

# MODELING OF A COMPACT PULSER FOR ISENTROPIC COMPRESSION EXPERIMENTS\*

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Haill, H.L. Hanshaw and C.A. Hall

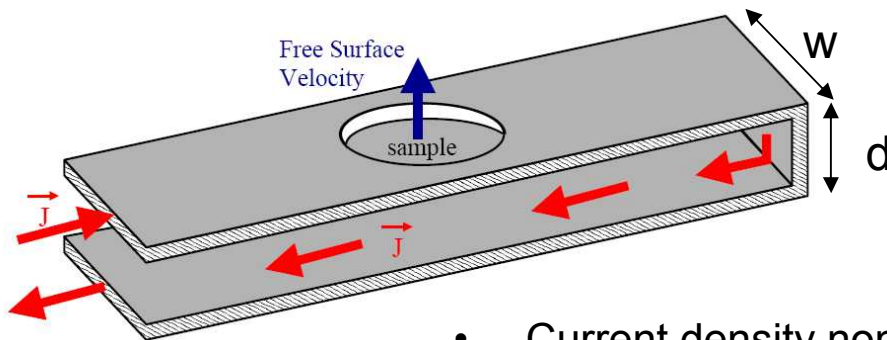
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<sup>a</sup>Ktech Corporation

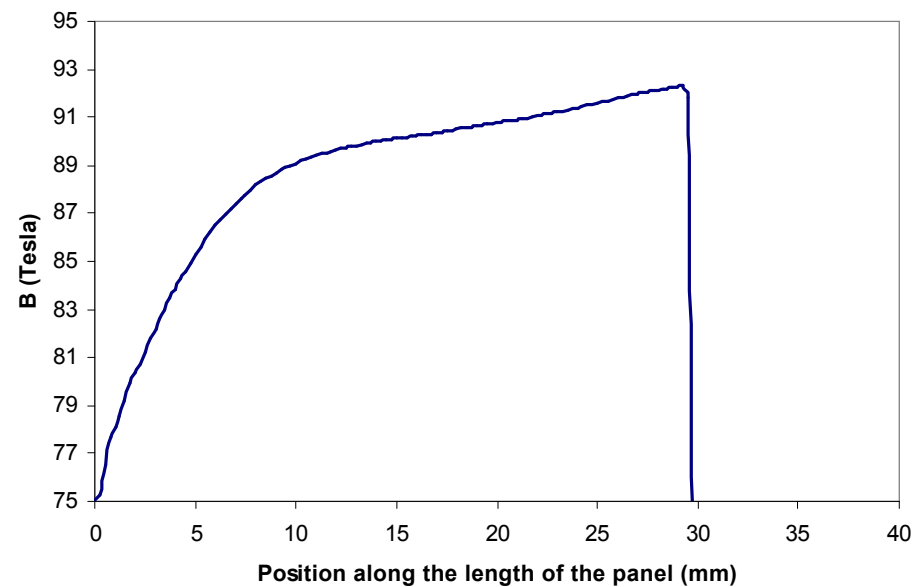
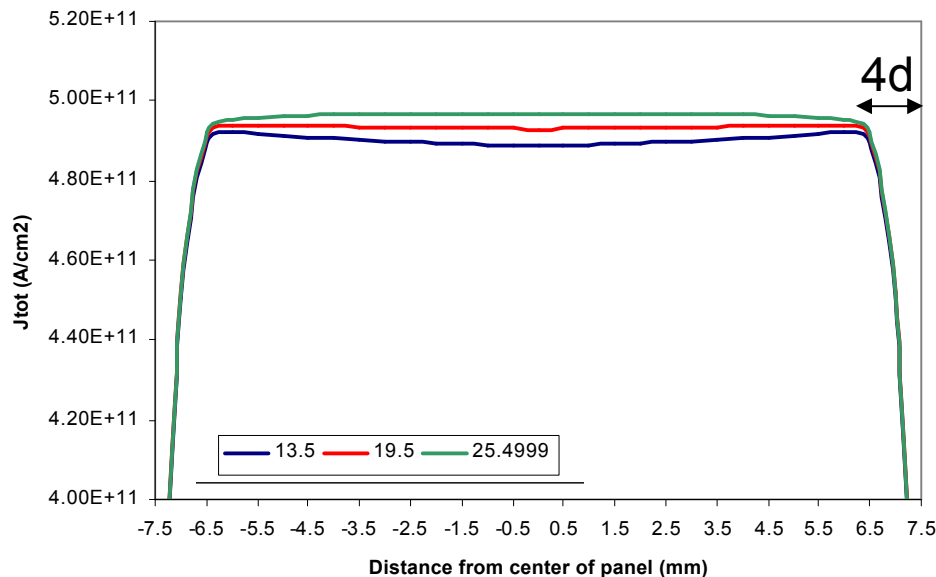


# Pressure uniformity issues in magnetically driven strip line configuration experiments



$$P_{\text{mag}} = K_1 \cdot \frac{\mu_0}{2} \left( \frac{I}{w} \right)^2$$

- Current density non-uniformity at the entrance of the strip line
- Current density rises along the length of strip line



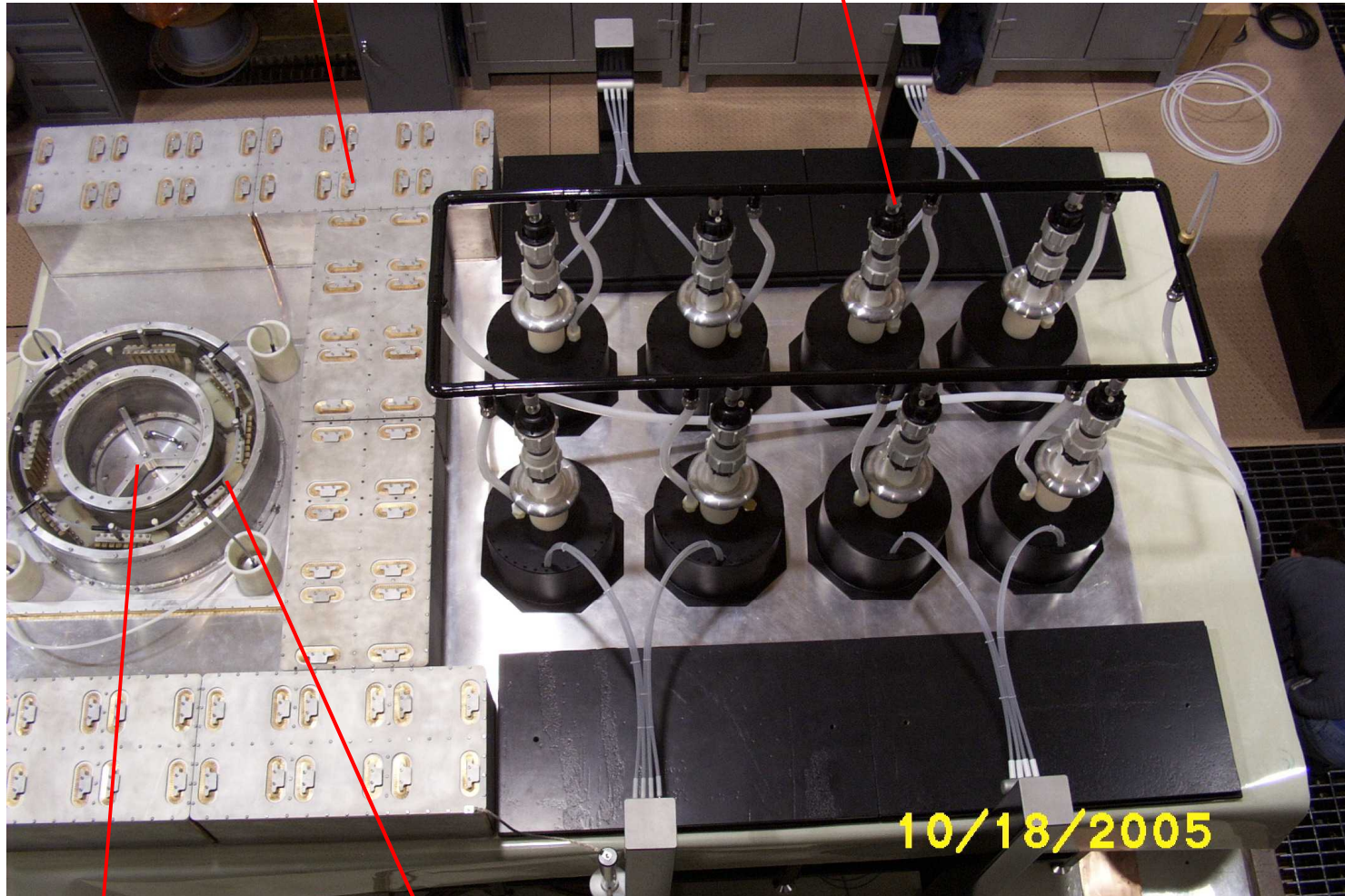


# VELOCE

B4 7: R.B. Spielman, et al (Monday)  
K1.00045: G. Avrillaud, et al (Tuesday)  
Q4 6: T. Jaglinski, et al (this session)  
Q4 7: T. Ao, et al (this session)

48 peaking capacitors

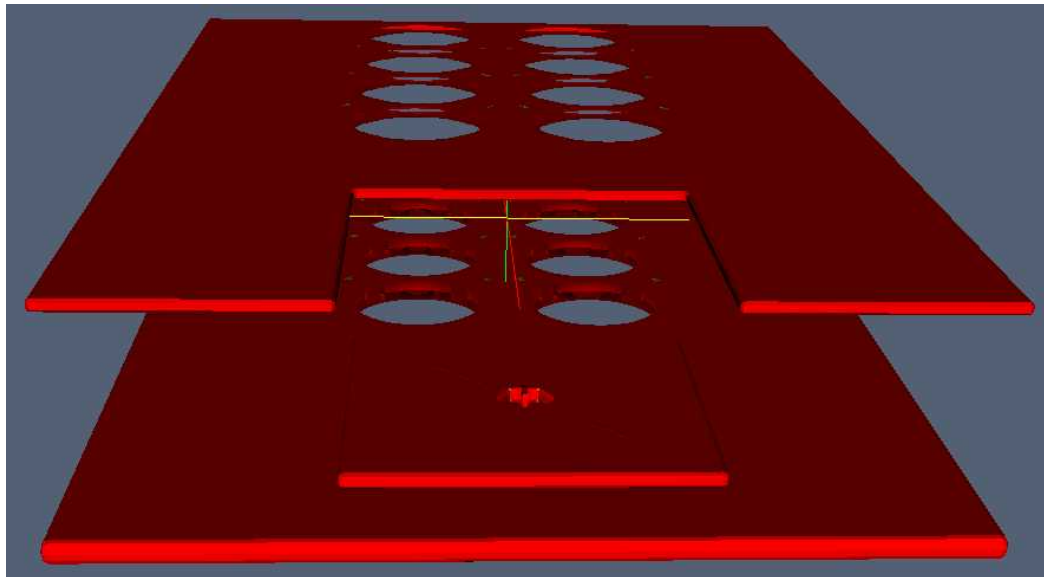
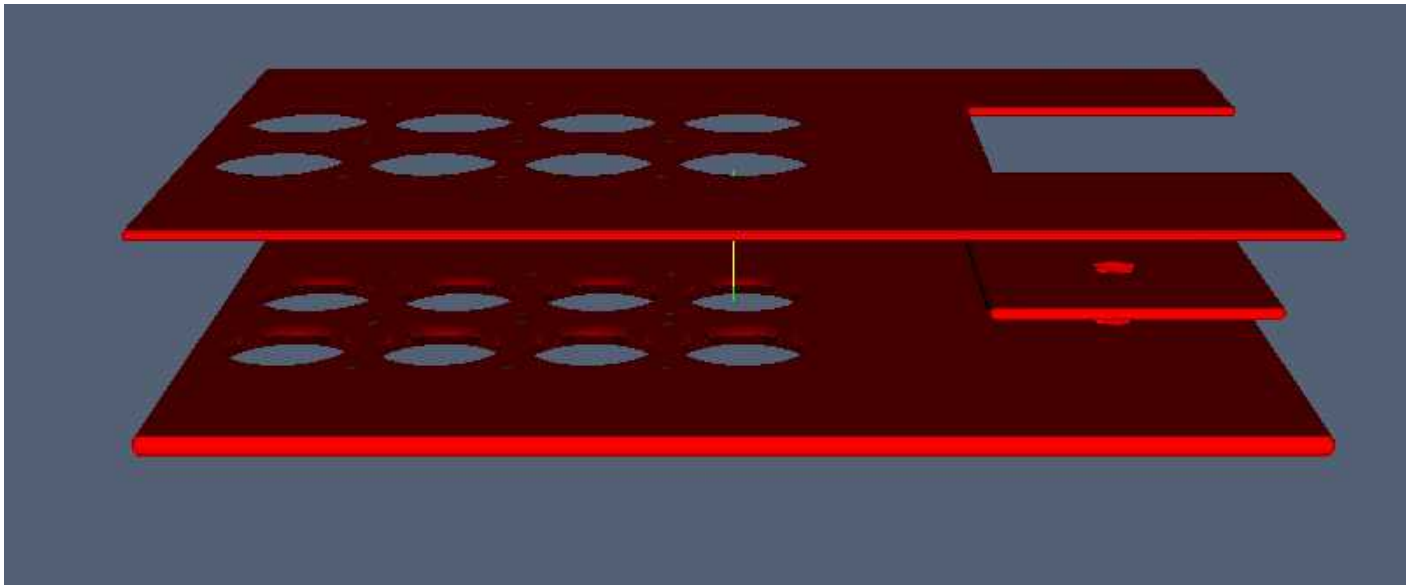
8 main capacitors



