

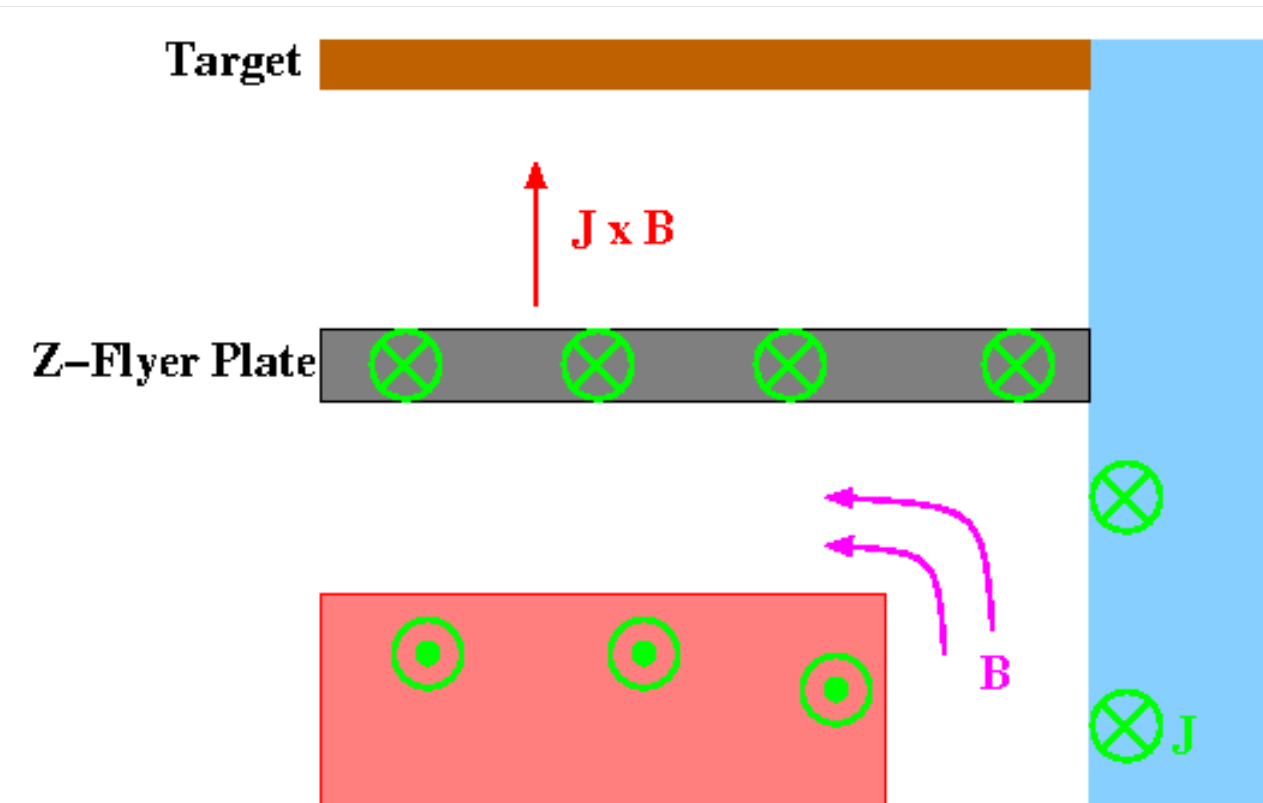
Extended and Conformal Decomposition Finite Elements for 3D Compatible Discretizations

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Motivating Application

Motivating application: Z-flyer plate

- Lorentz force accelerates plate towards target
- Goal: Shape current pulse to ensure plate
- is as *flat* and *solid* as possible on impact.



Current concentrates on material surfaces

- Material/void interfaces "count" for EM as voids must be meshed.
- Lagrangian only works for small deformation.
- Eulerian mixture models underdeveloped for EM.
- Solution: Interface tracking + local mesh or basis refinement.
- Basis refinement: eXtended Finite Element Method (XFEM).
- Mesh refinement: Conformal Decomposition Finite Element Method (CDFEM).

