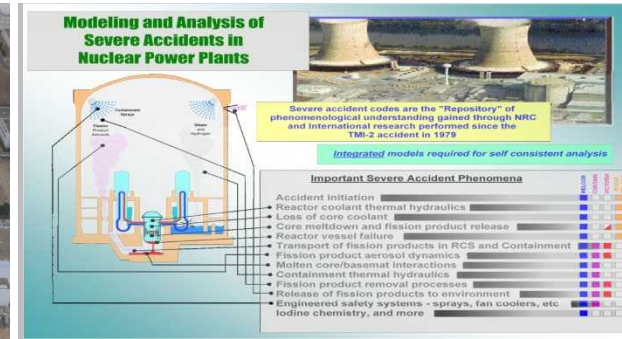


Exceptional service in the national interest



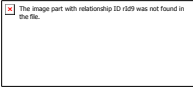
Source: Tokyo Electric Power Company



RCIC Operation in Fukushima Accidents as Modeled by MELCOR and Proposed Testing

R.O. Gauntt - Sandia National Laboratories
Presented at the BWR Owners Group General Meeting
Key West, Florida
October 7-8, 2014

Topics for discussion



- Background
- Key observations from Forensics Analyses of Fukushima Accidents
- Modeling RCIC water ingestion and equipment functioning in real-world accidents
- Proposed path forward

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Fukushima Daiichi Accident Study (Status as of April 2012)

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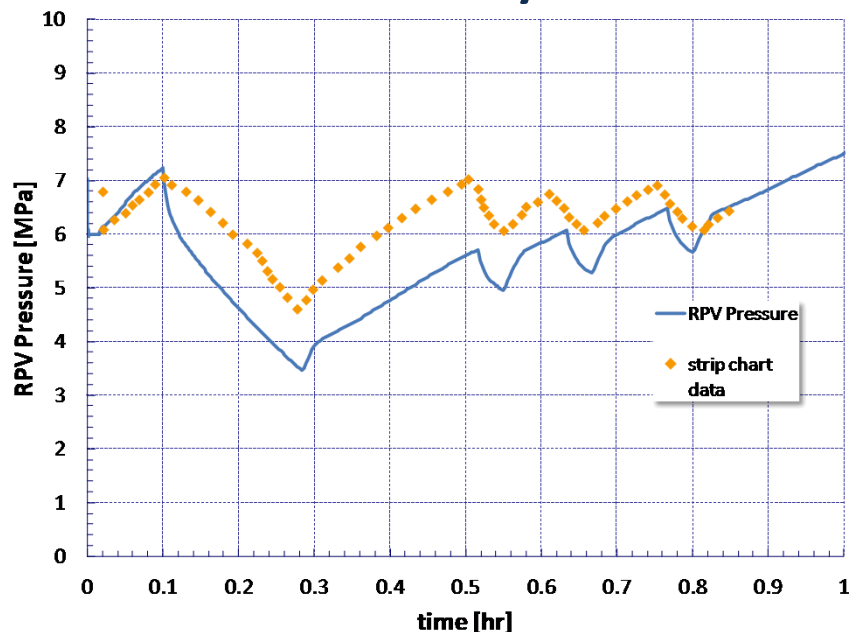


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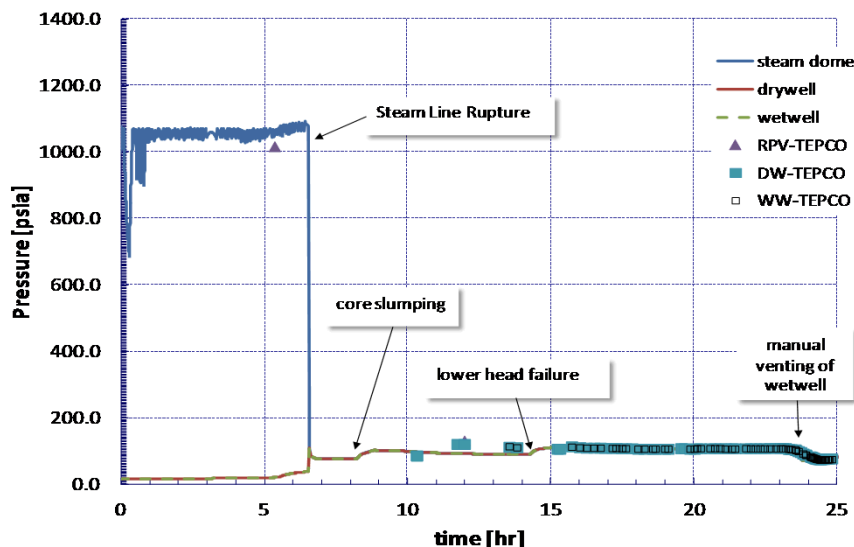
- Sandia commissioned by DOE to conduct forensics analyses of Fukushima accidents using MELCOR severe accident analysis code
- Comparison to pre-Fukushima analyses of SBO in Peach Bottom strikingly similar
- However, important differences observed in key areas
 - RCIC in particular

