

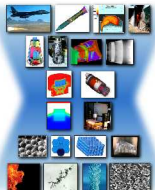
***Development of Experimental Model Validation Data
for
Viscoelastic Foam Models***

7th Biennial Tri-Laboratory
Engineering Conference

May 10th, 2007

Chris O’Gorman

Experimental Structural Dynamics, 01521
Sandia National Laboratories





Foam Development and Validation

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Lead Experimentalist

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Experimental Modal Data

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Management

T.Y. Chu

Management

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Model Validation

Jordan Massad

Model Validation

Brian Rutherford

Design of Experiments

Garth Reese

Code Development

Tim Walsh

Code Development

Terry Hinnerichs

Lead Analyst

Ed Russick

Foam Development

Tina Huber

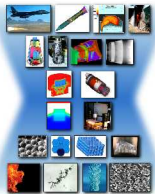
Foam Development

Jim Aubert

Foam Development

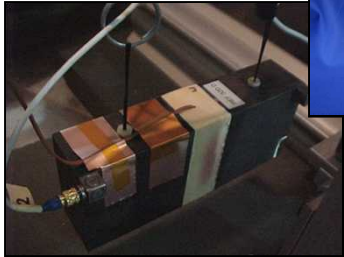
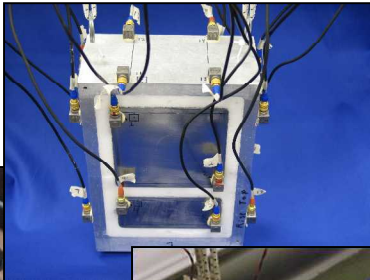
Doug Adolf

Foam Development

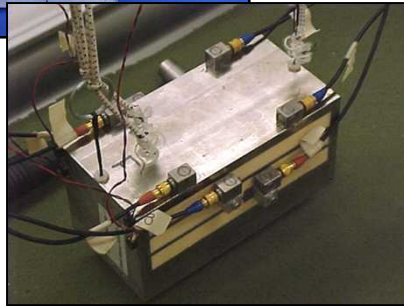


Potting Foam Validation

Phase II



Phase I



Phase III

Problem Description:

- Many weapon components use potting foam to mitigate shock and vibration
- The objective of this project is to improve the modeling capability of systems and components using foam encapsulants.

Technical Approach/Challenges:

- Complete temperature testing of Phase II and Phase III geometries
- Analyze and prepare data for use in validation process
- Support validation of Phase I, II and III models using sub-ambient and elevated temperature experimental data
- Archive data and write test and validation reports

Team Members

PI: *Chris O’Gorman, 1521*

Patrick Hunter, 1521

Computational PI:

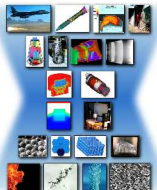
Terry Hinnerichs, 1524



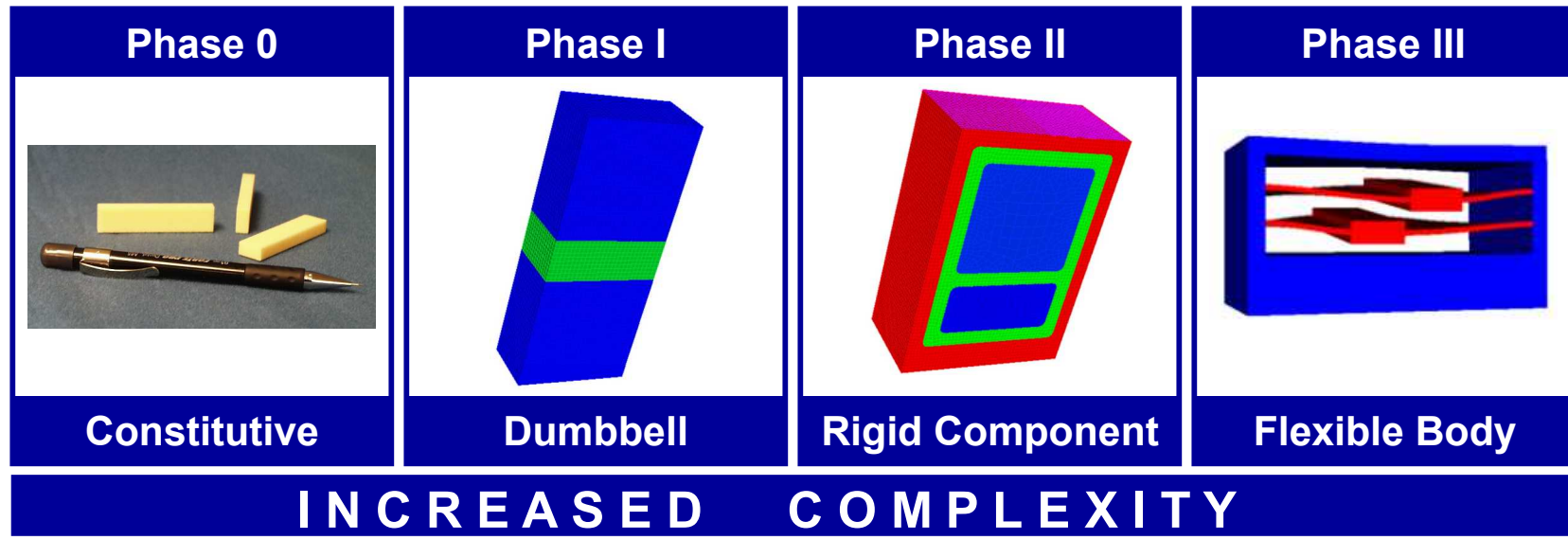
Project Objectives

Foam Development Activities

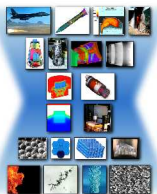
- **EF-AR20**
 - Constitutive, Phase I, Phase II and Phase II
 - Focus of Level II Hostile Blast Milepost
 - ECS and LFU
- **REF-308**
 - Constitutive, Phase I and Phase III
- **REF-320**
 - Constitutive and Phase I
- **RSF-200**
 - Constitutive and Phase I
- **PMDI-8**
 - Constitutive and Phase I
- **TF-6070-8.5**
 - Very little data (W80-3), system level tests performed



Development Process

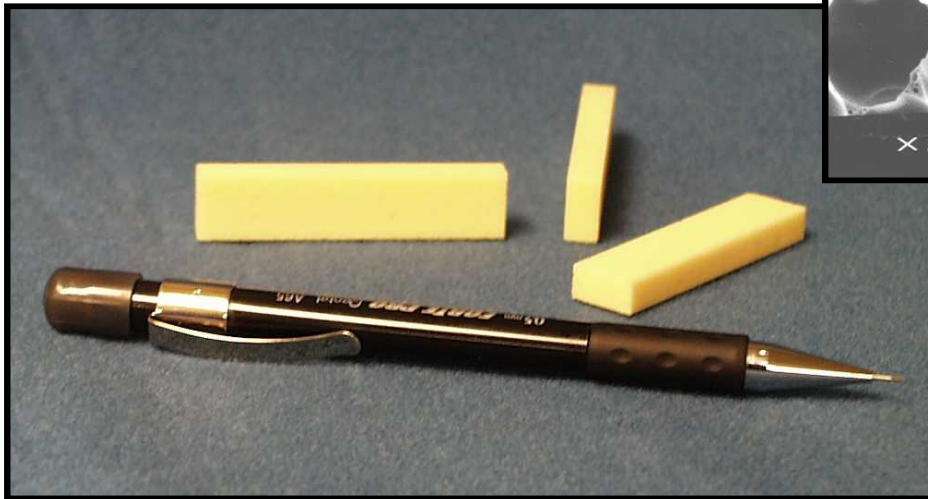
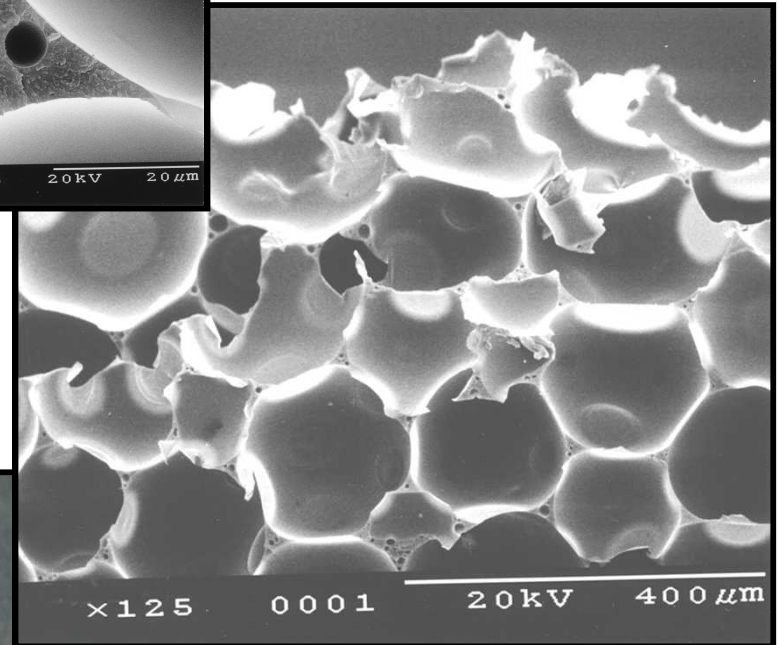
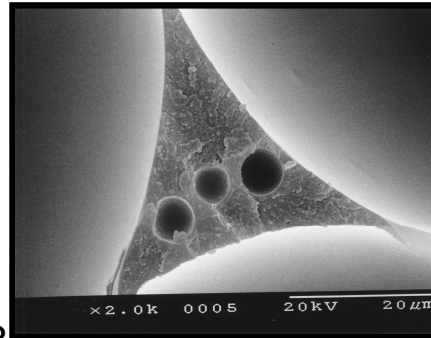


- Project experiments will emphasize the fundamental physics associated of foam-confined components with geometries of increased complexity
- The physical parameter space is significantly simplified, but the **environmental parameter space** involving temperature, frequency, strain and density **will be maintained**



Foam Description

- “Rigid” Epoxy Foam
- Closed-Cell
- Nominal Density - 20 lb/ft³
- Mitigate shock and vibration
- Average cell diam. ~200 μm



Ambient Calibration Geometries



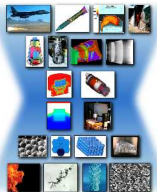
Phase 0 - Constitutive Testing with Foam Coupon Samples

- $E(\omega, T, \rho)$, $G(\omega, T, \rho)$, ν
- ω – DMA, Phase I Modes
- T – T_g , DMA, Phase I Modes



Phase I - Component Testing with Foam between end-blocks

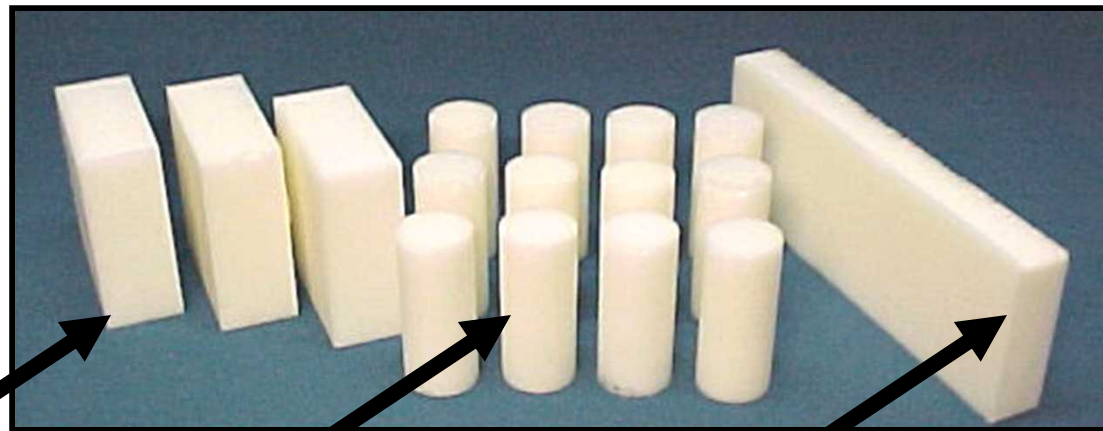
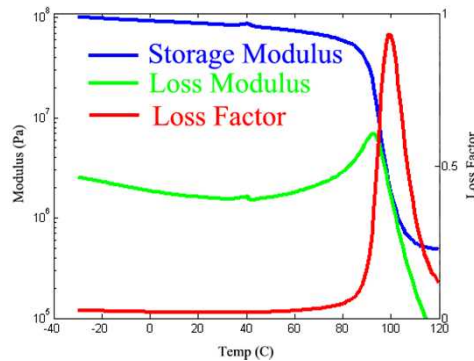
- Phase I Samples will be characterized using Modal Tests
- Foam properties are only unknowns
- Component Response is very sensitive to Foam properties



Constitutive Experiments

Foam Characterization

- 5 ea. Tensile Modulus Tests
- 5 ea. Compressive Modulus Tests
- 5 ea. Shear Modulus – T_g Tests
- 5 ea. Shear Modulus – DMA Tests
- Total of 20 data sets collected to characterize E and G
- Parameter space includes temperature and frequency
- Inherent variation as replicate samples differ in mean density



Phase I Blocks

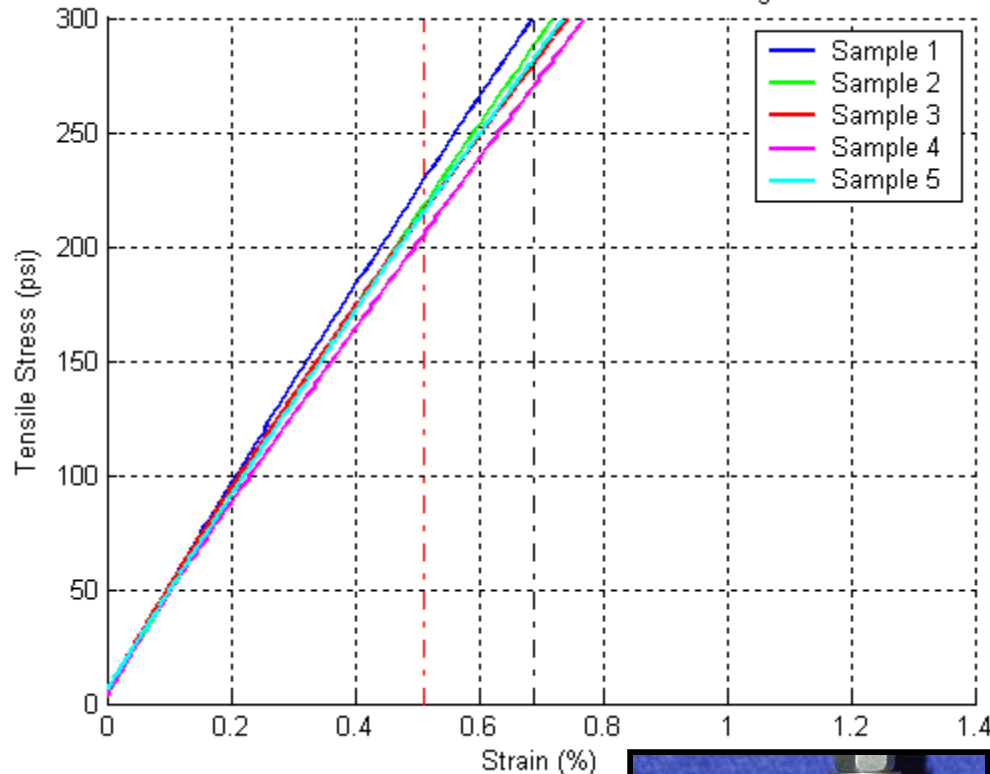
Tensile and Compressive
Modulus Blocks

T_g and DMA
Block

EF-AR20

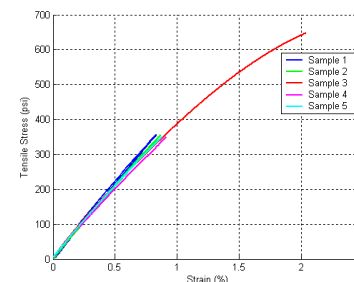
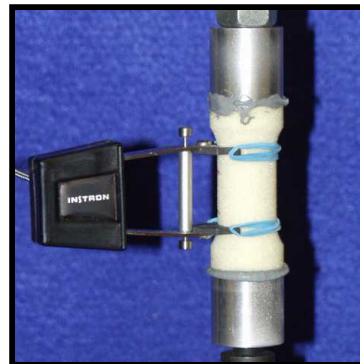
Tensile Modulus Testing

