



Fracture Behavior of Polyurethane Foams

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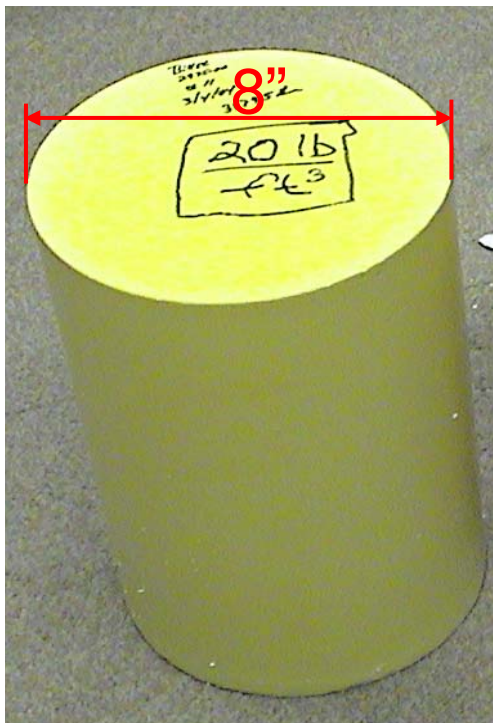
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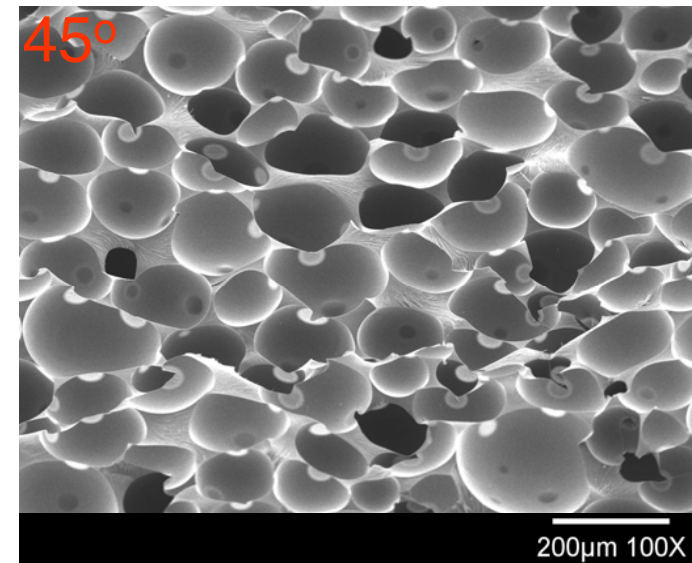
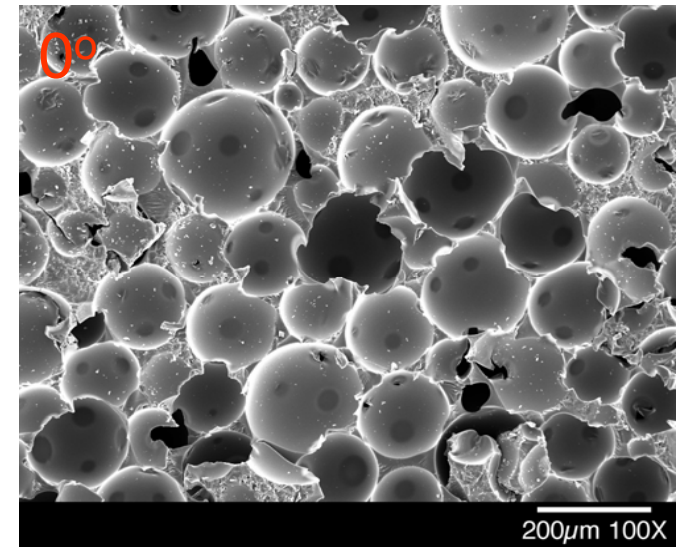


Investigated Material

- ❑ Closed cell polyurethane foam
- ❑ Nominal density of 20 pcf
- ❑ 8" diameter billet



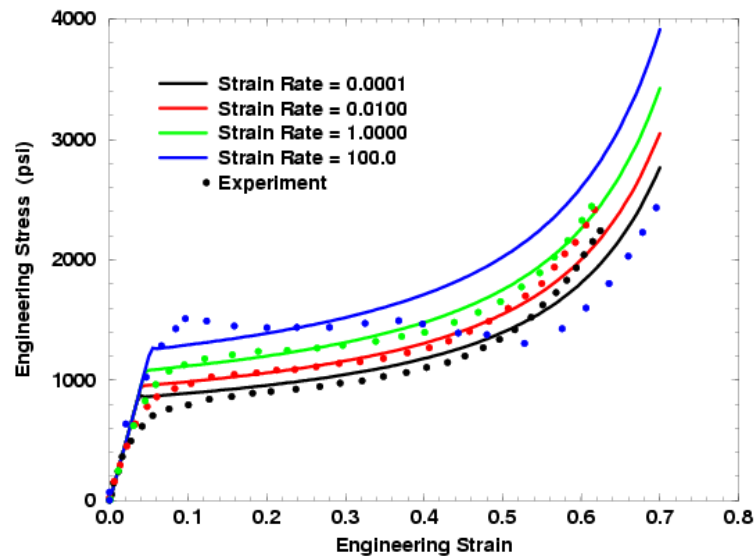
Billet of PMDI 20



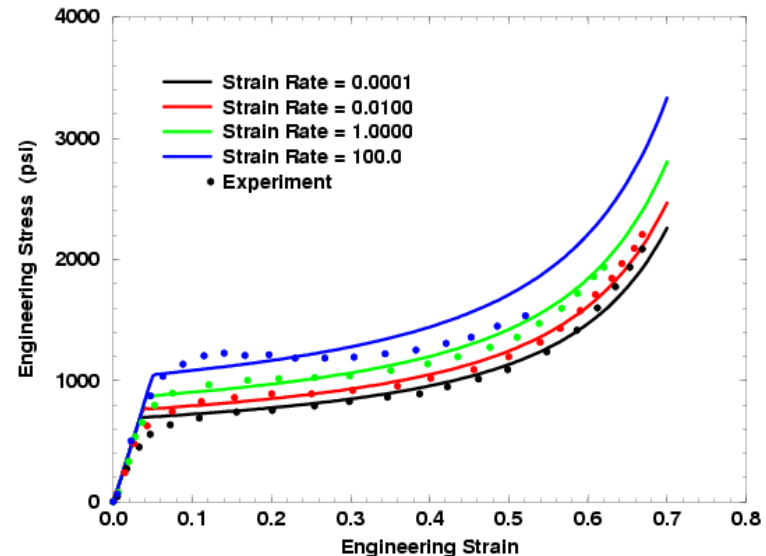


Background

- Characterization experiments of polyurethane (PU) foam materials at a wide range of strain rate and temperature were conducted to study
 - Effects of strain rate
 - Effects of temperature
- Viscoplastic Foam Model (VFM) based on the characterization tests were developed to predict the effects of temperature and strain rate



(a) 70°F

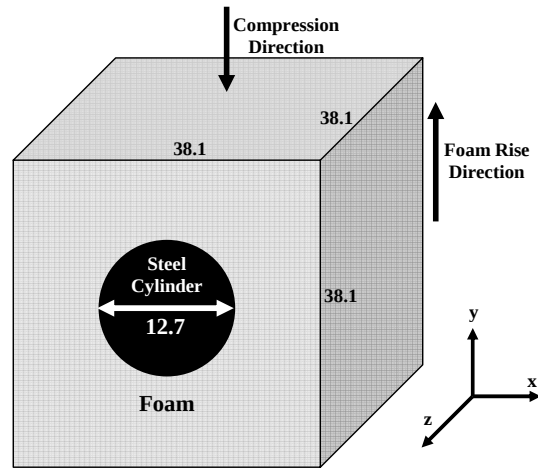


(b) 165°F

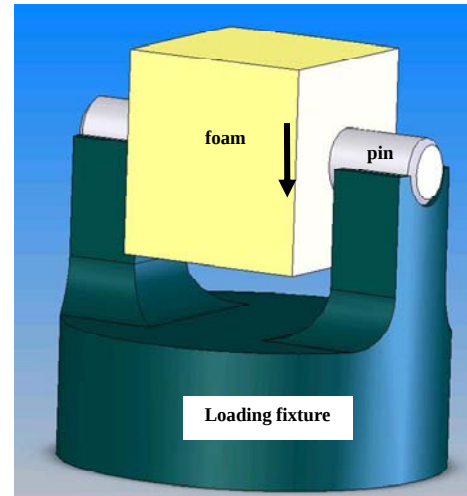
Simulation of characterization experiments using VFM