MELCOR Analysis of Fukushima Unit 1

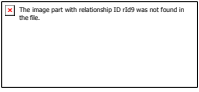
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- Prior to tsunami and loss of AC/DC
 - Isolation condensers cooling reactor
 - First two IC's then one
 - Exceeding cooldown rate of 100F/hr – too conservative?
- SBO at ~1 hour due to tsunami
 - Loss of control of functioning IC's
 - IC return valve closed
 - Loss of decay heat removal
- Core damage at ~4 hours
- MSL rupture at ~ 6.5 hours
 - Or SRV gasket failure
- Core slumping by ~8 hours
- Lower head failure ~12.5 hours

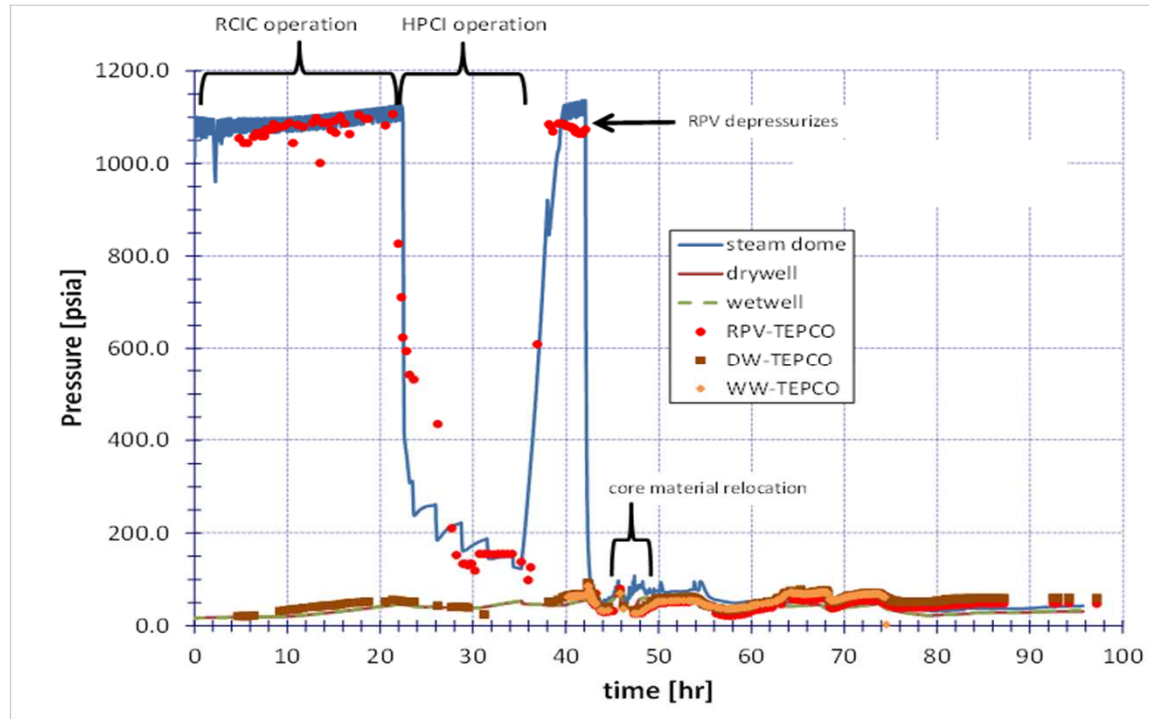
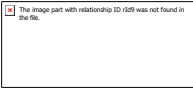


