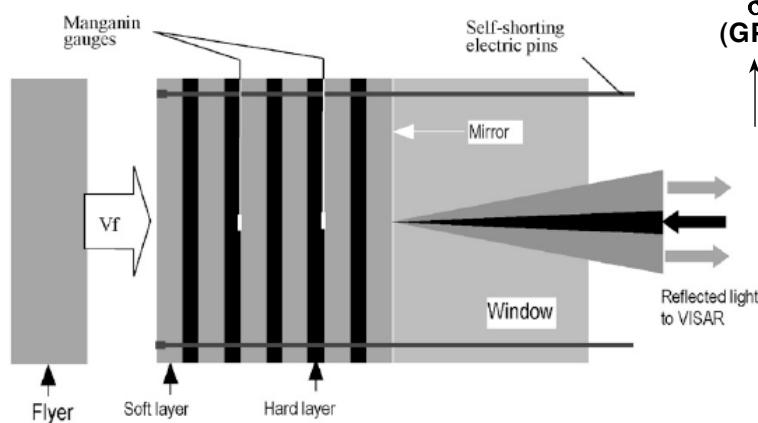
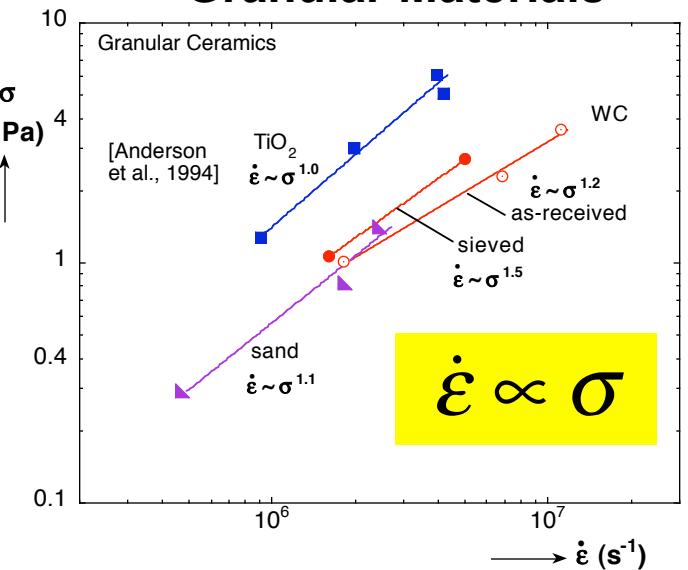


Scaling of Waves in Materials

“Homogeneous” Materials



Granular Materials

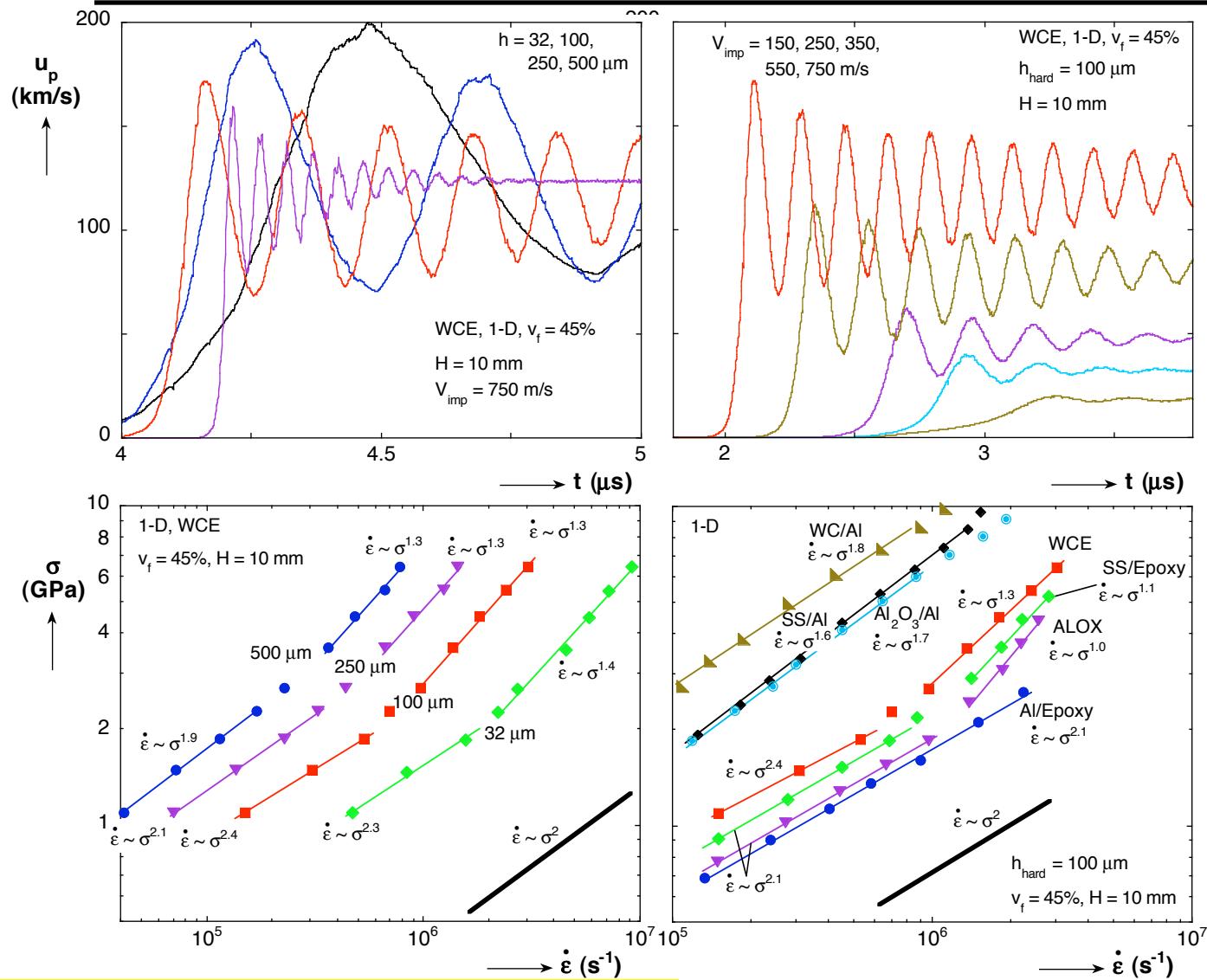


particulate composites (e.g. WC/epoxy, ALOX, PBX) show 4th power scaling



Simulations for Layered Materials

1-D CTH Calculations



$h \uparrow$ $\dot{\epsilon} \downarrow$
 $V, \sigma \uparrow$ $\dot{\epsilon} \uparrow$

also a function
of material
parameters of
layers



Dimensional Analysis for Layered Materials

variables of problem:

$$\sigma, \dot{\varepsilon}, h, v_f, C, (\rho_s, \rho_h) \text{ or } (z_s, z_h)$$

construct non-dimensional groups:

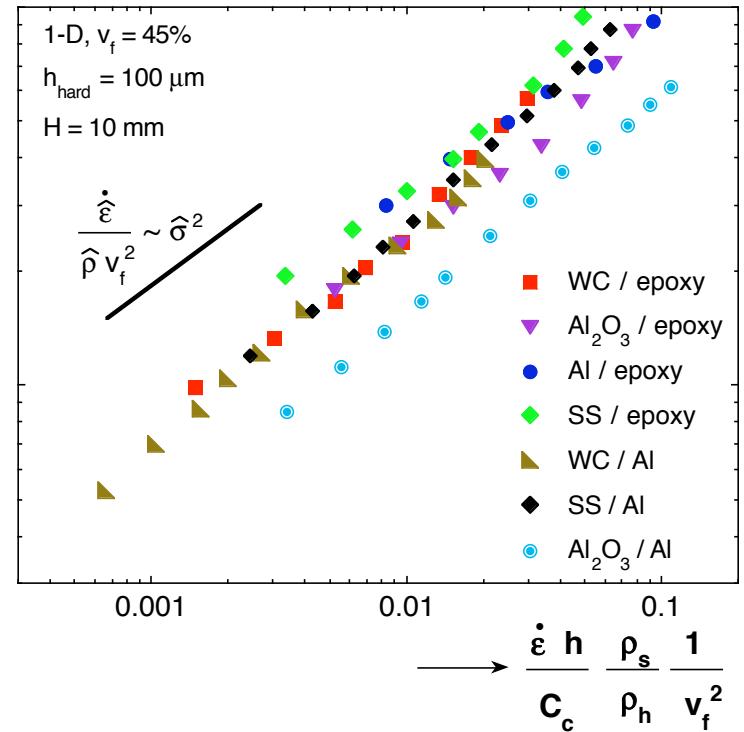
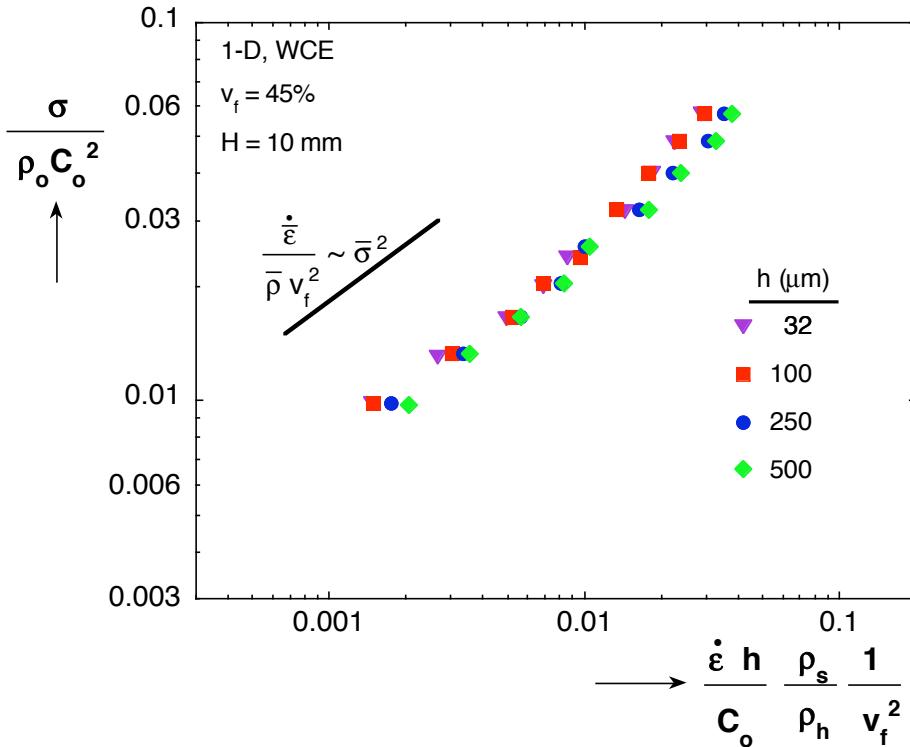
$$\dot{\bar{\varepsilon}} = \left(\frac{\dot{\varepsilon} h}{C_o} \right) \quad \bar{\sigma} = \left(\frac{\sigma}{\rho_o C_o^2} \right) \quad (v_f) \quad \bar{\rho} = \left(\frac{\rho_s}{\rho_h} \right)$$

$$C_o = \left(\frac{v_f}{C_h} + \frac{1-v_f}{C_s} \right)^{-1} \quad C_h, C_s = \begin{cases} C_B & \text{for polymers and metals} \\ C_L & \text{for ceramics} \end{cases}$$

