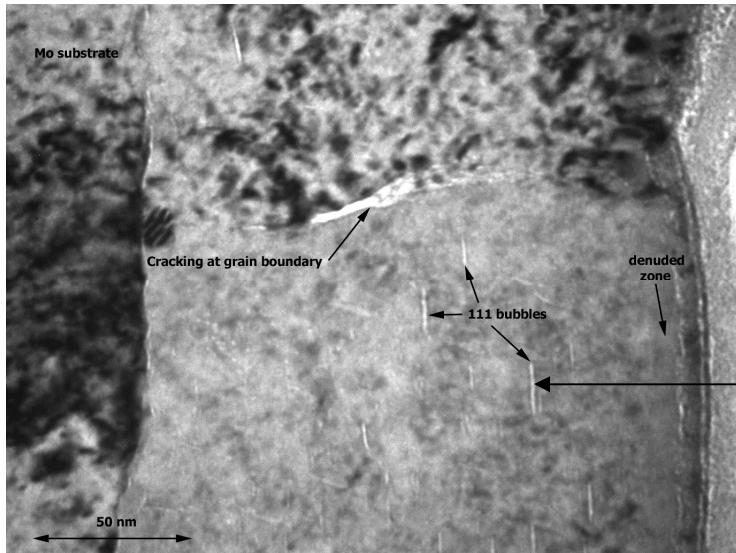


# Physics of He Platelets in Metal Tritides

SAND2007-4057C

Don Cowgill, SNL, Livermore CA USA

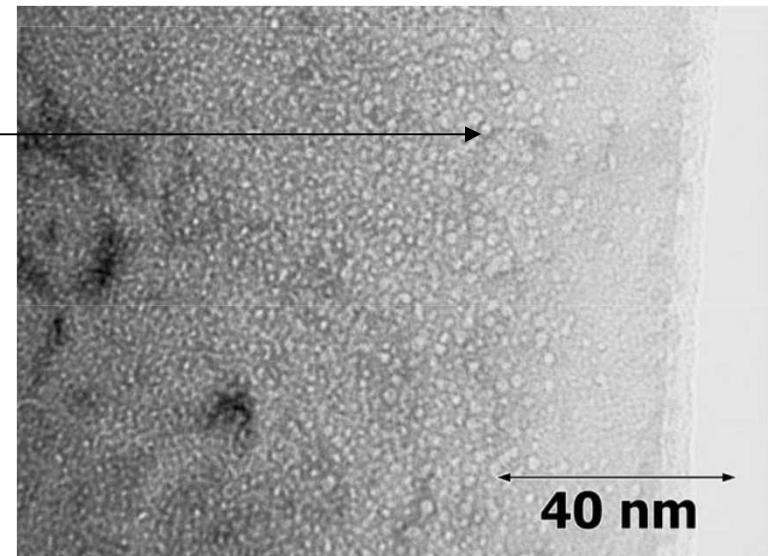
IHISM Workshop, St. Petersburg, Russia, 2-6 July 2007



*What causes the bubble shape difference?*

Pd tritide

Er tritide



## Outline

- Platelet stability and growth
- Pd vs Er system
- Model testing with XRD data
- Percolation of Interbubble Fracture
- Other materials & future efforts

TEM images by Brewer, Gelles, & Kotula

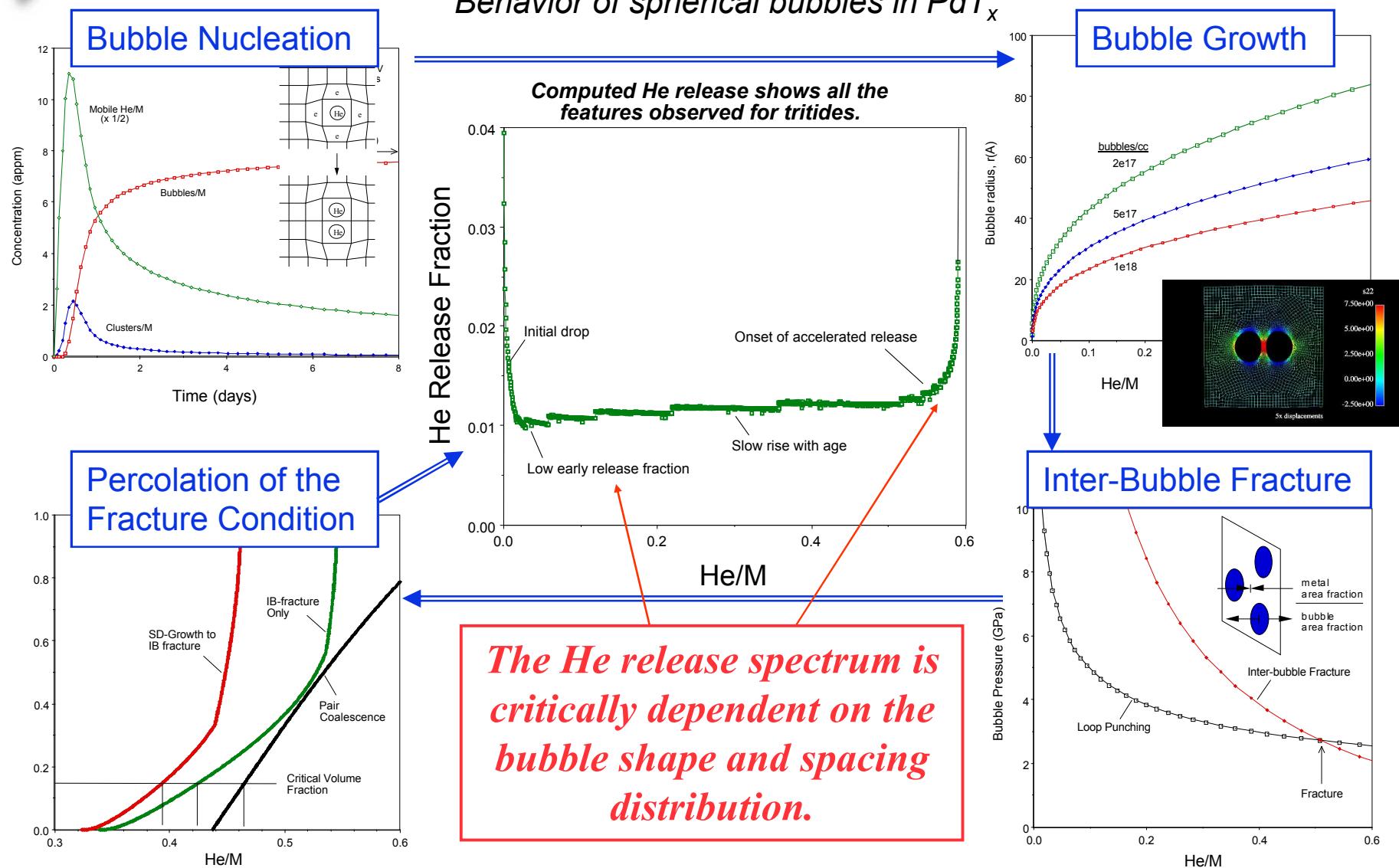
*“In the spirit of a workshop,  
this is work in progress.”*



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# The evolution of He bubbles/platelets is captured in a continuum-scale model.



# Bubble nucleation by self-trapping occurs during a short pulse in mobile He concentration.

- Model using 3 components: mobile He, He-pairs, “bubbles”:

$$\begin{aligned} dc_1/dt = & g - 2ps_1c_1^2 - ps_2c_1c_2 \\ & + 2q_2c_2 - ps_B(r)c_1c_B \end{aligned}$$