Fukushima Lessons Learned: Unit 1



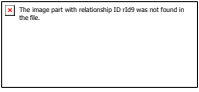
- Isolation condenser was functioning and cooling reactor
 - Operators were cycling IC on and off to avoid cooldown rate exceeding 100 F/hr
 - IC “caught “ in off-position when tsunami flooding disabled DC power
 - Tech Spec cooldown of 100F/hr may be over-conservative – should be re-evaluated
- Unit 1 accident could *perhaps* have been avoided had IC been operating
 - Operators would have to refill IC secondary HX shell
- Potential Industry Response
 - Relax cooldown limits to preserve essential cooling capability (keep IC operating) – *needs evaluation*
 - Make IC easier to actuate with loss of power

MELCOR Analysis of Unit 3



- Unit 3 maintained DC power
 - Active control of RCIC
- RCIC starts level control – runs 21 hours
 - Beyond most current SBO coping times
- RCIC shuts down automatically on high turbine exhaust pressure
 - Automatic system protection
 - Otherwise functioning injection system cannot be restarted
- HPCI is started
 - System run continuously using test line to recirculate water and avoid cycling HPCI on/off
 - Deep depressurization of RPV results
 - After 28 hours HPCI injection is ineffective
 - HPCI stops after ~35 hours
- Core damage underway prior to system depressurization
- Unit 3 probably worst damaged of units

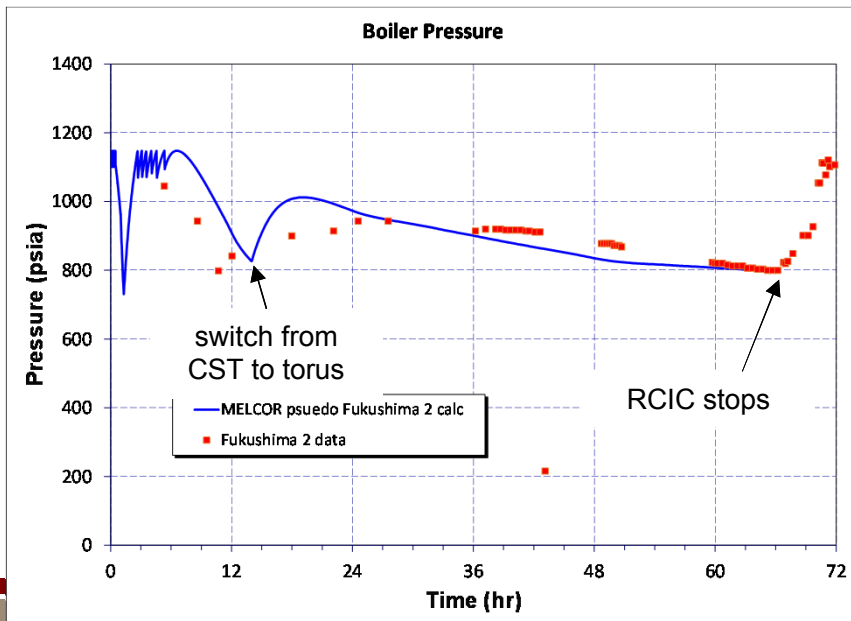
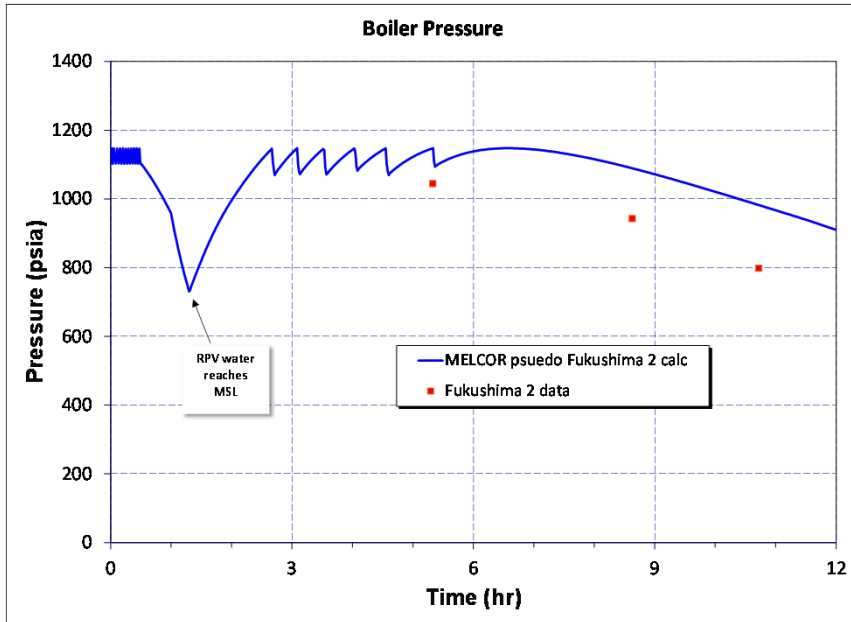
Fukushima Lessons Learned: Unit 3



