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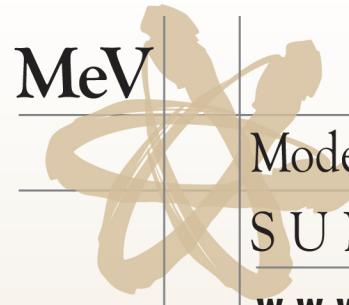
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# **Data Assimilation – Advances and Applications**

**Brian Williams**  
**Statistical Sciences Group**  
**Los Alamos National Laboratory**

**Session #7**

**23 July 2014**

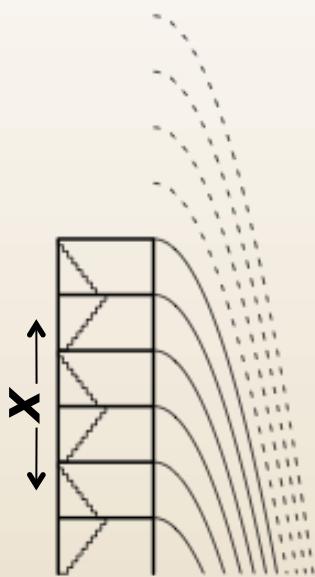
**10 – 11:30 AM**

# Abstract

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This presentation provides an overview of data assimilation (model calibration) for complex computer experiments. Calibration refers to the process of probabilistically constraining uncertain physics/engineering model inputs to be consistent with observed experimental data. An initial probability distribution for these parameters is updated using the experimental information. Utilization of surrogate models and empirical adjustment for model form error in code calibration form the basis for the statistical methodology considered. The role of probabilistic code calibration in supporting code validation is discussed. Incorporation of model form uncertainty in rigorous uncertainty quantification (UQ) analyses is also addressed. Design criteria used within a batch sequential design algorithm are introduced for efficiently achieving predictive maturity and improved code calibration. Predictive maturity refers to obtaining stable predictive inference with calibrated computer codes. These approaches allow for augmentation of initial experiment designs for collecting new physical data. A standard framework for data assimilation is presented and techniques for updating the posterior distribution of the state variables based on particle filtering and the ensemble Kalman filter are introduced.

# Calibration With Model Form Error

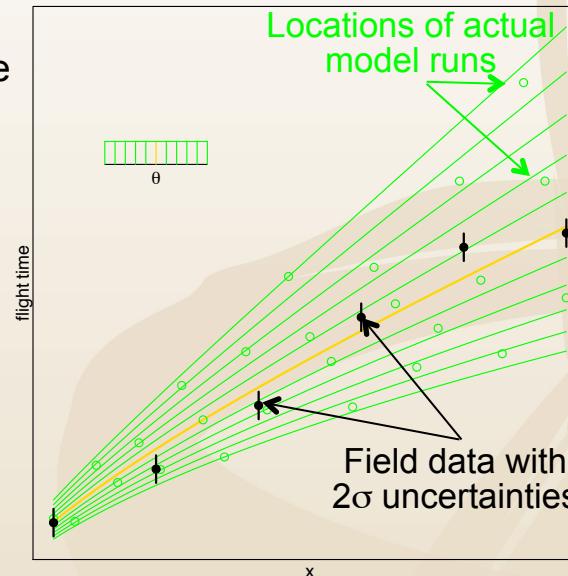


computer model  
 $s = \text{position}$ ;  $\tau = \text{time}$

$$\frac{d^2s}{d\tau^2} = -1 - \theta \frac{ds}{d\tau}$$

initial conditions

$$s(0) = x, \frac{ds}{d\tau} \bigg|_{\tau=0} = 0$$

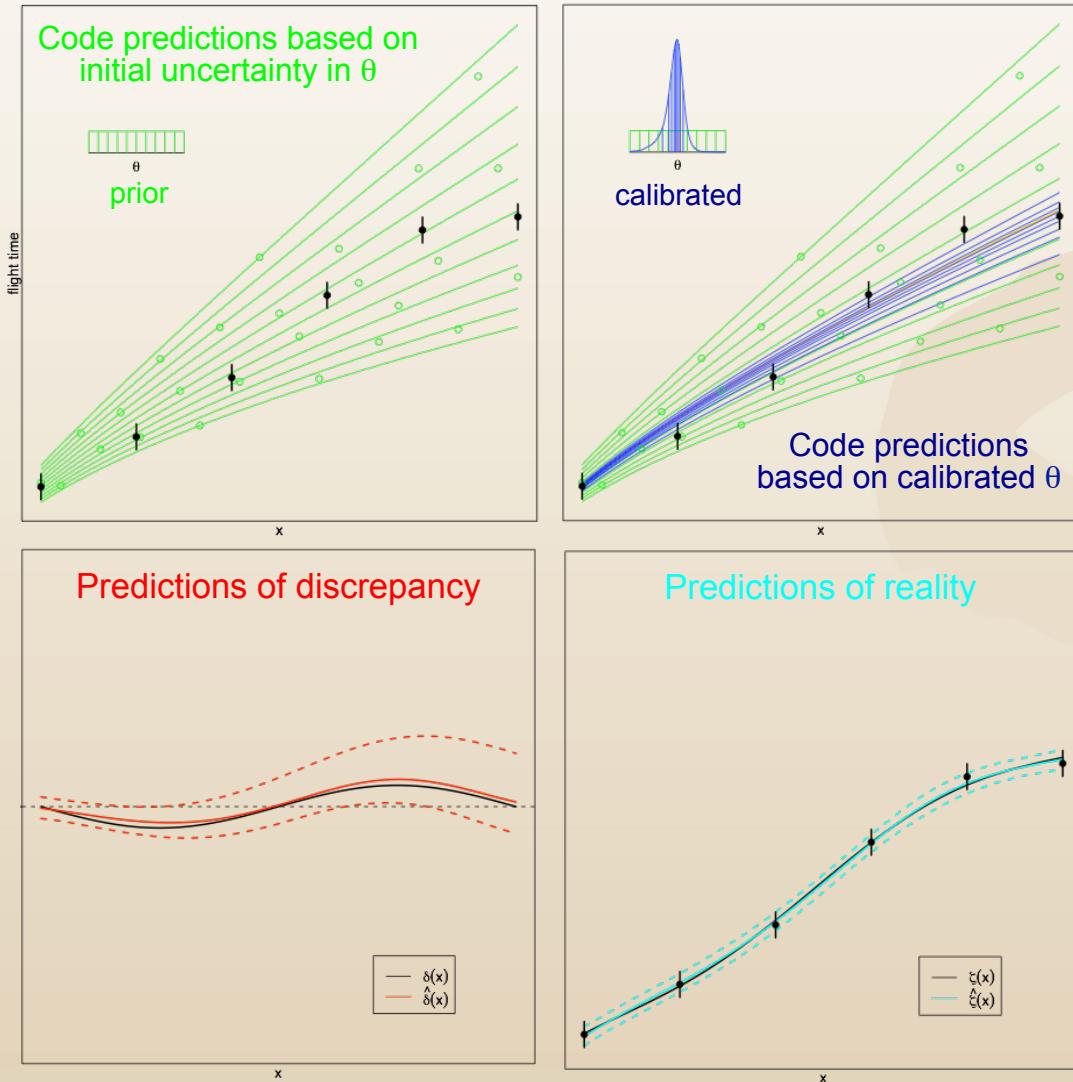


flight time

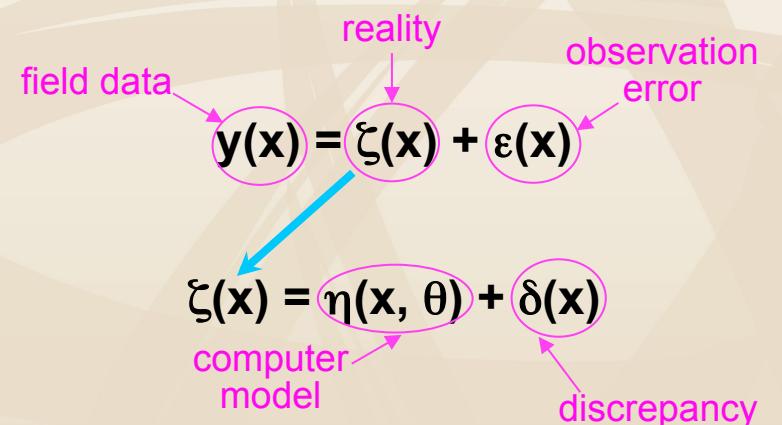
$\eta(x, \theta)$  is the root of the equation  $s(\tau) = 0$ .

- Experiment: Drop a solid ball from a specified height
  - Output: Measured flight time ( $y$ )
- Computer Model: Implements Newton's Law with drag coefficient
  - Two parameters:  $x$  = height (controlled)
  - $\theta$  = drag coefficient (uncertain physics)
  - Output: Calculated flight time ( $\eta(x, \theta)$ )

# Code Calibration: Statistical Model and Inference



Inputs  
 $x$  controllable  
 $t$  uncertain physics  
 $\theta$  best, unknown value of  $t$

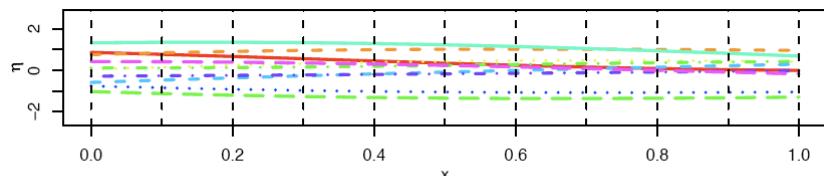


Basic steps in calibration analysis:

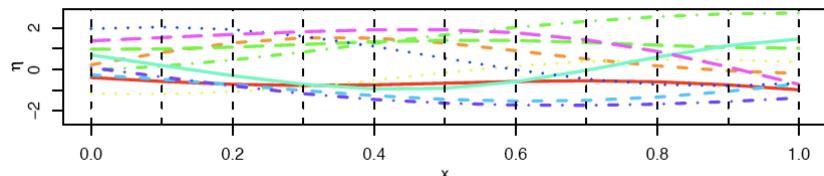
1. Assume prior probability distribution for physics uncertainties  $\theta$ .
2. Calibrate parameters  $\theta$  to field data and simultaneously infer model form error.

# Gaussian Process Review and Notation

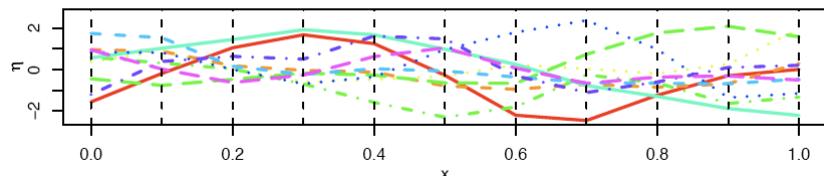
$\beta = 0.3; \rho = 0.93$



$\beta = 3; \rho = 0.47$



$\beta = 30; \rho = 0$



Semiparametric regression model for emulating code  $\eta(x)$

Joint distribution of surrogate outputs is multivariate Gaussian

Mean zero, precision  $\lambda$

Correlation function:

$$R(\eta(\mathbf{x}_1), \eta(\mathbf{x}_2) | \beta) = \exp\left(-\sum_{j=1}^d \beta_j (x_{1,j} - x_{2,j})^2\right)$$

Define correlation length:

$$\rho_j = \exp(-\beta_j / 4)$$

Notation:  $GP(0; \lambda, \rho)$

Correlation lengths  $\rho_j$  determine complexity of process realizations

# Calibration Framework: Scalar Output

- Experiments:  $\mathbf{x}_1, \dots, \mathbf{x}_n$
- Code Runs:  $(\mathbf{x}_1^c, \mathbf{t}_1), \dots, (\mathbf{x}_m^c, \mathbf{t}_m)$
- $\eta(\cdot) \sim GP(0; \lambda_\eta, \rho_\eta)$  independent of  $\delta(\cdot) \sim GP(0; \lambda_\delta, \rho_\delta)$
- Correlation functions  $R_\eta(\mathbf{x}_1 - \mathbf{x}_2, \mathbf{t}_1 - \mathbf{t}_2)$  and  $R_\delta(\mathbf{x}_1 - \mathbf{x}_2)$
- $\epsilon \sim \mathcal{N}(0, \Sigma_y)$
- Output Vector:  $\mathcal{D} = (y(\mathbf{x}_1), \dots, y(\mathbf{x}_n), \eta(\mathbf{x}_1^c, \mathbf{t}_1), \dots, \eta(\mathbf{x}_m^c, \mathbf{t}_m))$ 

Centered by Average Code Output  
Scaled by SD of Code Output

# Likelihood Function: Scalar Output

## Likelihood Function

$$L(\theta, \lambda_\eta, \rho_\eta, \lambda_\delta, \rho_\delta, \Sigma_y | \mathcal{D}) \propto |\Sigma_{\mathcal{D}}|^{-1/2} \exp \left\{ -\frac{1}{2} \mathcal{D}^T \Sigma_{\mathcal{D}}^{-1} \mathcal{D} \right\}$$

$$\Sigma_{\mathcal{D}} = \Sigma_\eta + \begin{pmatrix} \Sigma_y + \Sigma_\delta & 0 \\ 0 & 0 \end{pmatrix}$$

$\lambda_\eta \Sigma_\eta$ : Correlation matrix between  $(\mathbf{x}_1, \theta), \dots, (\mathbf{x}_n, \theta), (\mathbf{x}_1^c, \mathbf{t}_1), \dots, (\mathbf{x}_m^c, \mathbf{t}_m)$

$\lambda_\delta \Sigma_\delta$ : Correlation matrix between  $\mathbf{x}_1, \dots, \mathbf{x}_n$

$\lambda_y \Sigma_y = \mathbf{I}_n$  in many applications  
 $\lambda_y$  fixed or random

$R_\eta$

$R_\delta$

# Prior Distributions and Posterior Sampling

- Prior Distributions

→ Correlation parameters ( $\eta$  and  $\delta$ )

$$\pi(\boldsymbol{\rho}) \propto \prod_{j=1}^{n_p} (1 - \rho_j)^{(b_p - 1)}, 0 < \rho_j \leq 1$$

– Control degree of prior smoothness (variable importance)

→ Precision parameters ( $\eta$ ,  $\delta$ , and  $\epsilon$ )

$$\pi(\lambda) \propto \lambda^{(a_\lambda - 1)} \exp(-b_\lambda \lambda), \lambda > 0$$

– Set  $a_\eta = b_\eta$  (prior mean 1; larger  $b_\eta$  smaller prior variance)

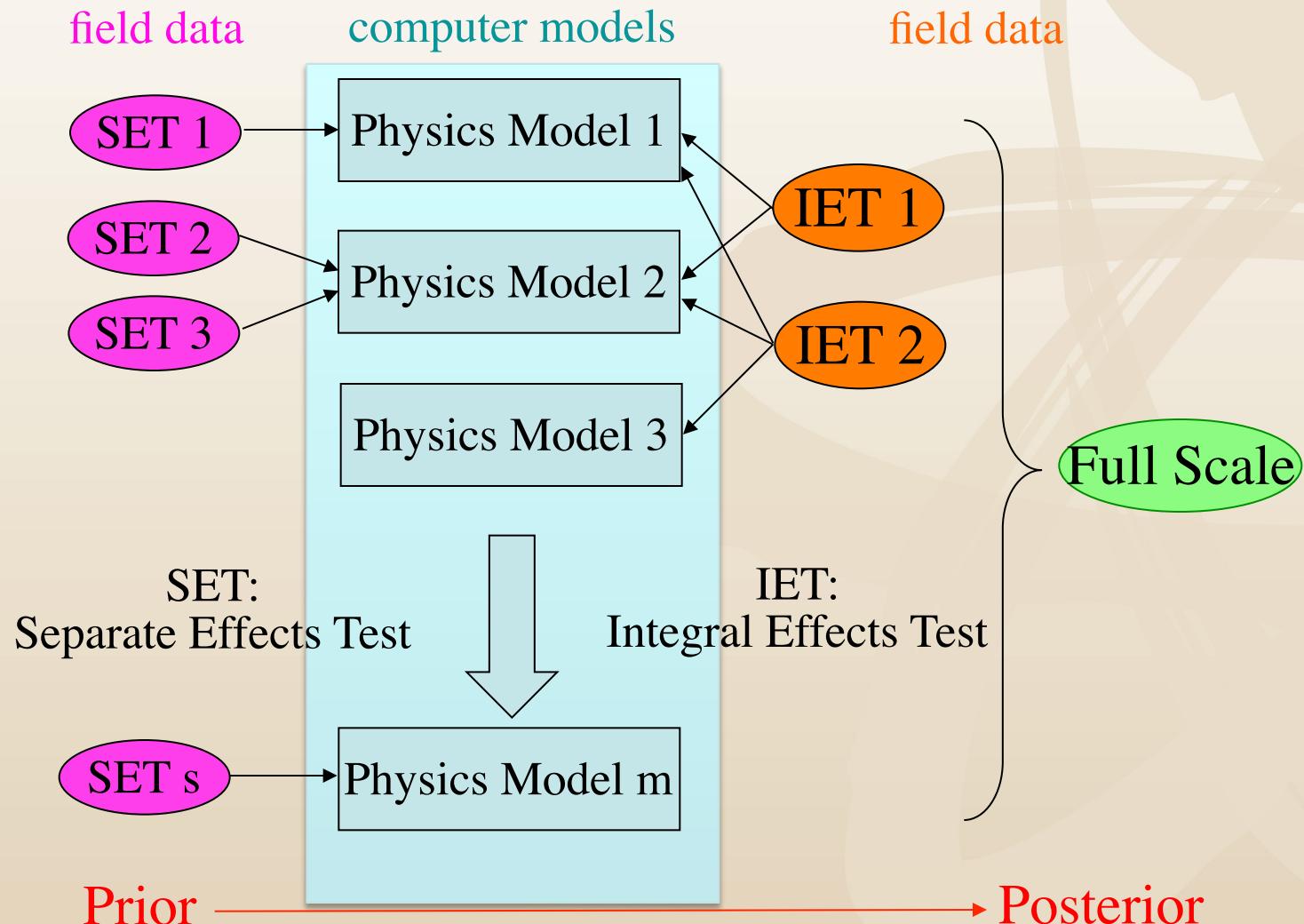
– Set  $b_\delta/a_\delta \approx 0$ , i.e. noninformative with large prior mean

