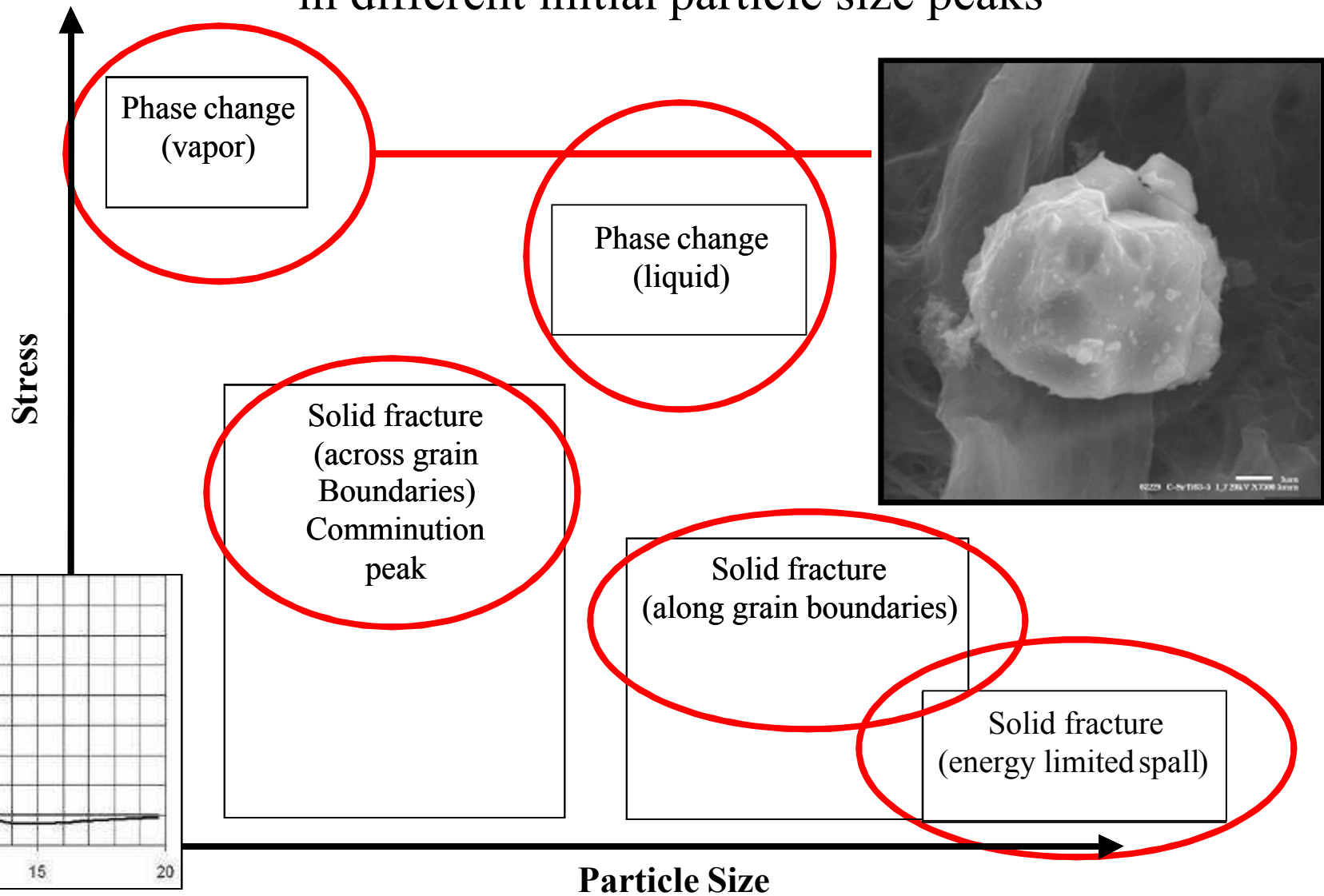


# **Radiological Dispersal Devices: Physically Based Dispersal Characteristics and Limitations**

Fred Harper  
Sandia National Laboratories

# Different stress induced mechanisms result in different initial particle size peaks



Final size distribution can be a combination of several of these Peaks and can be modified by combustion and agglomeration

# Priority Nuclides

Nuclide (Half life)	Large source size (Ci)	Typical source size (Ci)	Dominant physical form
Cs-137 (30 years)	250000	5000 - 10000	CsCl
Co-60 (5 years)	300000	1000 - 5000	Co metal (slugs and pellets)
Sr-90 (30 years)	300000	40000 - 100000	SrTiO <sub>3</sub> (ceramic)
Ir-192 (74 days)	100s	10 - 1000	Ir metal
Am-241 (432 years)	10s	10 - 20	AmO <sub>2</sub> in pressed powder form

# Point to make – varied particle/fragment sizes

- Will divide problem up into:
  - Respirable particles ( $< 10\text{ }\mu\text{m}$  aerodynamic) – I know it is an oversimplification
  - Intermediate size particles ( $> 10\text{ }\mu\text{m}$   $100\text{ }\mu\text{m}$ )
  - Large particles ( $> 100\text{ }\mu\text{m}$ ,  $< 500\text{ }\mu\text{m}$ )
  - Fragments ( $> 500\text{ }\mu\text{m}$ )
- All forms produce all sizes – relative fractions depend on material properties and device geometry

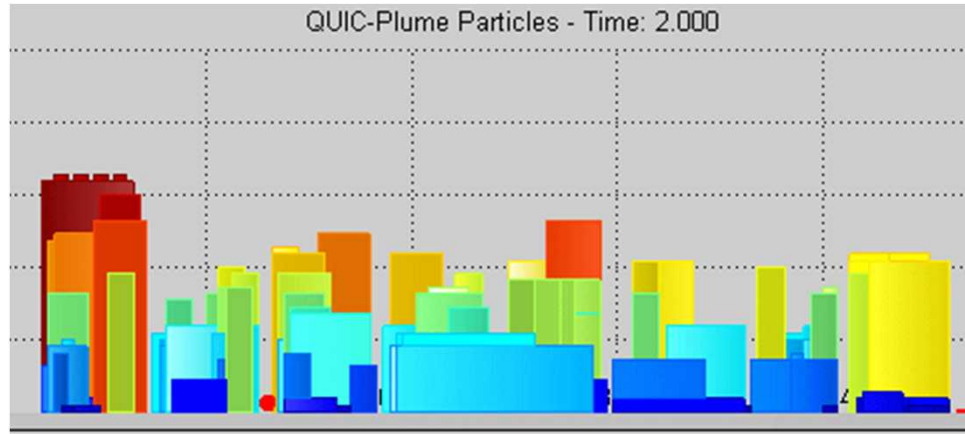
# Some basic concepts

- Small particles ( $< 10 \mu\text{m}$ ) -- primarily an inhalation problem, but can also be a shine problem
- Large particles ( $> 100 \mu\text{m}$  – primarily a shine problem)
- To be an inhalation problem, particles must be in the vicinity of people
- Will divide problem into small particles ( $< 10 \mu\text{m}$ ), intermediate particles ( $> 10 \mu\text{m}$ ,  $< 100 \mu\text{m}$ ), and larger particles ( $> 100 \mu\text{m}$ ,  $< 500 \mu\text{m}$ ), and fragments ( $> 500 \mu\text{m}$ )

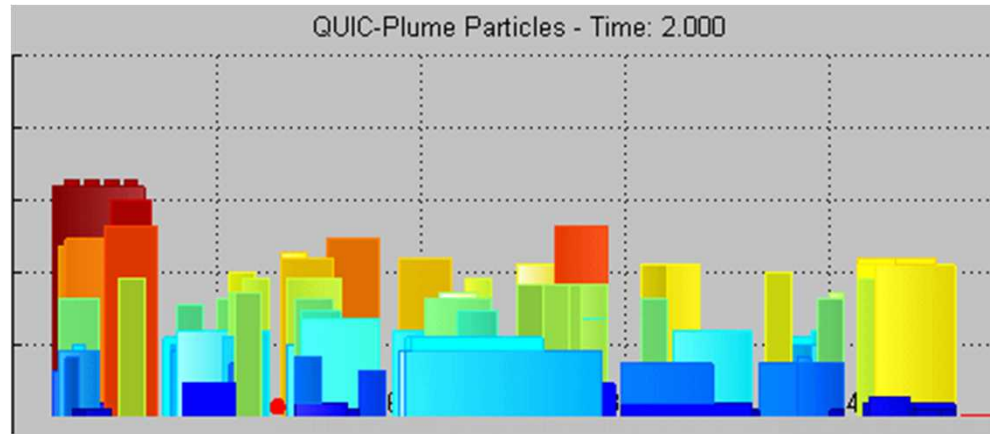
# Particle Size Effect From Mike Brown (LANL)

## Transport & Dispersion

5 micron particles



250 micron particles

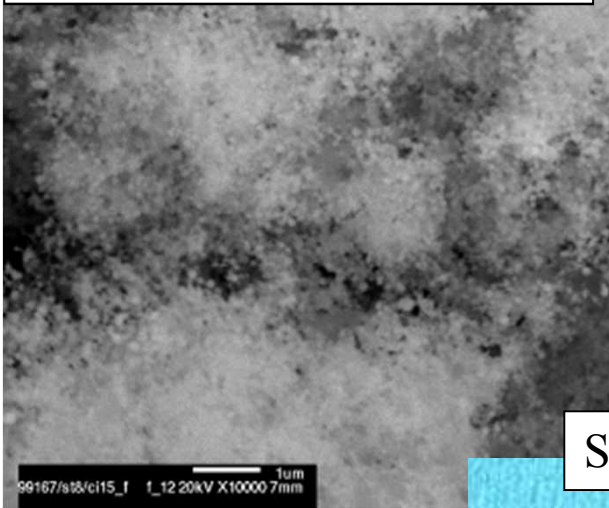


Applications

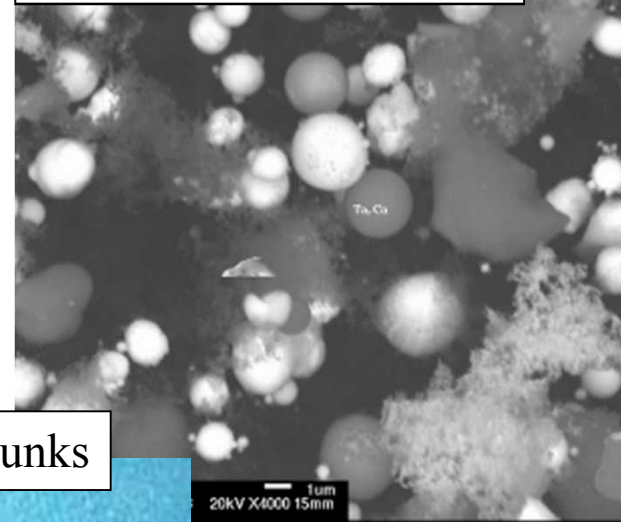
5 micron particles lofted high into the air, 250 micron particles settle towards ground