$$\rho_o = v_f \rho_h + (1-v_f) \rho_s$$



Non-Dimensional Simulation Results

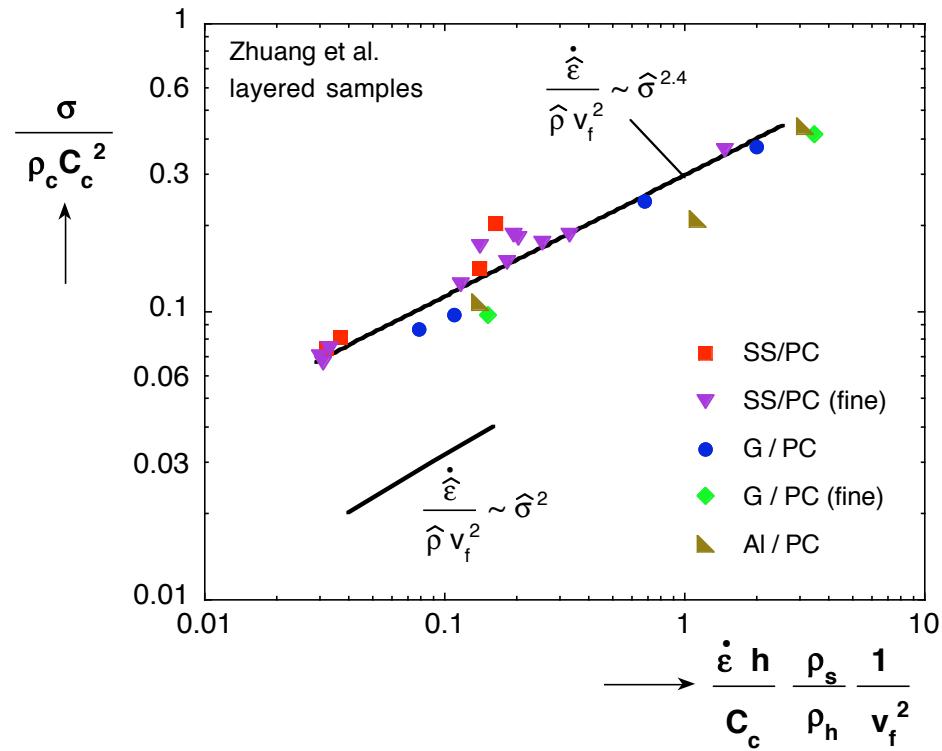


- non-dimensionalization collapses data for different layer thicknesses

- data for different material combinations collapse well using density ratio (with one exception)



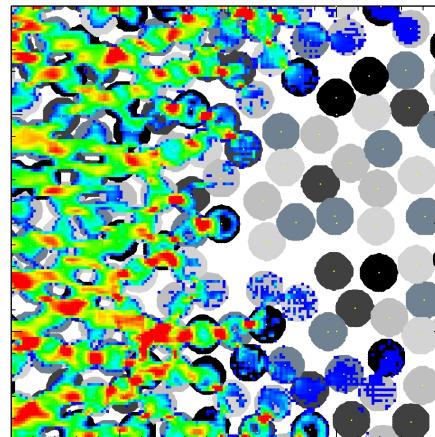
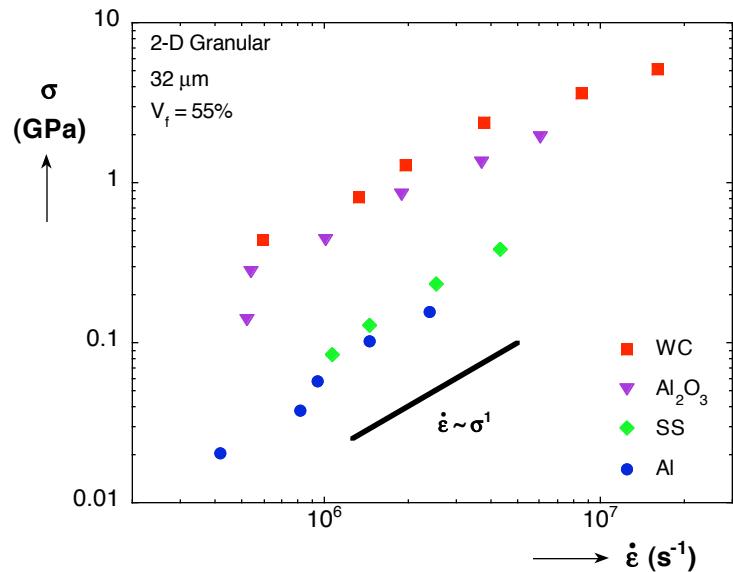
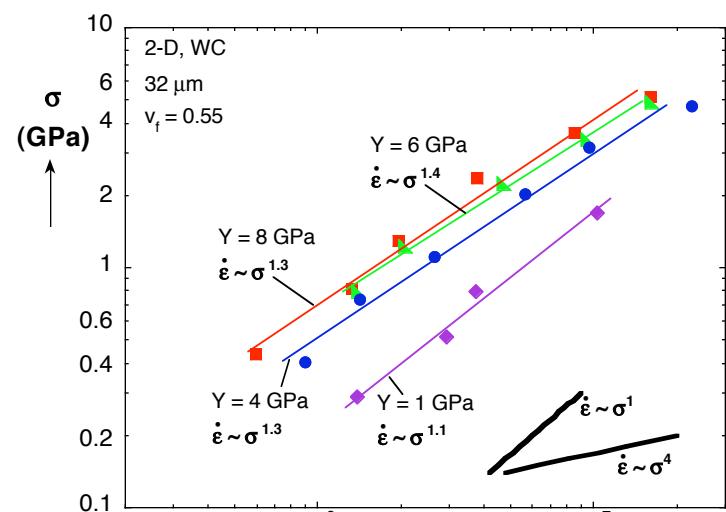
Non-Dimensionalized Experimental Results



- non-dimensional experimental results also collapse to a single curve (approximately to second power)



2-D CTH Simulations of Granular Materials

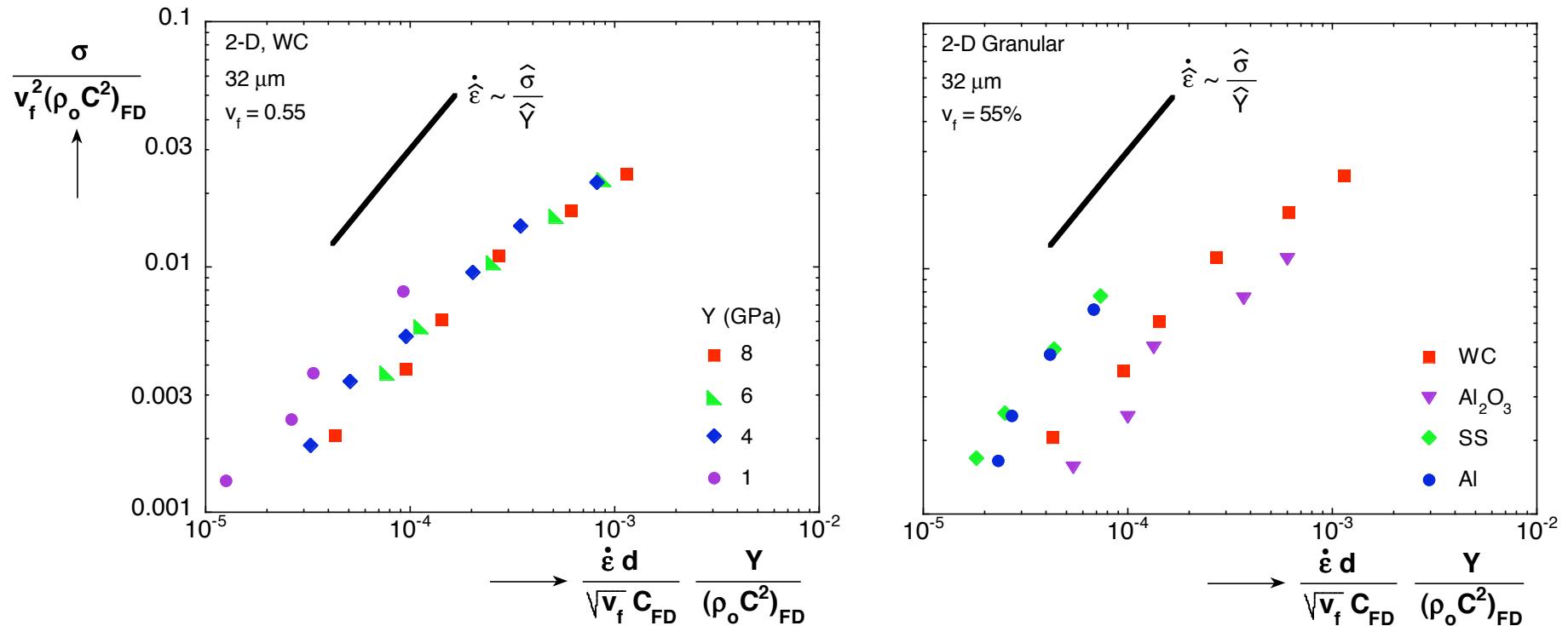


- non-planar shock structure
- CTH simulations reproduce first power scaling
- some dependence on Y , strong material dependence
- non-dimensionalization suggested by Grady (2010):

$$\frac{\sigma}{\dot{\epsilon}} \propto \left(\frac{\rho_o}{\rho_s} \right)^m \sqrt{\rho_o d^2 \sigma_c}$$



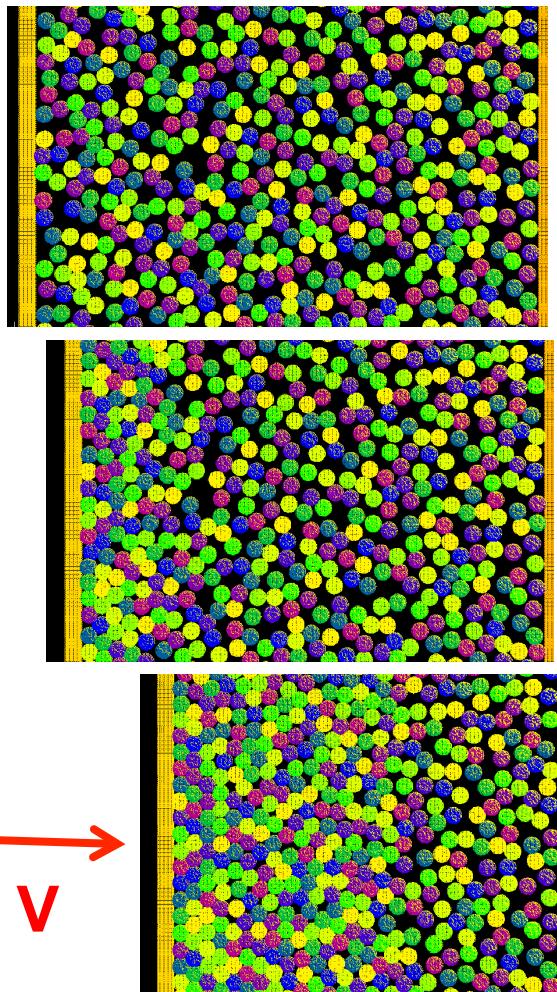
Non-Dimensionalization of CTH Results



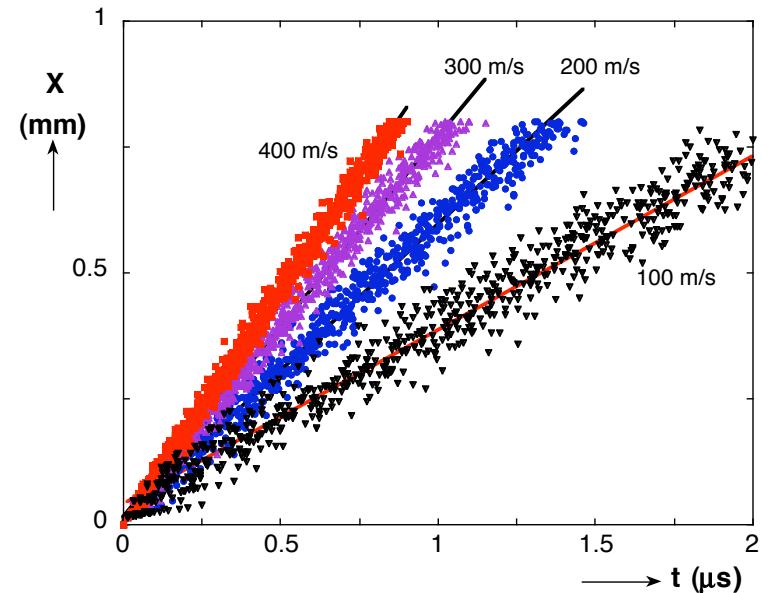
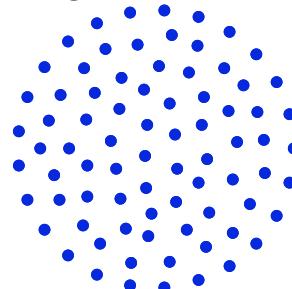
- scale wave speeds by square root of volume fraction (suggested by Steinberg, some validation by Bless)
- Y needed to collapse data, though metals and ceramics separated somewhat