Load chamber

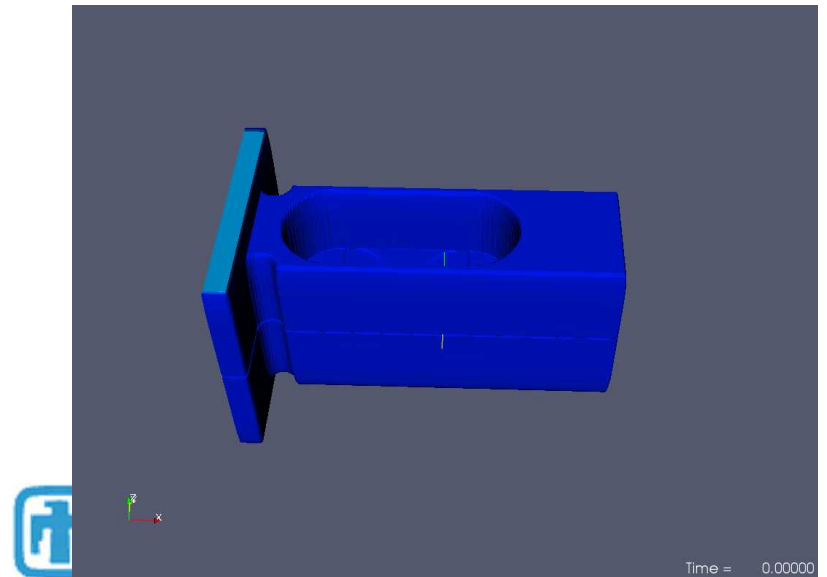
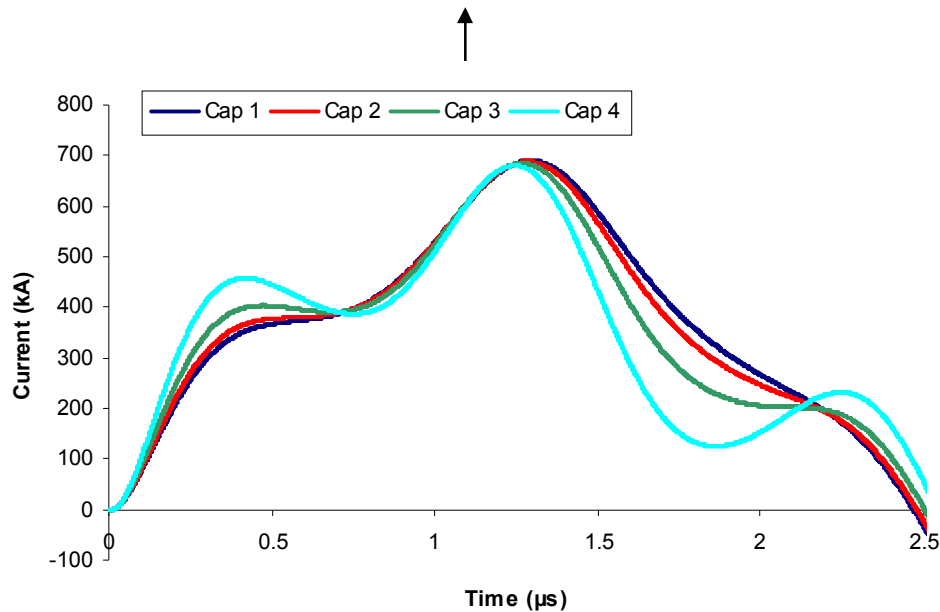
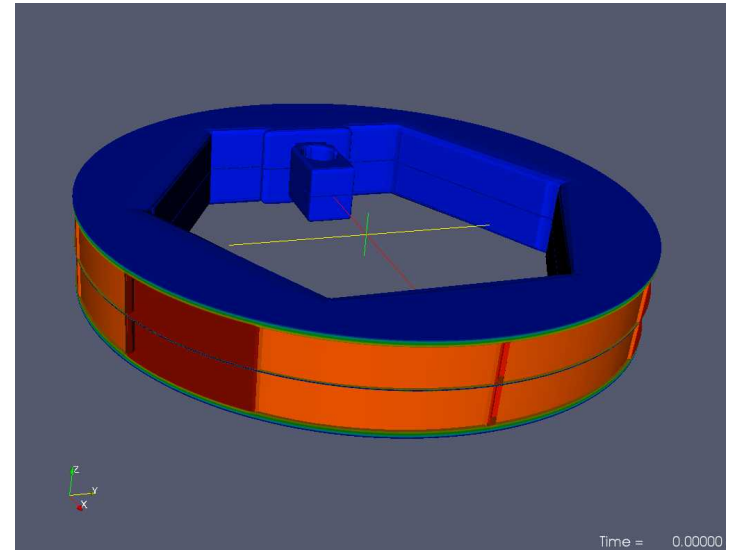
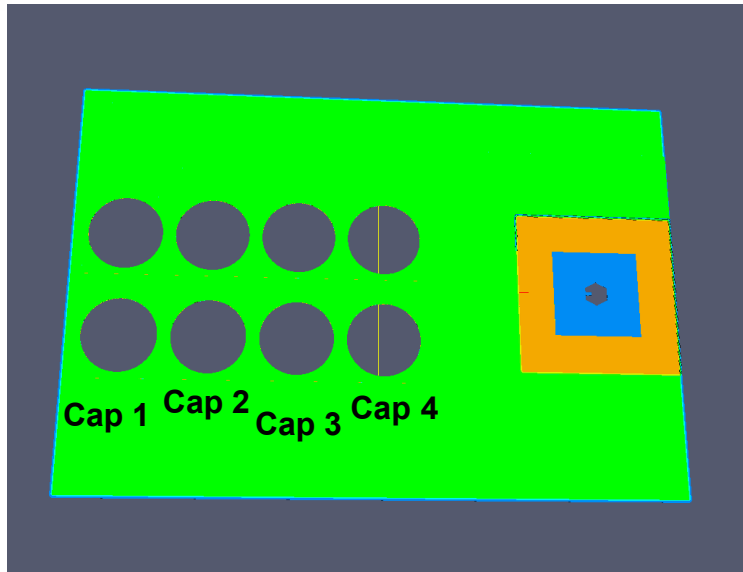
Dynamic Switch