– Settings for  $a_\epsilon$  and  $b_\epsilon$  depend on assumptions for observation error

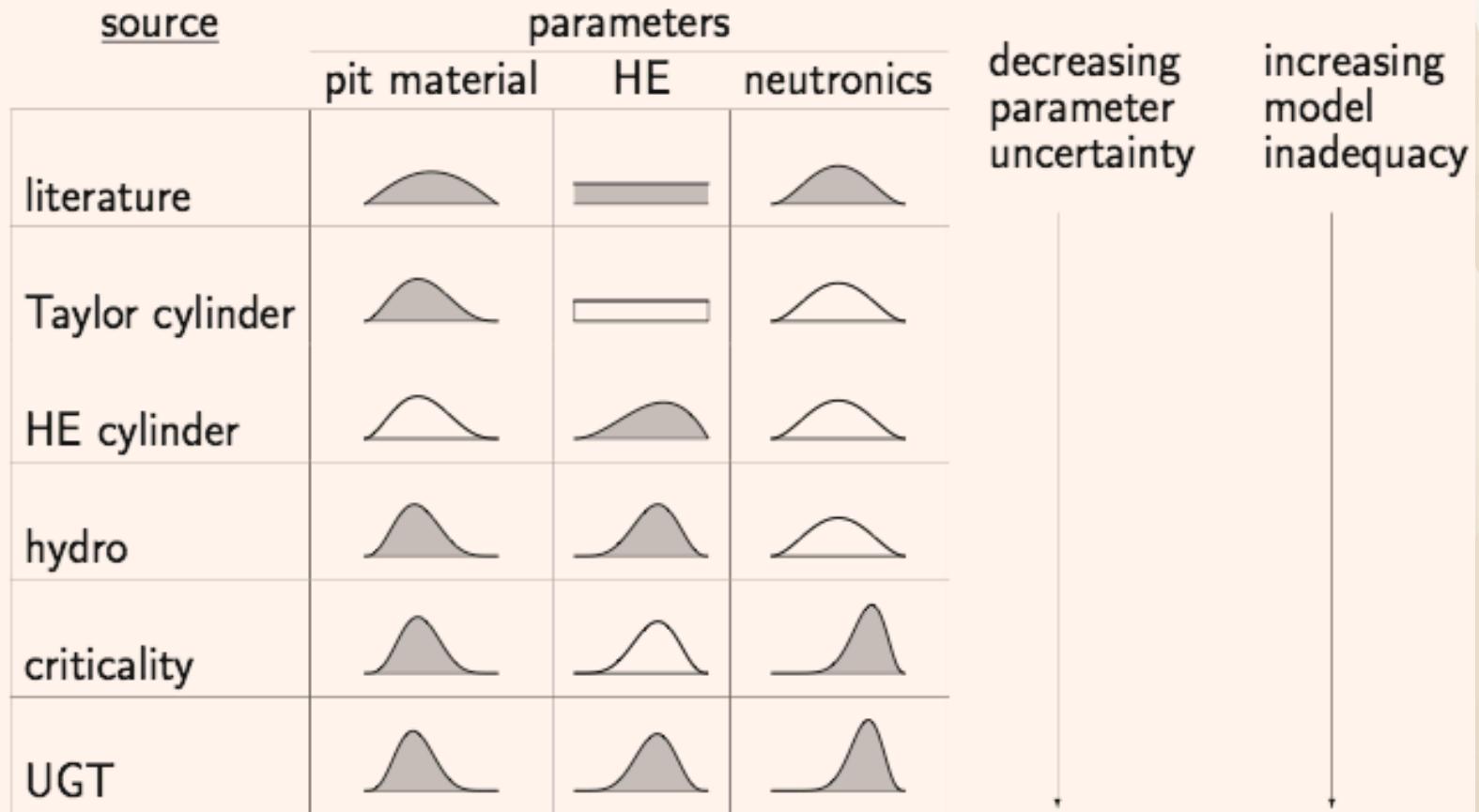
- Posterior Sampling

- Metropolis within Gibbs MCMC
- Burn-in + logistic regression to estimate step sizes

# Simultaneous Code Calibration for Multi-Physics Applications

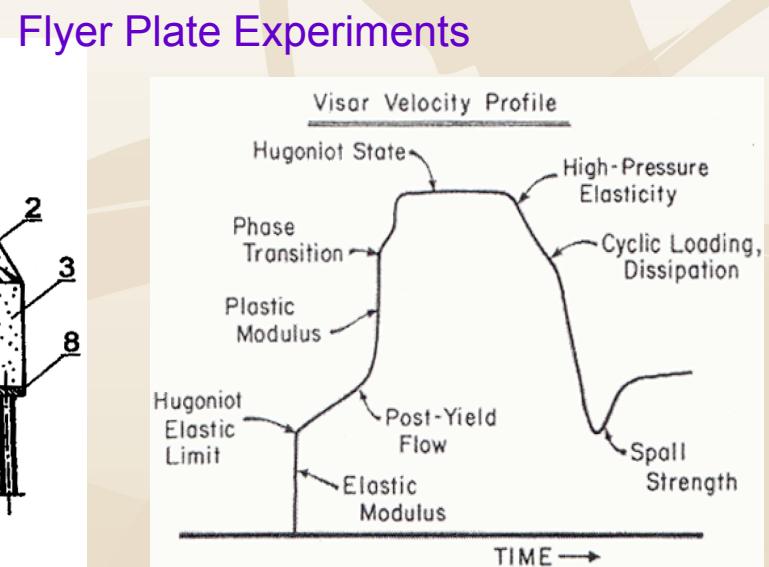
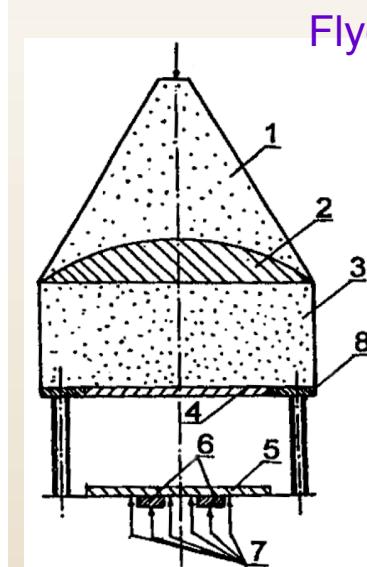
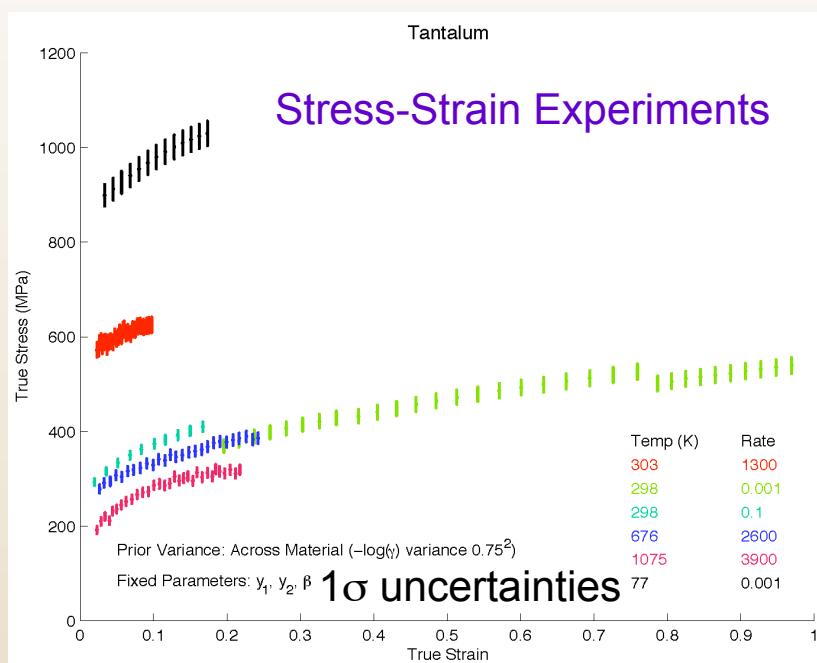


# Simultaneous Code Calibration for Weapon Performance Applications



- conditioning on more experiments  $\Rightarrow$  less parametric uncertainty
- prediction uncertainty becomes more affected by model inadequacies

# Code Calibration: Multiple Datasets and Functional Output



- **SET:** Stress-strain experiments are conducted to infer material strength
  - Physics model: PTW (Preston-Tonks-Wallace)
- **IET:** Flyer plate experiments are conducted to infer material equation of state (EOS), strength and damage simultaneously
  - Physics models: tabular EOS, PTW, tension limit

# PTW Plastic Deformation Model

$$\hat{\tau}_y = y_0 - (y_0 - y_\infty) \operatorname{erf} \left[ \kappa \hat{T} \ln \left( \gamma \dot{\xi} / \dot{\psi} \right) \right]$$

activation energy      strain rate

$$\hat{\tau}_s = s_0 - (s_0 - s_\infty) \operatorname{erf} \left[ \kappa \hat{T} \ln \left( \gamma \dot{\xi} / \dot{\psi} \right) \right]$$

T / T<sub>m(ρ)</sub>      yield stress

atomic vibration time      saturation stress

T = temperature  
T<sub>m(ρ)</sub> = melting temp.

$$\hat{\tau} = \hat{\tau}_s + \frac{1}{p} (s_0 - \hat{\tau}_y) \ln \left[ 1 - \left[ 1 - \exp \left( -p \frac{\hat{\tau}_s - \hat{\tau}_y}{s_0 - \hat{\tau}_y} \right) \right] \exp \left\{ - \frac{p \theta_0 \dot{\psi}}{(s_0 - \hat{\tau}_y) \left[ \exp \left( p \frac{\hat{\tau}_s - \hat{\tau}_y}{s_0 - \hat{\tau}_y} \right) - 1 \right]} \right\} \right]$$

strain  
↓

$$\theta = (\theta_0, p, \kappa, \gamma, y_0, y_\infty, s_0, s_\infty)$$

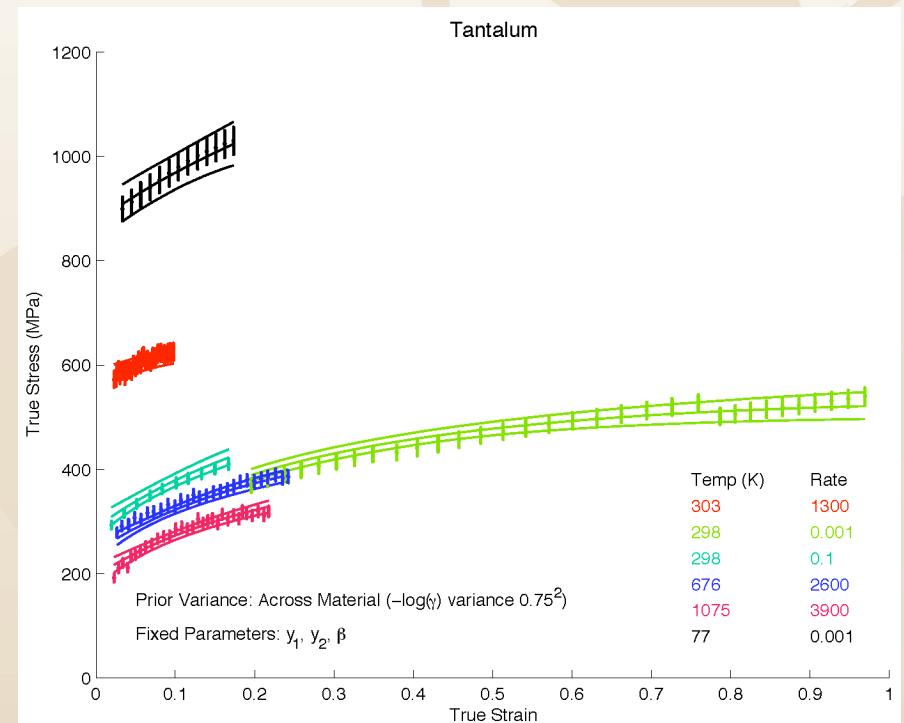
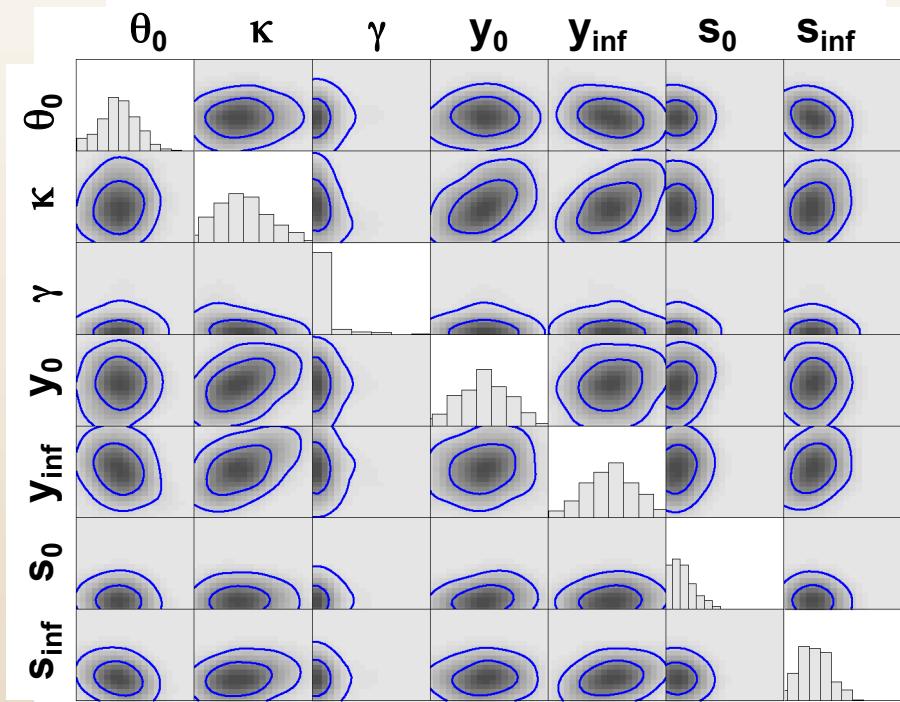
calibration  
parameters

# Calibration of PTW Model

$$\begin{aligned}
 & \text{stress} \quad \text{strain} \quad \text{dataset-specific parameters (temp., strain rate)} \quad \text{dataset-specific estimated uncertainty} \\
 & \mathbf{y}_{ij} = ptw(S_{ij}, \mathbf{x}_i, \boldsymbol{\theta}) + \boldsymbol{\varepsilon}_i; \quad \boldsymbol{\varepsilon}_i \sim N\left(\mathbf{0}, \frac{\sigma_i^2}{\lambda} \mathbf{I}\right); \\
 & \boldsymbol{\theta} \sim N(\mathbf{b}_0, \mathbf{V}_0^{-1}), \quad \lambda \sim \text{Gamma}(a, b); \\
 & \text{prior mean} \quad \text{prior covariance (depends on analysis)} \quad \text{adjustment to uncertainty} \\
 & \text{PTW} \\
 & \boldsymbol{\theta} = (\theta_0, p, \kappa, -\ln(\gamma), y_0, y_\infty, s_0, s_\infty)
 \end{aligned}$$

Uncertain parameters  $\theta$  “common” to all datasets

# Phase I: Calibration to Small-Scale Data



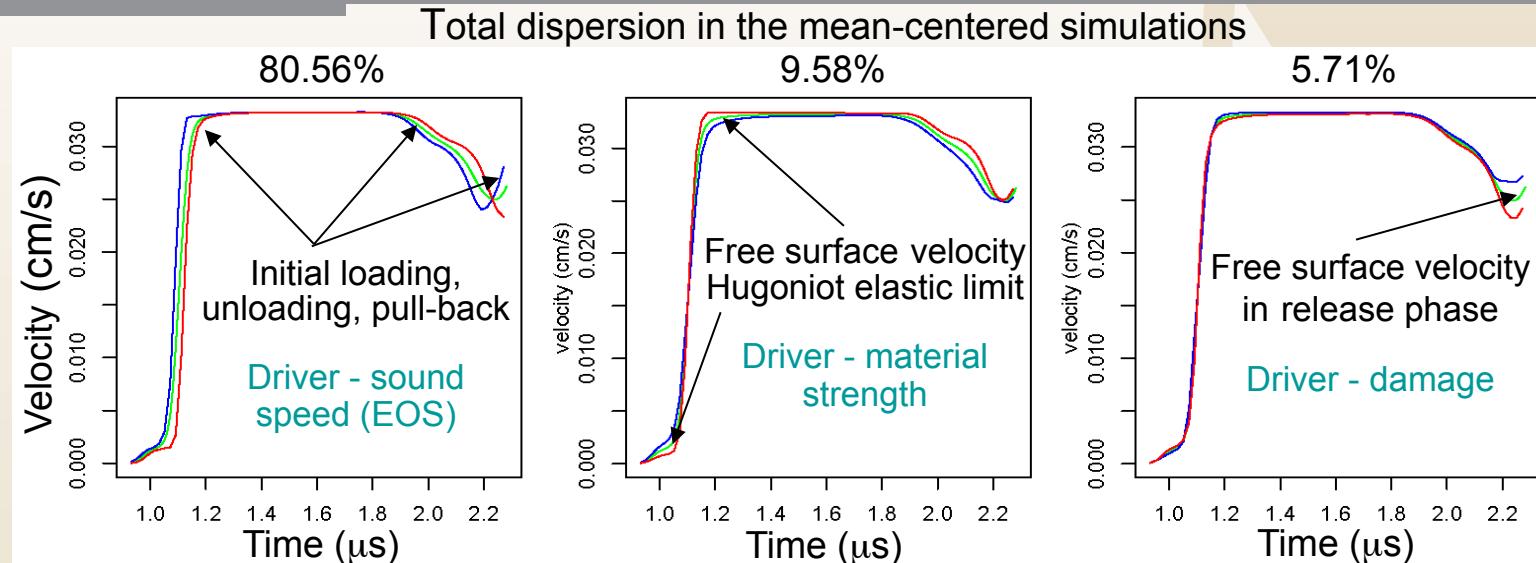
Prior constraint on PTW parameters for calibration of all parameters to integral data

