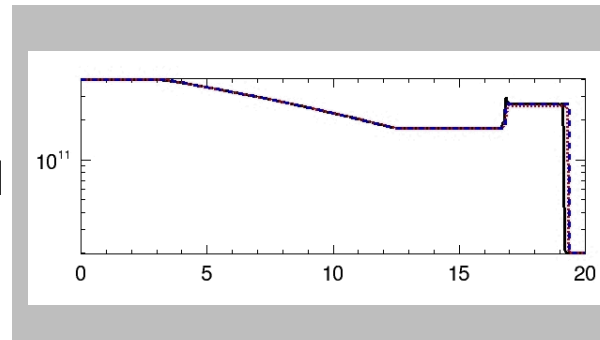
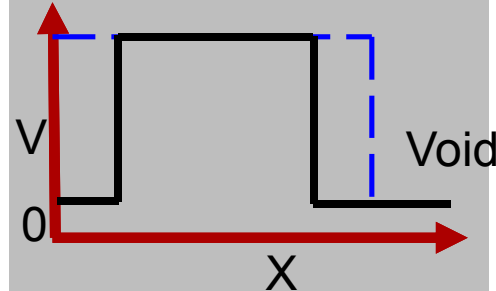
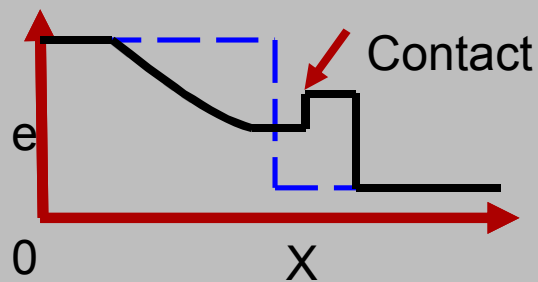


Exceptional service in the national interest

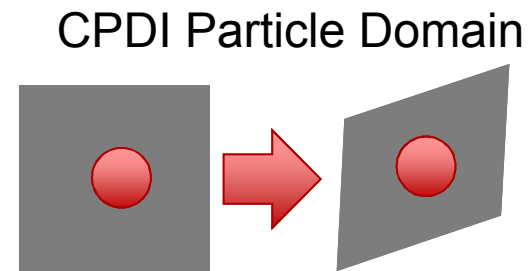


Current Status of the MPM in CTH

K. P. Ruggirello & S. C. Schumacher
8th MPM Workshop
Oregon State Univ. Corvallis, OR
Sept. 25th-26th, 2014

MPM and CTH

- MPM has been implemented into CTH at SNL
 - Joint effort with LANL, and Univ. Utah for CPDI* implementation
- On going verification of method has led to numerous bug fixes/improvements over the last year
- Majority of use cases involve shocks
 - Verification of shock response of MPM needed



*A. Sadeghirad, R. M. Brannon, and J. Burghardt, "A convected particle domain interpolation technique to extend applicability of the material point method for problems involving massive deformations," *International Journal for Numerical Methods in Engineering*, vol. 86, pp. 1435-1456, (2011).

Verification and Validation Problems Sandia National Laboratories

- Sod shock tube
 - Comparison with analytical solution for a variety of shock strengths
 - Initial discontinuity can be replaced with a material discontinuity
- 1D Flyer plate
 - Verification of shock response with material strength
 - Void interaction
- Taylor Anvil comparisons
 - Helps to validate material model response with method
- Breaking Dam
 - Identified as a good test problem by MPM community to show “popping” behavior
- MMS provides additional verification, but hard to implement currently in CTH

Verification and Validation Problems Sandia National Laboratories

- **Sod shock tube**

- Comparison with analytical solution for a variety of shock strengths
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- **1D Flyer plate**

- Verification of shock response with material strength
- Void interaction

- Taylor Anvil comparisons

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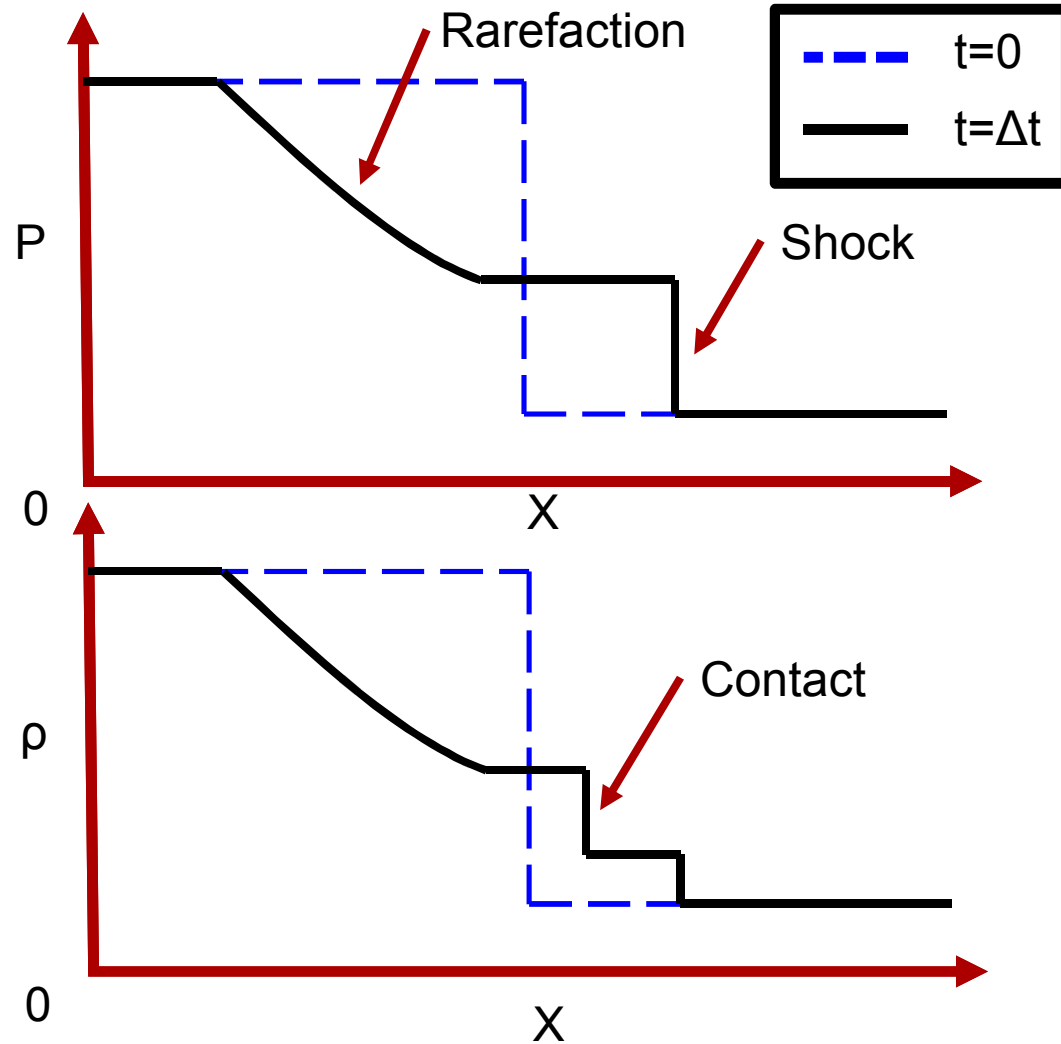
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- Identified as a good test problem by MPM community to show “popping” behavior