# Modeling of Veloce pulser



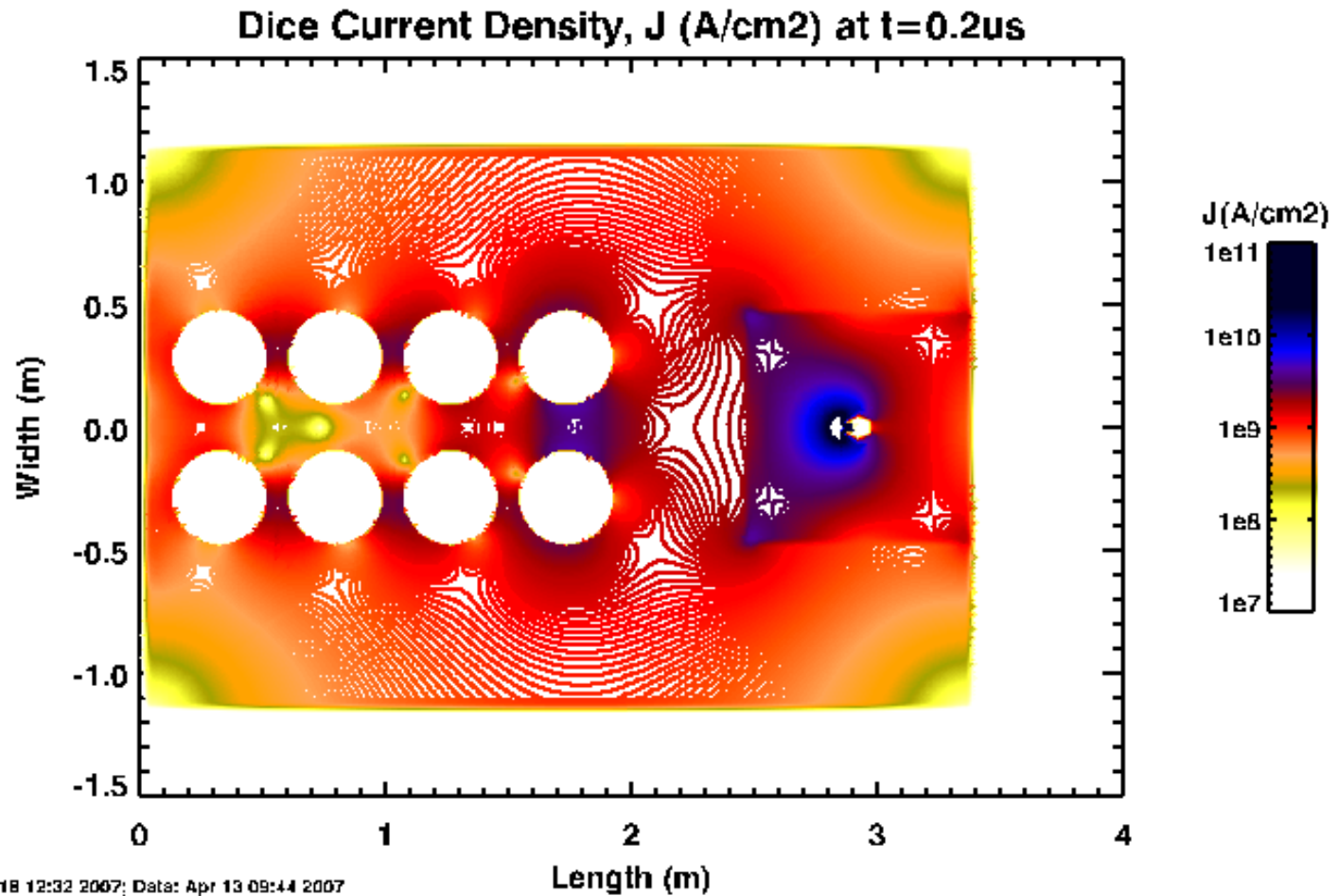
# VELOCE MHD Simulations

Goal: optimize current uniformity of the sample panel

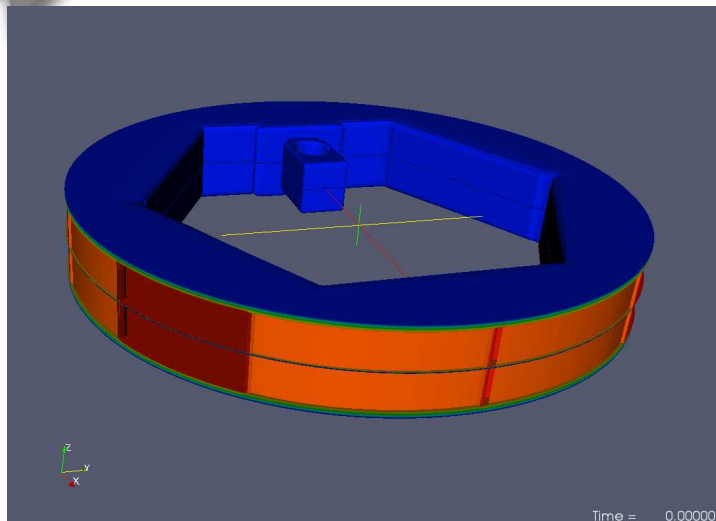




# VELOCE Simulations: full machine

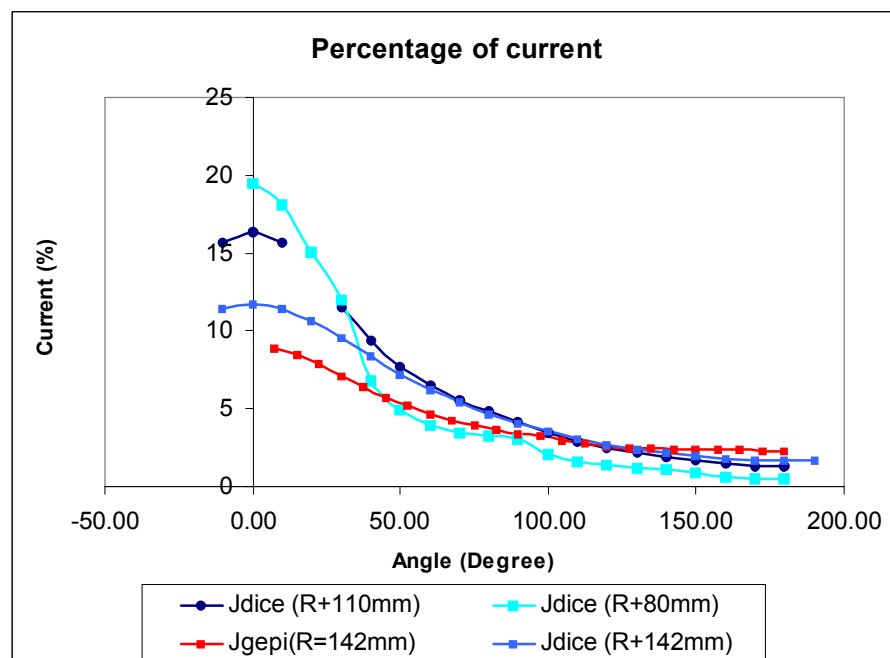
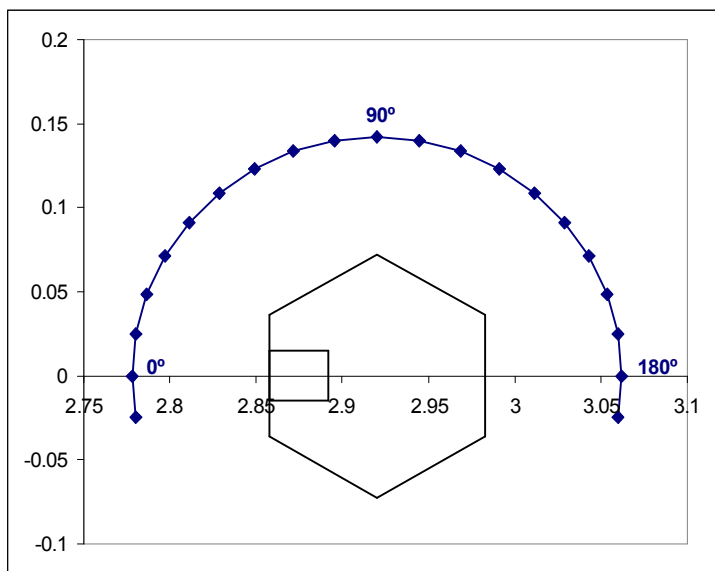


# VELOCE Simulations: Load Area



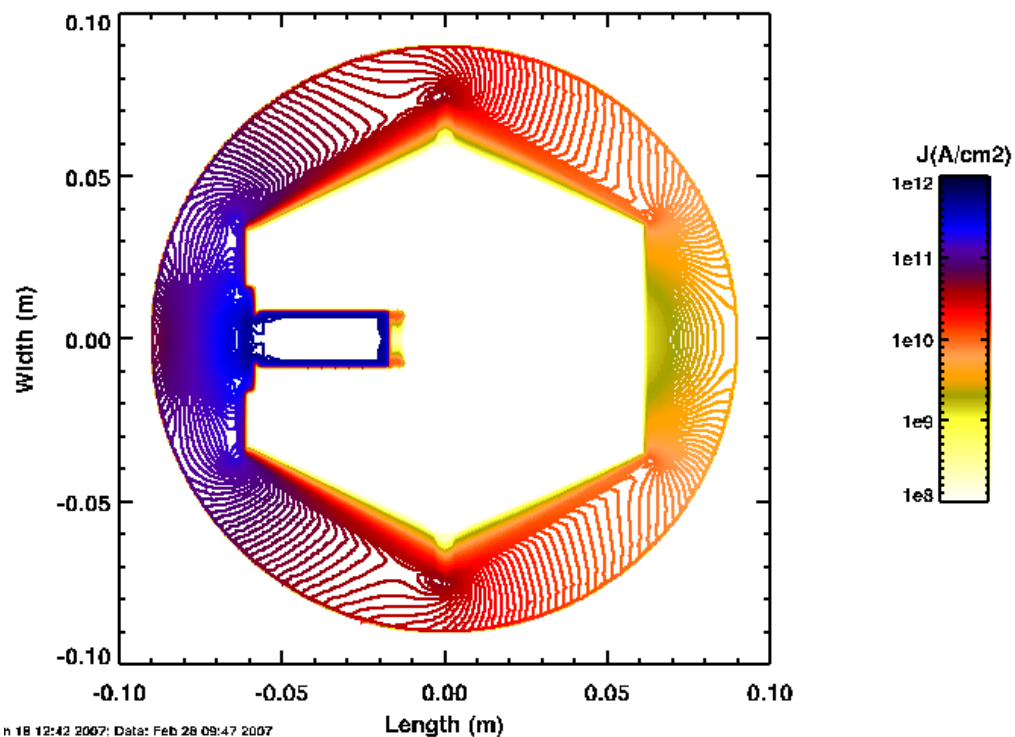
Circular boundary: input current distribution from whole Veloce simulation

Current distribution more favorable than for the French machine GEPI



# VELOCE Simulations: Load Area

Most of the current distributed on panel side

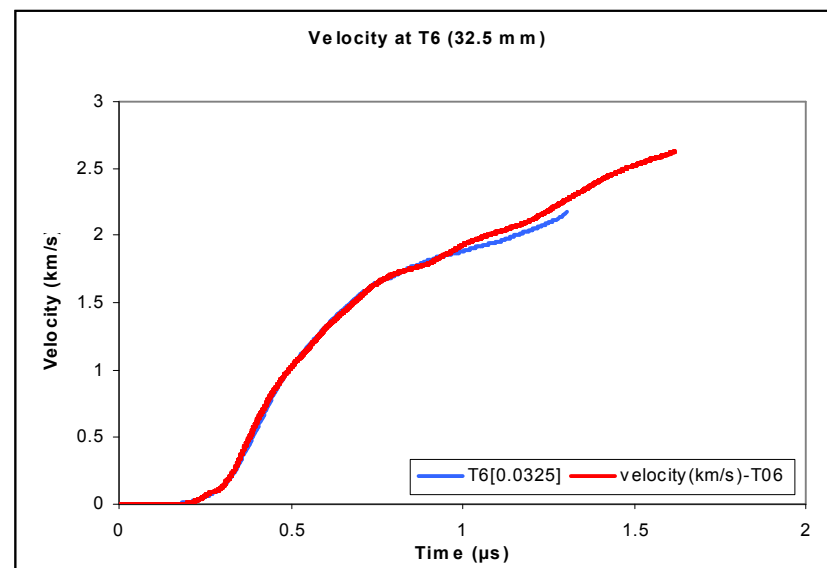
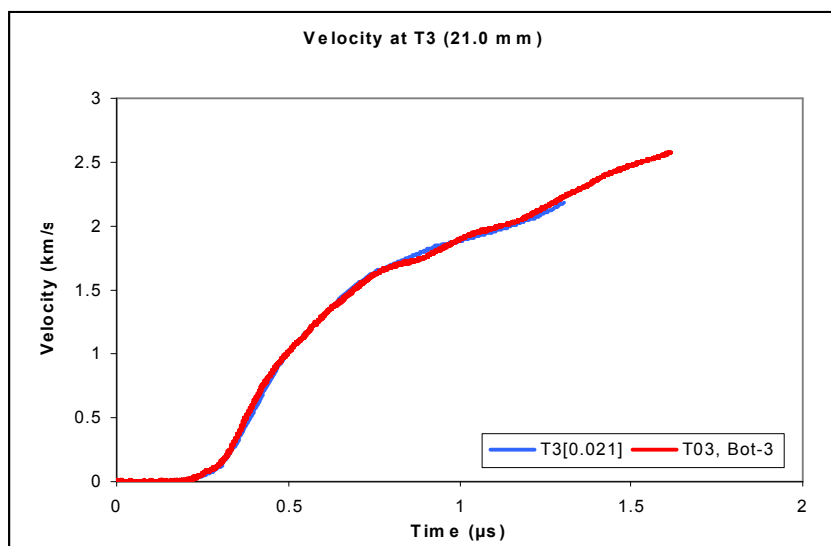
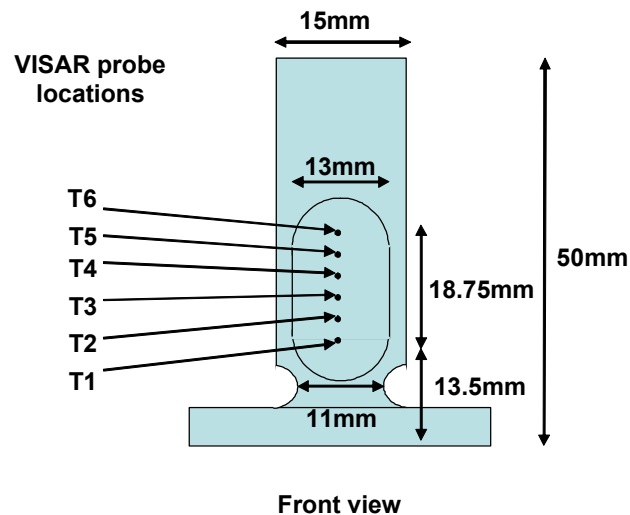
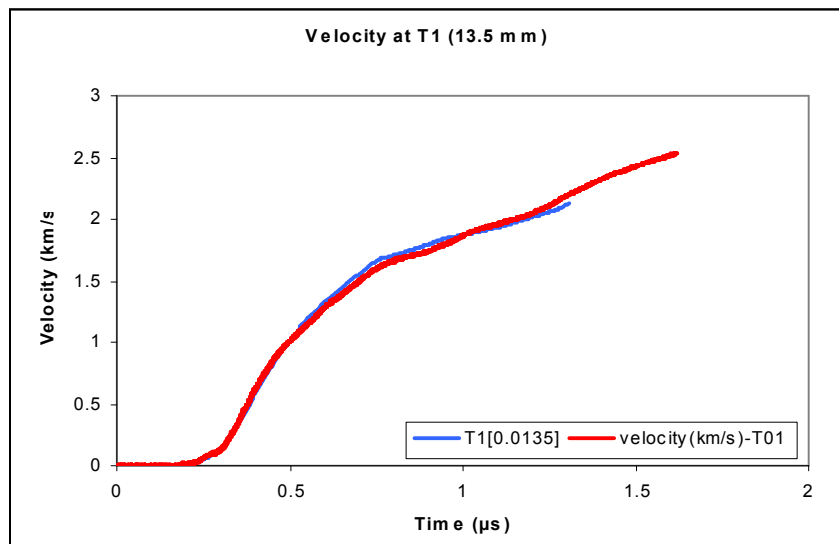


- Resolution limited because of size of simulation → Simulation of panel
- Input current distribution for panel simulation provided by whole load area simulation