# Physics Models and Parameters

Input	Description	Domain	
		Min	Max
$\epsilon$	Perturbation of EOS table from nominal	-5%	5%
$\theta_0$	Initial strain hardening rate	$2.78 \times 10^{-5}$	0.0336
$\kappa$	Material constant in thermal activation energy term – relates to the temperature dependence	0.438	1.11
$\gamma$	Material constant in thermal activation energy term – relates to the strain rate dependence	$6.96 \times 10^{-8}$	$6.76 \times 10^{-4}$
$y_0$	Maximum yield stress (at 0 K)	0.00686	0.0126
$y_\infty$	Minimum yield stress (~ melting)	$7.17 \times 10^{-4}$	0.00192
$s_0$	Maximum saturation stress (at 0 K)	0.0126	0.0564
$s_\infty$	Minimum saturation stress (~ melting)	0.00192	0.00616
$P_{\min}$	Spall strength	-0.055	-0.045
$v_s$	Flyer plate impact velocity	329.5	338.5

Calibrate all parameters to integral (flyer plate) data  
 128 flyer plate runs defined by an OA-based LH design

# Modeling Functional Computer Model Output

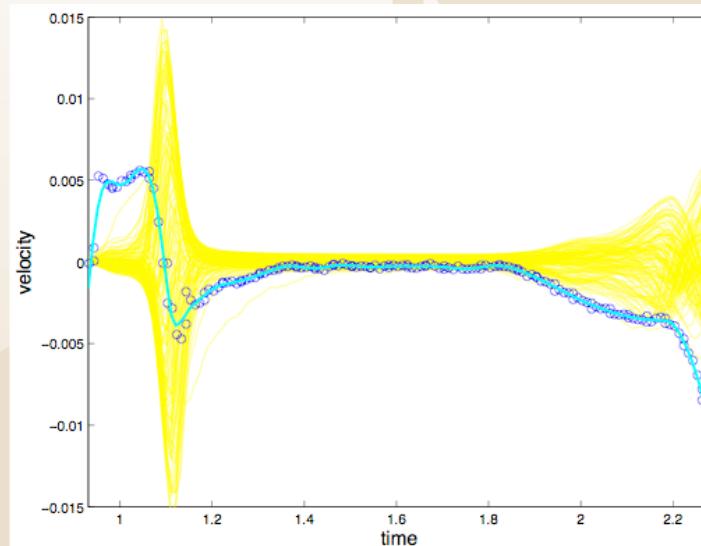
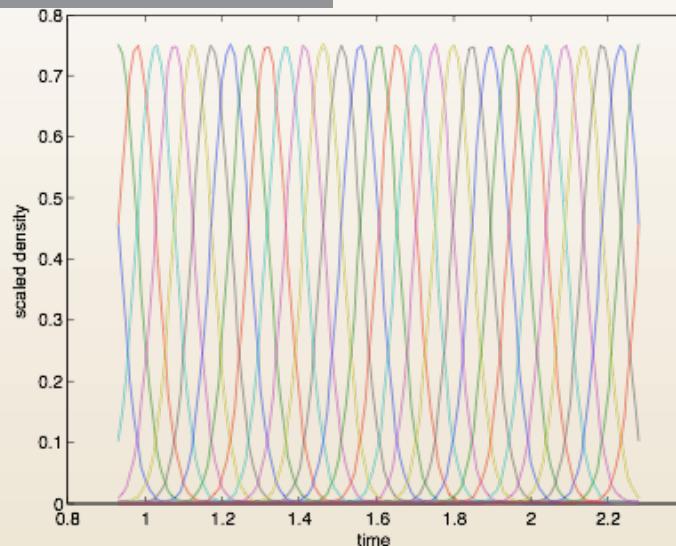


- $n_\eta \times m$  matrix of simulator output (“time” by “space”)
  - each row mean centered; entire matrix scaled so output has variance 1
- Statistical model:

$$\eta(\mathbf{x}, \mathbf{t}) = \sum_{i=1}^{p_\eta} \mathbf{k}_i w_i(\mathbf{x}, \mathbf{t}) + \epsilon$$

- $\mathbf{k}_1, \dots, \mathbf{k}_{p_\eta}$  are  $n_\eta \times 1$  orthogonal basis vectors (e.g. principal components)
- $w_i(\mathbf{x}, \mathbf{t})$ : basis coefficients; modeled as  $\text{GP}(\rho_{wi}, \lambda_{wi})$ ; independent
- $\epsilon$ : model error; modeled as  $\text{GP}(0, \lambda_\eta)$ ; independent of basis coefficients

# Modeling Functional Experimental Data



- $\mathbf{y}(\mathbf{x}_i)$  is  $n_{y_i} \times 1$  vector of centered/scaled experimental data,  $i = 1, \dots, n$
- Statistical model:

$$\mathbf{y}(\mathbf{x}_i) = \mathbf{K}_i \mathbf{w}(\mathbf{x}_i, \boldsymbol{\theta}) + \mathbf{D}_i \mathbf{v}(\mathbf{x}_i) + \boldsymbol{\epsilon}_i$$

- $\mathbf{K}_i$  is  $n_{y_i} \times p_\eta$  matrix of simulator basis vectors interpolated onto data grid
- $\mathbf{w}(\mathbf{x}_i, \boldsymbol{\theta})$ : simulator basis coefficients evaluated at best, unknown  $\boldsymbol{\theta}$
- $\mathbf{D}_i$  is  $n_{y_i} \times p_\delta$  matrix of discrepancy basis vectors
- $\mathbf{v}(\mathbf{x}_i)$ : discrepancy basis coefficients; modeled as  $\text{GP}(\boldsymbol{\rho}_v, \lambda_v)$ ; independent
- $\boldsymbol{\epsilon}_i$ : model error; modeled as  $\text{GP}(\mathbf{0}, \lambda_y)$ ; independent of basis coefficients

# Joint Prior Distribution of Coefficients

$$\mathbf{v} = \text{vec} \left( [\mathbf{v}(\mathbf{x}_1); \dots; \mathbf{v}(\mathbf{x}_n)]^T \right)$$

**Define**  $\mathbf{u}(\theta) = \text{vec} \left( [\mathbf{w}(\mathbf{x}_1, \theta); \dots; \mathbf{w}(\mathbf{x}_n, \theta)]^T \right)$

$$\mathbf{w} = \text{vec} \left( [\mathbf{w}(\mathbf{x}_1, \mathbf{t}_1); \dots; \mathbf{w}(\mathbf{x}_m, \mathbf{t}_m)]^T \right)$$

For  $\mathbf{z} = (\mathbf{v}^T, \mathbf{u}^T(\theta), \mathbf{w}^T)^T$ ,

$$\mathbf{z} \sim \mathcal{N} \left( \mathbf{0}, \Sigma_z = \begin{pmatrix} \Sigma_v & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \Sigma_u & \Sigma_{u,w} \\ \mathbf{0} & \Sigma_{u,w}^T & \Sigma_w \end{pmatrix} \right)$$

# Representation of Data and Error Model

Define  $\mathbf{y} = (\mathbf{y}^T(\mathbf{x}_1), \dots, \mathbf{y}^T(\mathbf{x}_n))^T$

$$\eta = (\eta^T(\mathbf{x}_1^c, \mathbf{t}_1), \dots, \eta^T(\mathbf{x}_m^c, \mathbf{t}_m))^T$$

Then  $\begin{pmatrix} \mathbf{y} \\ \eta \end{pmatrix} = \begin{pmatrix} \mathbf{B} & \mathbf{0} \\ \mathbf{0} & \mathbf{K} \end{pmatrix} \mathbf{z} + \begin{pmatrix} \boldsymbol{\epsilon} \\ \boldsymbol{\varepsilon} \end{pmatrix}$

where  $\begin{pmatrix} \boldsymbol{\epsilon} \\ \boldsymbol{\varepsilon} \end{pmatrix} \sim \mathcal{N} \left( \mathbf{0}, \begin{pmatrix} (\lambda_y \mathbf{W}_y)^{-1} & \mathbf{0} \\ \mathbf{0} & \lambda_\eta^{-1} \mathbf{I} \end{pmatrix} \right)$

$\boxed{\mathbf{W}_y = \text{diag}(\mathbf{W}_1, \dots, \mathbf{W}_n)}$

# Likelihood Function: Functional Output

## Likelihood Function

$$L(\theta, \lambda_\eta, \lambda_w, \rho_w, \lambda_y, \lambda_v, \rho_v | \mathbf{y}, \eta) \propto$$

$$|\Sigma_{\widehat{\mathbf{z}}}|^{-1/2} \exp \left\{ -\frac{1}{2} \widehat{\mathbf{z}}^T \Sigma_{\widehat{\mathbf{z}}}^{-1} \widehat{\mathbf{z}} \right\}$$

$$\widehat{\mathbf{z}} = \text{vec} \left( \left[ \left( \mathbf{B}^T \mathbf{W}_y \mathbf{B} \right)^{-1} \mathbf{B}^T \mathbf{W}_y \mathbf{y}; \left( \mathbf{K}^T \mathbf{K} \right)^{-1} \mathbf{K}^T \eta \right] \right)$$

$$\Sigma_{\widehat{\mathbf{z}}} = \Sigma_z + \begin{pmatrix} \left( \lambda_y \mathbf{B}^T \mathbf{W}_y \mathbf{B} \right)^{-1} & \mathbf{0} \\ \mathbf{0} & \left( \lambda_\eta \mathbf{K}^T \mathbf{K} \right)^{-1} \end{pmatrix}$$

# Prior Distributions: Functional Output

## Parameter Prior Distributions

Extension of scalar case, with modified Gamma parameters for  $\lambda_\eta$  and  $\lambda_y$

$$a'_\eta = a_\eta + \frac{m(n_\eta - p_\eta)}{2}$$

$$a'_y = a_y + \frac{n_y - \text{rank}(\mathbf{B})}{2}$$

$$b'_\eta = b_\eta + \frac{1}{2} \eta^T \left( \mathbf{I} - \mathbf{K} \left( \mathbf{K}^T \mathbf{K} \right)^{-1} \mathbf{K}^T \right) \eta$$

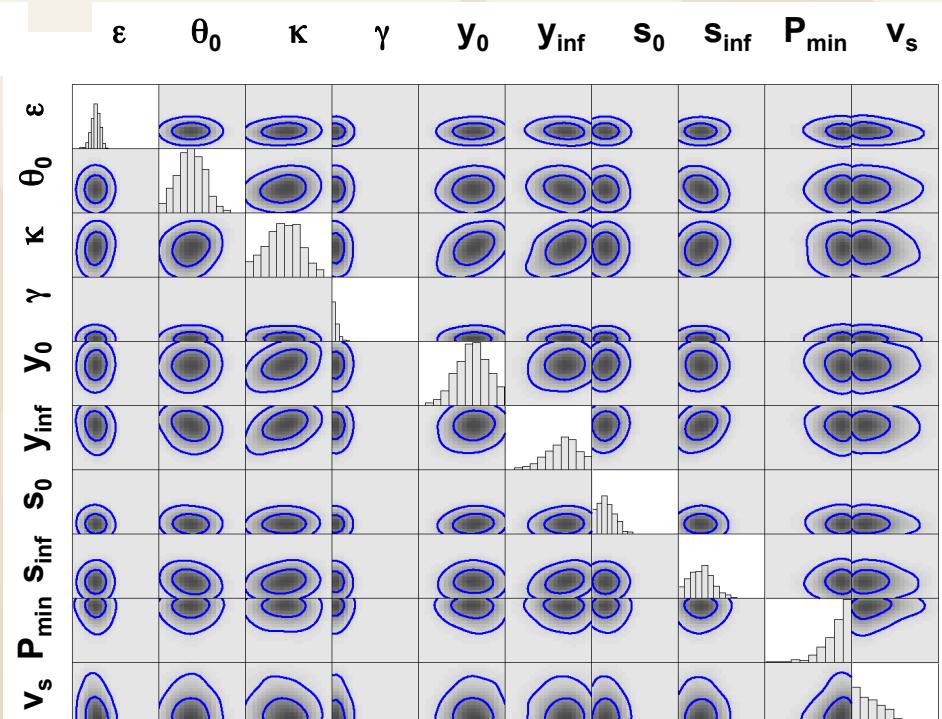
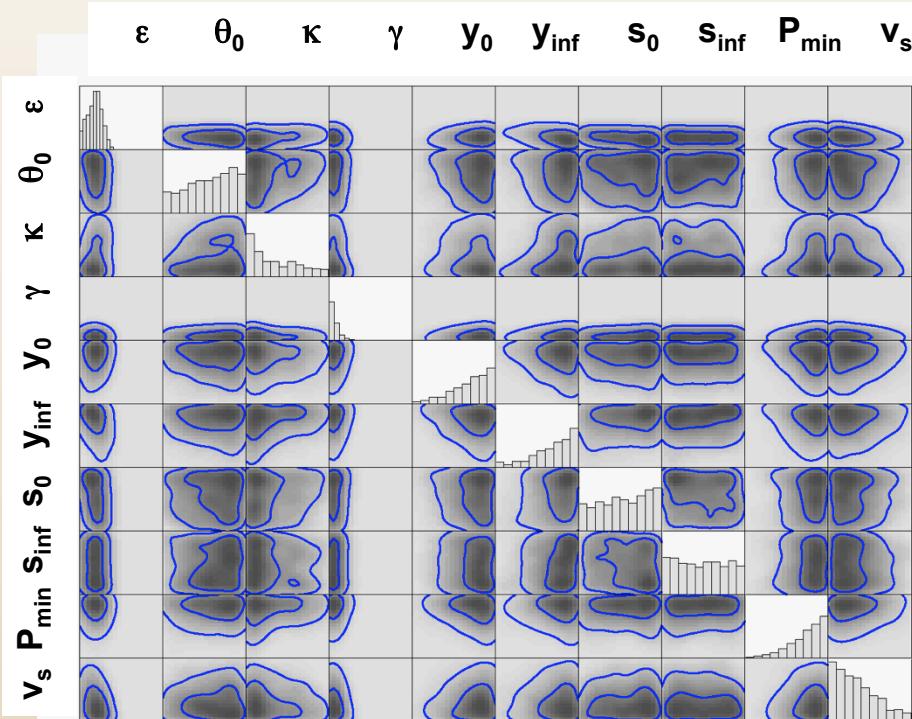
$$b'_y = b_y + \frac{1}{2} \mathbf{y}^T \left( \mathbf{W}_y - \mathbf{W}_y \mathbf{B} \left( \mathbf{B}^T \mathbf{W}_y \mathbf{B} \right)^{-1} \mathbf{B}^T \mathbf{W}_y \right) \mathbf{y}$$