# Phenomena: Explosive aerosolization of metals

Shock sublimation of metals  
→ particles  $< 1\ \mu\text{m}$



Shock melting of metals  
→ particles  $< 10\ \mu\text{m}$



Solid fracture → chunks

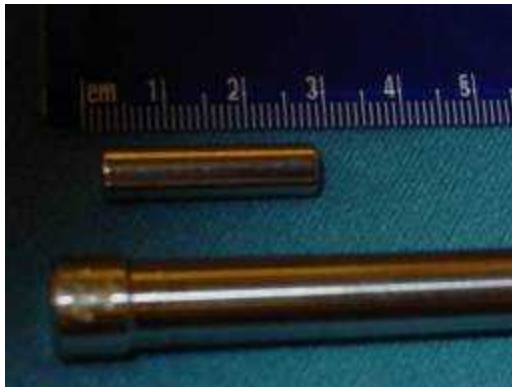
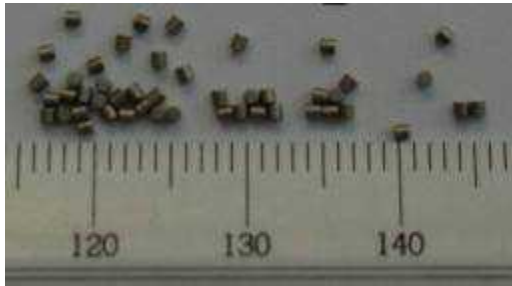


1000 Ci (20 g) Co pellet

- Fractions depend on material properties and device geometries
- Respirable aerosol ranged from .2 % to 80 %
- Very little aerosol generated between  $30\ \mu\text{m}$  and  $200\ \mu\text{m}$

# Materials of concern: Cobalt-60

- Half life: 5.27 years
- Gamma emitter
- Typical Form: Co metal (pellets or slugs)



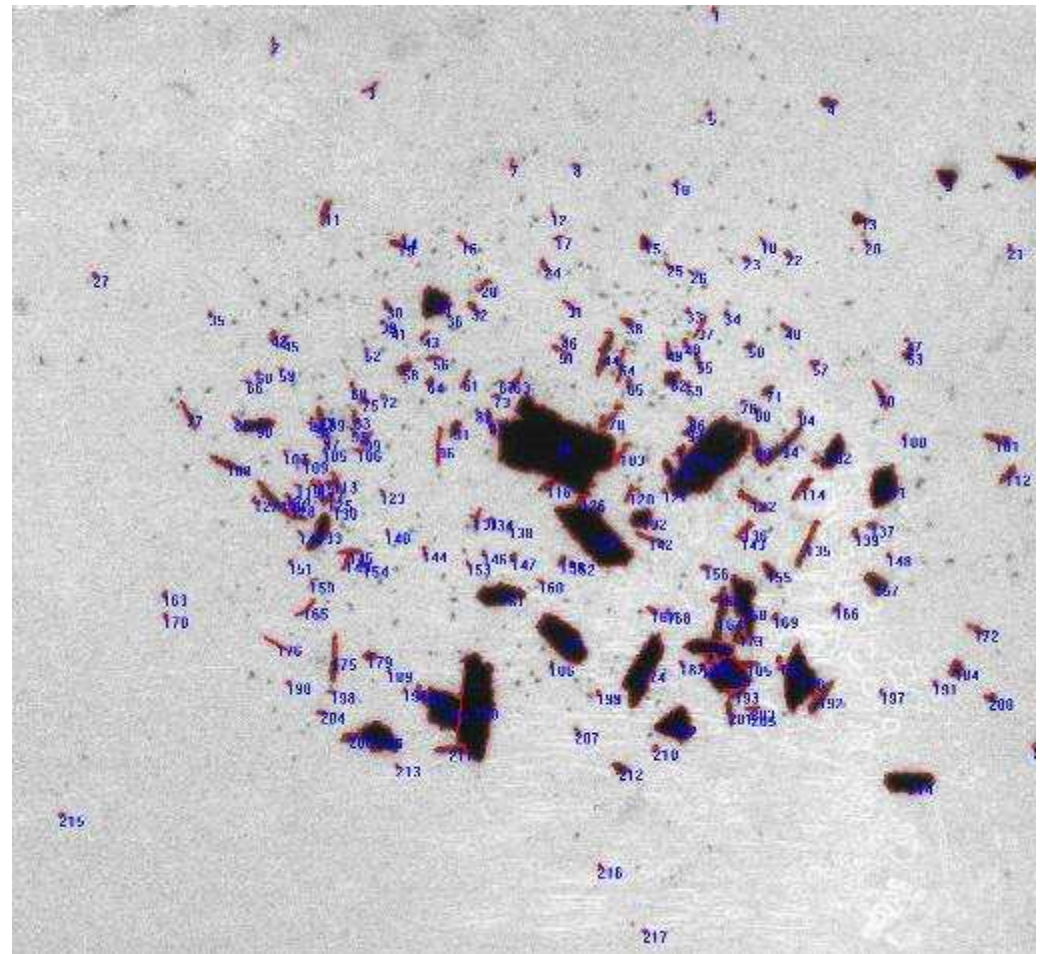
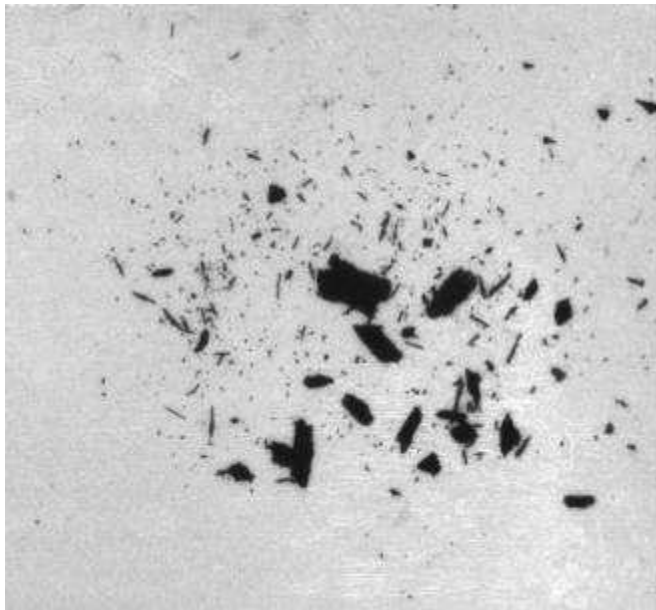
Typical Uses	Activity (Ci)		
	Min	Max	Typical
Irradiators: Sterilization	5k	15M	4M
Irradiators: Self shielded	1.5k	50k	25k
Irradiators: Blood/Tissue	1.5k	3k	2.4k
Gamma knife	4k	10k	7k
Teletherapy	1k	15k	4k
Industrial radiography	11	200	60
Brachytherapy	5	20	10
Various industrial gauges	0.1	10	2



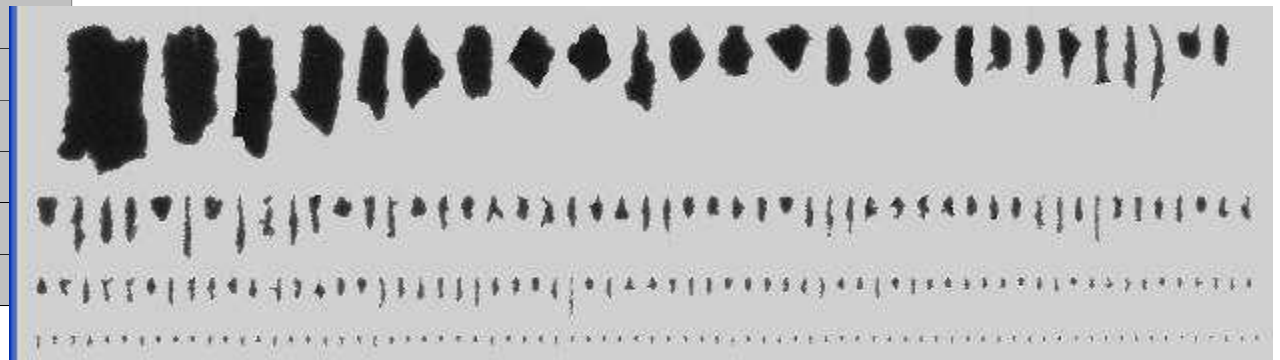
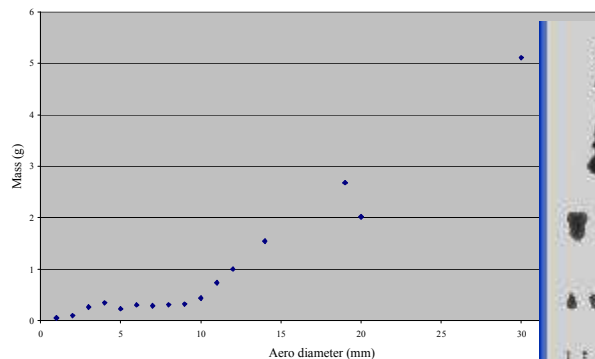
## Ballistic/fragmentation studies on irradiator slugs