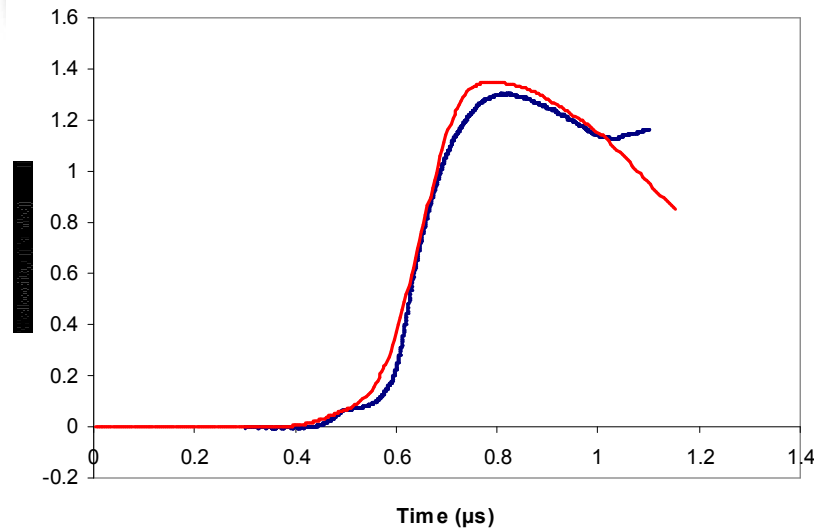
# DICE Simulations: Load Area

Comparison of measured and calculated free surface velocity at different probe positions  
( — model — experiment)

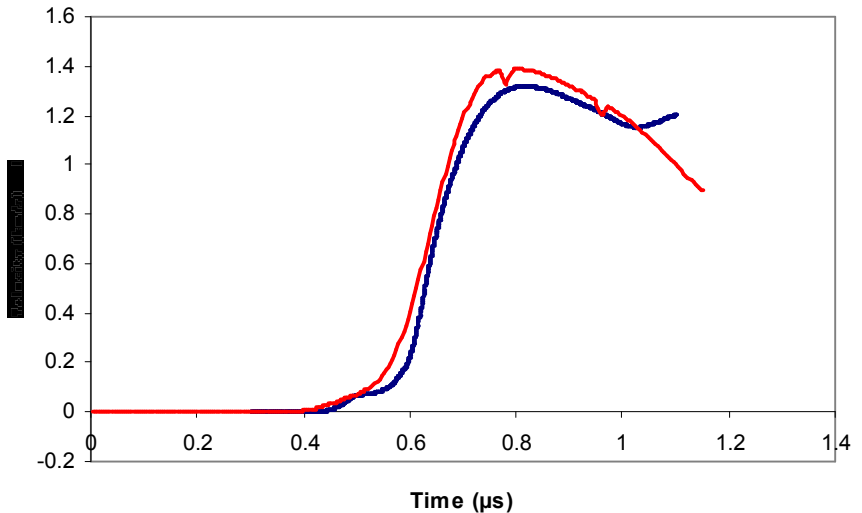


# Reference Panel: free-surface velocity curves

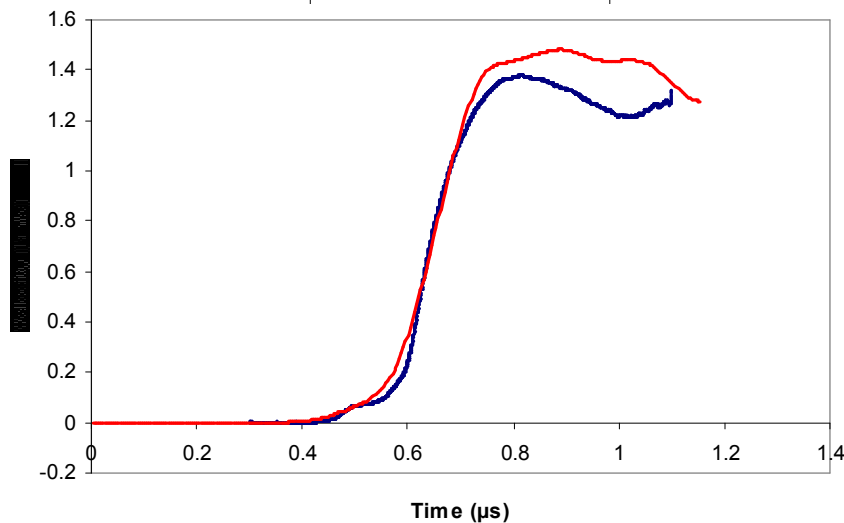
Previous results (lower resolution)



— T01, Bot-1 — x = 13.5



— T02, Bot-2 — x = 19.5



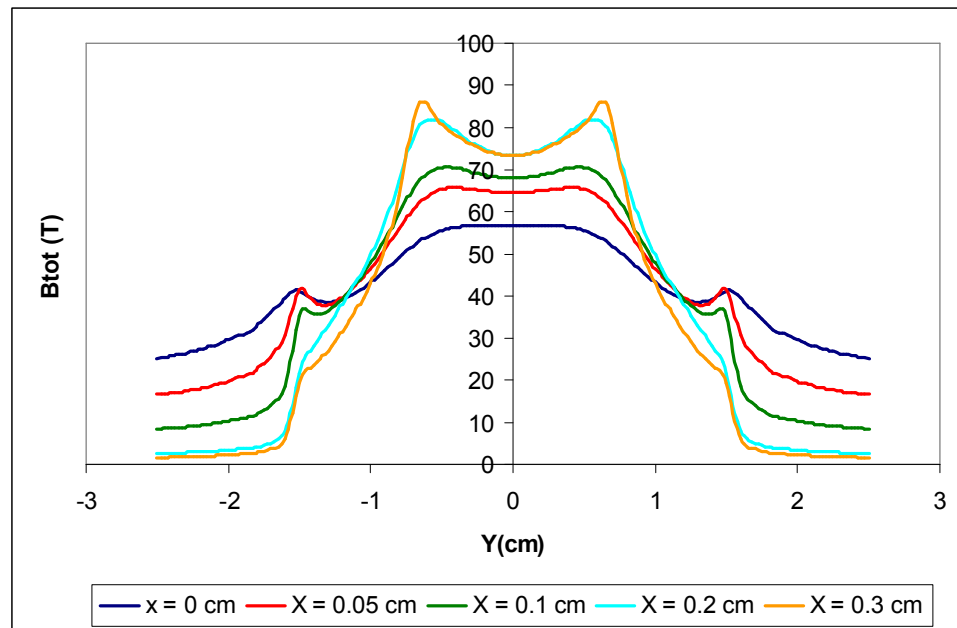
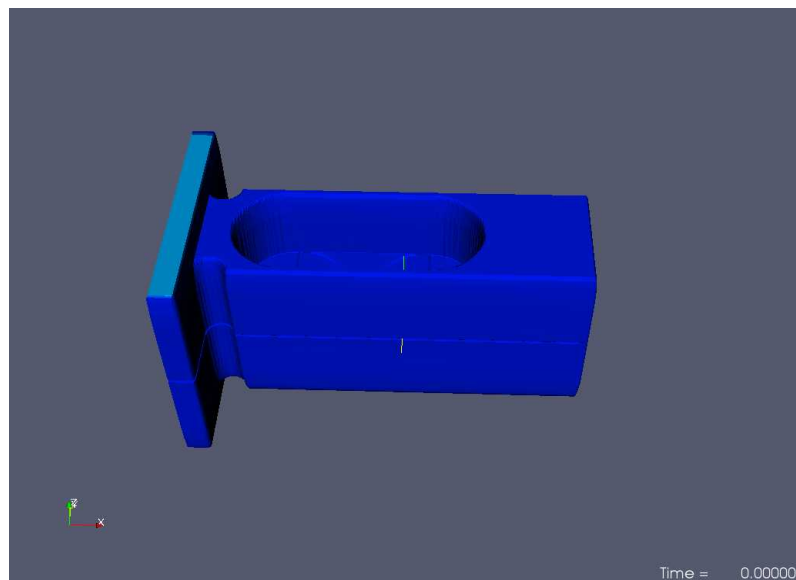
— T03, Bot-3 — x = 25.5

Simulation and experimental free-surface velocity as a function of time at three positions along the length of the panel : 13.5mm, 19.5mm and 25.5mm.

Reference panel: 15mm x 35mm x 2.5mm

# VELOCE Simulations: Panel Area

Input current distribution for panel simulation

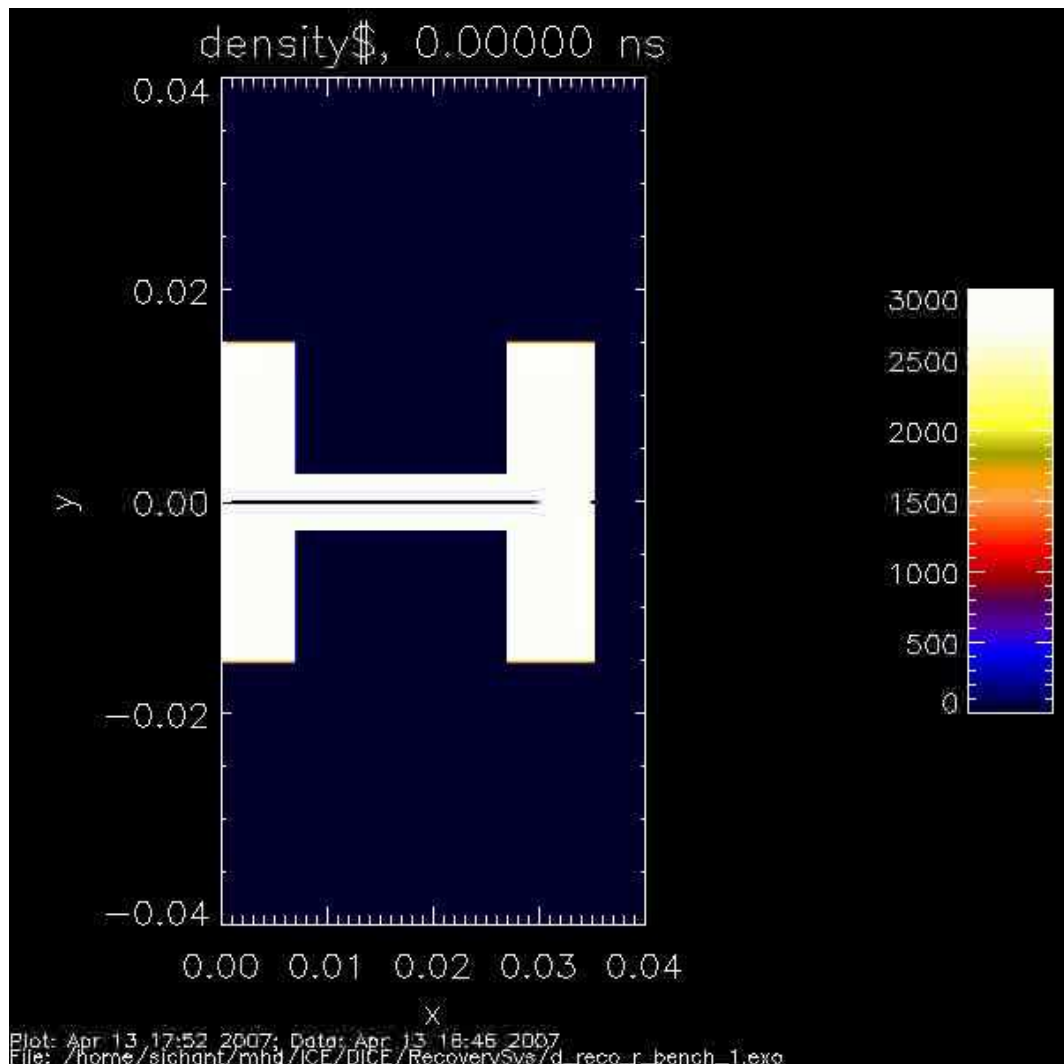


Resolution :

- 0.25 mm in X and Y direction (panel plane)
- 0.0425 mm graded to 0.25 in z direction