Governing PDEs

Nodes (2D/3D):

$$\tau \frac{\partial u}{\partial t} + \nabla \cdot \sigma \nabla u = 0$$

Edges (2D/3D) :

$$\sigma \frac{\partial \mathbf{E}}{\partial t} + \nabla \times \nu \nabla \times \mathbf{E} = 0$$

Faces (3D):

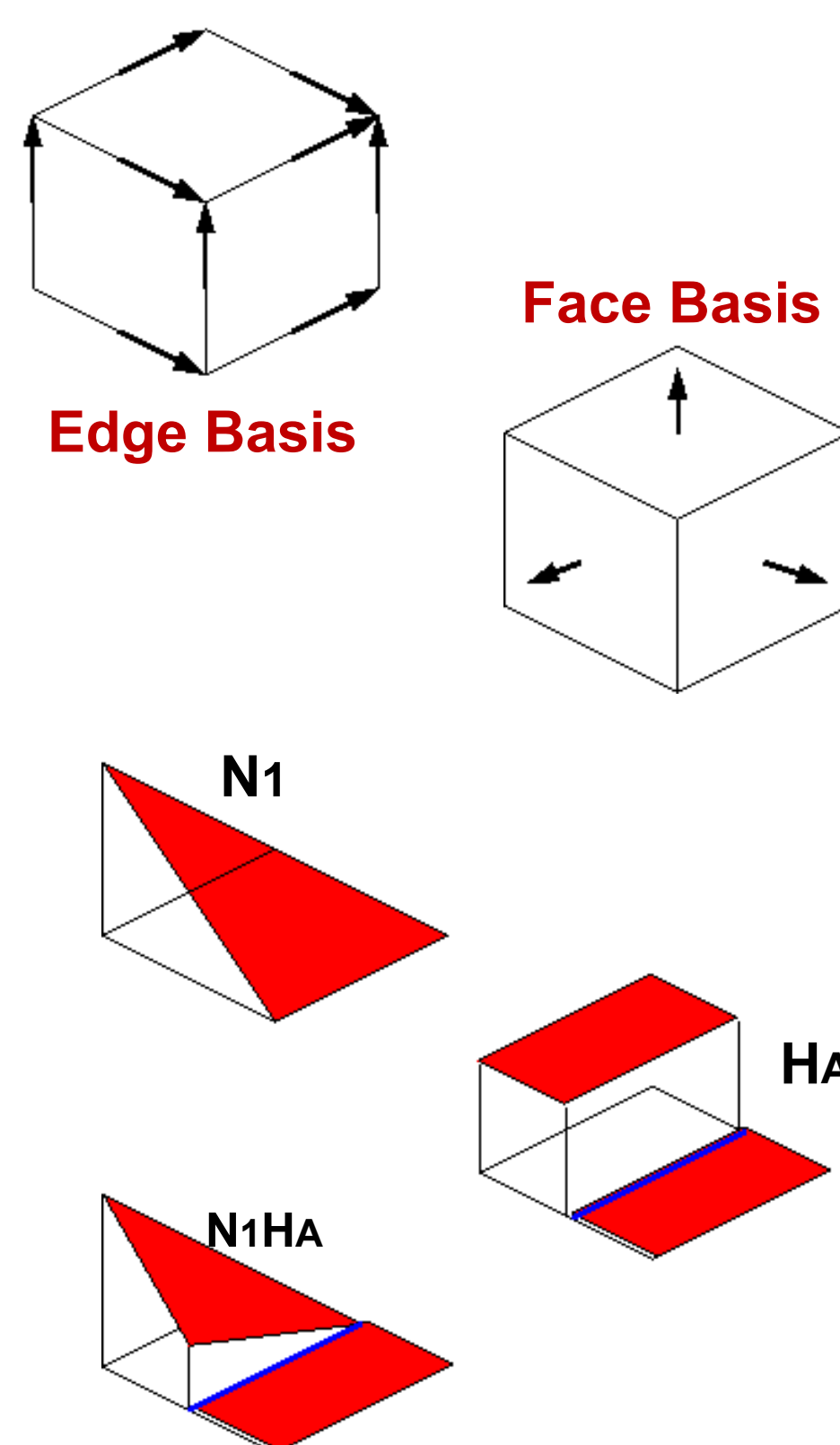
$$\nu \frac{\partial \mathbf{F}}{\partial t} + \nabla \kappa \nabla \cdot \mathbf{F} = 0$$

These PDEs capture electrostatics, magnetic diffusion and thermal diffusion (both nodal and flux-based).

Approach

Edge and Face Element Discretizations

- Preserves $\text{div curl} = 0$ and $\text{curl grad} = 0$ discretely.
- Fact: Lowest order edge basis functions on simplices (tris, tets) have a *constant tangential component* along any line.
- Fact: Lowest order face basis functions on simplices (tris, tets) have a *constant normal component* along any plane.



eXtended Finite Element Method (XFEM)

- Add *intra-element* discontinuities w/o changing mesh.
- Used here for **weak** (bonded materials) discontinuities.
- Uses Partition of Unity to preserve convergence:

