

Uncertainty Quantification in Reacting Flow

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The Validation Challenge

- Validation of a computational model :
 - Establish "agreement" between predictions and empirical observations
- Establishing model validity requires "error bars" on computational predictions
 - Disagreement without error bars cannot be used to conclude that a particular model is not valid
 - Disagreement within the range of uncertainty of the results can be due to parametric uncertainty

The Case for Uncertainty Quantification

- UQ is needed for :
 - validation of scientific models
 - validation of predictive codes
 - engineering design optimization
 - assessment of confidence in computational predictions
 - enabling decision-making strategies based on predictive models
 - assimilation of observational data and model construction in noisy environments
 - multiscale/multiphysics modeling

Sources of Uncertainty

- model structure
 - participating physical processes
 - governing equations
 - constitutive relations
- model parameters
 - transport properties
 - thermodynamic properties
 - constitutive relations
 - rate coefficients
- initial and boundary conditions
- geometry

Focus on parametric UQ

Elements of a UQ strategy

- Estimation of model/parametric uncertainties based on data
 - Deterministic framework
 - Regression analysis, fitting, parameter estimation
 - Probabilistic framework
 - Bayesian inference of uncertain models/parameters
- Forward propagation of uncertainty in computational models
 - Deterministic framework
 - Local Sensitivity analysis (SA); Error propagation
 - Interval math
 - Probabilistic framework – Global SA / stochastic UQ
 - Sampling based — non-intrusive
 - Direct — intrusive

Stochastic Framework

- Laplacian/Bayesian conception of probability
 - Probability $\equiv$ degree of knowledge
 - Uncertain quantity $\equiv$ random variable
 - Contrast with Frequentist framework
- Inference with Bayes theorem

$$p(m|d)p(d) = p(d|m)p(m)$$

A formal framework for

- representation of knowledge
- learning from data
- incorporation of prior knowledge
- construction of uncertain models
- avoidance of overfitting

Issues with Least Squares (LS) Parameter Estimation

- Choice of optimal number of fit parameters (p)
 - $\chi_R^2 = \chi^2 / (\mathcal{D} - p)$ decreases with increased p
 - Versus Ockham's razor principle in Bayesian analysis
- LS best fit is the Maximum Likelihood Estimate (MLE) assuming gaussian noise in the data
- LS Estimation of Uncertainty in inferred parameter values relies on assumed linearity of the model in the parameters
- No general means of handling nuisance parameters

Role of Bayes Formula in Parameter Inference

- Bayes Formula:

$$p(\lambda, y) = p(\lambda|y)p(y) = p(y|\lambda)p(\lambda)$$

or:

$$\underbrace{p(\lambda|y)}_{\text{Posterior}} = \frac{\overbrace{p(y|\lambda)}^{\text{Likelihood}} \overbrace{p(\lambda)}^{\text{Prior}}}{\underbrace{p(y)}_{\text{Evidence}}}$$

- Infer PDF of λ rather than the least-squares estimate of λ
- Posterior contains all information about λ
 - including both prior information and data
- Evidence is a normalizing constant – ignore

The Posterior — towards parametric uncertainties

Parameter λ_k marginal probability:

$$p(\lambda_k|y) = \int p(\lambda|y) d\lambda_{1:k-1} d\lambda_{k+1:\mathcal{M}}$$

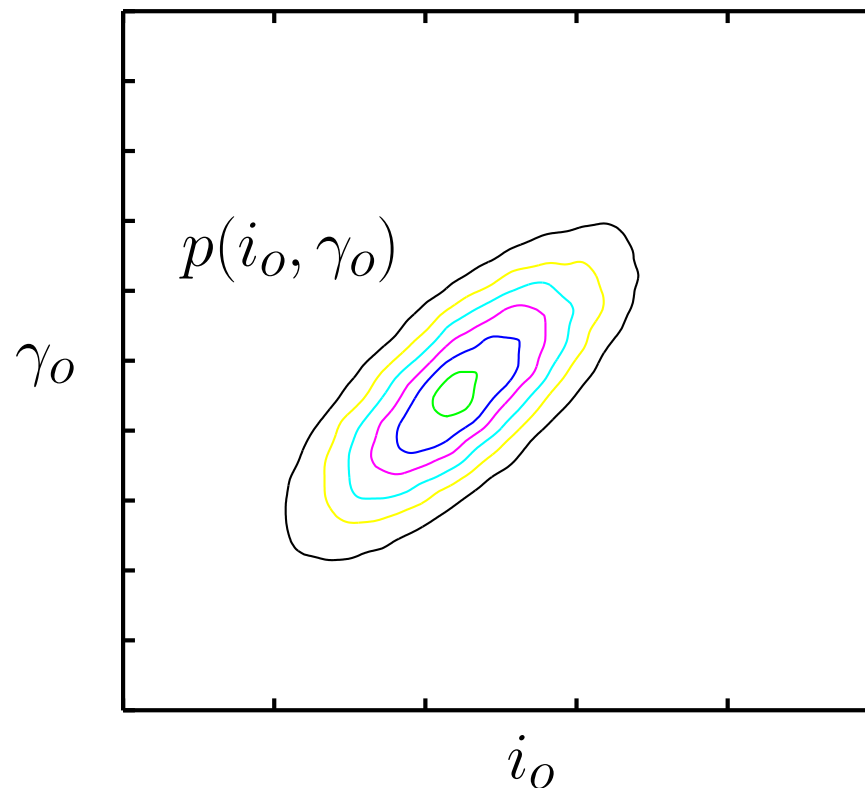
- Given any sample $\{\lambda\}$, the un-normalized posterior probability can be easily computed

$$p(\lambda|y) \propto p(y|\lambda)p(\lambda)$$

- Explore the posterior using Markov Chain Monte Carlo (MCMC)
- Can use uninformed priors
- Evaluate marginals from the MCMC statistics

Construction Allows Exploration of Correlations among Parameters

- Available naturally from the MCMC procedure
- Useful for understanding interplay between data and model
- Needed for subsequent UQ



Spectral Stochastic UQ Formulation — Polynomial Chaos

- An L_2 random variable $u(\mathbf{x}, t, \theta)$ can be described by a Polynomial Chaos (PC) expansion in terms of:
 - Hermite polynomials Ψ_k , $k = 1, \dots, \infty$;
 - the associated infinite-dimensional Gaussian basis $\{\xi_i(\theta)\}_{i=1}^{\infty}$;
 - spectral mode strengths $u_k(\mathbf{x}, t)$, $k = 1, \dots, \infty$.
- Truncated to finite dimension n and order p , the PC expansion for u is written as

$$u(\mathbf{x}, t, \theta) \simeq \sum_{k=0}^P u_k(\mathbf{x}, t) \Psi_k(\underline{\xi}(\theta))$$

where $\underline{\xi}(\theta) = \{\xi_1(\theta), \dots, \xi_n(\theta)\}$.