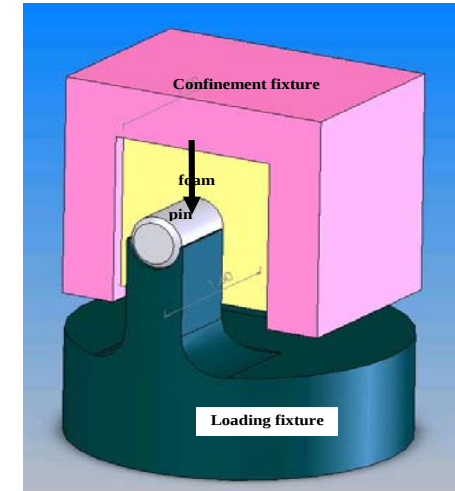
Model Validation Experiments



(I)



(II)



(III)

Three loading cases of foam with a steel pin inclusion are considered:

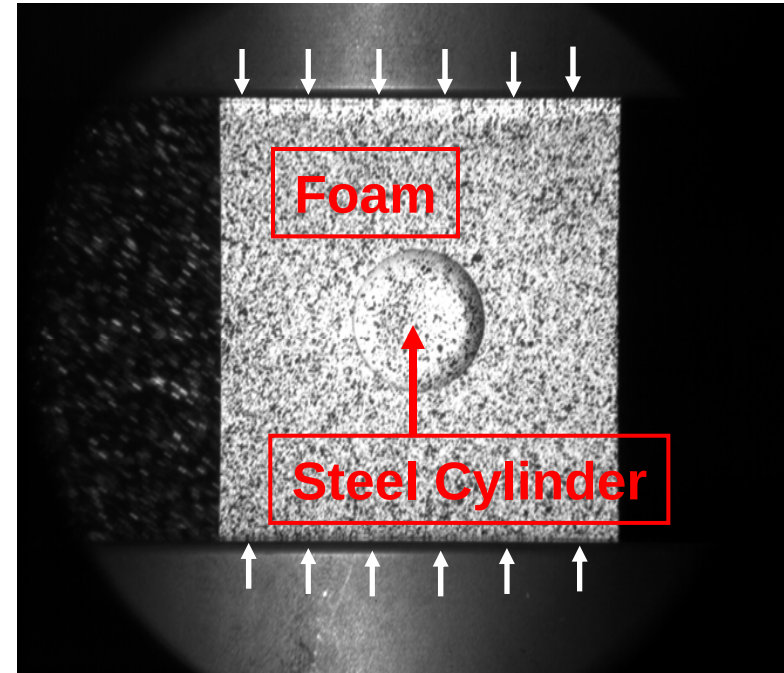
- (1) Loading from top and bottom surfaces, representing the crush of a foam package;
- (2) Loading from top surface and pin, representing the drop of a foam package; and
- (3) Same as (2), but the foam is confined to study the effects of confinement



Model Validation: Crush of Foam Package



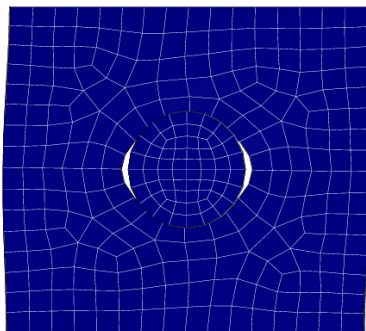
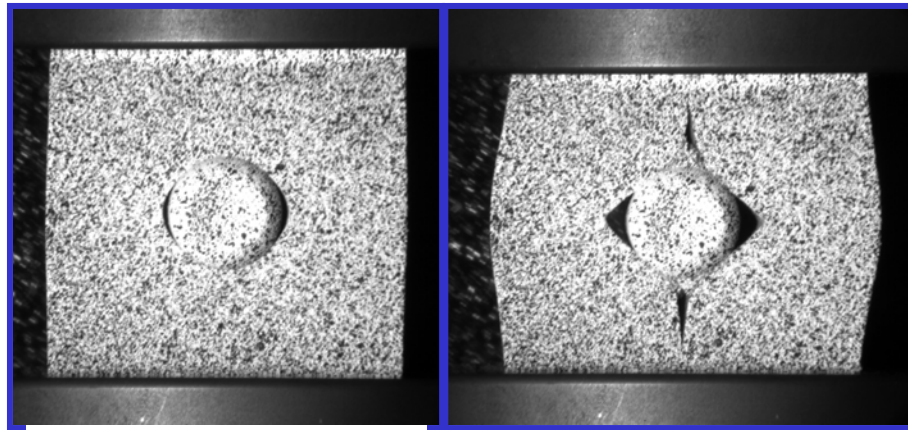
MTS 858 Mini Bionix with 3D-DIC System



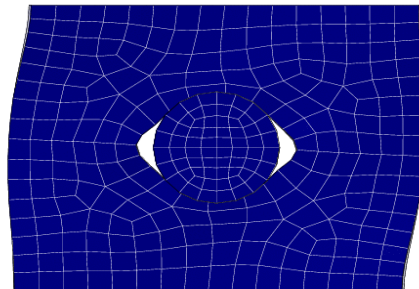
Experiment represents foam package crush



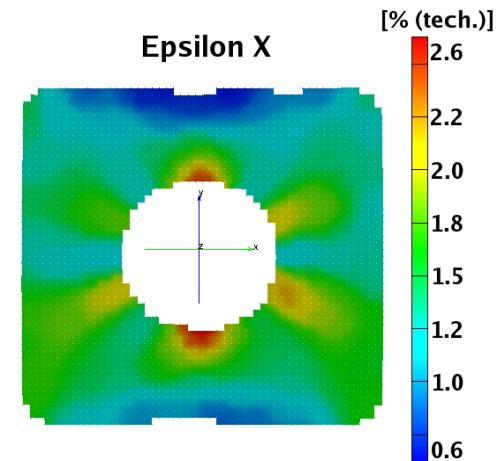
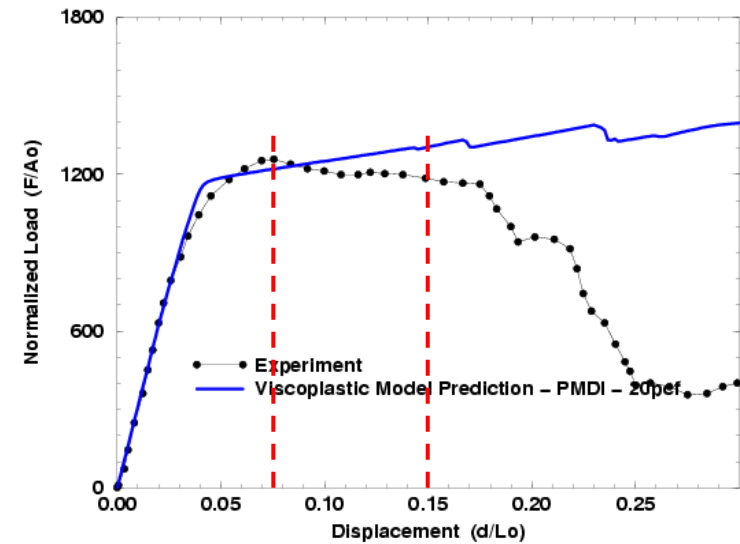
Simulation of Model Validation Test