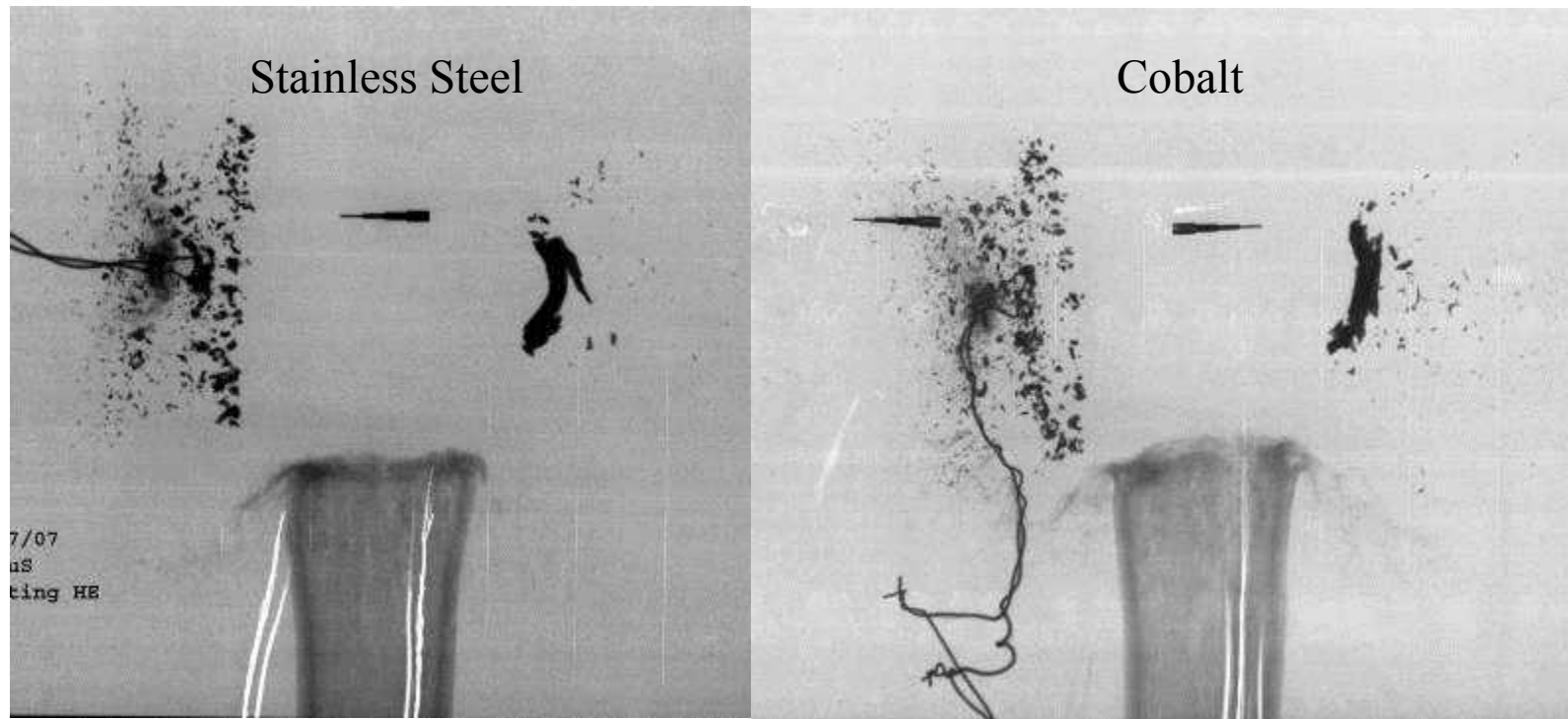
Photometric analysis of cobalt fragmentation – 90 % of mass in 20 frags out of about 200 – smallest frag about 1 mm (aero diameter)



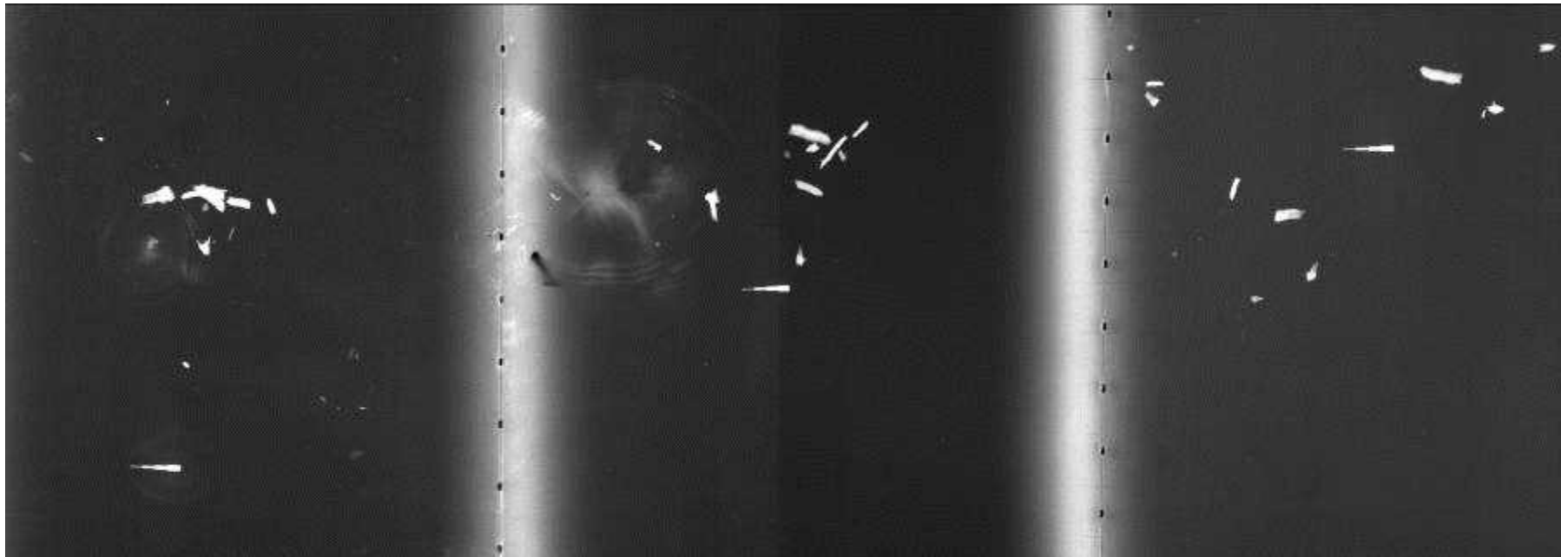
Mass vs diameter (Co Fragments)



# Comparison between stainless steel slug fragmentation and Nordion cobalt slug fragmentation



# Observed range of velocities from 3 exposure shot (419 – 580 m/s)





# Materials of concern: Iridium-192

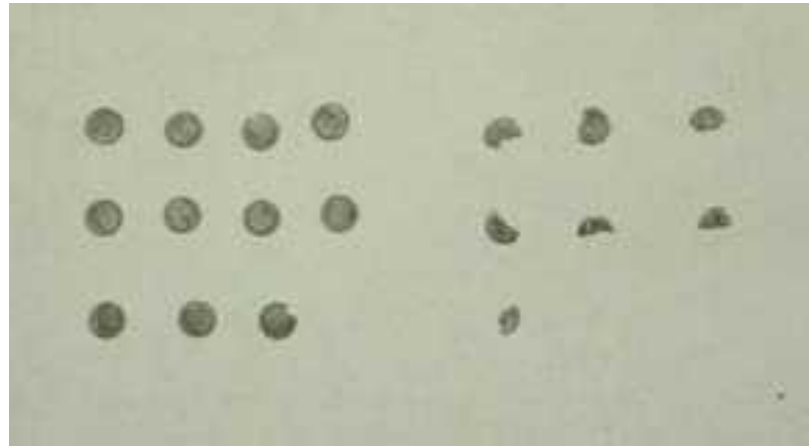
- Half life: 73.8 days
- Gamma emitter
- Typical Form: Ir metal pellets or wire



Typical Uses	Activity (Ci)		
	Min	Max	Typical
Industrial radiography	5	200	100
Brachytherapy	5	20	10



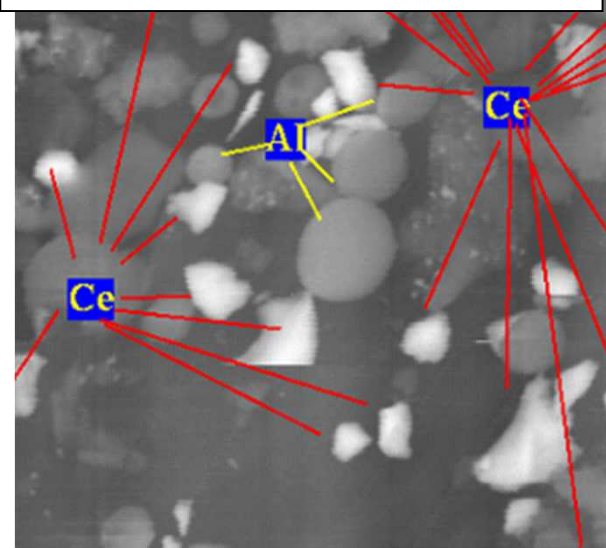
# Iridium fragmentation/aerosolization experiments