Non-intrusive – Sampling-Based – Spectral Projection (NISP) UQ

- Sample parameters using Monte Carlo
- Compute realizations of the model outputs
- Project MC statistics on the spectral mode strengths $u_k(t)$

$$u_k = \frac{\langle u \Psi_k \rangle}{\langle \Psi_k^2 \rangle} = \frac{1}{\langle \Psi_k^2 \rangle} \int u \Psi_k(\xi) \rho(\xi) d\xi, \quad k = 0, \dots, P$$

– Evaluate integrals numerically (MC, quadrature, cubature)

- Uncertain model output

$$u(x, t; \theta) = \sum_{k=0}^P u_k(x, t) \Psi_k(\xi(\theta))$$

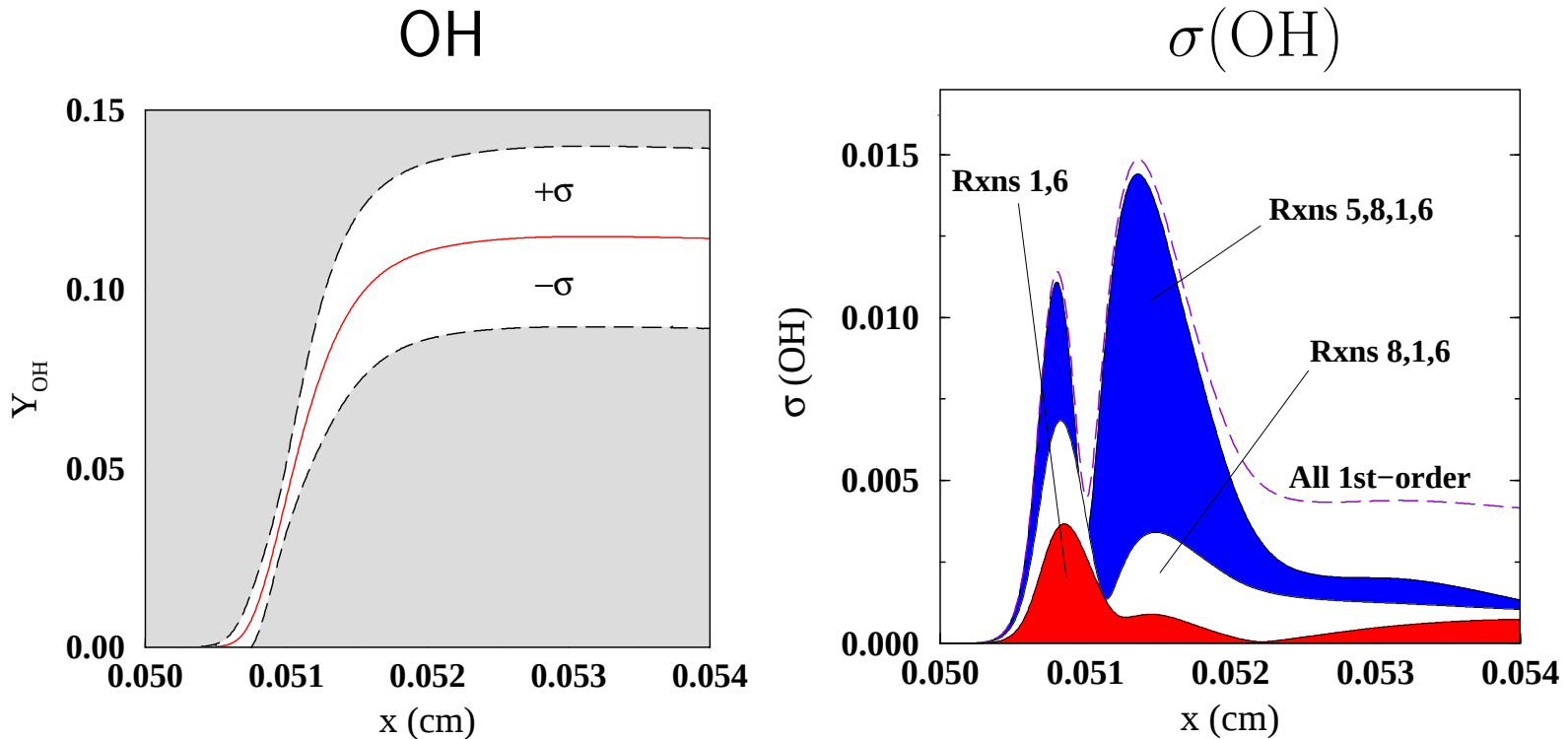
NISP UQ Application: Premixed H₂-O₂ Chemistry at Super-Critical Water Oxidation (SCWO) Conditions

- Allow uncertainties in reaction rate constants and thermodynamic properties, per published experimental data
- Wrap NISP processing around a deterministic reacting flow code
- Using 8-step simplified SCWO Hydrogen mechanism (McRae)

Reaction	A	n	E_a/R	UF
1. OH + H $\leftrightarrow$ H ₂ O	1.620E+14	0	75	3.16
2. H ₂ + OH $\leftrightarrow$ H ₂ O + H	1.024E+08	1.6	1660	1.26
3. H + O ₂ $\leftrightarrow$ HO ₂	1.481E+12	0.6	0	1.58
4. HO ₂ + HO ₂ $\leftrightarrow$ H ₂ O ₂ + O ₂	1.867E+12	0	775	1.41
5. H ₂ O ₂ + OH $\leftrightarrow$ H ₂ O + HO ₂	7.829E+12	0	670	1.58
6. H ₂ O ₂ + H $\leftrightarrow$ HO ₂ + H ₂	1.686E+12	0	1890	2.00
7. H ₂ O ₂ $\leftrightarrow$ OH + OH	3.0000E+14	0	24400	3.16
8. OH + HO ₂ $\leftrightarrow$ H ₂ O + O ₂	2.891E+13	0	-250	3.16

Species	μ_0	2σ
H	52.10	0.01
OH	9.3	0.2
H ₂ O	-57.80	0.01
H ₂ O ₂	-32.53	0.07
HO ₂	3.0	0.5

1D H₂-O₂ SCWO Flame NISP UQ/Chemkin-Premix



- Fast growth in OH uncertainty in the primary reaction zone
- Constant uncertainty and mean of OH in post-flame region
- Uncertainty in pre-exponential of Rxn.5 ($H_2O_2 + OH = H_2O + HO_2$) has largest contribution to uncertainty in predicted OH

First-Order Sensitivity Information in a PC Expansion

- Conventional sensitivity

$$u = u(x, t; \lambda) : \quad S = \left. \frac{\partial u}{\partial \lambda} \right|_{\lambda_0} \sim \left. \frac{\delta u}{\delta \lambda} \right|_{\lambda_0}$$

- Sensitivity in a stochastic UQ context

$$\lambda = \sum_{k=0}^P \lambda_k \Psi_k(\xi), \quad u = \sum_{k=0}^P u_k \Psi_k(\xi)$$

- For Hermite Ψ_k :

$$S = \frac{\partial u}{\partial \lambda} = \frac{\partial u / \partial \xi}{\partial \lambda / \partial \xi} = \frac{\sum_{k=0}^{P-1} (k+1) u_{k+1} \Psi_k}{\sum_{k=0}^{P-1} (k+1) \lambda_{k+1} \Psi_k} = \sum_{k=0}^P S_k \Psi_k$$

- Extends to multi-D case with independent parameters

Intrusive Spectral Stochastic UQ Formulation: ODE Example

- Sample ODE with parameter λ :

$$\frac{du}{dt} = \lambda u$$

- Let λ be uncertain; introduce $\xi \sim \mathcal{N}(0, 1)$.
Express λ and u using PCEs in ξ :

$$\lambda = \sum_{k=0}^P \lambda_k \Psi_k, \quad u = \sum_{k=0}^P u_k \Psi_k$$

- Substitute in ODE and apply a Galerkin projection on $\Psi_i(\xi)$,

$$\frac{du_i}{dt} = \sum_{p=0}^P \sum_{q=0}^P \lambda_p u_q C_{pqi}, \quad i = 0, \dots, P$$

where the $C_{pqi} = \langle \Psi_p \Psi_q \Psi_i \rangle / \langle \Psi_i^2 \rangle$ are known coefficients