FY03 EF-AR20 Tensile Modulus Testing



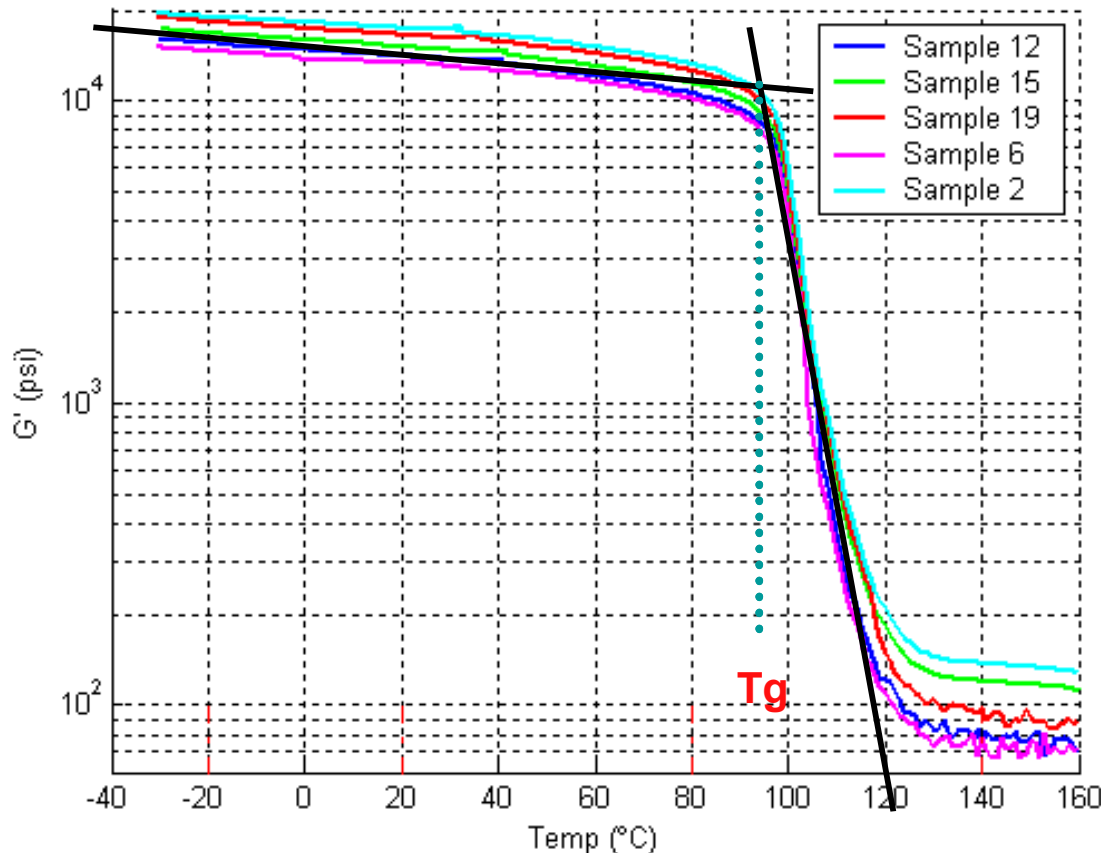
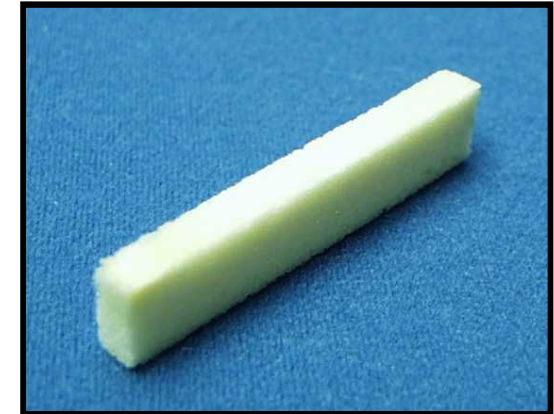
Sample	Density (lb/ft ³)	Strain (%)	Et (psi)
3	18.5	0.6	36,568
5	18.5	0.6	37,725
4	19.1	0.6	36,622
2	19.6	0.6	39,277
1	19.9	0.6	40,590

- Slightly nonlinear stress-strain relationship due to cellular interaction
- Specimen failure at ~2% strain
- Consistent failure at lower extensometer knife edge



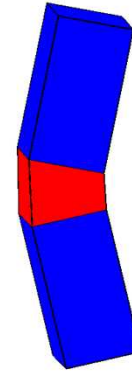
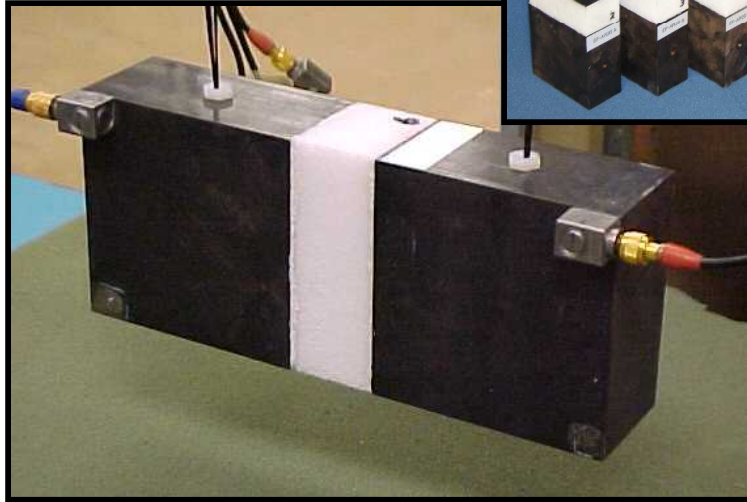
EF-AR20 T_g Calibration Data

Sample	Density (lb/ft ³)	G (psi)			
		Temp -20 C	Temp 20 C	Temp 80 C	Temp 140 C
6	18.2	14,649	13,445	10,080	72
12	18.4	15,519	14,040	10,588	82
15	19.5	16,679	15,229	11,400	120
19	20.5	18,275	16,534	12,488	97
2	20.7	19,000	17,405	13,155	137

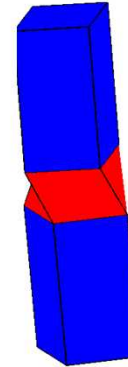


- Torsional strain at 1 Hz
- Temperature varied from -30°C to 160°C
- Temperatures defined by specified application space
- Modulus changes by 2 orders of magnitude from glassy to rubbery
- T_g ~ 95°C

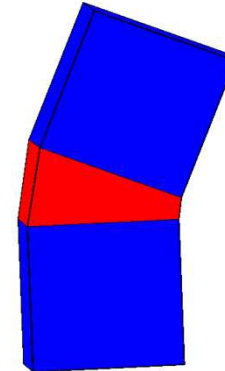
EF-AR20 Phase I Data



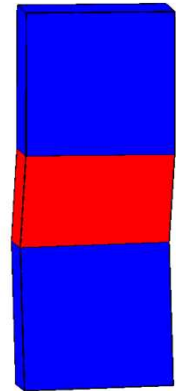
1st Bending X



Torsion

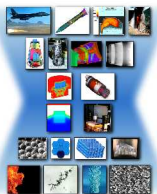


1st Bending Y

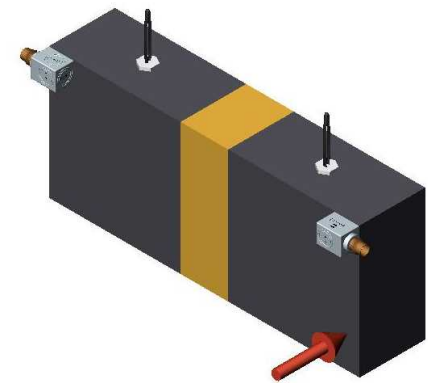


Axial

- Phase I samples used to supplement constitutive data
- Mechanism to test various frequencies at room temperature
- Low strain helps minimize uncertainties caused by cellular interaction



Calibration Data – Input 6x

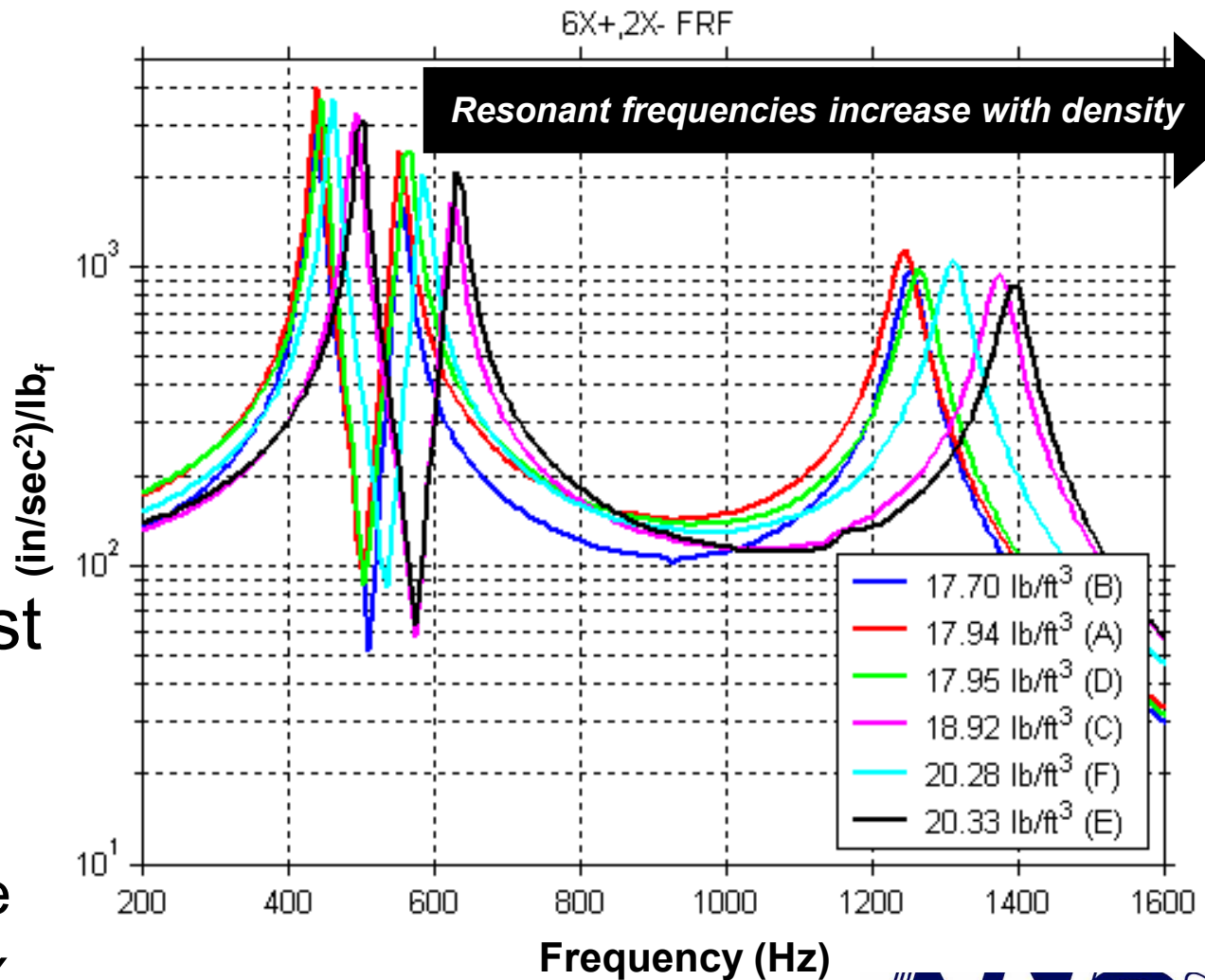
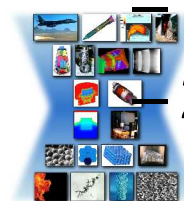


- Impacts optimized to excite the most modes

- 1st bending X

- Torsion mode

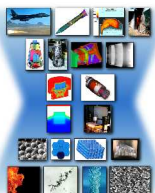
- 2nd bending X



Phase I Calibration Data Summary

Mode #	Mode Description	Sample A 17.94 lb/ft ³		Sample B 17.70 lb/ft ³		Sample C 18.92 lb/ft ³	
		Frequency (Hz)	Damping (%)	Frequency (Hz)	Damping (%)	Frequency (Hz)	Damping (%)
1	1st Bending X	440.7	1.3	430.5	1.3	462.3	1.3
2	Torsion	553.7	1.3	543.3	1.3	585.4	1.3
3	1st Bending Y	724.8	1.3	710.7	1.4	755.2	1.3
4	Axial	1045.2	1.4	1038.3	1.5	1088.7	1.4
5	2nd Bending Y	1113.1	1.4	1090.0	1.4	1176.1	1.4
6	2nd Bending X	1246.1	1.5	1226.9	1.5	1312.8	1.5

Mode #	Mode Description	Sample D 17.95 lb/ft ³		Sample E 20.33 lb/ft ³		Sample F 20.28 lb/ft ³	
		Frequency (Hz)	Damping (%)	Frequency (Hz)	Damping (%)	Frequency (Hz)	Damping (%)
1	1st Bending X	445.5	1.2	501.7	1.2	493.2	1.2
2	Torsion	561.0	1.3	633.8	1.2	626.9	1.3
3	1st Bending Y	730.7	1.3	814.9	1.3	807.1	1.3
4	Axial	1053.3	1.4	1159.6	1.3	1144.9	1.3
5	2nd Bending Y	1119.6	1.4	1234.6	1.4	1227.5	1.4
6	2nd Bending X	1258.7	1.5	1396.0	1.4	1375.4	1.4





Characterization of Test Uncertainty

Magnitude Error 4.7%

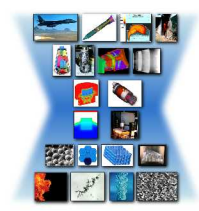
1. Accelerometer 4%
 - Impact Level
 - Orientation
2. Data Acquisition 2.5%
 - Meter
 - DC Offset
 - Mean Amplification
 - Amplification Uncertainty

Error Description	Error (%)
Meter Uncertainty	0.1
DC Offset	0.3
Error in Mean Amplification	2.1
Amplification Uncertainty	1.3
Total Uncertainty	2.5

Frequency Error 2.4%

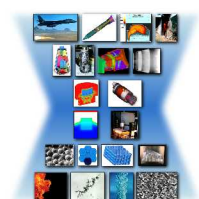
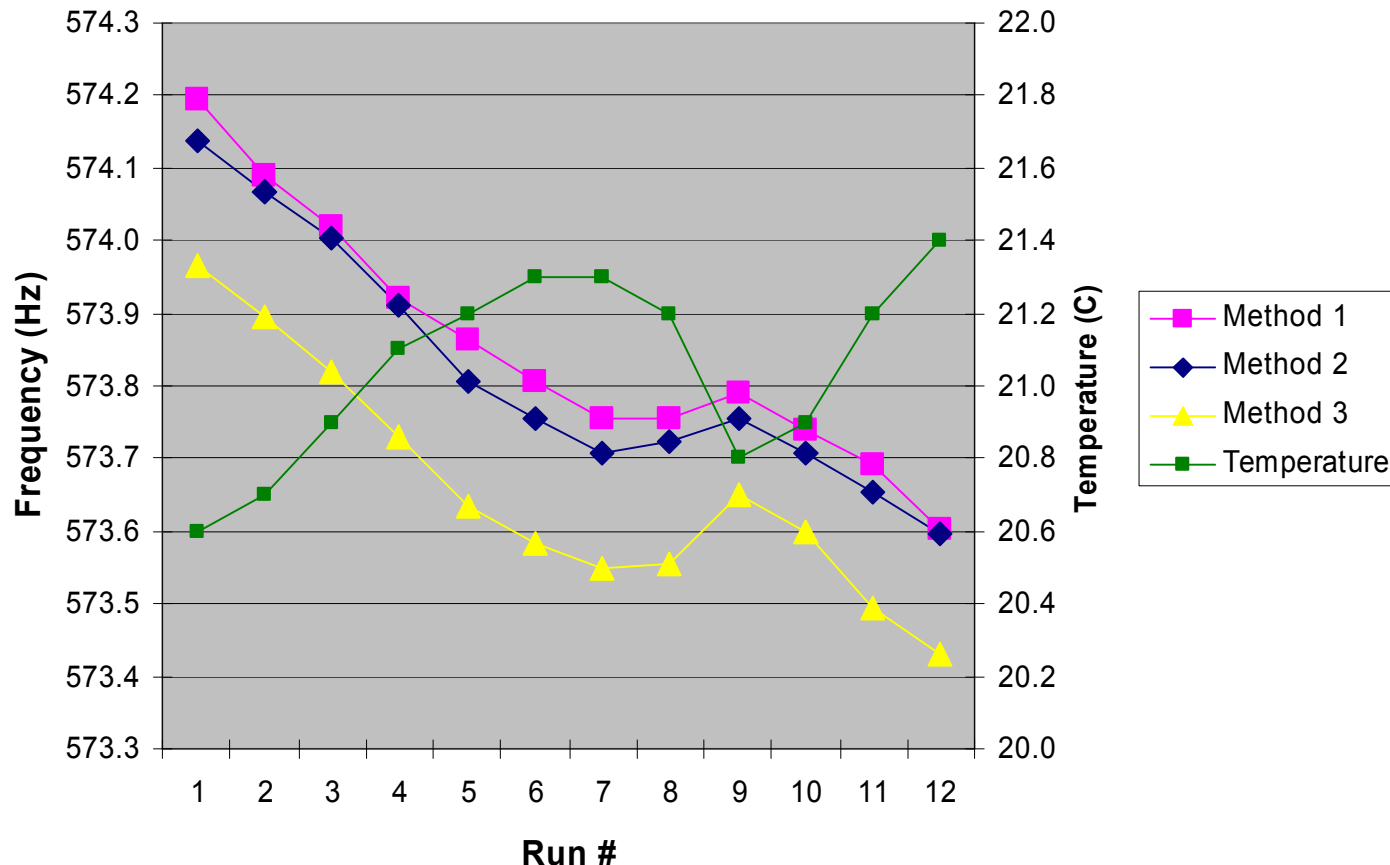
Damping Error 13.3%