- RCIC and HPCI were both operational due to DC availability
 - RCIC ran for 21 hours before shutting down on high turbine exhaust signal
 - RCIC and HPCI have numerous automated shutdown criteria to protect turbine and pump
 - HPCI started up but created such extreme RPV depressurization that HPCI pump was not injecting water
 - Core uncovering and early damage occurring as HPCI manually stopped
- Core damage could *perhaps* have been prevented had RCIC not automatically shut itself down
- Possible Industry Response
 - Disable some auto shutdown features in extended ELAP to keep critical equipment operating
 - Better understand operational capabilities of RCIC/HPCI under beyond design basis circumstances

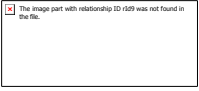
MELCOR Analysis of Unit 2 RCIC

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- First 45 minutes RCIC operates normally
- Arrival of tsunami results in loss of AC/DC power
 - RCIC runs uncontrolled (full open)
 - RPV pressure drops until water level reached main steam line (MSL)
 - Water carryover into RCIC turbine degrades performance and RPV heats up
- RCIC operates in self-regulating cyclic mode thereafter
 - RPV water level maintained near MSL with cyclic water ingestion and subsequent clearing
- MELCOR model was developed to account for water ingestion
- Long term pressure trends captured
- RCIC runs for nearly three days
- Eventual shutdown thought due to turbine over-speed
 - Pump cavitation?

Fukushima Lessons Learned: Unit 2



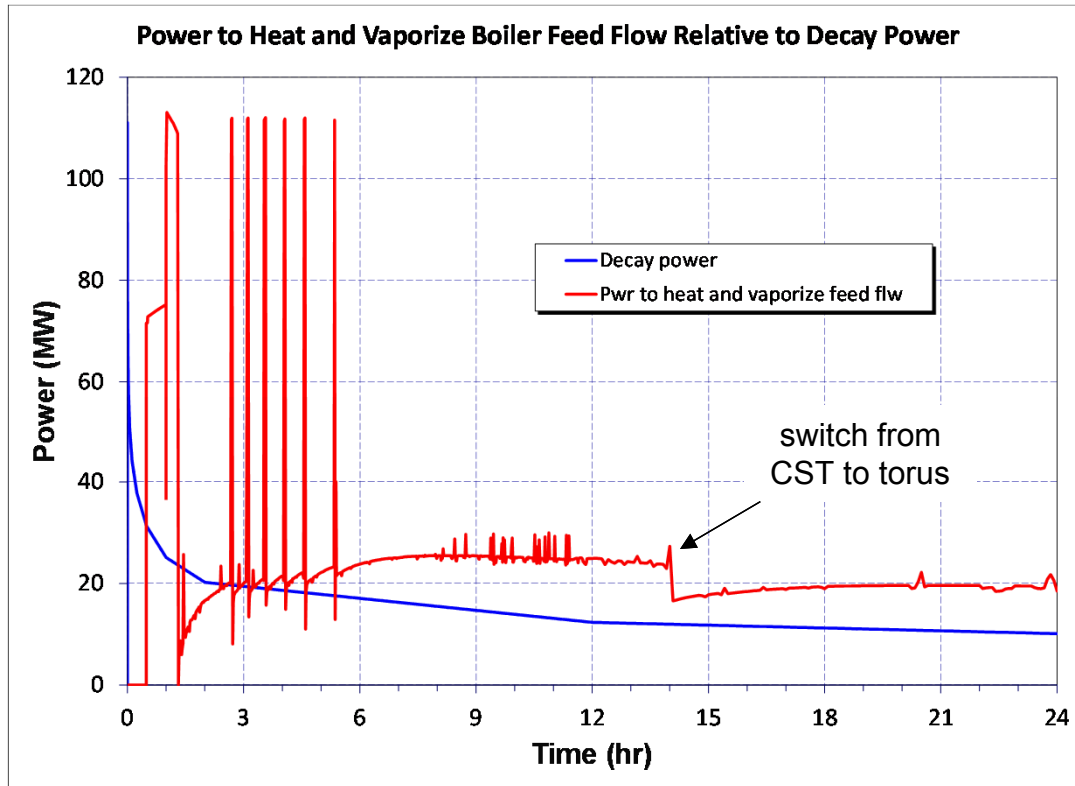
- RCIC operating at time of loss of power and continued to operate
 - Turbine governor opens fully
 - Electrical shutdown interlocks non-functional due to loss of DC: especially high RPV water level shutdown
 - Water level rose to top of steam lines by 1.5 hours producing liquid water ingestion by RCIC turbine
- RCIC ran for 72 hours running in uncontrolled mode
 - Water carryover did not shut down turbine
 - That's because the Terry Turbine design is *really robust*
- RCIC termination likely by cavitation-induced over-speed trip
 - Suppression pool saturation may have eventually led to pump cavitation and turbine over-speed trip (Mizokami 2013 TEPCO)
- System protection interlocks were defeated by loss of DC allowing RCIC to remain in service