Pseudo-Spectral Implementation

Spectral Product : $w = uv$

$$w = u * v \quad \Rightarrow \quad w_i = \langle uv \rangle_i, \quad i = 0, \dots, P$$

Pseudo-spectral higher-order polynomial terms :

$$w = \lambda u^2 v \quad \Rightarrow \quad w = \lambda * (u * (u * v))$$

Division :

$$w = \frac{u}{v} \quad \Rightarrow \quad \langle vw \rangle_k = u_k, \quad \text{solve linear equation system for } w_k$$

Arbitrary functions $u = f(x)$ where $\dot{u} = \frac{df}{dx}$ is a rational function of x & u :

$$u_k(x_b) - u_k(x_a) = \sum_{j=0}^P \int_{(x_a)_j}^{(x_b)_j} \sum_{i=0}^P C_{ijk} (\dot{u})_i dx_j$$

Spectral UQ: Incompressible Flow - Stochastic Projection Method

- $(P+1)$ Galerkin-Projected Momentum equations, $q = 0, \dots, P$:

$$\frac{\partial \mathbf{v}_q}{\partial t} + \nabla \cdot \langle \mathbf{v} \mathbf{v} \rangle_q = -\nabla p_q + \frac{1}{\text{Re}} \nabla \cdot \left\langle \mu [(\nabla \mathbf{v}) + (\nabla \mathbf{v})^T] \right\rangle_q$$

- Projection: for $q = 0, \dots, P$:

$$\begin{aligned} \frac{\tilde{\mathbf{v}}_q - \mathbf{v}_q^n}{\Delta t} &= C_q^n + D_q^n \\ \nabla^2 p_q &= -\frac{1}{\Delta t} \nabla \cdot \tilde{\mathbf{v}}_q \\ \frac{\mathbf{v}_q^{n+1} - \tilde{\mathbf{v}}_q}{\Delta t} &= -\nabla p_q \end{aligned}$$

- $P + 1$ *decoupled* Poisson Equation solutions for the pressure modes.

Laminar 2D Channel Flow with Uncertain Viscosity

- Incompressible flow
- Gaussian viscosity PDF

$$- \nu = \nu_0 + \nu_1 \xi$$

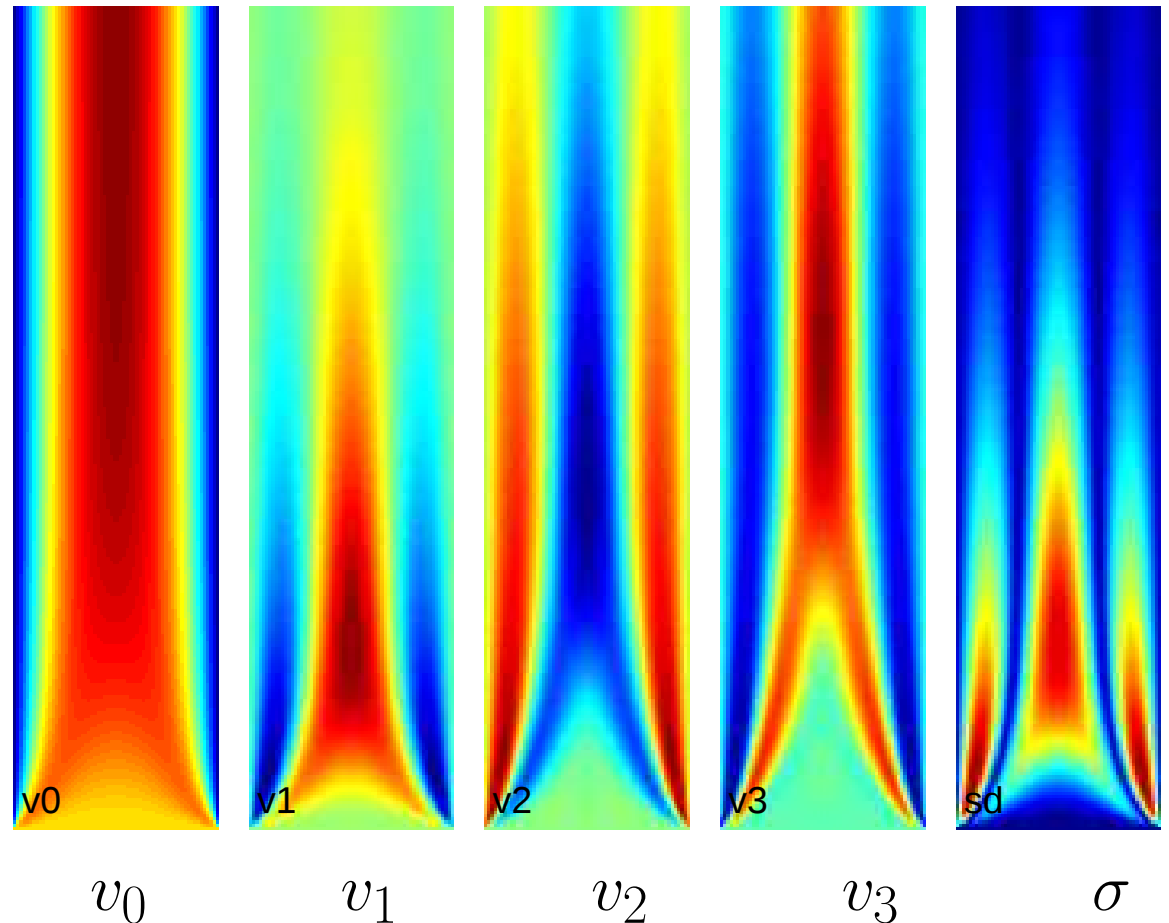
- Streamwise velocity

$$- v = \sum_{i=0}^P v_i \Psi_i$$

– v_0 : mean

– v_i : i -th order mode

$$- \sigma^2 = \sum_{i=1}^P v_i^2 \langle \Psi_i^2 \rangle$$



Spectral UQ Formulation: low M 2D Reacting Flow Equations

$$\frac{\partial \rho_q}{\partial t} + \nabla \cdot \langle \rho \mathbf{v} \rangle_q = 0$$

$$\frac{\partial \langle \rho \mathbf{v} \rangle_q}{\partial t} + \nabla \cdot \langle \rho \mathbf{v} \mathbf{v} \rangle_q = -\nabla p_q + \frac{1}{Re} \nabla \cdot \left\langle \mu [(\nabla \mathbf{v}) + (\nabla \mathbf{v})^T] - \frac{2}{3} \mu (\nabla \cdot \mathbf{v}) \mathbf{U} \right\rangle_q$$

$$\begin{aligned} \frac{\partial T_q}{\partial t} + \langle \mathbf{v} \cdot \nabla T \rangle_q &= \left\langle \frac{(\gamma - 1) dp_o}{\gamma \rho c_p} \frac{dt}{dt} \right\rangle_q + \frac{1}{RePr} \left\langle \frac{\nabla \cdot (\lambda \nabla T)}{\rho c_p} \right\rangle_q - \frac{1}{ReSc} \left\langle \sum_{i=1}^N \frac{c_{p,i}}{c_p} \mathbf{V}_i \cdot \nabla T \right\rangle_q \\ &\quad - Da \left\langle \frac{1}{\rho c_p} \sum_{i=1}^N h_i w_i \right\rangle_q \end{aligned}$$

$$\frac{\partial \langle \rho Y_i \rangle_q}{\partial t} + \nabla \cdot \langle \rho \mathbf{v} Y_i \rangle_q = -\frac{1}{ReSc} \nabla \cdot \langle \rho Y_i \mathbf{V}_i \rangle_q + Da \langle w_i \rangle_q \quad i = 1, \dots, N$$