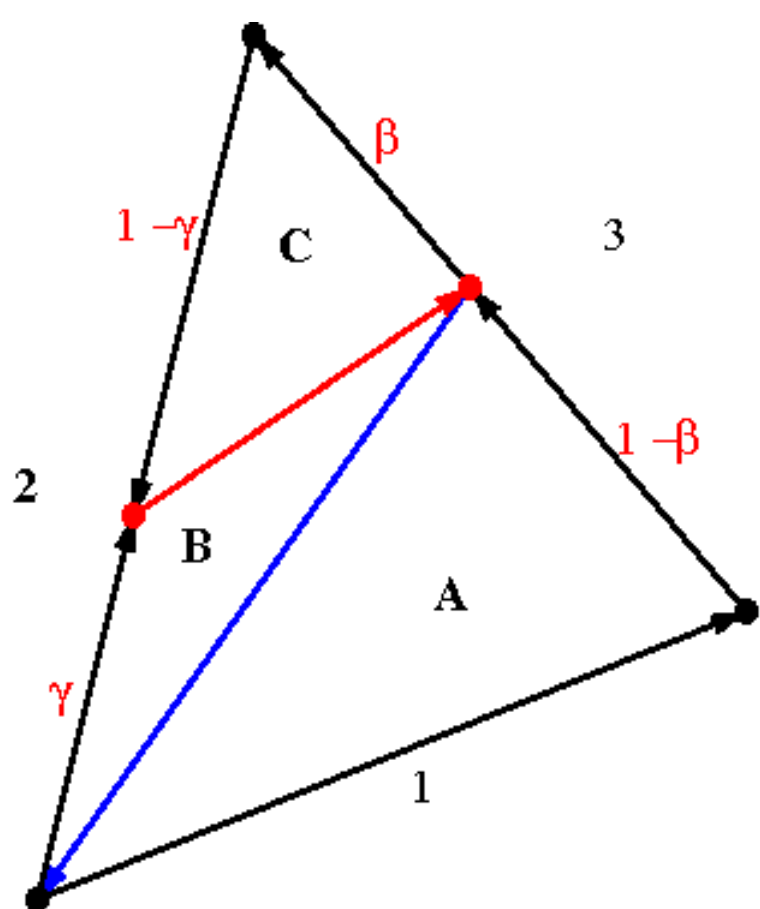
$$u^h(x) = \sum_A \sum_I N_i(x) H_A(x) u_{I,A}$$

where the constant is in the span of the F_s

- Tie solution together w/ *virtual algebraic constraints*.
- Idea #1: Start w/ simplices, decompose into simplices.
- Idea #2: Apply just enough constraints to tie *everywhere*.