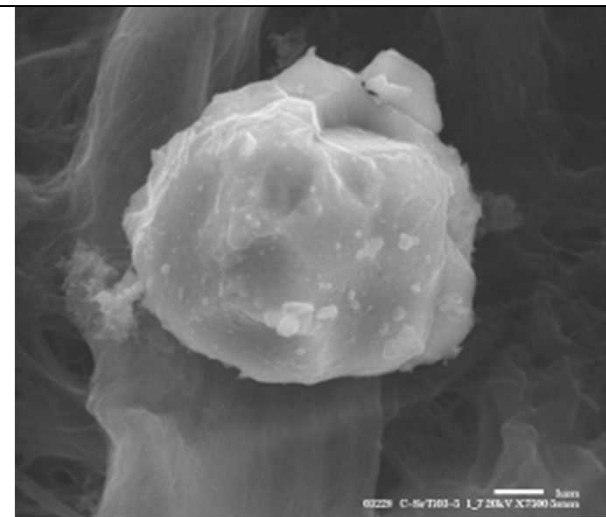
# Phenomena: Explosive aerosolization of ceramics

- Fractions depend on material properties and device geometries
- Respirable aerosol ranged from 2 % to 40 %
- No phase change
- A lot of aerosol generated between 30  $\mu\text{m}$  and 200  $\mu\text{m}$

Aerosol produced from shear

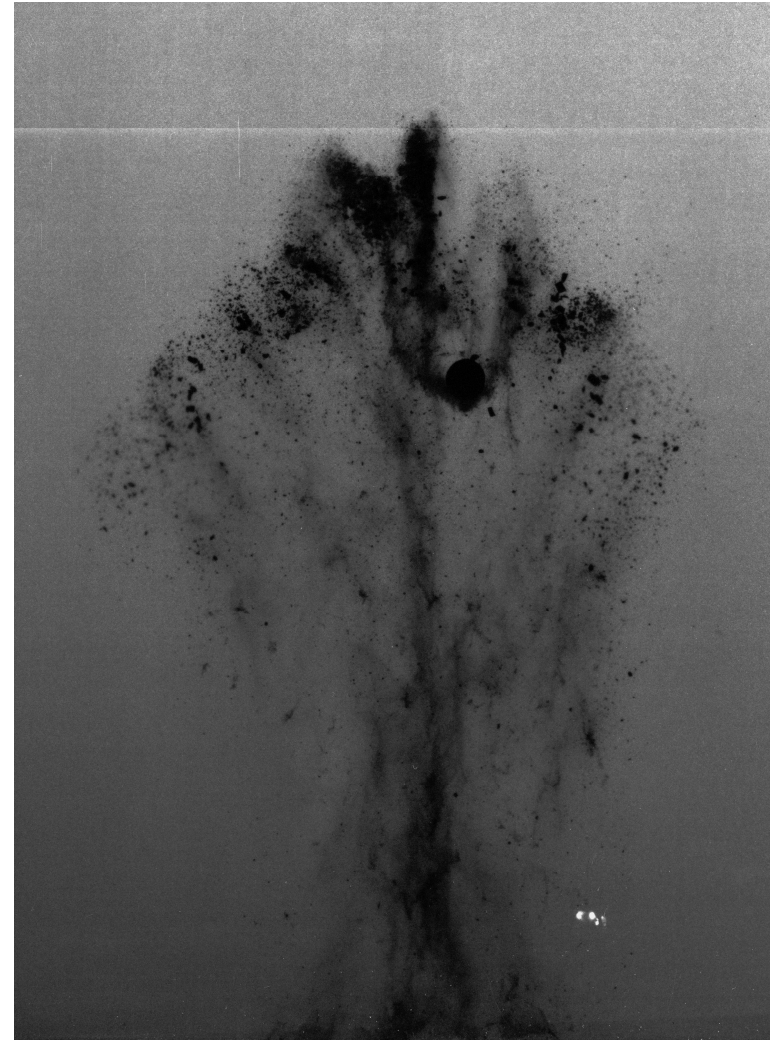
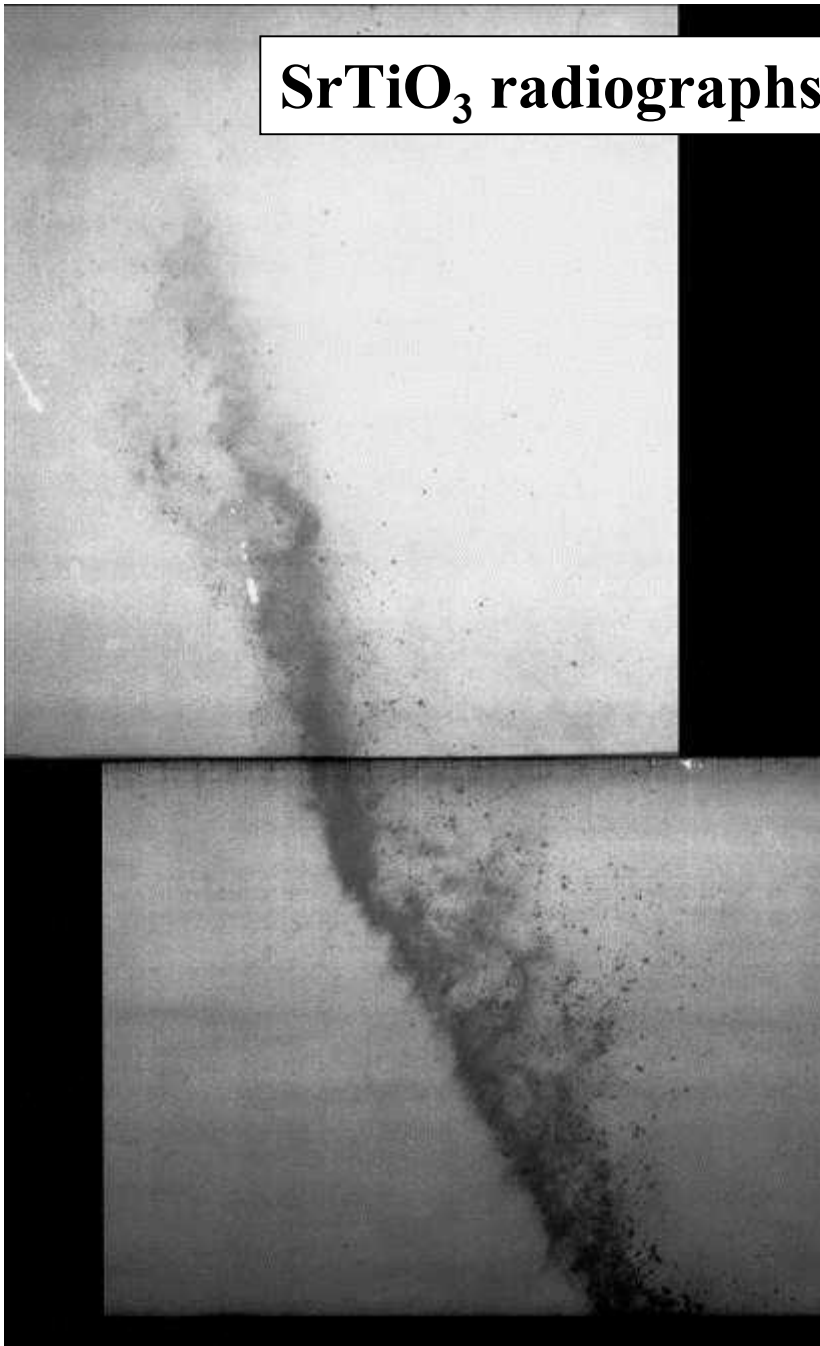


Aerosol produced from compressive stress



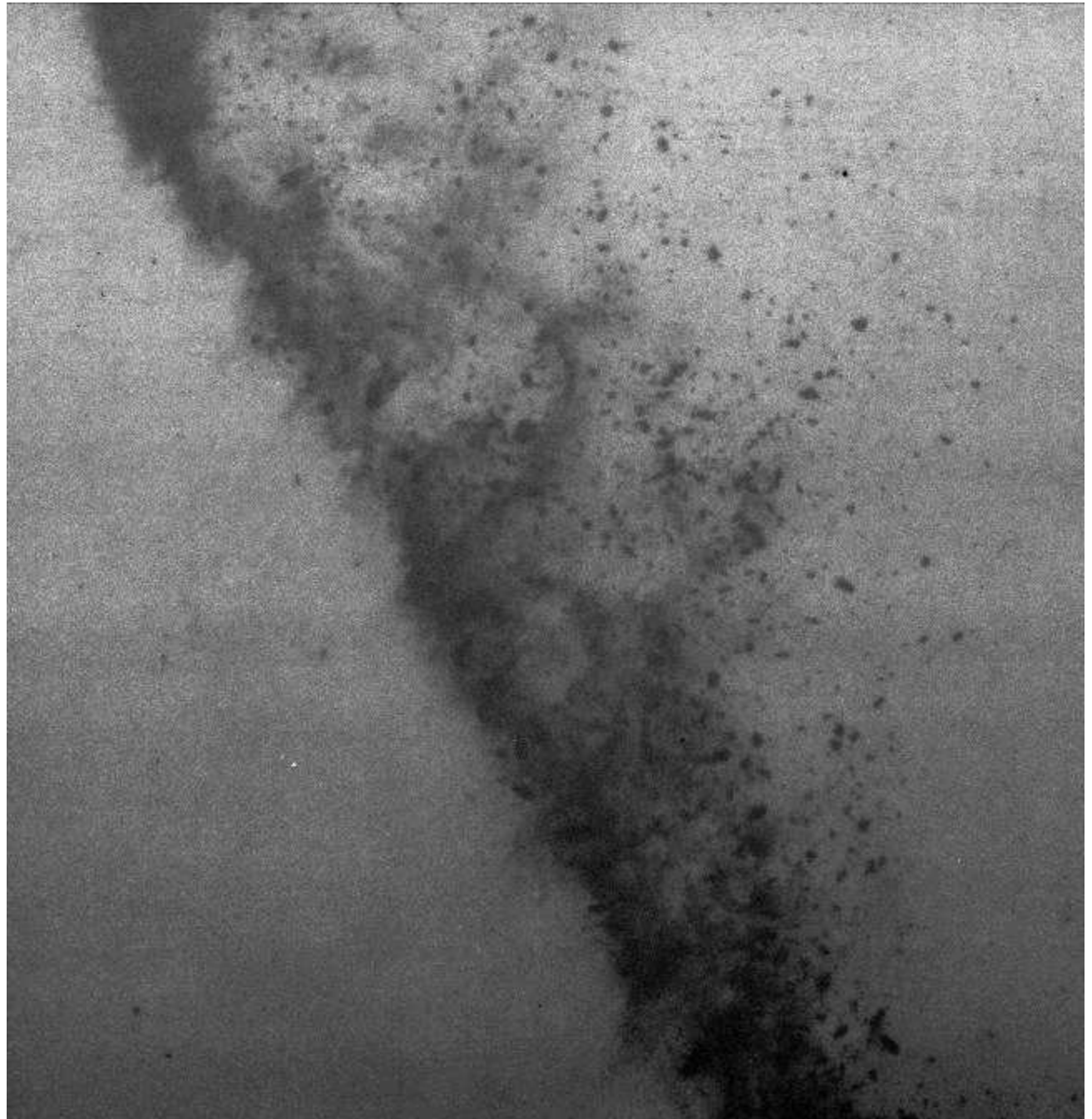
Courtesy of B. Wham, B. Patton, B. Jubin (ORNL)