- Time Integration:
 - Operator-Split reaction-diffusion integration of $(P + 1)(N + 1)$ species and energy eqns
 - Stochastic Projection Method integration of $(P + 1)$ momentum equations

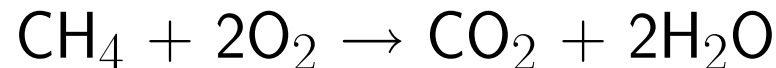
UQ in constant-pressure ignition

N -species, with mass fractions Y_i :

$$\frac{dY_i}{dt} = \frac{w_i}{\rho}, \quad i = 1, \dots, N$$
$$\frac{dT}{dt} = \frac{w_T}{\rho c_p}$$

with $w_T = -\sum_{i=1}^N w_i$ and $w_i = \sum_{k=1}^M \nu_{ik} \mathcal{R}_k$

Example:



Stoichiometric coefficients : $\nu_{ik} = \{1, 2, 1, 2\}$

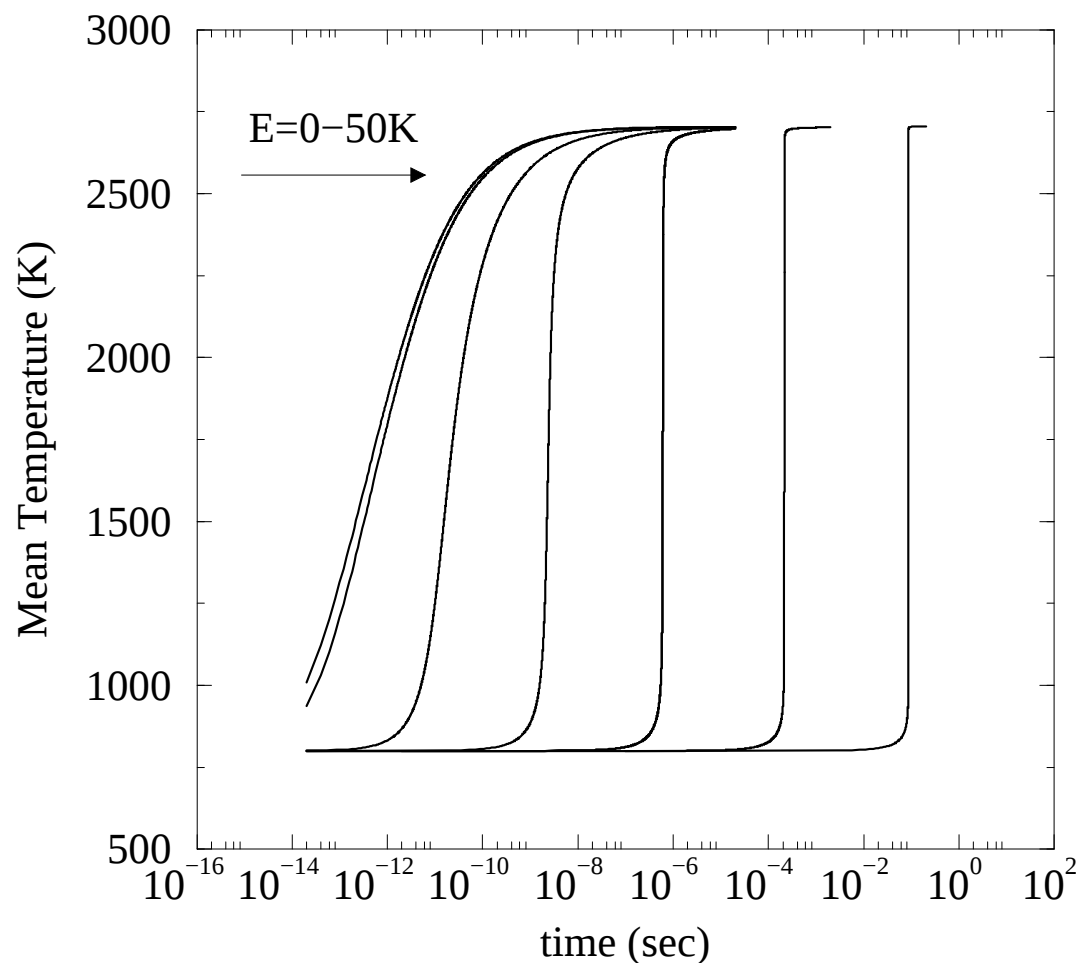
Reaction rate of progress : $\mathcal{R}_k = [\text{CH}_4][\text{O}_2]^2 A_k T^{n_k} e^{-E_k/T}$

- Quantify reaction-rate pre-exponential (A_k) uncertainty with multiplicative factor F_k :

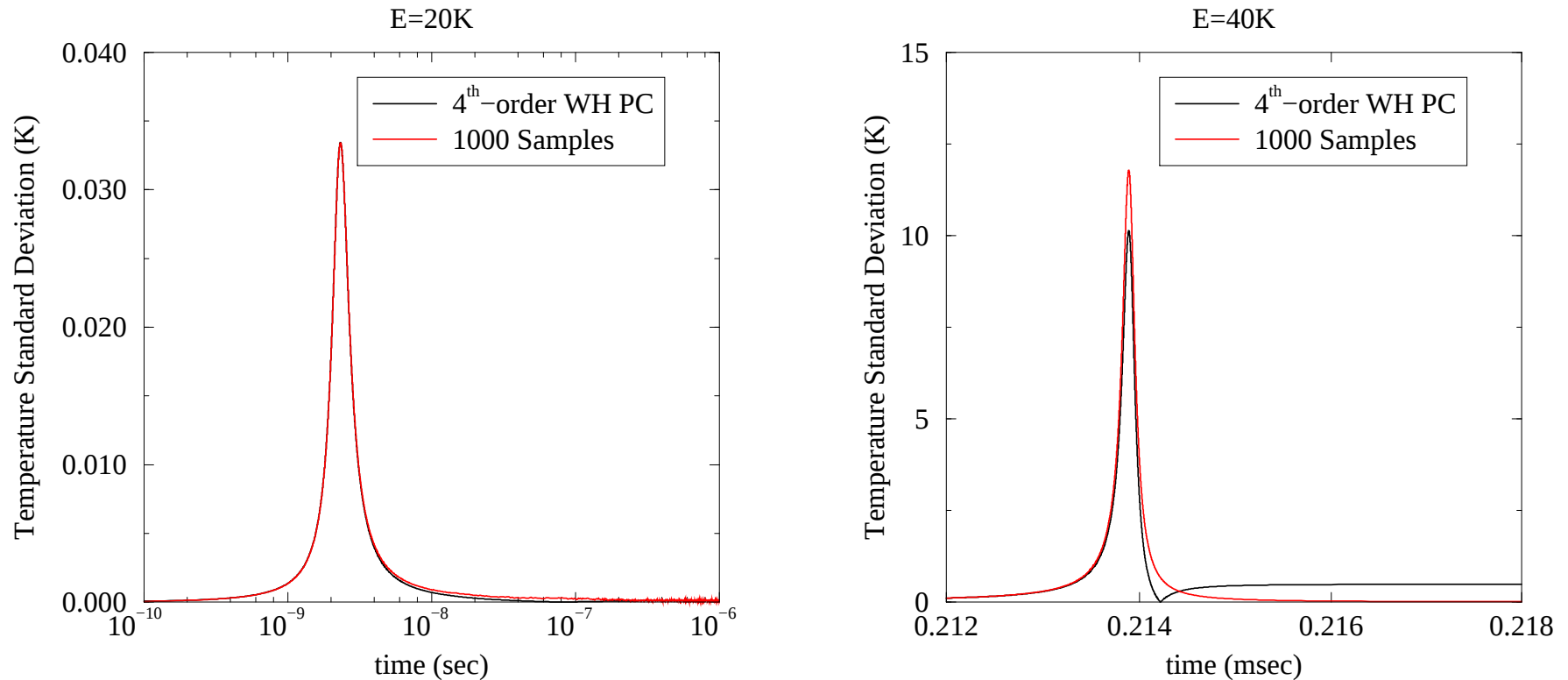
$$P \left(\frac{A_k}{F_k} < A_k < F_k A_k \right) = 0.95$$

