

Parametric Study of PV Arc-Fault Generation Methods and Analysis of Conducted DC Spectrum

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Arc-Fault Codes and Standards

- *National Electrical Code® (NEC) 690.11*
 - 2011 *NEC* requires arc-fault mitigation for PV systems on/penetrating a building
 - 2014 *NEC* requires arc-fault mitigation for all PV systems

- Arc-fault circuit interrupters are listed using Underwriters Laboratories (UL) 1699B, *“Outline of Investigation for Photovoltaic (PV) DC Arc-Fault Circuit Protection”*
 - Not a standard yet! Needs to be improved and voted on by the UL Standards Technical Panel (STP) first.
 - To move UL 1699B to a certification standard, the outline of investigation must be improved.
 - The Sept 2013 STP meeting identified the following areas for development:
 - Arc-fault testing parameters (e.g., inclusion of ballast resistors, capacitors, etc.)
 - DC power supplies for PV simulation
 - Unwanted tripping tests
 - **Arc generation methods**

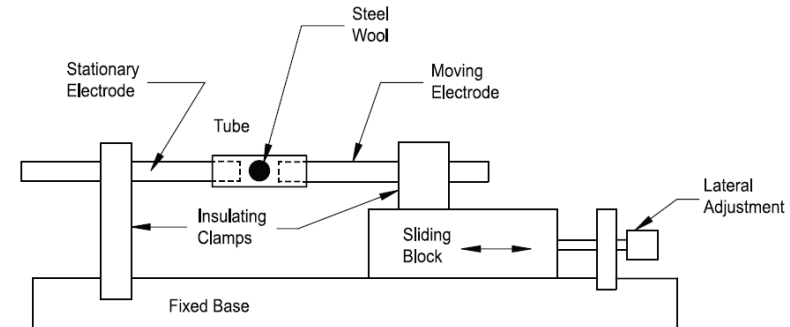
Arc Generation Research Goals

- Determining the most repeatable, 'worst case' tests for adoption by the UL 1699B STP

- The ideal UL 1699B arc-fault generation method:
 - reduces experimental setup complexity
 - improves testing repeatability
 - minimizes arc-fault radio frequency (RF) noise because this is how many arc-fault detectors identify a fault

Arc-fault generation in UL 1699B

- Currently UL 1699B requires the arc to be created with a tuft of steel wool between the ¼" Cu electrodes
- Electrodes are set to a fixed gap
- 4 tests are required with arc powers between 300-900 W



Arc Powers

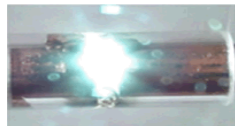
Trip Times

Arcing current (amps) ^{a, d}	Arcing voltage ^b (volts)	Average Arcing Watts ^a	Approximate electrode, inches (mm) ^b	Max time (sec) ^c
7	43	300	1/16 (1.6)	2
7	71	500	3/16 (4.8)	1.5
14	46	650	1/8 (3.2)	1.2
14	64	900	1/4 (6.4)	0.8

Alternative arc-fault generation methods

The following variables were parameterized:

**Arc
Power**

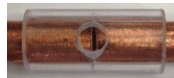


100 W

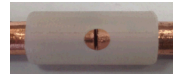


300 W

**Sheath
Material**



Polycarbonate



PET

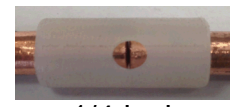


Nylon 6,6

**Electrode
Diameter**

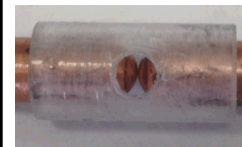


1/8 inch

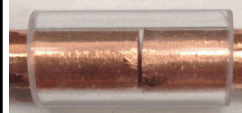


1/4 inch

**Electrode
Tip**

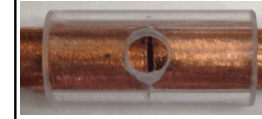


Rounded Tip

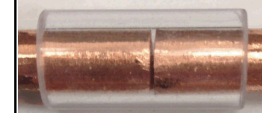


Flat Tip

**Hole for
O₂ Ingress**



Hole



No Hole

**Steel Wool
Igniter**



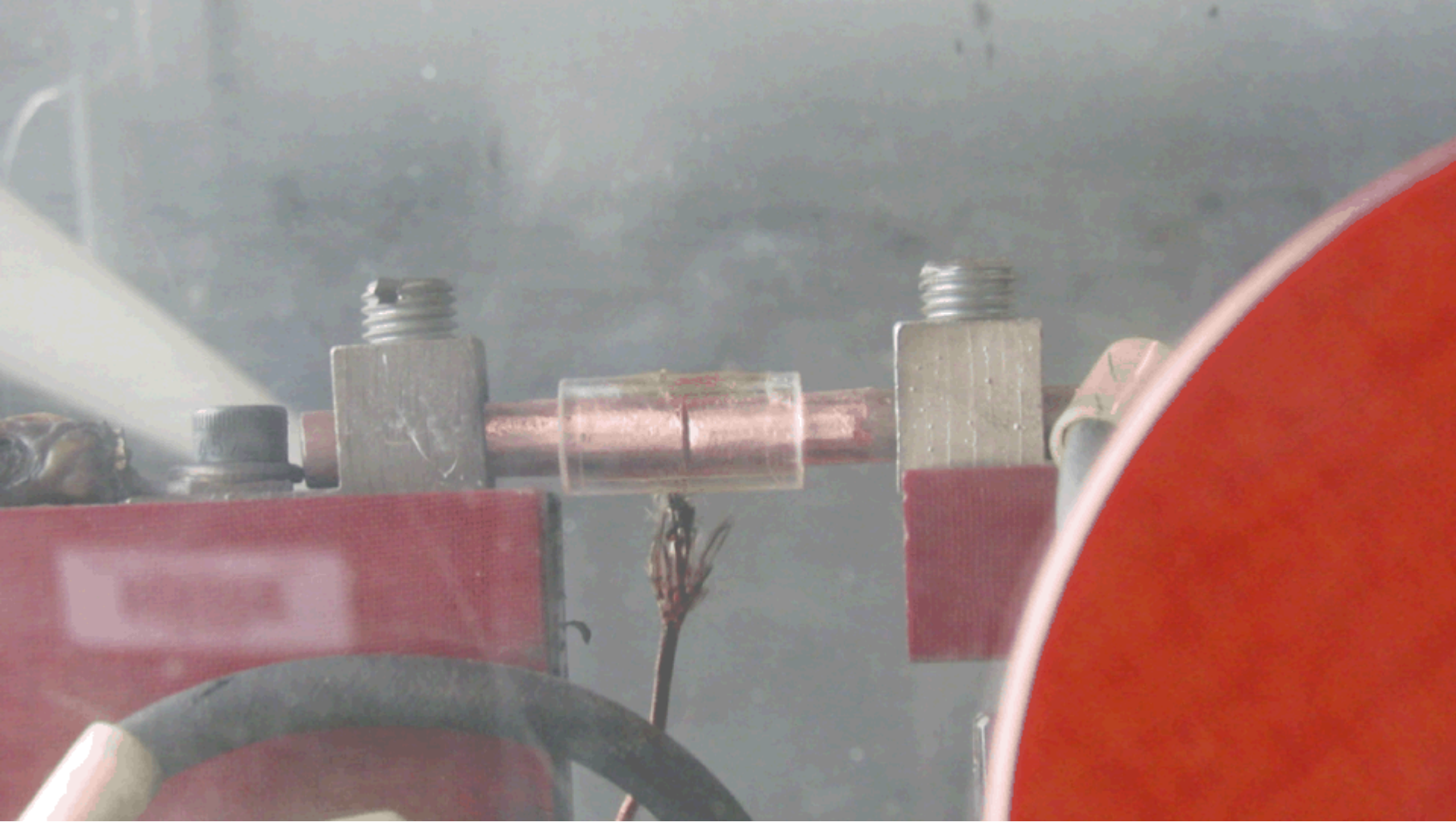
Steel Wool



No Steel Wool

Test Number	Arc Power	Polymer	Electrode Diameter	Electrode Tip	Hole	Steel Wool
1 (UL 1699B)	300 W	Polycarbonate	1/4"	Flat	No	Yes
2	300 W	Polycarbonate	1/4"	Flat	Yes	Yes
3	300 W	Polycarbonate	1/4"	Flat	No	No
4	300 W	Polycarbonate	1/4"	Flat	Yes	No
5	300 W	PET	1/4"	Flat	Yes	No
6	300 W	Nylon 6,6	1/4"	Flat	Yes	No
7	100 W	Polycarbonate	1/4"	Flat	No	No
8	100 W	Polycarbonate	1/4"	Flat	Yes	No
9	100 W	Nylon 6,6	1/4"	Flat	No	No
10	100 W	Nylon 6,6	1/4"	Flat	Yes	No
11	100 W	PET	1/4"	Flat	No	No
12	100 W	PET	1/4"	Flat	Yes	No
13	100 W	Polycarbonate	1/4"	Round	Yes	No
14	100 W	Polycarbonate	1/8"	Flat	Yes	No
15	100 W	PET	1/8"	Flat	Yes	No
16	100 W	Nylon 6,6	1/8"	Flat	Yes	No
17	300 W	Polycarbonate	1/8"	Flat	Yes	No