# Phase II: Calibration to Integral Data

Small scale posterior is prior for material strength parameters

Uniform prior for other parameters

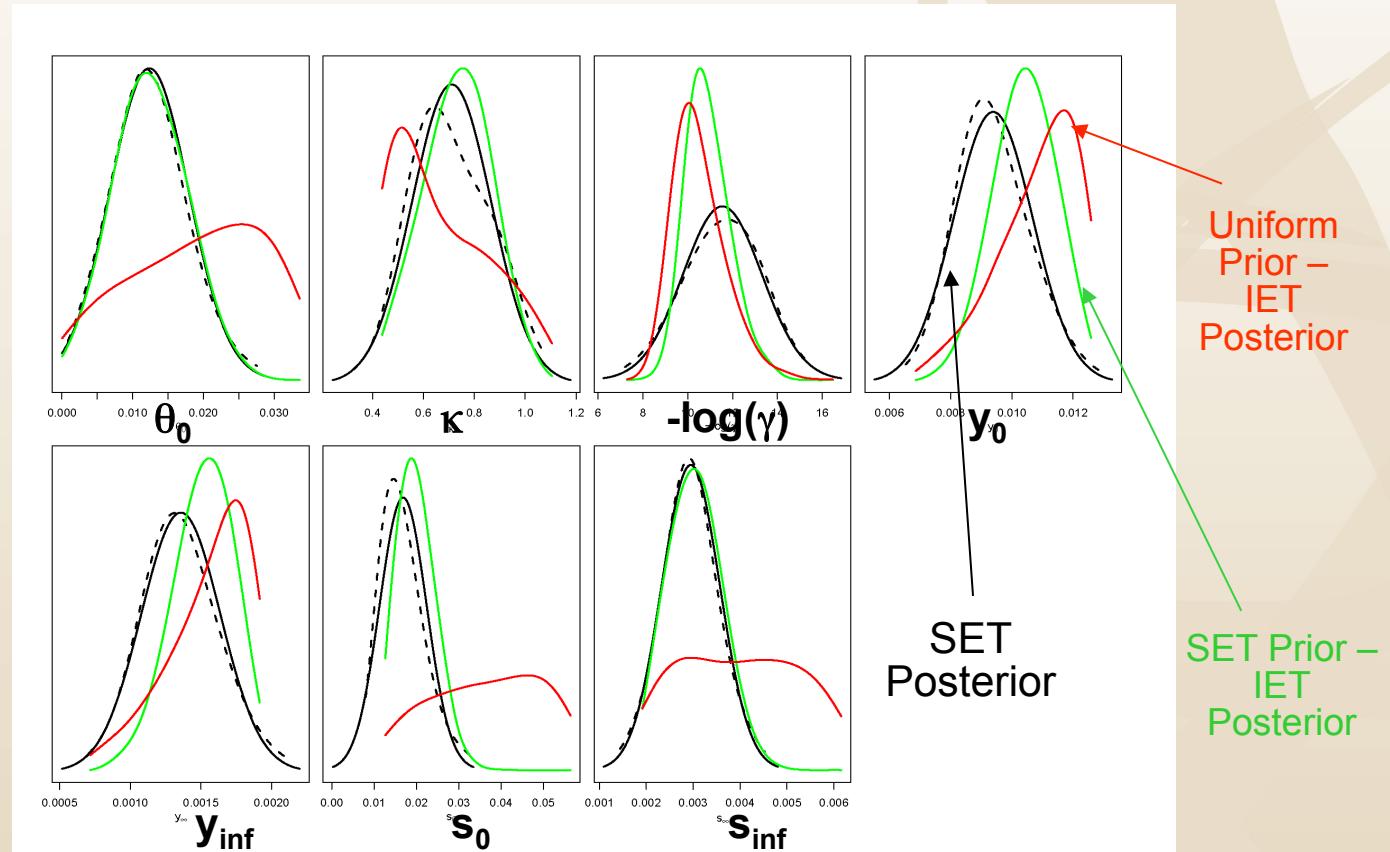
Uniform prior for all parameters



Small-scale data often helps reduce compensating errors

# Marginal Effects of Parameter Prior Assumptions

- Sensitivity to priors
- Same prior and posterior indicates no value for IET

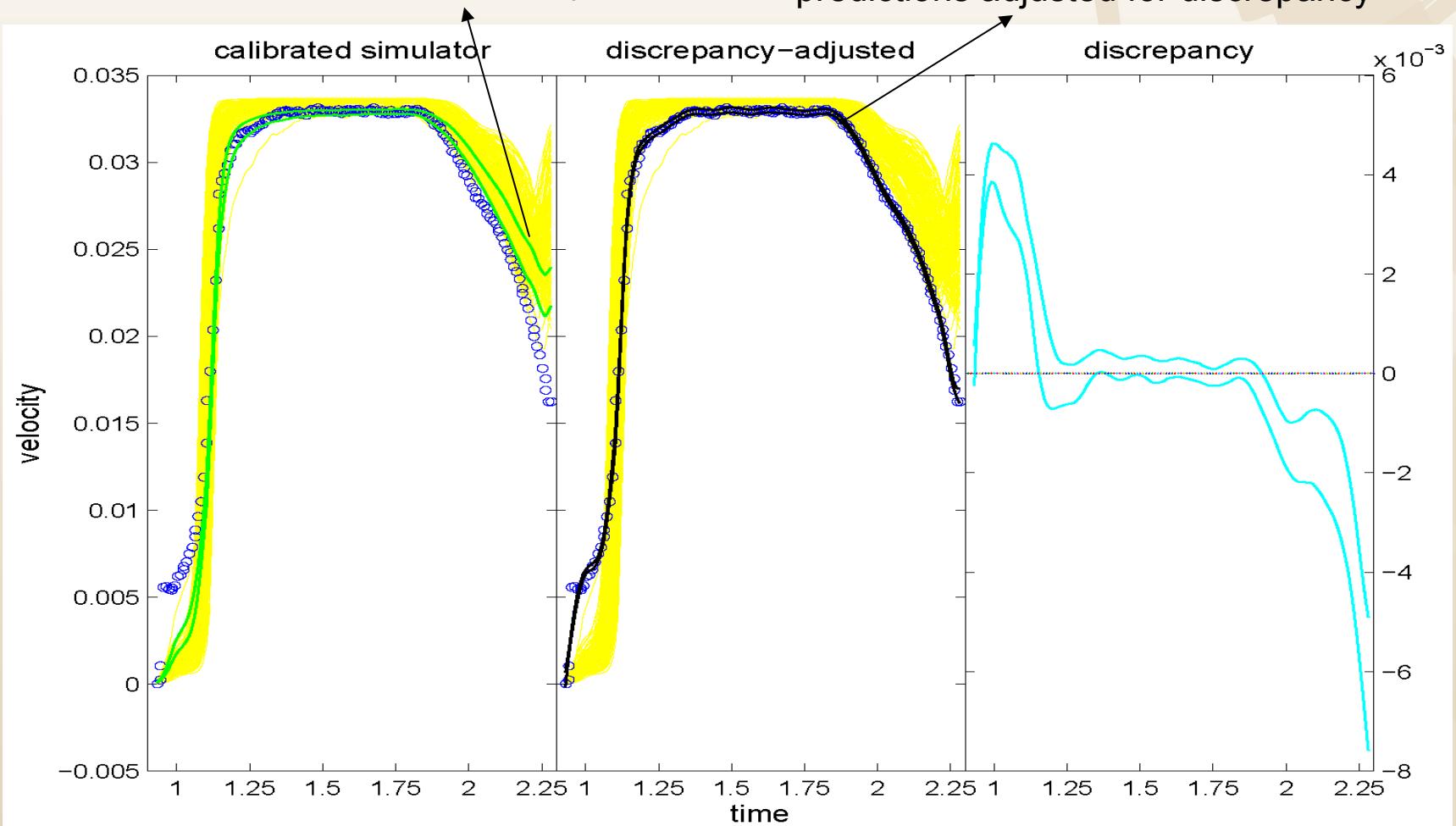


Flyer plate data refines knowledge about activation energy and yield stress parameters

# Calibrated Prediction

5%-95% bounds on calibrated code predictions (no discrepancy)

5%-95% bounds on calibrated code predictions adjusted for discrepancy

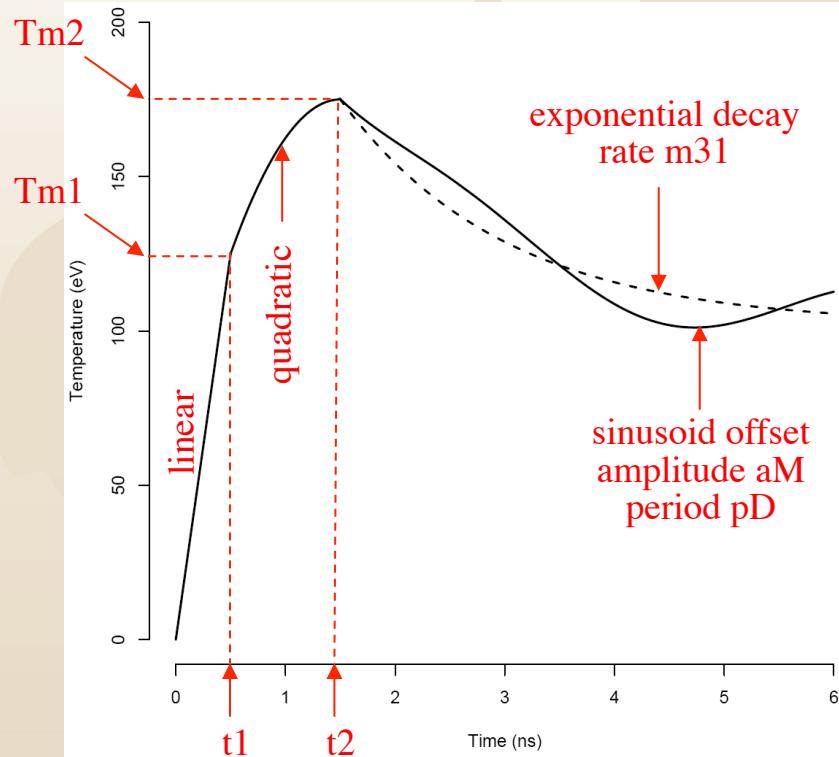
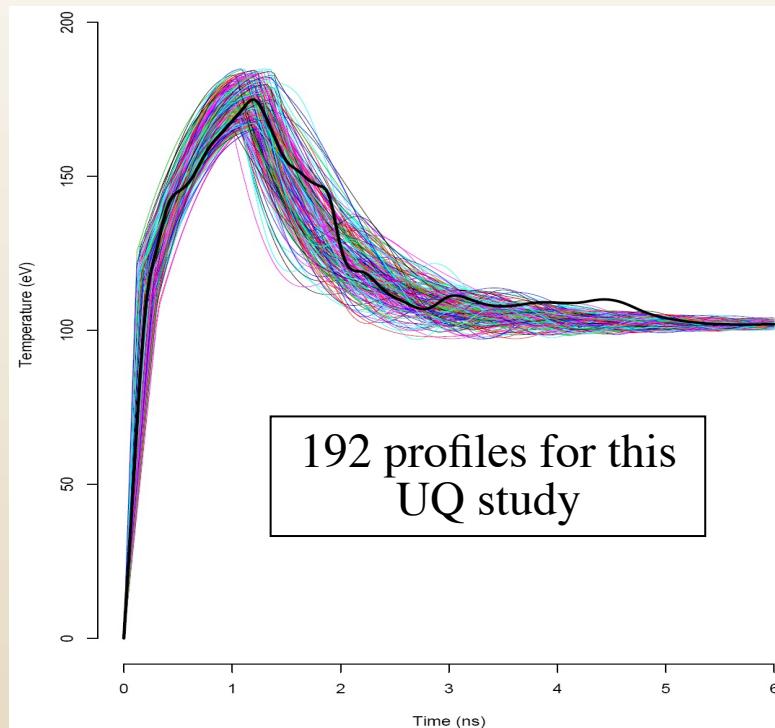


# Implementation Considerations

- Check sensitivity analysis on prior ranges
  - Parameter screening may be important
- Observational error model
- Discrepancy model (if included)
  - Multiple scalars different than functional
- Prior distribution for calibration parameters and statistical model parameters
- Check emulator performance (if code surrogate is required)
  - Cross-validation, out-of-sample validation
- Check posteriors and predictions carefully

# Calibration: A Cautionary Tale

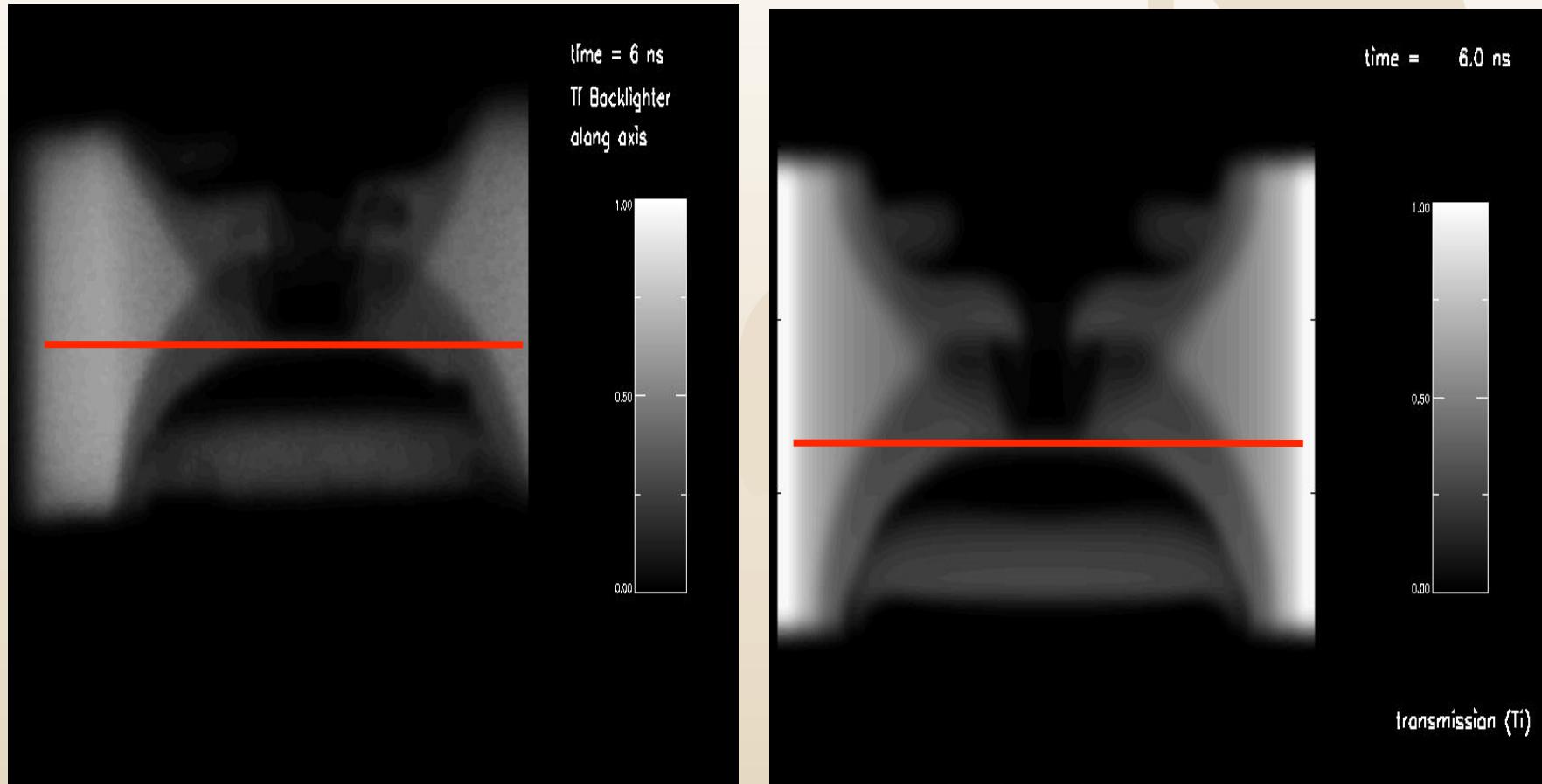
Simulation Input



Drive conditions specified by temperature profiles

- Continuous family of functions indexed by 7 parameters

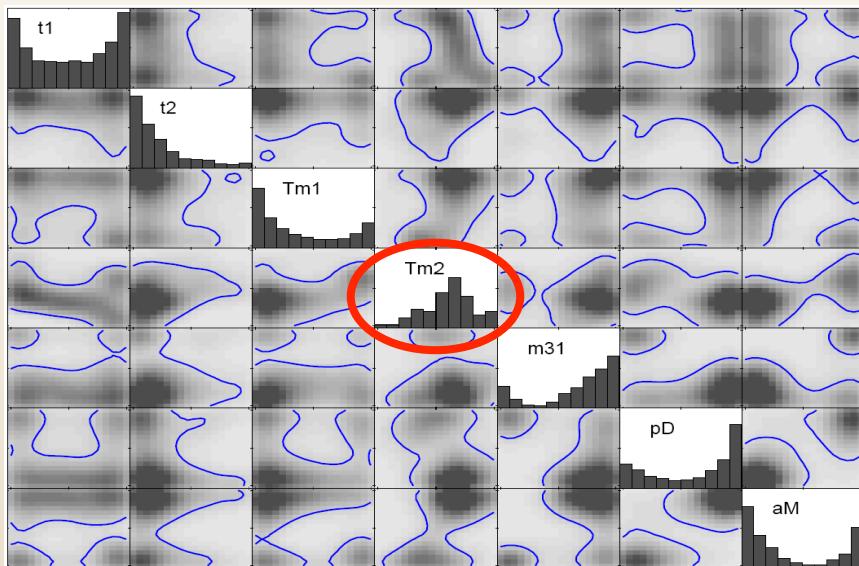
# Data and Simulations are Radiographic Images



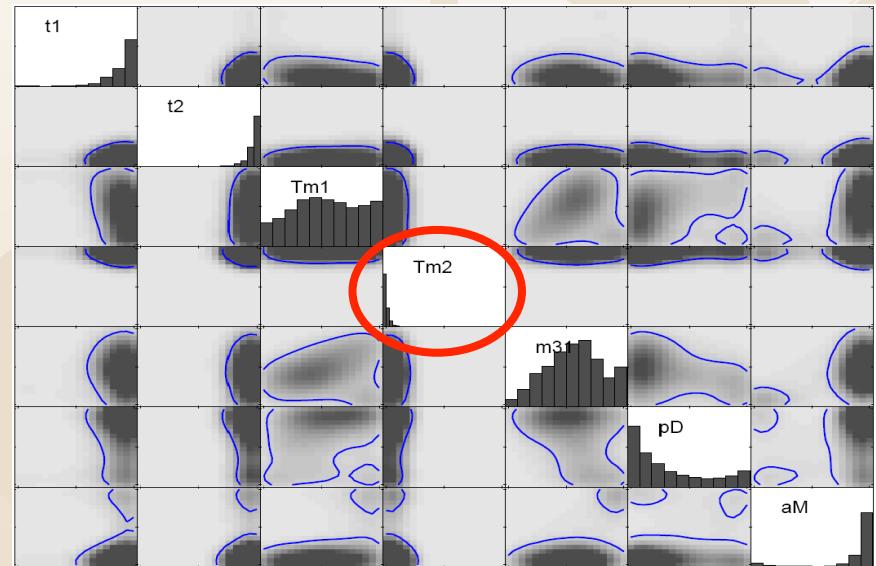
Quantity of Interest is transmission along a selected lineout as a function of distance from centerline