Large activation energy (E_k) exponentials lead to very fast changes in species concentrations and temperature

- Methane-air ignition — Global single-step irreversible mechanism
- Initial $T = 800K$
- Stoichiometric
- $p = 1$ atm (constant)

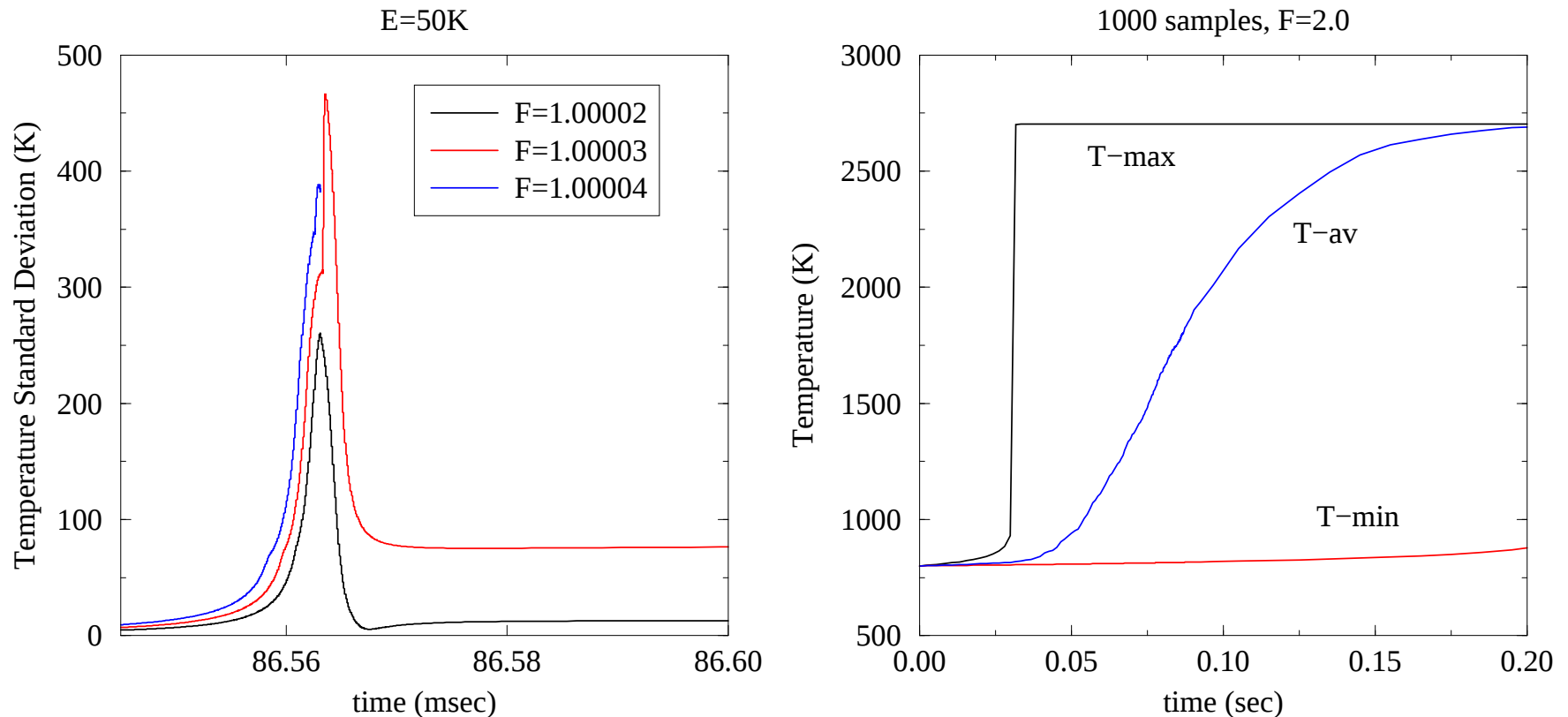


Increased E_k leads to higher peak dT/dt and higher consequence of small uncertainties in reaction rate constants



- $A_k = A_k(\xi)$, 1-D Wiener-Hermite
- PC UQ captures sampled stochastic behavior at low E_k
 - with miniscule uncertainty in A_k ($F = 1.00002$, $\text{COV} = 10^{-5}$).
- Unphysical effects observed at high activation energy

Increasing A_k COV towards minimally-practical levels leads to failed time integration

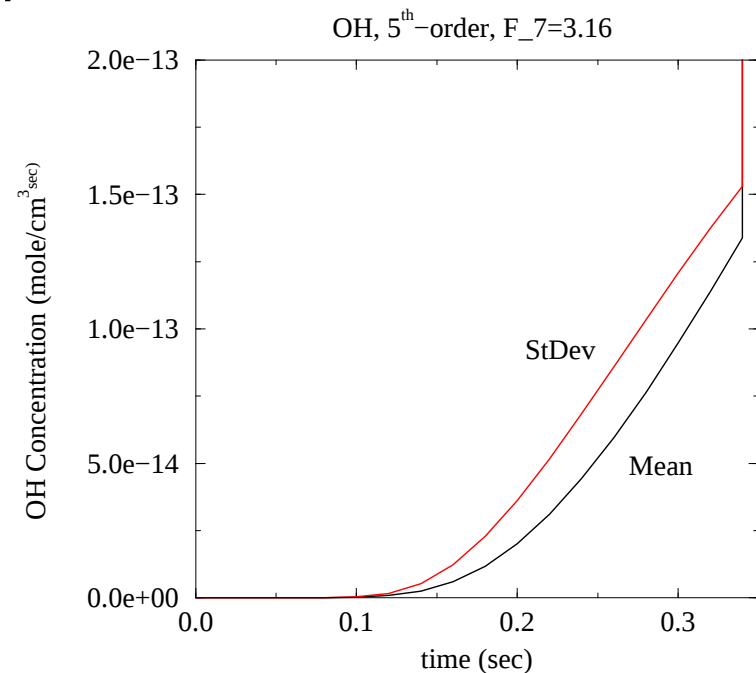


- Unrealistic to expect a WH PC expansion in 1D to capture expected PDFs at realistic reaction-rate parametric uncertainties
- Need increased dimensionality of the PCEs, using multiple ξ 's for each uncertain parameter, for increased accuracy and stability