1. Test/Test
2. Setup/Setup
 - Cable Slack
 - Mass Loading/Damping
 - Impact Level
 - Orientation
 - Frequency Resolution
3. Unit/Unit
4. Environmental
 - Temperature
 - Pressure
 - Humidity
5. Other
 - Aging



Test/Test Variability

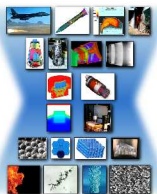
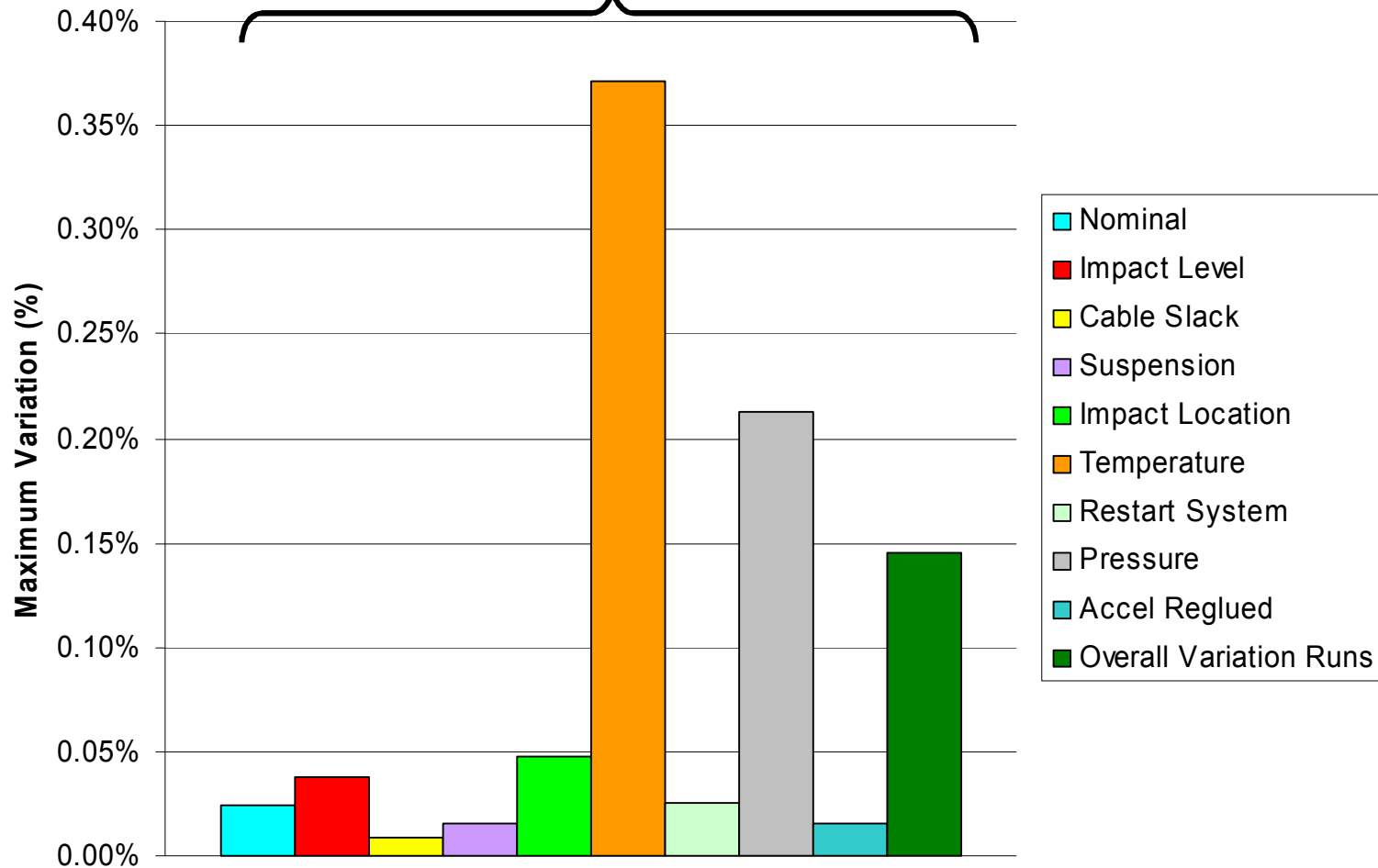
- “Bias” variation in fit method
- Frequencies appear to be decreasing
- Minimal Test/Test variation ($\sim 0.14\%$)
- Technique able to observe small variations



Phase I

Test Uncertainty – Frequency

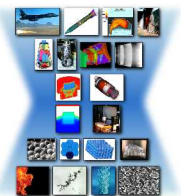
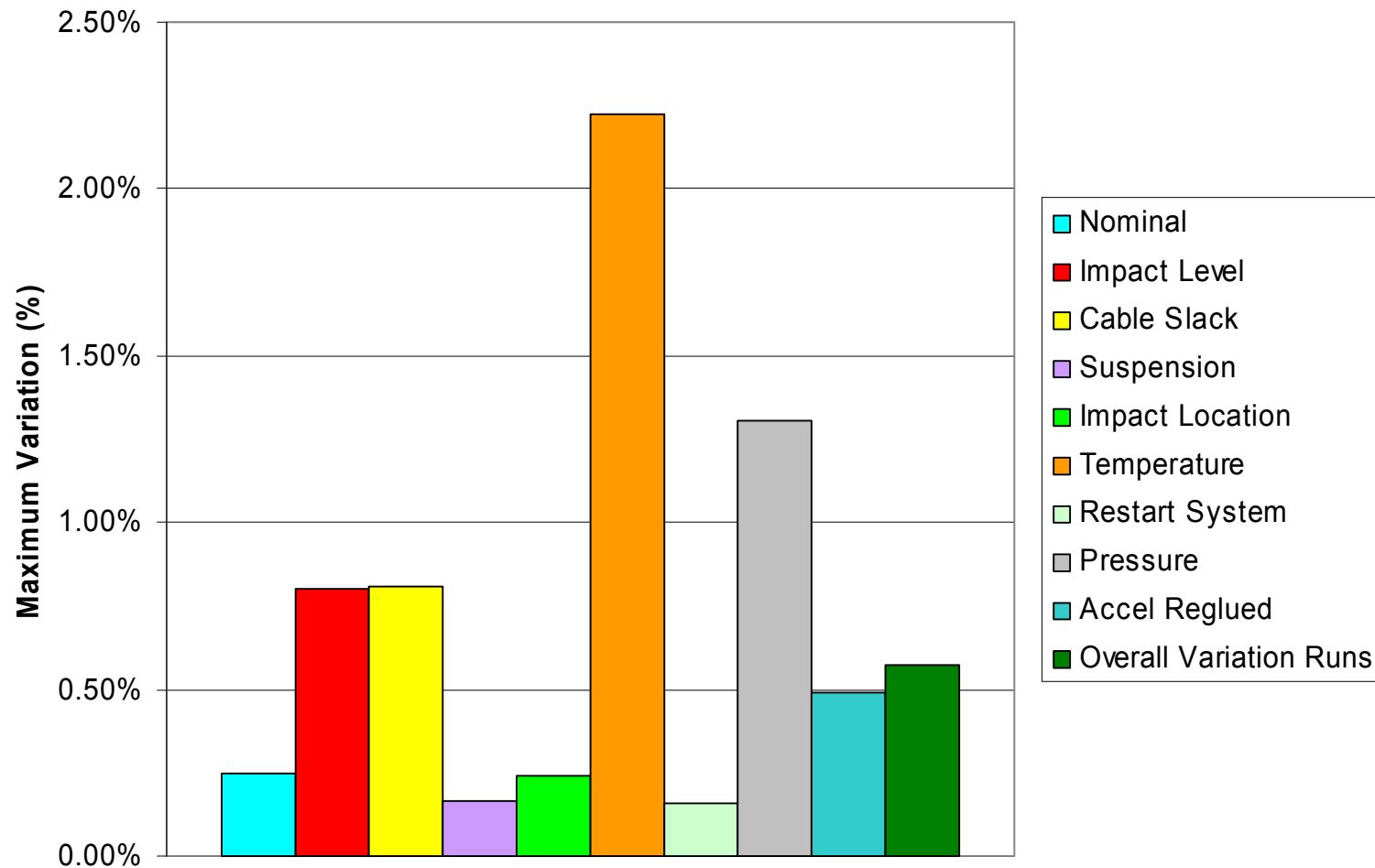
Parameters varied over representative ranges





Phase I

Test Uncertainty – Damping



Experiment/Model Prediction

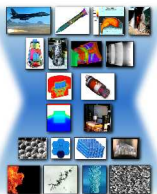
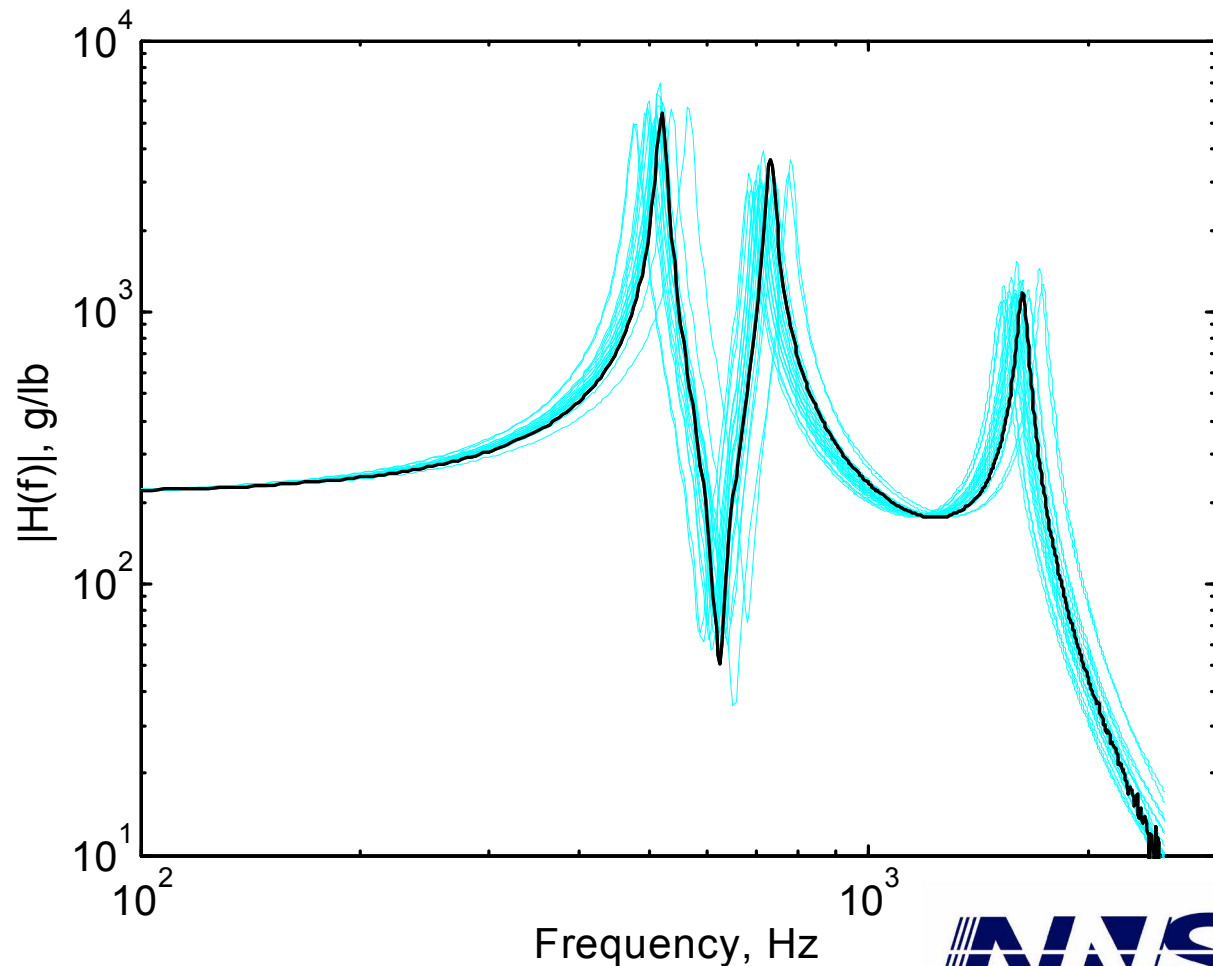
x – direction, $\rho = 16.42 \text{ lb/ft}^3$

Experiment

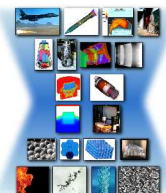
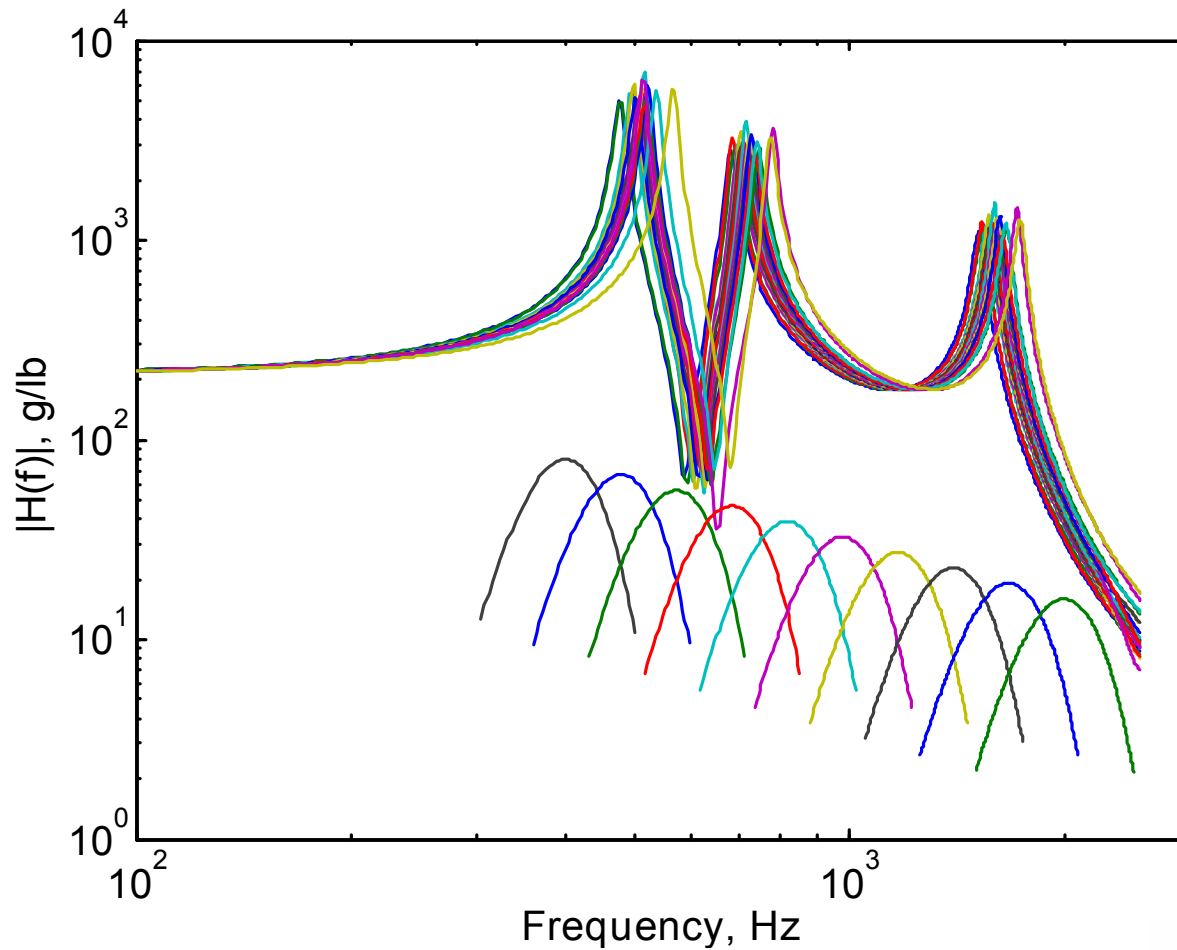
- One realization
- At each of five densities
- Tested in three directions

Model

- 20 Realizations
- At each of the five densities
- Predicted in three directions



Computation Graphic



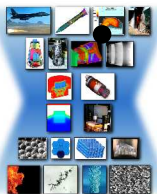
The figure is a scatter plot showing the relationship between Frequency (Hz) on the x-axis and Response Measure, $M(f_c)$, g/(lb-sec) on the y-axis. The x-axis ranges from 0 to 2500 Hz with major ticks every 500 Hz. The y-axis ranges from 0 to 1600 g/(lb-sec) with major ticks every 200 units. Multiple data series are plotted, each represented by a different color (blue, red, green, yellow, cyan, magenta, grey). The data points show a general trend of decreasing response measure as frequency increases, with a notable peak or cluster of high values between 400 and 600 Hz. For example, at approximately 450 Hz, the response measure for some series reaches nearly 1600 g/(lb-sec). By 1000 Hz, the response measure for all series has dropped significantly, mostly falling below 400 g/(lb-sec). At 2000 Hz, the response measure is at its lowest, with most points below 200 g/(lb-sec).