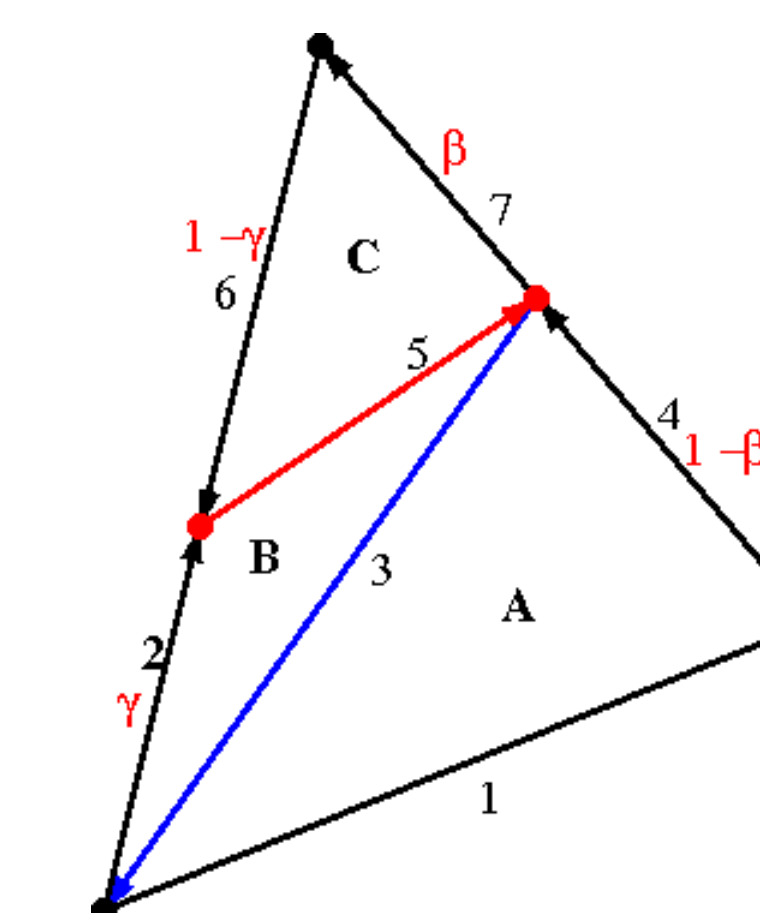
XFEM Basis

3 Edges x 3 Materials –
2 Curt * 1 Constraint
= **7 Effective DOFs**



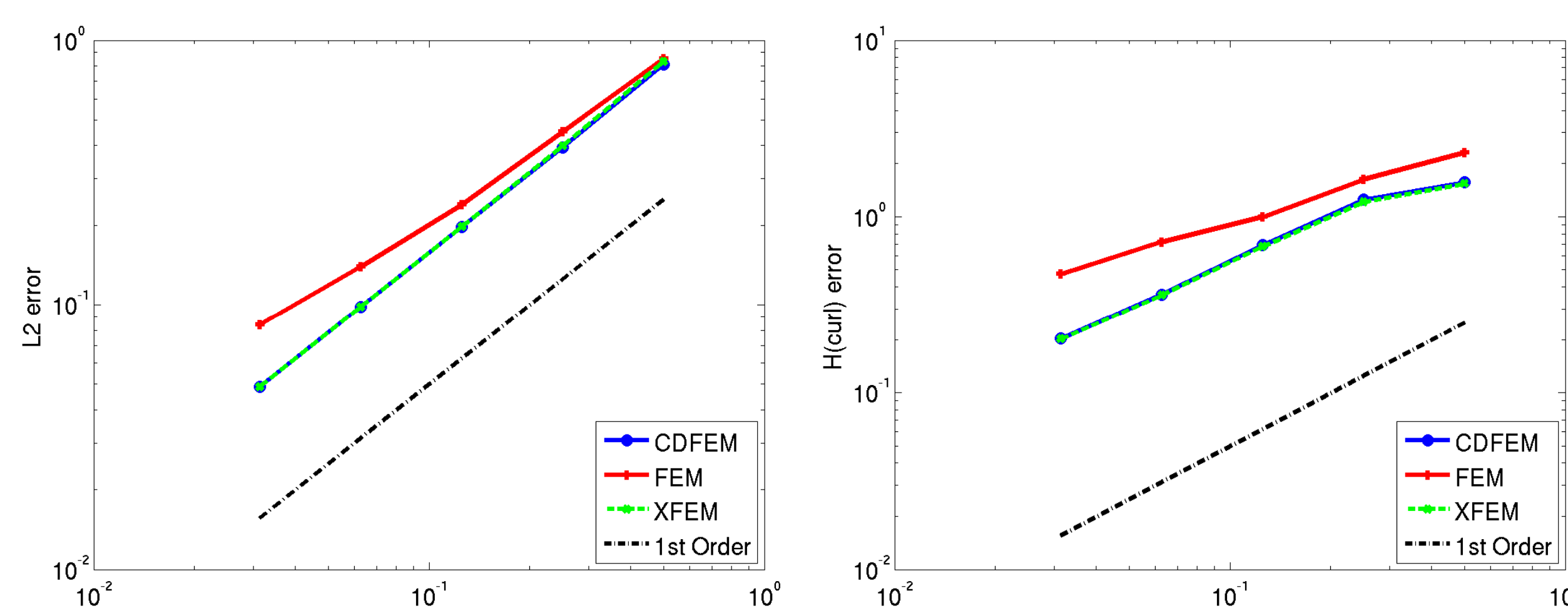
CDFEM Basis

7 Edges
= **7 Effective DOFs**

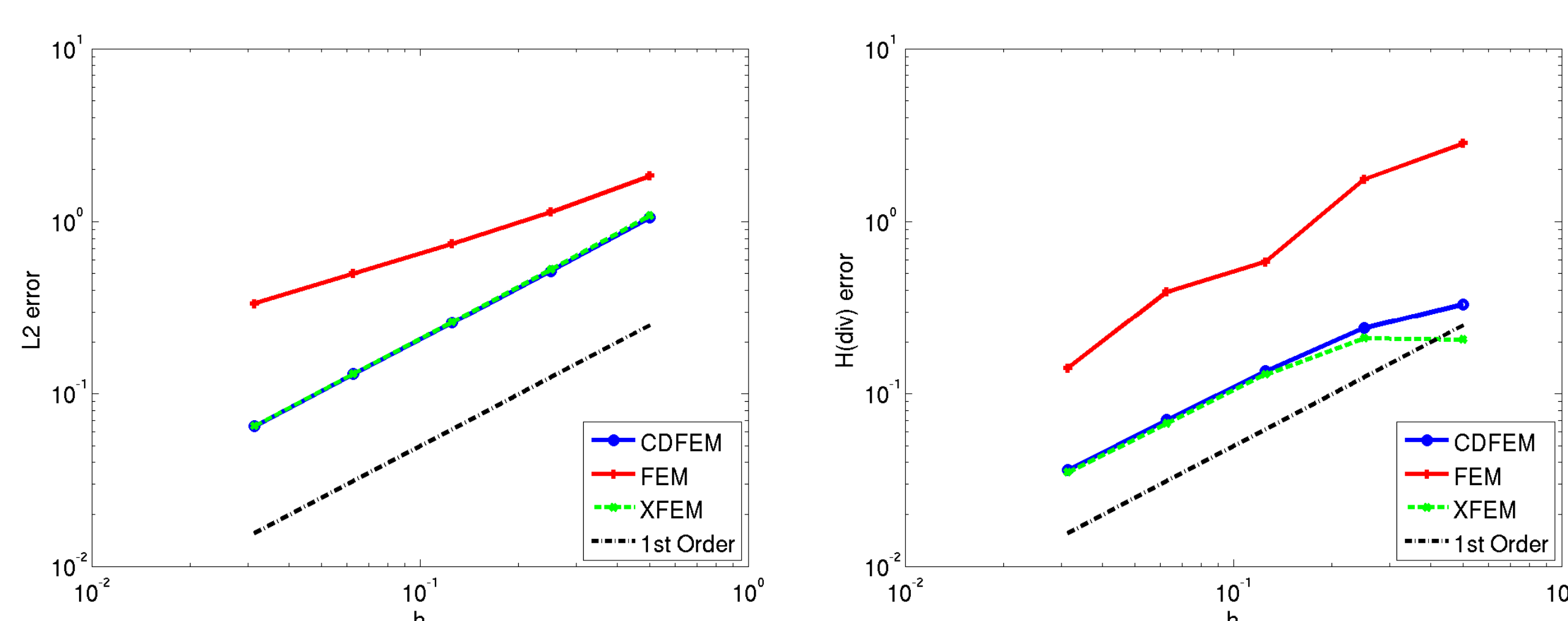


3D Verification Results

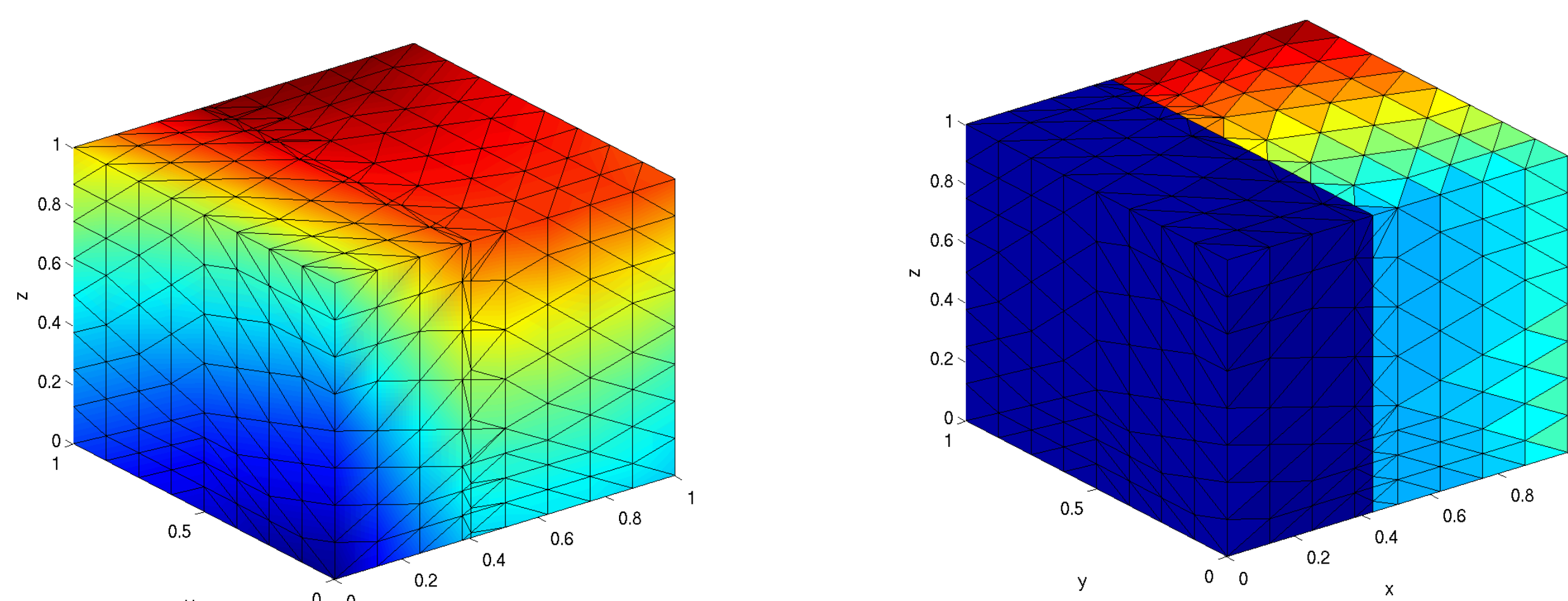
3D Edge Verification (Transient)



3D Face Verification (Transient)



3D Visualizations



Remap Algorithms

The starting point for our remap method is:

P. Bochev and M. Shashkov. Constrained interpolation (remap) of divergence-free fields. *Comput. Methods Appl. Mech. Engrg.*, 194:511–530, 2005.