UQ in constant-pressure isothermal ignition – H₂-O₂ SCWO system

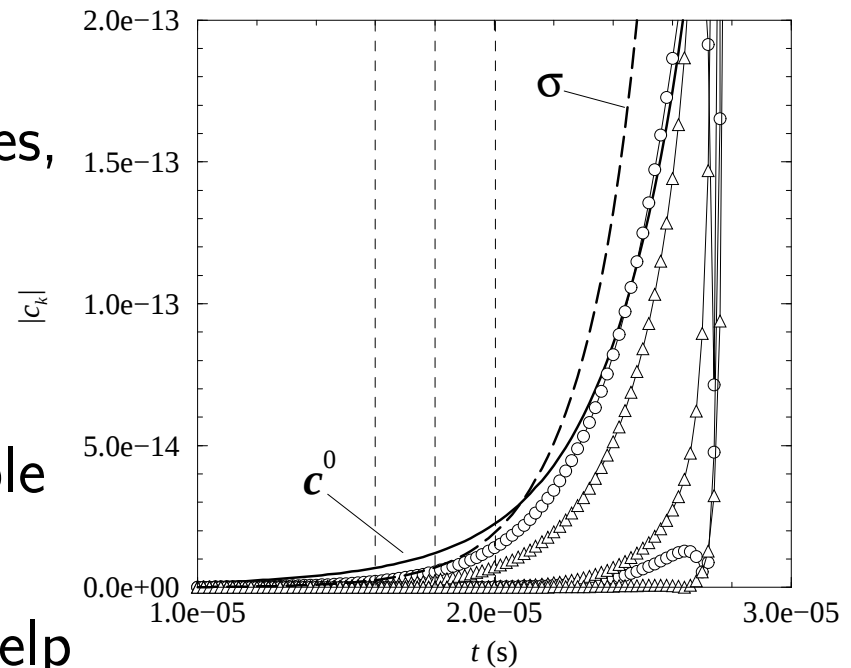
- Using 1D Wiener-Hermite PC, with order P
- Computations stable for small reaction-rate uncertainty
- SCWO with only Rxn-7 uncertain :
 - $P = 1$: stable*
 - $P = 2$: fails for $UF_k \geq 2.55$
 - $P = 3$: stable*
 - $P = 4, 5$: fails for $UF_k \geq 2.23$

*(up to empirical $UF_k = 3.16$)



Experience with Instabilities and Intrusive PC UQ

- Regions of explosive mode growth can lead to instabilities.
- Fast growth of high-order modes, and fast drift of the solution towards unphysical values
- Standard deviation increases significantly, becoming a sizeable fraction of the mean.
- Increasing PC order does not help
- NB. all with fixed PC dimension



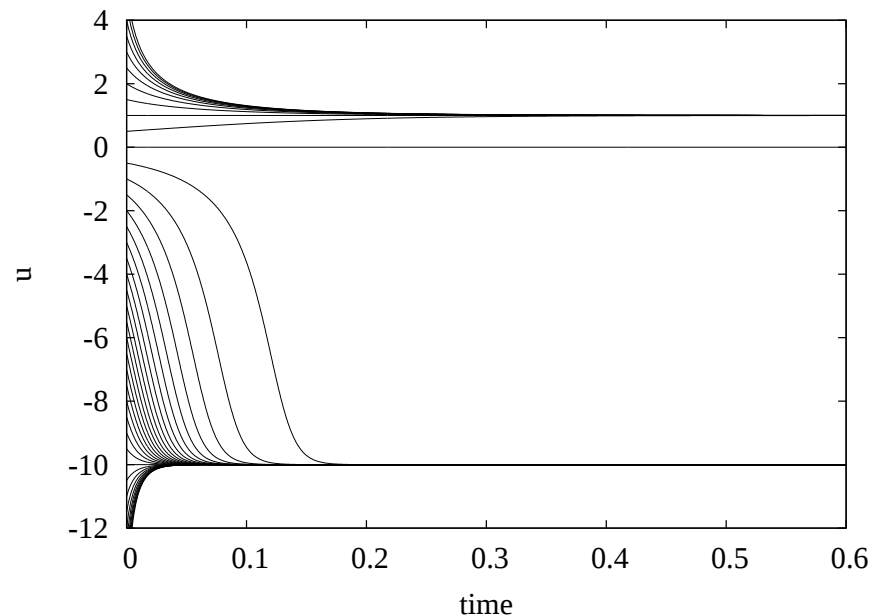
Reagan, Najm, Debusschere, Le Maître,
Knio, and Ghanem, *CTM*, 2004;

Causes of instability in Chemical Systems

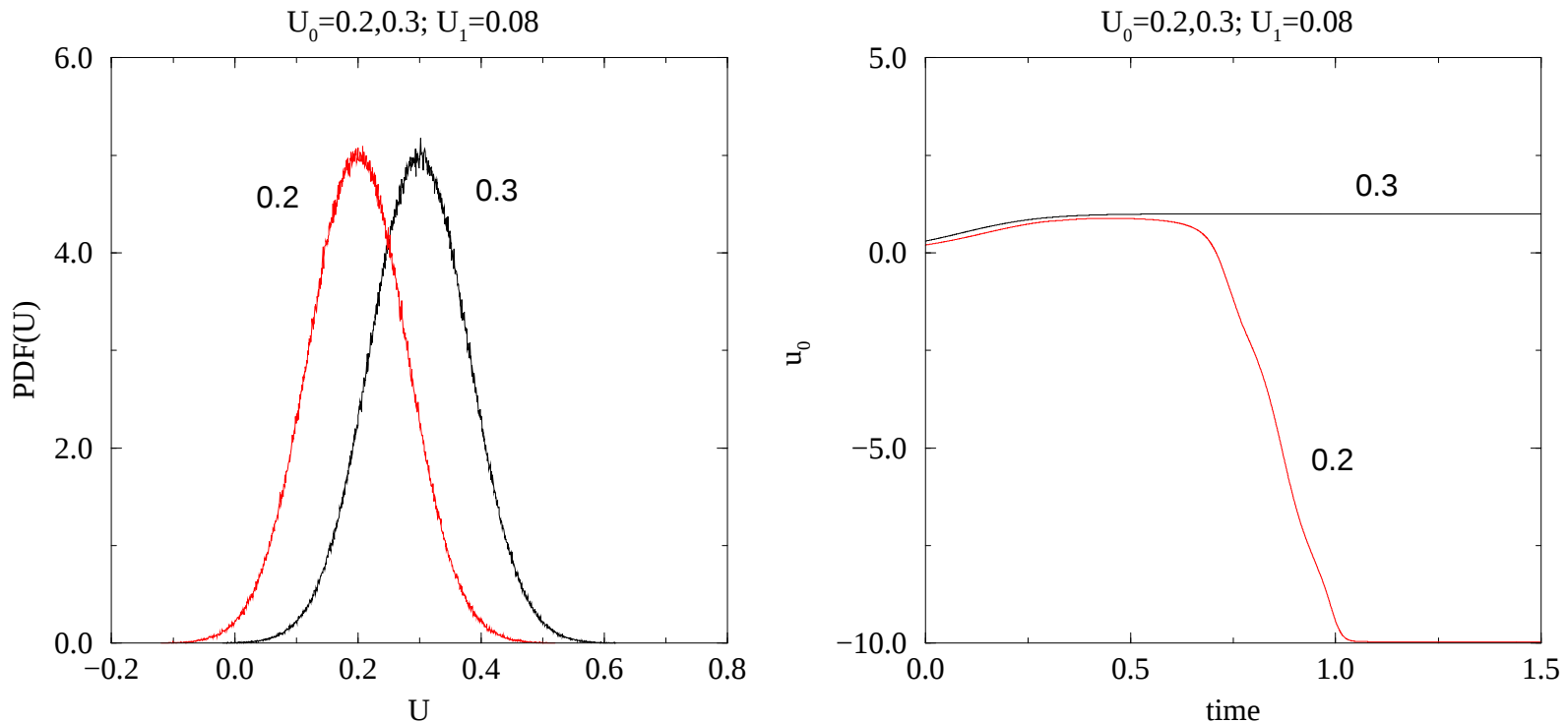
- Gaussian has infinite support
- Finite probability of negative concentrations
 - Cannot satisfy strict positivity
 - Result of finite PC order and fixed PC dimension
- Fails in chemical systems