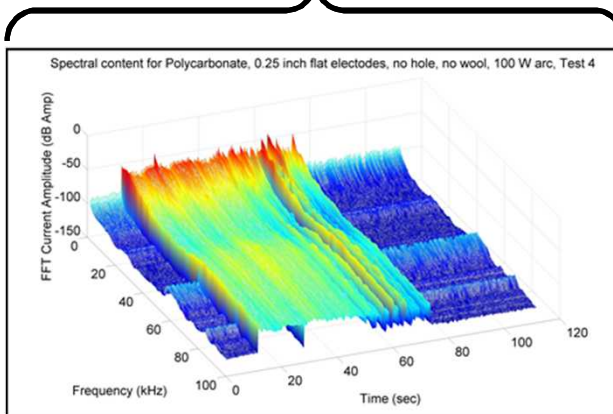
Videos of Arc-fault Tests



Arc-fault Noise Signatures

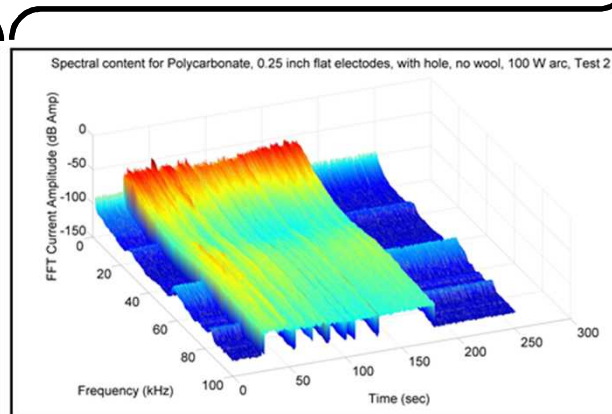
- Discrete Fourier Transforms (DFTs) of the DC current during the arc-fault tests were saved at a rate of ~ 0.28 DFTs/sec.
- Arc stability and polymer pyrolyzation determine arc-fault noise patterns
 - If liquid polymer, steel wool, or copper dust from electrode enter plasma stream the arc can flicker or self-extinguish
 - Only the first 2 seconds are of importance because the AFCI must trip by that point to pass UL 1699B.