7.5% compression
Peak load



15% compression

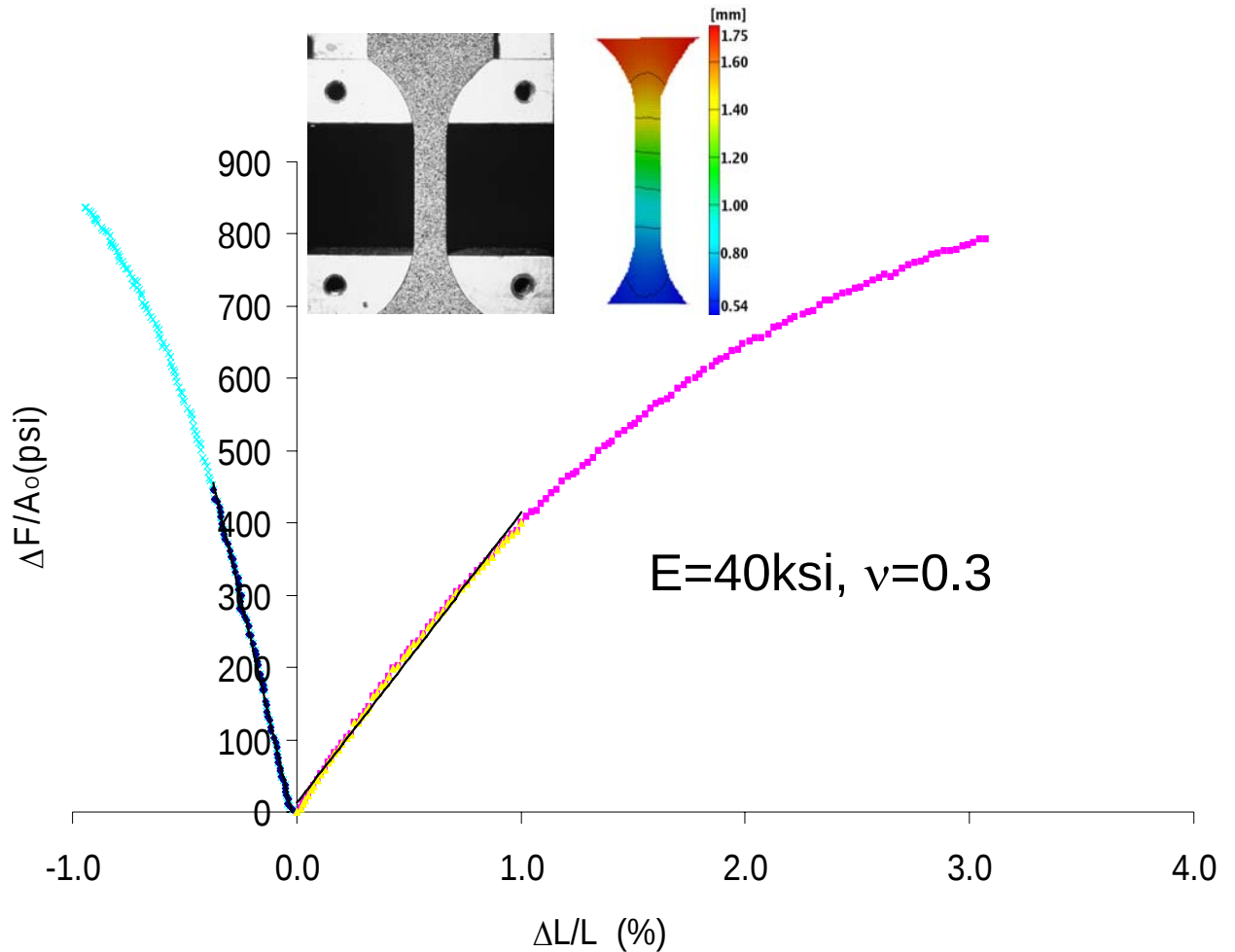
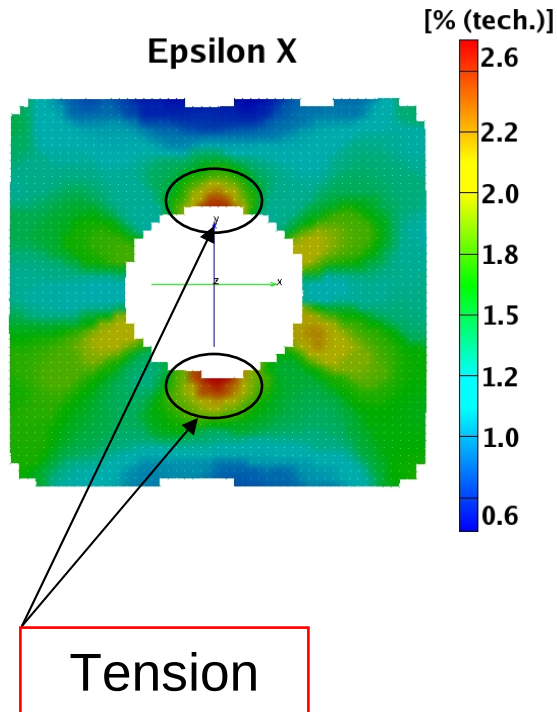


Failure criteria needs to be included in the viscoplastic foam model (VFM)



Tensile behavior of PMDI 20

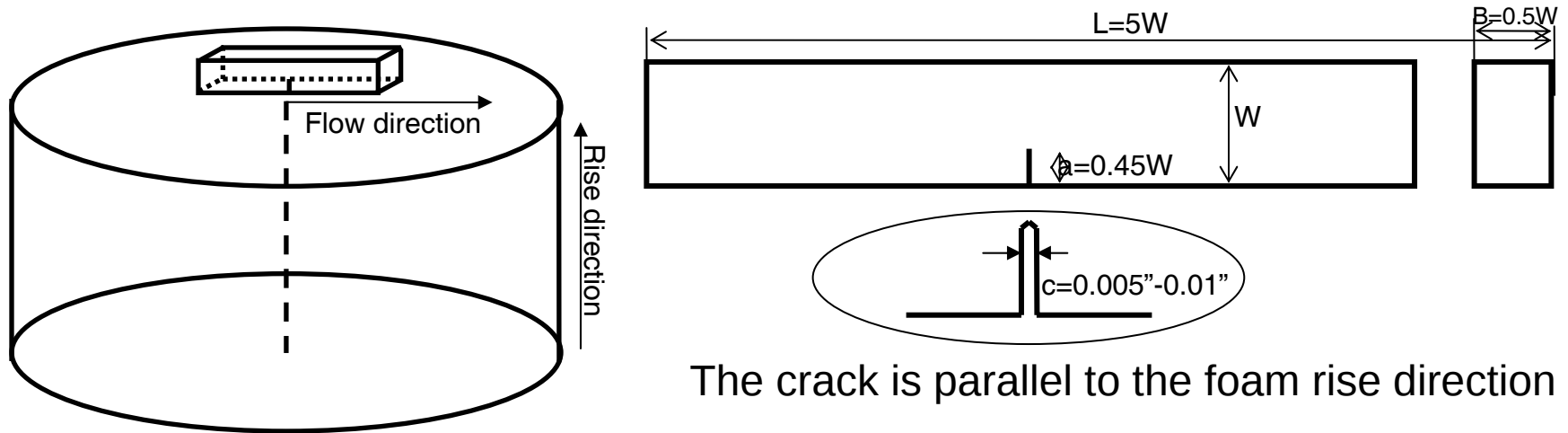
□ Rigid Foam



Typical Tensile Stress~strain curve for PMDI 20
at room temperature, rise direction



Foam Fracture Tests

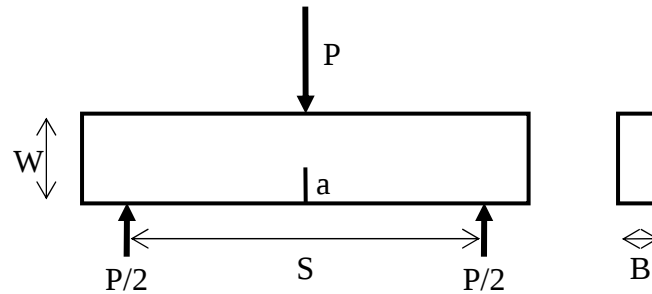


Matrix of different tests and specimens:

	A	B	C	D
W (in)	0.5	1	1	1
B (in)	0.25	0.5	0.5	0.5
L (in)	2.5	5	5	5
A (in)	0.225	0.45	0.45	0.45
Test	SENB	SENB	SENB	SENT