Model Problem: Bifurcations and Intrusive PC UQ

- Consider a model problem : $\frac{du}{dt} = u(u + 10)(1 - u)$
- Fixed points: attractive: $u = -10, 1$; repulsive: $u = 0$
- Initial condition stochastic: $U = \sum_{k=0}^P U_k \Psi_k$.
- Integrate for $u_k(t)$, $k = 0, \dots, P$



Model Problem: Consequence of Initial PDF tail zero crossing



- $\sigma_U/U_0 > \approx 30\%$ attracts u_0 towards negative region
- Even for low σ_U , increasing PC order leads to similar drift
- Similar behavior for Gaussian or Lognormal initial condition
- Similarly with Laguerre polynomial/Gamma distribution basis

Challenges with the use of a Global PC Basis for Intrusive UQ

- Global PC expansion with N -th order polynomial will have N roots/zero-crossings in general
- Representing a RV with a global PC expansion (over all ξ)
 - with fixed dimensionality and order
 - will 'sample' both positive and negative u -realizations
 - irrespective of $\text{PDF}(u)$
- Fails when strict positivity is necessary for stability
 - e.g. reaction rate constants, concentrations, temp
- Possible remedies with appropriate filtering strategies
- Eval local low order basis vs. the global high order approach
 - Wavelets, Multi-Resolution Analysis

Le Maître *et al.*, *J. Comp. Phys.*, 197, 28-57, 2004
Le Maître *et al.*, *J. Comp. Phys.*, 197, 502-531, 2004

Uncertainty Quantification with Multiwavelets

- An uncertain field quantity $u(\mathbf{x}, t, \theta)$ is expressed using PC

$$u = \sum_{k=0}^P u_k(\mathbf{x}, t) \Psi_k(\xi_1, \dots, \xi_N)$$

- Introduce $\zeta_i = p(\xi_i)$: CDF of ξ_i , where ζ_i is on $[0,1]$

$$u = g(\xi_1, \dots, \xi_N) = f(\zeta_1, \dots, \zeta_N)$$

- Represent $f(\zeta)$ using N -D multiwavelets (Alpert, 1993)

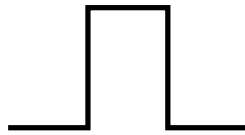
$$u = \sum_{\lambda=0}^Q \tilde{u}_\lambda(\mathbf{x}, t) \mathcal{W}_\lambda(\zeta_1, \dots, \zeta_N)$$

Le Maître, Ghanem, Knio, and Najm, *J. Comp. Phys.*, 197:28-57 (2004)

Le Maître, Najm, Ghanem, and Knio, *J. Comp. Phys.*, 197:502-531 (2004)

Haar-Wavelets

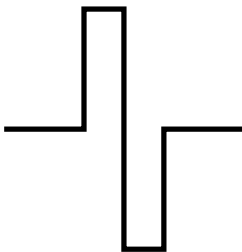
Haar scaling functions

$$\phi^w(y) = \begin{cases} 1, & 0 \leq y < 1 \\ 0 & \text{otherwise} \end{cases}$$


Scaled Haar functions, scaling factor j , and sliding factor k ,

$$\phi_{jk}^w(y) = 2^{j/2} \phi^w(2^j y - k)$$

Haar function (mother wavelet)

$$\psi^w(y) \equiv \frac{1}{\sqrt{2}} \phi_{1,0}^w(y) - \frac{1}{\sqrt{2}} \phi_{1,1}^w(y) = \begin{cases} 1, & 0 \leq y < \frac{1}{2}, \\ -1, & \frac{1}{2} \leq y < 1, \\ 0, & \text{otherwise.} \end{cases}$$


Wavelet family

$$\psi_{j,k}^w(y) = 2^{j/2} \psi^w(2^j y - k), \quad j = 0, 1, \dots \text{ and } k = 0, \dots, 2^j - 1$$

Wiener-Haar Construction

The set of $\psi_{j,k}^w(y)$ is an orthonormal system

Any function $f \in L^2([0, 1])$ can be arbitrarily well approximated by the sum of its mean and a finite linear combination of the $\psi_{j,k}^w(y)$.

The wavelet set $W_{j,k}(\xi(\theta)) \equiv \psi_{j,k}^w(p(\xi))$ forms a basis for the space of L^2 random processes.

$$X(\xi(\theta)) = X_o + \sum_{j=0}^{\infty} \sum_{k=0}^{2^j-1} X_{j,k}^w \psi_{j,k}^w(p(\xi)) = \sum_{\lambda} X_{\lambda} W_{\lambda}(\xi(\theta))$$