Results from a Particle-Based Peridynamics Code



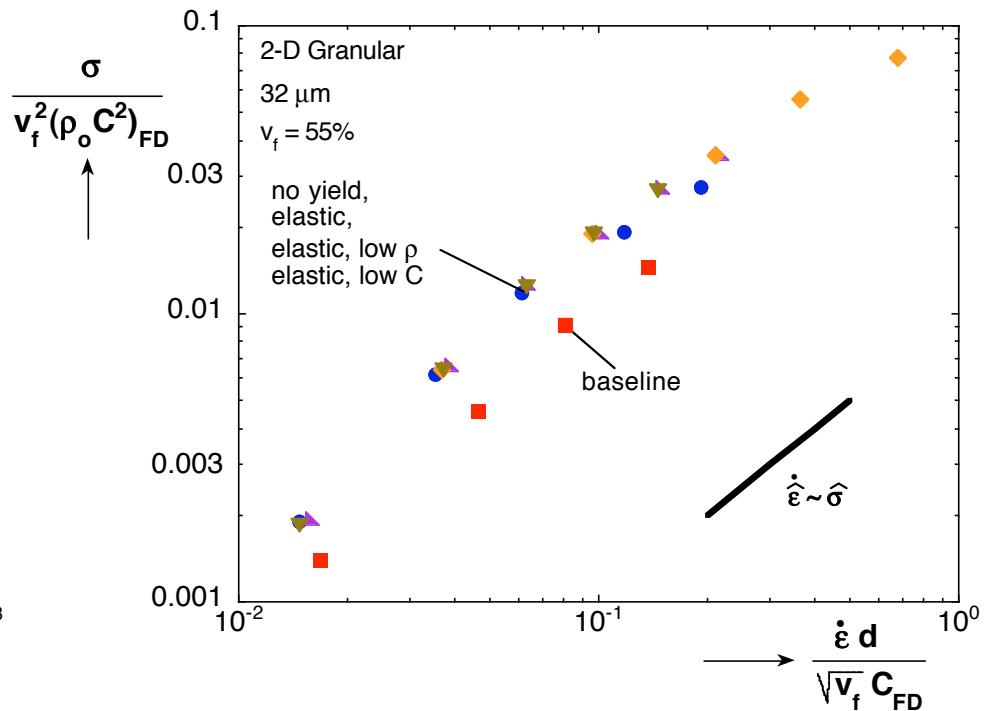
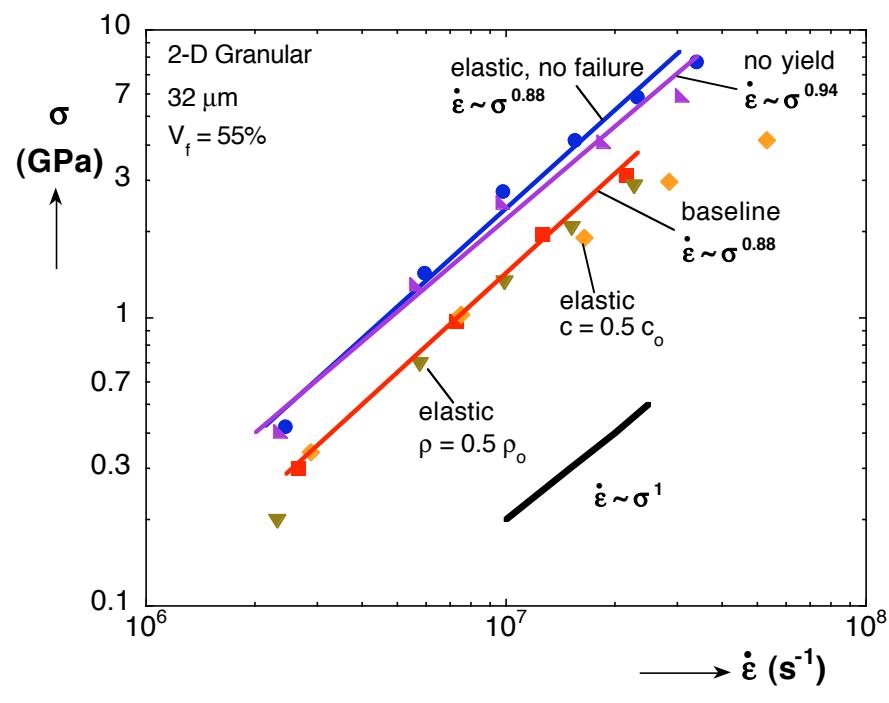
discretization
of grains



- waves are steady
- wave speed increases with V
- width of band decreases with V
- elastic simulations yield same scaling
 - Grady's scaling doesn't work



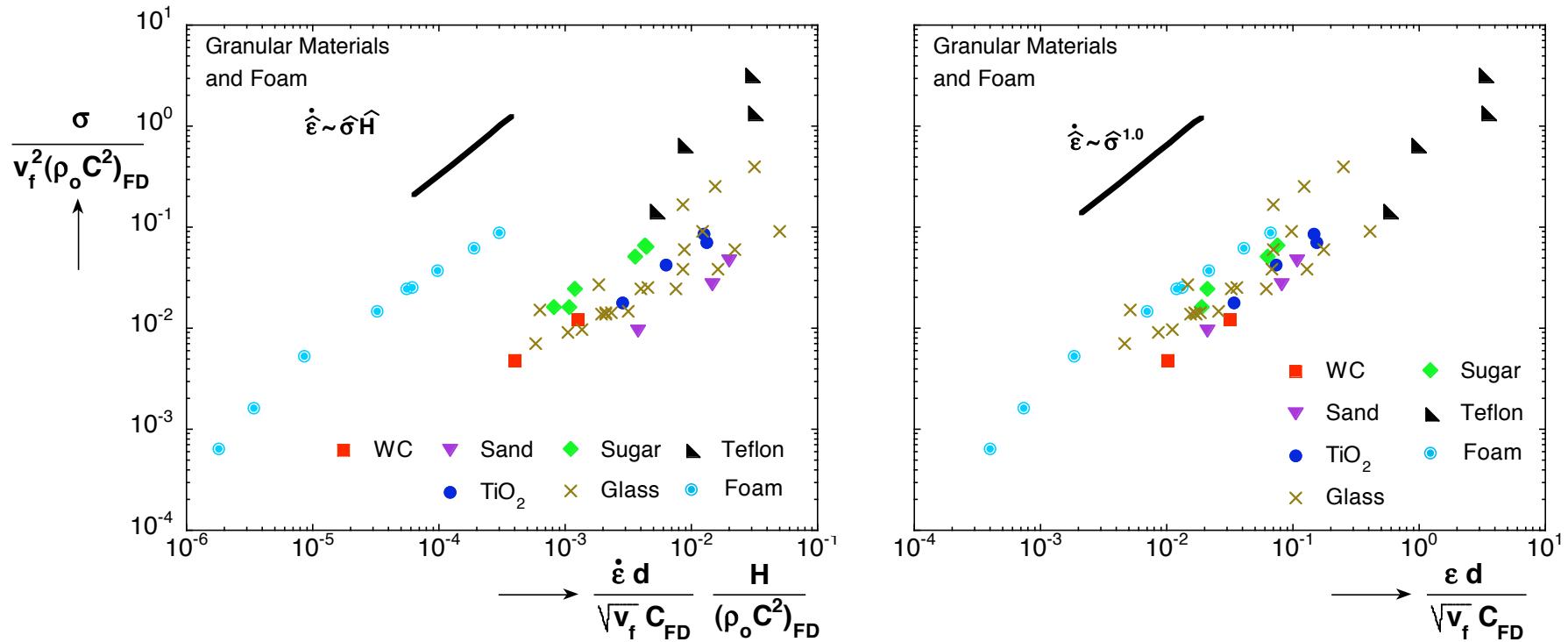
Non-Dimensionalization of Peridynamics Results



- no strength in problem if material elastic
 - fracture does not seem to affect scaling
 - elastic-plastic material (baseline) has lower characteristic wave speed → will shift data upward



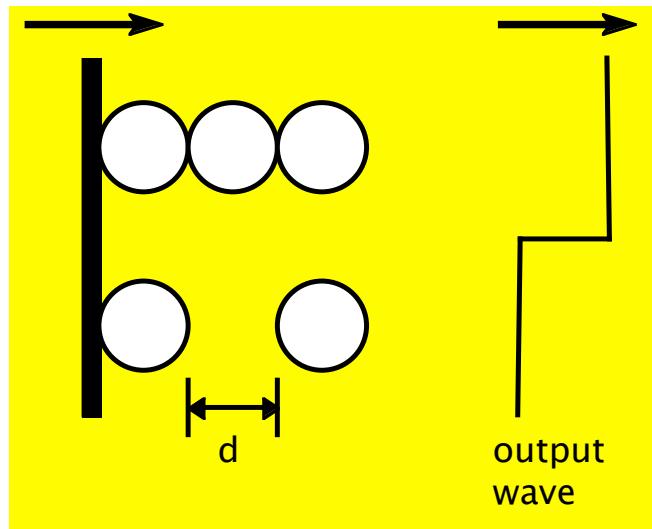
Non-Dimensionalization of Experimental Results



- use hardness (H) as characteristic strength
- does volume fraction enter in separately?
- collapse is better without H
- polyurethane foam (Zaretsky et al., 2012) consistent



A Simple Scaling Argument for Granular Materials (1)



$$\varepsilon = \frac{u_p}{U_s} \quad (\text{conservation of mass})$$

$$\dot{\varepsilon} \propto \frac{\varepsilon}{\Delta t} = \frac{u_p / U_s}{d / u_p}$$

mass traversing pores controls width of shock front

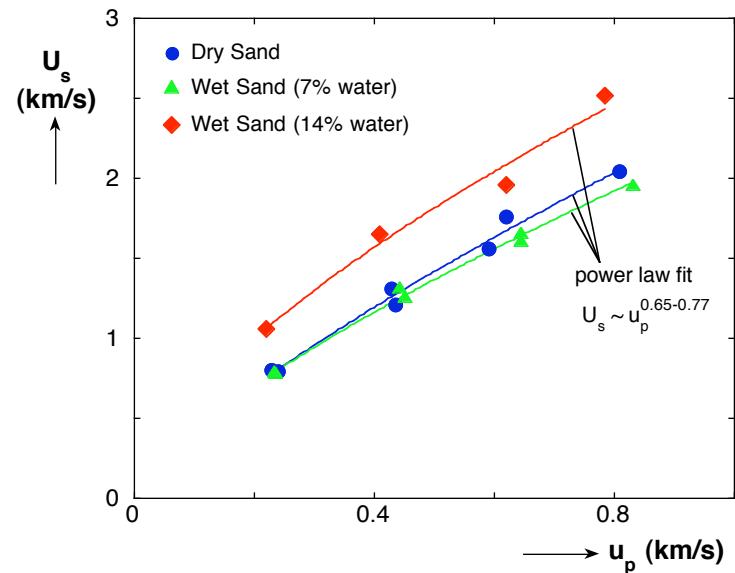
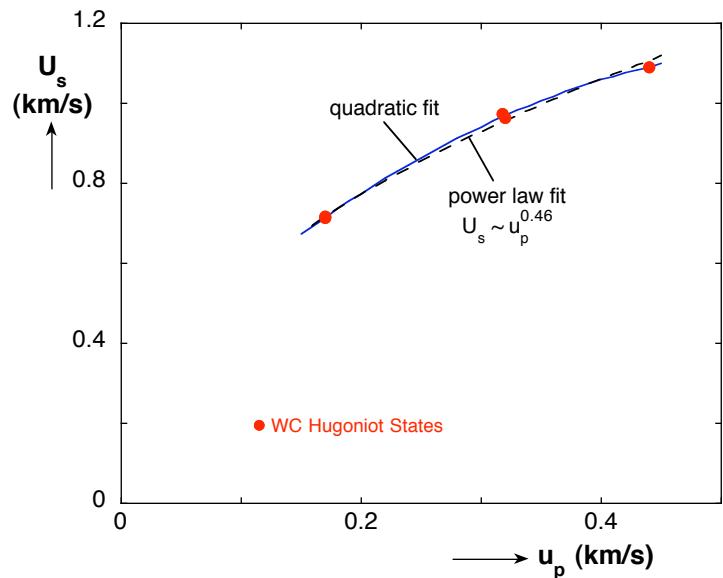
$$\dot{\varepsilon} \propto \frac{u_p^2}{d U_s}$$