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Sod Shock Tube*: Analytical Soln.

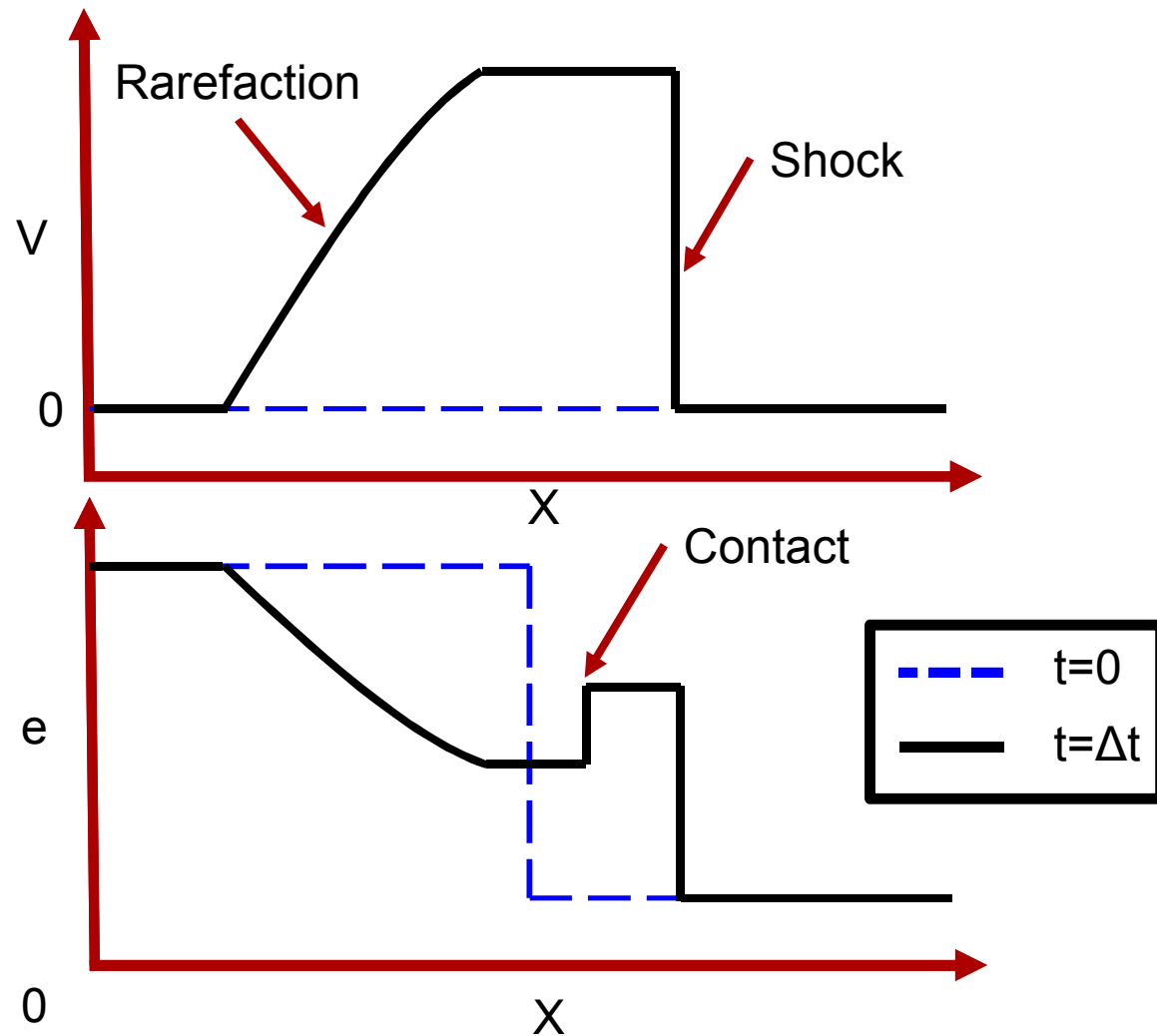
- Ideal gas
 - $\gamma=1.67$
 - $C_v=2.0E11 \frac{\text{erg}}{\text{g eV}}$
- 1024 cells
- 4 PPC



*Sod, G. A., "A Survey of Several Finite Difference Methods for Systems of Nonlinear Hyperbolic Conservation Laws", J. Comput. Phys. 27: 1-31 (1973).

Sod Shock Tube*: Analytical Soln.