Fracture Toughness K_{Qc}

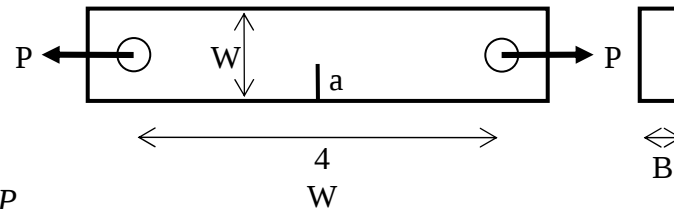


$$\sigma = \frac{6M}{BW^2} = \frac{3}{2} \frac{PS}{BW^2} \quad \left(M = \frac{PS}{4} \right)$$

$$K_I = \sigma \sqrt{\pi a} F(a/W)$$

For $S/W = 4$:

$$F(a/W) = 1.090 - 1.735(a/W) + 8.20(a/W)^2 - 14.18(a/W)^3 + 14.57(a/W)^4$$



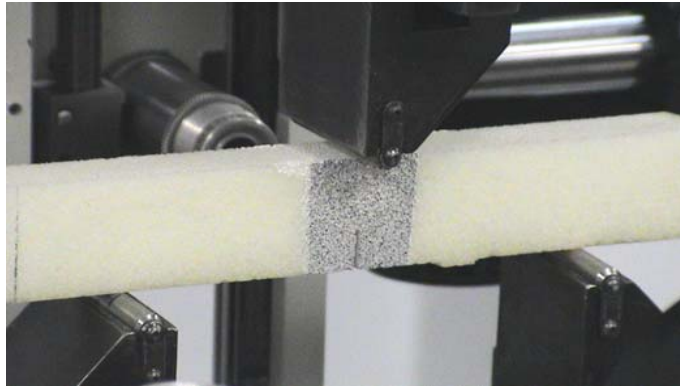
$$\sigma = \frac{P}{BW}$$

$$K_I = \sigma \sqrt{\pi a} F(a/W)$$

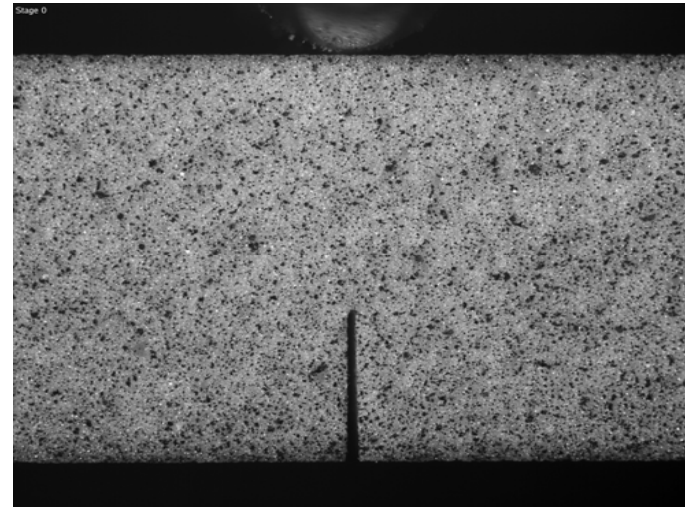
$$F(a/W) = 1.12 - 0.231(a/W) + 10.55(a/W)^2 - 21.72(a/W)^3 + 30.39(a/W)^4$$



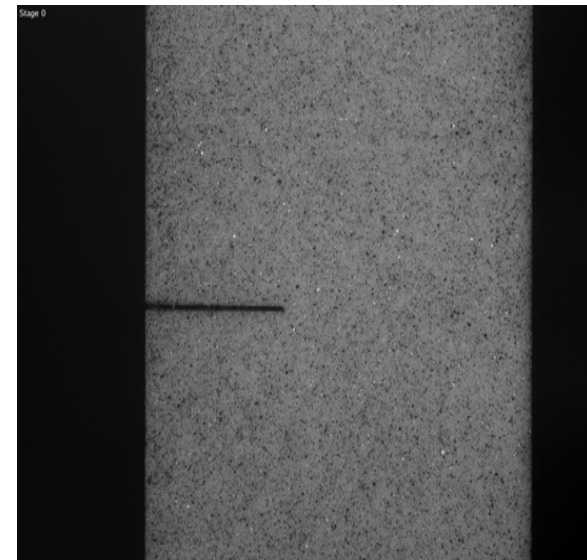
Foam Fracture Tests



Single Edge Notch Bending (SENB) setup



Single Edge Notch Tensile (SENT) setup



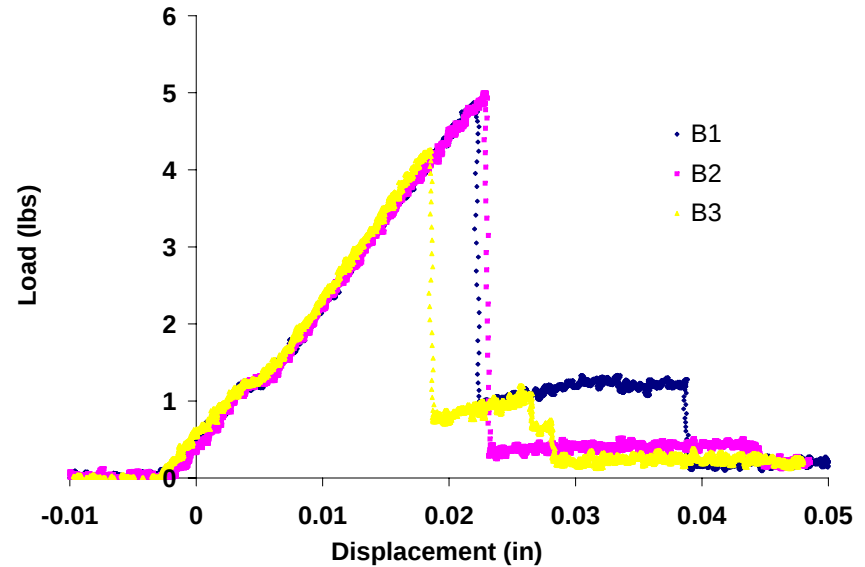
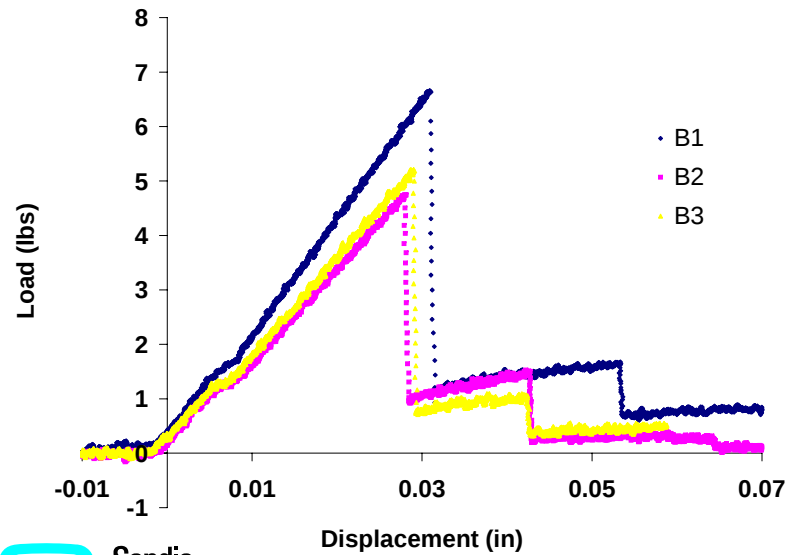
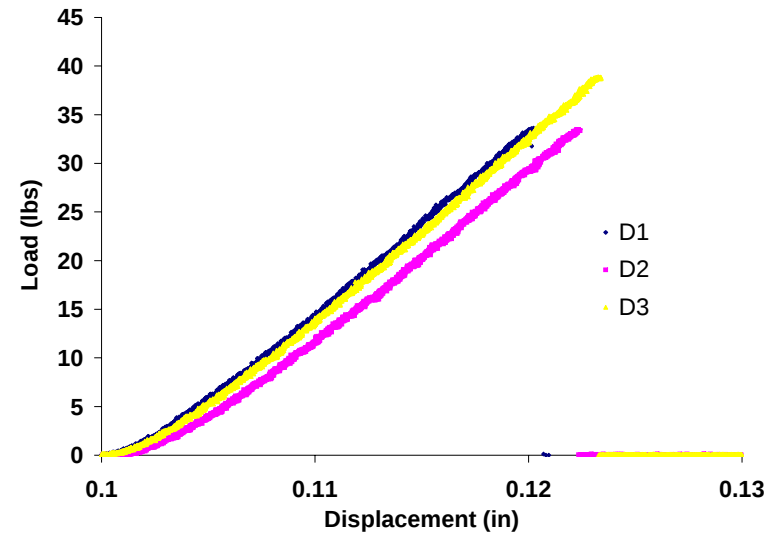
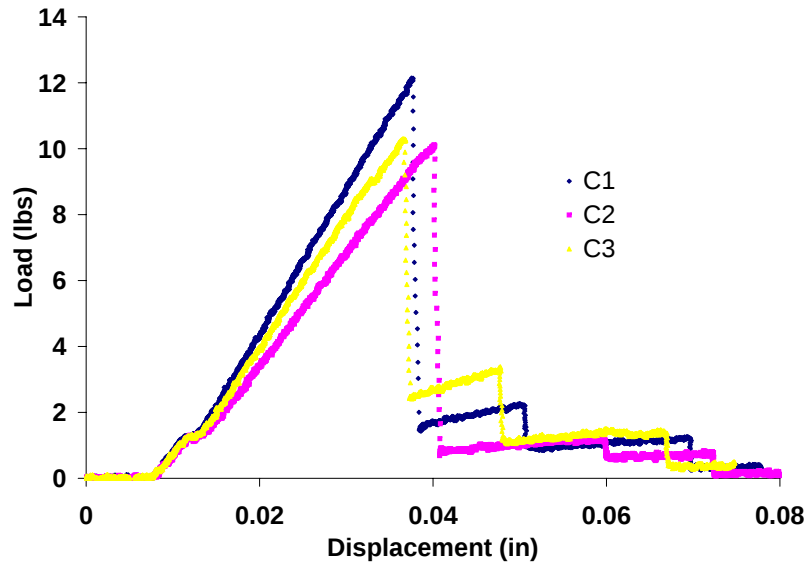
Area of Interest (AOI) for DIC