**SrTiO<sub>3</sub> radiographs of particles (2 geometries)**





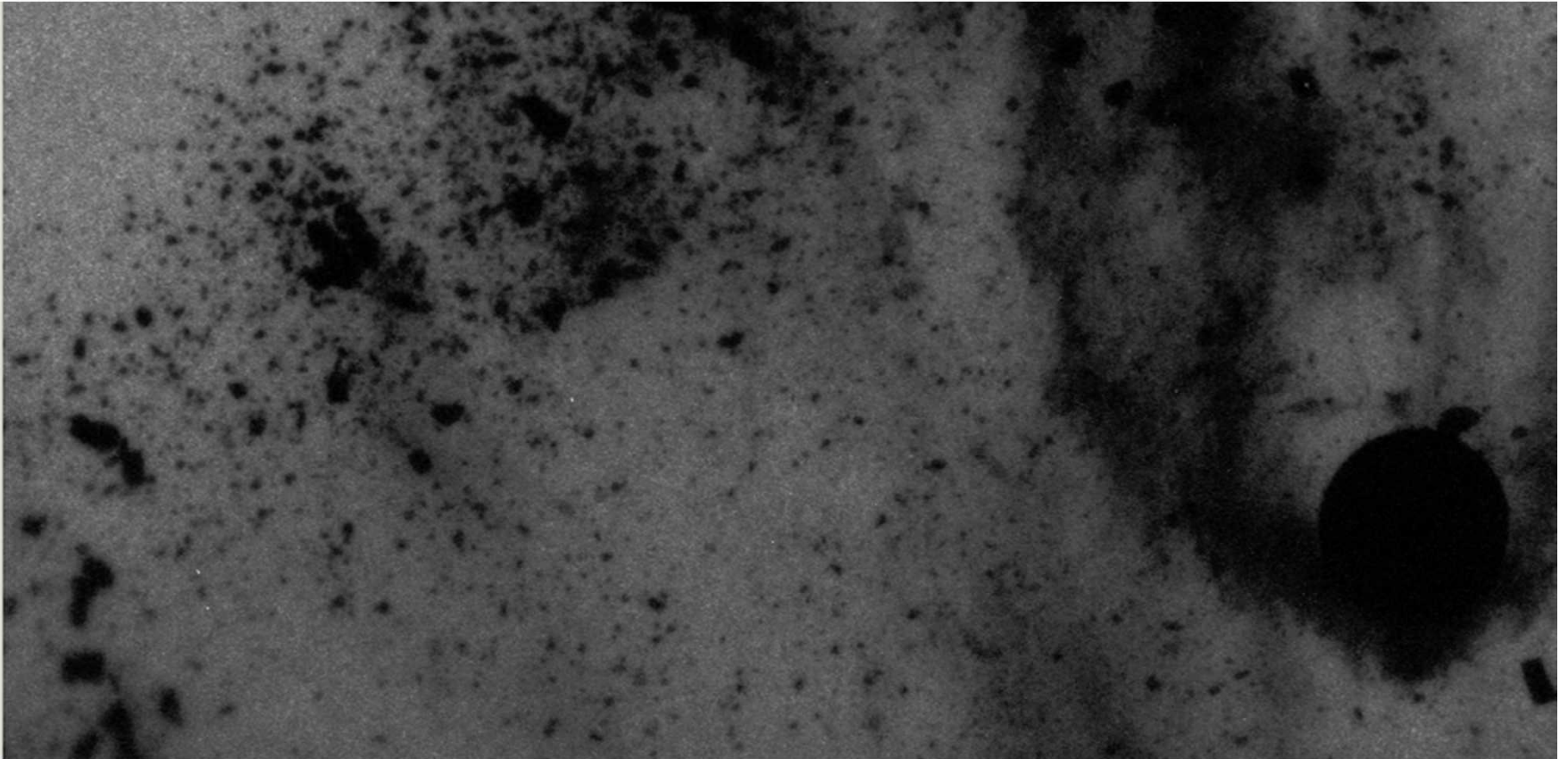
Expanded view  
 $\text{SrTiO}_3$   
(Largest particles  
About 1 mm)



Expanded view  $\text{SrTiO}_3$



Reference (.5 in) – large particles 3 – 4 mm, most small distinguishable in this  
Image are between .5 and 1 mm



# Materials of concern: Americium-241

- Half life: 432.7 years
- Alpha emitter, AmBe is a neutron emitter
- Typical Form: AmO<sub>2</sub> or encased AmO<sub>2</sub> with Be metal



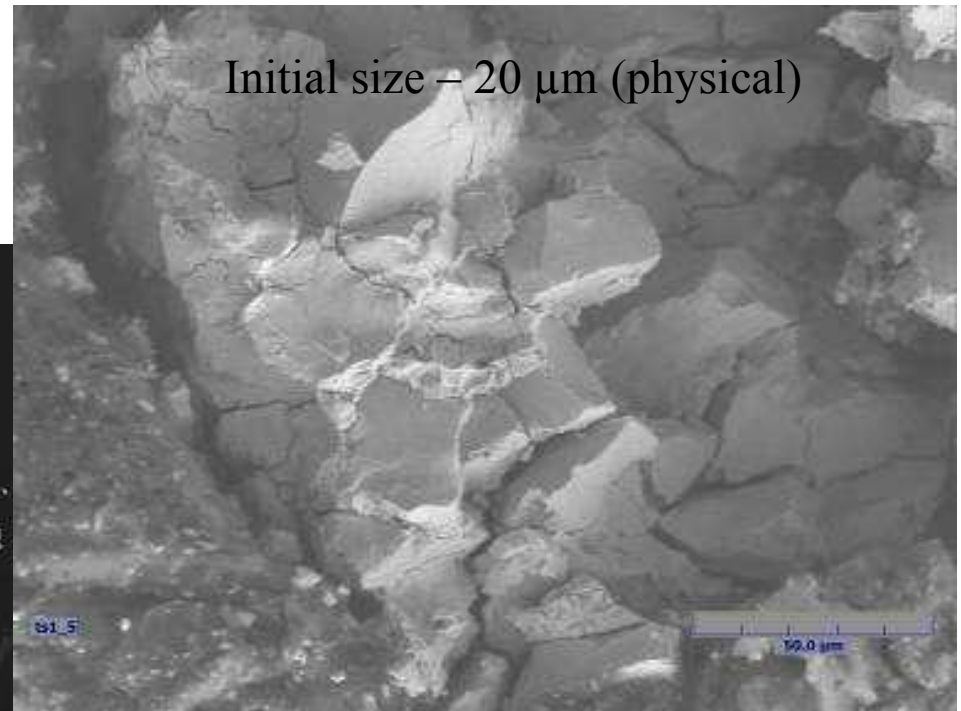
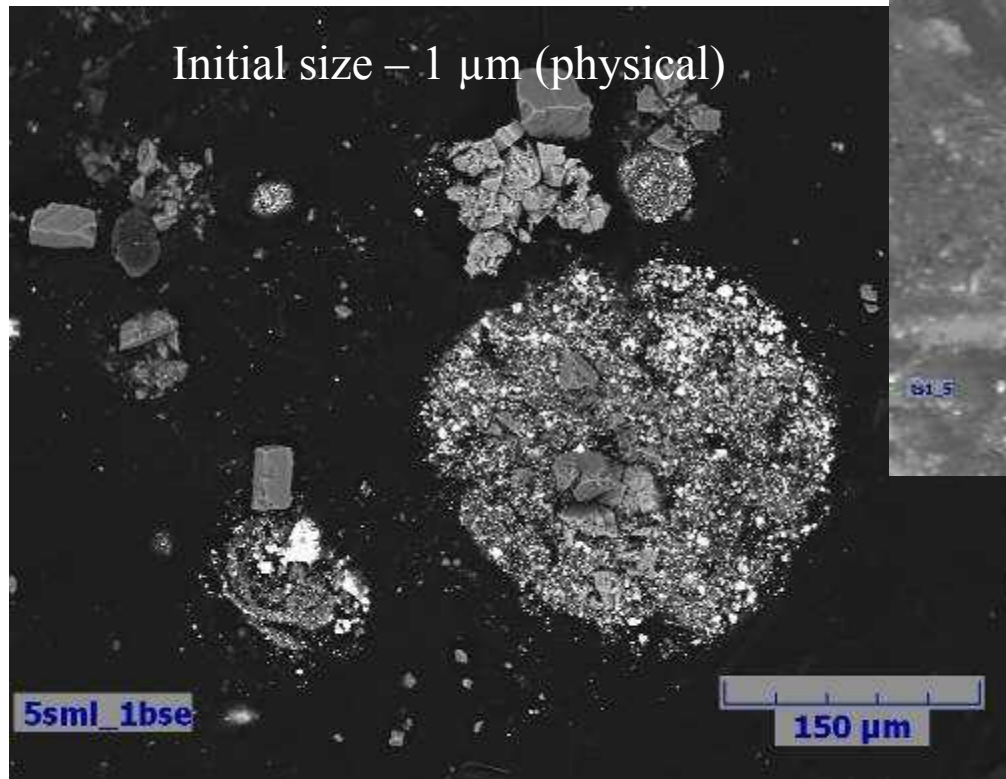
Damaged AmBe  
Well logging  
Source