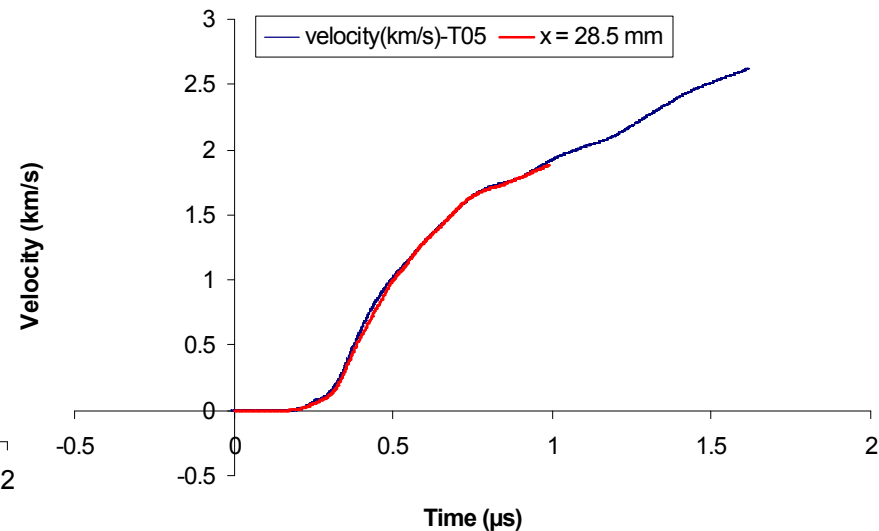
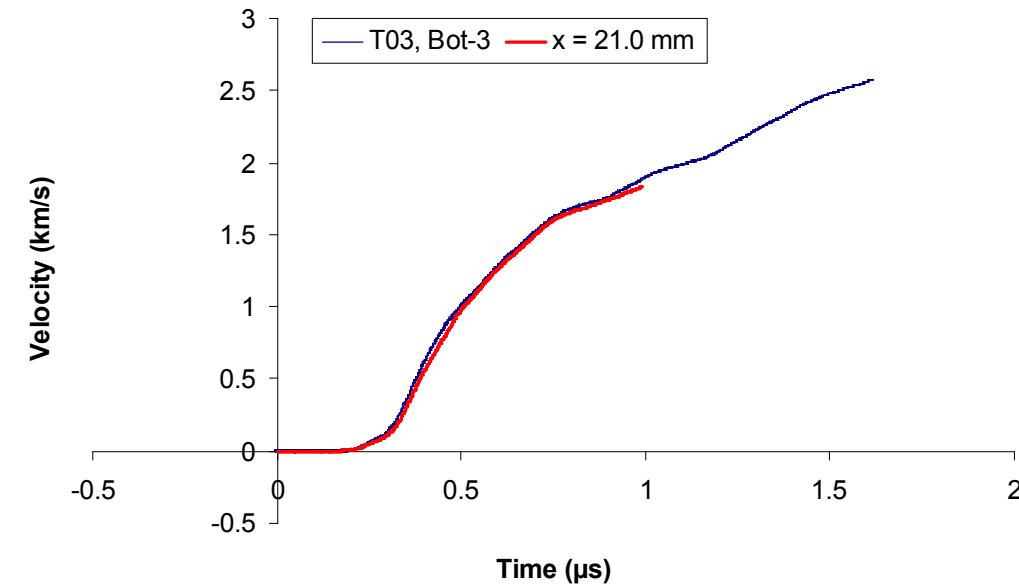
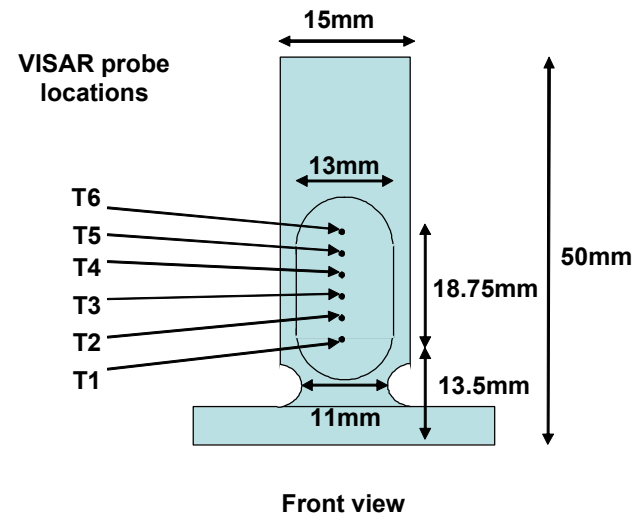
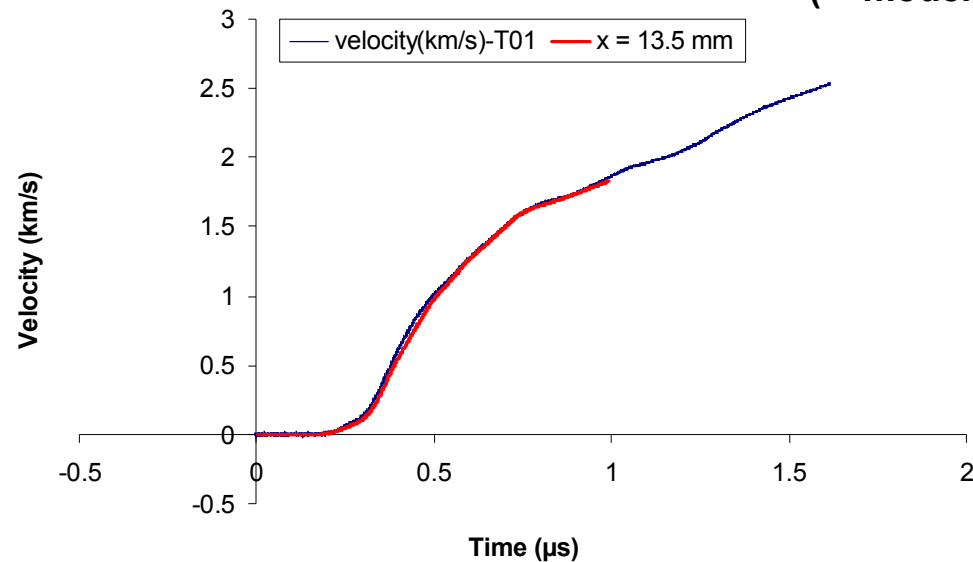
# VELOCE Simulations: Panel Area

Density profile as a function of time



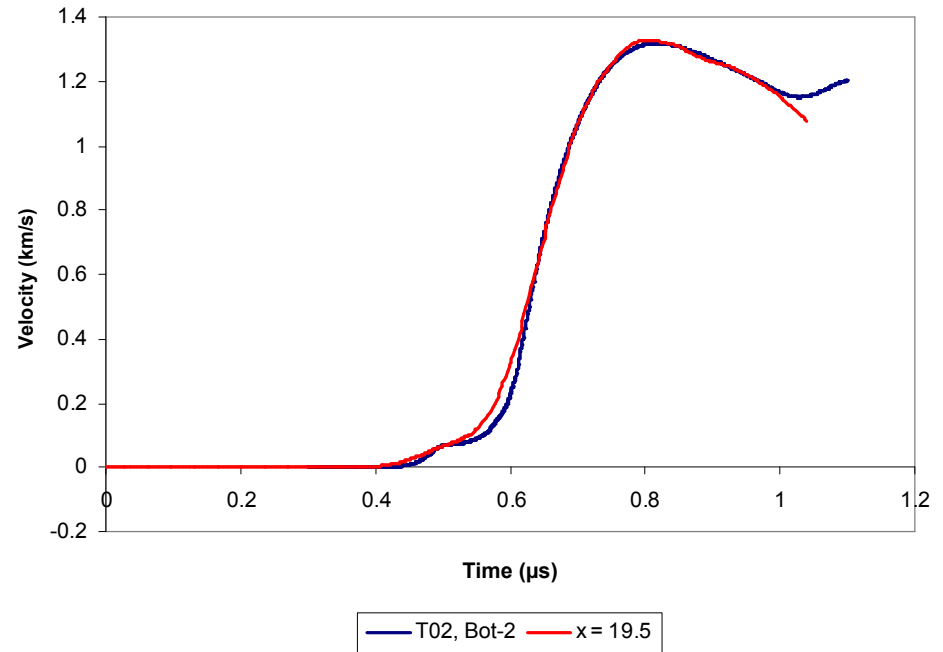
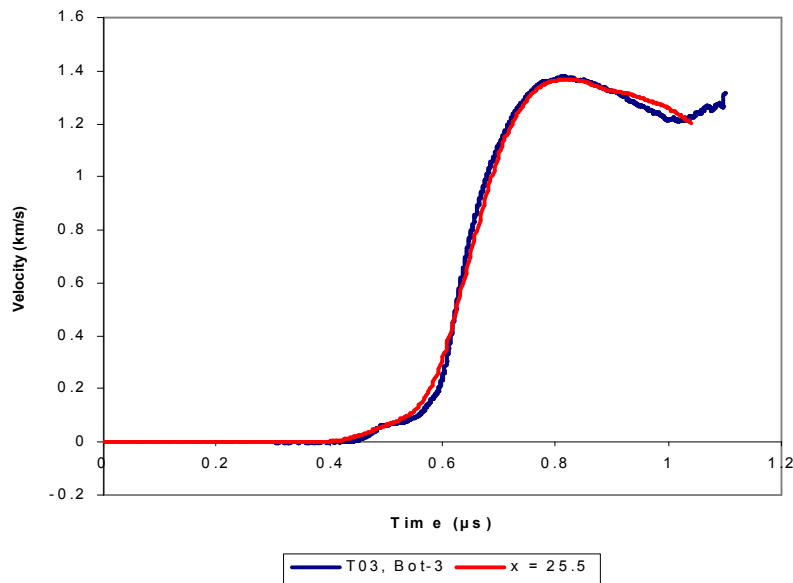
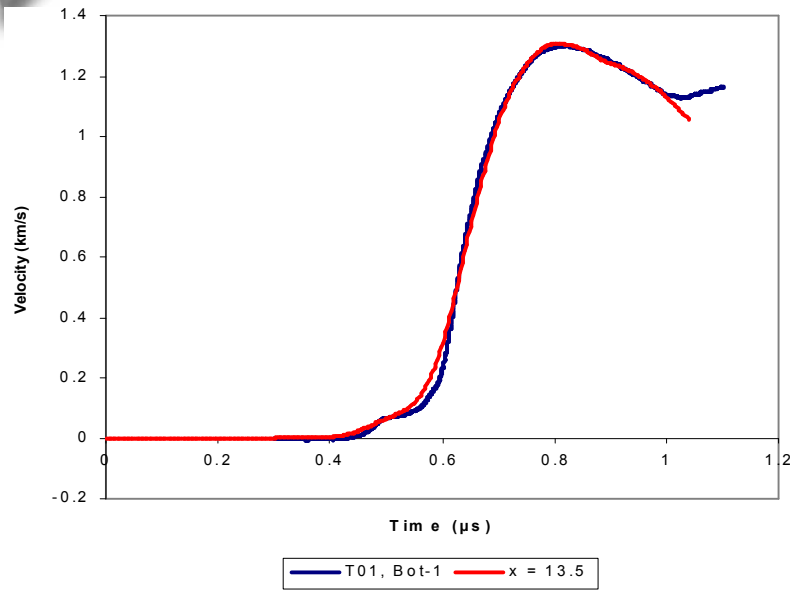
# VELOCE Simulations Benchmarking

Comparison of measured and calculated free surface velocity at different probe positions  
( — model — experiment)



# VELOCE Simulations: Panel Area

## Reference Panel: free-surface velocity curves



Simulation and experimental free-surface velocity as a function of time at three positions along the length of the panel : 13.5 mm, 19.5 mm and 25.5 mm.