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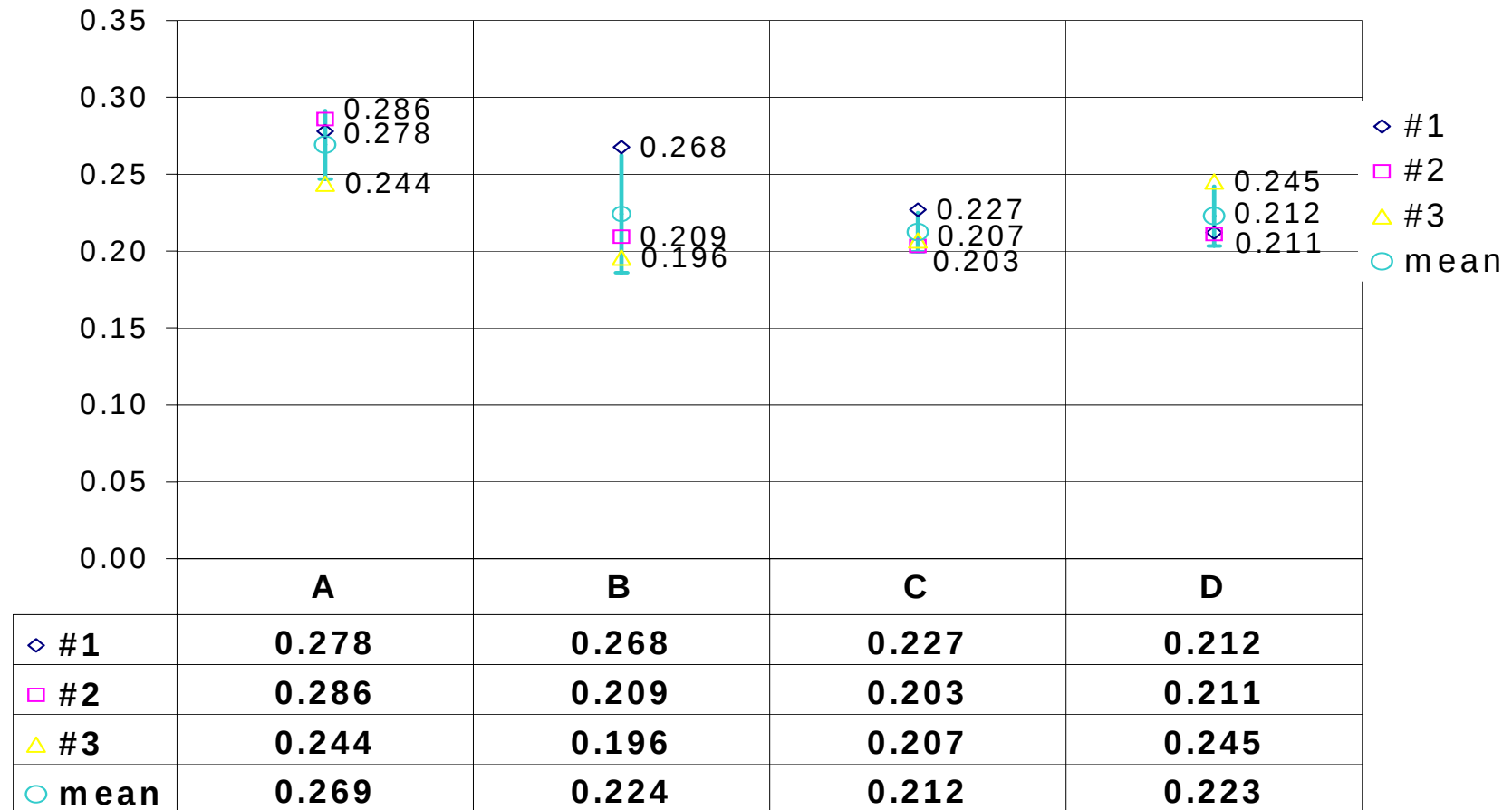