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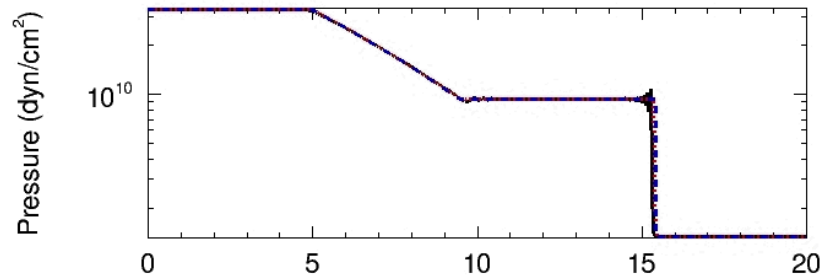
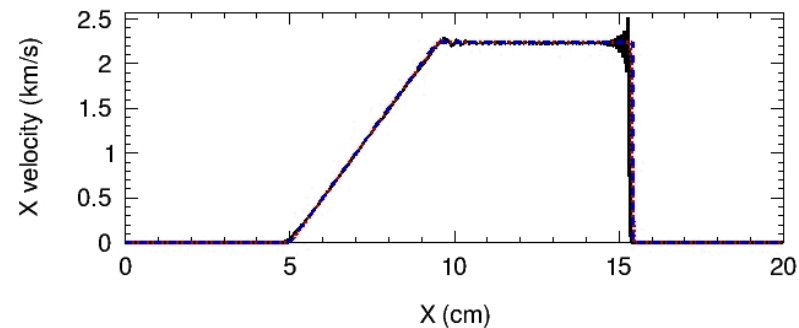
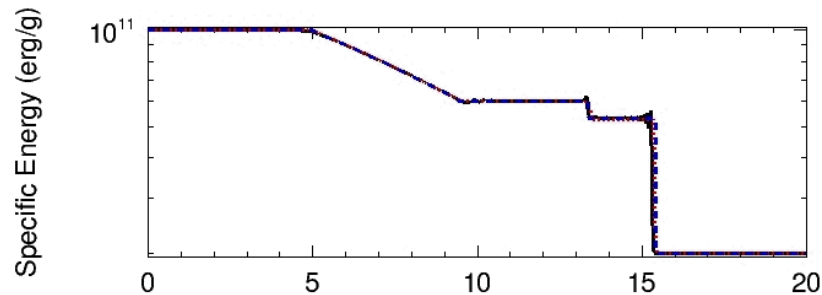
*Sod, G. A., "A Survey of Several Finite Difference Methods for Systems of Nonlinear Hyperbolic Conservation Laws", J. Comput. Phys. 27: 1-31 (1973).

Sod Shock Tube: FLIP Results

Weak Shock

Property	Left	Right
T (eV)	0.5	0.1
P (g/cm ³)	0.5	0.1

- FLIP result noisy across discontinuities

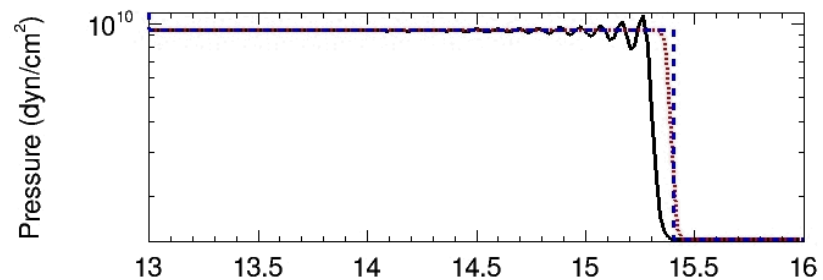
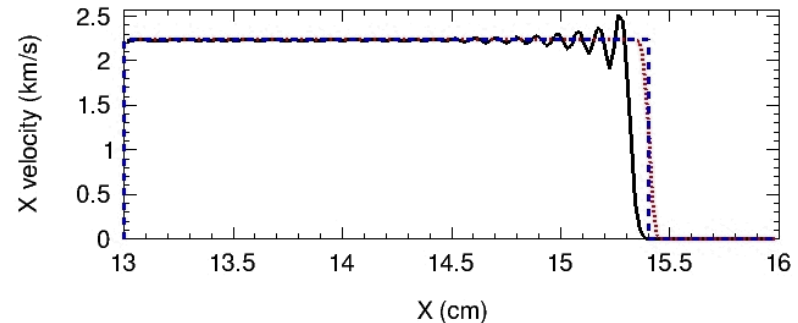
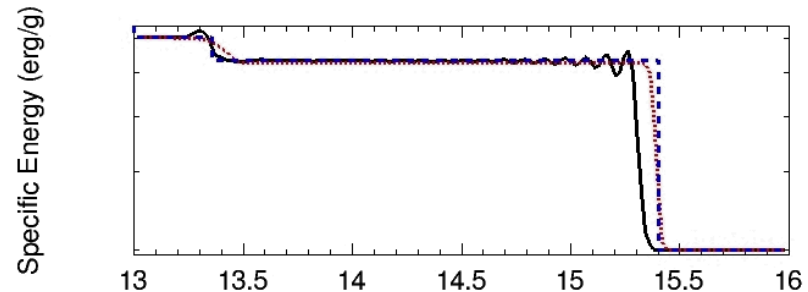


Sod Shock Tube: FLIP Results

Weak Shock

Property	Left	Right
T (eV)	0.5	0.1
P (g/cm ³)	0.5	0.1

- FLIP result noisy across discontinuities
- FLIP more diffusive than CTH solution
- FLIP shock speed slightly slower



FLIP at 1.501e-05 s.

CTH at 1.501e-05 s.

Analytical 8

Limited Artificial Viscosity*

- CTH solution not perfectly monotone across discontinuities
- Limited artificial viscosity implemented to introduce more diffusion and keep the solution monotone

$$\Delta u_{i+\frac{1}{2}} = \Delta t \frac{(P_i + Q_i) - (P_{i+1} + Q_{i+1})}{M_{i+\frac{1}{2}}}$$

$$Q_i = -\frac{1}{2} \rho_i (B_l \Delta u_i (1 - \phi) + B_q |\Delta u_i| \Delta u_i (1 - \phi^2))$$

$$\phi = \max(0, \min(\frac{1}{2}(R_L + R_R), 2R_L, 2R_R, 1))$$

$$R_L = \frac{\partial u}{\partial x_L} \bigg/ \frac{\partial u}{\partial x_C} \quad R_R = \frac{\partial u}{\partial x_R} \bigg/ \frac{\partial u}{\partial x_C}$$

$$\frac{\partial u}{\partial x_L} = \frac{u_{i-\frac{1}{2}} - u_{i-\frac{3}{2}}}{x_{i-\frac{1}{2}} - x_{i-\frac{3}{2}}} \quad \frac{\partial u}{\partial x_R} = \frac{u_{i+\frac{3}{2}} - u_{i+\frac{1}{2}}}{x_{i+\frac{3}{2}} - x_{i+\frac{1}{2}}} \quad \frac{\partial u}{\partial x_C} = \frac{u_{i+\frac{1}{2}} - u_{i-\frac{1}{2}}}{x_{i+\frac{1}{2}} - x_{i-\frac{1}{2}}}$$

- See R. B. Christensen* for corresponding energy term
- D_L, D_R are left and right divergences of \mathbf{u}
- $B_l=0.167$ $B_q=0.667$ for CTH staggered mesh