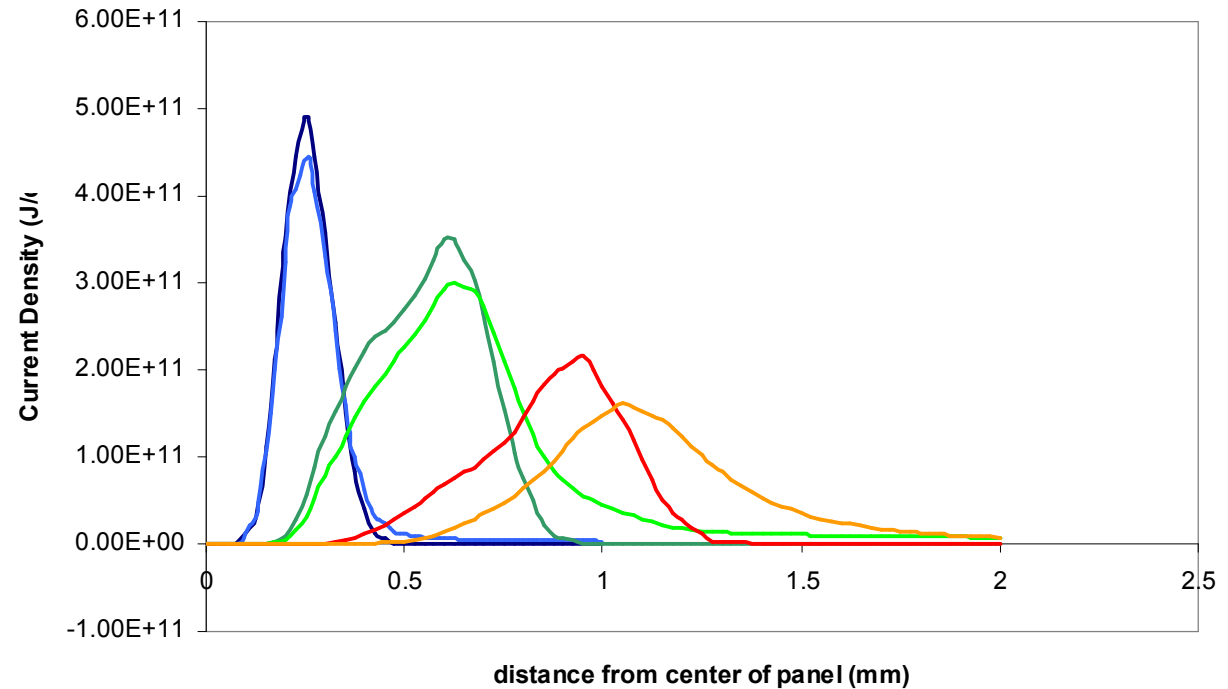
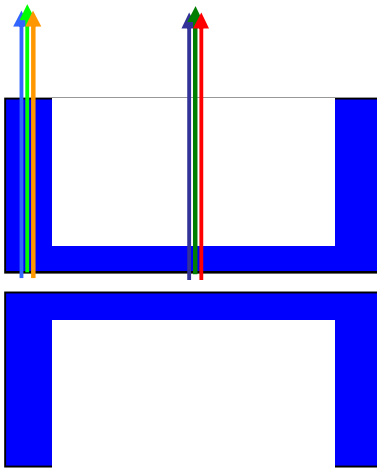
Reference panel: 15 mm x 35 mm x 2.5 mm



# VELOCE Simulations: Load Area

## Current Diffusion in the Panel

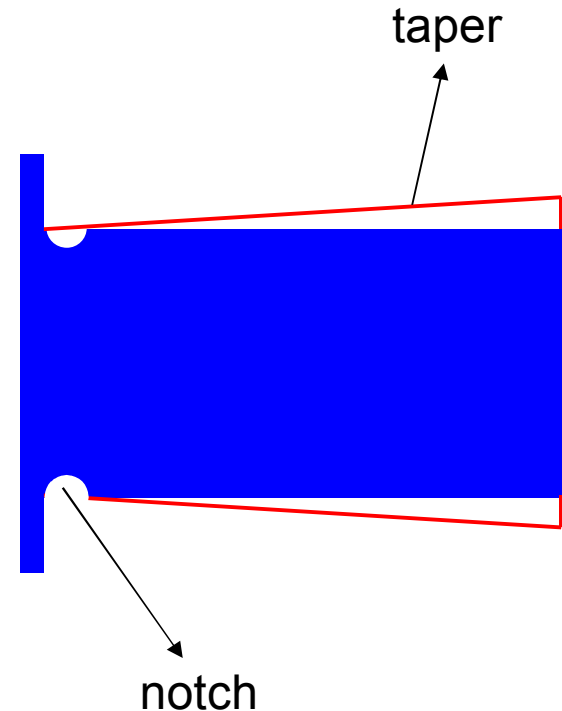
Current diffusion across the thickness of the panel



Total current density across the thickness of the panel at 2 cm from the bottom of the panel at three different times: 0.2  $\mu$ s (blue curves), 0.5  $\mu$ s (green curves) and 0.8  $\mu$ s (red-orange curves). The current density is estimated in the center of the panel width (Y=0 mm) and at the edge of the panel width (Y=7mm).

# DICE Simulations: Panel Area

- Reference panel: 15mm x 35mm x 2.5mm
  - Different notch size
  - Different taper
- Long panel: 15mm x 50mm x 1mm
  - Different notch size
  - Different taper
- Reference panel: 20mm x 45mm x 1mm
  - Different notch size
  - Different taper
- Tilted panel

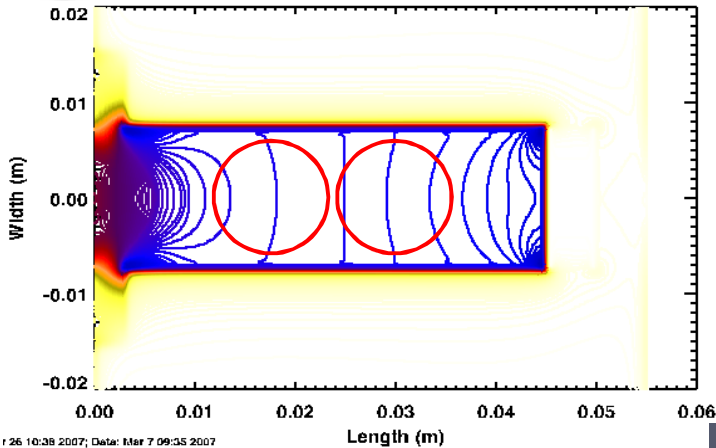


**Reference:** T. Ao, J.R. Asay, S. Chantrenne, M.R. Baer, and C.A. Hall, 'A compact strip-line pulse power generator for isentropic compression experiments'

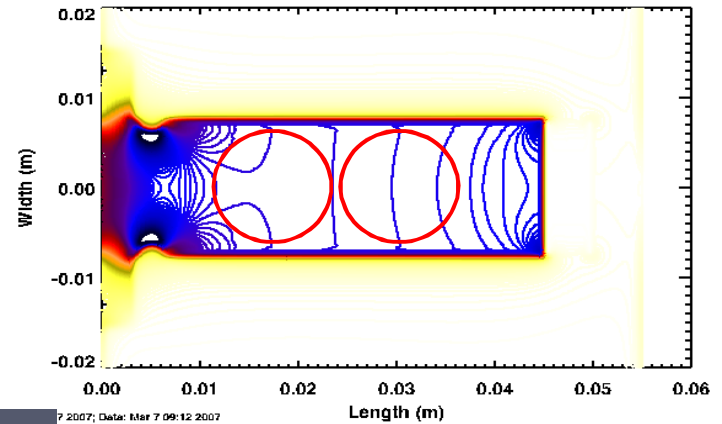
# Simulation Results – Long Panel

notch size variation - R = 1.5mm, 1.0mm, 0.5mm and no notch

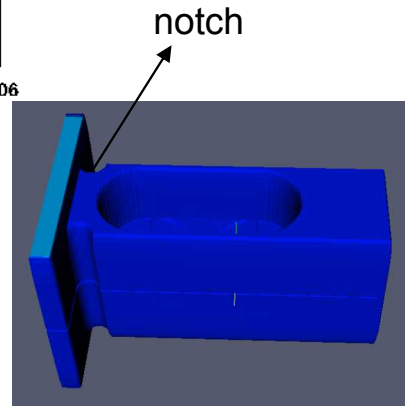
15mmx50mm panel, no notch, B at  $t=0.2\mu\text{s}$



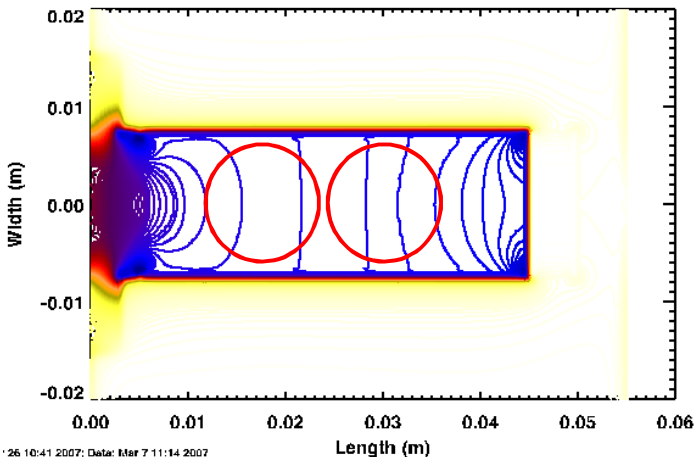
15mmx50mm panel, notch r=1.0mm, B at  $t=0.2\mu\text{s}$