Observations

- RCIC system ubiquitous at BWR installations world-wide
 - And widely used in PWR Aux Feed systems
- RCIC system more robust than previously credited
 - PRA and safety studies assume RCIC failure with loss of batteries after 4 to 8 hours – coping times short
- Post-Fukushima NRC Rulemaking will require extension of coping time considerably
- Existing RCIC system seems capable of extended operation even with loss of DC control
- Demonstrating extended RCIC operation under ELAP conditions can bridge gap between current coping times and FLEX implementation by 24 hours
- Propose full scale testing to demonstrate technical basis for extended RCIC operation

Power Requirements for Full Scale Testing

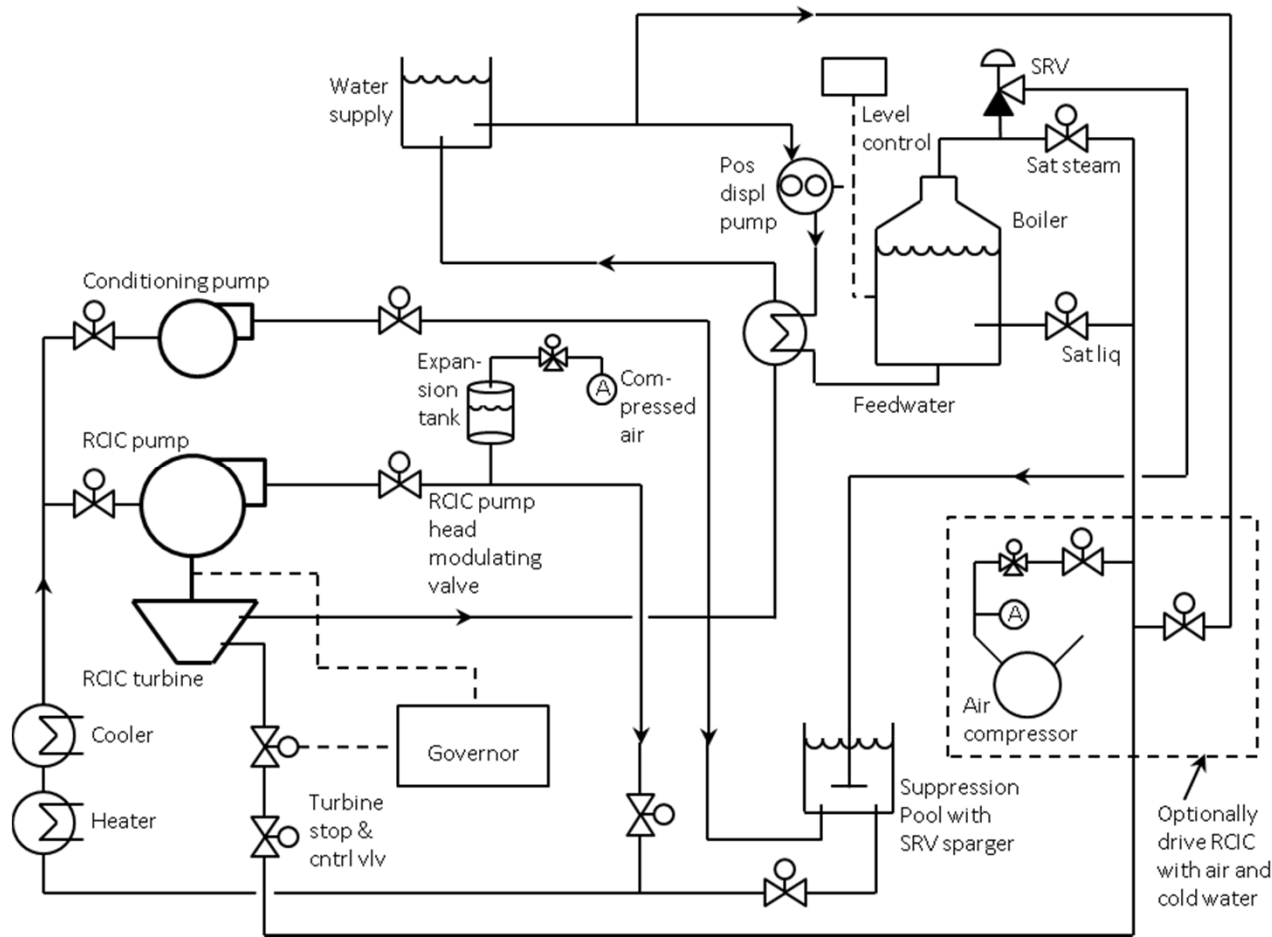
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- Normal RCIC energy requirements in MW range
 - 500 hp typical pump power
- Energy draw with water ingestion is considerably larger
 - Larger specific enthalpy of water carryover
- Steam/water system required to demonstrate operation under water ingestion is roughly decay heat levels
 - 20 to 30 MW

Conceptual Design for General Test Facility – 30MW Boiler

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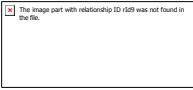


- Considers wide range of testing capability
 - Turbine
 - Pump
 - WW
 - SRV
- Simpler design can be made for RCIC only
- MELCOR model to be developed
- 30 MW facility under consideration

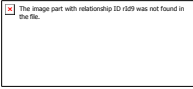
Objectives of RCIC Testing

(and other critical systems and components)

- Confirm self-regulating operational mode of RCIC