Typical Uses	Form	Activity (Ci)		
		Min	Max	Typical
Calibration Facilities	Am	5	20	10
Research reactor startup	AmBe	2	5	2
Well logging	AmBe	0.5	23	20
Thickness gauges	Am	0.3	0.6	0.6
Fill level gauges	Am	0.012	0.12	0.06
Moisture detectors	AmBe	0.05	0.1	0.05
Moisture/density gauges	AmBe	0.01	0.1	0.05
Bone densitometry	Am	0.027	0.27	0.14
Static eliminators	Am	0.03	0.11	0.03



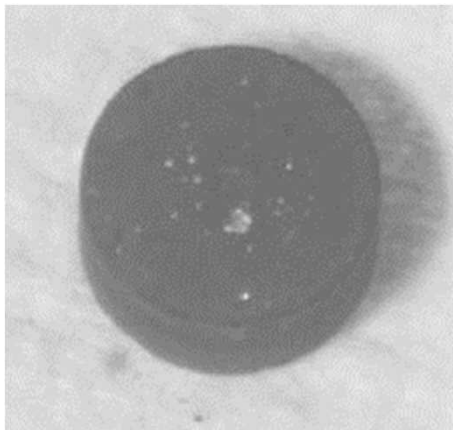


# Shock sintering of ceramics results in larger particles



# Materials of concern: Cesium-137

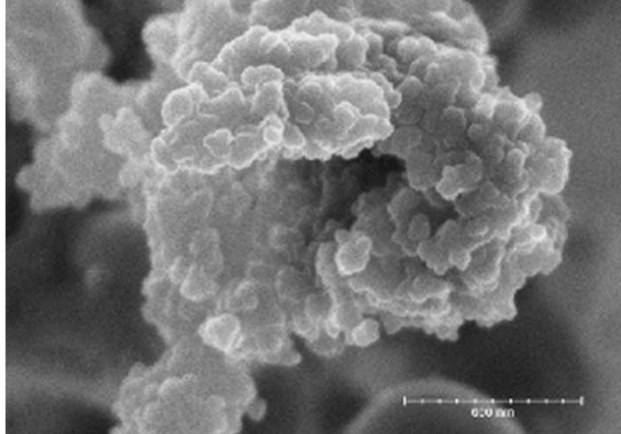
- Half life: 30.2 years
- Gamma emitter
- Typical Form: Encapsulated CsCl salt



Typical Uses	Activity (Ci)		
	Min	Max	Typical
Irradiators: Sterilization	5k	5M	3M
Irradiators: Self shielded	2.5k	42k	15k
Irradiators: Blood/Tissue	1k	12k	7k
Teletherapy	500	1.5k	500
Calibration facilities	1.5	3k	60
Brachytherapy	3	8	3
Various industrial gauges	0.01	5	2
Well logging	1	2	2

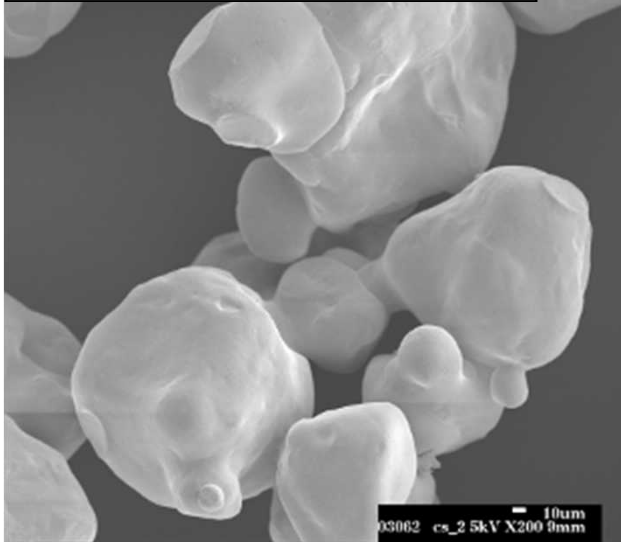
# Phenomena: Explosive aerosolization of powders

Shock sublimation of salts  
→ particles  $< 1 \mu\text{m}$

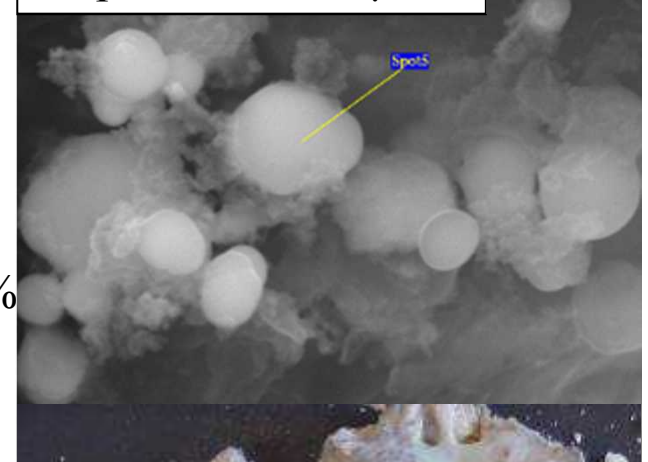


- Fractions depend on material properties and device geometries
- Respirable aerosol ranged from 20 % to 80 %
- Very little aerosol generated between 30  $\mu\text{m}$  and 200  $\mu\text{m}$

Initial salt grains → large



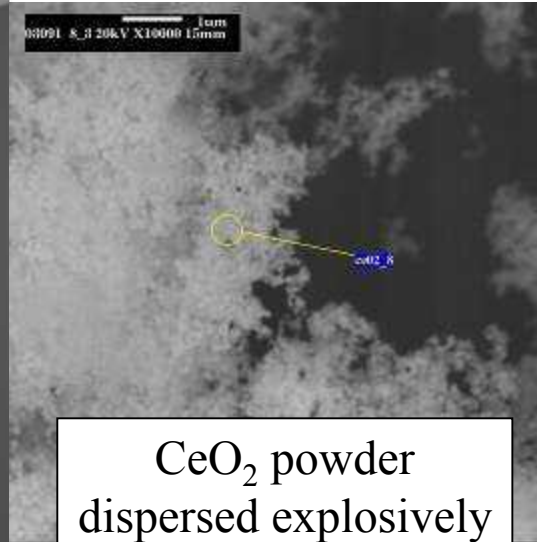
Shock melting of salts  
→ particles  $< 10 \mu\text{m}$



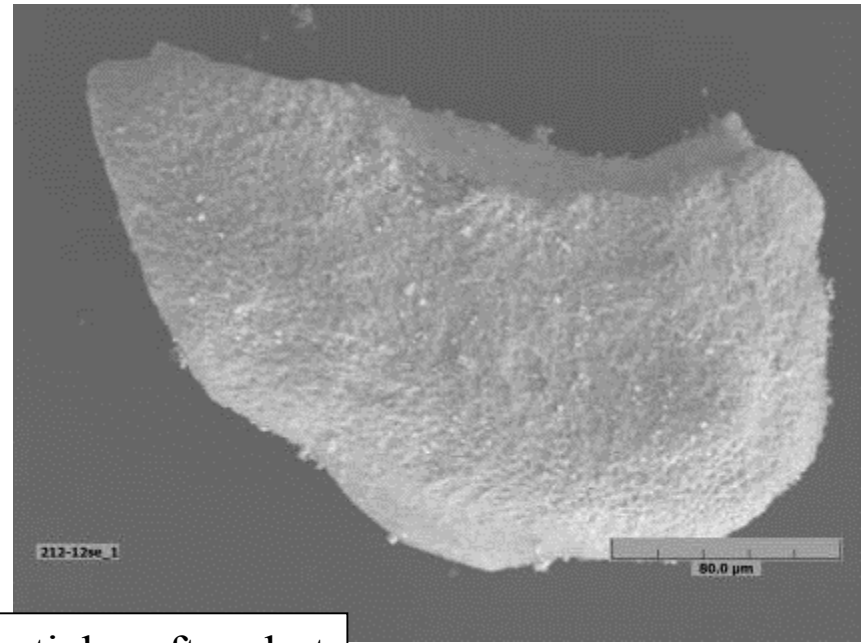
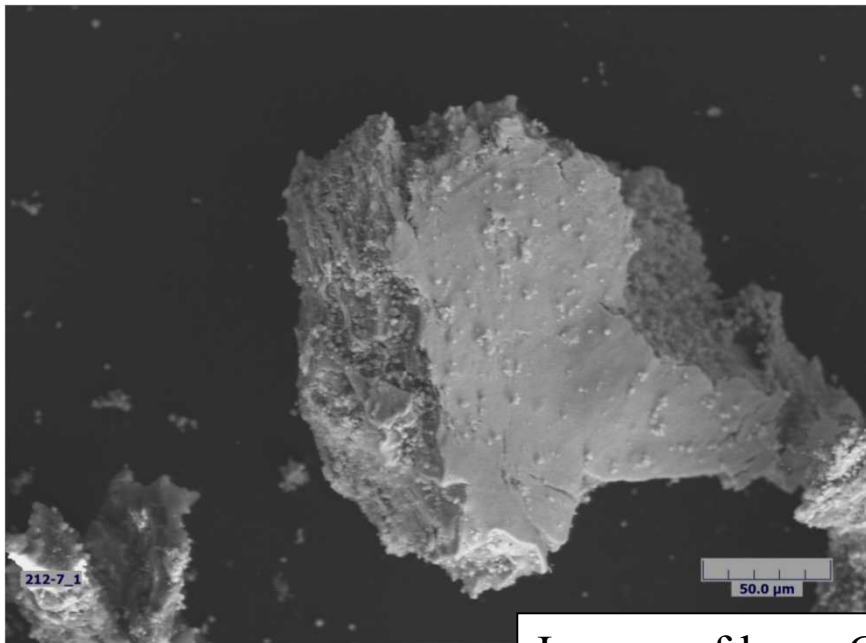
Shock sintered ceramic powder