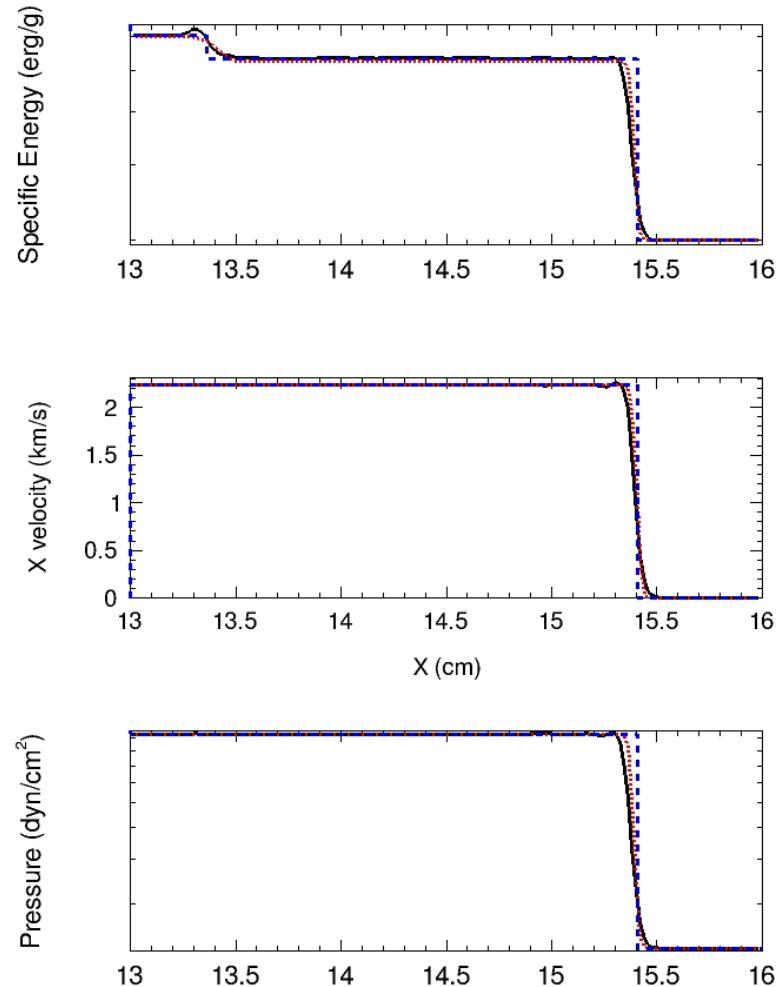
*R. B. Christensen, "Godunov Methods on a Staggered Mesh – An Improved Artificial Viscosity", UCRL-JC-105269, LLNL (1990).

Sod Shock Tube: FLIP Results

Weak Shock

Property	Left	Right
T (eV)	0.5	0.1
P (g/cm ³)	0.5	0.1

- Using limited artificial viscosity removes oscillations at shock
- Shock speed comparable to CTH
- FLIP solution 2-3 cells more diffusive than CTH



FLIP at 1.502e-05 s.

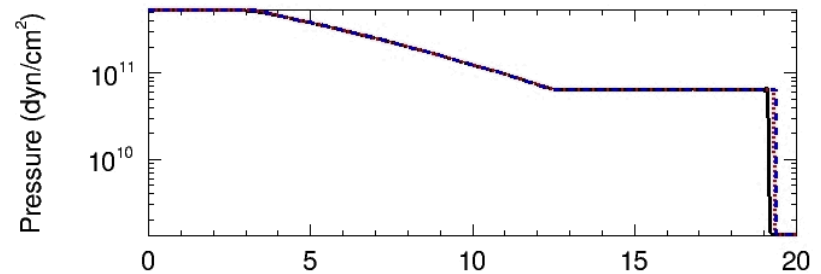
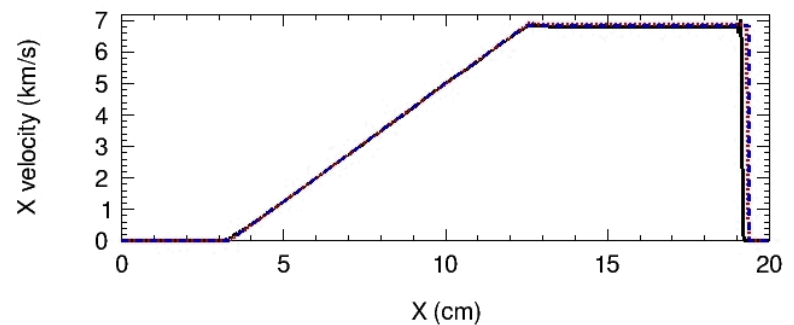
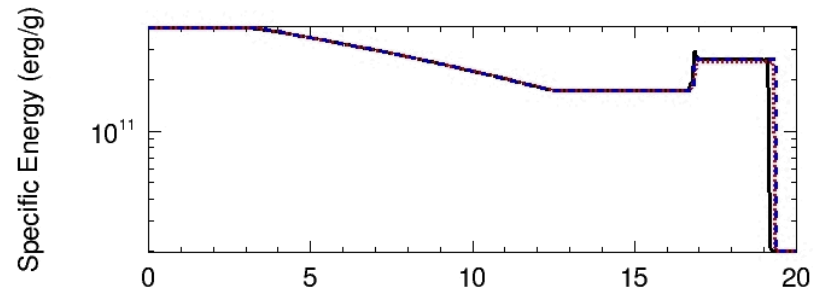
CTH at 1.501e-05 s.