The key: Think about remap as a method to transfer a representation of a field from one mesh to another.

Given the source field \mathbf{B}^o ,

$$\lambda_{\text{opt}}^e = \arg\min \|\mathbf{B}^o\|_e^2 - \|\mathbf{B}^n(\lambda^e)\|_e^2 \quad \forall e \in T^n.$$

where (element-wise)

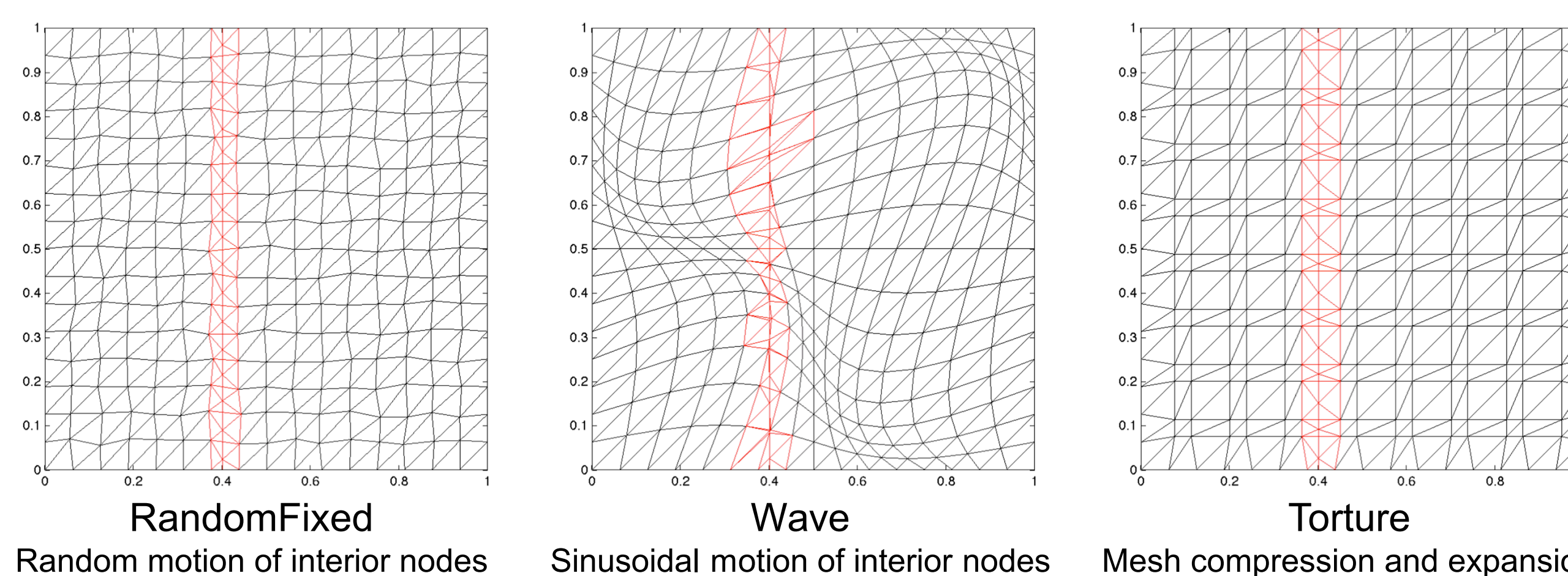
$$\begin{matrix} \text{Low order (dissipative)} \\ \text{field approximation} \\ \mathbf{B}_{\text{lo}}^n \end{matrix} + \begin{matrix} \text{High order (accurate)} \\ \text{field approximation} \\ \mathbf{B}_{\text{hi}}^n \end{matrix} = \begin{matrix} \text{Accurate and conservative} \\ \text{remapped field} \\ \mathbf{B}^n = \lambda_{\text{opt}} \mathbf{B}_{\text{lo}}^n + (1 - \lambda_{\text{opt}}) \mathbf{B}_{\text{hi}}^n \end{matrix}$$

on the destination mesh T^n .

Remap Tests

Remap testing uses three different mesh motions, shown below.

A fixed material interface is located at $x = 0.4$; elements cut by the interface are enriched and shown in red. Each mesh increment is independently enriched.