$$dc_2/dt = ps_1c_1^2 - q_2c_2 - ps_2c_1c_2$$

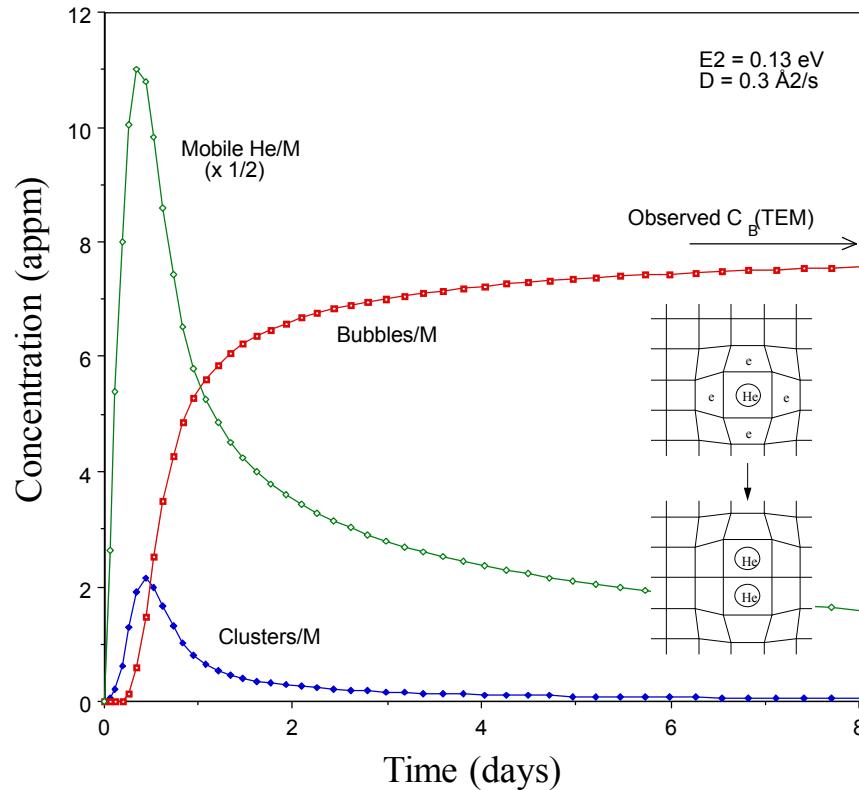
$$dc_B/dt = ps_2c_1c_2$$

generation rate,  $g = \lambda(^3\text{H}/\text{M})$

jump rate,  $p = 12D_{\text{He}}/a^2$

pair dissoc. rate,  $q_2 = 2pe^{-E_2/kT}$

- The mobile concentration drops as bubbles produce traps.



*Using theoretical  $E_2$  and experimental  $D_{\text{He}}$  gives correct  $c_B$ .*

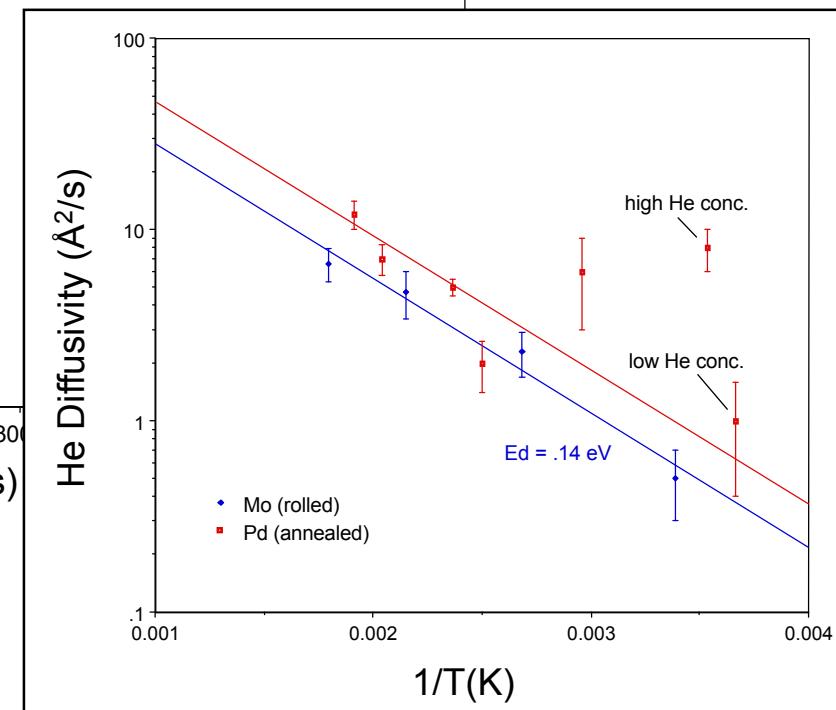
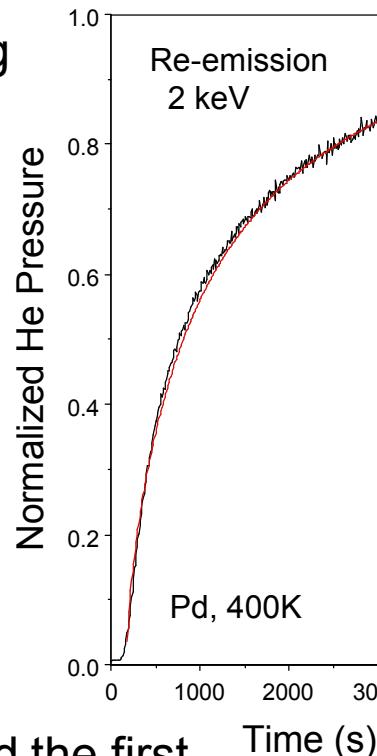
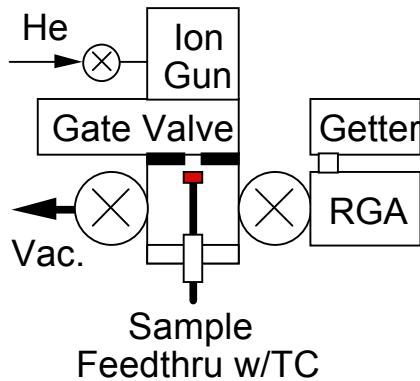
- Bubble nucleation is 90% complete in a 2 days.



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# Nucleation parameters are being measured by our He Implant/Re-emission technique.

- He re-emission following a short implant pulse is fitted to the self-trapping model.



- This technique produced the first measurements of He diffusion in metals near room temperature.
- Self-trapping energies can be determined by varying the implant pulse characteristics.

# Each bubble's growth is determined by its He supply rate -- its tritium source volume.

- Bubble growth relations:

- Mass conservation:  $(r/R)^3 f_p = (v_{He}/v_{MH})(He/M)$   
( $v$ =molar volume,  $f_p = .64$  for random array packing)

- Dislocation loop-punching:  $p = 2\gamma/r + \mu b/r(1+\varepsilon)$   
( $\gamma$ =surface energy,  $\mu$ =shear modulus,  $b$ =Burgers vector)

- Bulk He EOS:  $v_{He}(p, T)$

- For a given bubble spacing  $R$ : At each  $He/M$  there is a unique  $r, p, v_{He}$ :

*Modeled bubble pressures agree with  $p_{Av}$  deduced by NMR.*

Bubble Radius (Å)

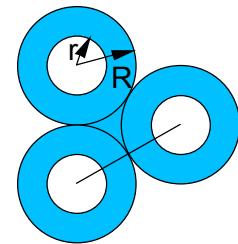
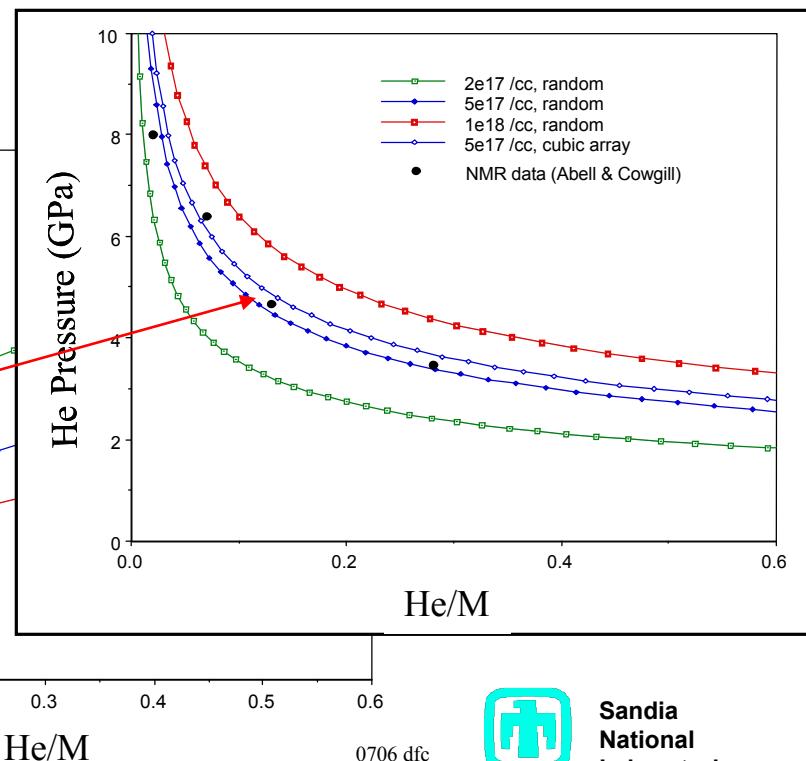
He/M