Analytical

Sod Shock Tube: FLIP Results

Strong Shock		
Property	Left	Right
T (eV)	2.0	0.1
P (g/cm ³)	2.0	0.1

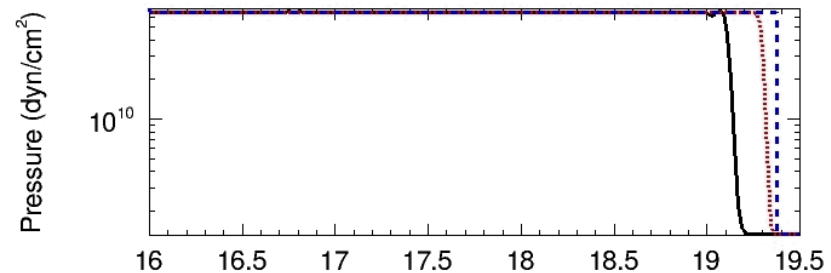
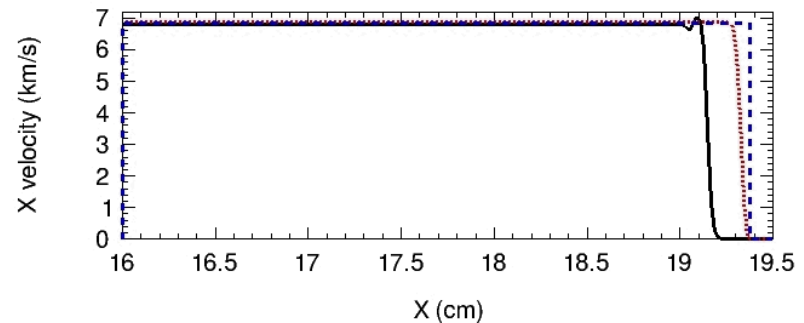
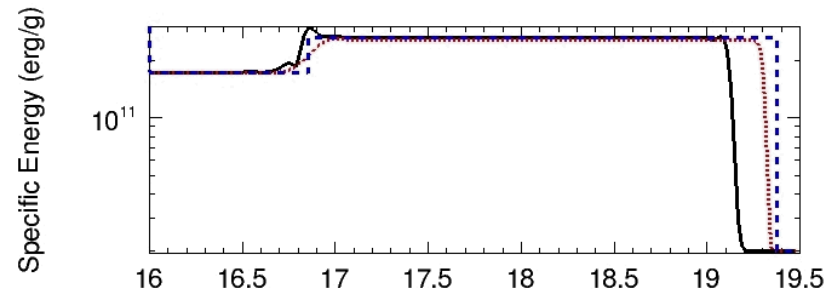
- Need limited artificial viscosity to get solution
 - Oscillations produce negative densities
- FLIP shows oscillations at discontinuities



Sod Shock Tube: FLIP Results

Strong Shock		
Property	Left	Right
T (eV)	2.0	0.1
P (g/cm ³)	2.0	0.1

- Need limited artificial viscosity to get solution
 - Oscillations produce negative densities
- FLIP shows oscillations at discontinuities
- FLIP Shock speed slower than CTH
- “Odd” oscillation at contact surface



FLIP at 1.000e-05 s.

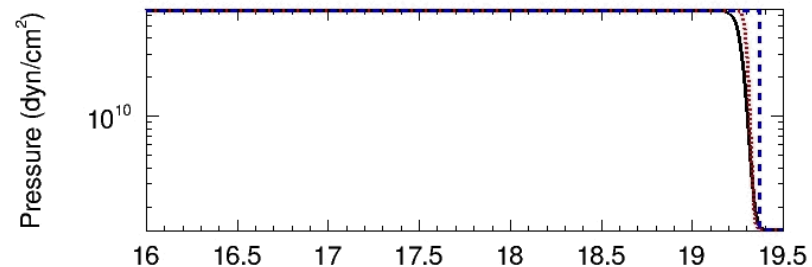
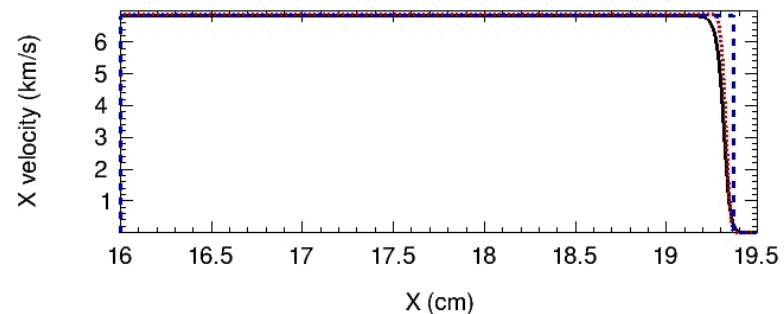
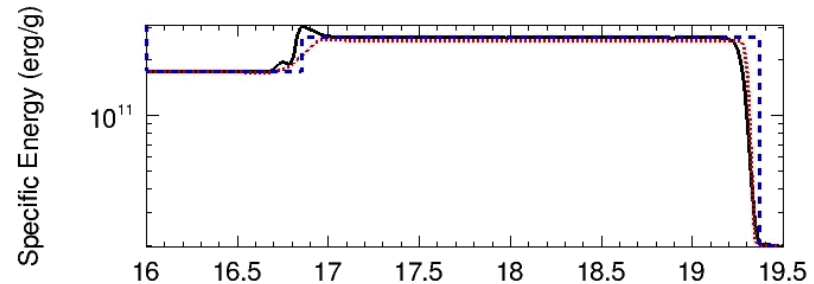
CTH at 1.000e-05 s.

Analytical

Sod Shock Tube: FLIP Results

Strong Shock		
Property	Left	Right
T (eV)	2.0	0.1
P (g/cm ³)	2.0	0.1

- Increasing B_q from 0.667 to 1 removes oscillations at shock
- Shock speed comparable to CTH with increased B_q
- “Odd” oscillation at contact surface
- CPDI did not improve solution significantly



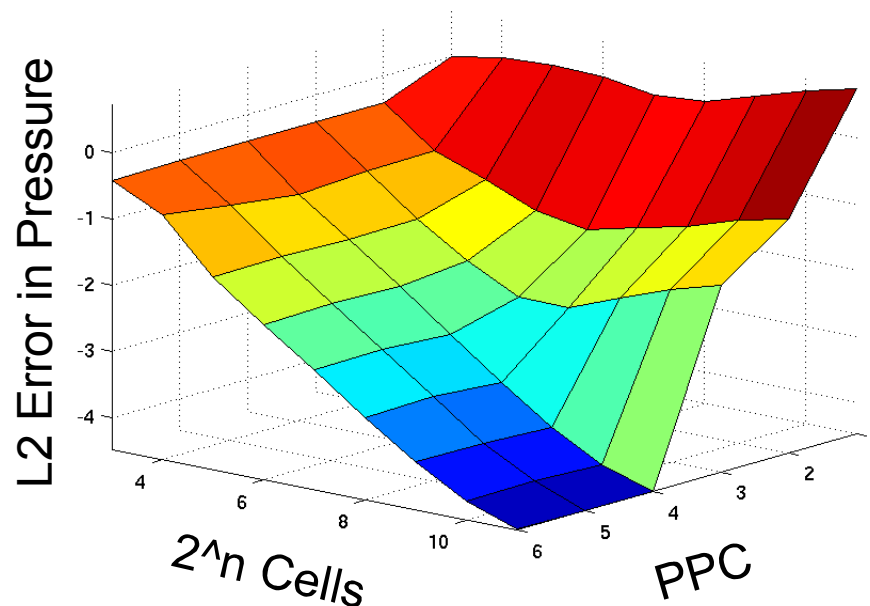
FLIP at 1.000e-05 s.