Validation Comparison

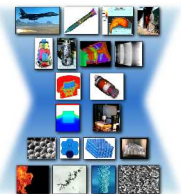
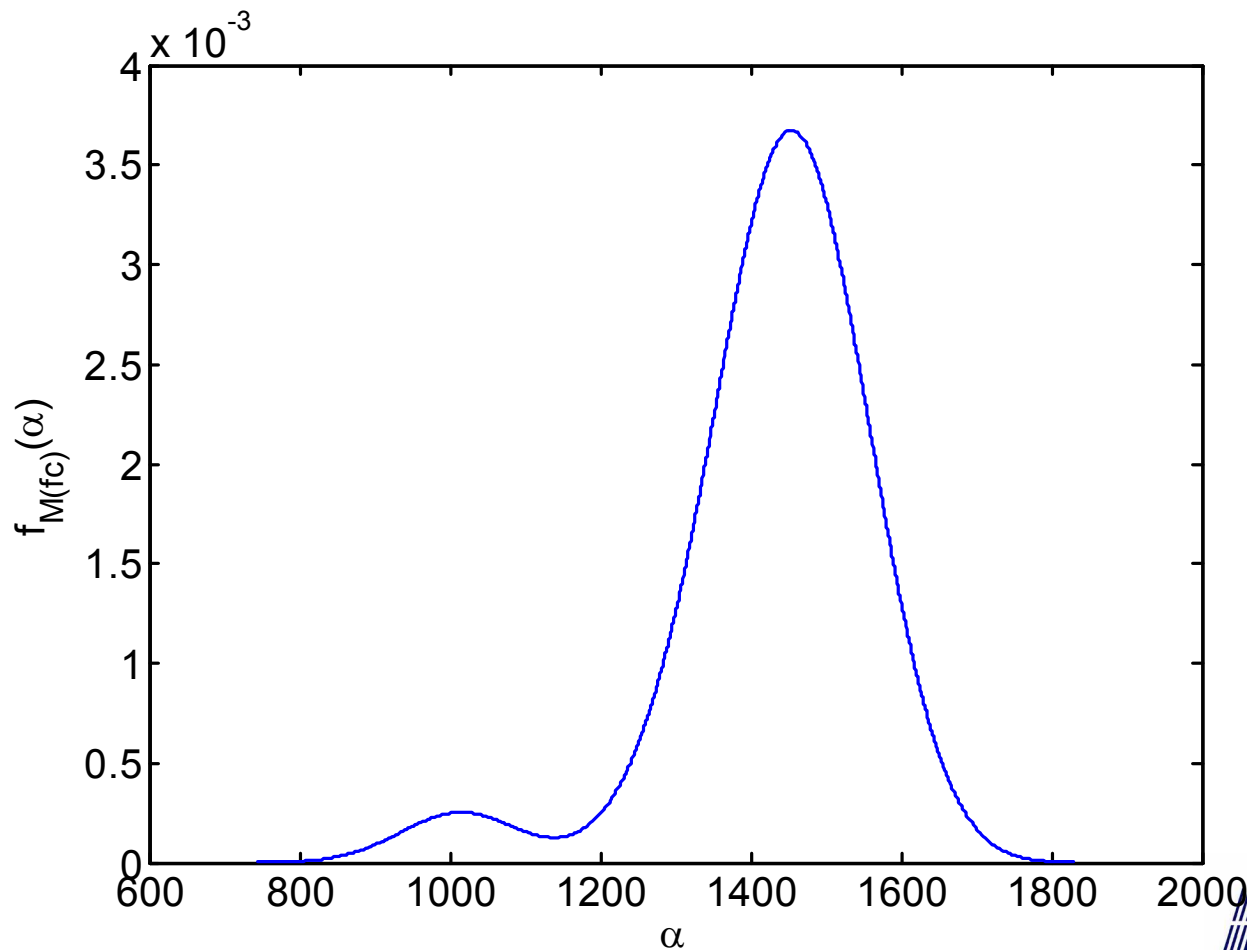
- Estimate the PDF of response measures from realizations of mathematical model FRF.
- Compute 90% probability intervals of response measures from PDFs.
- Locate experimental response measures, $M_{exp}(f_c)$, wrt 90% probability intervals $[L_{90}, U_{90}]$ of math model-predicted response measures, $M_{mod}(f_c)$.
- If $M_{exp}(f_c) \in [L_{90}, U_{90}]$ model acceptable
- Else, model not acceptable

85%



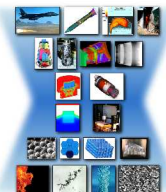
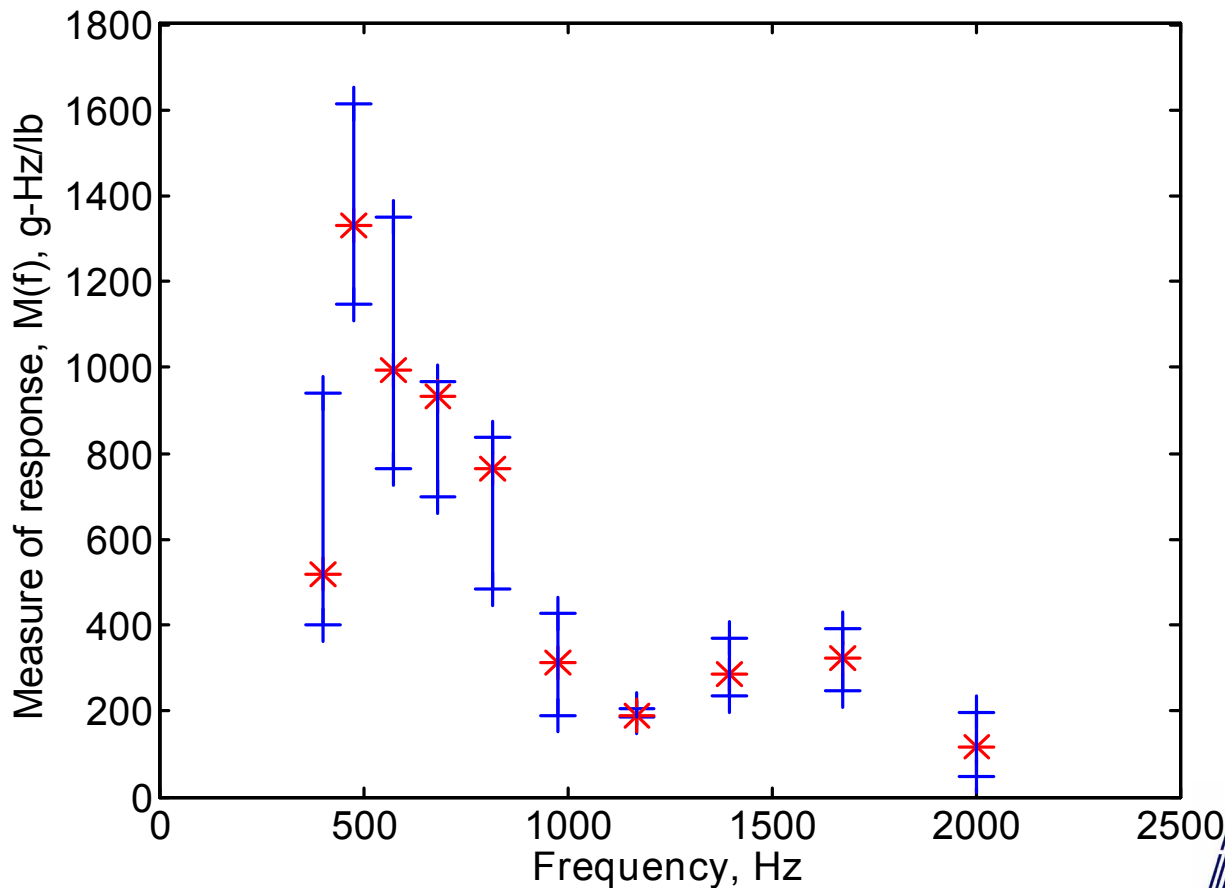
Example

Phase I Validation Specimen, 16.42 lb/ft³, x - direction $f_c = 478$ Hz



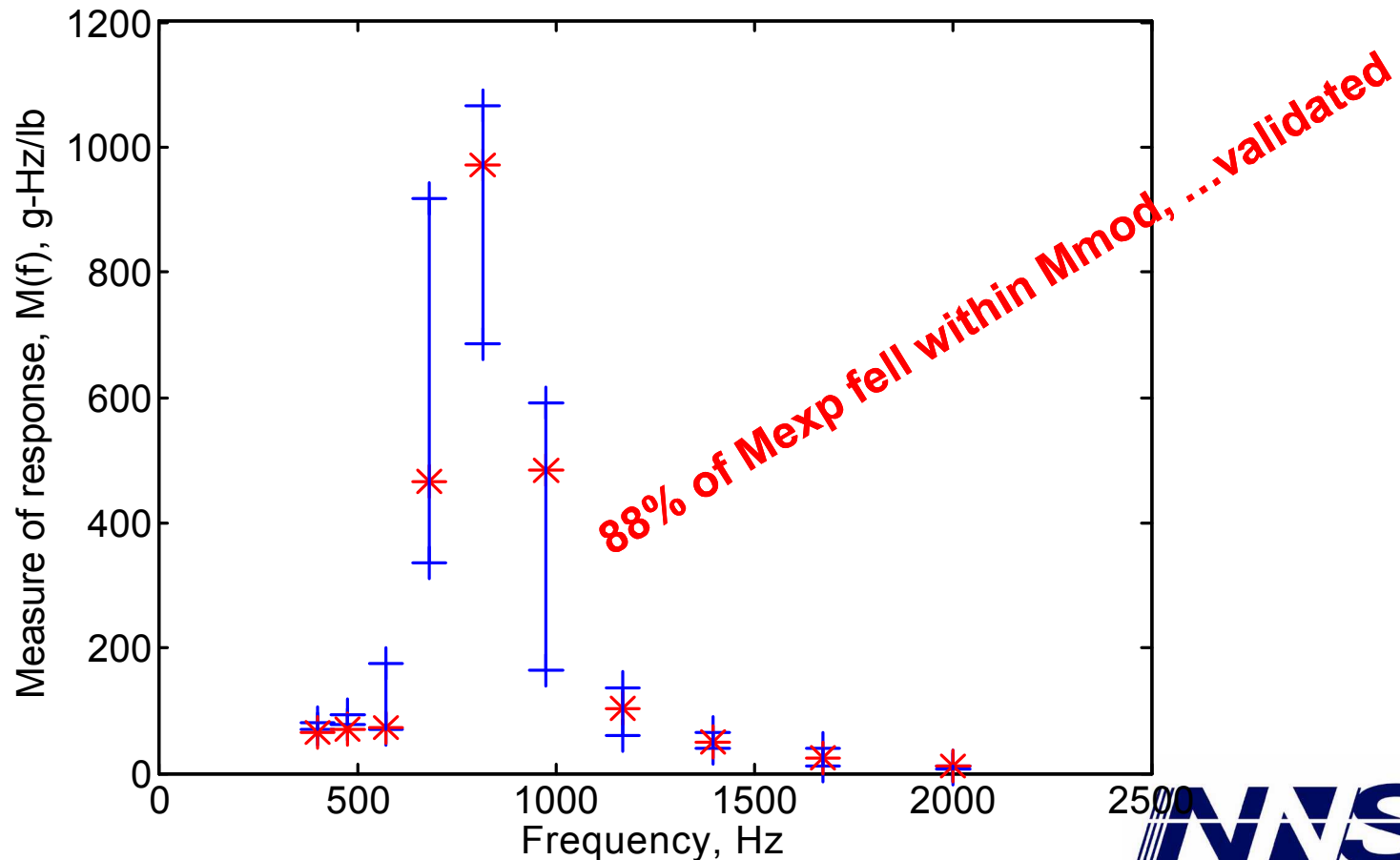
Example

Phase I Validation Specimen, 16.42 lb/ft³, x – direction, 90% prob intervals $[L_{90}, U_{90}]$ of $M_{mod}(f_c)$ and $M_{exp}(f_c)$

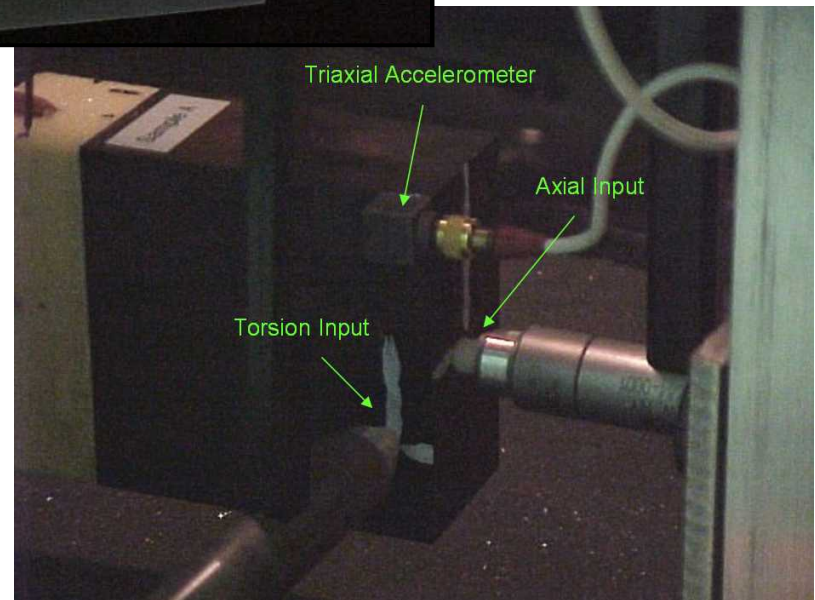
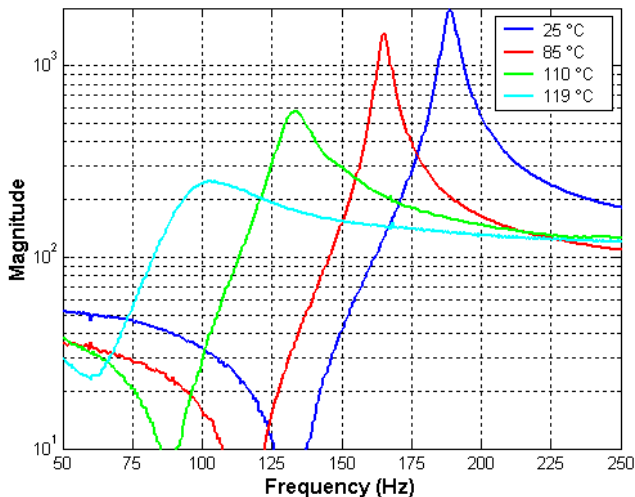


Example

Phase I Validation Specimen, 16.42 lb/ft³, y – direction, 90% prob intervals $[L_{90}, U_{90}]$ of $M_{mod}(f_c)$ and $M_{exp}(f_c)$



Testing conducted inside thermal chamber

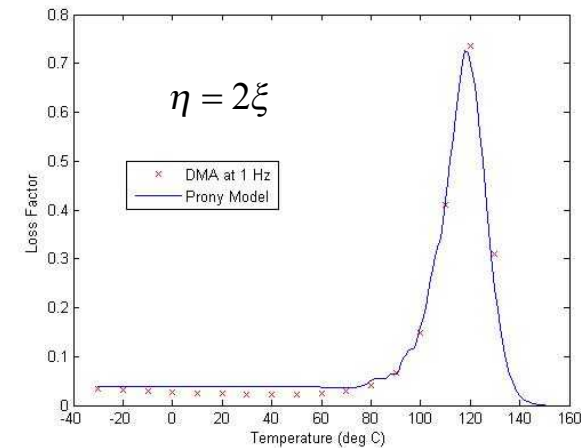


Phase I Temperature Testing

Reference Sample

Thermocouple going into hole to center of foam

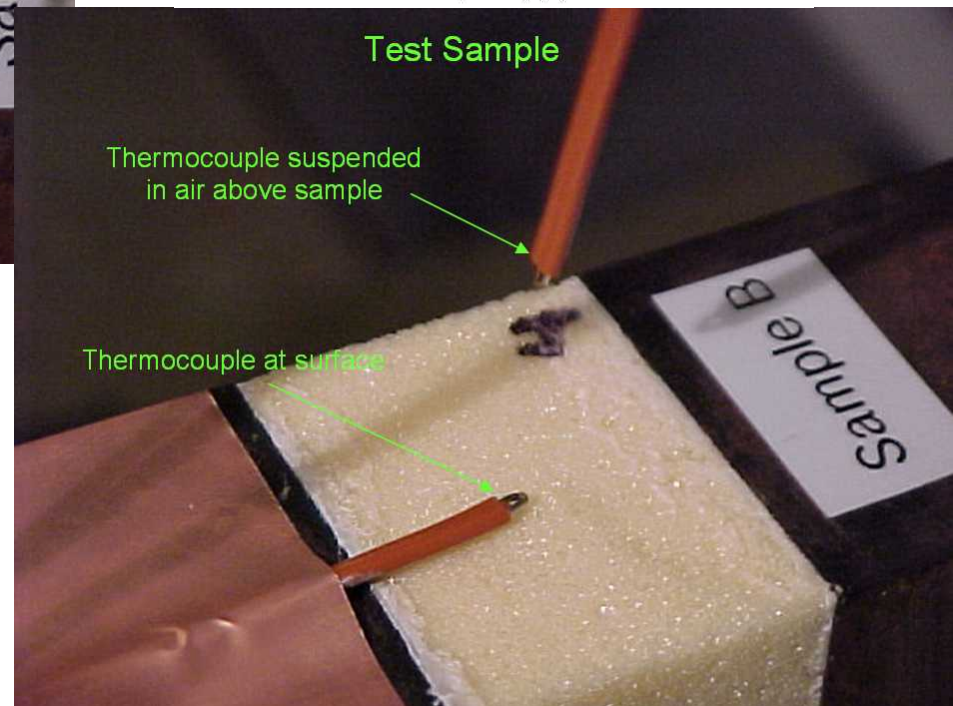
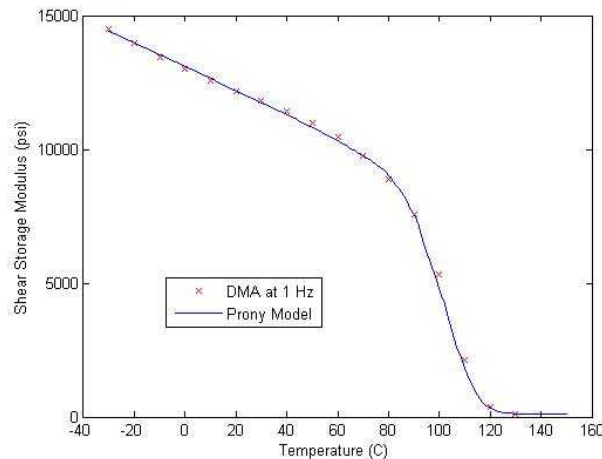
Thermocouple at surface