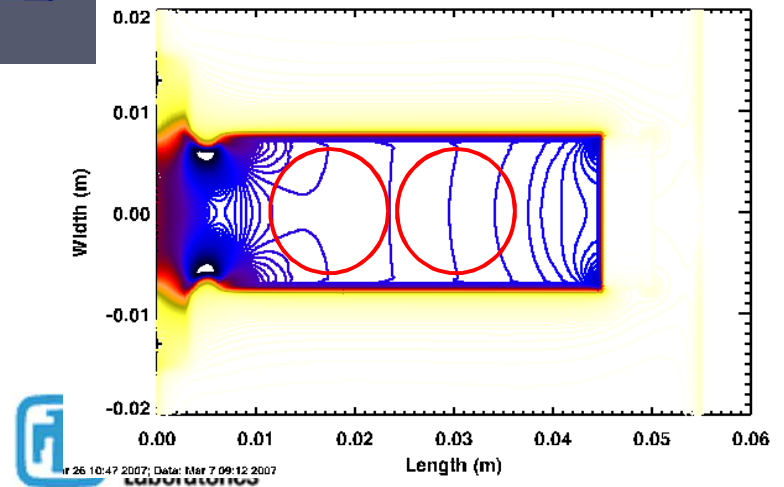
Resolution: ~0.5 % between levels



15mmx50mm panel, notch r=0.5mm, B at  $t=0.2\mu\text{s}$

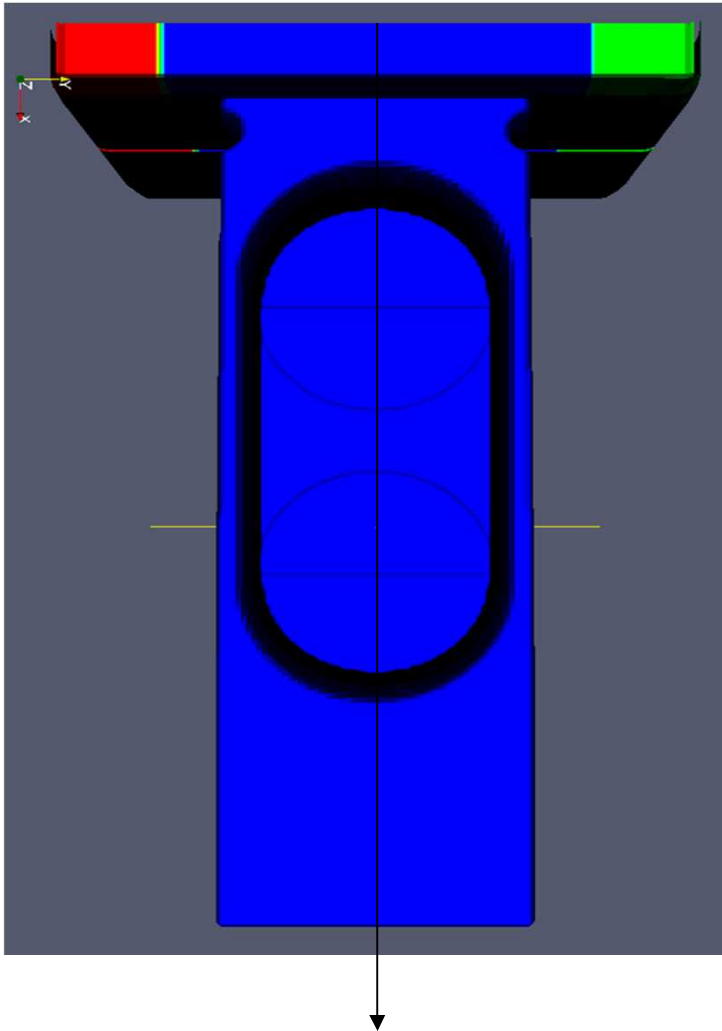


15mmx50mm panel, notch r=1.5mm, B at  $t=0.2\mu\text{s}$

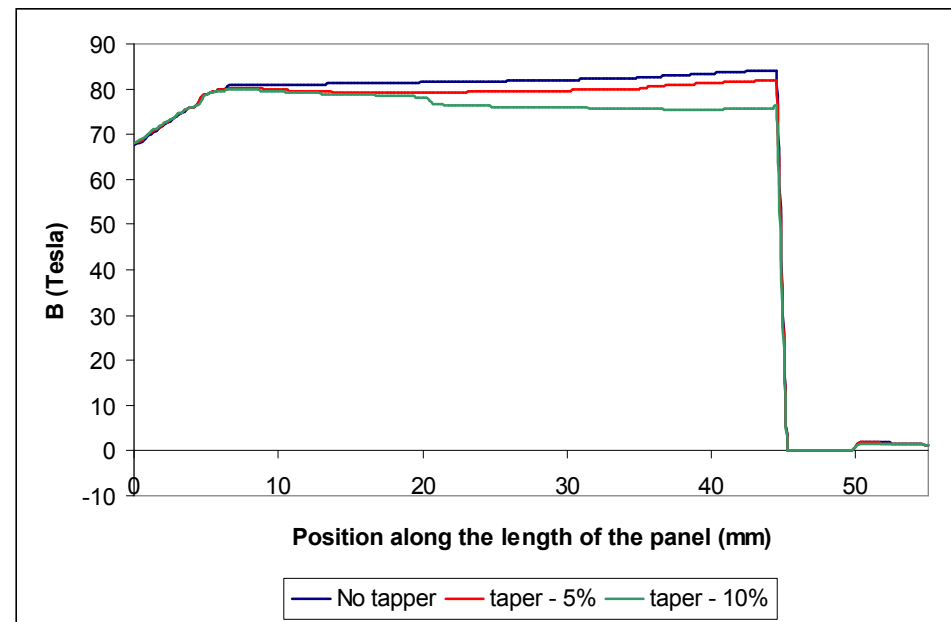


# Tapered Long Panel: 0% - 5% - 10%

Taper = 5%

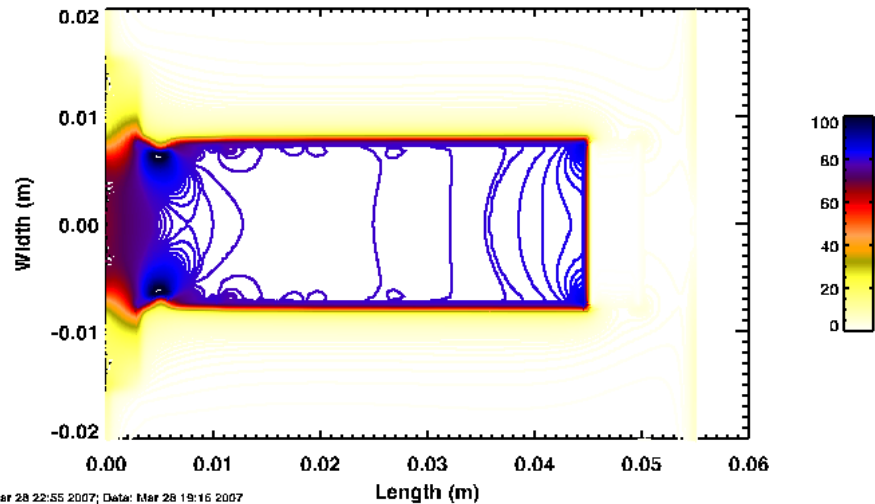


$B$  (T) at the edge of the panel between the two panels.  $B$  is directly proportional to  $J_{tot}$ .

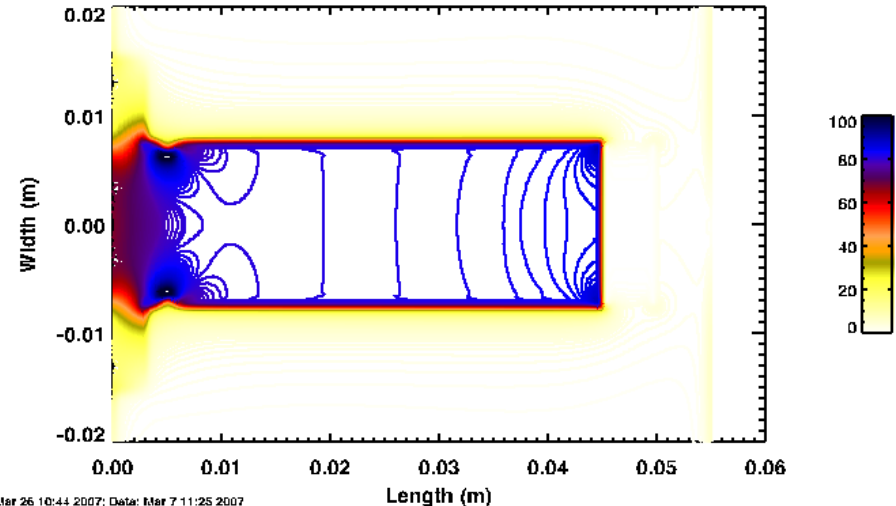


# Tapered Long Panel: 0% - 5% - 10%

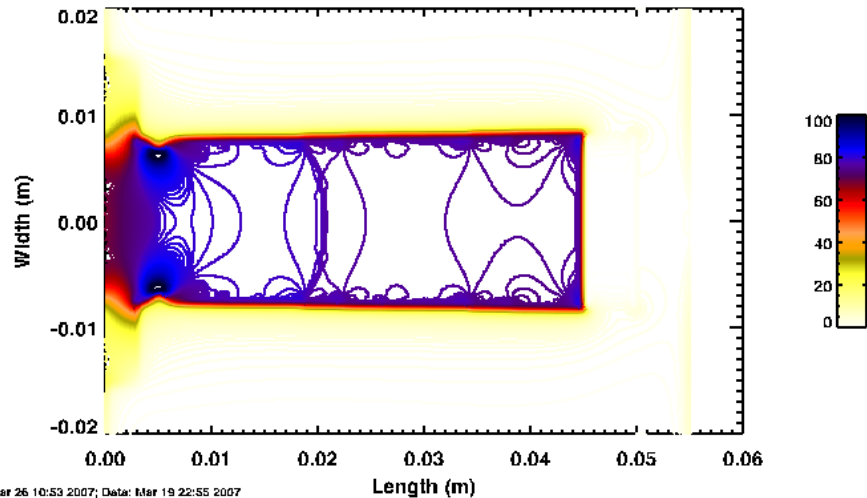
15mmx50mm tapered panel (5%), notch  $r=1.0\text{mm}$ , B at  $t=0.2\mu\text{s}$



15mm x 50mm panel, notches  $r=1.0\text{mm}$ , B at  $t=0.2\mu\text{s}$

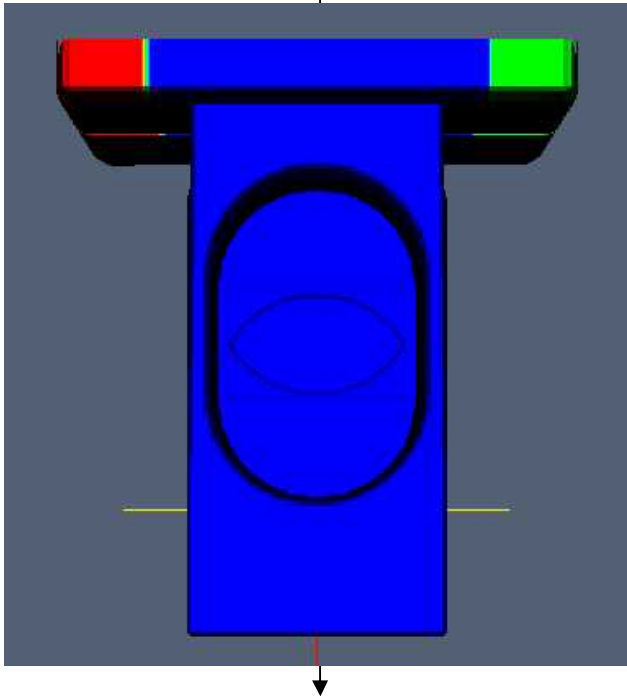


15mmx50mm tapered panel (10%), notch  $r=1.0\text{mm}$ , B at  $t=0.2\mu\text{s}$

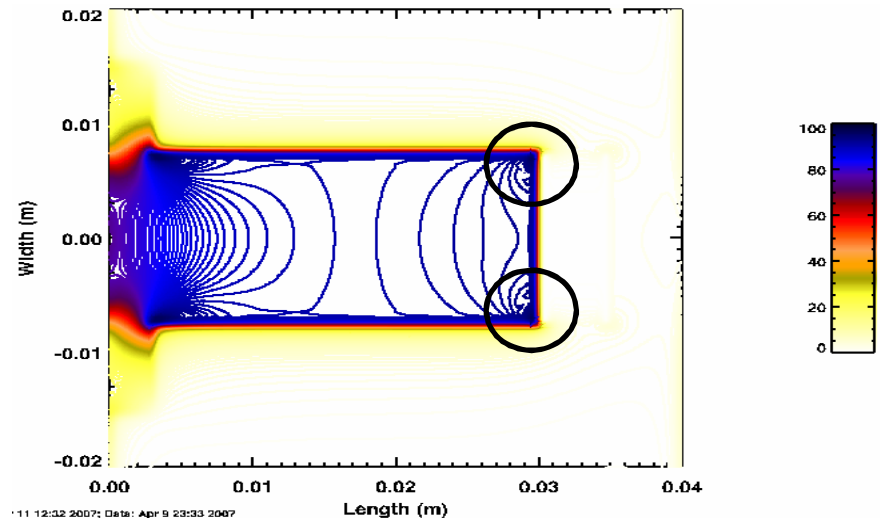
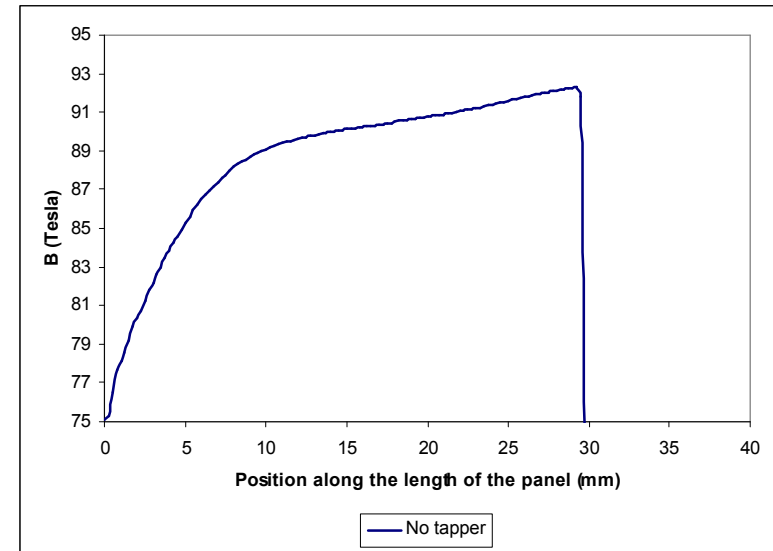


Resolution: 0.5 % between levels  
The contour irregularities at the edges are due to the mesh that is not parallel to the edge

# Current density non uniformity at the end of the panel



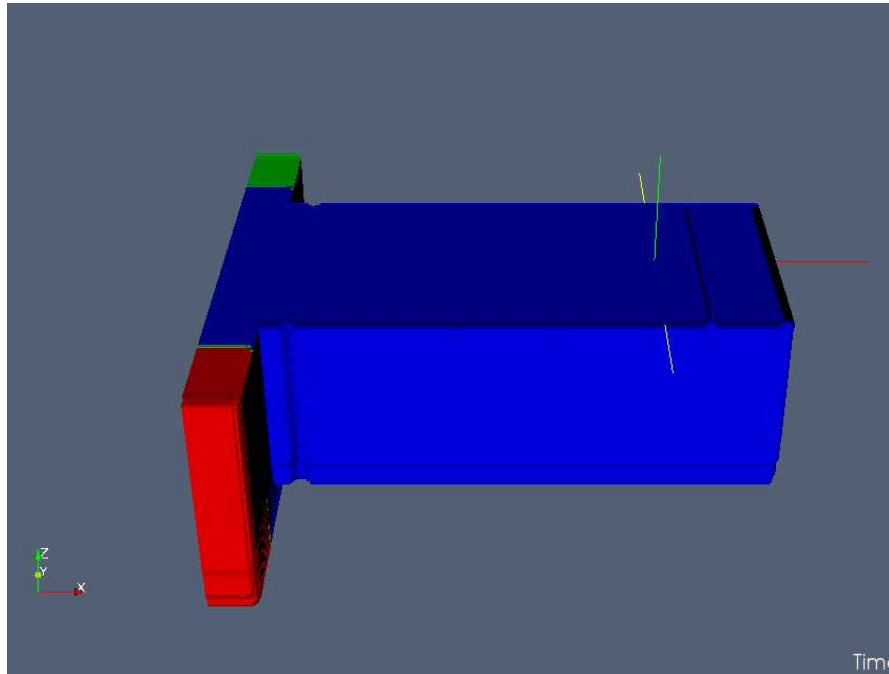
**Problem:** B at the edge of the contact is about 15% higher than in the center, causing B to increase by about 3% along the usable part of the panel → need to reduce/eliminate the hot spot at the end of the contact by modifying the contact area of the panel