CTH at 1.000e-05 s.

Analytical

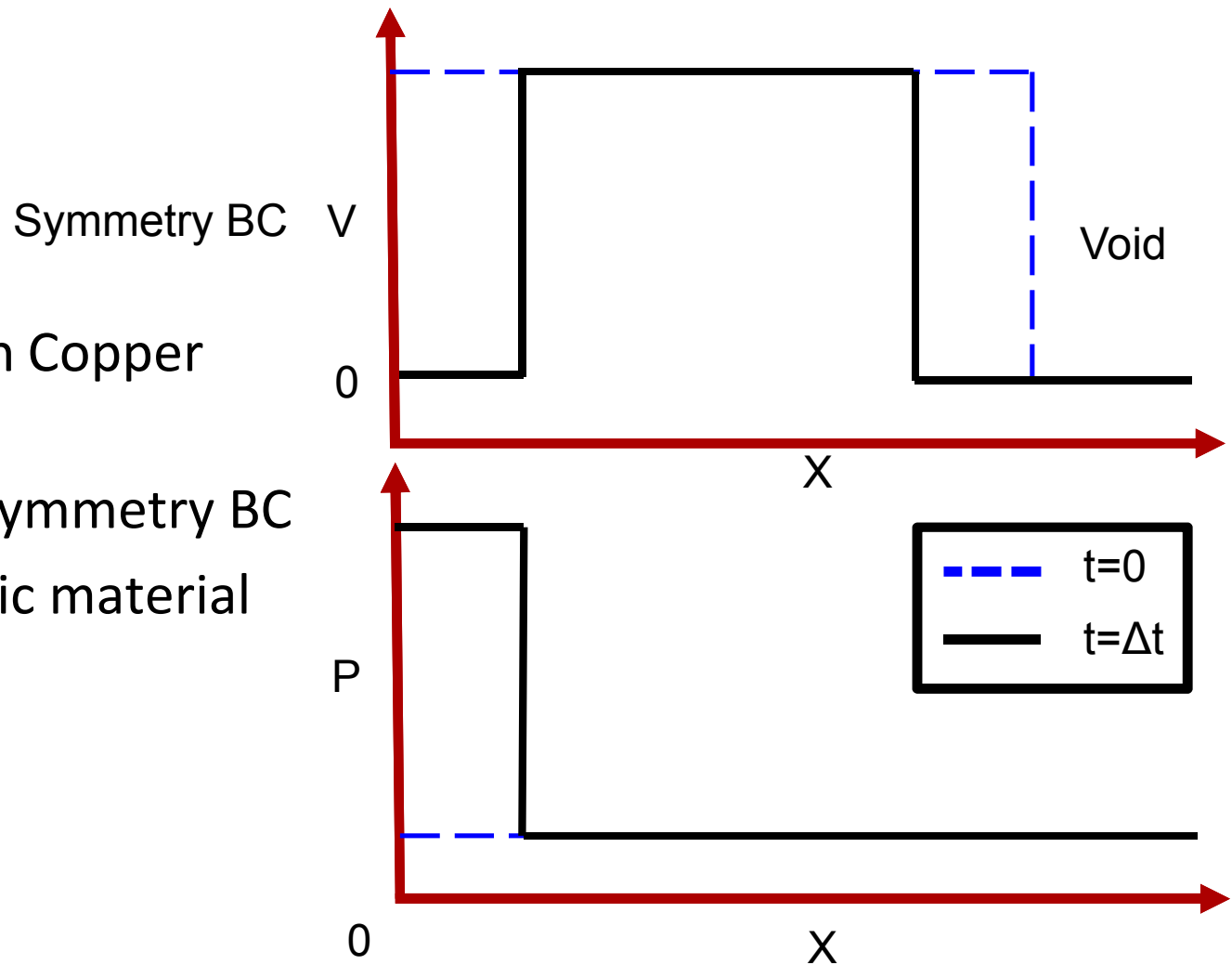
Sod Shock Tube: Convergence

- Convergence based on L2 norm found to be approximately 0.55 for both CTH and FLIP
- FLIP showed no convergence for PPC of 1-3
- PPC 4 and above converged
- Higher PPC than 4 did not show better convergence



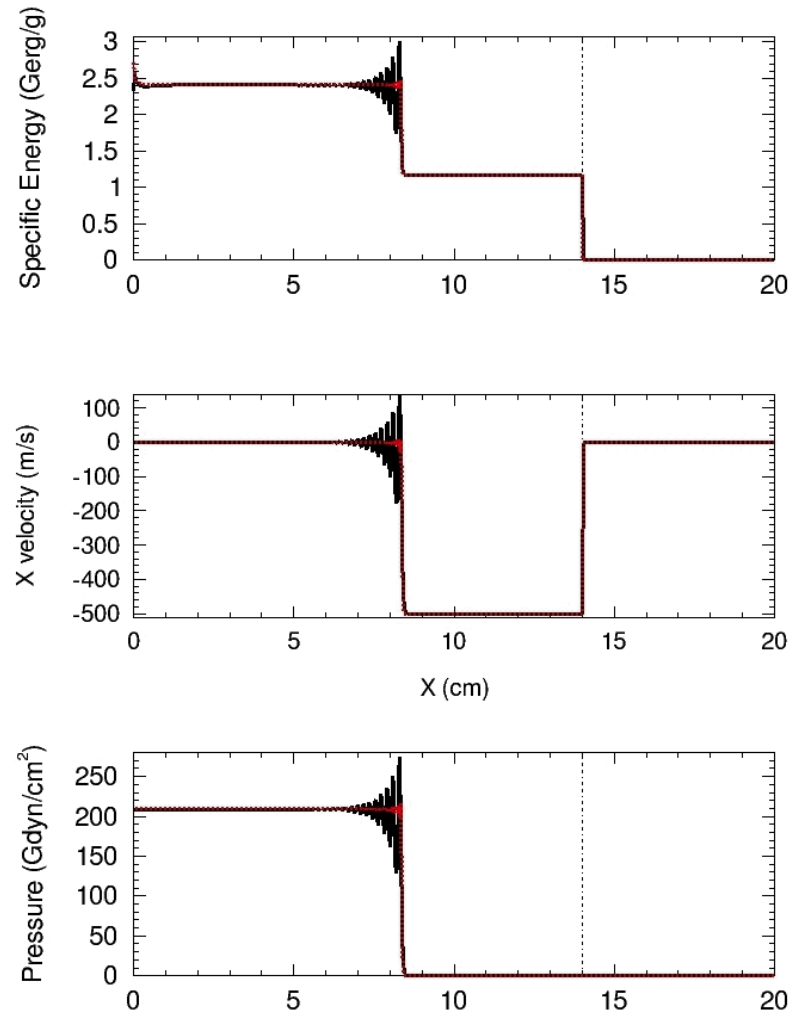
Flyer Plate: Problem Setup

- Mie-Gruneisen Copper EOS
- 500 m/s into symmetry BC
- Perfectly elastic material model
- 1024 cells
- 4 PPC