A Simple Scaling Argument for Granular Materials (2)

$$\sigma = \rho_{oo} U_s u_p$$

$$\dot{\varepsilon} \propto \frac{u_p^2}{dU_s}$$



$$\text{if } U_s \propto u_p^{0.5}$$

$$\sigma \propto u_p^{3/2}$$

$$\dot{\varepsilon} \propto u_p^{3/2} \rightarrow \dot{\varepsilon} \propto \sigma$$

$$\text{if } U_s \propto u_p^{0.75}$$

$$\dot{\varepsilon} \propto \sigma^{0.7}$$

mass transfer across void is critical aspect, thus granular WC ($n=1$) and WC/epoxy ($n=4$) behave very differently

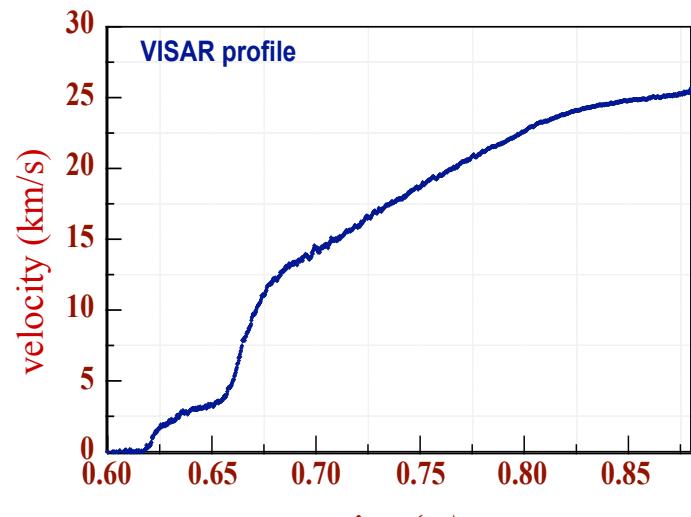
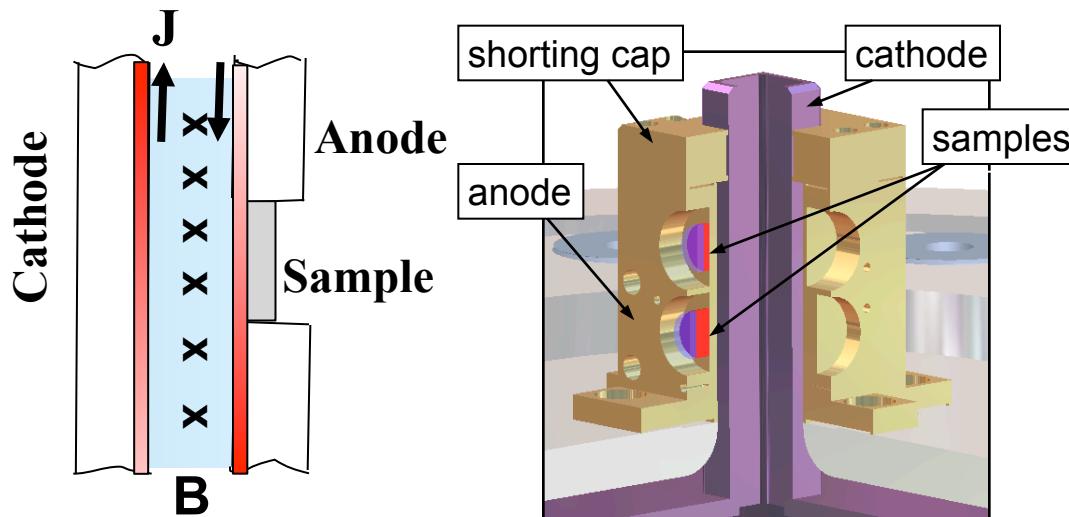
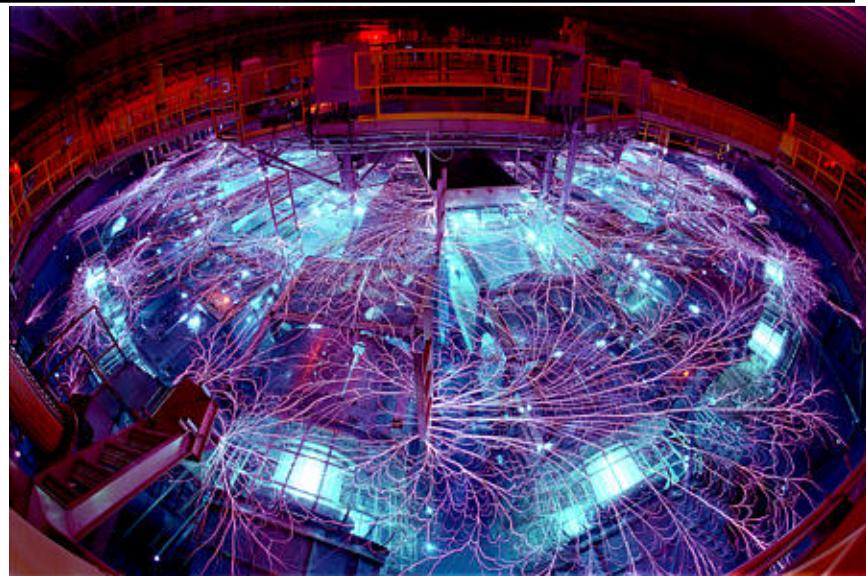


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Z Pulsed Power Machine

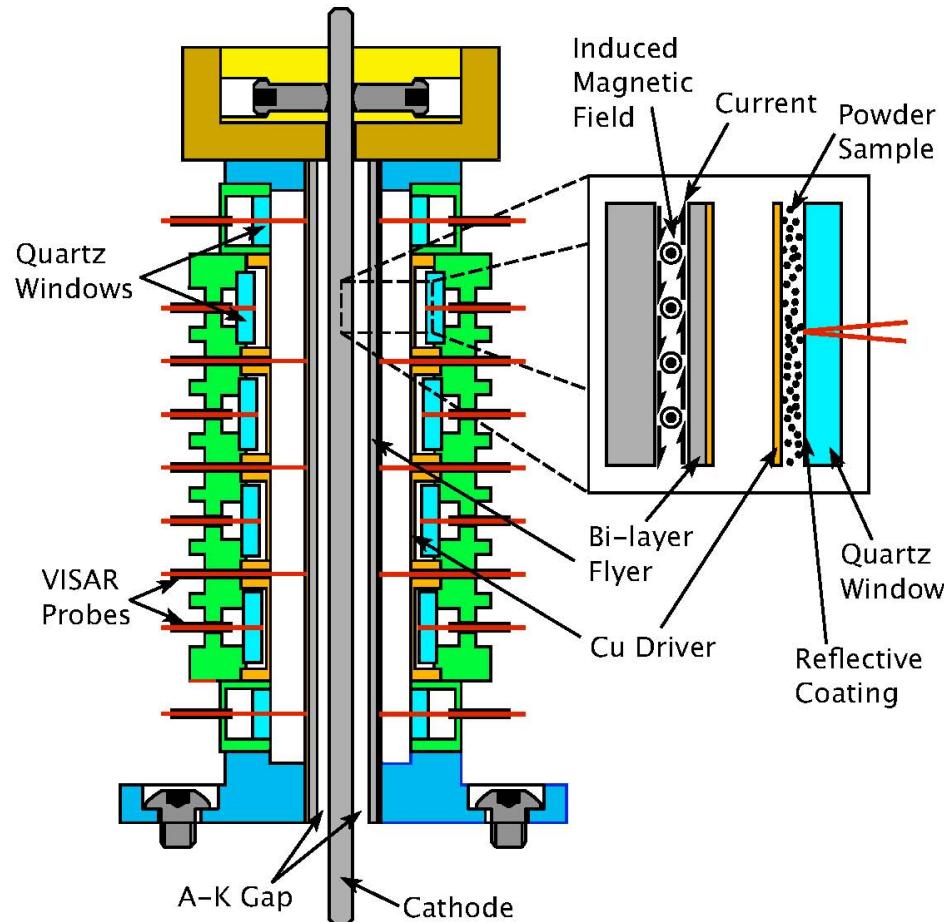
- Generates ~ 26 MA over 100's of ns
- Utilize current to generate magnetic forces
- Magnetic forces create smooth waves in materials
- Waves used for isentropic loading (to ~ 400 GPa) and to launch high-velocity flyer plates (to ~ 40 km/s, pressures > 1 TPa)



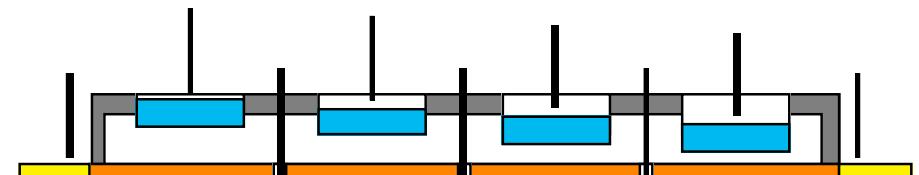
Davis, J.-P., Deeney, C., Knudson, M. D., Lemke, R. L., Pointon, T. D., and Bliss, D. E. (2005). "Magnetically driven isentropic compression to multimegabar pressures using shaped current pulses on the Z accelerator," *Physics of Plasmas* 12, 056310.