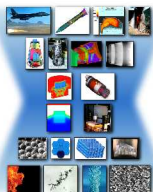
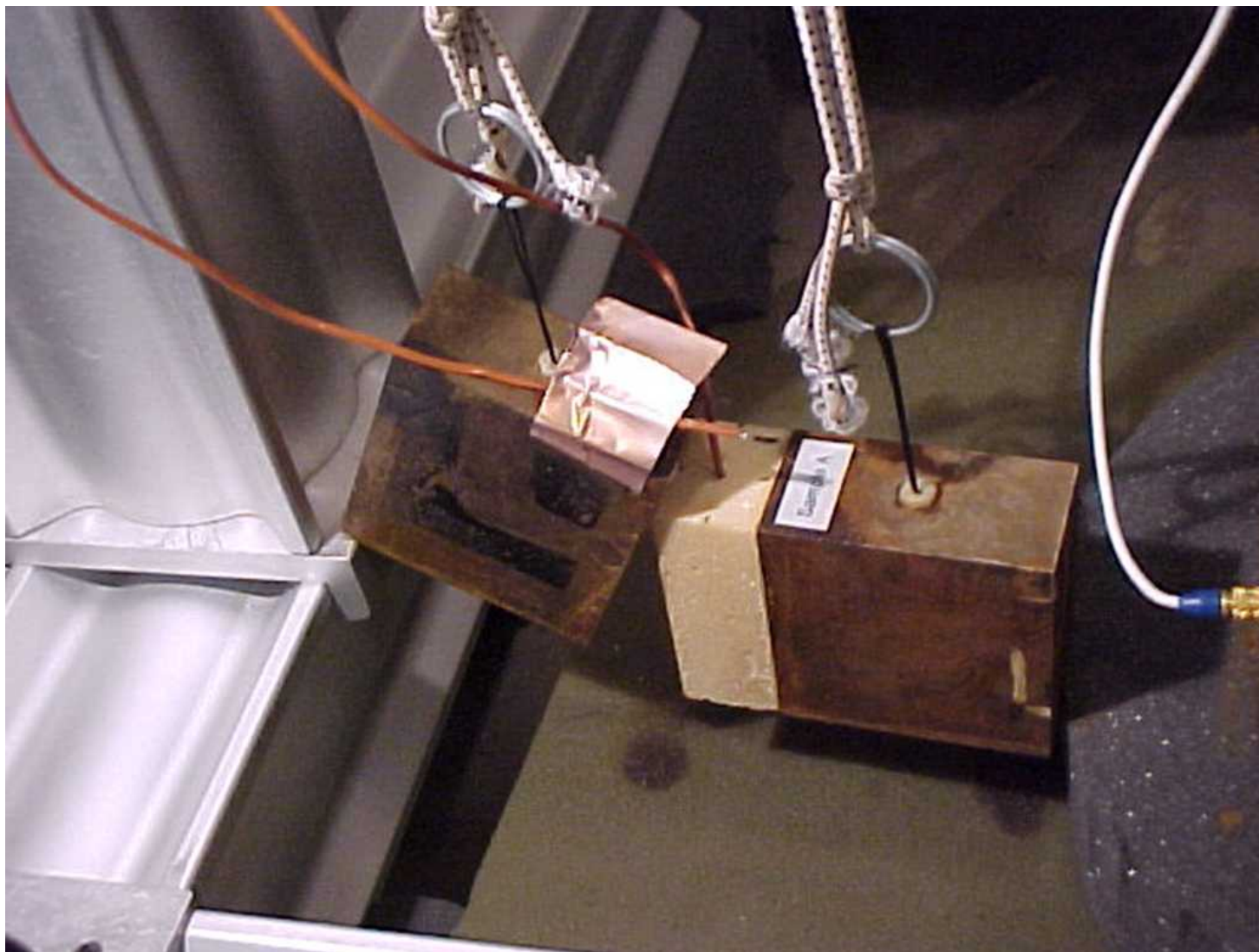
Test Sample

Thermocouple suspended in air above sample

Thermocouple at surface



Breaking at cold temperatures

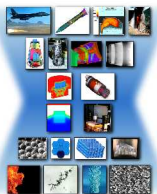
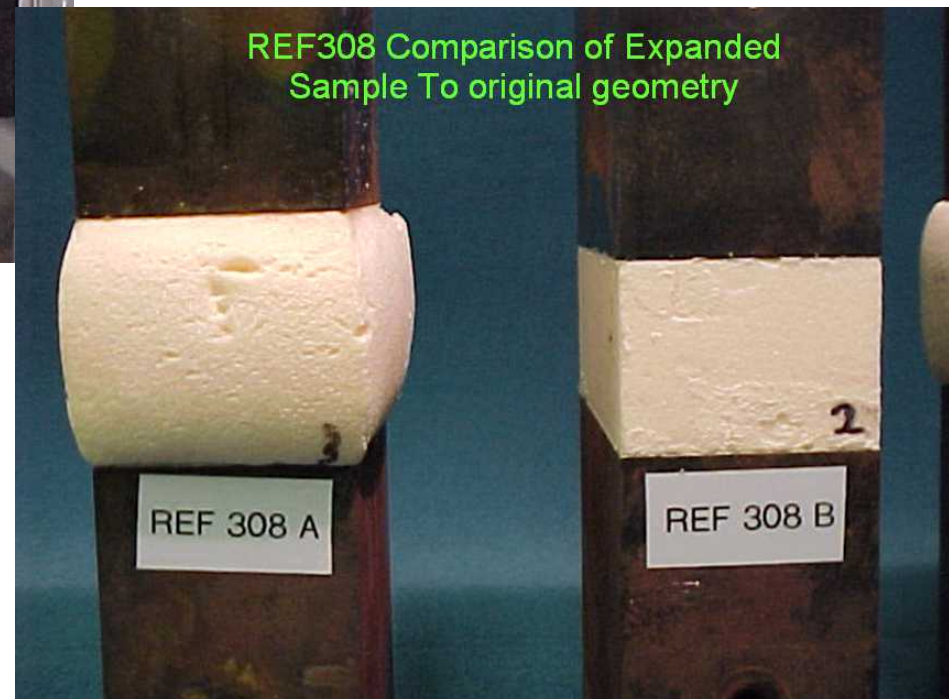


Swelling at hot temperatures

REF308 Sample that Swelled
after the temperature passed T_g

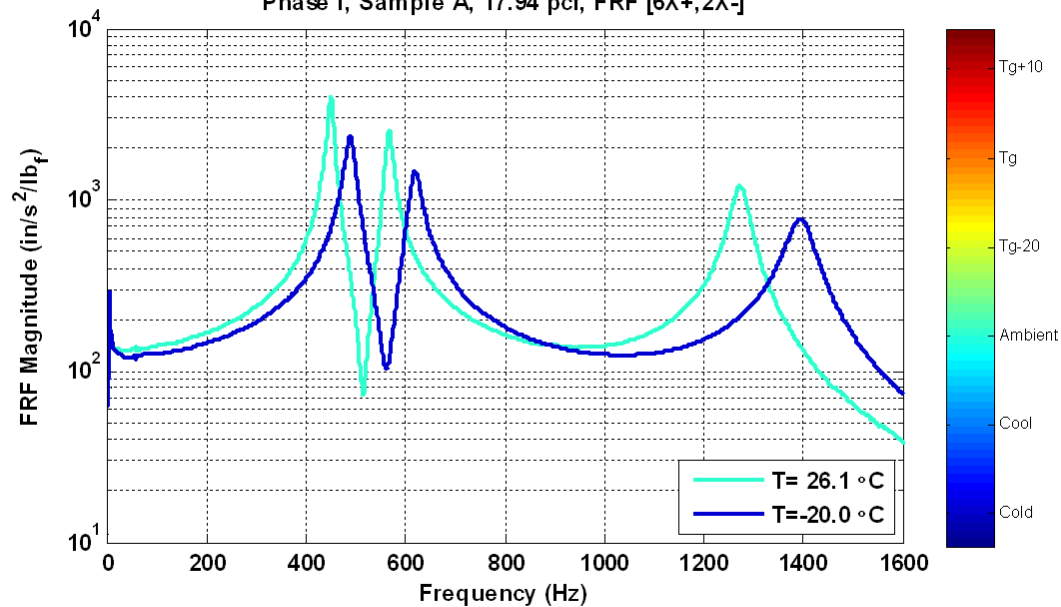


REF308 Comparison of Expanded
Sample To original geometry



EF-AR20, Sample A

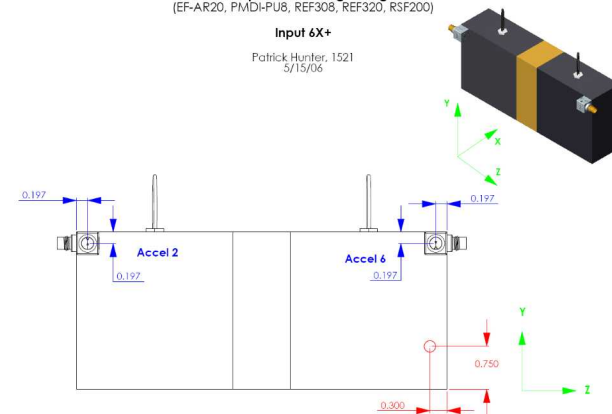
Phase I, Sample A, 17.94 pcf, FRF [6X+,2X-]



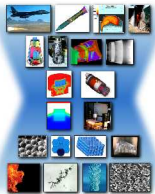
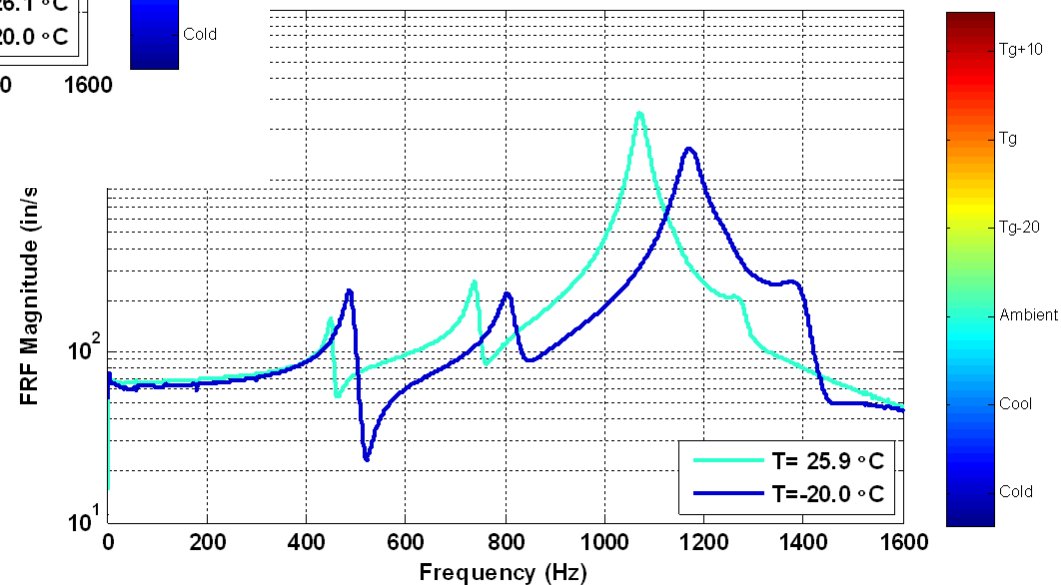
Phase I Temperature Testing Configuration
(EF-AR20, PMDI-PUB, REF308, REF320, RSF200)

Input 6X+

Patrick Hunter, 1521
5/15/06

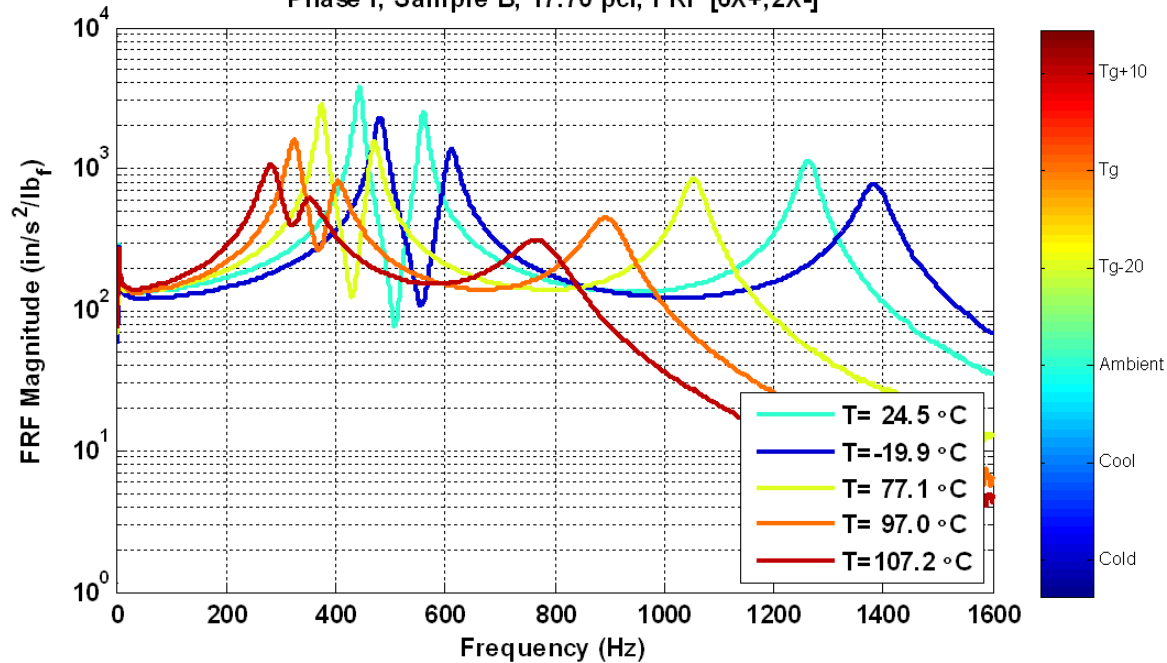


Phase I, Sample A, 17.94 pcf, FRF [6Z-,2Z+]

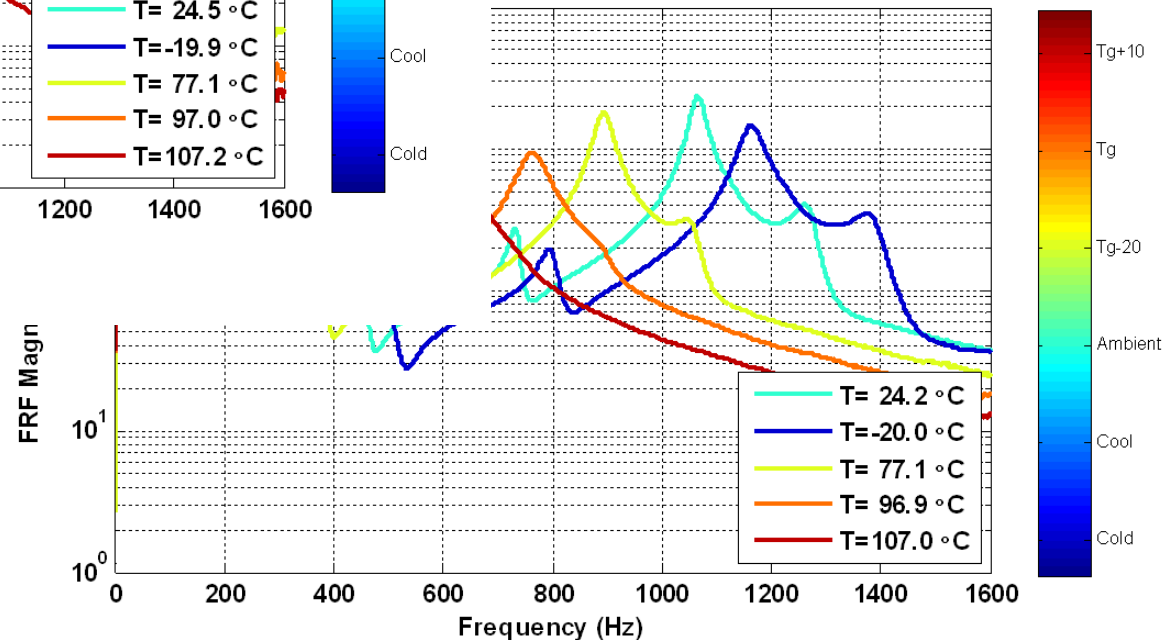


EF-AR20, Sample B

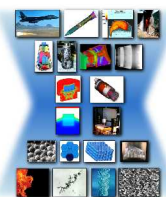
Phase I, Sample B, 17.70 pcf, FRF [6X+,2X-]