Load versus Displacement Curves





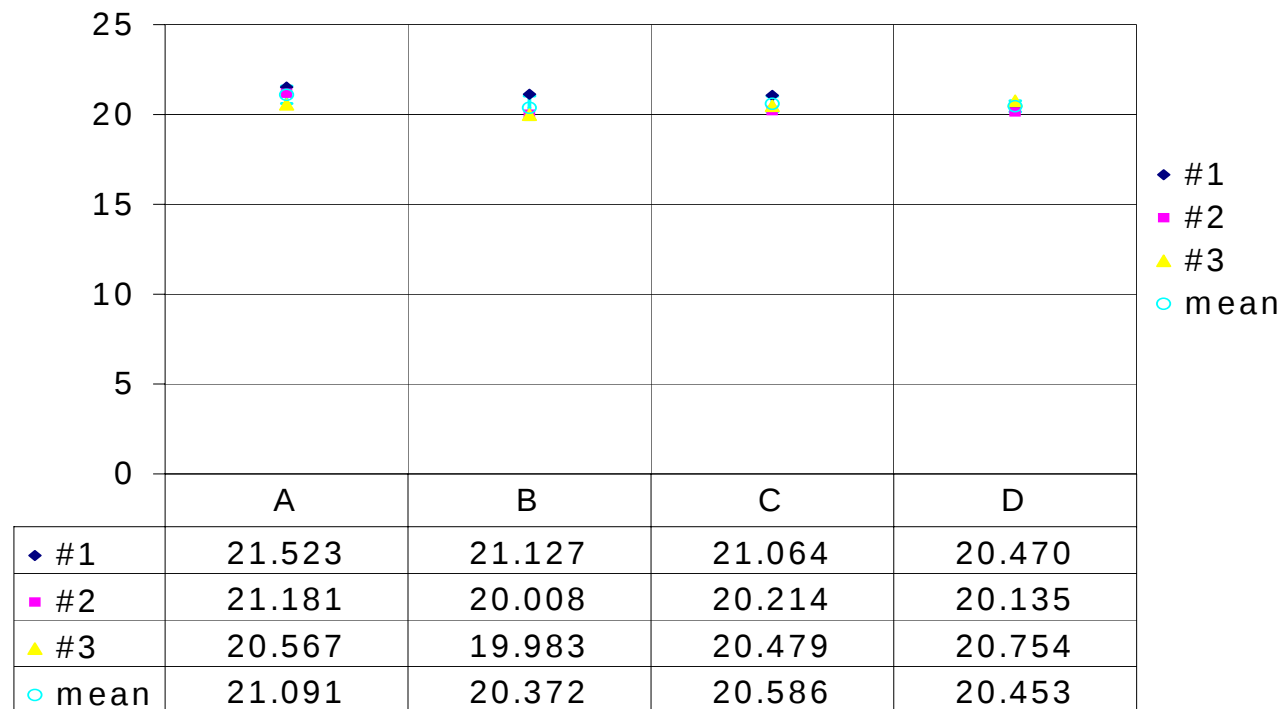
Fracture Toughness K_{Qc}





Fracture Toughness Uncertainty

1. Density variation:



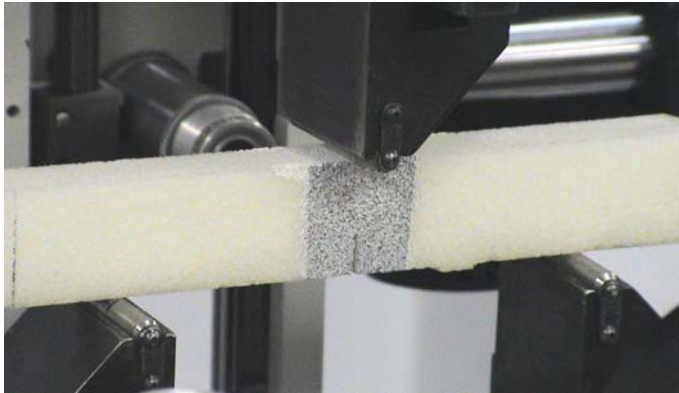
2. Crack length uncertainty

3. Material inhomogeneity

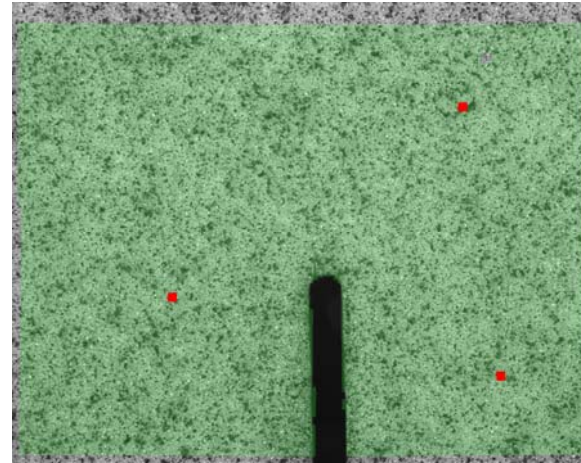
4. Size effect



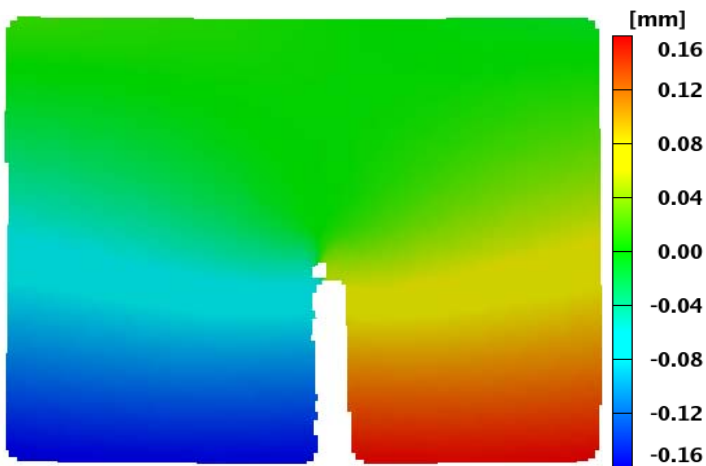
Full-field Deformation using DIC



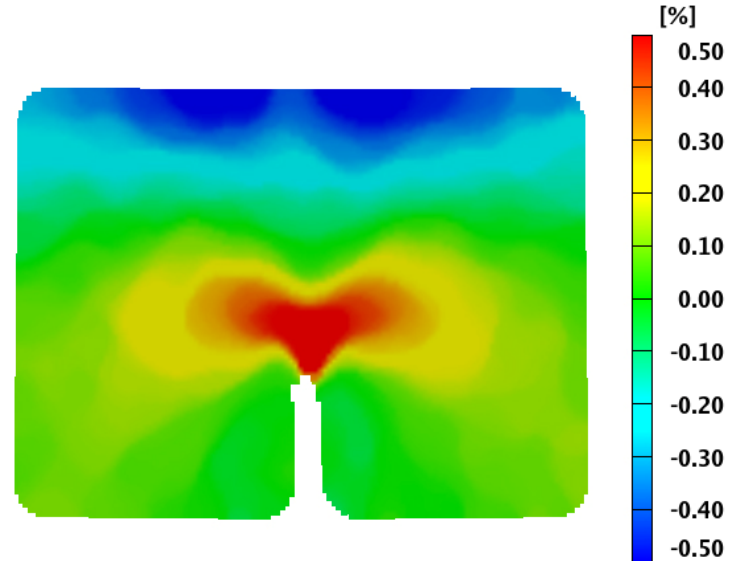
SENB setup



AOI for DIC



Displacement field U



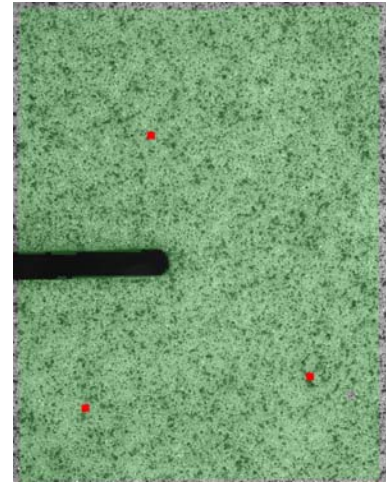
Strain field E_{xx}



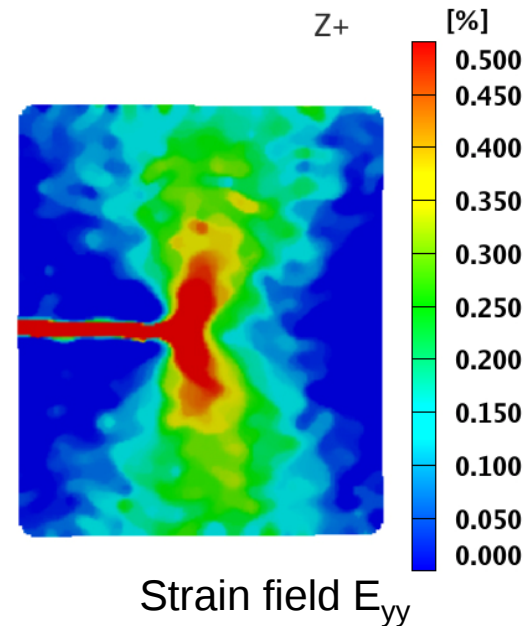
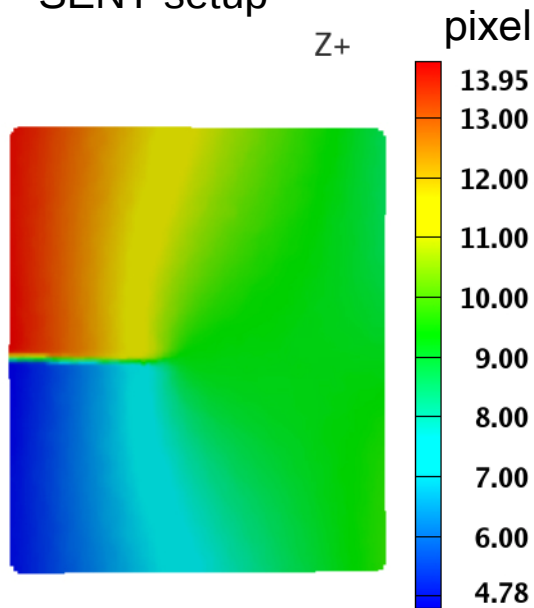
Full-field Deformation using DIC



SENT setup



AOI for DIC

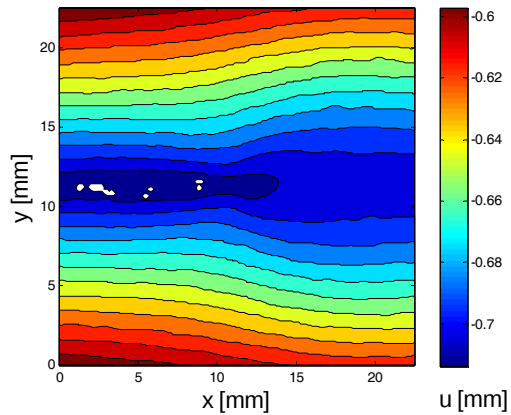


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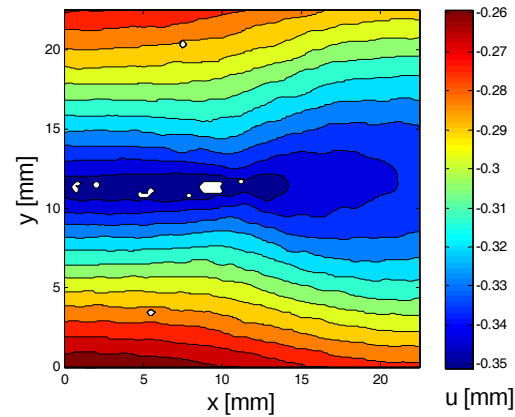