bubbles/cc

2e17

5e17

1e18



Array of Spherical Source Volumes

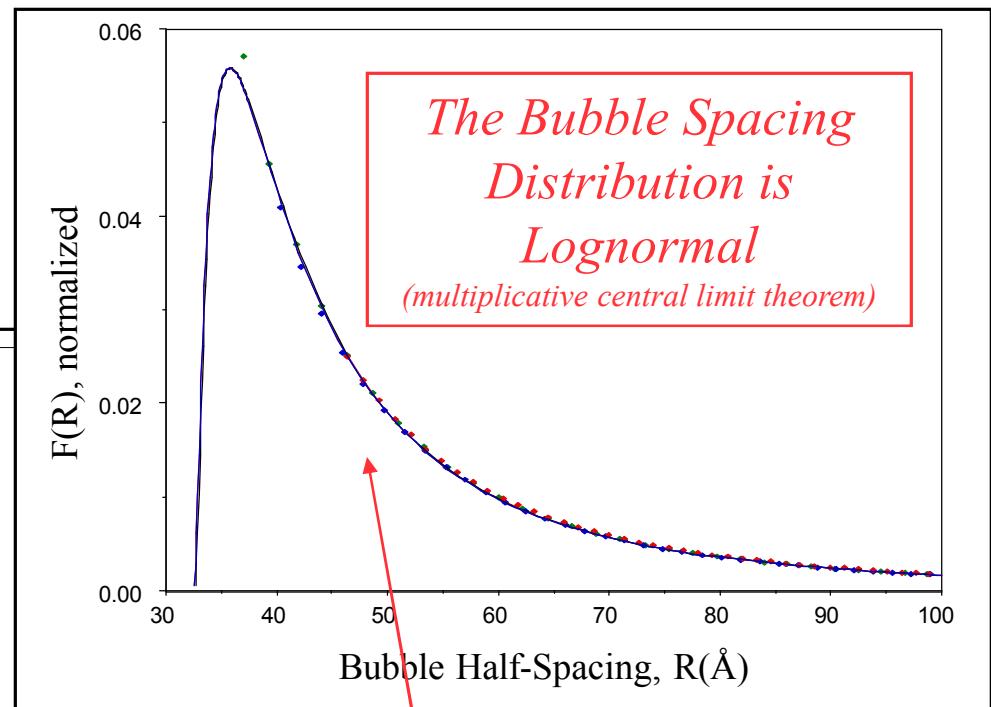
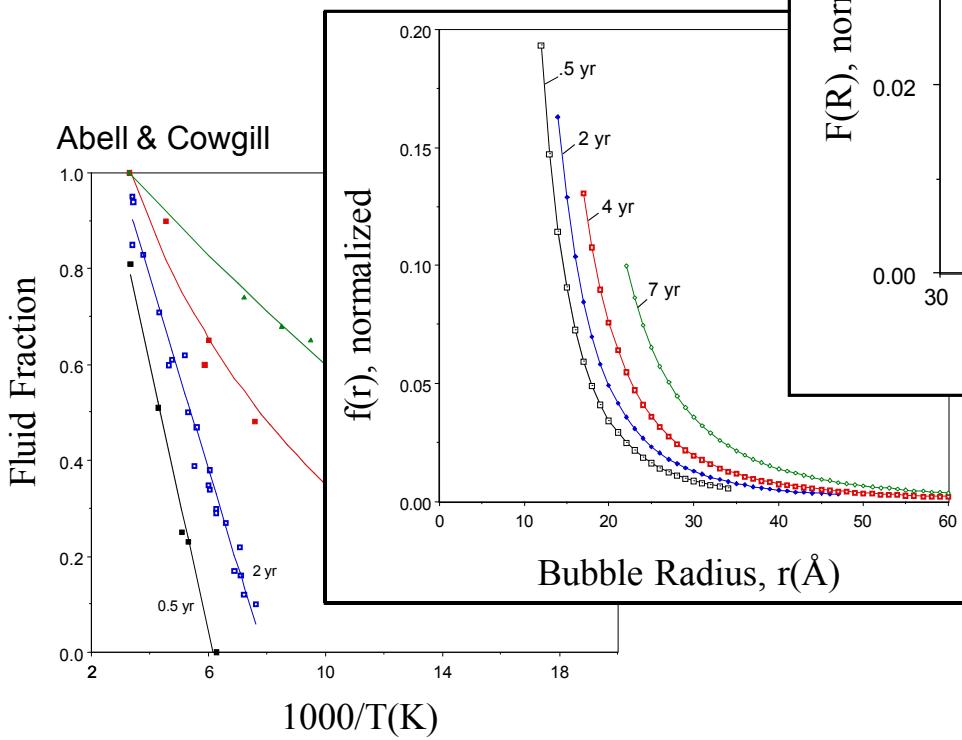


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# The bubble spacing distribution in $\text{PdT}_x$ has been determined by $^3\text{He}$ NMR.

- $^3\text{He}$   $T_1$  (motion) separates sol-He from liq-He in bubbles.
- Growth relations convert fluid fractions to bubble distributions.



*The constant spacing distribution*

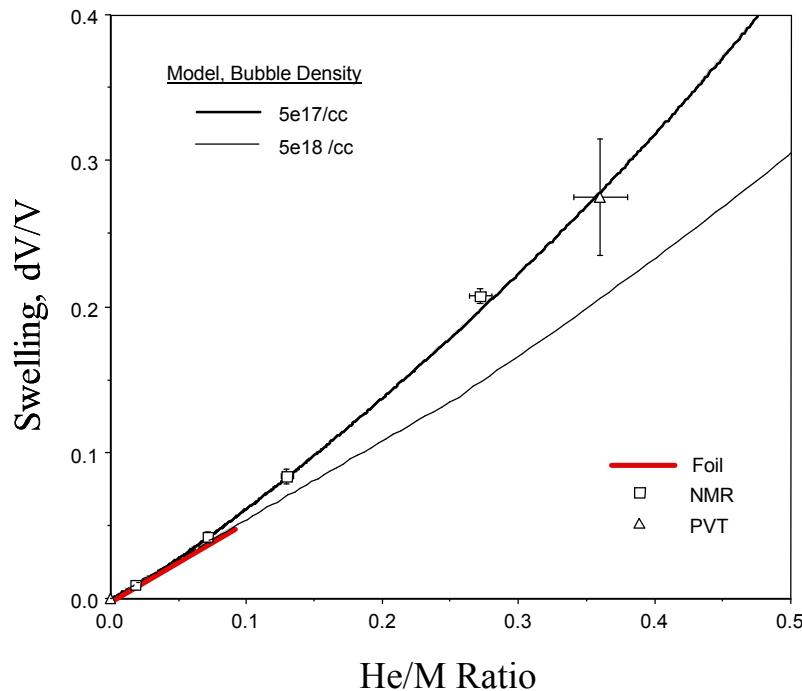
- verifies nucleation has stopped
- provides a sensitive test of the nucleation and growth models.



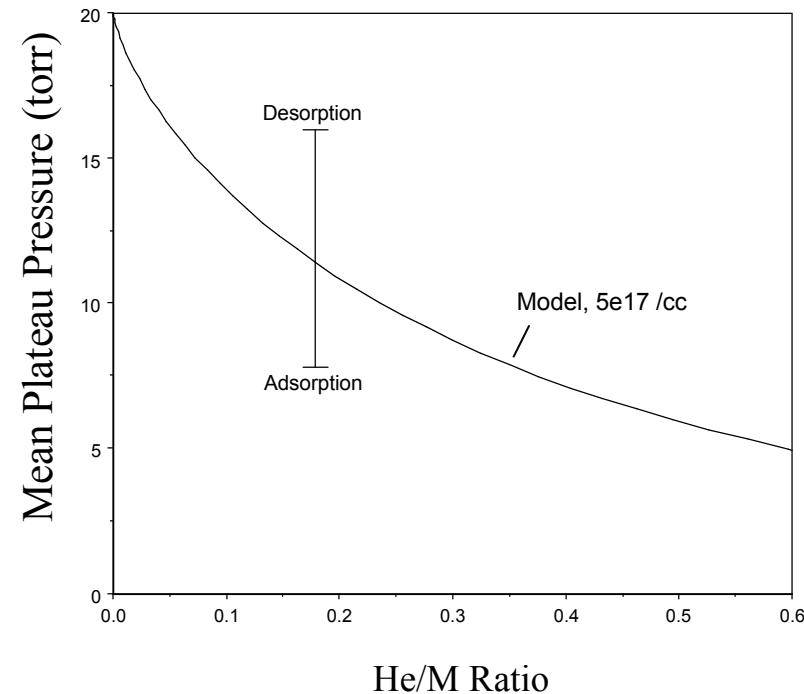
# The bubbles cause swelling and lattice stress, which produces a shift in the hydride PCT.