No Hole

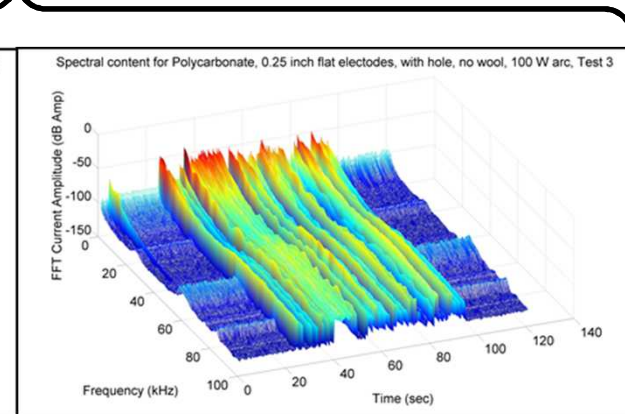


Stable Arc-Fault until $t = \sim 60$ s

Identical Tests with Hole



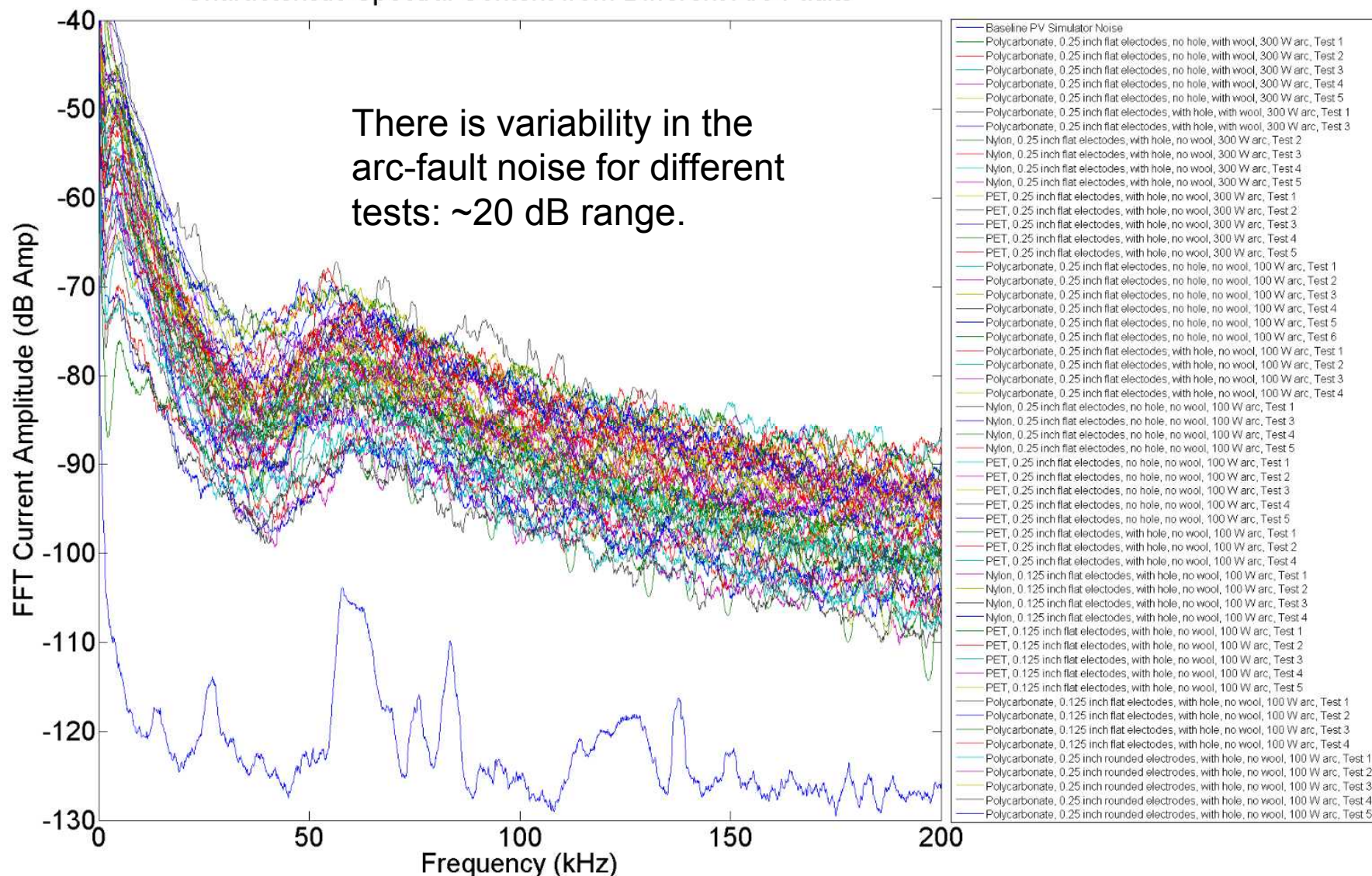
Stable Arc-Fault



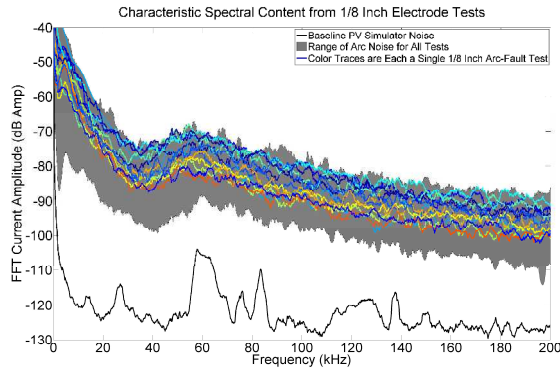
Less Stable Arc-Fault

Arc-Fault Noise at *Initiation*

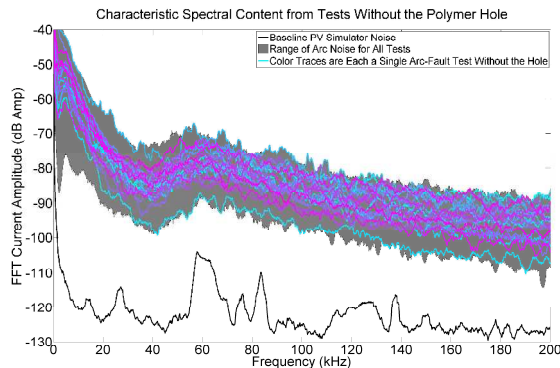
Characteristic Spectral Content from Different Arc-Faults