Remap Algorithm Overview

Construct 'low'- and 'high'-order interpolations of the source field on the destination mesh

Form the desired reference norm from the source field

(Locally) optimize the combination of low- and high-order interpolations such that the norm is preserved

Patch recovery

Nodal: Standard procedure to extract element-wise quadratic approximations from linear FEM over element neighbors.

Edge: Extract coefficients for 2nd-order Nédélec edge shape function polynomials from the 1st order approximation.
Respects material interfaces.

Reference Norm

Perfect remap idealization: Integrate the known analytic solution over each destination element to define the reference norm.

Practical alternatives:

- Intersection remap of element quantities from source to destination elements.
- Approximate integration of source field on the dest mesh.

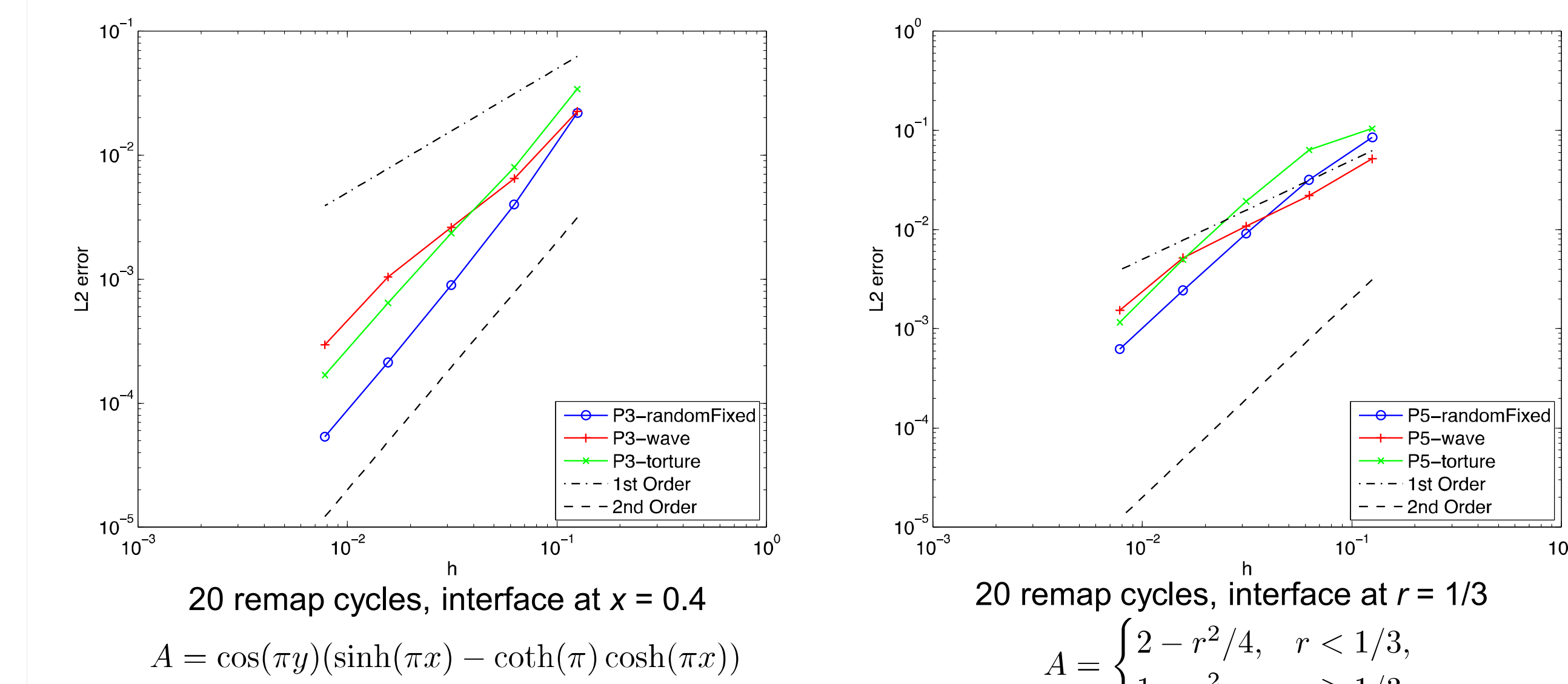
Optimization

Each element generates a simple squared quadratic objective function: roots at which local minima and maxima occur can be evaluated analytically (minimizes computational cost and improves accuracy).