Volume occupied by He bubbles:

$$dV/V = (v_{He}/v_{MH})(He/M)$$



Plateau  $p_H = p_o \exp(-2\sigma_{hy} v_H / R_g T)$ ,  
hydrostatic stress,  $\sigma_{hy} = p_{He}(dV/V)$



*Swelling and PCT behavior are consistent with the lower bubble density found by TEM (Thomas et al., 1983), not higher (Thiebaut et al., 2000).*

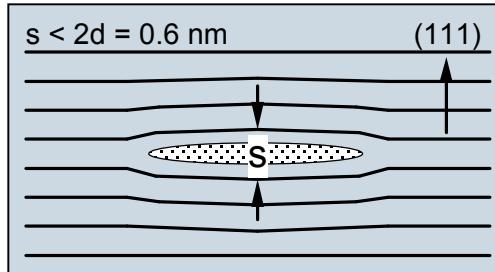


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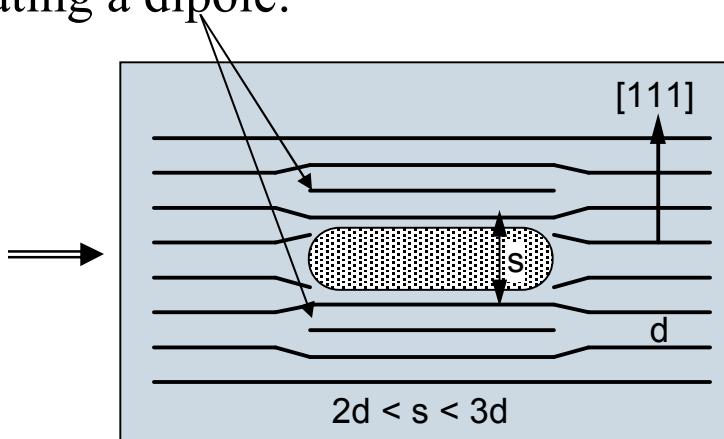
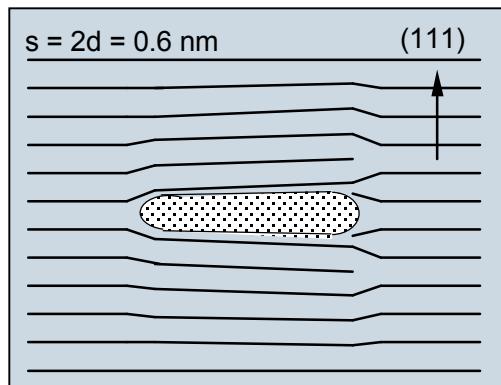
# The bubbles in fcc materials likely evolve from nano-cracks.

- He atoms accumulate in “relatively open” spaces between (111) planes, where they open Griffith-like nano-cracks:



HR-TEM of n-crack in PdT by Thiebaut

- When the crack opens to  $s=2d$ , dislocation loops begin to form, creating a dipole:



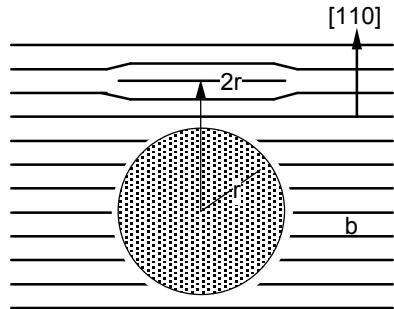
[110] view



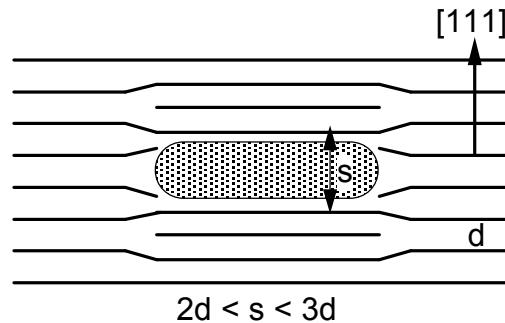
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# The He pressure within the precipitate has components due to surface and strain energies.

Spherical bubbles grow by  
“dislocation loop punching”



Platelets can grow by  
“dislocation dipole expansion”



Surface Energy:  $p_e dV = \gamma dA$

$$p_e \pi r^2 b = \gamma 2\pi r b$$

$$p_e = 2\gamma/r$$

$$p_e \pi [(r+b)^2 - r^2] s = \gamma 2\pi [(r+b)^2 - r^2 + (r+b)s - rs]$$

$$p_e = (2\gamma/s) [(2r+b+s)/(2r+b)]$$

Lattice Strain: stress =  $\mu$  strain

$$p_s \pi r^2 = \mu [(b/2)/d] 2\pi r d$$

$$p_s = \mu b/r$$

$$p_s \pi [(r+b)^2 - r^2] = \mu [(d/2)/b] 2\pi [(r+b)-r] b$$

$$p_s = \mu d/(2r+b)$$

Bubble Pressure:  $p = p_e + p_s$

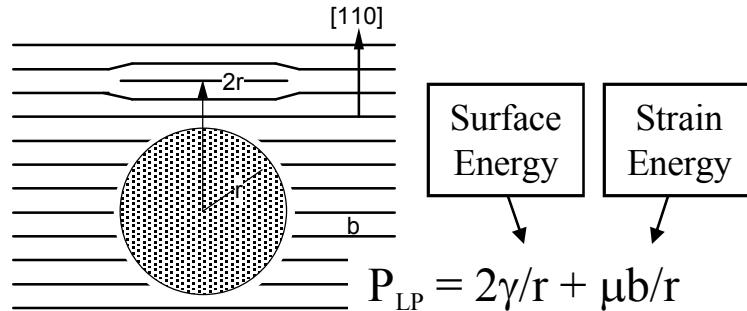
$$p_{lp} = 2\gamma/r + \mu b/r$$

$$p_{de} = (2\gamma/s) [(2r+b+s)/(2r+b)] + \mu d/(2r+b)$$

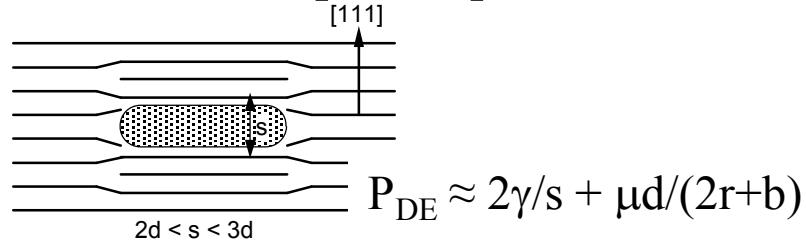
$$p_{de} = 2\gamma/s + \mu d/2r, \text{ at large } r$$

# The bubble shape and growth process depend on the tritide's mechanical properties.

- Dislocation loop punching



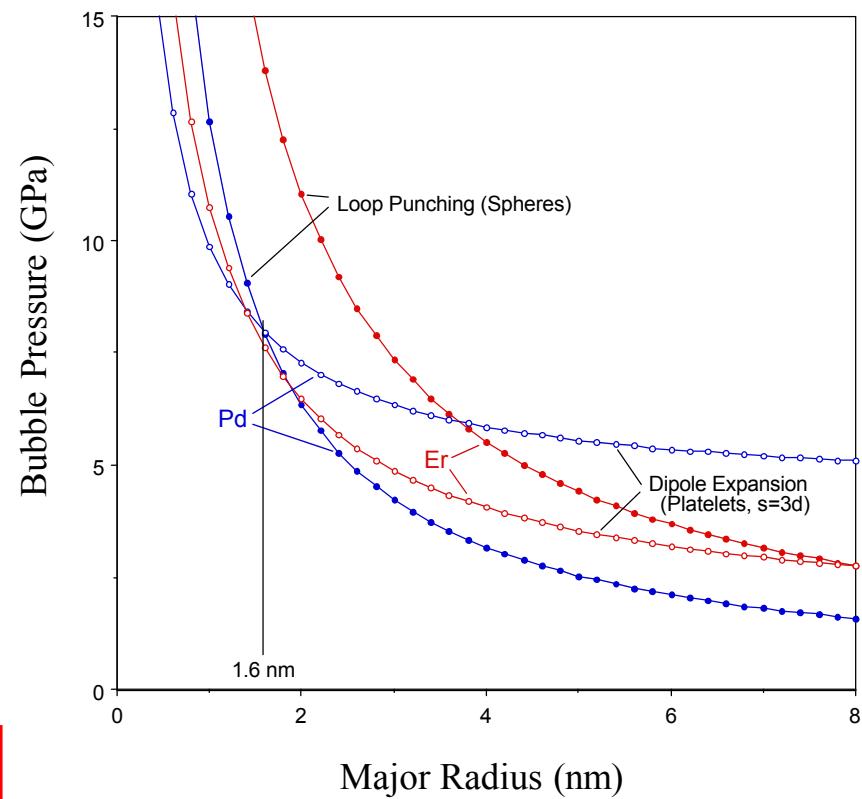
- Dislocation dipole expansion



- Thin, disk-shaped bubbles are caused by a low surface energy (low  $\gamma/\mu b$ ).