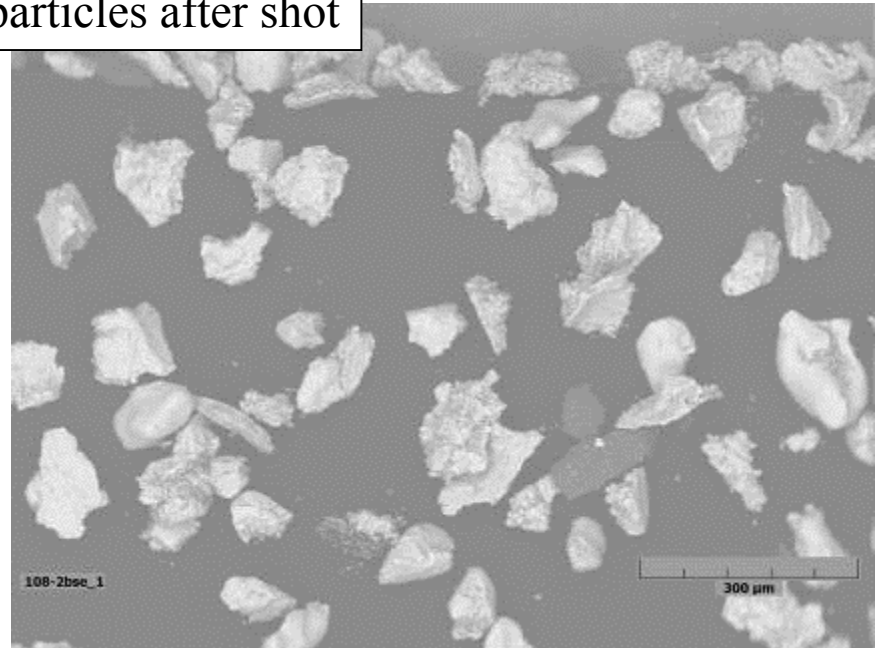
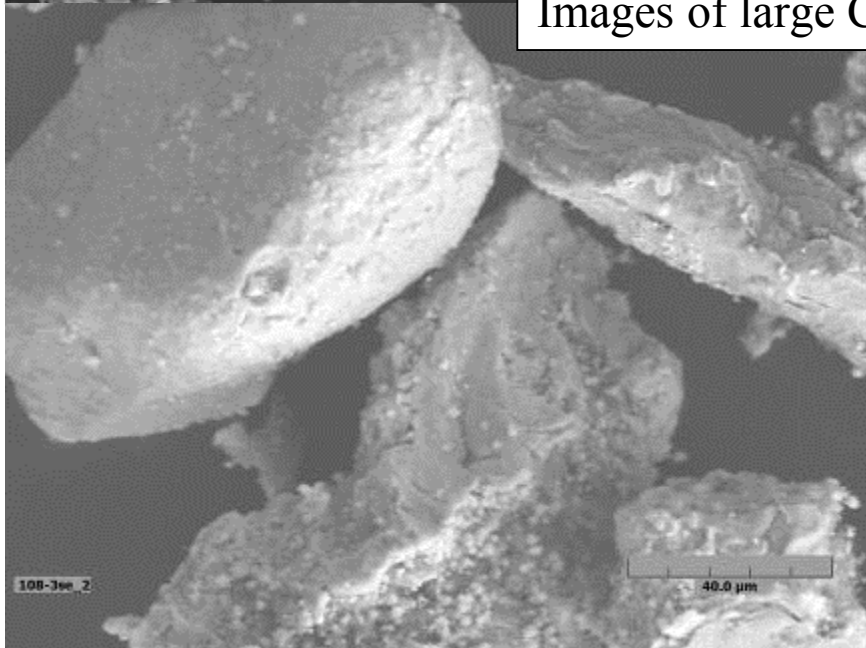
$\text{CeO}_2$  powder  
dispersed explosively







Images of large CsCl particles after shot



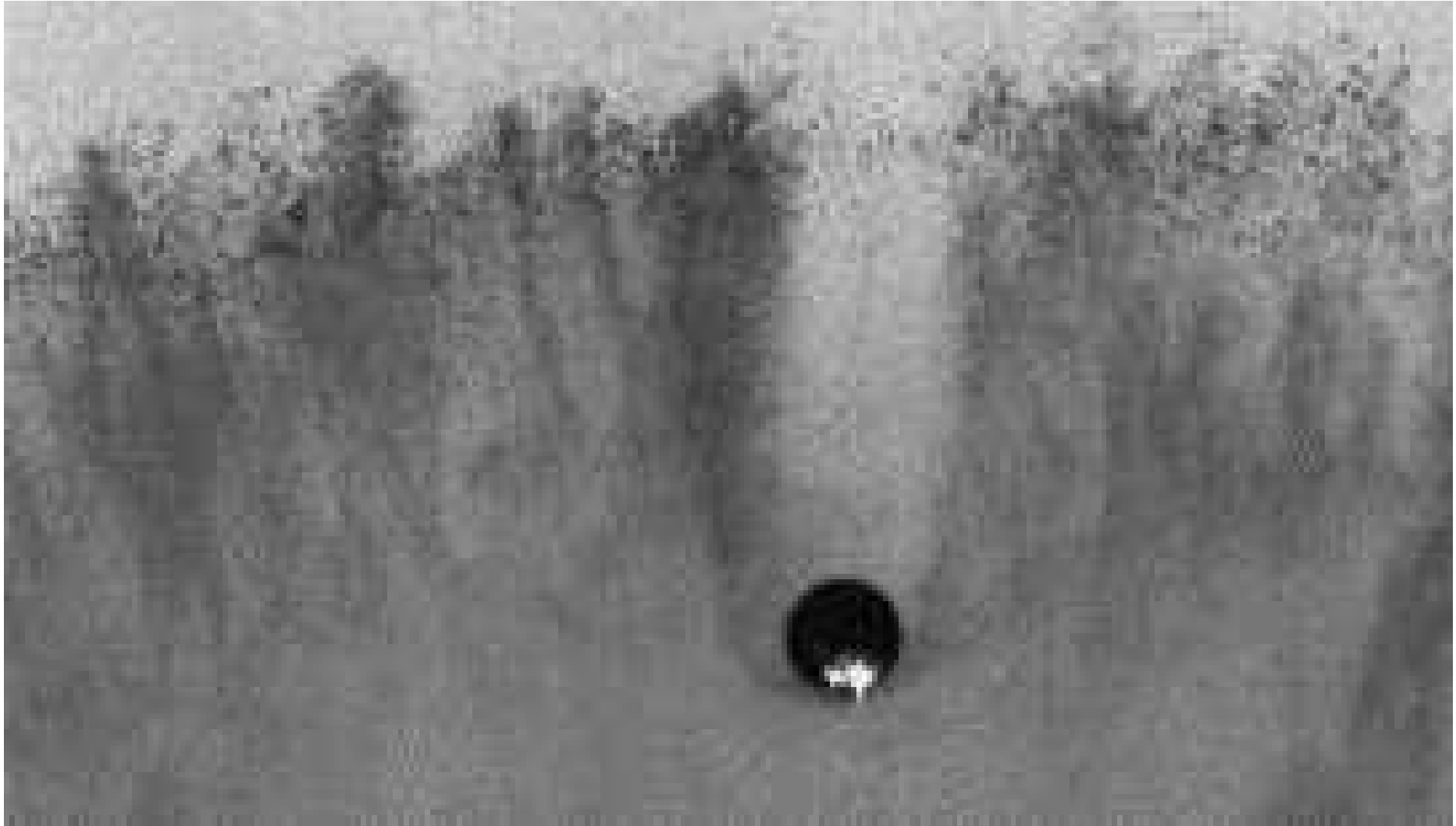
Note evidence of plastic deformation and evidence of bimodal size distribution