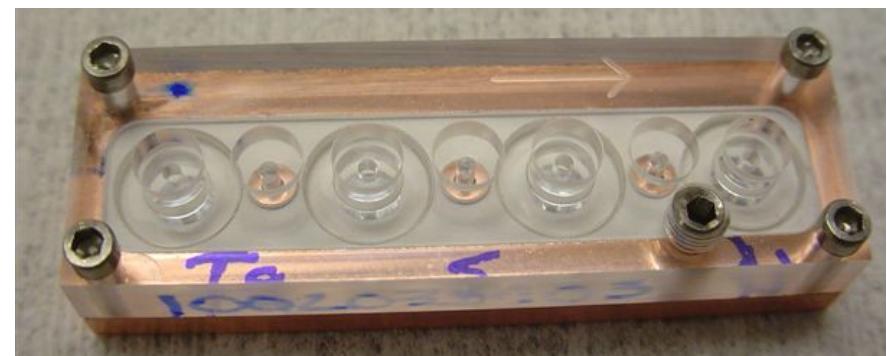
High Pressure Z Experiments



400, 600, 800, and 1000 micron samples



300 micron thick copper driver

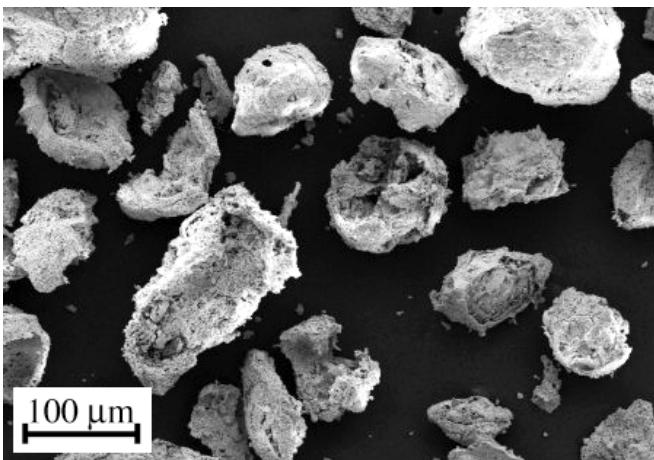


$V = 9.9-10.3$ and $11.2-11.4$ km/s

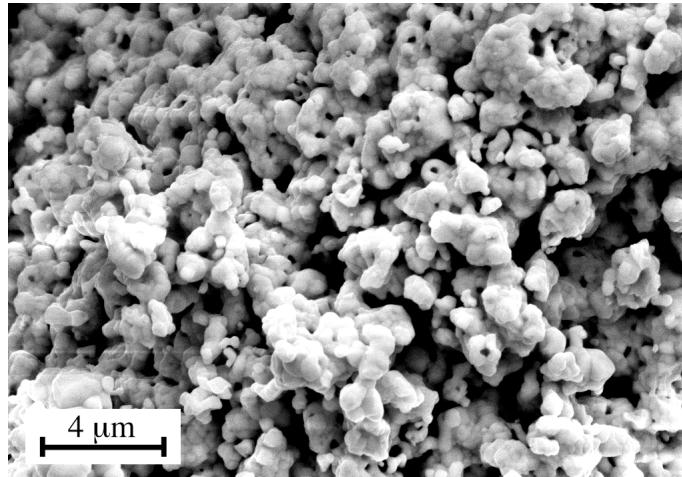
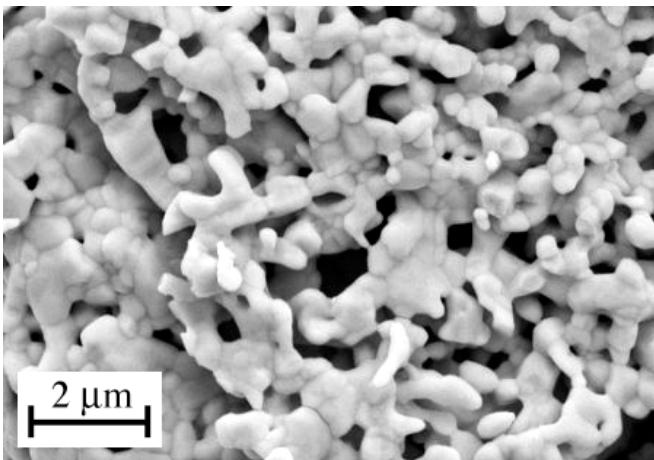
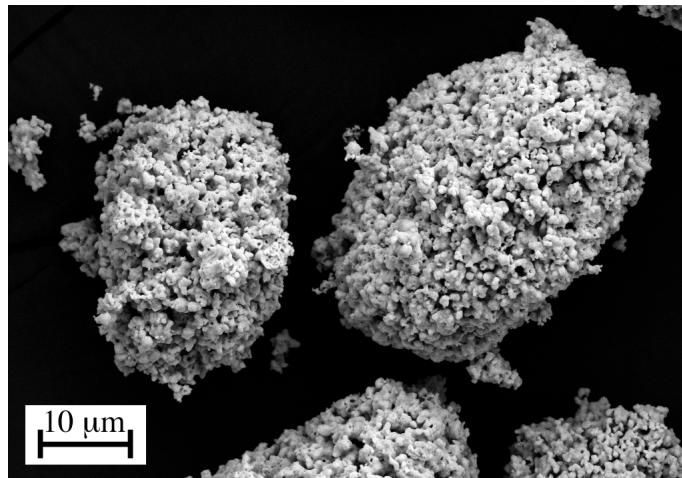


Two Different Forms of Granular Ta_2O_5

~1.3 g/cc from Cerac



~3 g/cc from American Elements

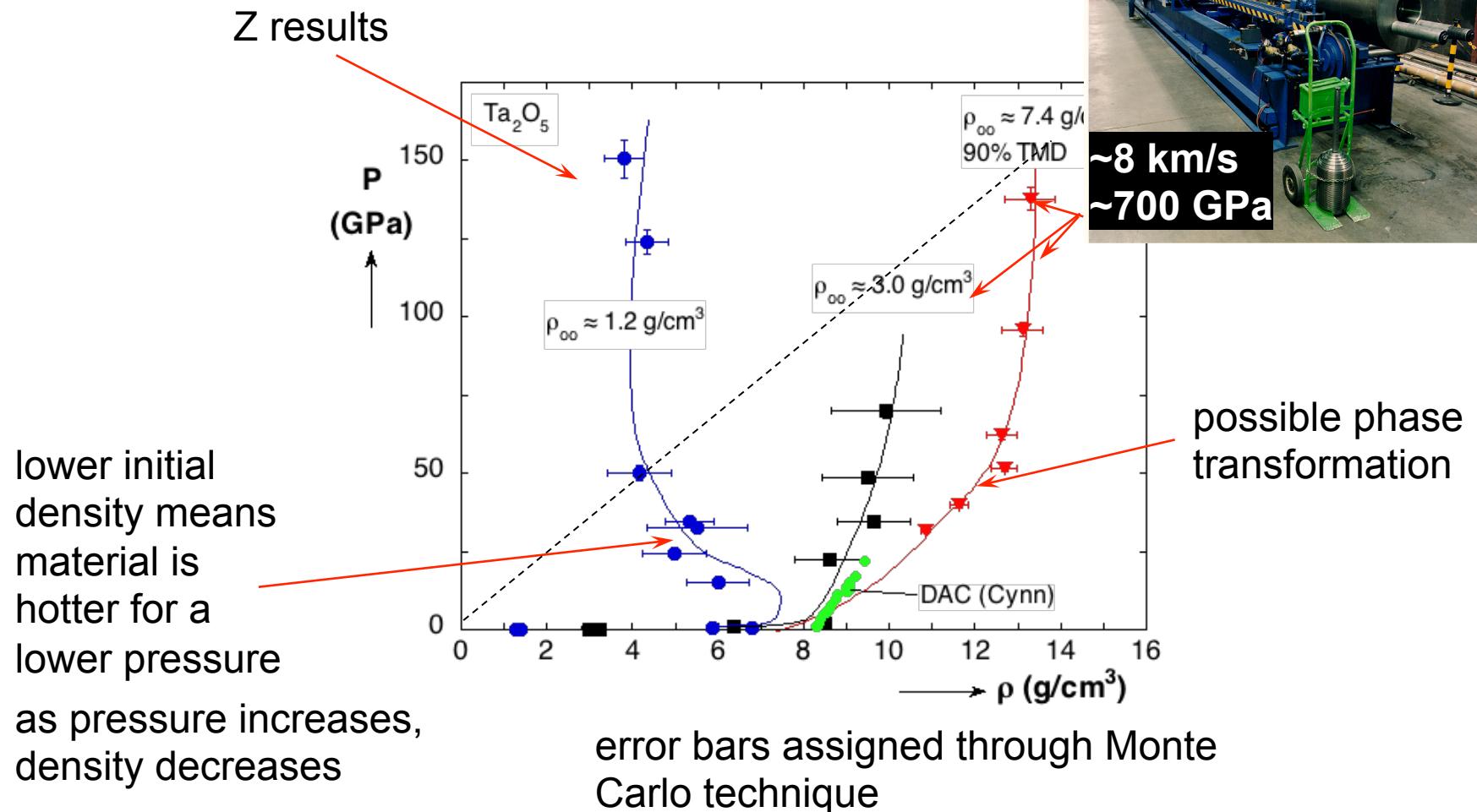


X-ray diffraction shows all material is in orthorhombic phase
also 90% dense disks from cold pressing or low temperature sintering



High-Pressure Shock Results

Two-Stage Gun 29mm

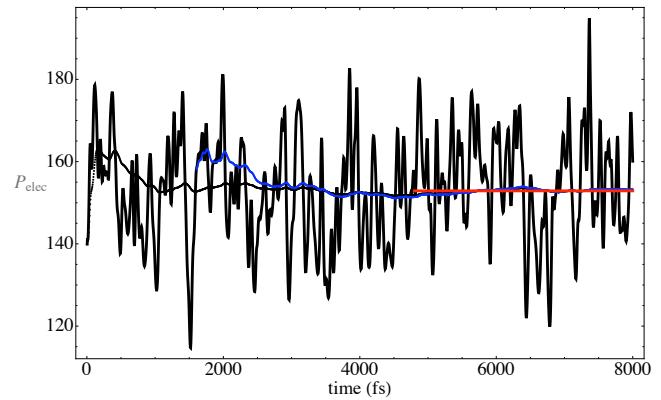
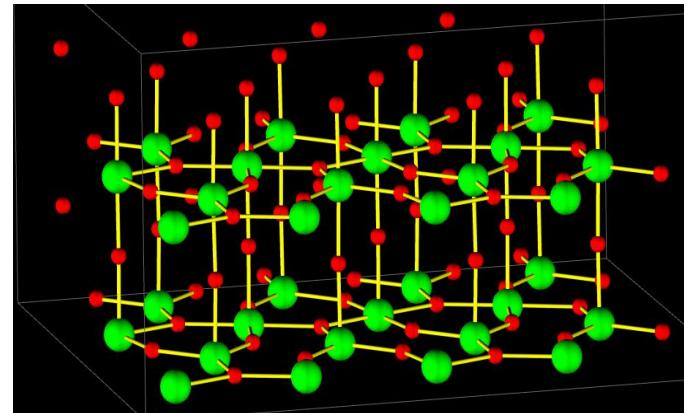
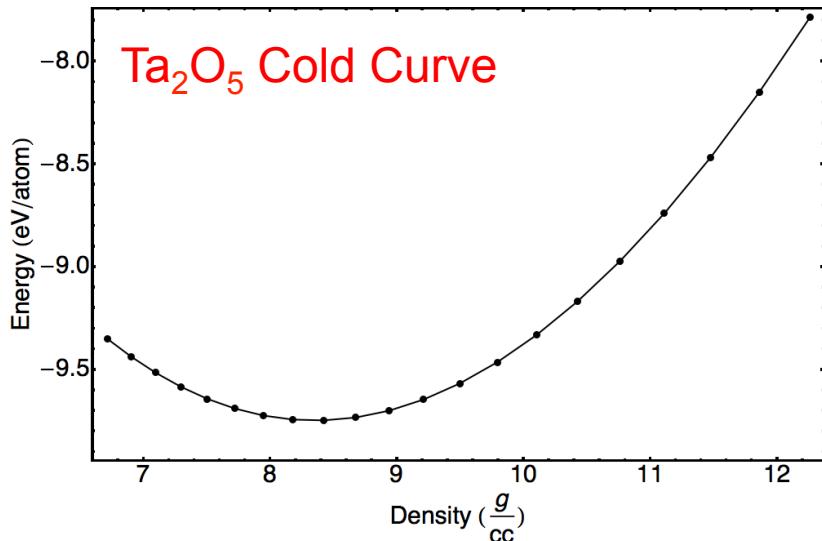




Density Functional Theory Modeling of Porous Tantala

K. Cochrane
L. Shulenburger
P. Weck

- ◆ solve approximation to Shroedinger's equation
- ◆ 32 Ta atoms and 80 O atoms.
- ◆ equilibrate for mean P and E
- ◆ LDA potential with 11 electron Ta pseudo potential and 6 electron O potential