2D Remap Results

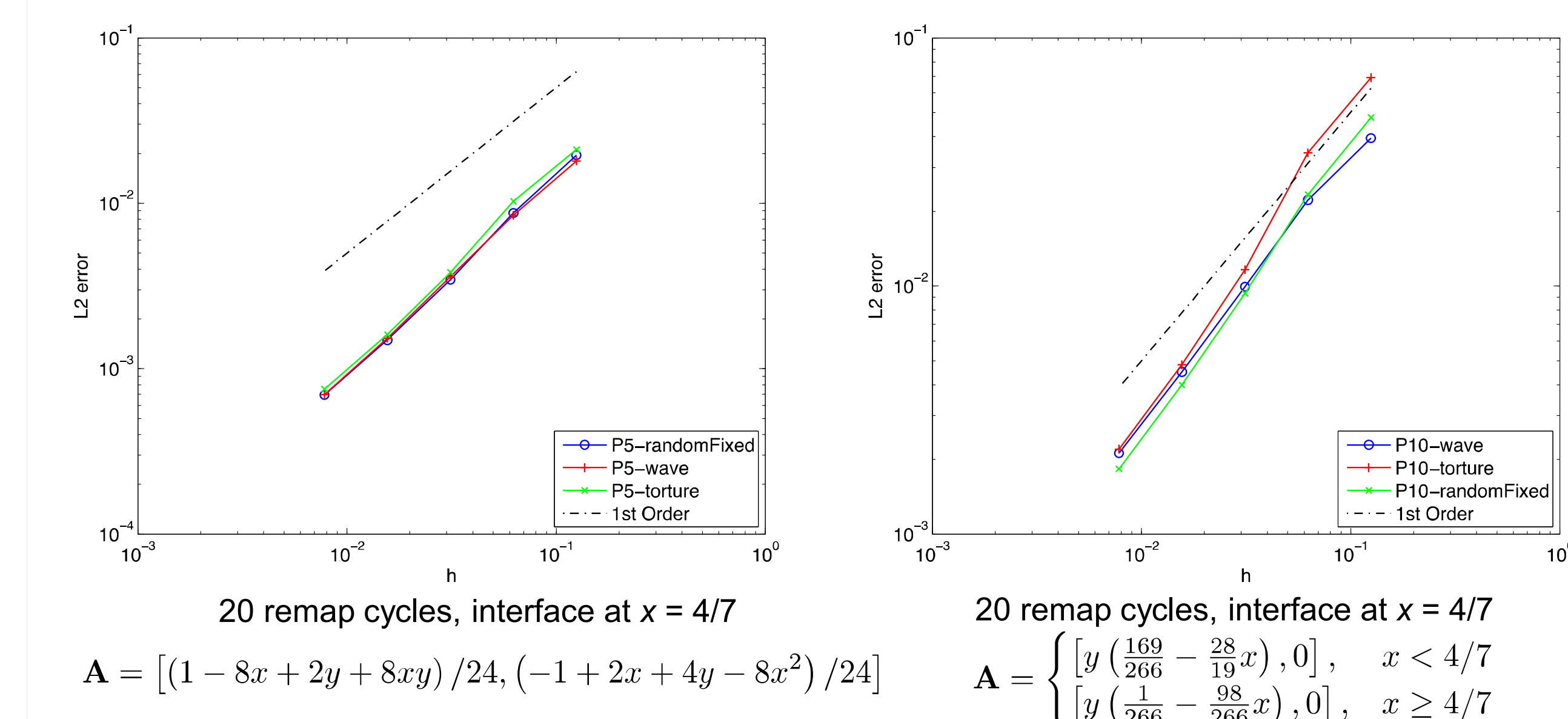
Nodal A-form (transverse magnetic):

Equation (1) solved assuming $A = A(x, y)$, with a nodal compatible discretization, where A is a scalar potential of the \mathbf{B} field such that $\mathbf{B} = \text{curl}(A)$. Norm preserved is H^1 seminorm of the field, i.e., $|\text{grad}(A)|^2 = \|\mathbf{B}\|^2$.



Compatible transverse electric:

Equation (1) solved assuming $\mathbf{A} = [A_x, A_y, 0]$, with an edge-based compatible discretization, where \mathbf{A} is a vector potential of the \mathbf{B} -field such that $\mathbf{B} = \text{curl}(\mathbf{A})$. Norm preserved is $H(\text{curl})$ of the field, i.e., $|\text{curl}(\mathbf{A})|^2 = \|\mathbf{B}\|^2$.



Current and Future Work

- Improved (piecewise linear) interface reconstruction.
- Mixed meshes (quad/tri and hex/pyramid/prism/tet).
- Extending remap algorithms to 3D.
- Improved patch recovery for edge element discretizations.

References:

- R. Kramer, P. Bochev, C. Siefert and T. Voth. *An extended finite element method with algebraic constraints (XFEM-AC) for problems with weak discontinuities. Computer Methods in Applied Mechanics and Engineering*, Volume 266, pp. 70–80, 2013.
- R. Kramer, P. Bochev, C. Siefert and T. Voth. *Algebraically constrained extended edge element method (eXFEM-AC) for resolution of multi-material cells. Journal of Computational Physics*, Volume 276, Pages 596–612, 2014.

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