Crack-tip displacement field

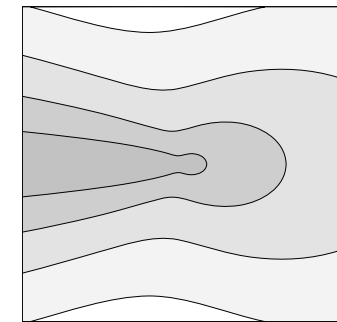
SENB



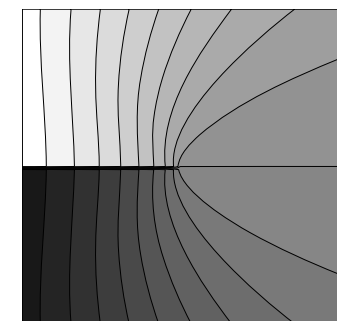
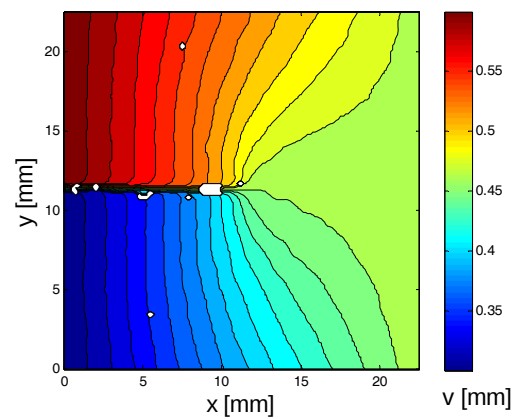
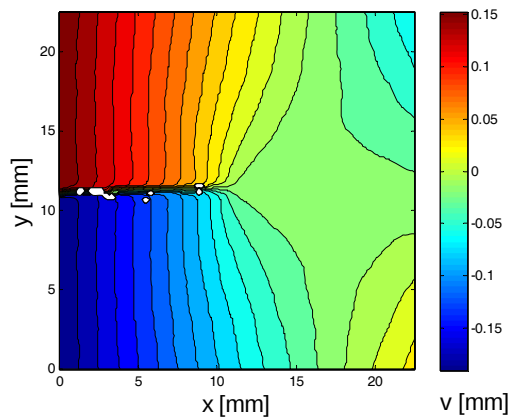
SENT



Analytical K_I -field



u



v



Path-independent integral

J contour integral

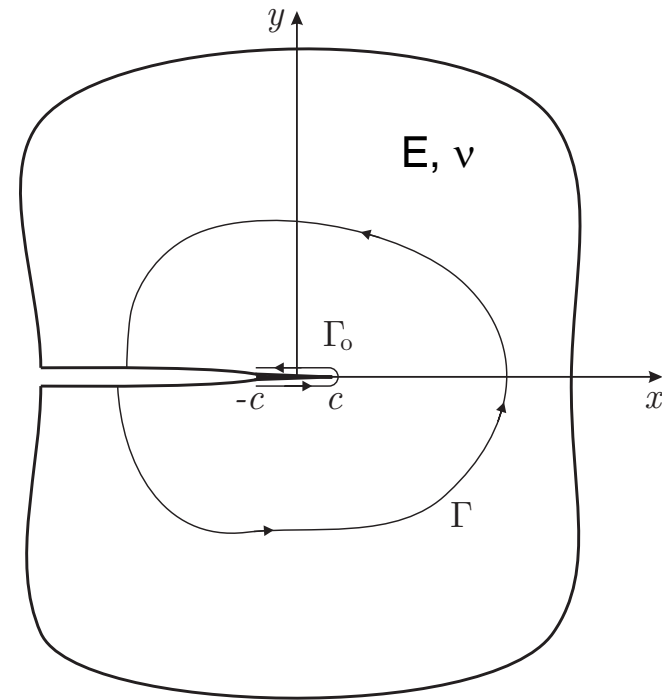
$$J = \int_{\Gamma} \left(\frac{1}{2} \sigma_{\alpha\beta} u_{\alpha,\beta} n_1 - \sigma_{\alpha\beta} u_{\beta,1} n_{\alpha} \right) ds$$

Energy release rate

$$G = \frac{K_I^2}{E'}$$

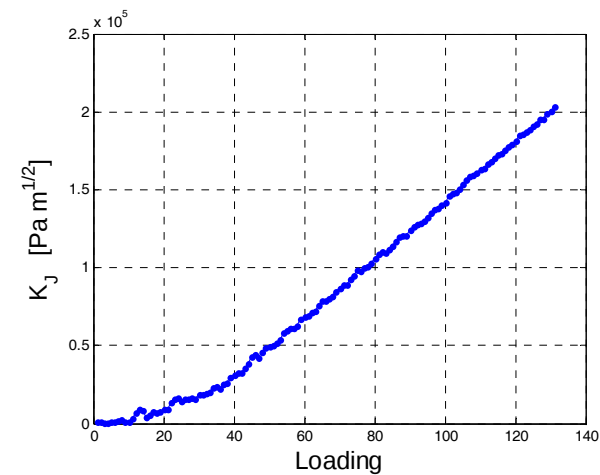
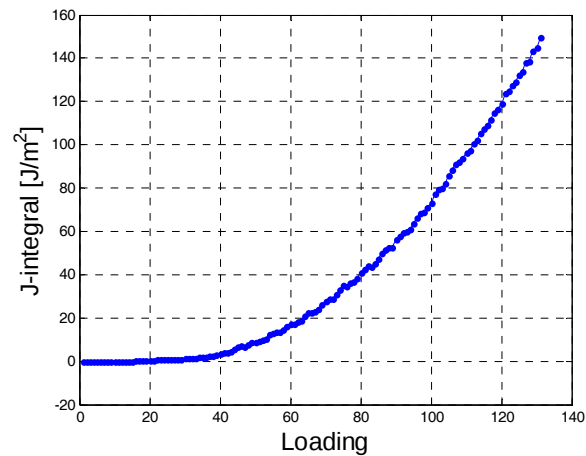
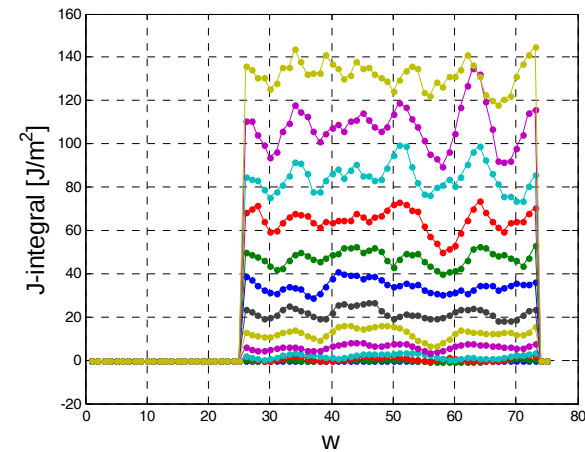
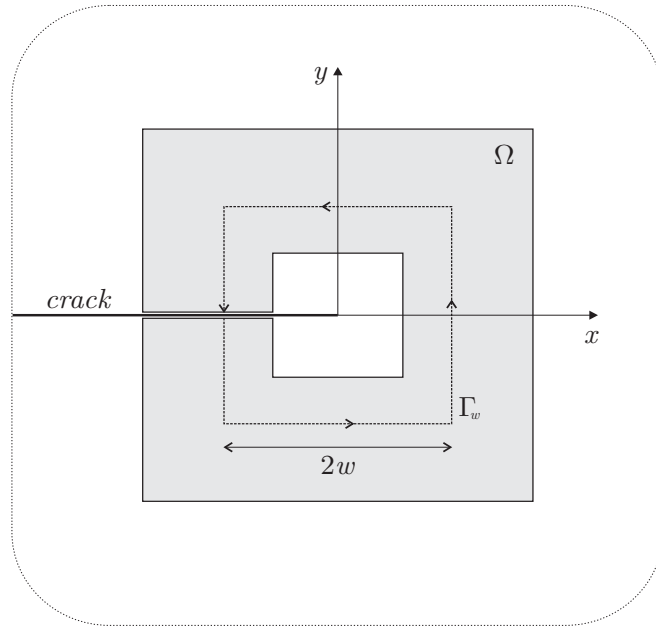
Elastic material under quasistatic condition ($G=J$)