# Statistical Model Permits Tradeoff Between Model Fit and Model Form Error

## No Discrepancy



# Discrepancy



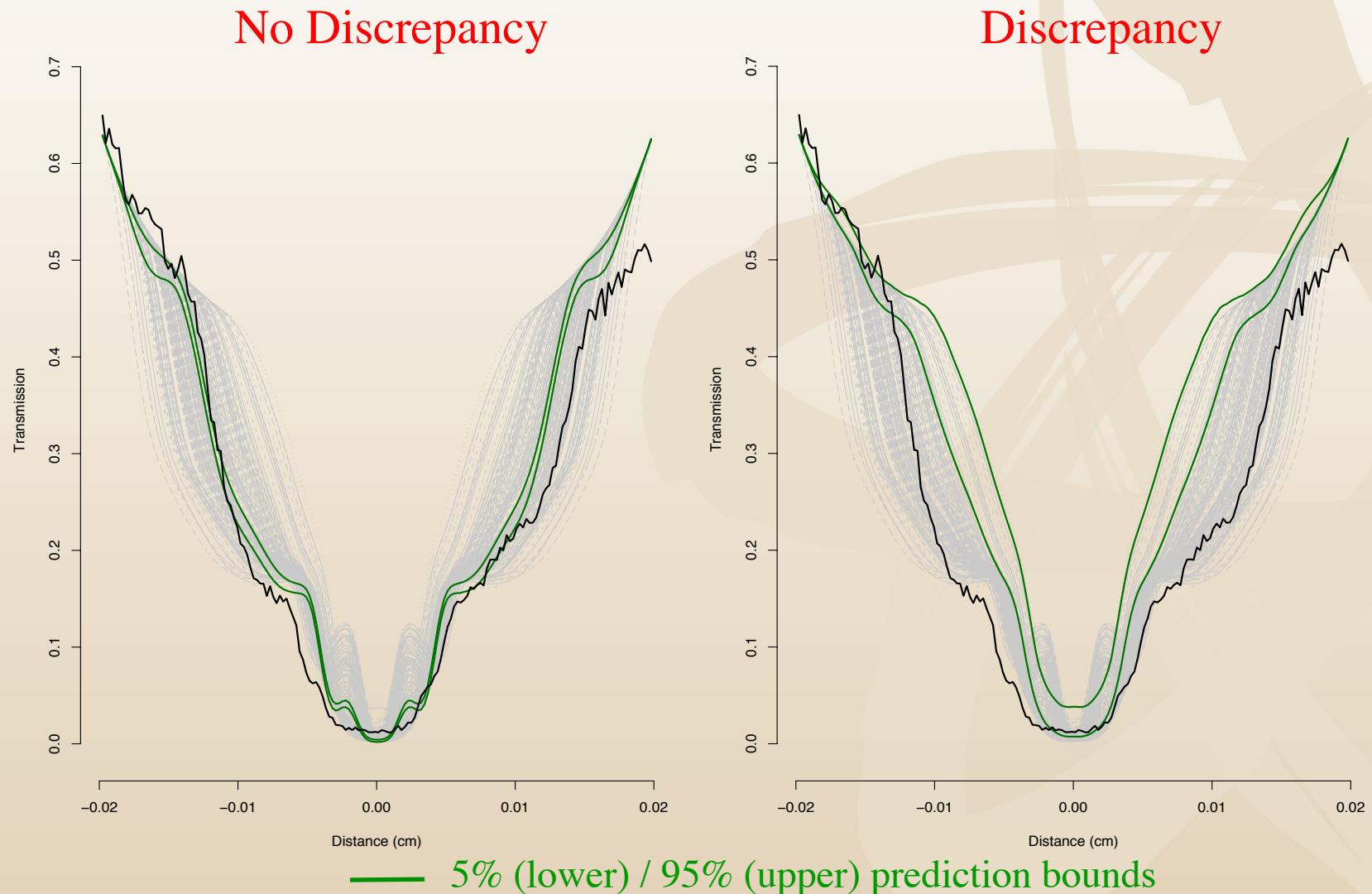
## Substantial difference in the calibrated Tm2 marginal distributions

Would like “data - best code”,  $\chi(\theta) = y - \eta(\theta)$ , small (absolute sense)  
To first order, accomplished for small values of quadratic error:

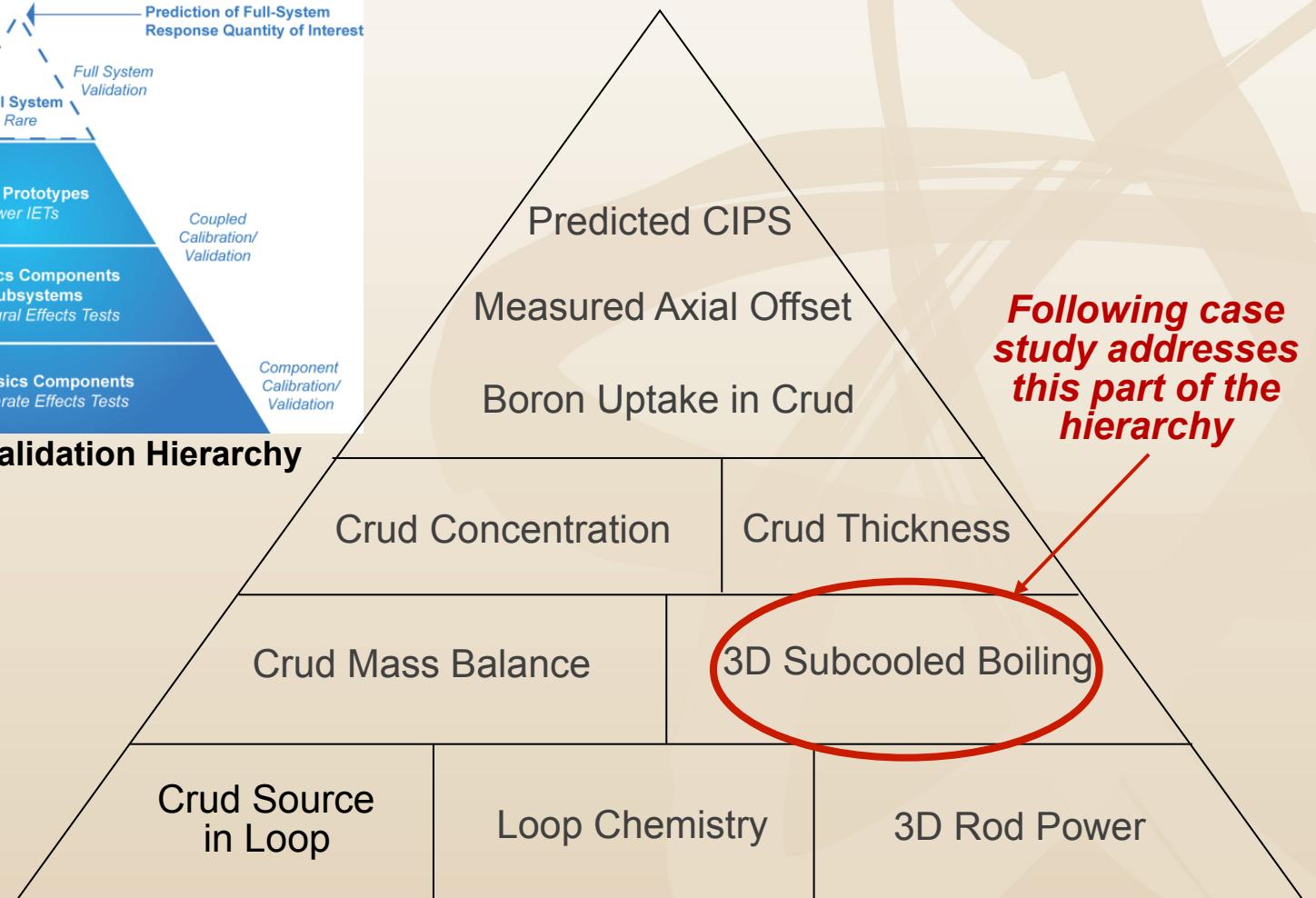
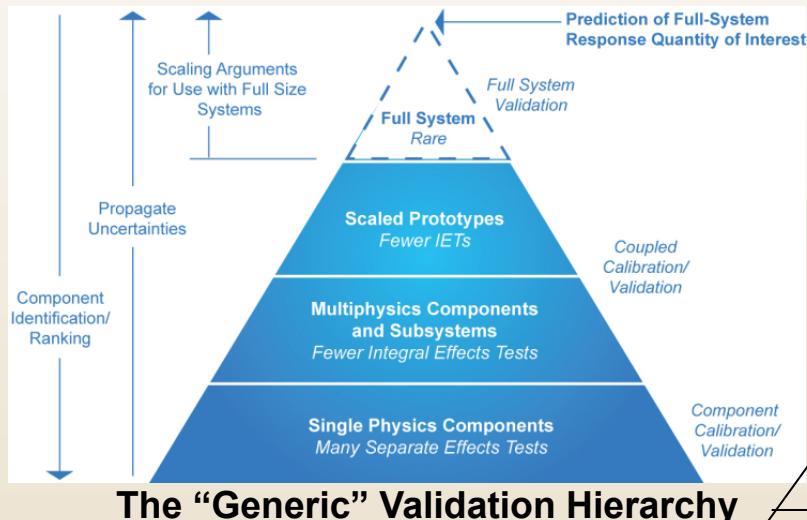
$$Q(\theta, \delta) = (\chi(\theta) - \delta)^T W_y (\chi(\theta) - \delta) + \delta^T W_\delta \delta$$

  discrepancy  
  discrepancy precision  
  field data precision  
  discrepancy precision

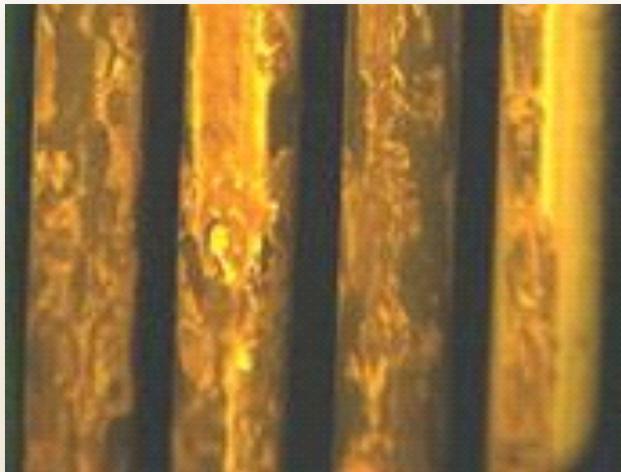
# Undesirable Tradeoff Between Model Fit and Model Form Error



# Calibration Supports Validation of Computational Models

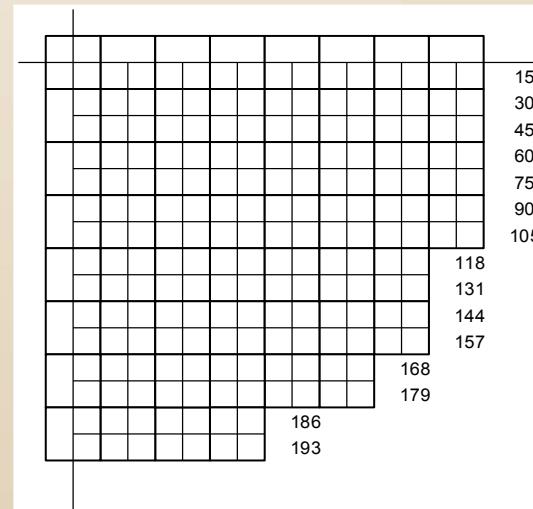


# Validation is a Key Component of Predictive Capability Assessment



**Crud deposits**

**Westinghouse VIPRE-W Thermal-Hydraulics Simulator quarter-core geometry and axial channel layout**



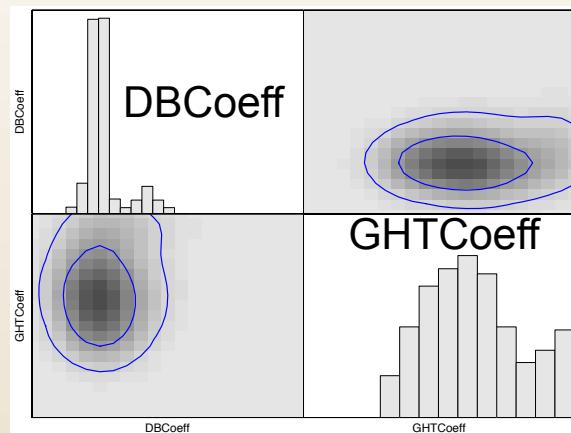
Assess predicted mass evaporation (boiling) rate and compare to Plant B Crud index data

- Calibration to assemblies F71, F22, and F88
- Validation to assembly F09

Parameter	Range
Lead coefficient of Dittus-Boelter Correlation (DBCoeff)	0.019 – 0.033
Lead Coefficient of Grid Heat Transfer Model (GHTCoeff)	2 - 6
Axial Friction Correlation Coefficient (AFCCoeff)	0.1 - 0.25
Lateral Resistance Correlation Coefficient (LRCCoeff)	1.5 - 4
Exponent of Partial Boiling Model (ExpPBM)	1 - 4

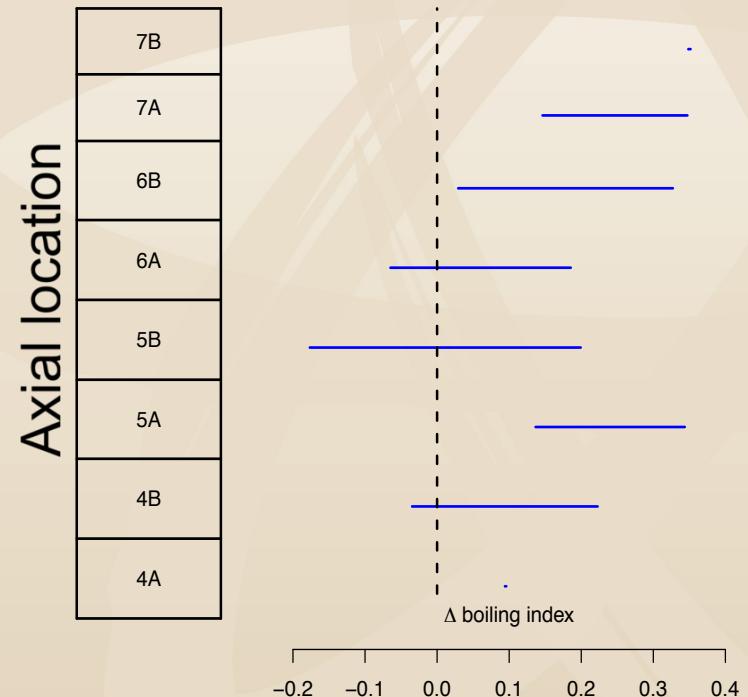
# Calibration Methodology Implemented Treating Boiling/Crud Index as Functional

Crud Index = VIPRE-W Boiling Index (calibration parameters) + Discrepancy + Error

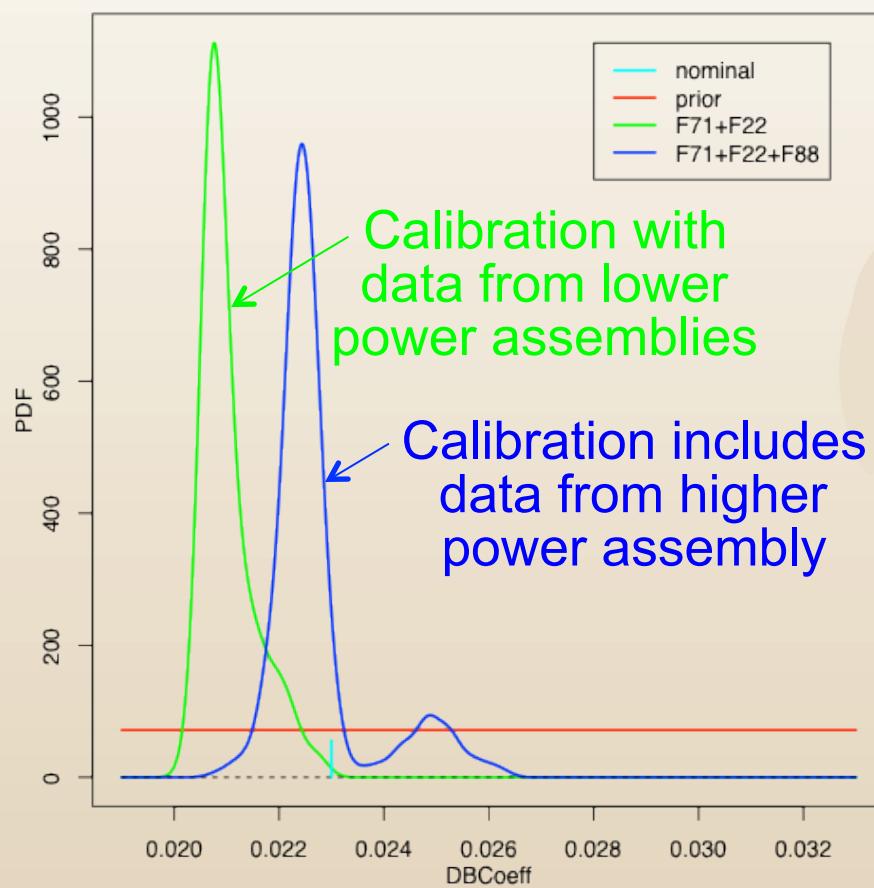


## Sensitivity Analysis

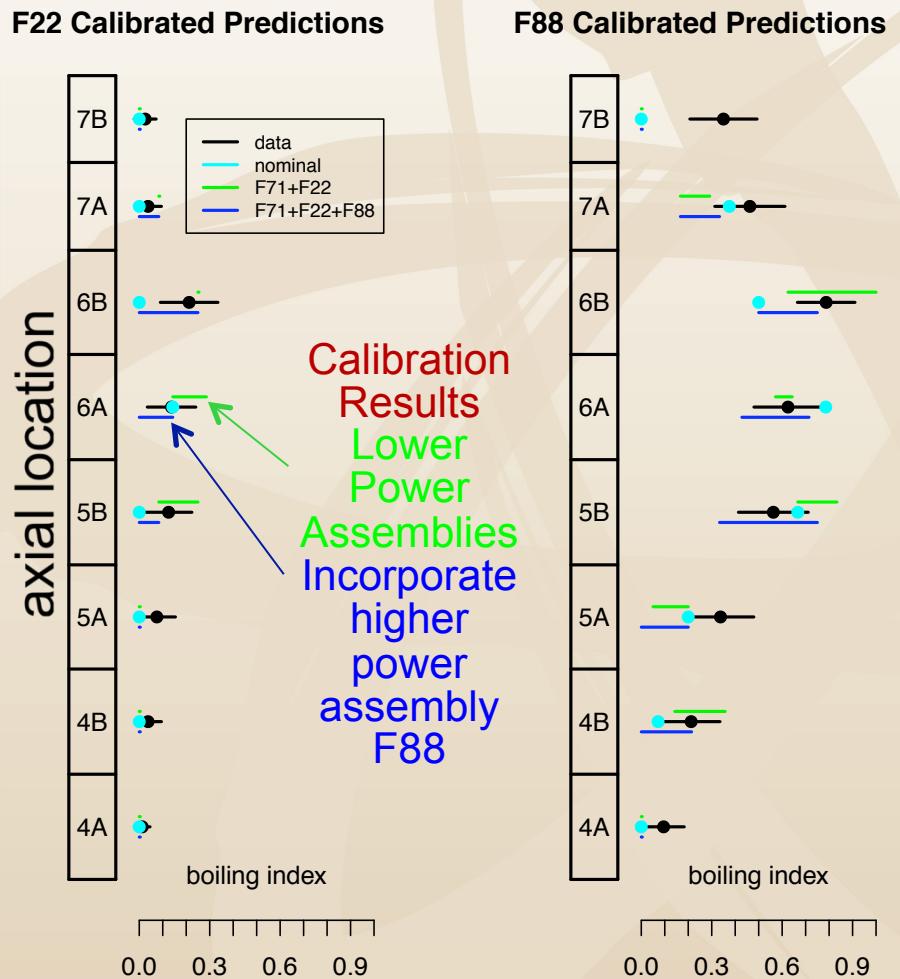
	F71		F22		F88		F09	
Parameter	ME (%)	TE (%)						
DBCoeff	94.8	98.1	93.6	98.1	93.1	96.8	96.6	98.4
GHTCoeff	1.7	4.8	0.4	3.3	2.5	5.6	1.2	2.8
AFCCoeff	0	0.4	0.2	3.2	0.4	1.6	0.3	0.7
LRCCoeff	0	0.4	0.1	2.8	0	0.6	0	0.2
ExpPBM	0	0.3	0.1	2.8	0	0.4	0	0.2