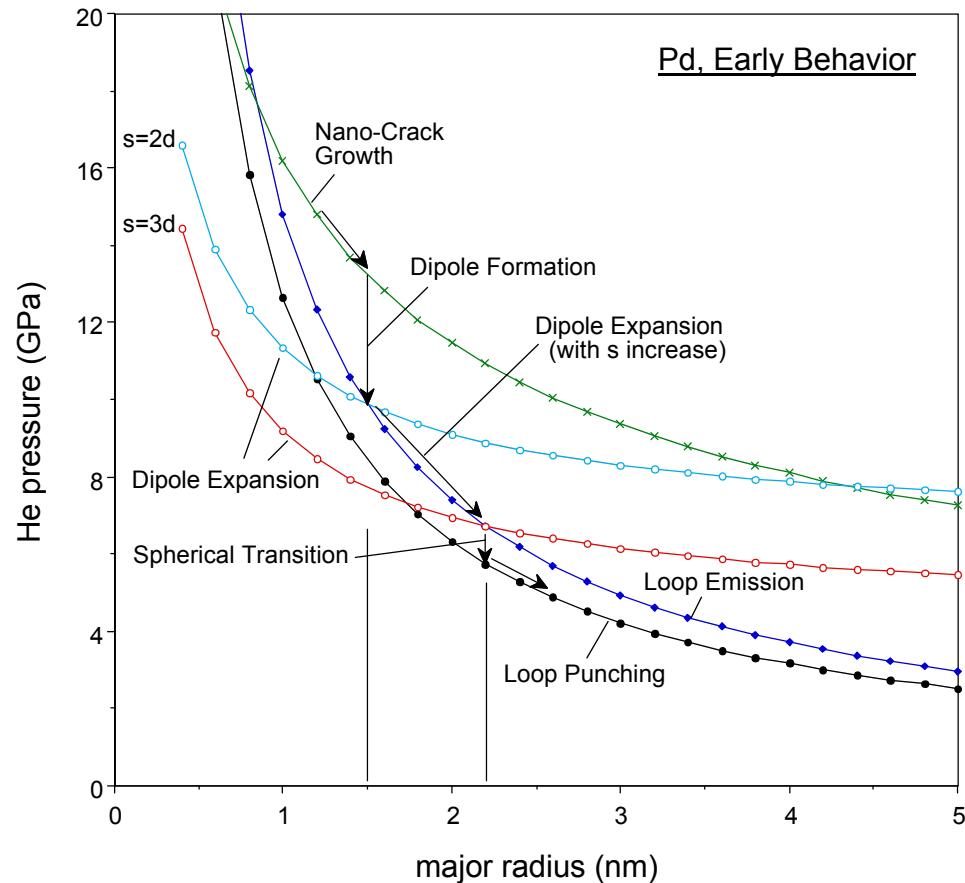
Note: Platelets are also the preferred shape in young Pd tritide (<50 days).

Tritide	$\gamma(\text{GPa}\cdot\text{nm})$	$\mu(\text{GPa})$	$b(\text{nm})$	$\gamma/\mu b$
Pd	1.54	33.6	.2852	0.16
Er	0.637	57.4	.3623	0.03



# The early growth of bubbles in PdT appears to have several stages.

1. He atoms collect in (111) planes and open nano-cracks (Griffith):  
 $P_{nC} = 4\gamma/s$ ,  $s = 4[\gamma(1-\nu)r/\pi\mu]^{1/2}$ .
2. Dislocation dipoles form when the nano-crack gap reaches  $s=2d$ .
3. Platelet pressures drop as their thicknesses increase to  $s\approx2.5d$ .
4. The platelets expand radially until  $s=3d$ , where the dipole escapes.
5. [110] loops are emitted as the platelets transition to spheres.
6. Spherical bubbles continue to grow by normal loop-punching.



# Testing of pressure formulation is provided by lattice dilation data on aged tritides.

---

- Tensile stress created by the precipitates produces a positive  $da/a$ .

- Spherical bubbles at Loop Punching pressure:

Hydrostatic tensile stress balances bubble pressure

$$p_{LP}(\Delta V/V) = B^*(3 da/a)_{LP}, \quad B^* = \text{bulk modulus of aged material}$$

where  $\Delta V/V = (4/3) \pi r^3 n_B$ ,  $n_B = \text{bubbles/cm}^3$

$$(da/a)_{LP} = [1/3 B^*] p_{LP}(\Delta V/V)$$

- Platelets at Dipole Expansion pressure:

[111] tensile stress balances platelet pressure, 4 components

Projection along [100] cubic axes =  $1/3^{1/2}$

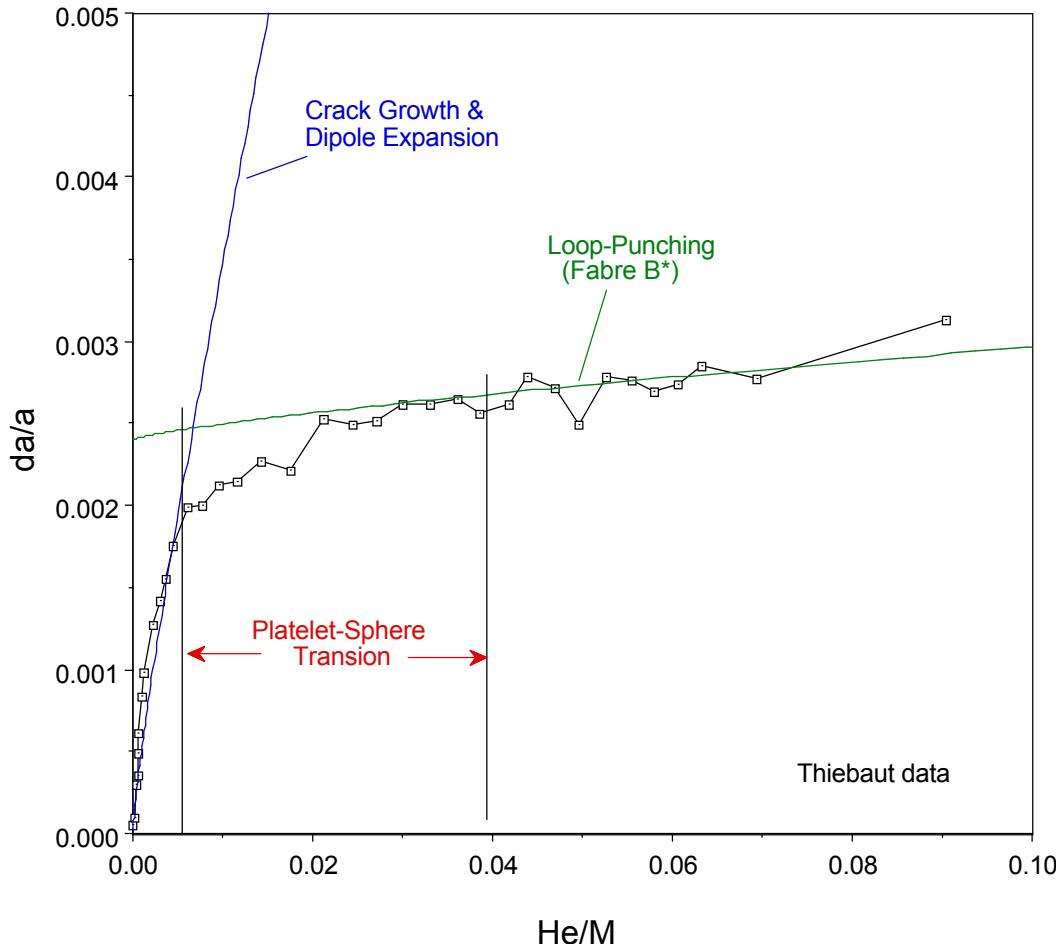
$$p_{DE}(\Delta A/A) 4/3^{1/2} = E^*(da/a)_{DE}, \quad E^* = \text{Young's modulus of aged material}$$