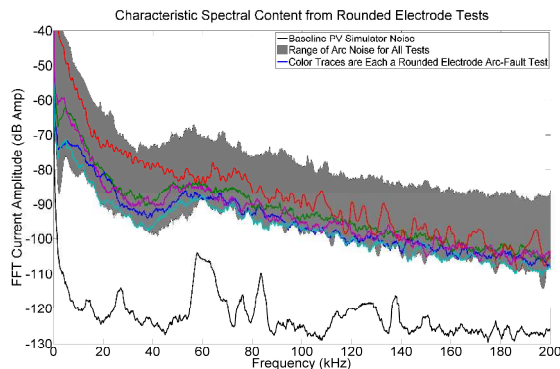
Factors for Noise Generation



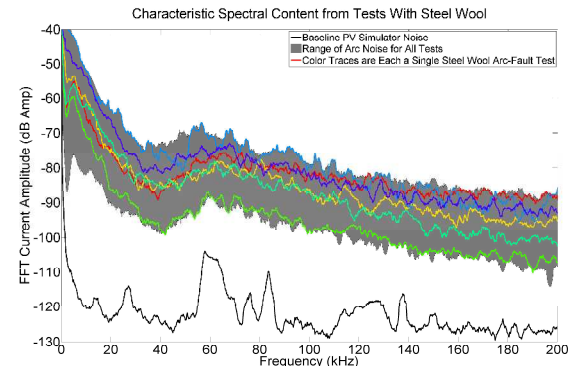
Smaller electrodes produce high noise signatures due to increased off-gassing rates and oxygen depletion.



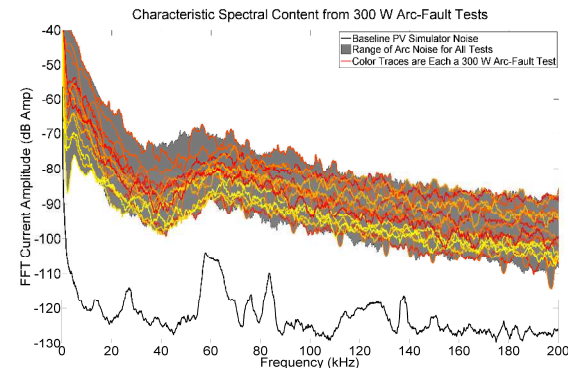
Holes produced slightly cleaner burning arc-faults, possibly because of the increased presence of oxygen.



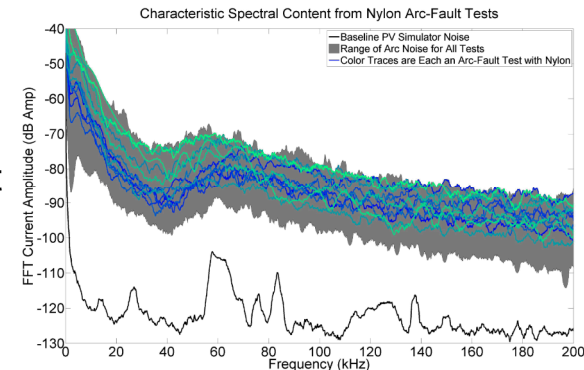
Rounded electrodes tend to produce less arc-fault noise because the arc-fault is 'cleanly' established at the center of the electrodes.



Steel wool tests had a large noise range but the wool tended to produce signatures toward the upper end of the spectral band.



Higher power arc-faults tend to create more stable, cleaner burning, *slightly* less noisy arcs.



Arc-faults with Nylon 6,6 created more noise than the polycarbonate and PET tests.

Conclusions

- A parametric study of various geometries, materials, and powers was conducted to determine repeatable arc-fault certification tests for UL 1699B.
- Frequency-based arc-fault detection would be the most difficult with the following:
 - Larger (1/4") diameter electrodes. Plus 1/8" tend to melt and weld at 300 W.
 - "Pull-apart" generation method (no steel wool) . This is also more repeatable than using steel wool.
 - A hole in polymer sheath. More setup time, but arcing is more consistent and repeatable.
 - Rounded electrode tips. Not recommended because the machining time is onerous for test operator.
 - 300 W power. Hard to tell, but it may have slightly less conducted noise.
- A 100 W arc-fault test has been recommended by the UL 1699B Arc Generator Task Group because low power arcs cause fires and AFCIs using time-based methods would have difficulty with this scenario. (Frequency-based methods would not.)
 - To establish low power arcs, the pull apart method is most consistent. To compensate for the variability in operator-selected gap sizes, a $\pm 30\%$ arc power tolerance is recommended.
 - A hole will be allowed for more consistent arcing.
 - Flat electrodes are preferred because creating rounded-tip electrodes with tight tolerances is difficult.
- Stay tuned for 1699B changes after the Sept 2014 STP meeting!

Acknowledgements

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Questions?