# Calibration Results Strongly Dependent on Reference Experimental Data

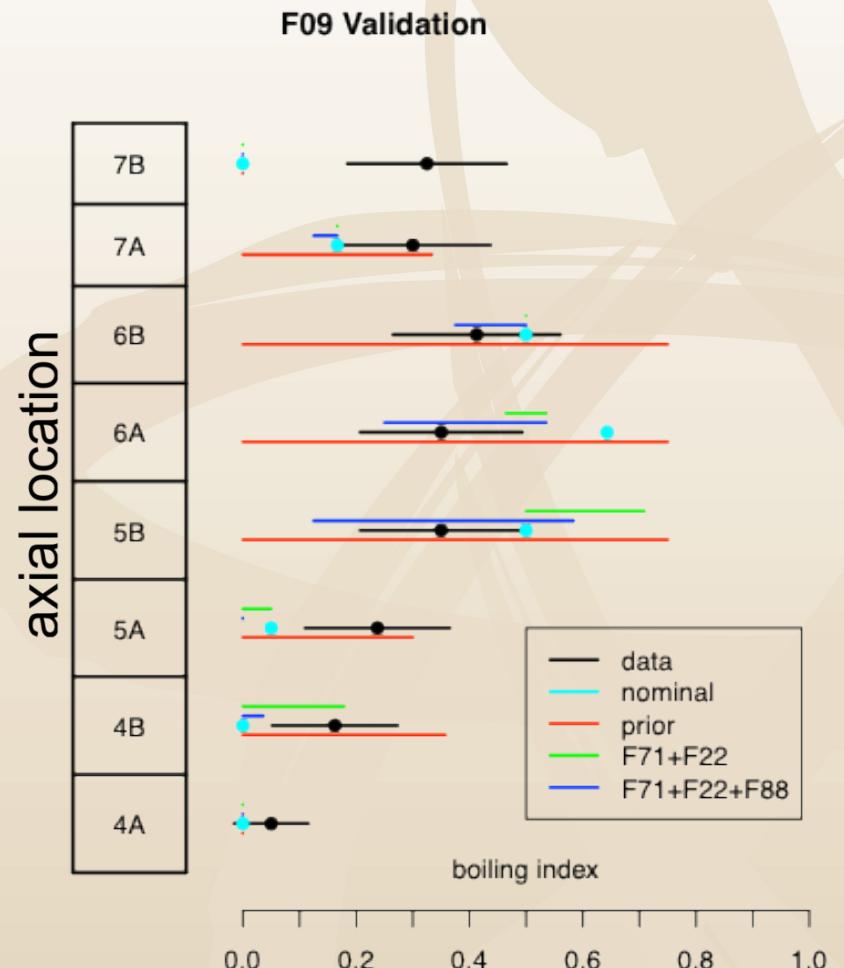
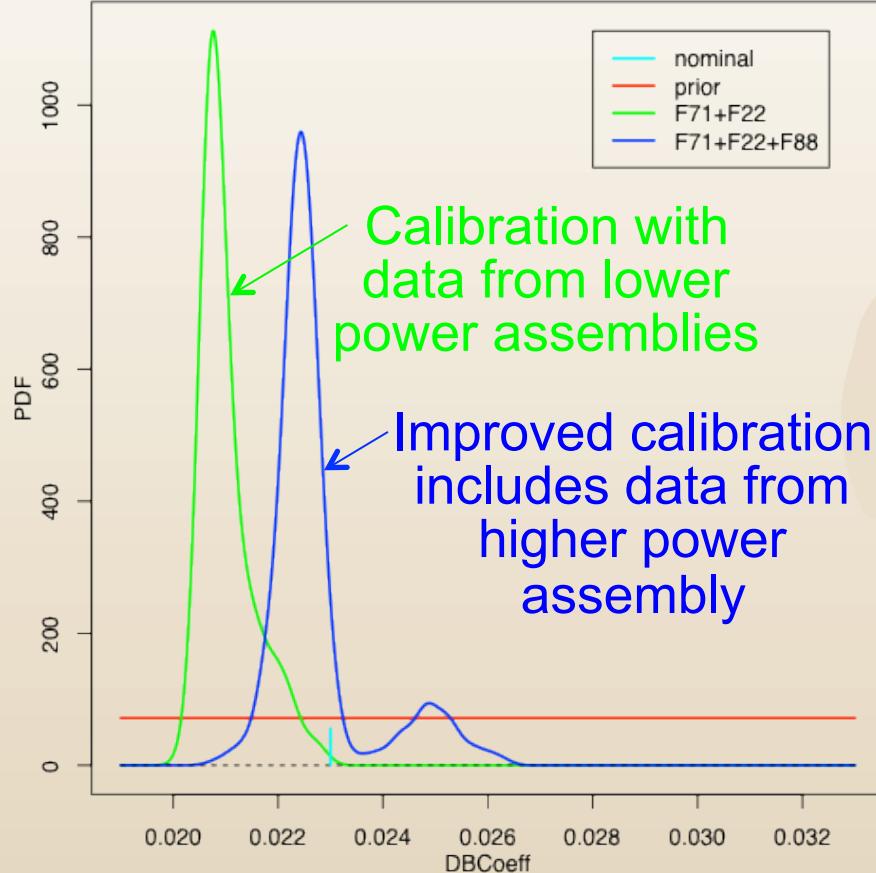


F22 Calibrated Predictions



F88 Calibrated Predictions

# Validation Establishes Domain of Applicability

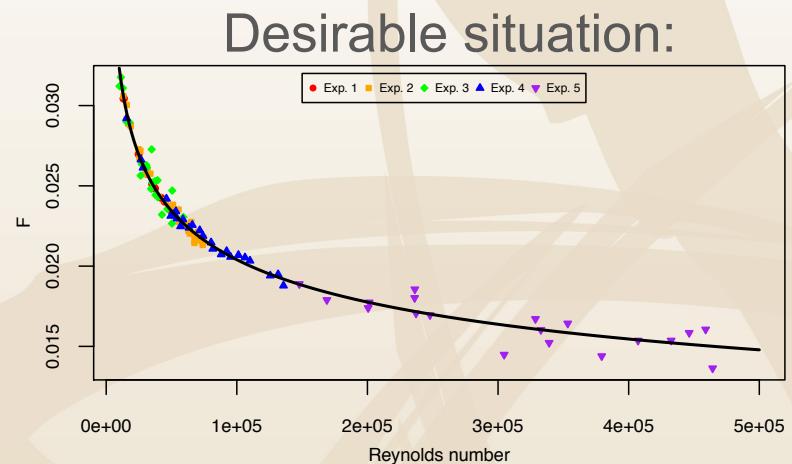
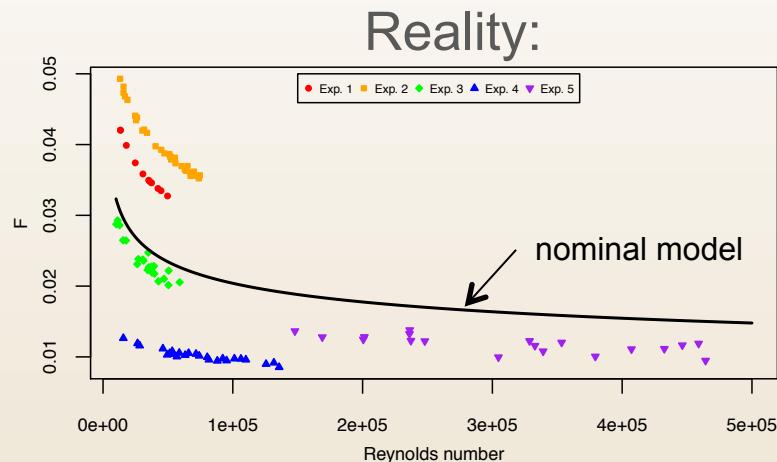


Uncertainties have been reduced (blue vs. red), but predictability not uniformly attained at all locations

# Quantitative Validation Metric

- Let  $p(\mathbf{y}_V | \mathbf{y}_C)$  refer to the predictive distribution of validation data  $\mathbf{y}_V$ , given calibration data  $\mathbf{y}_C$
- Let  $q(\mathbf{y})$  denote a specified reference distribution
- Let  $\mathbf{Y}_V$  denote the observed validation data and define
 
$$S = \left\{ \mathbf{y} : \frac{p(\mathbf{y} | \mathbf{y}_C)}{q(\mathbf{y})} \geq \frac{p(\mathbf{Y}_V | \mathbf{y}_C)}{q(\mathbf{Y}_V)} \right\}$$
- Compute  $\gamma(\mathbf{Y}_V) = 1 - \int_S p(\mathbf{y} | \mathbf{y}_C) d\mathbf{y}$
- If  $\gamma(\mathbf{Y}_V) < T$ , validation data are implausible
  - Threshold  $T$  set to, e.g., 0.05 or 0.01

# Code Calibration in Mixed Effect Settings

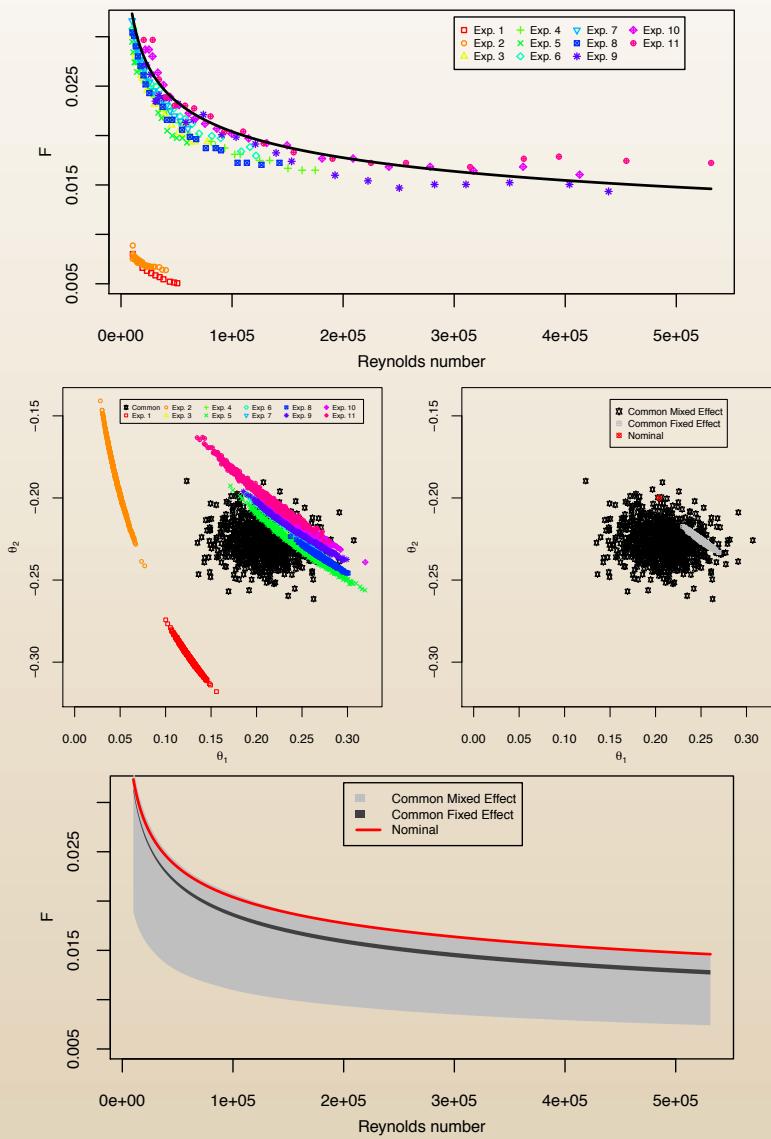


- **Calibration process:**
- Prior distributions on  $\theta$  and  $\lambda$
- Prior distribution on group model parameter perturbations ( $d_i$ ) and covariance matrix parameters ( $\phi$ )
$$d_i|\phi \sim \mathcal{N}(0, \Phi(\phi)), \phi \sim \pi(\phi)$$
- Statistical model for experimental data
$$y_i(x_j) = \eta(x_j, \theta + d_i) + \epsilon_{ij}$$
- Posterior distributions on  $\theta, \lambda, d_i, \phi$
- Statistical model has special case of common  $\theta$  ( $d_i = 0$ )

- **Calibration process:**
- Prior distributions on model parameters ( $\theta$ ) and error precisions ( $\lambda$ )
- Statistical model to explain variation in experimental data
$$y_i(x_j) = \eta(x_j, \theta) + \epsilon_{ij}$$

$$\epsilon_i \sim \mathcal{N}(0, \lambda_i^{-1} I_{n_i})$$
- Posterior distributions on model parameters ( $\theta$ ) and error precisions ( $\lambda$ )

# Calibration of the McAdams Correlation

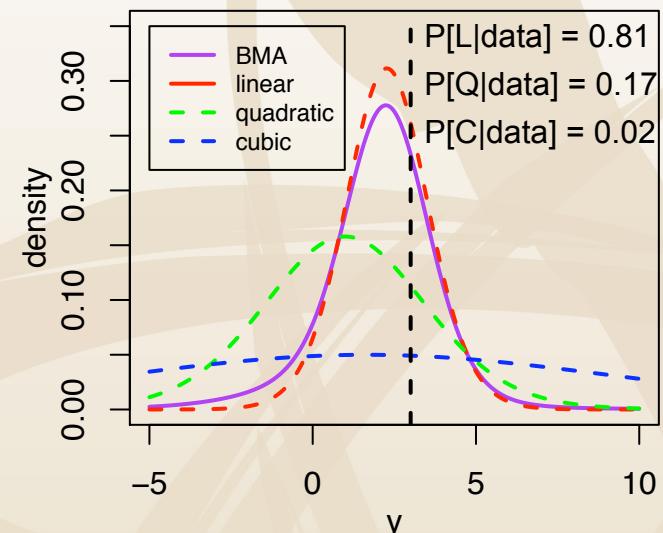
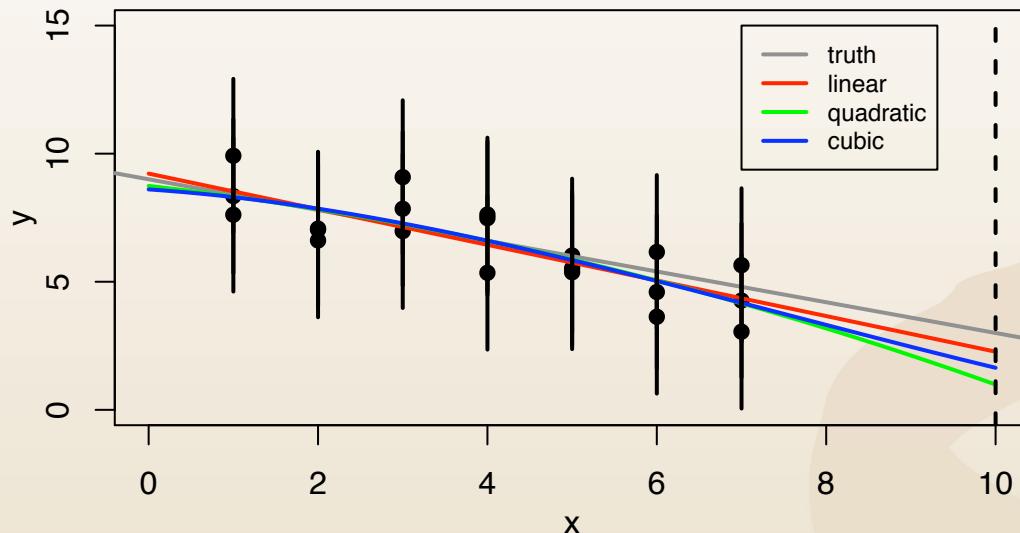


- McAdams is an empirical model for friction due to the boundary layer in forced convection and turbulent flow
  - Friction factor ( $f$ ): Proportionality constant in pressure loss correlation
  - Reynolds number ( $Re$ ): Ratio of inertial to viscous forces
- $$f = \theta_1 Re^{\theta_2}$$
- Prior for  $\theta$ : Uniform on SME provided ranges
- In some cases, residual correlation persists after random effects adjustment
  - Modify error model:
 
$$\epsilon_{ij} = \delta_i(x_j) + \varepsilon_{ij}$$
- Code calibration accounts for differences among relevant experiments while also accounting for model form error

# Software for Code Calibration

- **Software for Code Calibration**
  - Gaussian Process Models for Simulation Analysis
    - Gaussian process-based surrogate models  
<http://www.stat.lanl.gov/source/orgs/ccs/ccs6/gpmsa/gpmsa.html>
  - Bayesian Analysis of Computer Code Output (BACCO)
    - R package implementation of Kennedy-O'Hagan  
<http://cran.r-project.org/web/packages/BACCO>
  - Dakota
    - Sandia National Laboratories optimization and UQ  
<http://dakota.sandia.gov>
  - QUESO
    - UT Austin calibration and UQ  
<https://red.ices.utexas.edu/projects/software/wiki/QUESO>