Flyer Plate: MPM Results

- CTH solution not monotone
- Oscillations amplified for MPM at shock
- Shock speed the same for CTH and MPM, within 1% of analytical solution

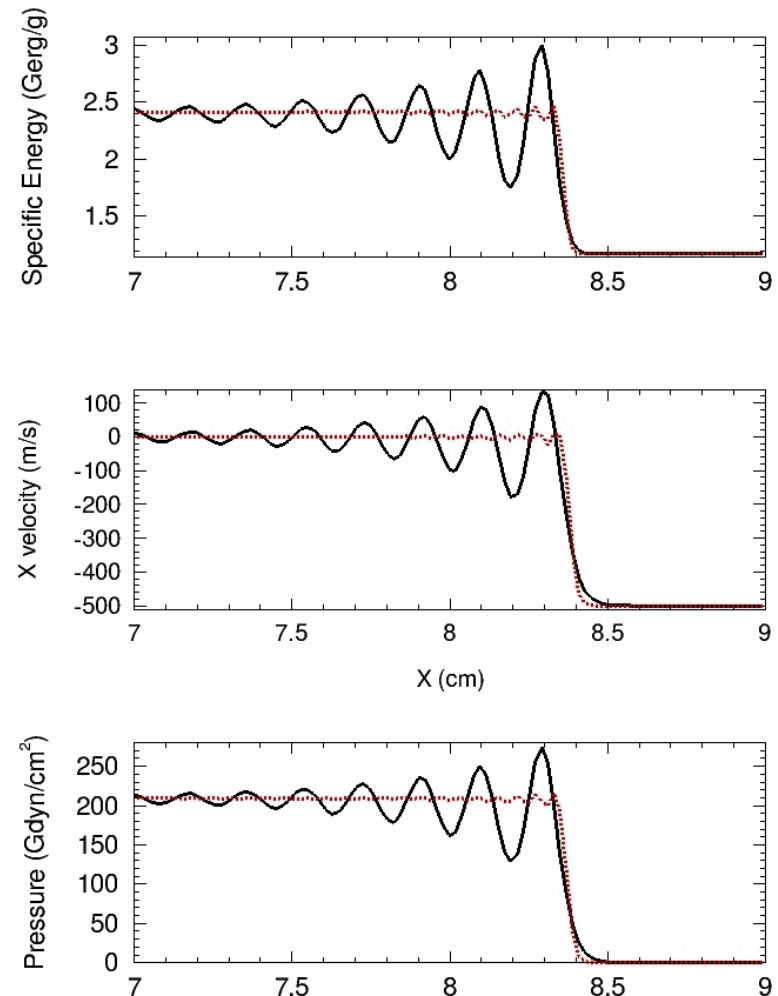


MPM at 2.002e-05 s.

CTH at 2.001e-05 s.

Flyer Plate: MPM Results

- CTH solution not monotone
- Oscillations amplified for MPM at shock
- Shock speed the same for CTH and MPM, within 1% of analytical solution
- MPM solution has about 3 additional cells of diffusion

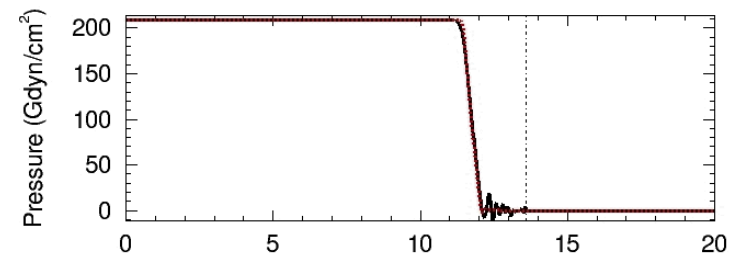
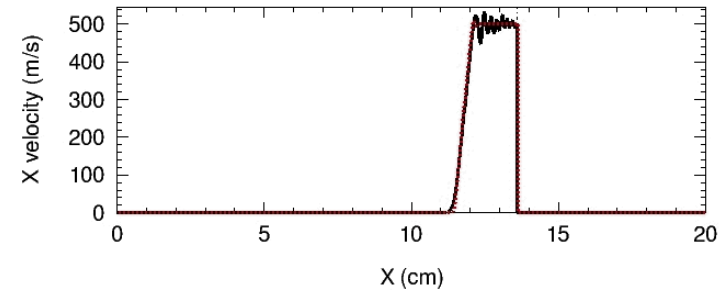
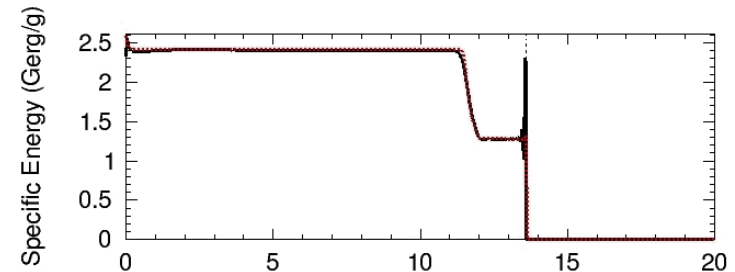


MPM at 2.002e-05 s.

CTH at 2.001e-05 s.