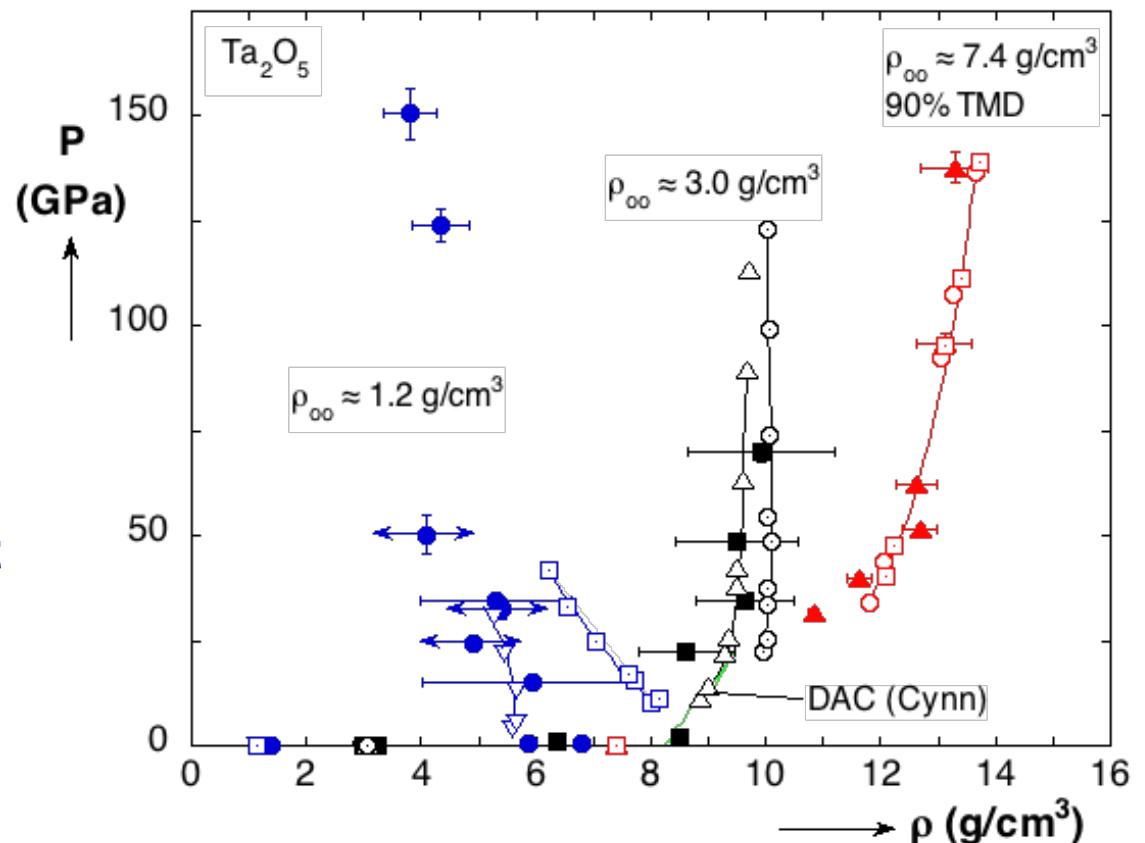
satisfy energy equation to determine Hugoniot state

$$0 = (E - E_o) - \left(\frac{P + P_o}{2} \right) (V_o - V)$$



Porous Hugoniot Calculated for Ta_2O_5 Using DFT

- include the surface energy in energy equation
- δ = surface energy
- E_{solid} - energy at the reference density
- P_{solid} is the pressure and usually NOT Zero (although experimentally it should be)
- $V_{initial}$ – porous volume
- method of including porosity is empirical but seems to work

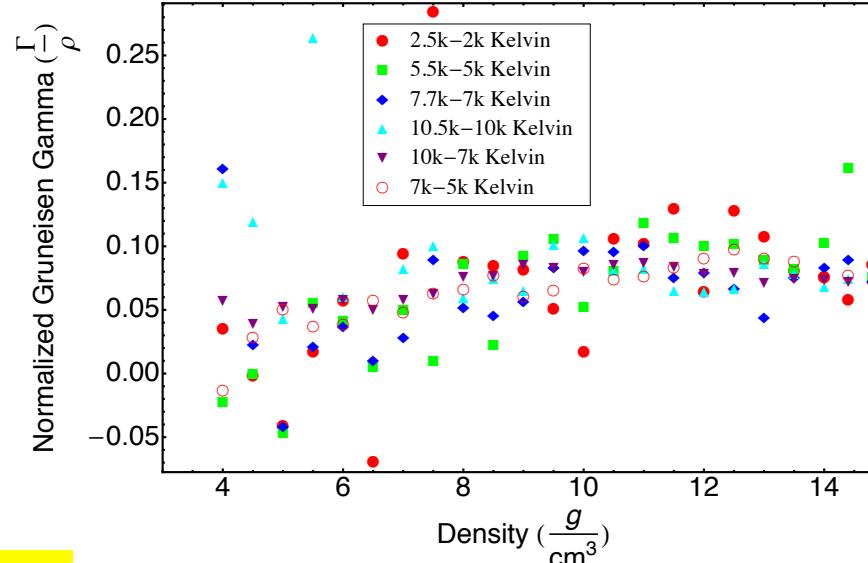
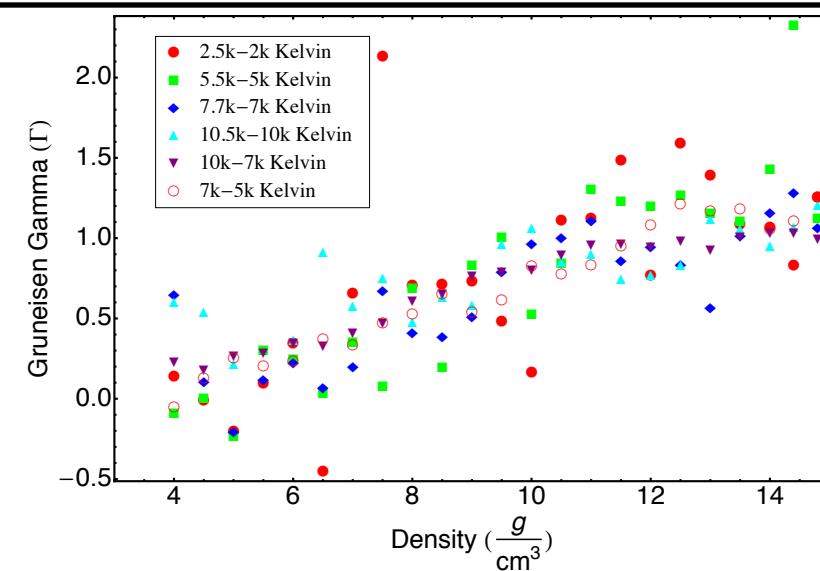
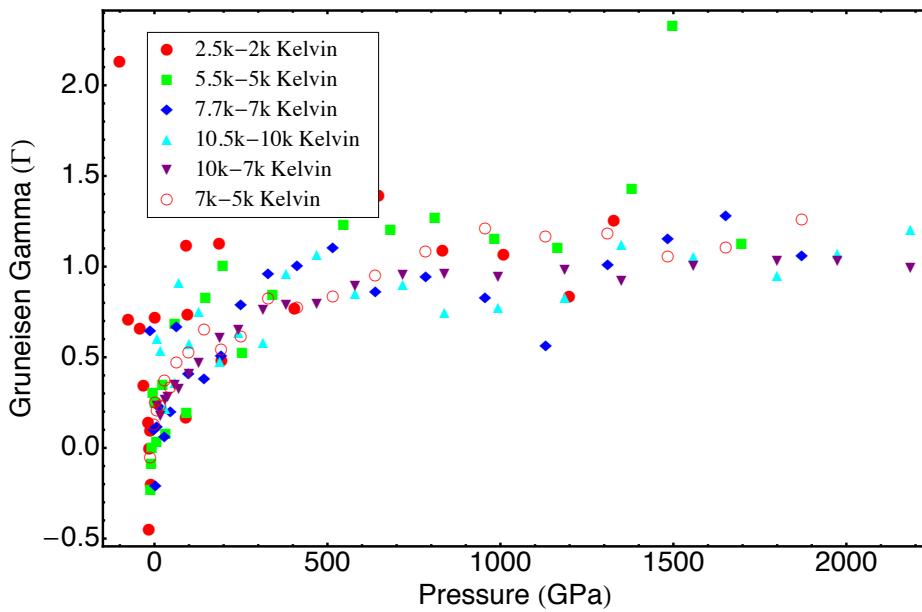


$$0 = \left(E - E_{solid} - \delta \left[\frac{V_{initial}}{V_{solid}} - 1 \right] \right) - \left(\frac{P + P_{solid}}{2} \right) (V_{initial} - V)$$



Values for the Gruneisen Γ Extracted from DFT

- ◆ We can extract trends for Γ
- ◆ Γ is not constant as a function of density
- ◆ Γ is constant as a function of pressure at higher pressure
- ◆ Γ is constant as a function of temperature





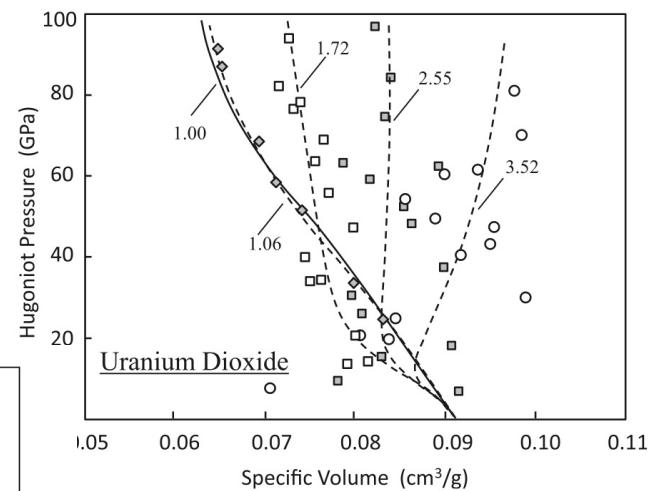
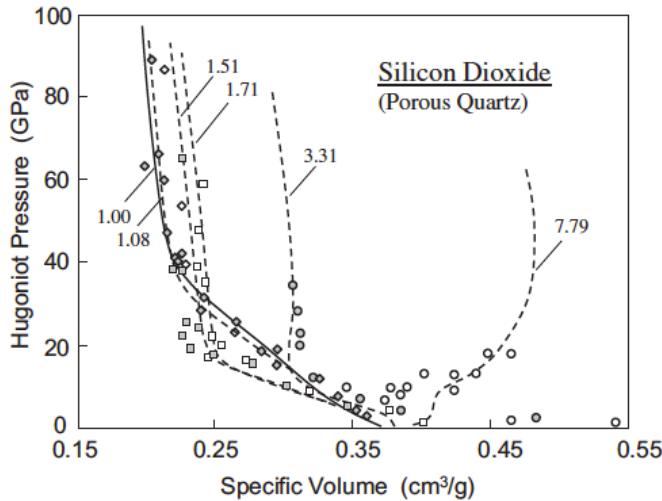
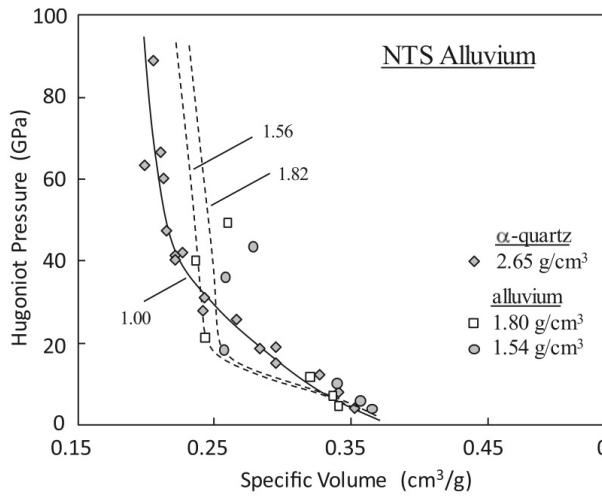
- **Introduction to Shock and High-Pressure Physics**
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- **Closure and Acknowledgements**



Porosity Enhanced Densification Observed in Some Porous Ceramics

Some porous material can reach higher densities than the fully-dense form shocked to the same pressure

Grady et al. proposed that void collapse can cause phase transformations to occur at lower pressure due to enhanced shear stresses