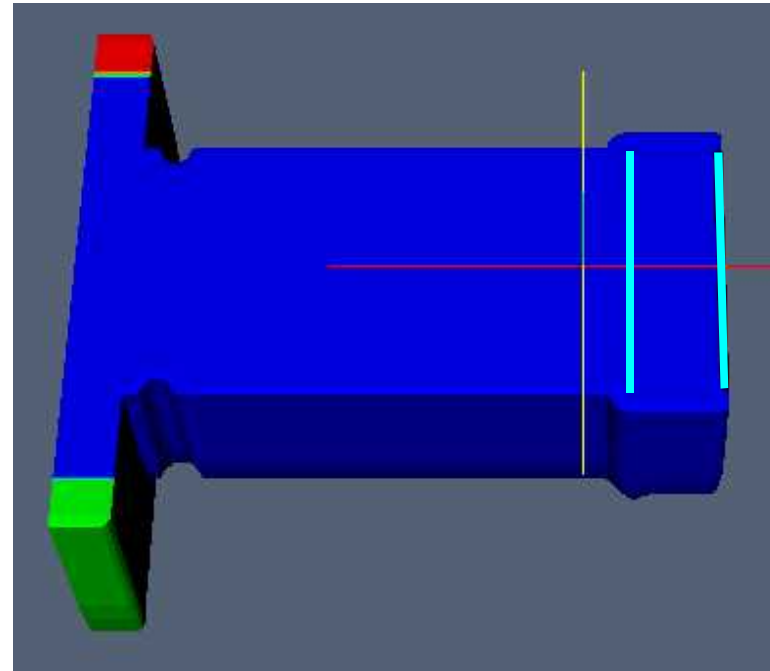


# Proposed modification

Original panel



Modified panel

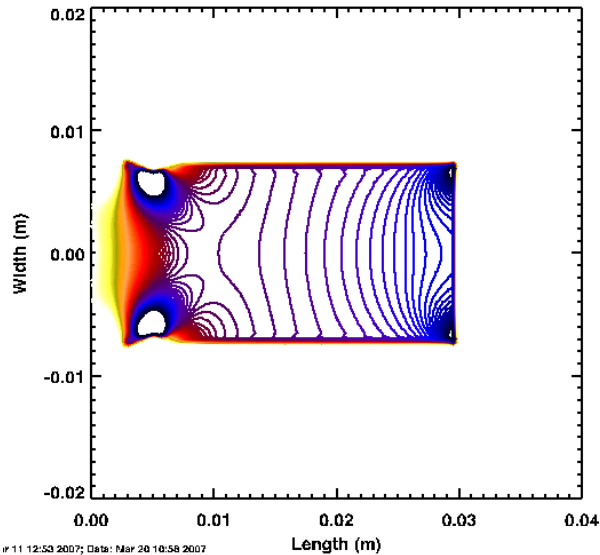
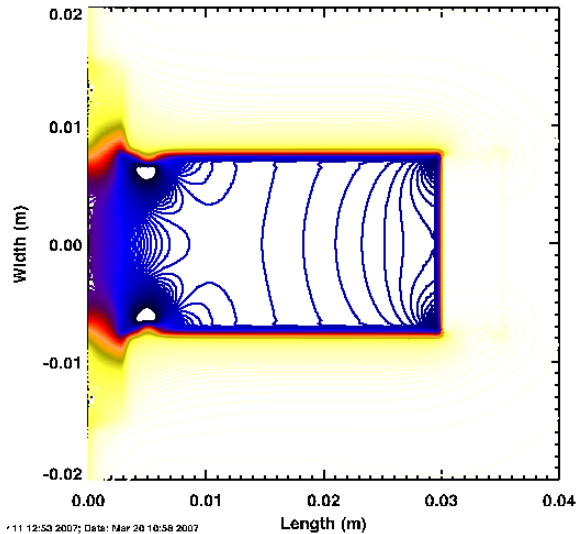


Bottom panel with contact. Contact does not show well because we are limited by the resolution of the simulation.

# Preliminary Results

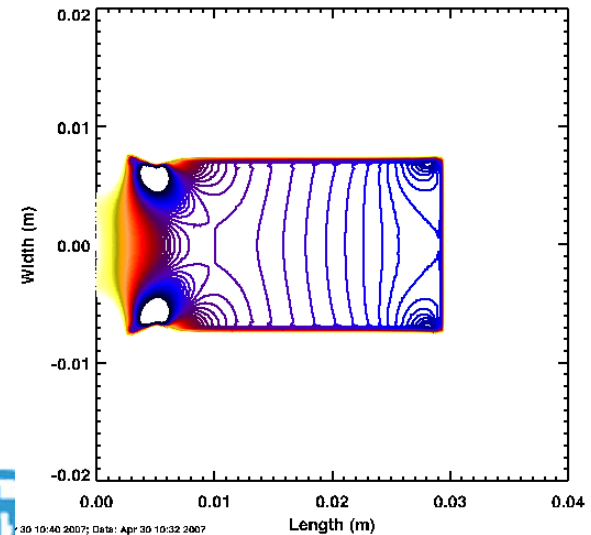
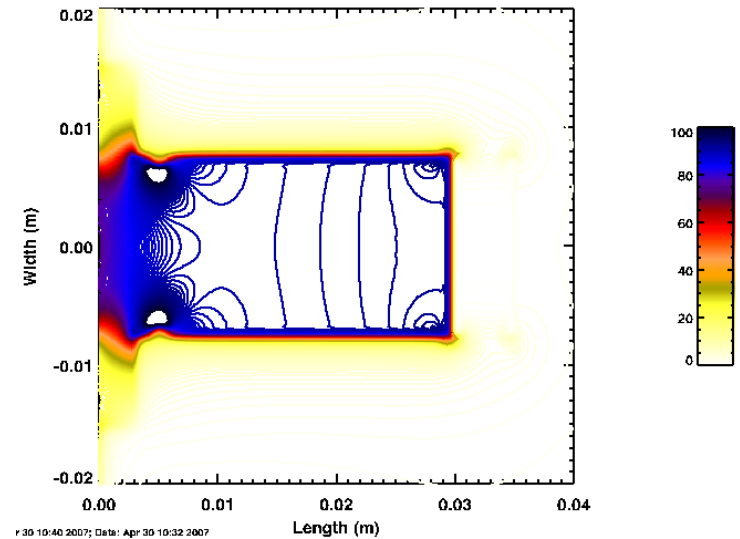
## Original panel

15 mm x 35 mm, 1 mm notch  
original panel, B at 0.2  $\mu$ s



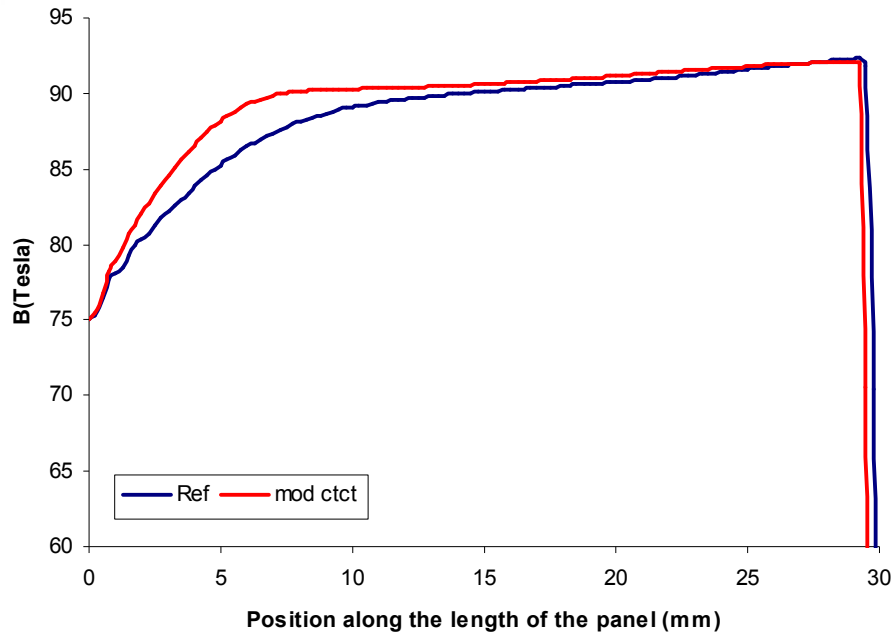
## Modified panel

15 mm x 35 mm, 1 mm notch  
extended panel in contact area, B at 0.2  $\mu$ s

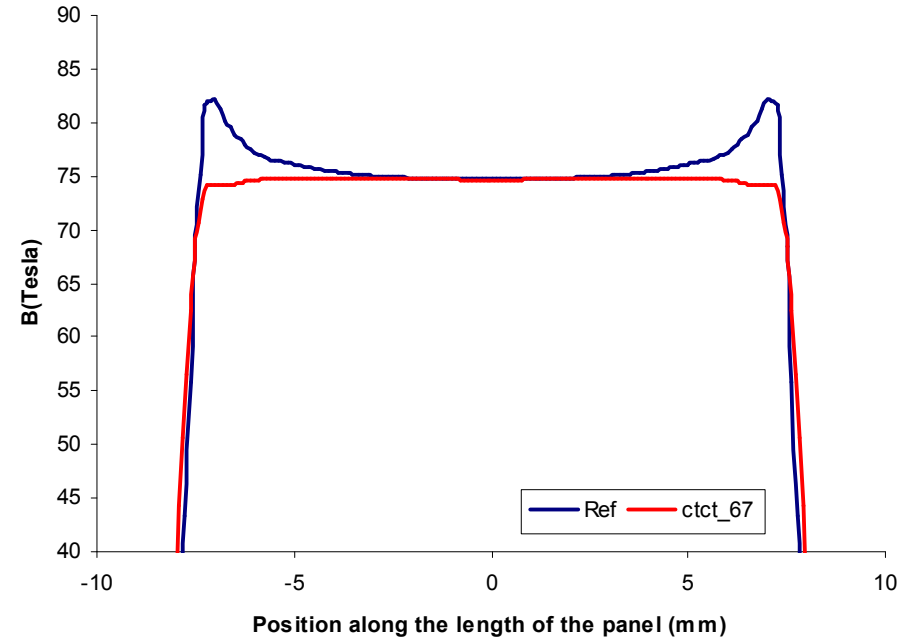


Resolution:  
Top plots: 0.45 %  
Bottom plots: 0.25%

# Results



B at the edge of the panel between the two panels.

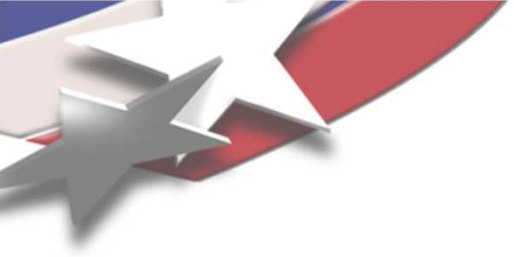


B along the width of the panel at the edge of the contact between the two panels.



# Conclusions

- 3D simulations of VELOCE allow us to:
  - understand the current density distribution across the sample panel for a wide variety of panels thereby increasing the uniformity of the current and improving measurement accuracy
  - design the optimum panel for a specific sample minimizing the number of shots required for a given sample
- The simulations reproduced experimental free-surface velocities very well; resolution is the only limitation in 3D



# Backup slides



# ALEGRA: a Magneto Hydrodynamic Code

- Arbitrary Lagrangian-Eulerian finite element 2-D and 3-D code
- Includes:
  - Magneto hydrodynamics (MHD)
  - Thermal conduction
  - Radiation transport
  - Material models
- Coupled with large number of material data (equation of states, opacity tables...)

## References:

1. R. M. Summers, J. S. Peery, M. W. Wong et al., Int. J. Impact Engineering, 20 (1997), pp. 779–788.
2. J. S. Peery & D. E. Carroll, Computer Methods in Applied Mechanics and Engineering, 187 (2000), pp. 591–619.