 - Early testing of RCIC response to “water slug” suggests RCIC not damaged
 - Operational characteristics need to be demonstrated
 - Effect of liquid water fraction in steam flow
 - Long-term RCIC operation needs to be demonstrated
- Potential scope of investigations
 - Operating pressure and water carry-over fraction
 - Pump head versus water carryover
 - Turbine speed and pump effectiveness (flow and head)
 - Potential response of interlocks in self-regulating mode
 - Response to turbine exhaust pressure and other environmental conditions



Potential Participants



- Department of Energy
- Industry and Owners Groups
- EPRI
- International – Japan Institute of Applied Energy/TEPCO
- SNL performing scoping studies on RCIC model development, Costs and Requirements
 - Facilities – existing or new ?, will assess situation.
 - FY-15 initial DOE funds (\$250K) for model/design development and test protocol
 - FY-16 to 19 TBD

Summary

- Fukushima analyses have revealed deep insights into real-world operation of critical systems
 - Currently too conservative assumptions of operational capabilities
- Capable cooling systems disabled by:
 - loss of DC (IC control in Unit 1)
 - Shutdown interlocks (*availability of DC* caused shutdown of Unit 3 RCIC)
 - Long term operability of RCIC under water ingestion conditions suggested by Unit 2 *due to loss of DC*
- RCIC system can potentially bridge gap between current coping times and FLEX implementation
 - Full scale testing can confirm technical basis
 - Analogous benefit likely for turbine-driven Aux feed in PWR's