Flyer Plate: MPM Results

- Shock reflection off void interface at end of the rod
- Reflected shock speed the same for MPM and CTH
- Large oscillation in energy/density at interface that does not dampen for MPM
- Velocity/pressure have oscillations for MPM

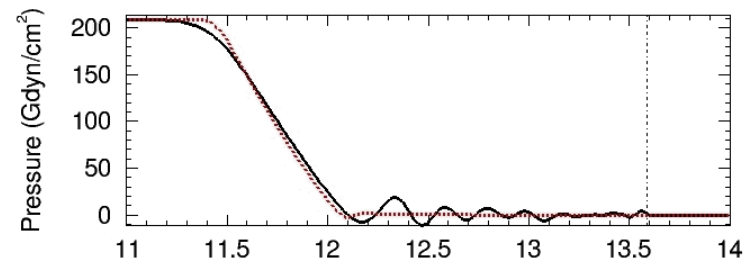
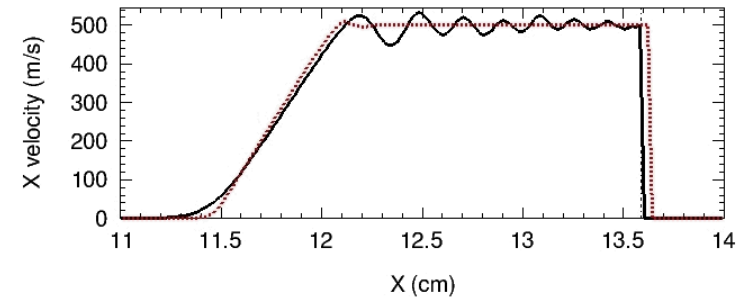
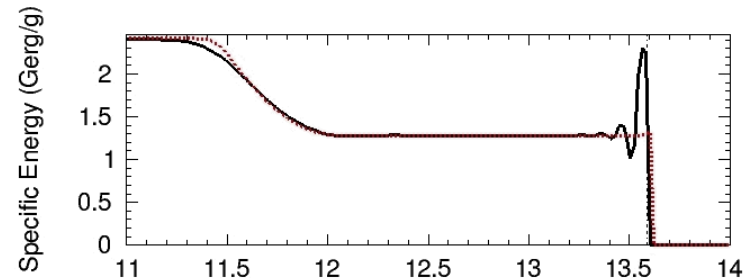


MPM at 3.601e-05 s.

CTH at 3.601e-05 s.

Flyer Plate: MPM Results

- Shock reflection off void interface at end of the rod
- Reflected shock speed the same for MPM and CTH
- Large oscillation in energy/density at interface that does not dampen for MPM
- Velocity/pressure have oscillations for MPM

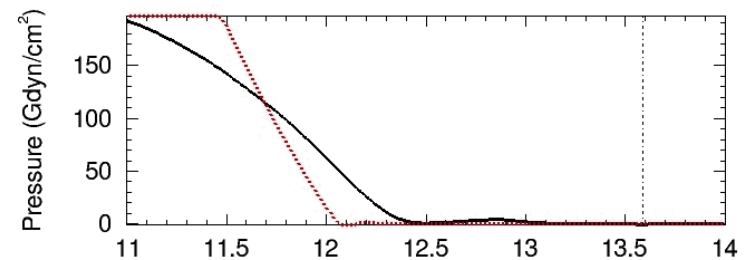
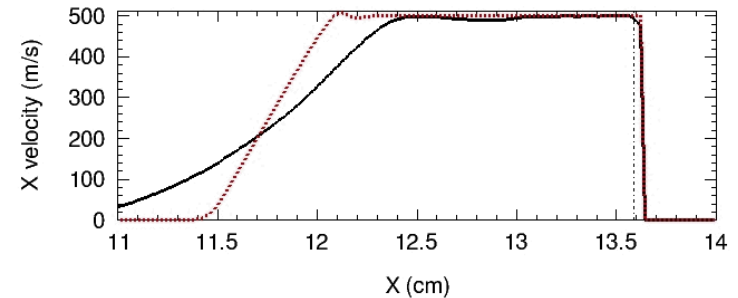
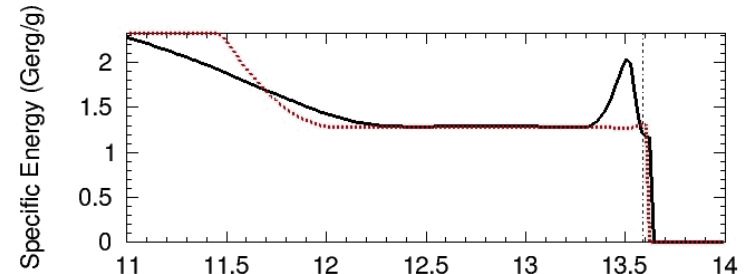


MPM at 3.601e-05 s.

CTH at 3.601e-05 s.

Flyer Plate: MPM Results

- Limited artificial viscosity removes most oscillations
 - Energy jump still present but diffused over ~15 cells now
- Increasing/decreasing artificial viscosity coefficients did not significantly improve the solution
- Possibly related to oscillation in energy at contact surface of shock tube problem

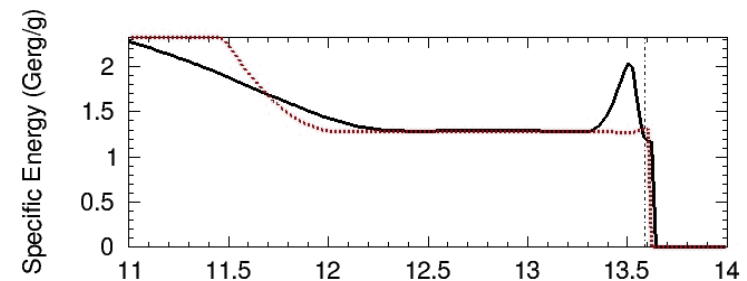
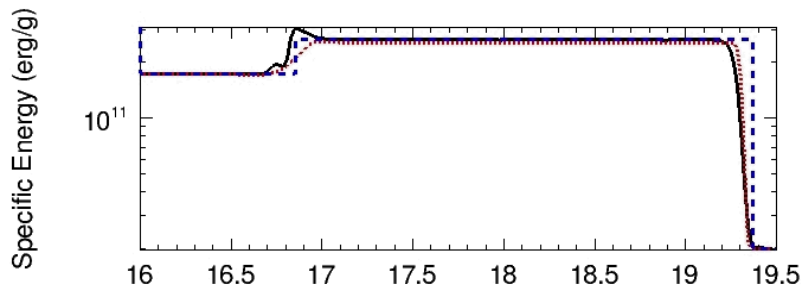


MPM at 3.601e-05 s.

CTH at 3.601e-05 s.

Conclusions

- FLIP and the MPM are very sensitive to monotonicity of underlying numerical method
- Additional diffusion included through the use of limited artificial viscosity to enforce monotonicity at discontinuities
- Still looking at the energy jump at contact/material interfaces



Questions

Thank you