where  $\Delta A/A = \pi r^2 (n_B/4)^{2/3}$ ,  $n_B = \text{bubbles/cm}^3$

$$(da/a)_{DE} = [4/3^{1/2} E^*] p_{DE}(\Delta A/A)$$



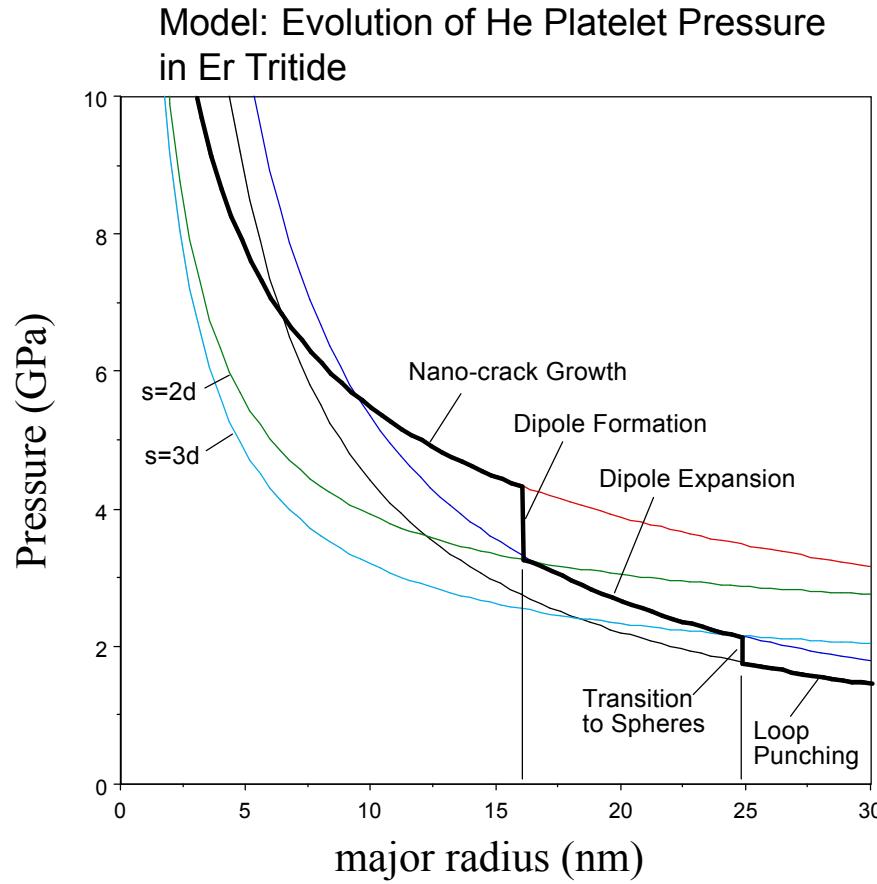
# Lattice dilation “details” of PdT appear to support the existence of multiple stages.



- Initial Griffith crack growth at high pressure will produce an even rise.
- The bubble volume increases by 8X during the transition from platelets to spheres.
- Emitted dislocations must remain trapped between “bubbles”.
  - Bubble source volumes remain constant!)



# The He precipitates in Er tritide remain 2-dimensional platelets throughout life.

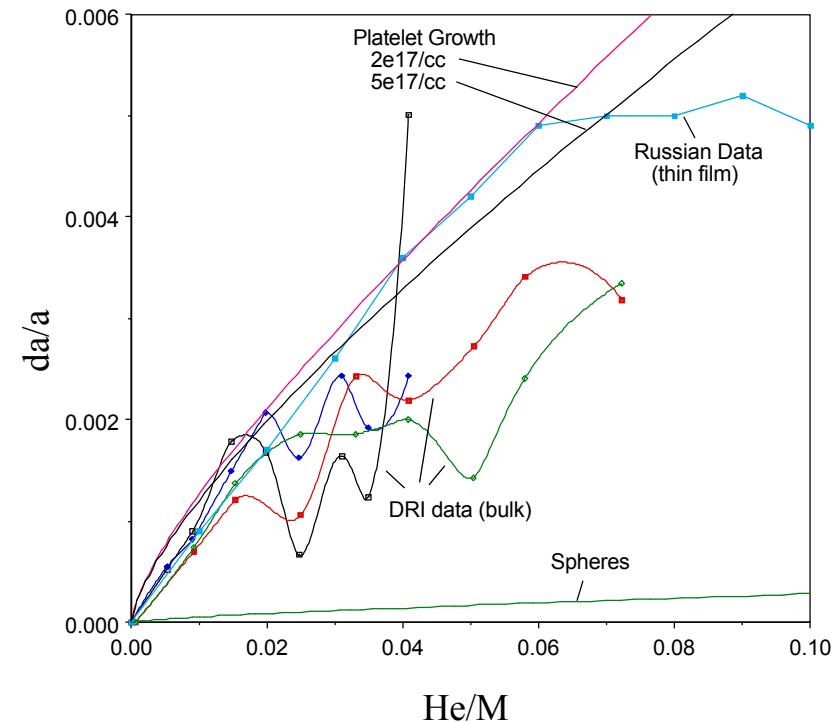
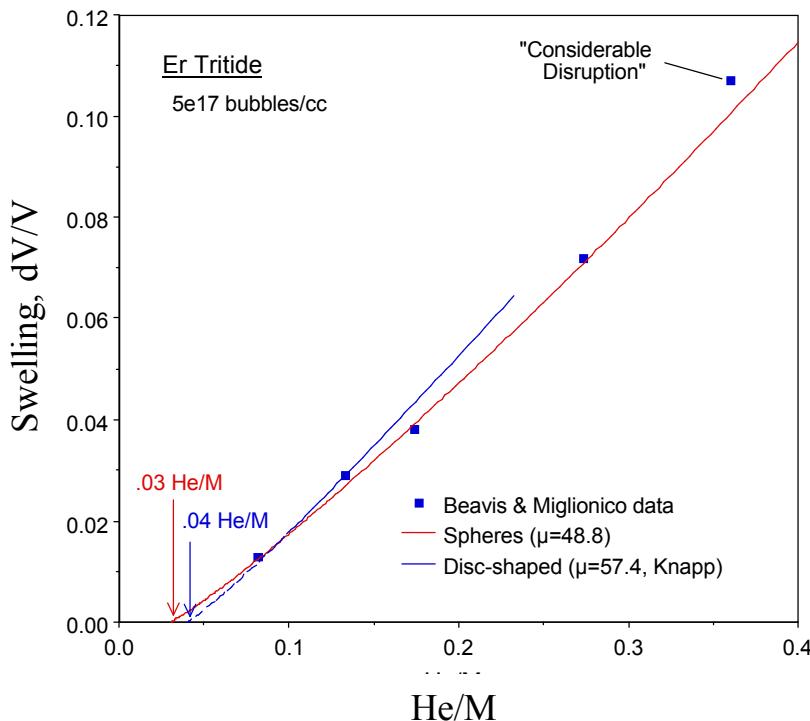


- He pressure decreases as the nano-crack opens.
  - He becomes liquid at  $\sim 12$  GPa.
- When the crack width reaches  $2d$ , a dislocation dipole begins to form, causing a drop in pressure.
- The pressure decreases further as the completed dipole expands and its width increases to  $3d$ .
- Linking of the platelets will occur prior to their spherical transition.
  - At  $r \approx 25$  nm, the co-planar platelet area  $>1$  (area projections overlap).



# Lattice dilation is significantly greater for platelets.

- Swelling data can be fitted by either growth mechanism; but the *initial incubation period is not consistent with loop punching*.



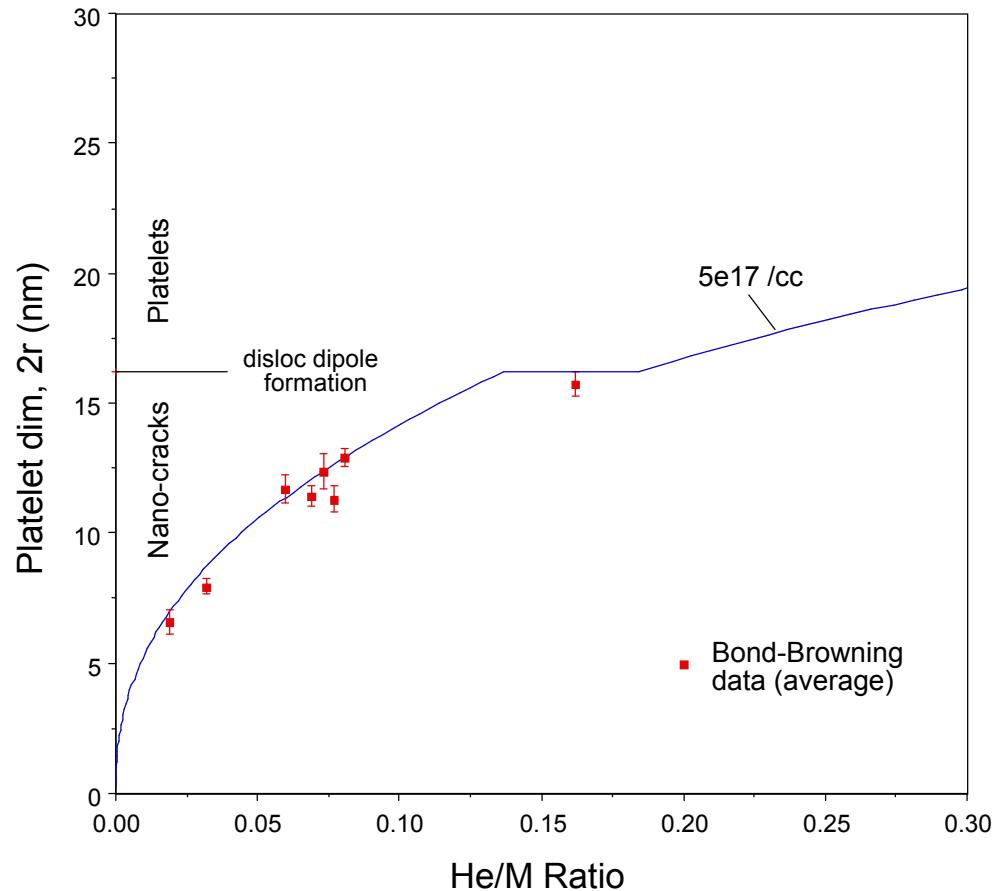
- Platelets produce greater lattice strain and can account for the rapidly increasing lattice parameter.