B, 17.70 pcf, FRF [6Z-,2Z+]



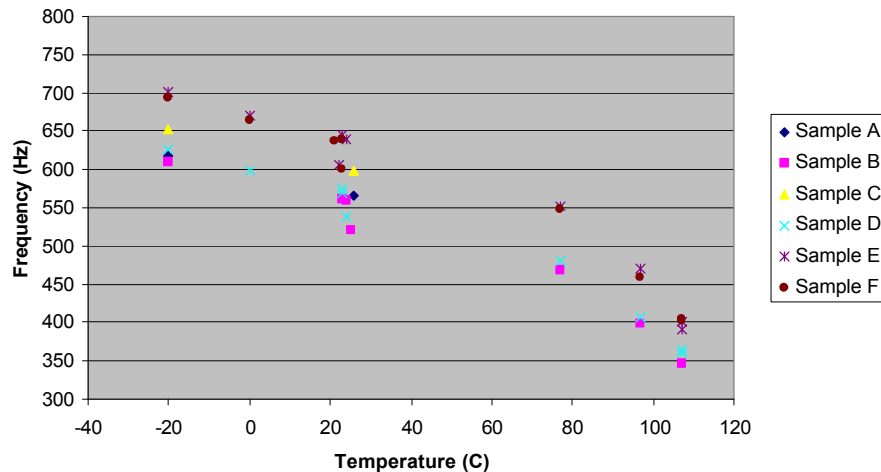
**Sample C, D, E
and F tested
similarly**



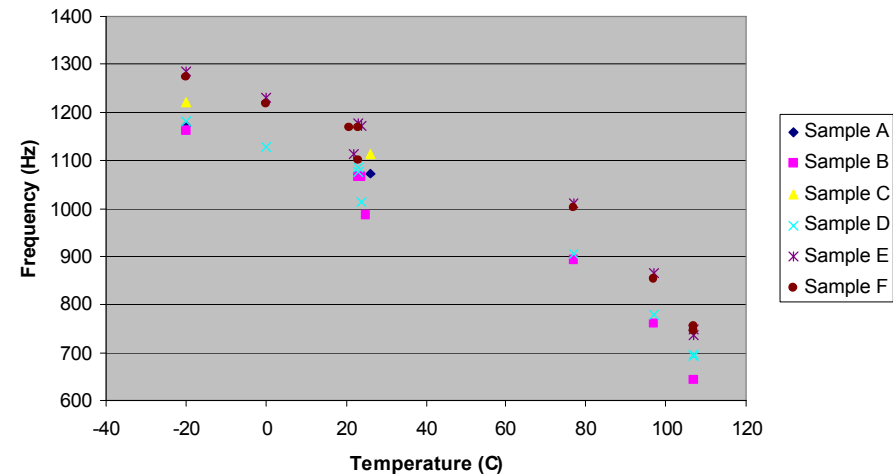
Summary

EF-AR20 Phase I Temperature Data

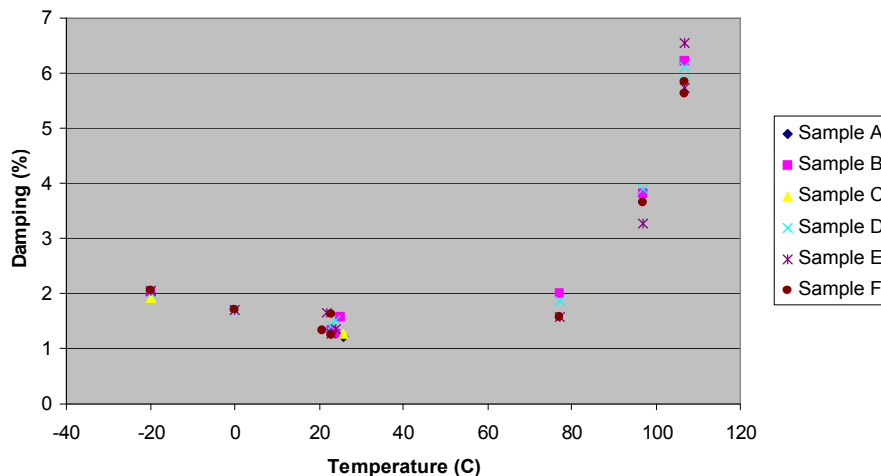
Phase I EF-AR20 Torsion Frequency vs. Temperature



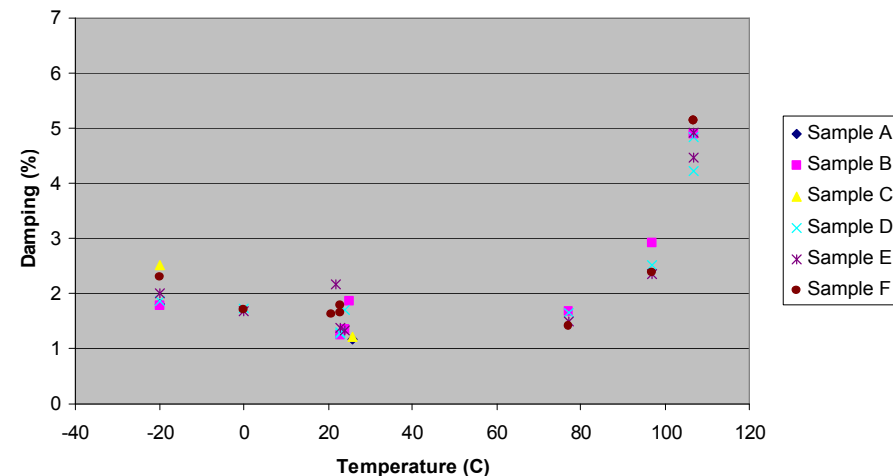
Phase I EF-AR20 Axial Frequency vs. Temperature



Phase I EF-AR20 Torsion Damping vs. Temperature



Phase I EF-AR20 Axial Damping vs. Temperature





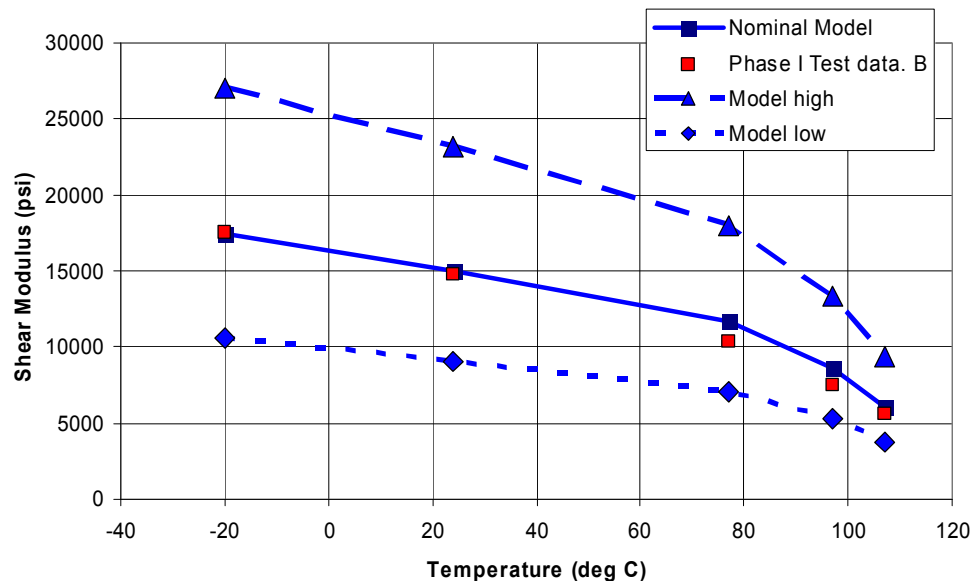
EF-AR20

Viscoelastic Model Validation

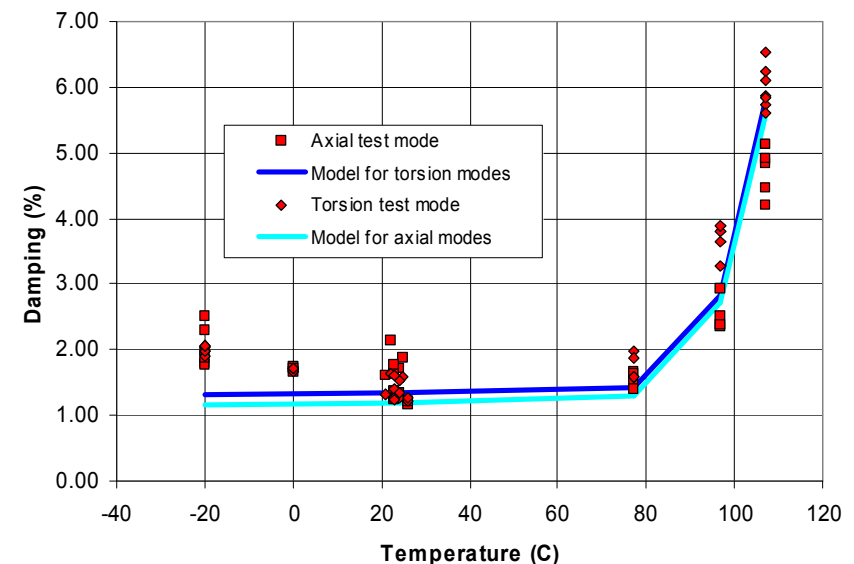
Temperature range of -20 to 107 deg C

Model predictions of modulus and damping vs. test data
- Uncertainty of foam density and modulus factored in

Model vs Test inferred Shear Modulus for Test Article B

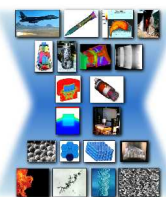


Dumbbell with EF-AR20 foam Damping vs. Temperature



Shear Modulus vs. Temperature

Damping vs. Temperature



EF-AR20

SALINAS input definition for Viscoelastic Model

```
ISOTROPIC_VISCOELASTIC
density 13.2e-3
T_0 90.0
T_current 90.0
C_1 31.6
C_2 111.5
aT_1 2.5
aT_2 0.09
K_g 59978.
K_inf 203.
G_g 30926.
G_inf 104.69
K_relax
#include Prony time constants
K_coeff
#include Prony series coefficients
G_relax
#include tp.dat
G_coeff
#include mp.dat
END
```

Temperature dependence of the Glassy Shear Modulus

$$G_g = G_{g0} * 2.778 * (1 - 0.64 * (T_{\text{current}} / T_0))$$

only for $T_{\text{current}} < T_0$

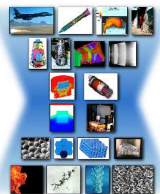
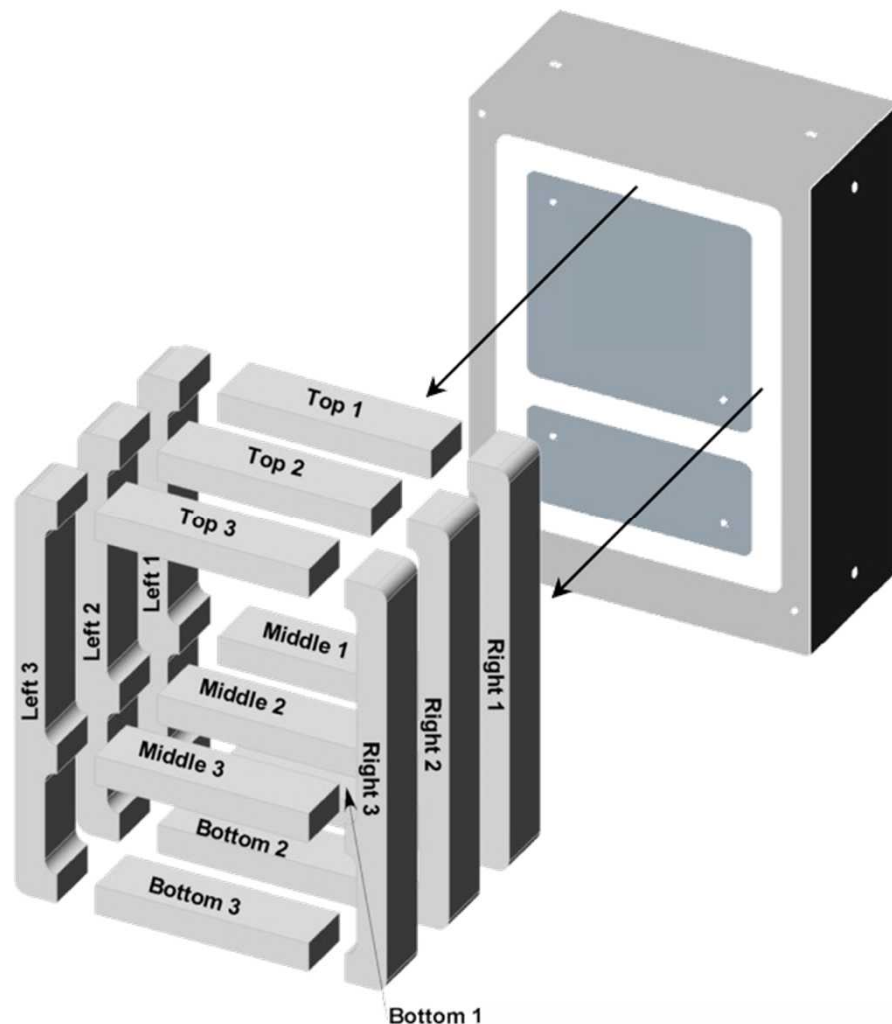
$$K_g = 1.9394 * G_g \text{ based on Poisson's ratio of } 0.28$$

Match Shear Modulus to room temperature value

Density dependence of the Shear Modulus

$$\text{at room temperature: } G = 46 * (\text{density})^2$$

Foam Process Development



Phase II Samples

Benchmark Validation - Shaker Testing			
Sample #	Density (lb/ft ³)	Uncertainty (%)	Notes
1	23.0	7.7	Vented through top plate
2	20.3	8.7	
3	23.0	7.7	Did not fully rise
4	18.6	9.5	
5	20.3	8.7	
6	20.3	8.7	