# Role of Model Form Uncertainty in UQ

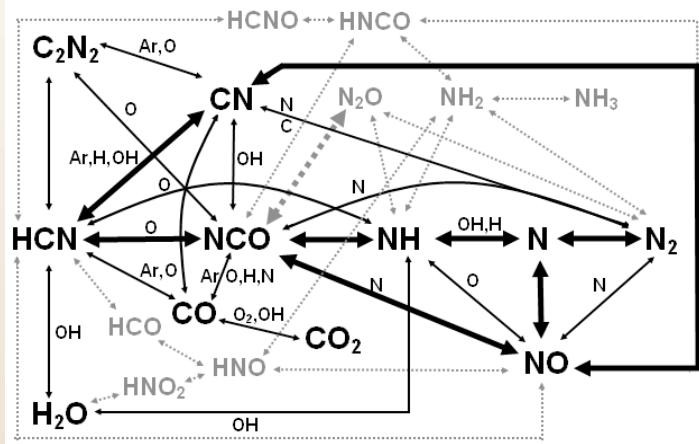


- Model form uncertainty should be incorporated in formal UQ
  - Model form *and* parametric uncertainties should be *simultaneously* calibrated to experimental data
  - Principled methodologies such as Bayesian model averaging

$$p(Y_P | \text{data}) = \underbrace{\sum_{k=1}^K p(M_k | \text{data})}_{\text{predictive performance distribution}} \underbrace{\int p(Y_P | \theta_k, M_k, \text{data}) p(\theta_k | M_k, \text{data}) d\theta_k}_{\text{posterior model probability}} \underbrace{p(Y_P | \theta_k, M_k, \text{data})}_{\text{predictive performance distribution given model } M_k \text{ with parameters } \theta_k}$$

# Example: Calibration and Multi-Model Inference

- HCN/O<sub>2</sub>/Ar kinetics



## 6 Reactions

R1:  $\text{HCN} + \text{Ar} \rightarrow \text{H} + \text{Cn} + \text{Ar}$

R2:  $\text{O}_2 + \text{H} \rightarrow \text{OH} + \text{O}$

R3:  $\text{O}_2 + \text{CN} \rightarrow \text{NCO} + \text{O}$

R4:  $\text{HCN} + \text{O} \rightarrow \text{NCO} + \text{H}$

R5:  $\text{NCO} + \text{Ar} \rightarrow \text{CO} + \text{N} + \text{Ar}$

R6:  $\text{O}_2 + \text{N} \rightarrow \text{NO} + \text{O}$

- Mass reaction rate of  $m$ -th species ( $N_r = 6$ ,  $N_s = 11$ )

$$\frac{d[X_m]}{dt} = \sum_{r=1}^{N_r} \left\{ (\nu''_{m,r} - \nu'_{m,r}) k_{f,r} \prod_{m=1}^{N_s} [X_m]^{\nu'_{m,r}} + (\nu'_{m,r} - \nu''_{m,r}) k_{b,r} \prod_{m=1}^{N_s} [X_m]^{\nu''_{m,r}} \right\}$$

stoichiometric coefficient

- Reaction rate of  $r$ -th reactions

$$k_{f,r} = 10^{A_r} T^{m_r} \exp\left(-\frac{\Theta_r}{T}\right), k_{f,b} = \frac{k_{f,r}}{K_{C,r}} \quad r = 1, \dots, N_r$$

- State equation:  $p = \rho RT$

# Experimental Data

T (K)	[Ar] $\times 10^6$ (mol cm $^{-3}$ )	[HCN]/[O <sub>2</sub> ] (ppm/ppm)	[N] $\times 10^{12}$ mol cm $^{-3}$					
			100 μs	200 μs	300 μs	400 μs	600 μs	800 μs
2233	10.30	200/200	—	—	0.71	1.28	3.30	5.83
2382	9.50		0.97	2.30	4.33	6.50	12.50	21.60
2566	8.62		2.50	9.50	17.00	23.30	29.00	—
2447	9.13	100/100	—	0.82	1.73	2.83	6.50	11.70
2551	8.63		—	1.67	4.08	7.50	13.80	19.00
2690	8.17		1.78	7.00	13.30	20.00	31.60	—
2595	8.37	50/50	—	0.85	1.58	2.76	5.42	8.33
2600	8.36		—	0.70	1.50	2.63	5.67	8.50
2888	7.15		1.55	5.17	10.30	15.80	24.10	25.80
2998	6.80		2.75	9.67	15.80	23.30	—	—
2512	8.67	50/250	—	0.83	1.37	1.92	3.08	4.33
2594	8.28		0.67	1.58	2.83	3.83	5.58	7.75
2760	7.55		2.00	5.00	7.50	9.17	11.70	12.70
3028	6.65		8.50	16.30	20.80	20.00	14.50	9.17
3169	6.12		16.67	25.00	25.00	20.00	10.00	2.75
3391	5.42		23.00	33.30	25.00	14.20	2.42	—
2655	8.08	100/1000	2.50	4.50	6.50	7.83	9.50	8.33
2690	7.93		1.92	4.67	7.83	10.30	10.00	5.33
2718	7.97		3.16	6.17	9.17	11.50	11.30	5.83
2720	7.70		2.42	5.33	8.34	10.30	11.70	8.67
2894	7.15		8.34	13.30	15.80	14.17	5.50	1.00
2962	6.83		9.34	16.20	17.30	12.80	4.40	0.67
2989	6.85		12.00	16.70	17.50	11.70	3.00	1.17
3013	6.62		14.20	18.30	15.00	9.67	1.17	—
3110	6.23		19.00	19.20	13.30	5.83	—	—
2833	7.42	25/1000	—	1.41	1.58	1.67	1.70	1.41
3009	6.83		2.50	2.92	2.83	2.47	1.67	0.83
3241	5.97		5.67	4.83	3.33	1.67	—	—

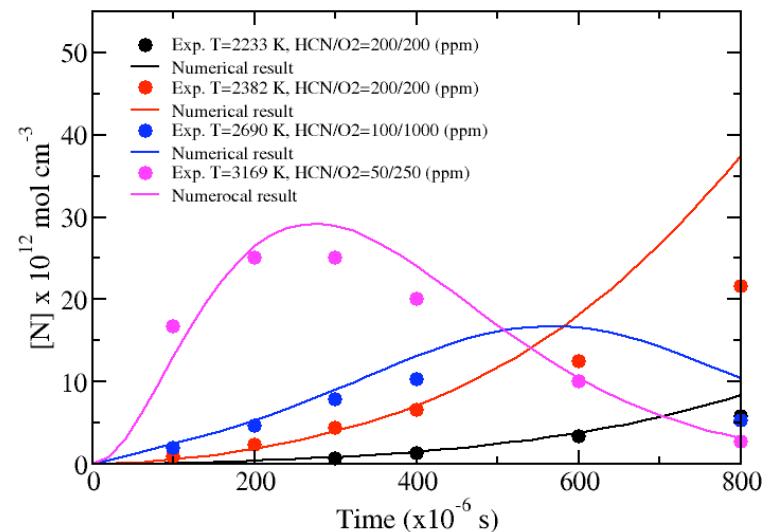


Figure: Comparison experimental data and model result

- Experimental data available ([O], [N], and [H]) for different initial conditions
  - $N_{\text{exp}} = 79$  data sets, each set has time history data at  $N_T = 6$  time points

# Stochastic Models

- General form of stochastic models

$$\mathbf{x}(0) = \mathbf{x}(0; \mathbf{u}(0))$$

$$\mathbf{x}(t) = \mathbf{f}(t, \mathbf{x}(t), \mathbf{u}(t), \gamma(t), \boldsymbol{\theta}) \in \Re^{N_s}$$

$$\mathbf{y}(t) = \mathbf{h}(t, \mathbf{x}(t), \mathbf{u}(t), \varepsilon(t), \boldsymbol{\theta}) \in \Re^{N_o}$$

[stochastic dynamic model]

[observation equation]

- Definitions

- $t$  = time
- $\mathbf{x}(t)$  = model state vector at time  $t$
- $\mathbf{y}(t)$  = measured output vector at time  $t$
- $\mathbf{u}(t)$  = system input vector (eg. temperature, pressure, etc.) at time  $t$
- $\boldsymbol{\theta}$  = uncertain model parameters (calibration)
- $\gamma(t) \in \Re^{N_s}$  = model equation error function/noise at time  $t$
- $\varepsilon(t) \in \Re^{N_o}$  = output equation error function/noise at time  $t$

# Model Class

- $M_1$ - $M_4$ 
  - Multiplicative error function in output equations  $y(t) = x(t) \gamma(t) \varepsilon(t)$
  - 11 uncertain parameters (including the physical parameters  $A_i$ ,  $m_i$ , and  $\Theta_i$  ( $i = 1, 3, 4$ ) and the error function variances  $\sigma_s^2$  and  $\sigma_o^2$ )
- $M_5$ 
  - Same as  $M_3$  except different error structure  $y(t) = x(t) (1 + \gamma(t)) + \varepsilon(t)$
- $M_6$ 
  - Same as  $M_3$  except obs. errors have a covariance structure in time
- $M_7$ 

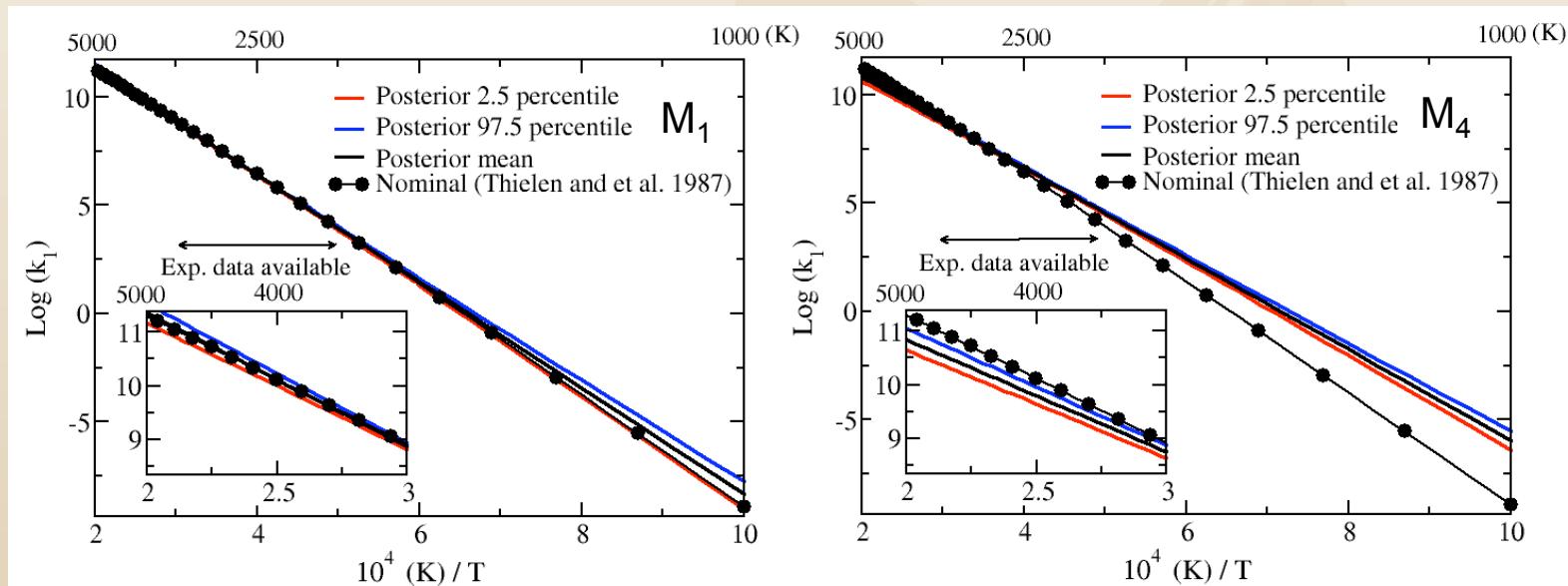
$$\text{cov}(\varepsilon(t_m), \varepsilon(t_n)) = \sigma_o^2 \exp\left[-\left(\frac{|t_m - t_n|}{l_o}\right)^{r_0}\right]; \quad \sigma_o^2, l_o, r_0 \text{ uncertain}$$
  - Same as  $M_6$  with modified state equation  $x_k(t) = f_k(t, \mathbf{x}(t), \mathbf{u}(t), \boldsymbol{\theta}) \exp(\gamma_k(t))$
  - $\gamma_k(t)$  modeled as a Gaussian process
  - Cross-correlation structure

$$\text{cov}(\gamma_k(t_m), \gamma_l(t_n)) = \sigma_s^2 \exp\left[-\left(\frac{|t_m - t_n|}{l_s}\right)^{r_s}\right]; \quad \sigma_s^2, l_s, r_s \text{ uncertain}$$

# Model Plausibility

- Reaction rates are sensitive to choice of hypotheses
  - Uncertainties quantified: parametric, model and observational errors, and model form

	$M_1$	$M_2$	$M_3$	$M_4$	$M_5$	$M_6$	$M_7$
$\log(L(M_j   \text{data}))$	-264.0	-264.6	-256.9	-269.2	-313.5	-260.6	-249.0
$P(M_j   \text{data})$	3.1e-7	1.7e-7	3.7e-4	1.7e-9	0	9e-6	0.9996



Courtesy: Bob Moser

# Predictive Maturity

- Efficiently achieve accuracy in global predictions of **discrepancy**, calibrated code, or physical reality

$$y(x_i) = \eta(x_i; \theta) + \delta(x_i) + \varepsilon(x_i) \text{ for } i = 1 \dots N_{\text{Tests}}$$

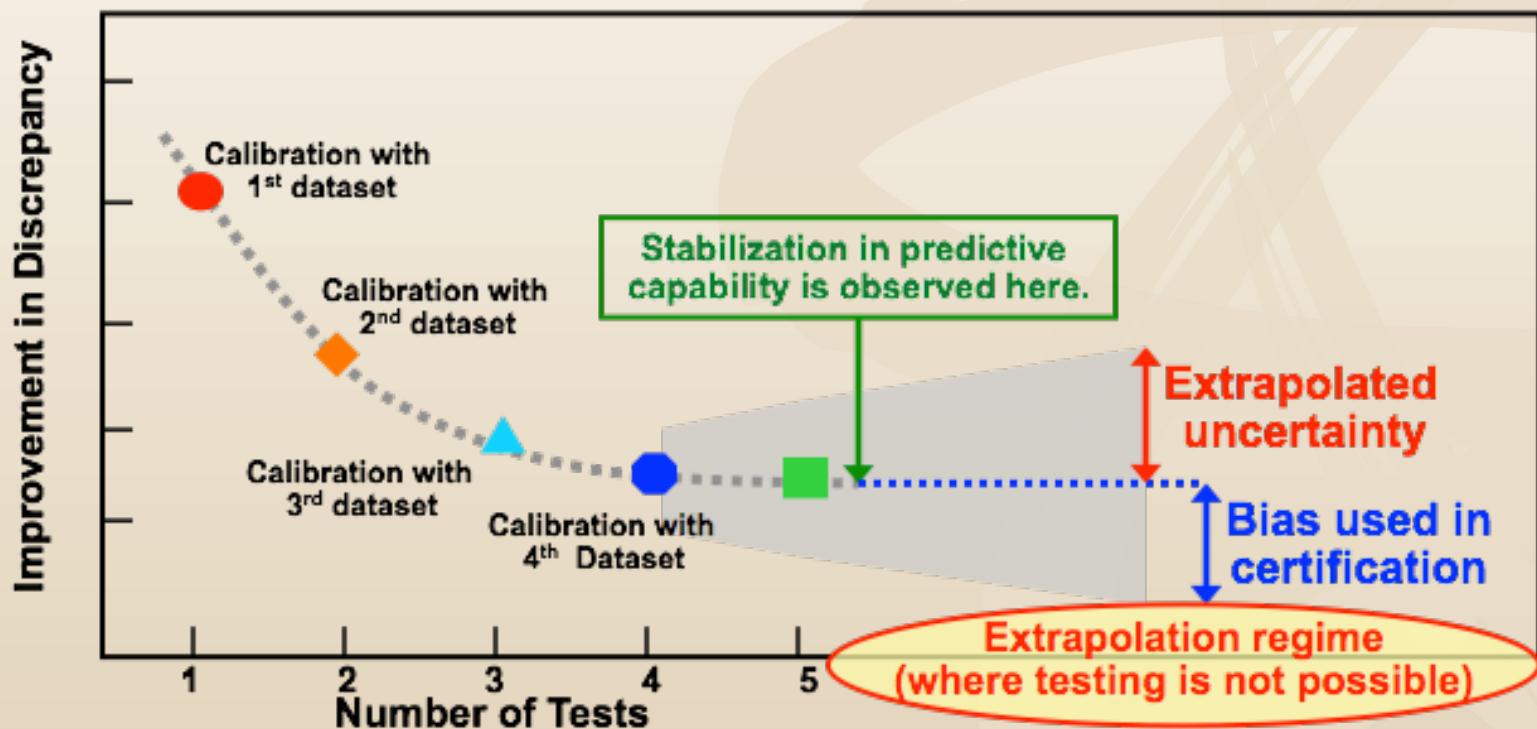


Figure: F. Hemez

# Experiment Design Strategies

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- Several options exist if given a fixed experimental budget
  - single-stage design
    - space-filling LHD, Sobol' sequence, scrambled Sobol' sequence
  - sequential design
    - Initial space-filling design followed by sequential augmentation
- Sequential design required for augmenting existing data
  - Design criteria used for augmentation
    - distance-based criteria
    - IMSE, MMSE
    - Minimum information gain, Maximum entropy
    - Lam and Notz (2008) EIGF criterion
  - Batches of runs desired

# A Batch Sequential Algorithm

---

- Estimate model parameters using runs from initial design  $X_0$
- Set  $X_1 = (X_0^t, X_b^t)^t$  and obtain  $X_b$  by optimizing a design criterion with respect to the proposed  $b$  additional runs
- Collect runs from  $X_b$  and re-estimate model parameters using the entire set of runs from the augmented design  $X_1$
- Set  $X_0$  to the augmented design  $X_1$  and repeat steps (2)-(3) until termination
  - stopping criteria: experiment budget expended, insignificant improvement in design criterion value

# Optimization: Modified Federov Exchange

---

Initialize  $\mathbf{x}_1^*, \dots, \mathbf{x}_b^*$ .

While ( $\Delta\text{Criterion} > \text{Stopping Value}$  &  $\text{Count} < \text{MaxCount}$ )

    For  $i = 1, \dots, b$

        Optimize Criterion w.r.t.  $\mathbf{x}_i^*$ ,  
        holding all other input vectors fixed.