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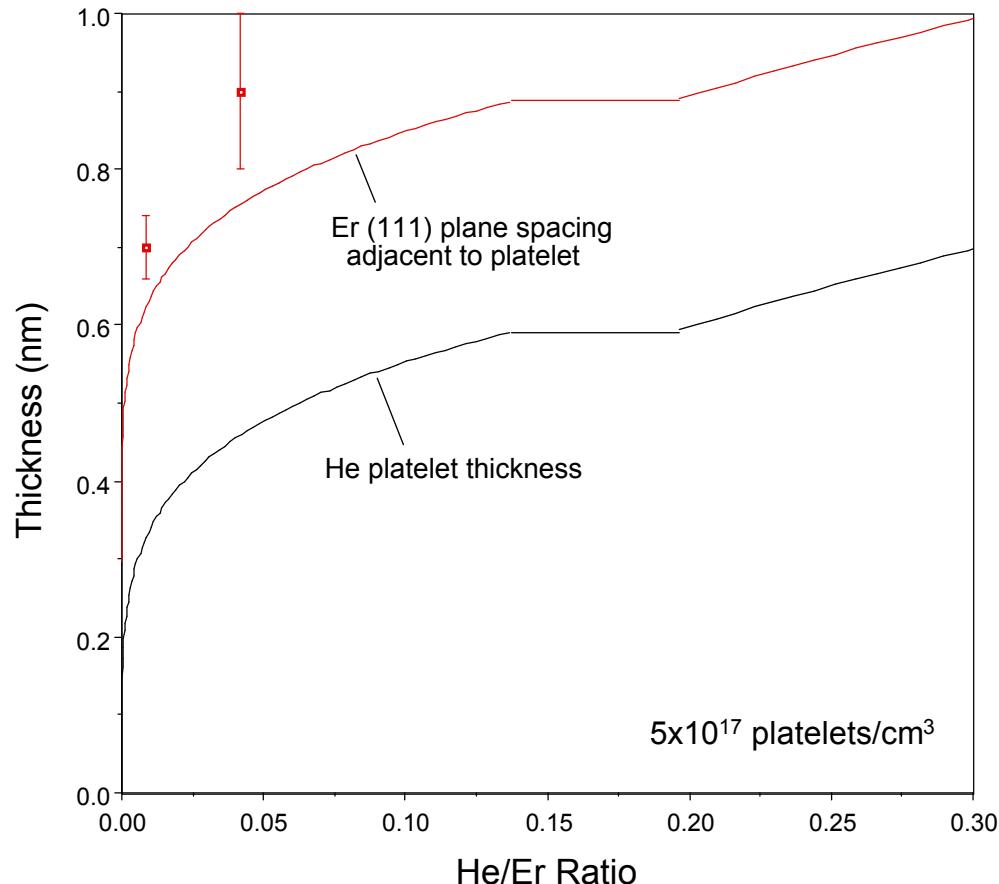
# Model accounts for the platelet growth observed by Bond & Browning.



- Model calculation for an average platelet density of  $5 \times 10^{17}$  platelets/cm<sup>3</sup>.
  - Pd tritide bubble density!
- Here, platelet interactions are assumed negligible.
  - We must revisit this!
- For Er tritide, rapid He release occurs around 0.3 He/Er, when the average platelet is 20 nm.



# The platelet thickness is nearly constant, but is should increase slowly with age.



- Predicted thickness appears slightly less than the TEM determination?  
Need more data.  
X-ray diffraction?
- Accurate measurement of the platelet thickness and density can provide a determination of the surface energy:

$$\gamma = \frac{\pi \mu s^2}{4(1-v)r}$$



# The bubble shape condition appears to hold for precipitates in fcc, hex, and bcc materials.

Material	$\gamma$ (GPa-nm)	$\mu$ (GPa)	b(nm)	$2\gamma/\mu b$	shape
ErT	0.637	57.4	.3623 fcc	.061	platelets
ScT	0.954	54.0	.3382 fcc	.104	early platelets, then?
TiT	1.39	76.2	.3111 fcc	.117	platelets & elongated?
Ni	1.72	76.5	.2490 fcc	.180	spheres?
ZrT	1.48	32.6	.3522 fcc	.258	spheres
PdT	1.54	33.6	.2852 fcc	.322	spheres
Be	1.10	146	.359 hex	.051	platelets
Ti- $\alpha$	1.39	40.1	.291 hex	.238	platelets
W	2.22	158	.273 bcc	.103	platelets
V- $\alpha$	1.95	47.4	.263 bcc	.312	spheres
Nb- $\alpha$	1.90	38.2	.285 bcc	.350	spheres

- Surface energy/strain energy ratio for spherical bubbles
- Platelets are preferred for small  $r$ , where  $s/2r > 2\gamma/\mu b$ .



# Work on platelet structures is continuing.

---

- Thin (111) platelet bubbles can be associated with nano-cracks or dislocation dipole structures.
- Additional theoretical work is examining
  - formulations of platelet characteristics
  - linking of platelets by inter-platelet fracture
- Continued testing should examine
  - the bubble pressure and spacing distribution in young Pd tritide (in spherical transition stage).
  - bubble shapes in other materials (e.g. SiC).
  - bubble shapes in implanted materials.
- TEM and XRD studies in selected materials are needed to characterize bubble shapes and transition points.

# For spherical bubbles, Rapid He Release is modeled using a ligament fracture criterion.

- As the bubbles grow, tension on the inter-bubble ligament increases.
- Evans' fracture criterion:

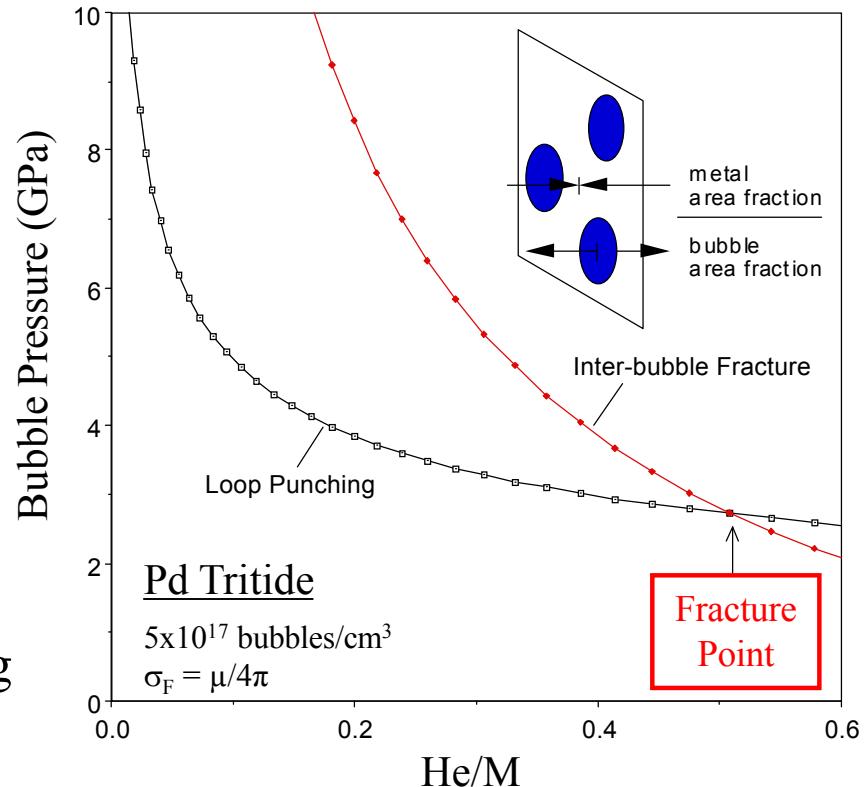
For plane through adjacent bubbles, fracture occurs when:

$$p_{LP} \text{ (bubble area)} > \sigma_F \text{ (metal area)}$$

$$(\sigma_F = \text{fracture strength} \approx \mu/4\pi)$$

- Valid when neighboring ligaments fracture simultaneously (surrounding lattice provides no support).

*Rapid release should occur when bubbles at mean bubble density undergo inter-bubble fracture.*



- Both curves are modified by local stresses due to bubble interactions.