$$K_J = \sqrt{E' J}$$



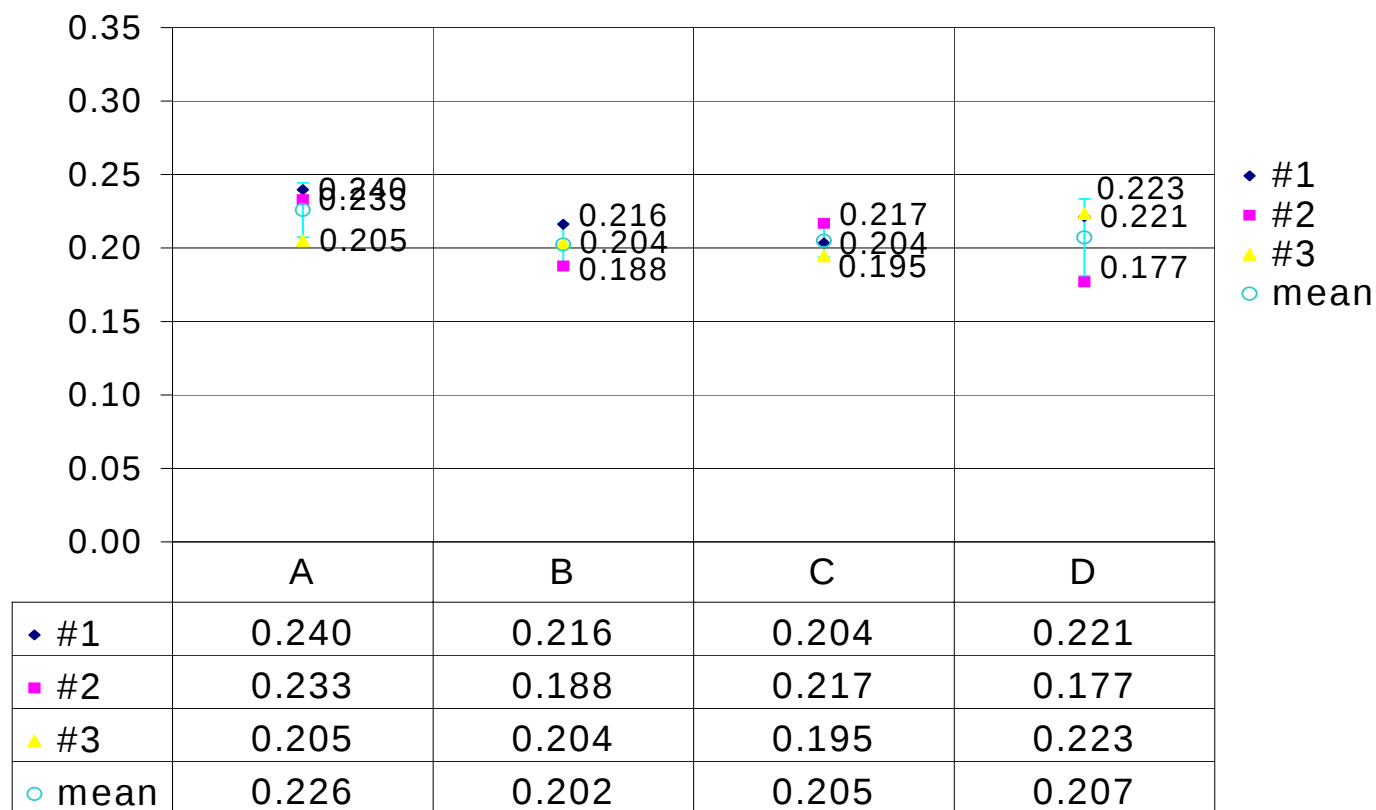


Calculating J-integral





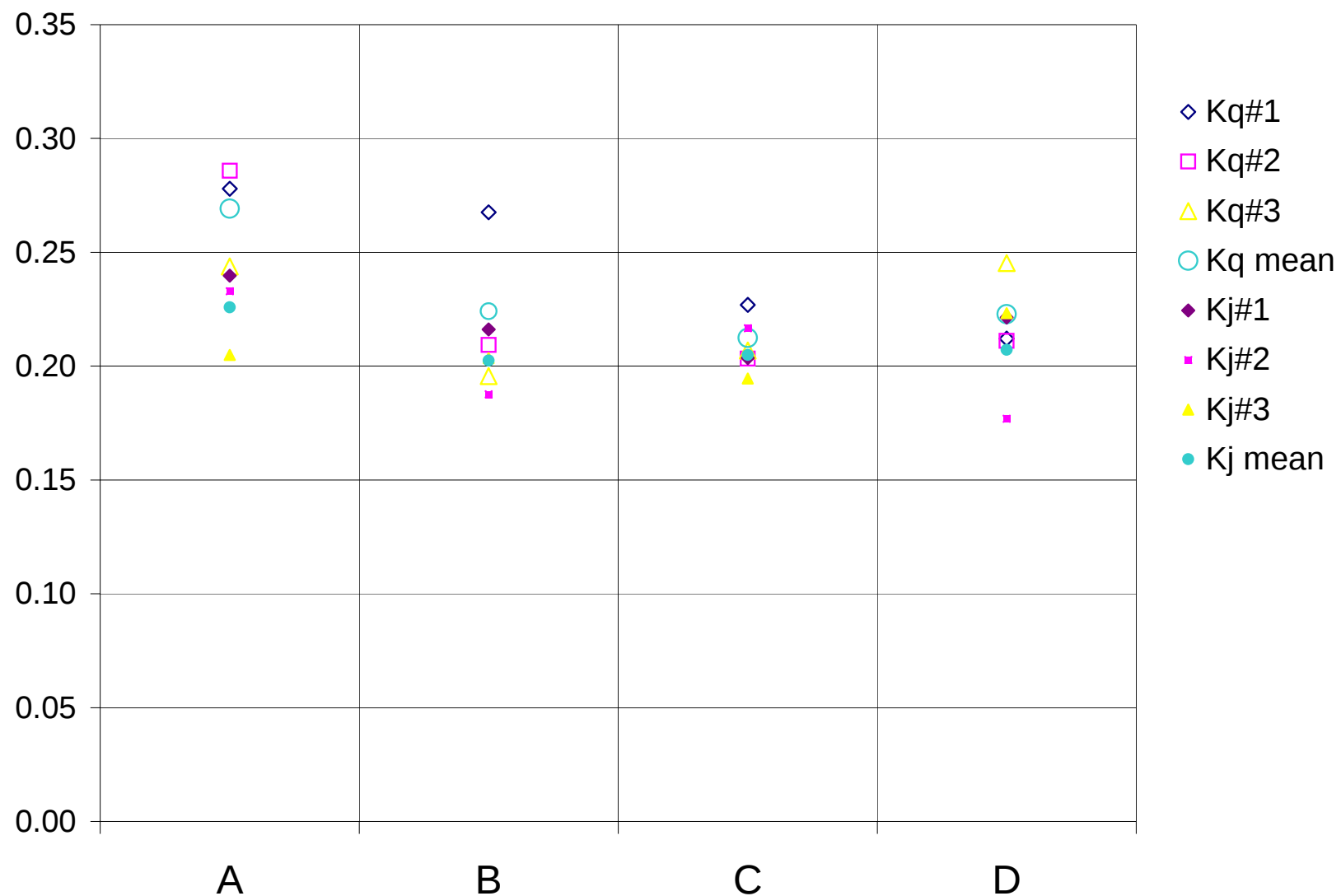
K_{Jc}



Effects to K_{Jc} : Young's modulus E , Displacement field



K_{Jc} and K_{Qc}





Summary

- The fracture toughness of PMDI 20 was measured using both SENB and SENT under LEFM assumptions;
- DIC was applied to obtain the full-field displacement and strain around the crack tip;
- Path-independent J-integral was calculated from the DIC full field displacement;
- K_Q and K_{Jc} are overall matching well except for smaller size specimens, where K_J gives more accurate value.



Thank you!

Questions?