Molecular Dynamics (NEMD) Methodology

Solve Newton's equations

$$m_i \frac{d^2 \mathbf{r}_i}{dt^2} = \mathbf{F}_i$$

$$\mathbf{F}_i = -\nabla V_i$$

Mathematical Formulation

Classical Mechanics

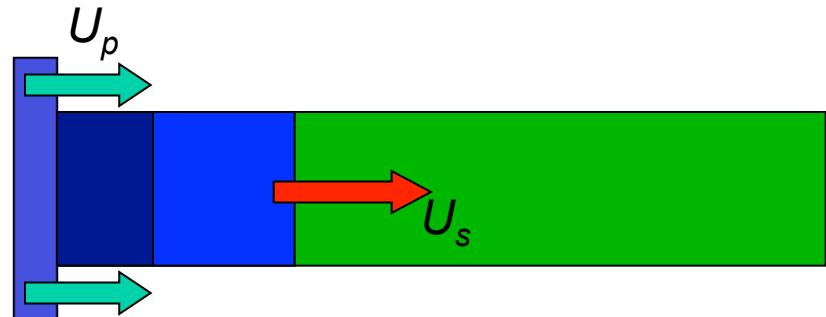
Atoms are Point Masses: $\mathbf{r}_1, \mathbf{r}_2, \dots, \mathbf{r}_N$

Positions, Velocities, Forces: $\mathbf{r}_i, \mathbf{v}_i, \mathbf{F}_i$

Potential Energy Function = $V_i(\mathbf{r}^N)$

Sandia's LAMMPS code is spatially parallel

Large-scale Atomic/Molecular Massively Parallel Simulator



Warm piston driving into 300 K single-crystal Silicon along $\langle 111 \rangle$ and $\langle 100 \rangle$

Systems $13.1 \times 13.1 \times 320 \text{ nm}^3$ and periodic

Timescales 60 to 150 ps

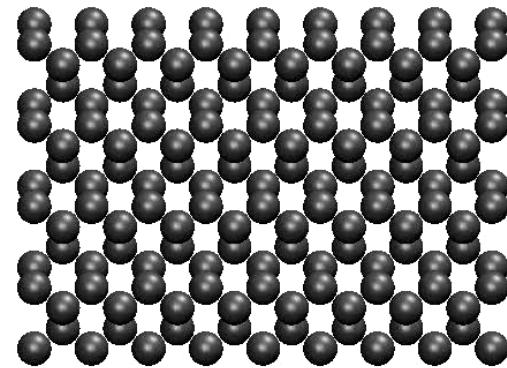
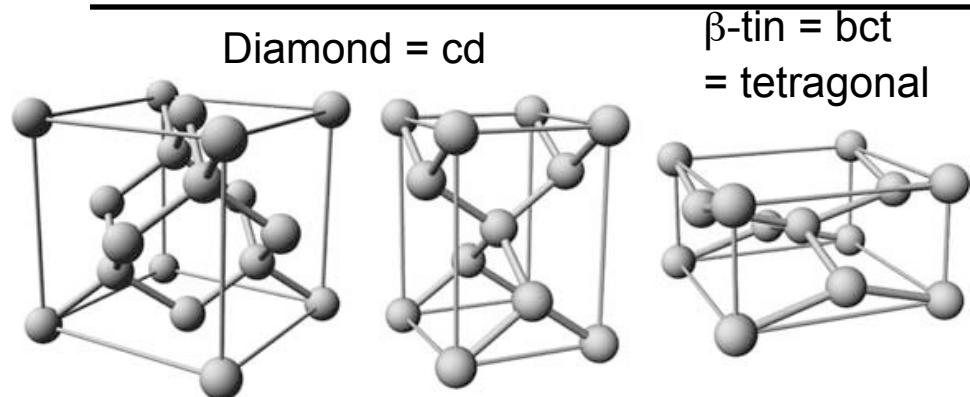
Modified Embedded Atom Method (MEAM) of M. I. Baskes et al.

- Uses a two-body and environment dependent term.

Voids are introduced either by carving out atoms from a single crystal, or by building up polycrystals from nano-grains

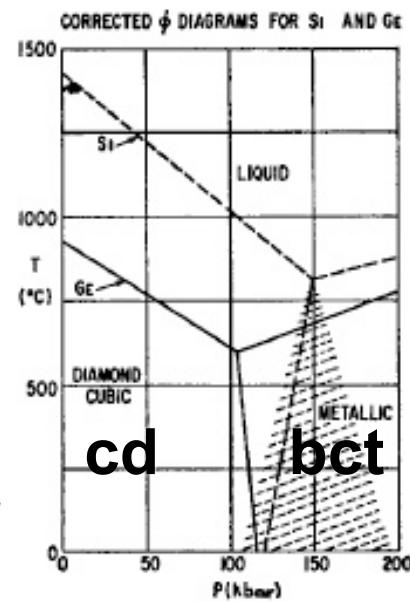
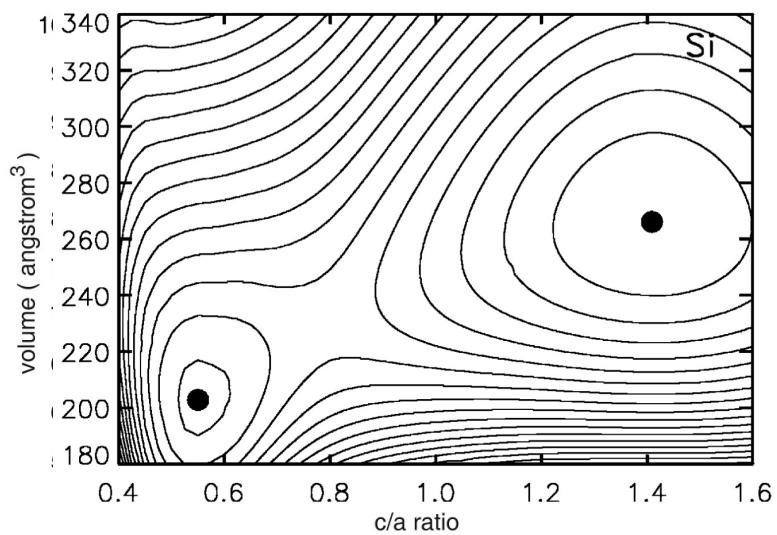


Silicon as a Model System



DFT

Gaal-Nagy, et al., Comp. Mat. Sci., 30, 1



Bundy, J. Chem Phys., 41, 3809

Silicon goes through a low temperature solid-solid phase transition from diamond to tetragonal in molecular dynamics simulation.

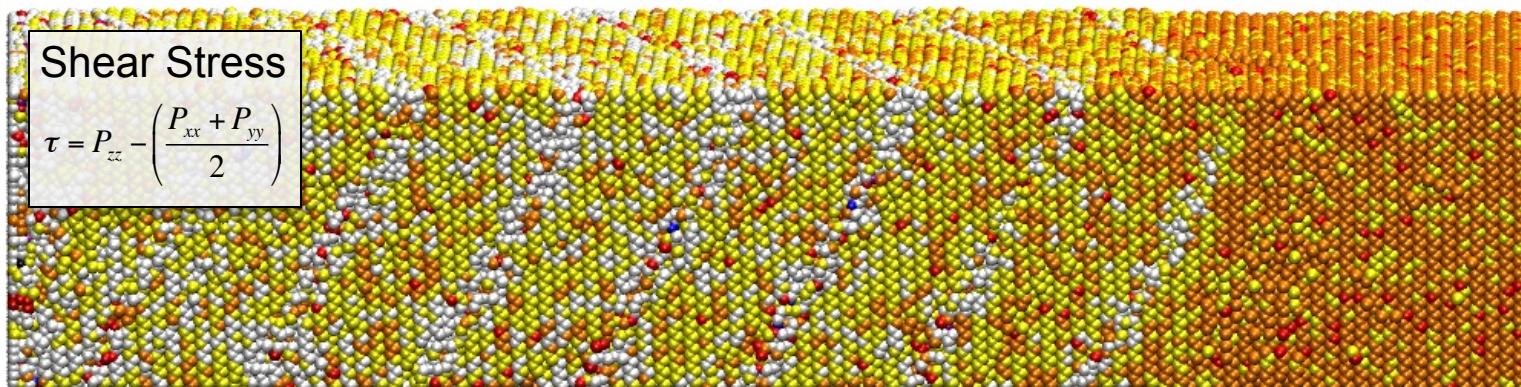
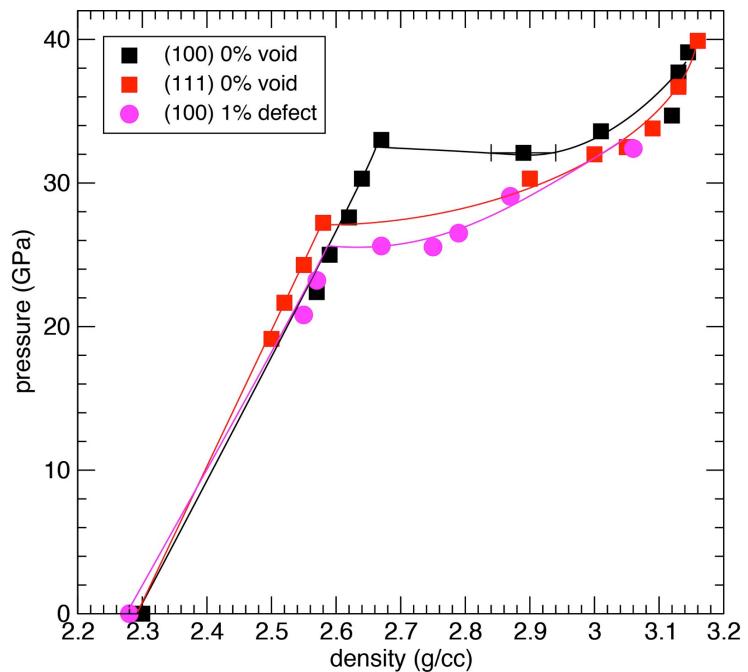
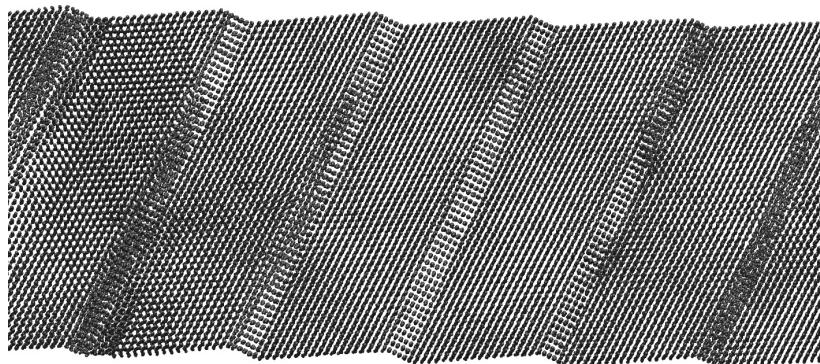
Voids can be introduced through helium implantation and annealing



Fully-Dense Silicon Undergoes a Partial Phase Transition

Silicon is an important covalent solid known to undergo a solid-solid phase transition.

Recent work in germanium and silicon has shown a shear-induced transition from diamond (cd) to a tetragonal (bct) phase is observed in MD simulation.

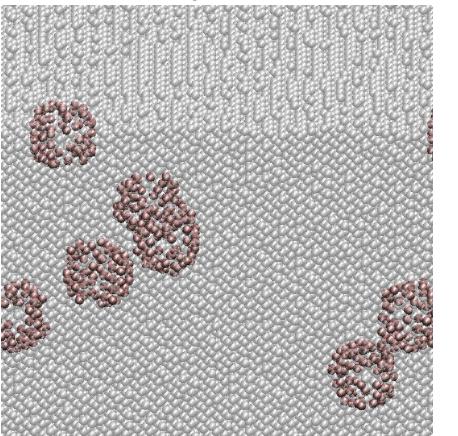




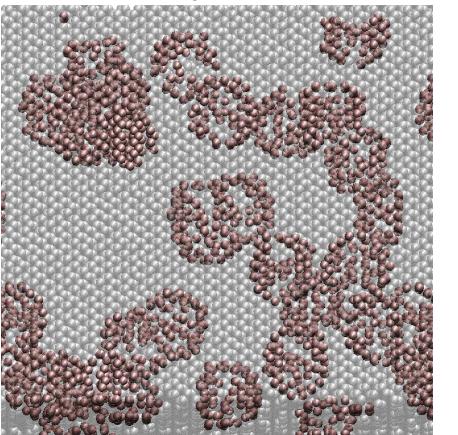
Low Porosity Silicon Behaves Like Silicon with Defects

Low porosity systems created by cutting randomly spaced 1 nm diameter spherical voids from single-crystal silicon.