Multidimensional $\{\xi_1, \xi_2, \dots, \xi_N\}$,

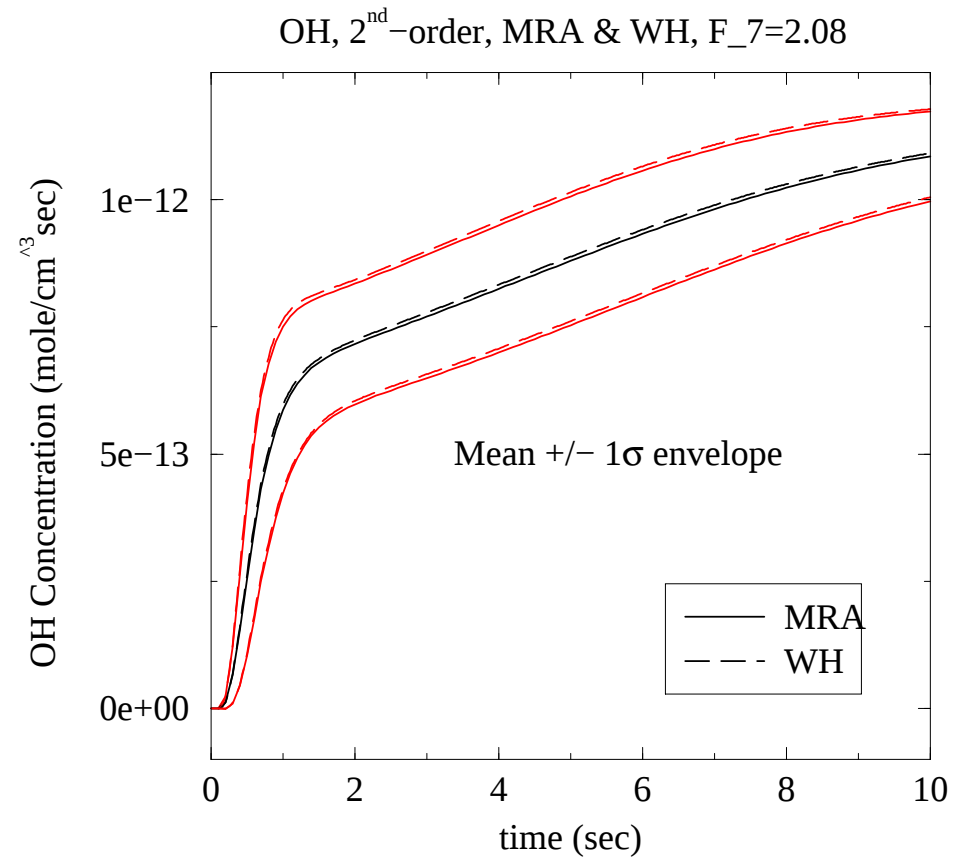
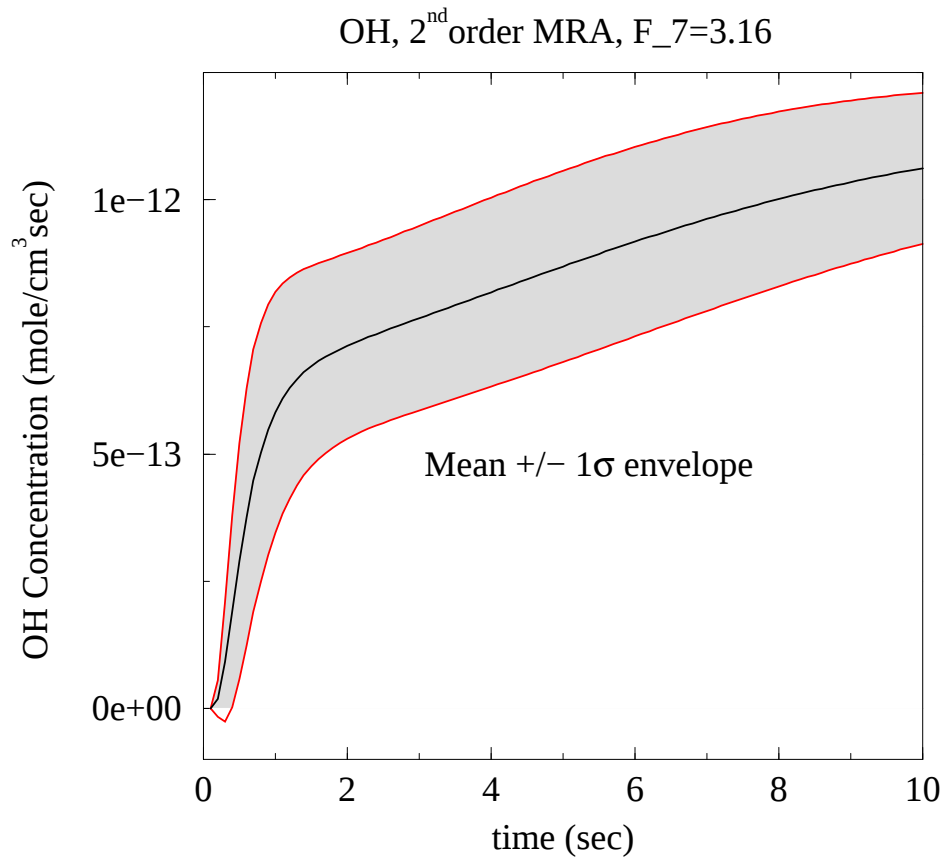
$$\mathcal{W} = \prod_{k=1}^N W_{\lambda_k}(\xi_k)$$

Multidimensional Multiwavelet Construction

- Wiener-Haar PC able to represent uncertainty in systems exhibiting bifurcations depending on parameter values
- Poor convergence relative to PC constructions with smooth global bases on smooth functions
- Use multiwavelet construction (Alpert, 1993) employing higher order polynomials instead of the Haar-functions
- For efficient multidimensional construction, use
 - Block-decomposition of the stochastic space
 - A local MW construction on each block employing
 - Scaled Legendre polynomials on $[0, 1]$
 - First level Multiwavelet details
 - Adaptive resolution in each dimension on each block

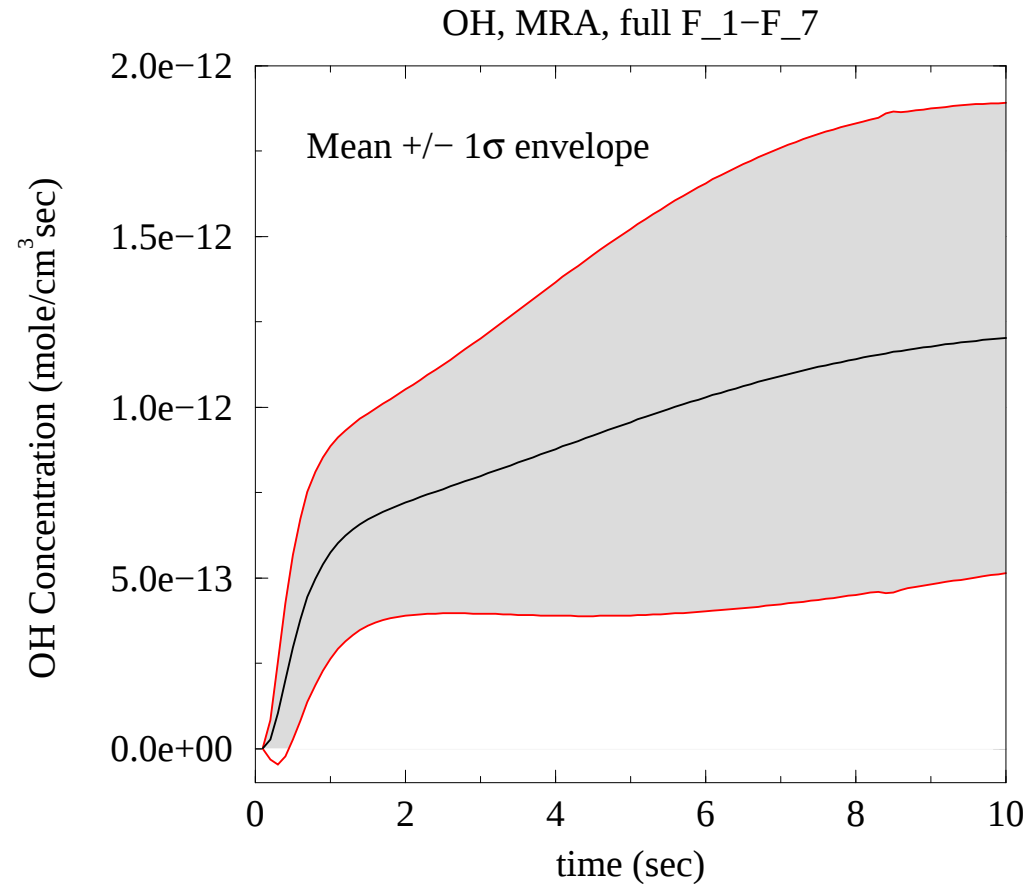
UQ in constant-pressure isothermal ignition — MRA

- $\text{H}_2\text{-O}_2$ SCWO with only Rxn-7 uncertain ($F_7 = 3.16$)



UQ in constant-pressure isothermal ignition — MRA

- $\text{H}_2\text{-O}_2$ supercritical water oxidation model
- Empirically-based uncertainty in all 7 reactions
- Adaptive refinement of MW block decomposition in each dimension



Le Maître, Najm, Pébay, Ghanem, and Knio,
SIAM J. Sci. Comp., 22(2):864-889, 2007

Conclusions

- Non-intrusive Spectral UQ
 - PC-construction enables extraction of sensitivities
 - Quadrature and cubature to reduce no. of samples
- Intrusive Spectral UQ in reacting flow
 - Global basis OK for weakly non-linear systems
 - Potential utility of multiple ξ 's per uncertain parameter
 - Adaptive multiwavelet MRA construction
 - Accuracy, robustness, and efficiency demonstrated on a number of model problems
 - Resolves global PC difficulties
 - Demonstration in exothermic ignition and flames in progress

Prospects

- Cubature methods for efficient evaluation of high dimensional integrals
- Adaptive general multiwavelet solution of non-linear systems
- Challenges
 - Convection
 - Limit-cycle and chaotic systems
 - Dimensionality