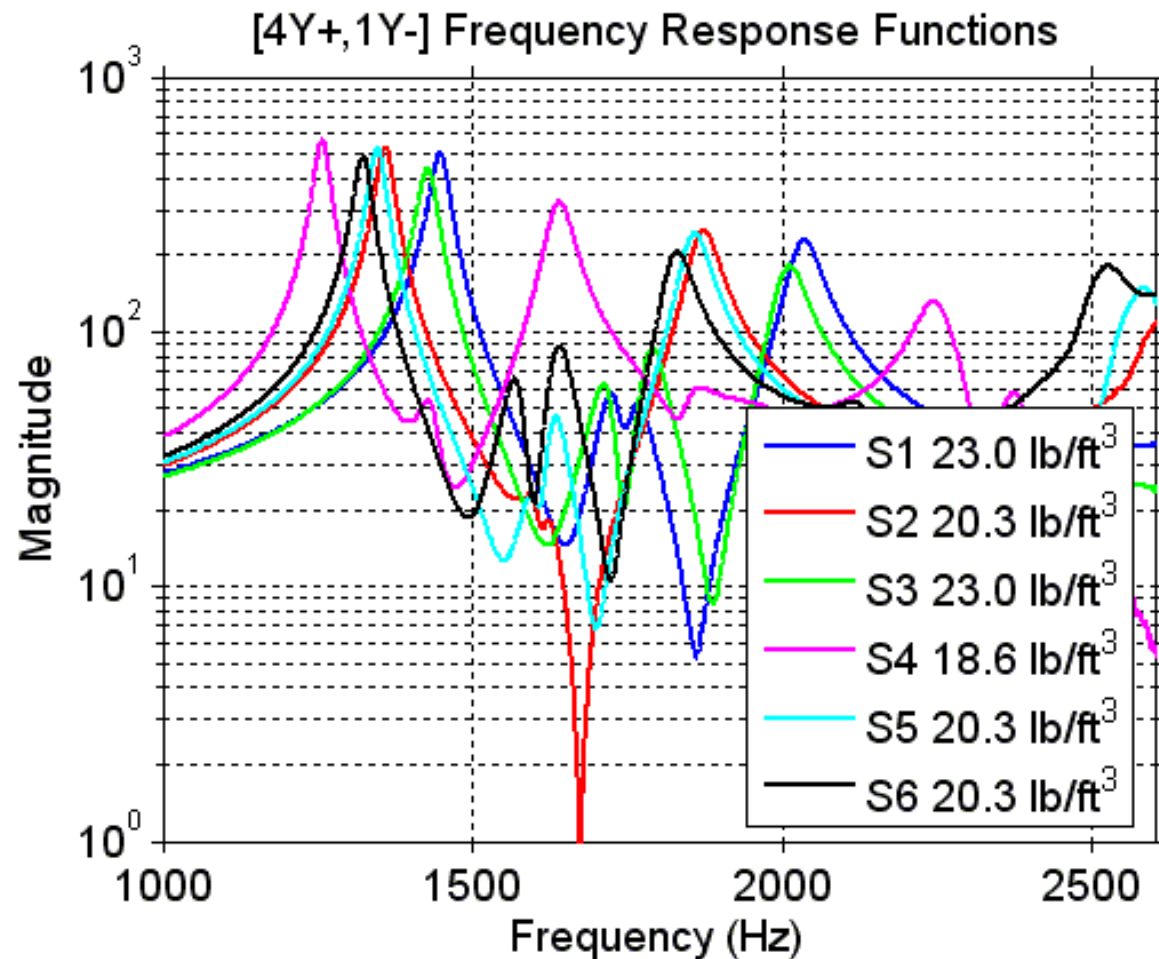
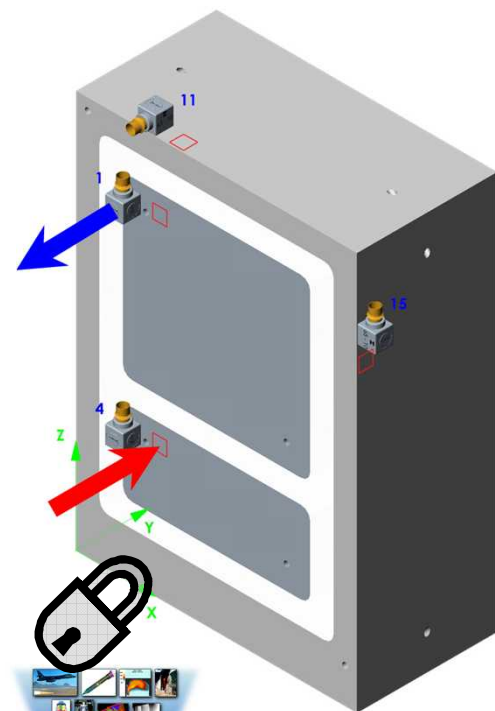


- Parameters from Foam Process Development
- 45°C Preheat, 40% Excess and 9 vent holes

Phase II Modal Validation

In-Axis

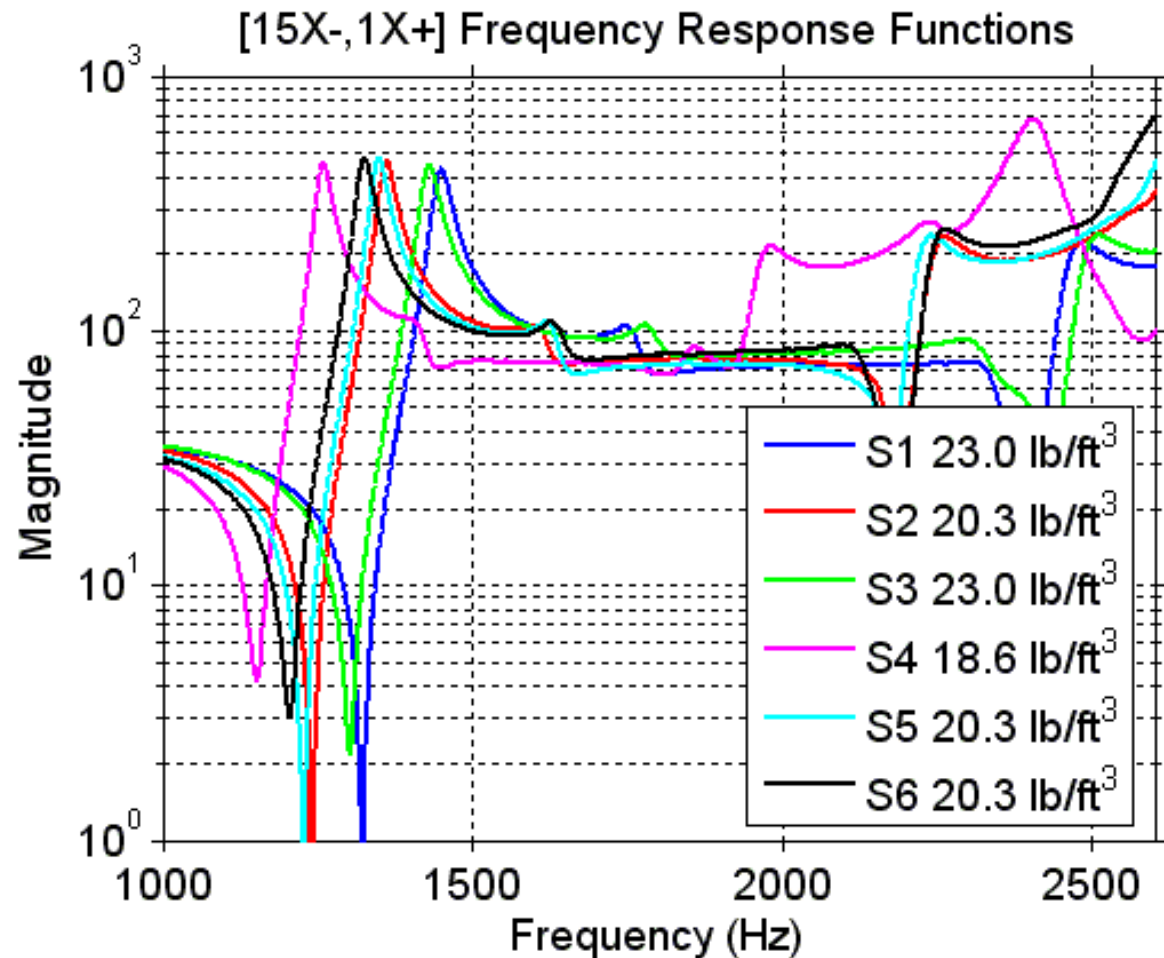
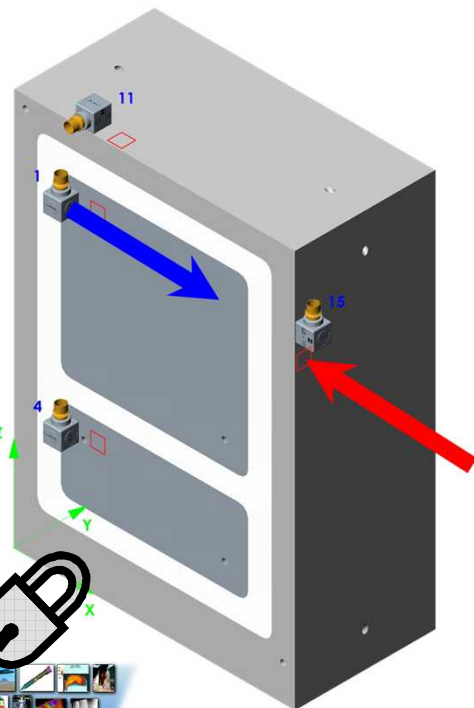
4Y+ 1Y-



Phase II Modal Validation

In-Axis

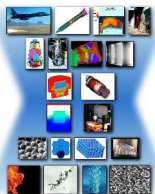
15X- 1X+



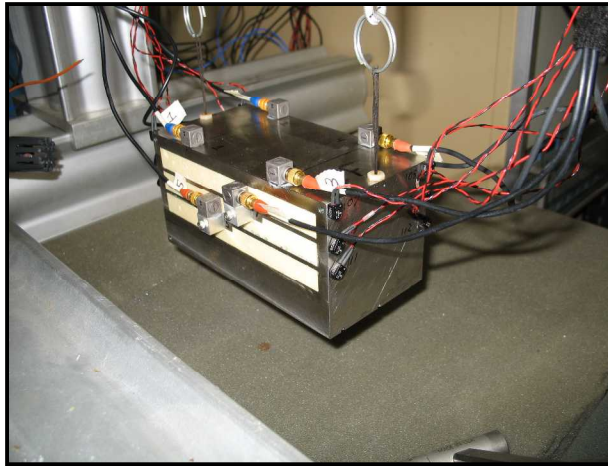
Phase II Modal Validation

Mode #	Sample 1 23.0 lb/ft ³		Sample 2 20.3 lb/ft ³		Sample 3 23.0 lb/ft ³		Sample 4 18.6 lb/ft ³		Sample 5 20.3 lb/ft ³		Sample 6 20.3 lb/ft ³	
	Freq. (Hz)	Damp. (%)	Freq. (Hz)	Damp. (%)	Freq. (Hz)	Damp. (%)	Freq. (Hz)	Damp. (%)	Freq. (Hz)	Damp. (%)	Freq. (Hz)	Damp. (%)
1	1449.0	1.1	1360.0	1.0	1429.0	1.1	1258.0	1.0	1348.0	1.0	1325.3	1.0
2	1726.7	1.1	1610.0	1.3	1718.7	1.2	1419.9	1.3	1603.8	1.2	1574.0	1.1
3	1761.0	1.3	1616.0	1.3	1787.2	1.2	1436.0	1.3	1632.0	1.2	1636.0	1.2
4	2032.0	1.4	1871.0	1.4	2007.0	1.4	1639.0	1.4	1856.0	1.4	1827.0	1.4
5	2339.3	1.3	2165.2	1.4	2324.0	1.4	1843.0	1.3	2167.2	1.3	2126.0	1.4
6	2465.0	1.3	2243.8	1.3	2489.0	1.2	1964.0	1.3	2223.8	1.3	2244.0	1.3

- Modal parameters extracted between 1000 and 2500 Hz
- Average Phase II damping is 1.2%
- Phase I calibration damping varied between 1.2% and 1.5%



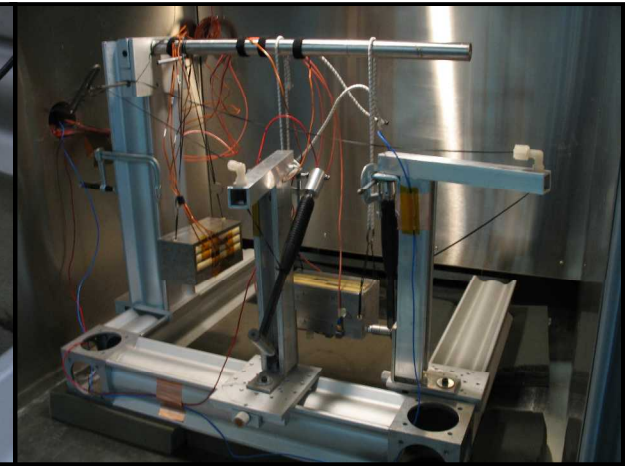
Phase III Temperature Testing



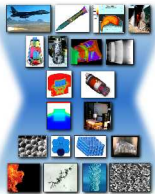
Step 1:
Ambient
Full Instrumentation



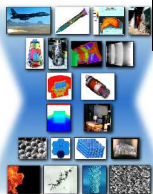
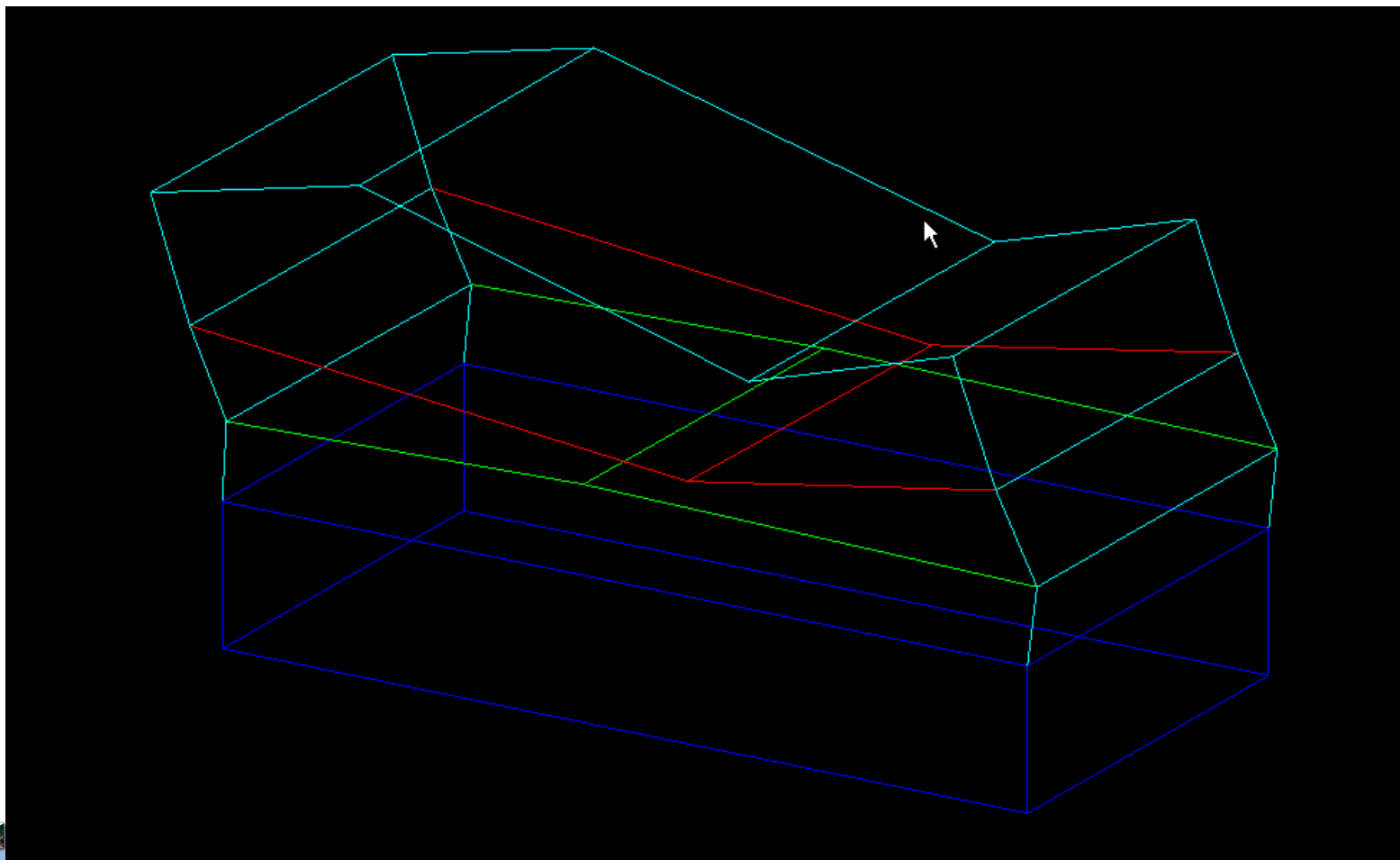
Step 2:
Ambient
Reduced Instrumentation