    End

    Compute  $\Delta\text{Criterion}$ .

End

Return optimized  $\mathbf{x}_1^*, \dots, \mathbf{x}_b^*$  and Criterion.

# Batch Sequential Expected Improvement Criteria

- Expected improvement criteria are typically formulated as one-step iterations

Choose next design site  $\mathbf{x}$  to *maximize*  $E [I(\mathbf{x})|\mathbf{y}_2]$



Improvement Function

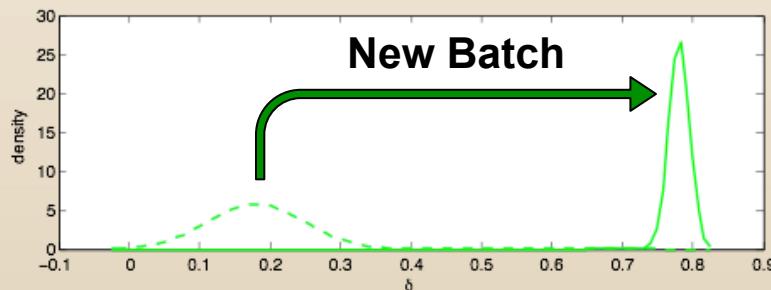
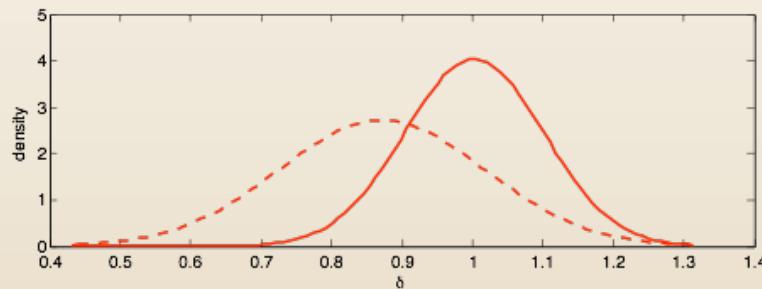
Current Data

- Straightforward extension allows for batch updates

Choose next design sites  $\mathbf{x}_1^*, \dots, \mathbf{x}_b^*$  to *minimize* the *maximum*  $E [I(\mathbf{x}|\mathbf{x}_1^*, \dots, \mathbf{x}_b^*)|\mathbf{y}_2]$

# Bayesian Design

- Consider impact of a new batch of data on prediction at arbitrary input  $\mathbf{x}$  in design region
- Improvement function:



“Maximize the minimum information gain”

$$I = -\log \left( \frac{\pi(\mathbf{y}_1|\mathbf{y}_2, \mathbf{y}_3)}{\pi(\mathbf{y}_1|\mathbf{y}_2)} \right)$$

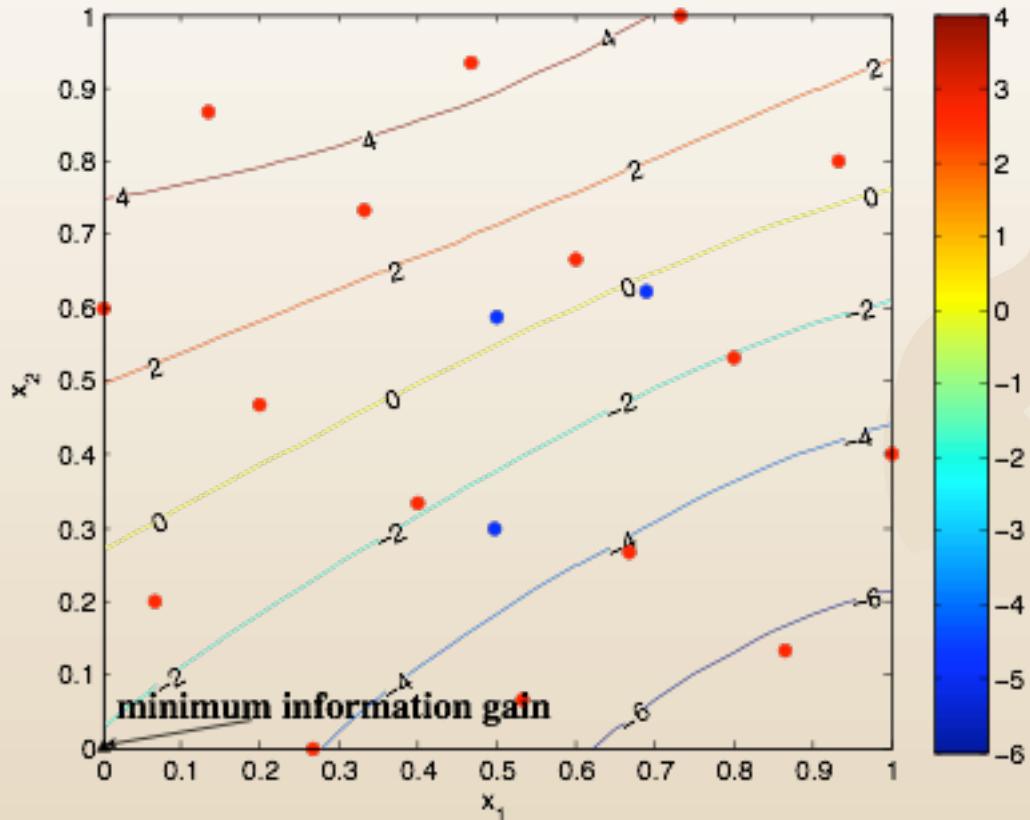
$\mathbf{y}_1$ : output predicted at input  $\mathbf{x}$

$\mathbf{y}_2$ : current data

$\mathbf{y}_3$ : hypothetical data from new batch

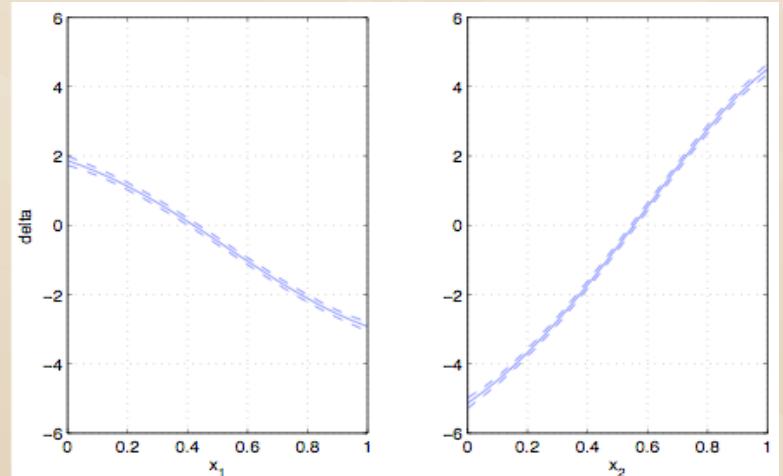
Choose batch  $\mathbf{x}_1^*, \dots, \mathbf{x}_b^*$  to minimize  $\max_{\mathbf{x}} E(I|\mathbf{y}_2)$

# Example: Bayesian Design



- 2 x, 1 θ
- 16 initial experiments
- 3 new experiments
- Use IG criterion
- Minimum IG: 0.044

Main Effect Functions



# Sequential Design for Optimal Calibration

- Utility function defined as entropy loss due to new data  $\mathbf{y}_3$

$$U(\mathbf{y}_3) = \int_{\Theta} \pi(\theta | \mathbf{y}_2, \mathbf{y}_3) \log \pi(\theta | \mathbf{y}_2, \mathbf{y}_3) d\theta - \int_{\Theta} \pi(\theta | \mathbf{y}_2) \log \pi(\theta | \mathbf{y}_2) d\theta$$

- Compute expected utility with respect to unknown future observations

$$E [ U(\mathbf{y}_3) | \mathbf{y}_2 ] = \int \int_{\Theta} \pi(\theta, \mathbf{y}_3 | \mathbf{y}_2) \log \frac{\pi(\theta, \mathbf{y}_3 | \mathbf{y}_2)}{\pi(\theta | \mathbf{y}_2) \pi(\mathbf{y}_3 | \mathbf{y}_2)} d\theta d\mathbf{y}_3$$

- Mutual information between model parameters  $\theta$  and new data  $\mathbf{y}_3$  given available data  $\mathbf{y}_2$
- Smaller expected utility implies new data  $\mathbf{y}_3$  does not inform as well about model parameters  $\theta$  given available data  $\mathbf{y}_2$

Choose batch  $\mathbf{x}_1^*, \dots, \mathbf{x}_b^*$  to maximize  $E [ U(\mathbf{y}_3) | \mathbf{y}_2 ]$

# Data Assimilation Framework

---

- Time steps  $t = 1, 2, \dots$ 
  - State vector  $\{\theta_1, \theta_2, \dots\}$  and observations  $\{y_1, y_2, \dots\}$
- Prior model for state process
  - $\pi(\theta_1)$  and  $\pi(\theta_t | \theta_{t-1})$
- Observational data model
  - $y_t = \eta(\theta_t) + e_t ; e_t \text{ iid } N(0, \Sigma_y)$
- **Goal:** At each time  $t$ , produce draws from  $\pi(\theta_t | y_{1:t})$ 
  - $y_{1:t}$  denotes all data up to time  $t$

# Data Assimilation Algorithm

---

1. At time  $t - 1$ , the ensemble of state vectors  $\{\theta_{t-1,1}^{(1)}, \dots, \theta_{t-1,M}^{(1)}\}$  are treated as draws from  $\pi(\theta_{t-1} | \mathbf{y}_{1:t-1})$
2. Propagate each  $\theta_{t-1,k}^{(1)}$  according to  $\pi(\theta_t | \theta_{t-1})$ , producing an ensemble of draws  $\{\theta_{t,1}^\circ, \dots, \theta_{t,M}^\circ\}$ , from  $\pi(\theta_t | \mathbf{y}_{1:t-1})$
3. Given observations  $\mathbf{y}_t$ , update each  $\theta_{t,k}^\circ$ , producing an ensemble  $\{\theta_{t,1}^{(1)}, \dots, \theta_{t,M}^{(1)}\}$  from  $\pi(\theta_t | \mathbf{y}_{1:t})$

# Filtering Methods

- **Particle Filter**

Sample from  $\{\theta_{t,1}^\circ, \dots, \theta_{t,M}^\circ\}$  according to importance weights  $\{w_1, \dots, w_M\}$  given by

$$w_k \propto \exp \left[ -\frac{1}{2} (\mathbf{y}_t - \eta(\theta_{t,k}^\circ))^T \Sigma_y^{-1} (\mathbf{y}_t - \eta(\theta_{t,k}^\circ)) \right]$$

- **Ensemble Kalman Filter (EnKF)**

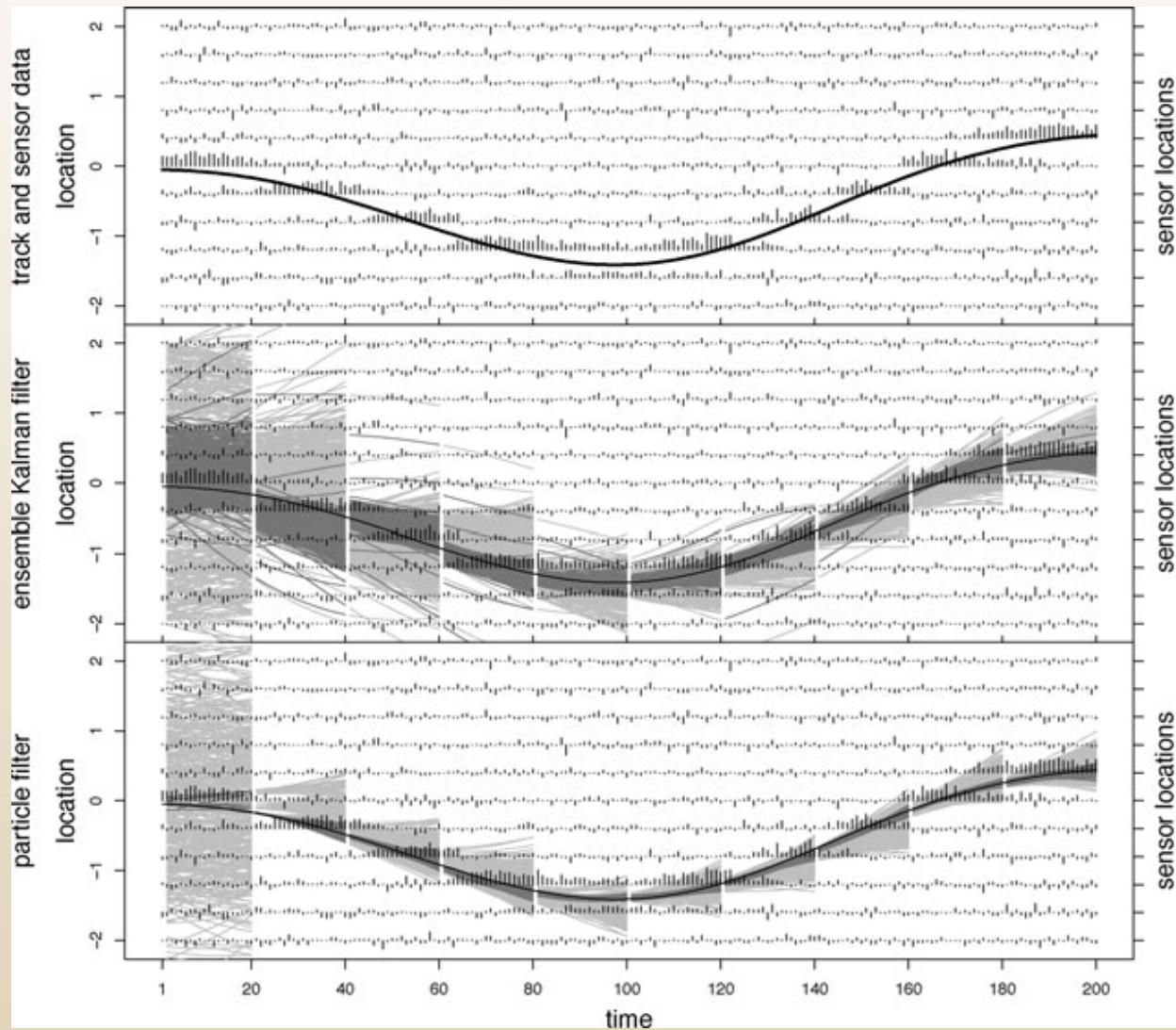
1. From  $\left\{ \begin{pmatrix} \theta_{t,1}^\circ \\ \eta(\theta_{t,1}^\circ) \end{pmatrix}, \dots, \begin{pmatrix} \theta_{t,M}^\circ \\ \eta(\theta_{t,M}^\circ) \end{pmatrix} \right\}$  construct

$$\text{the sample covariance } \Sigma_{\text{pr}} = \begin{pmatrix} \Sigma_{\theta\theta} & \Sigma_{\theta\eta} \\ \Sigma_{\eta\theta} & \Sigma_{\eta\eta} \end{pmatrix}$$

2. Draw perturbed data vector  $\mathbf{y}_k \sim \mathcal{N}(\mathbf{y}_t, \Sigma_y)$ ,  $k = 1, \dots, M$

3. Set  $\theta_{t,k}^{(1)} = \theta_{t,k}^\circ + \Sigma_{\theta\eta} (\Sigma_{\eta\eta} + \Sigma_y)^{-1} (\mathbf{y}_k - \eta(\theta_{t,k}^\circ))$ ,  $k = 1, \dots, M$  (\*)

# Data Assimilation Example



An object moves vertically over time in the presence of 11 sensors whose locations are shown in the right, vertical axis. Its path is given by the solid black line. The sensor signals are given by the 11 horizontal time series. As the object nears a sensor, the signal becomes elevated.

Every 20 seconds, the object's path is predicted 20 seconds into the future using the EnKF (middle) and the particle filter (bottom).

Prior paths  $\theta_t$  (light lines) are extended from the previous time period's posterior paths  $\theta_{t-1}$  (dark lines) according to a stochastic model for the object's path. Given the sensor reading for the current time period  $y_t$ , these prior paths are updated.

A model  $\eta(\theta_t)$  produces an expected signal given a path  $\theta_t$  that is comparable to the sensor signals  $y_t$  for the current time period.

The EnKF perturbs each prior path to produce a posterior path according to the formula in (\*). The particle filter samples posterior paths using likelihood weighted draws over the prior paths.

# References

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Kennedy, M. and O'Hagan, A. (2001). "Bayesian calibration of computer models (with discussion)," *Journal of the Royal Statistical Society, Series B*, 63, 425-464.

Higdon, D., Kennedy, M., Cavendish, J. C., Cafeo, J. A., and Ryne, R. D. (2004). "Combining field data and computer simulations for calibration and prediction," *SIAM Journal on Scientific Computing*, 26, 448-466.

Higdon, D., Gattiker, J., Lawrence, E., Jackson, C., Tobis, M., Pratola, M., Habib, S., Heitmann, K., and Price, S. (2013). "Computer model calibration using the ensemble Kalman filter," *Technometrics*, 55, 488-500.

Higdon, D., Gattiker, J., Williams, B., and Rightley, M. (2008). "Computer model calibration using high-dimensional output," *Journal of the American Statistical Association*, 103, 570-583.

Terejanu, G., Upadhyay, R.R., and Miki, K. (2012). "Bayesian experimental design for the active nitridation of graphite by atomic nitrogen," *Experimental Thermal and Fluid Science*, 36, 178-193.

Wasserman, L. (2000). "Bayesian model selection and model averaging," *Journal of Mathematical Psychology*, 44, 92-107.

Williams, B., Higdon, D., Gattiker, J., Moore, L., McKay, M., and Keller-McNulty, S. (2006). "Combining experimental data and computer simulations, with an application to flyer plate experiments," *Bayesian Analysis*, 1, 765-792.

Williams, B.J., Loepky, J.L., Moore, L.M., and Macklem, M.S. (2011). "Batch sequential design to achieve predictive maturity with calibrated computer models," *Reliability Engineering and System Safety*, 96, 1208-1219.