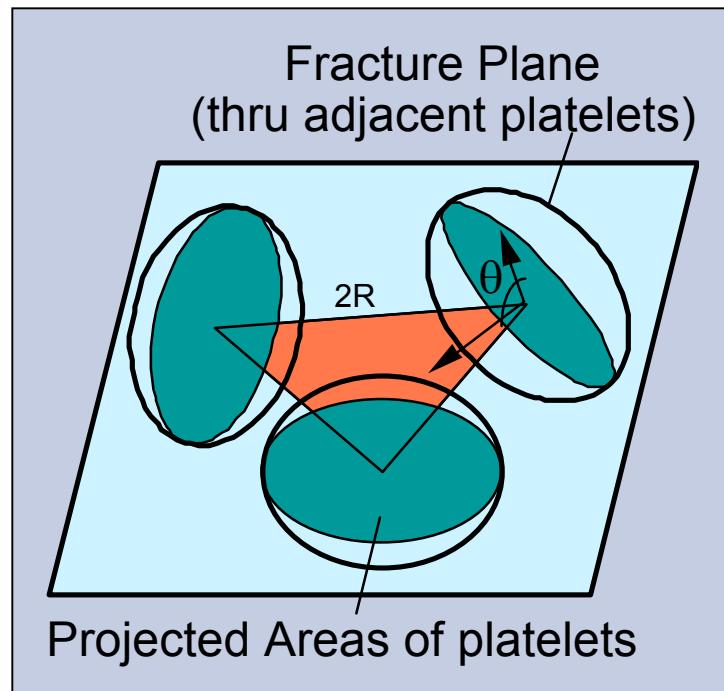


# Inter-platelet fracture can be modeled using platelet area projections in the fracture plane.

- Equating stresses on the ligament between 3 adjacent platelets:

$$p_S \text{ (projected platelet area)} = \sigma_F \text{ (projected metal area)}$$

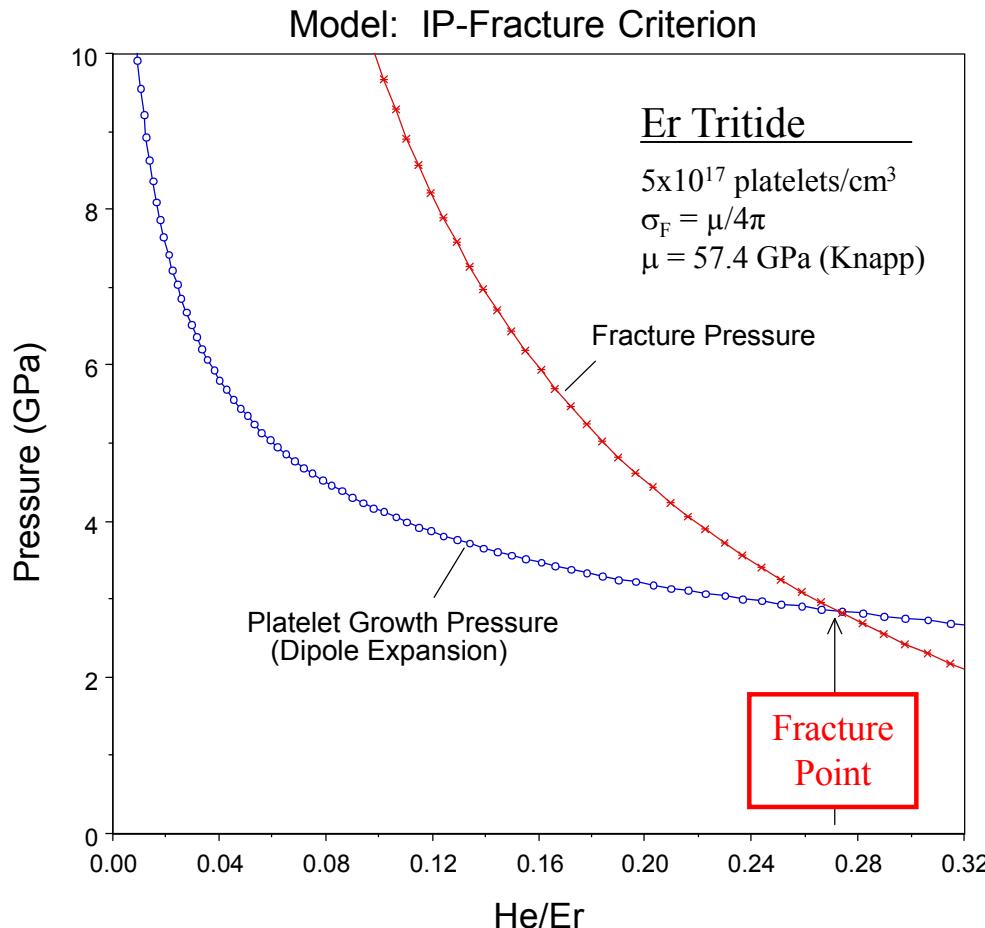
$$(p_F - 2\gamma/s) (\pi r^2/2) \cos \theta = \sigma_F [3^{1/3} R^2 - (\pi r^2/2) \cos \theta]$$



- $\theta$  = Platelet angle in the fracture plane.
- Relative angle between platelets is zero or angle between [111] directions,  $70.529^\circ$ .
- Averaging areas using (100), (110), (111) principle planes, considering the frequency in each geometry, gives  $\langle \cos \theta \rangle = 0.4755$ .
- IP-Fracture criterion:

$$p_F = 2\gamma/s + \sigma_F \{ [\pi r^2 n_P^{2/3} \langle \cos \theta \rangle]^{-1} - 1 \}.$$

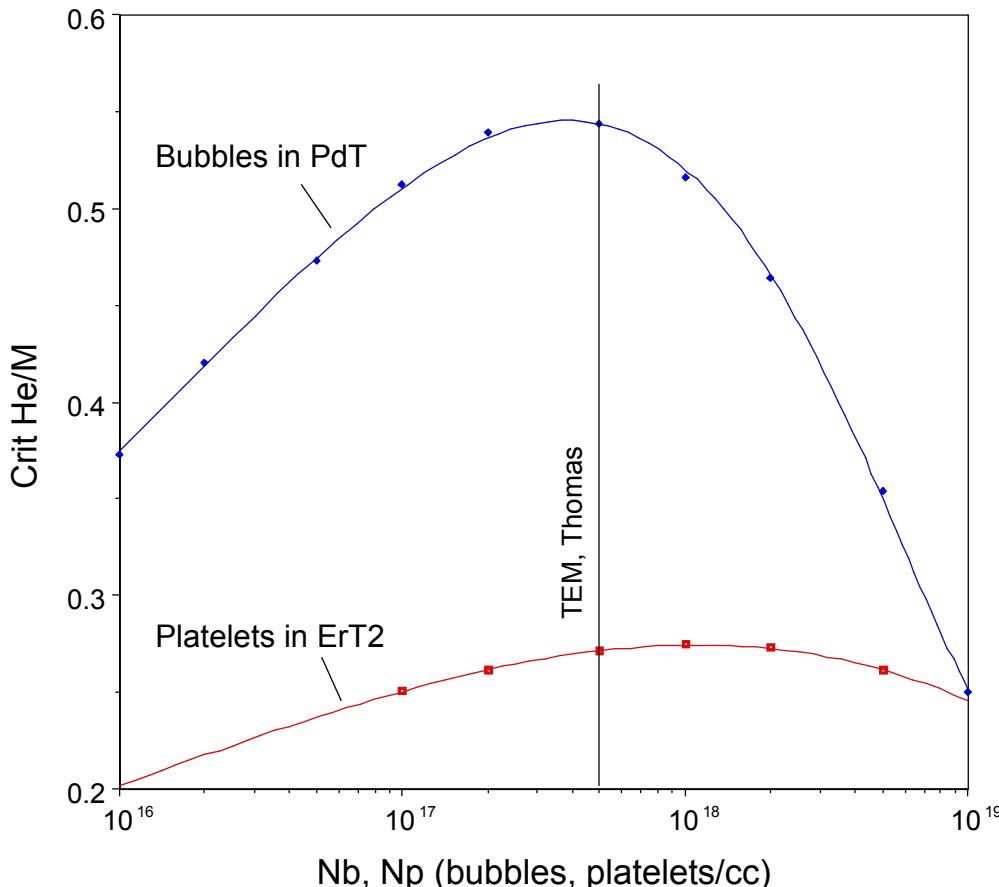

# The pressure for inter-platelet fracture drops below that for platelet growth at 0.27 He/Er.



- This fracture condition depends on platelet density and fracture strength  $\sigma_F$ .
- Rapid He release will occur when this condition extends over several platelet spacings
  - when platelets at the mean density undergo IP-fracture.



# Dependence of the Crit He/M on “bubble” density is weaker for platelets.



- The optimum density appears slightly higher for Er platelets, compared to Pd bubbles.
- For spherical bubbles in PdT, regions with high bubble density begin linkage first.
- By contrast, the ligaments between platelets in ErT<sub>2</sub> should all fracture at about the same time -
  - producing a more abrupt transition to Rapid Release.



# Work on platelet structures is continuing.

---

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