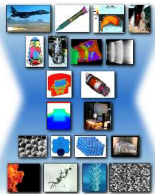
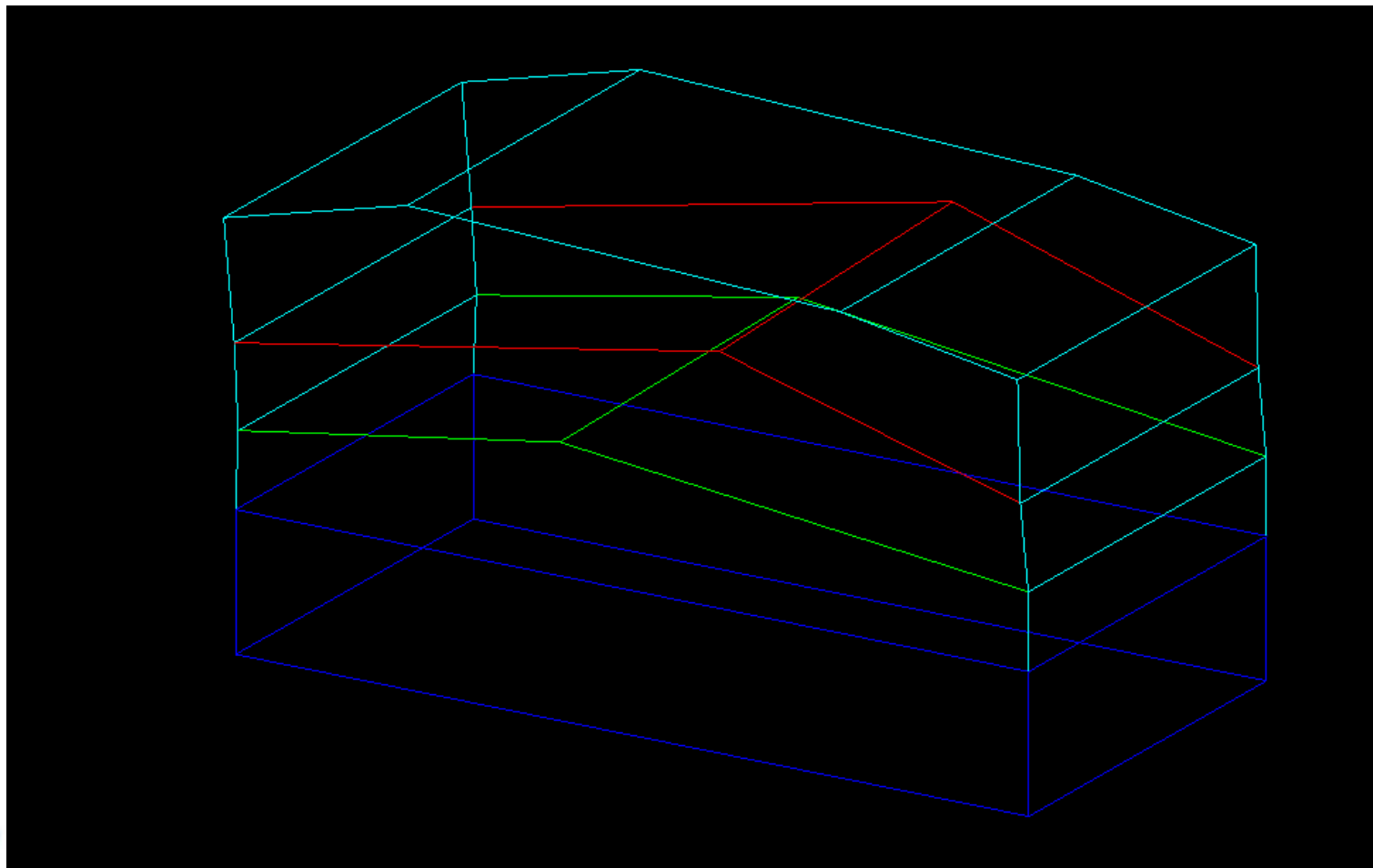
Step 3:
Temperature
Reduced Instrumentation



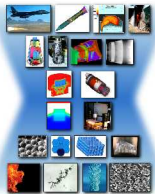
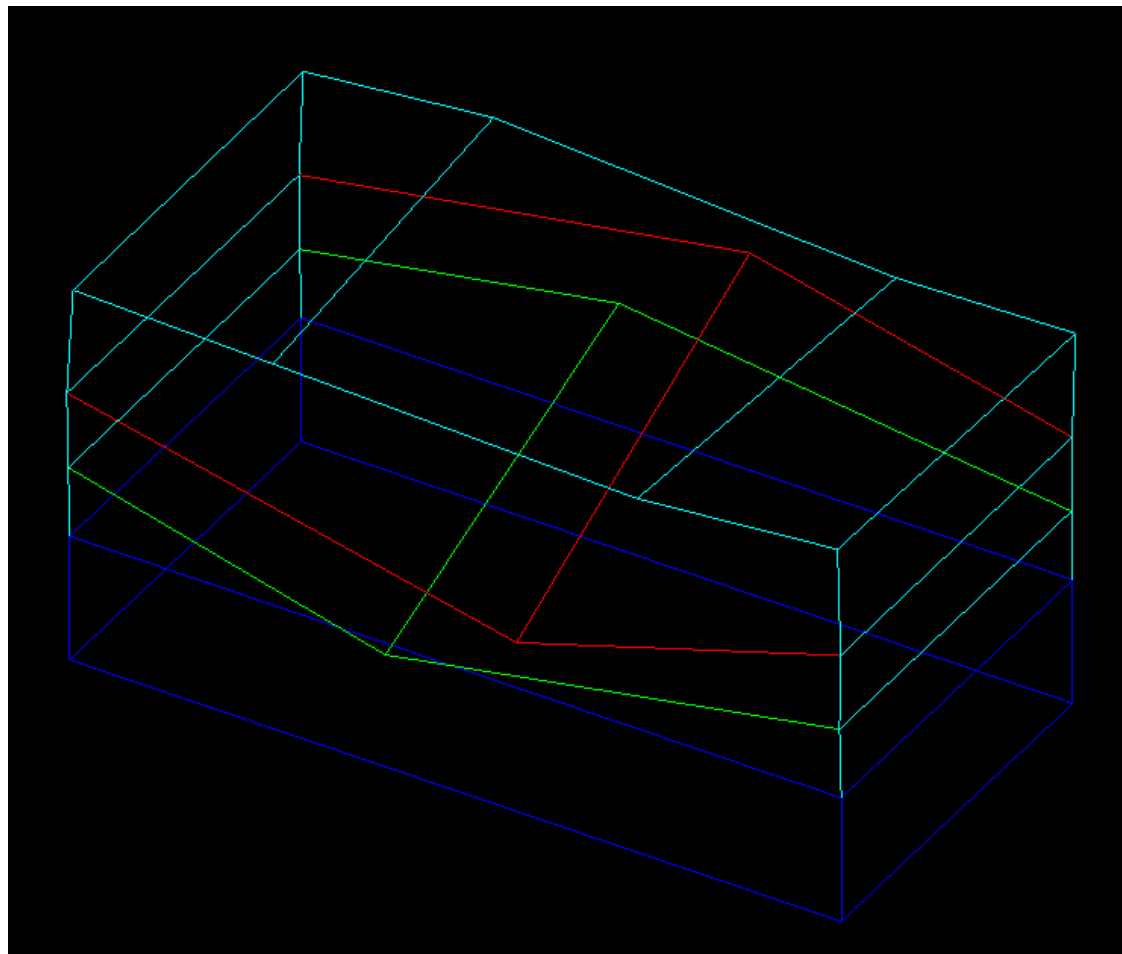
Phase III (F, 1616 Hz, 0.4%)



Phase III (F, 1764 Hz, 0.6%)

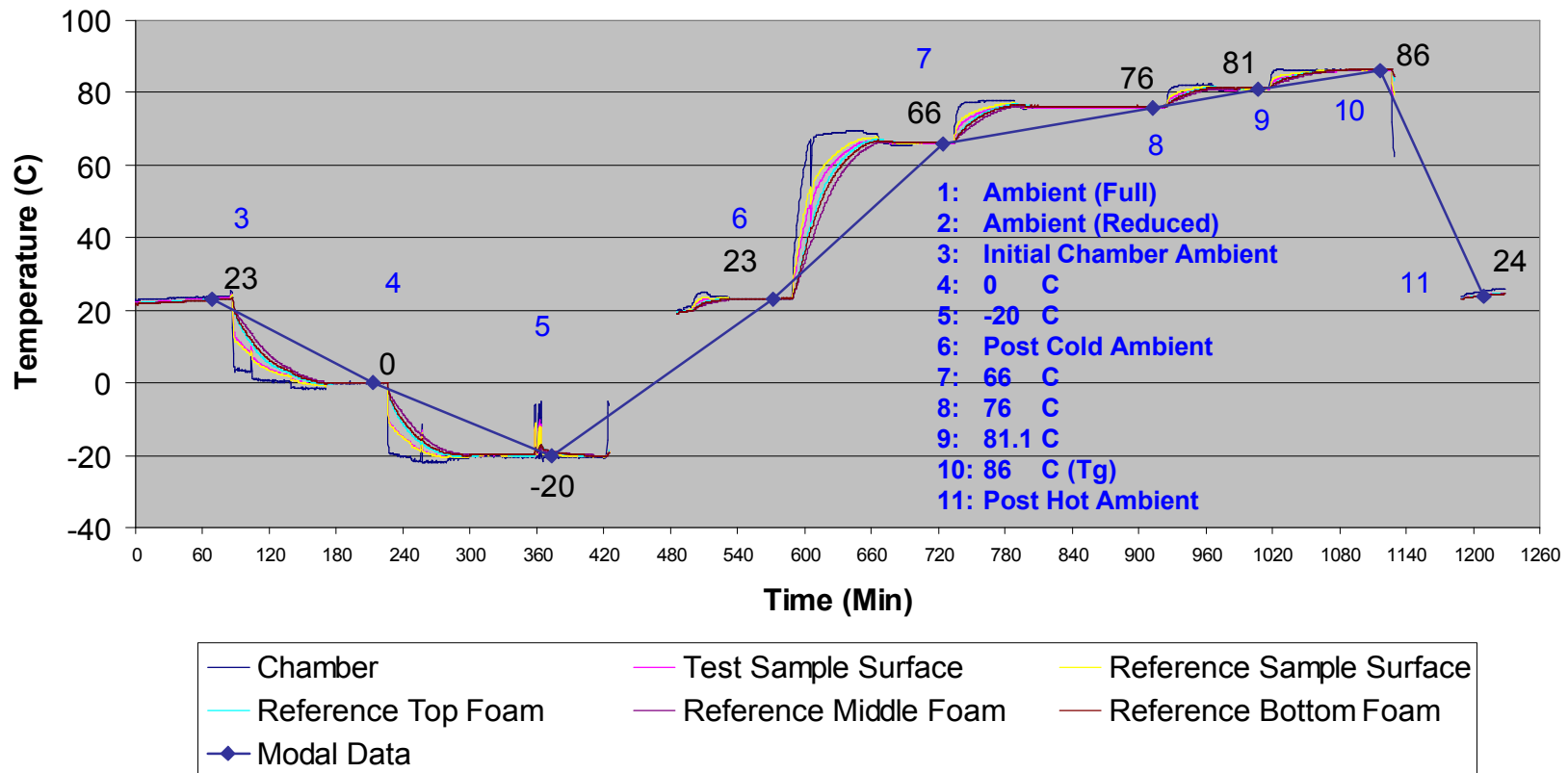


Phase III (F, 1899 Hz, 1.3%)



Phase III Test Temperatures

REF308 Phase III Sample F Temperature Profile



Preliminary Validation

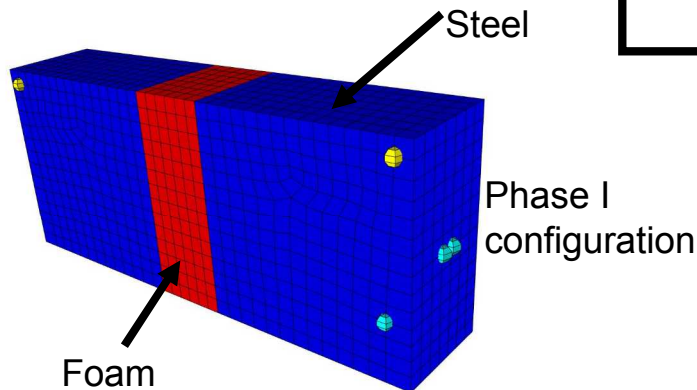
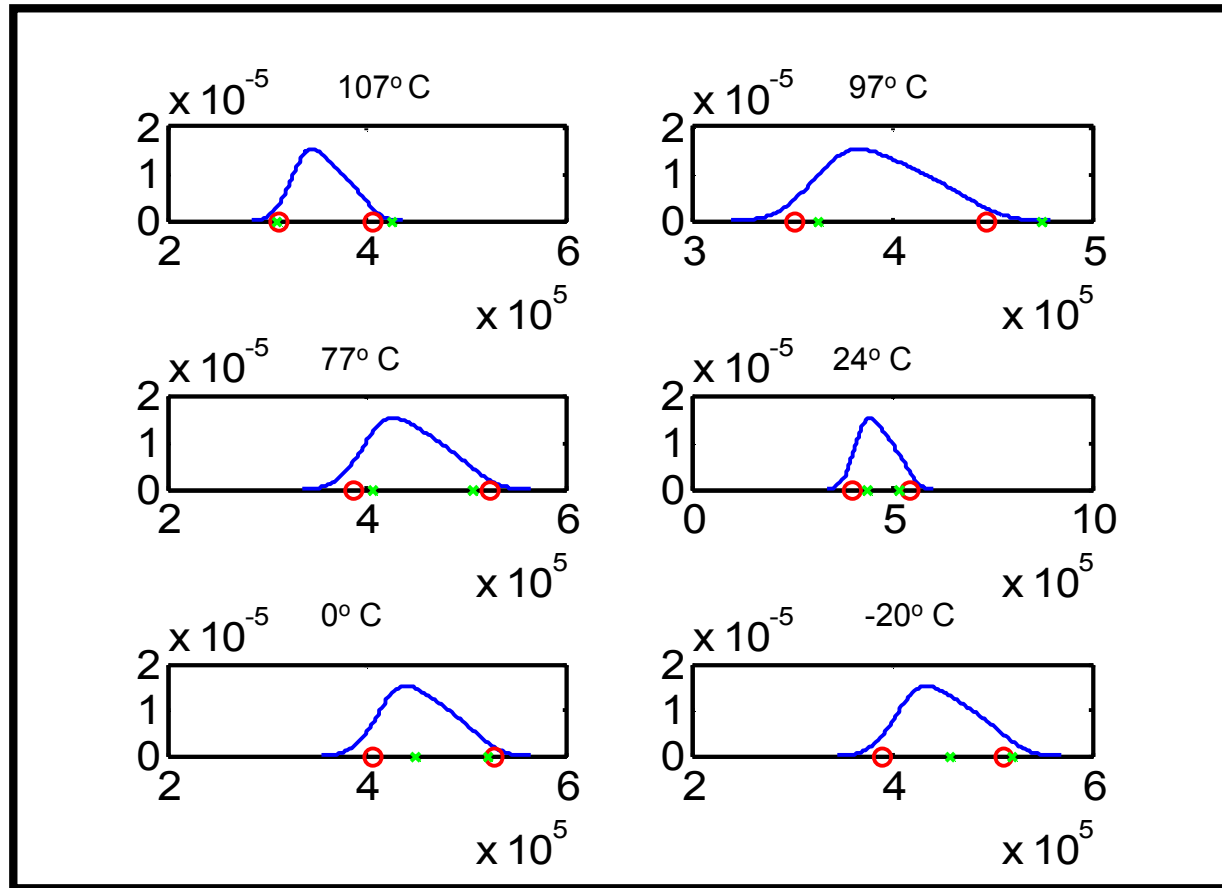
Team Members:

Terry Hinnerichs, 1524
Tom Paez, 1544
Jordan Massad, 1526
Chris O'Gorman, 1521
Patrick Hunter, 1521

Peak Acceleration Results

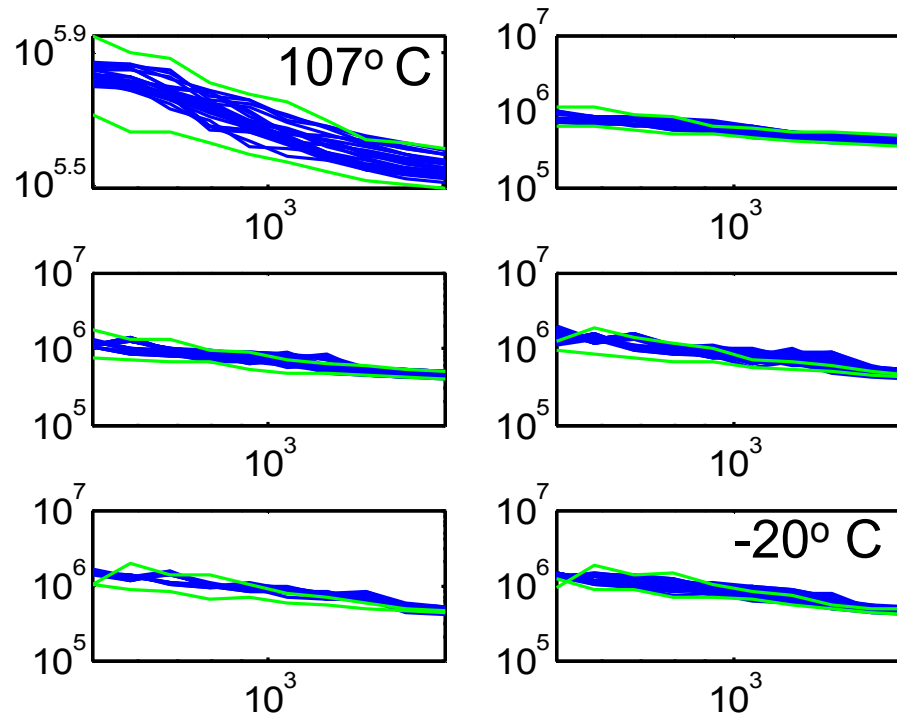
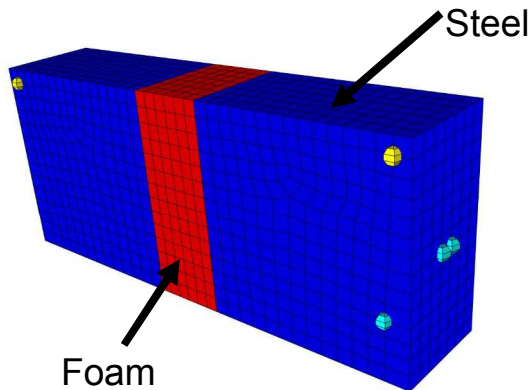
Red circles are
95% CI Test data

Green circles are
95% CI Model
predictions



Preliminary Validation

Shock Response Spectra from Model (green) and Test data (blue)



Preliminary validation results of the Viscoelastic Model using Shock Response Spectra for EF-AR20 foam over -20 to 107 deg C.