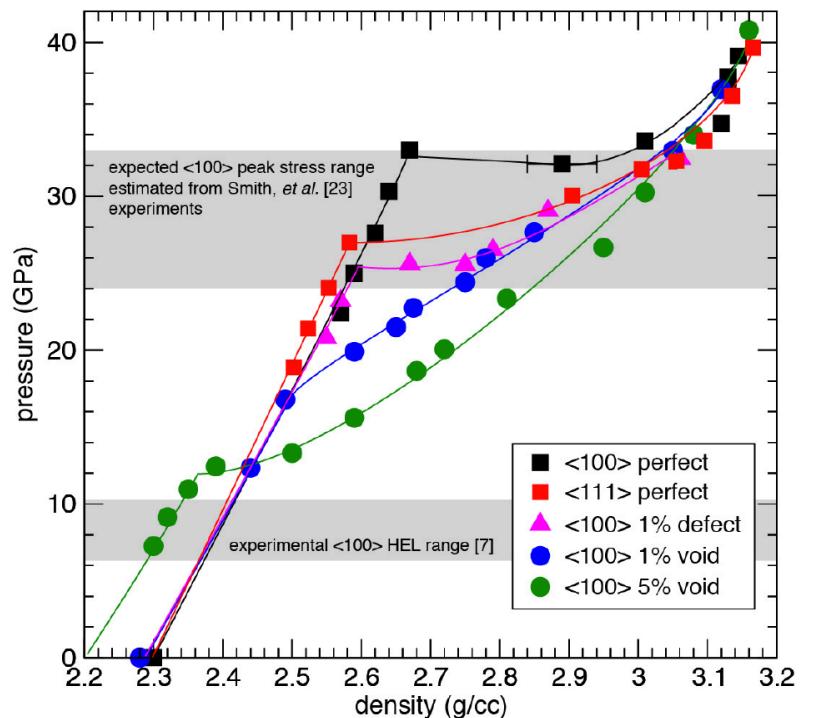
1% porosity: (left) cut voids



5% porosity: cut voids



Hugoniot density rises at lower pressure as seen in experiments, then joins the principal Hugoniot at higher pressures.



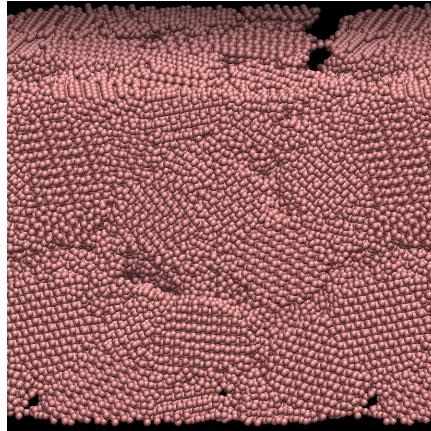
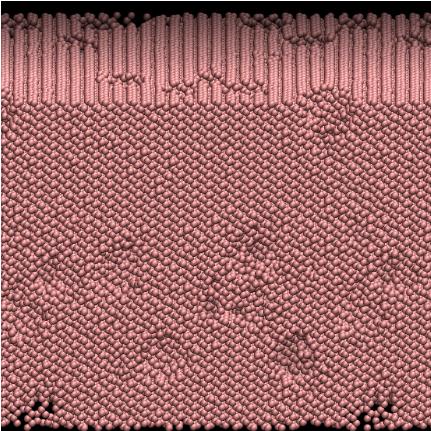


High Porosity Silicon Displays

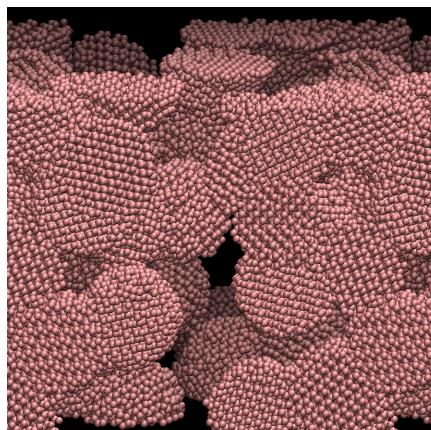
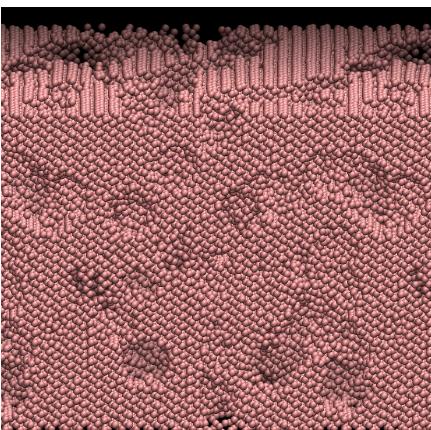
Porosity Enhanced Densification

High porosities are made by cutting 1 nm spherical voids from single crystal, or as a polycrystal of 4 nm spherical grains, w/ overlap removal, and annealing.

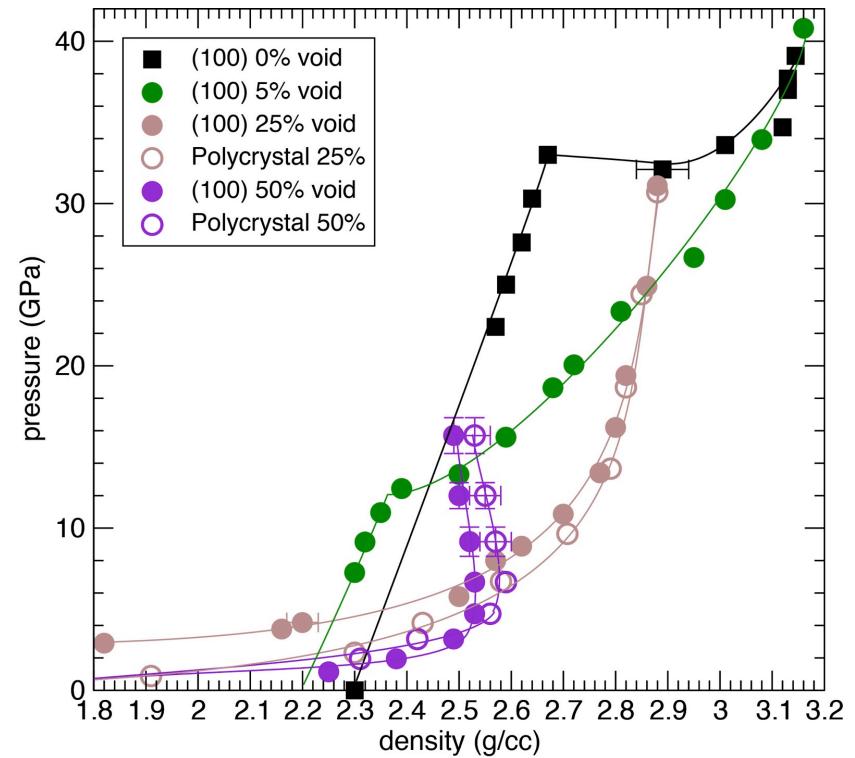
25% porosity: (l) cut voids, (r) polycrystal spheres



50% porosity: (l) cut voids, (r) polycrystal spheres



The Hugoniot density quickly collapses in the polycrystal, and slightly more slowly in the void-cut single crystal before rising steeply due to heating from rapid void collapse.



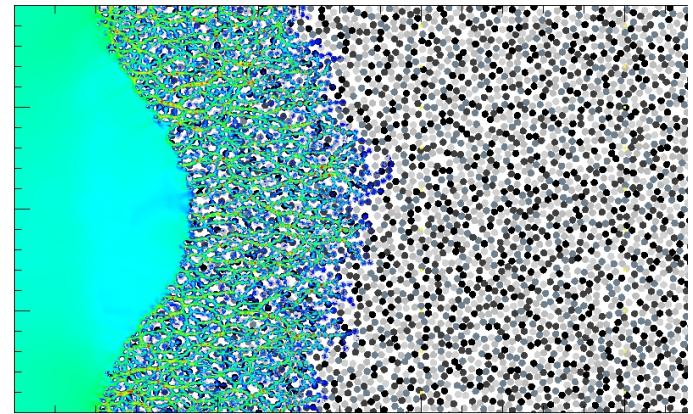
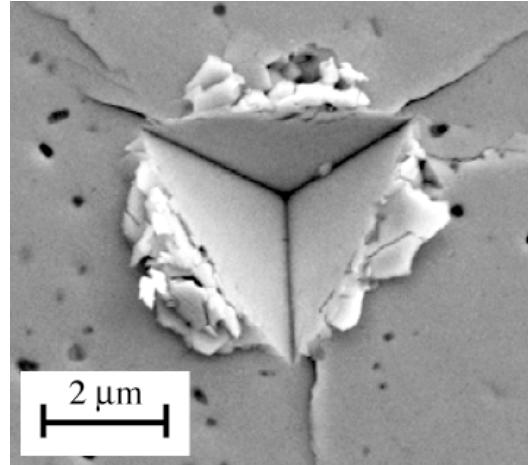
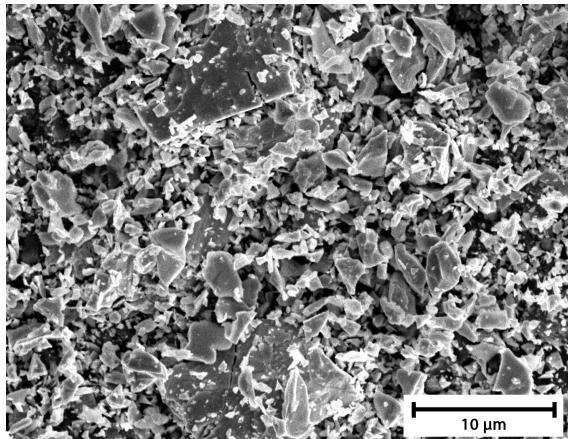
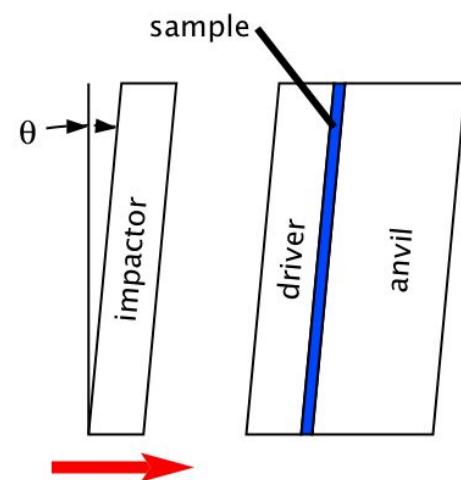


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Topics Not Covered

- pressure-shear loading and other approaches for measuring strength
- role of particle fracture
- mesoscale modeling
- EOS for granular materials and mixtures in the high-pressure regime
- perturbation decay experiments





Acknowledgements

J.P. Borg, C. Lammi, J. Foster - mesoscale modeling

M. Lane - molecular dynamics modeling

K. Cochrane, P. Weck, L. Shulenburger - DFT

**W.D. Reinhart, T.F. Thornhill, J. Martinez, R. Palomino,
H. Anderson - STAR facility gas gun experiments**

**Z - the large crew for design, assembly and operations;
S. Root, R. Lemke, M. Knudson for design & analysis**

D. Sandoval, K. Lappo - validation experiments

T. Buchheit - nanoindentation

**J.R. Asay, L.C. Chhabildas, D.E. Grady - decades of
shock physics experience**