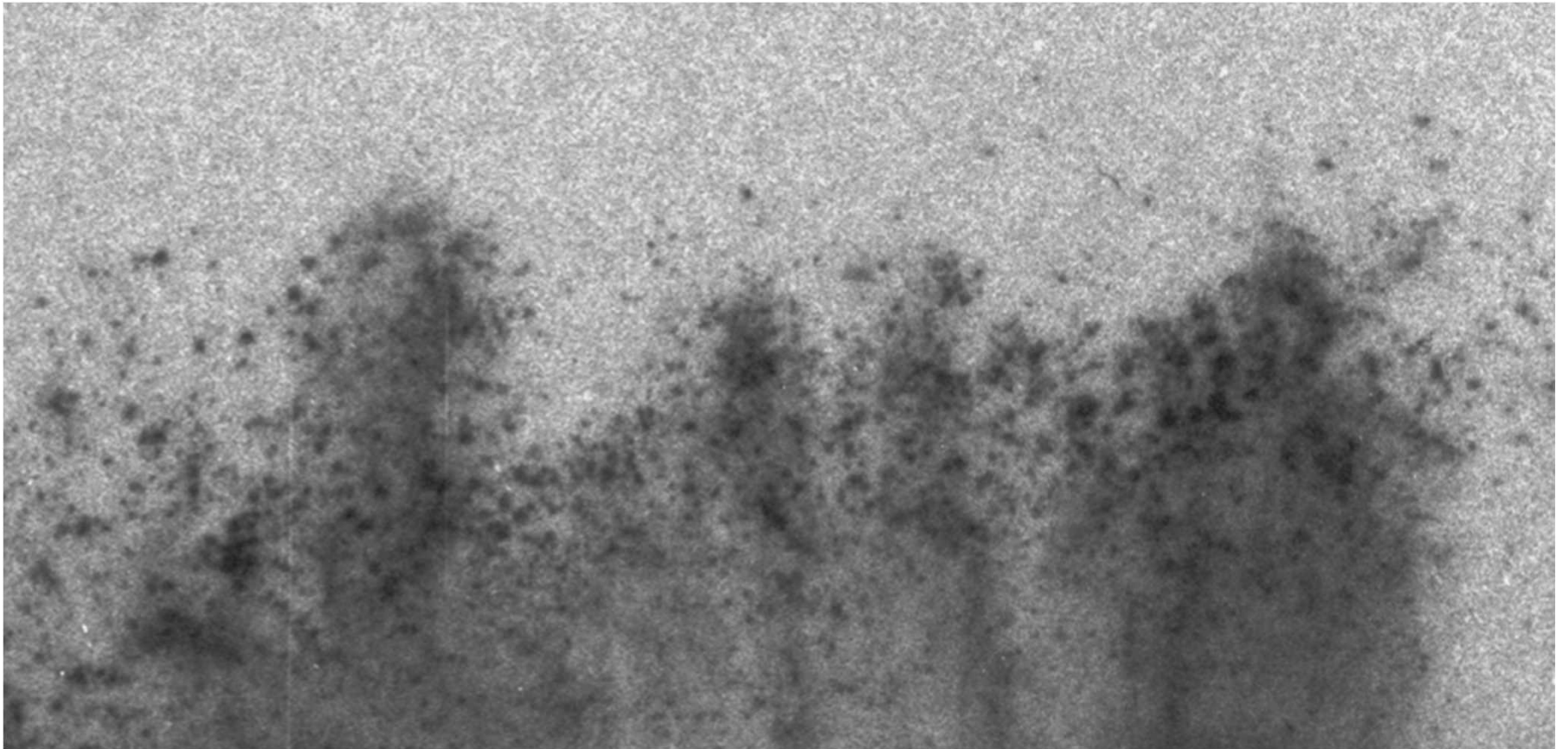
# CsCl Powder – geometry 1



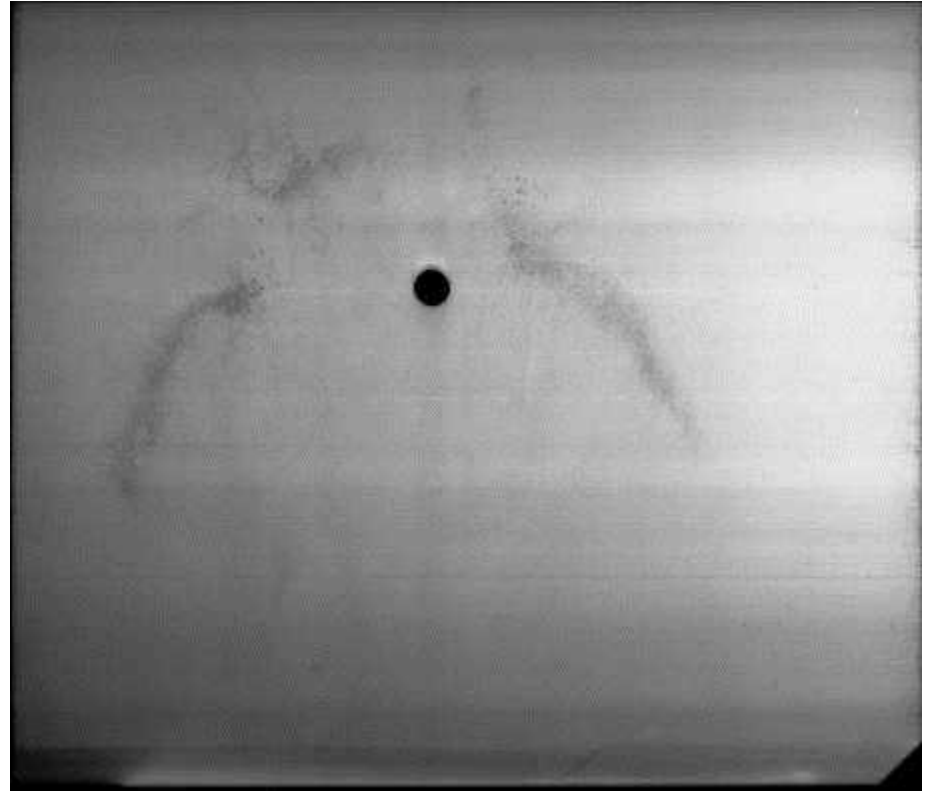
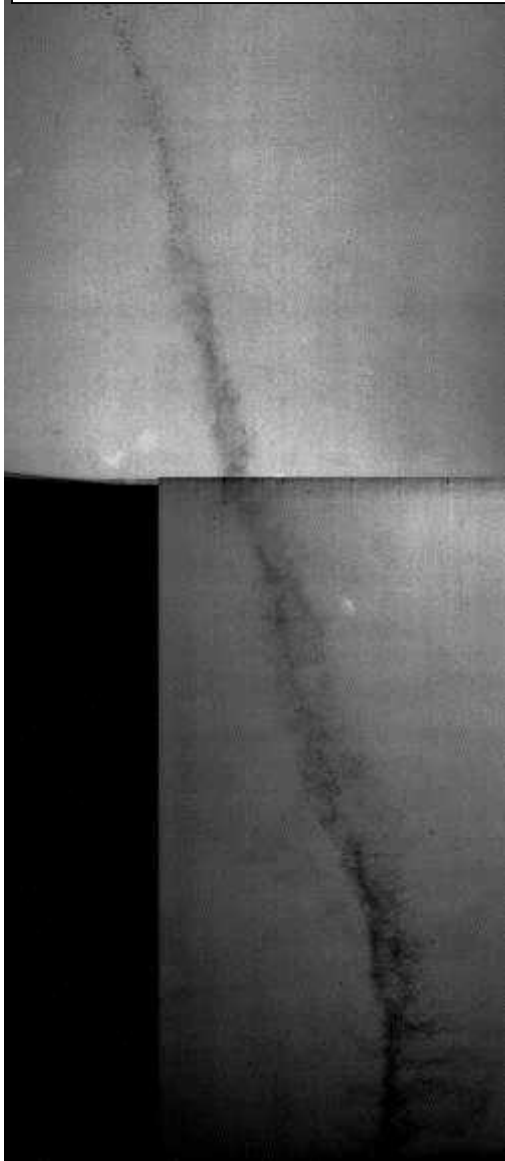
# CsCl geometry 1 (expanded)



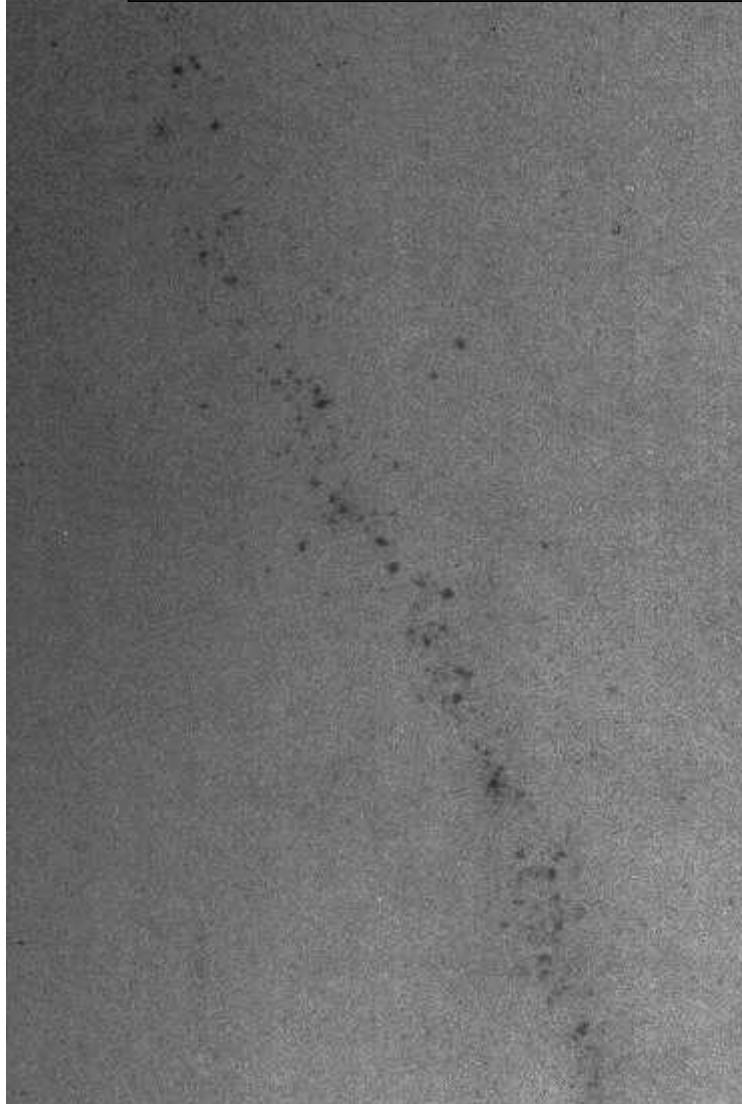
Most distinguishable particles between  
.3 and 1 mm



**CsCl radiograph of particles (Geometry 2 and 3)  
(pressed pellet 2.7 g/cm<sup>3</sup>)**



**CsCl pressed pellet 2.7 g/cm<sup>3</sup> – geometry 2**  
**Expanded view**

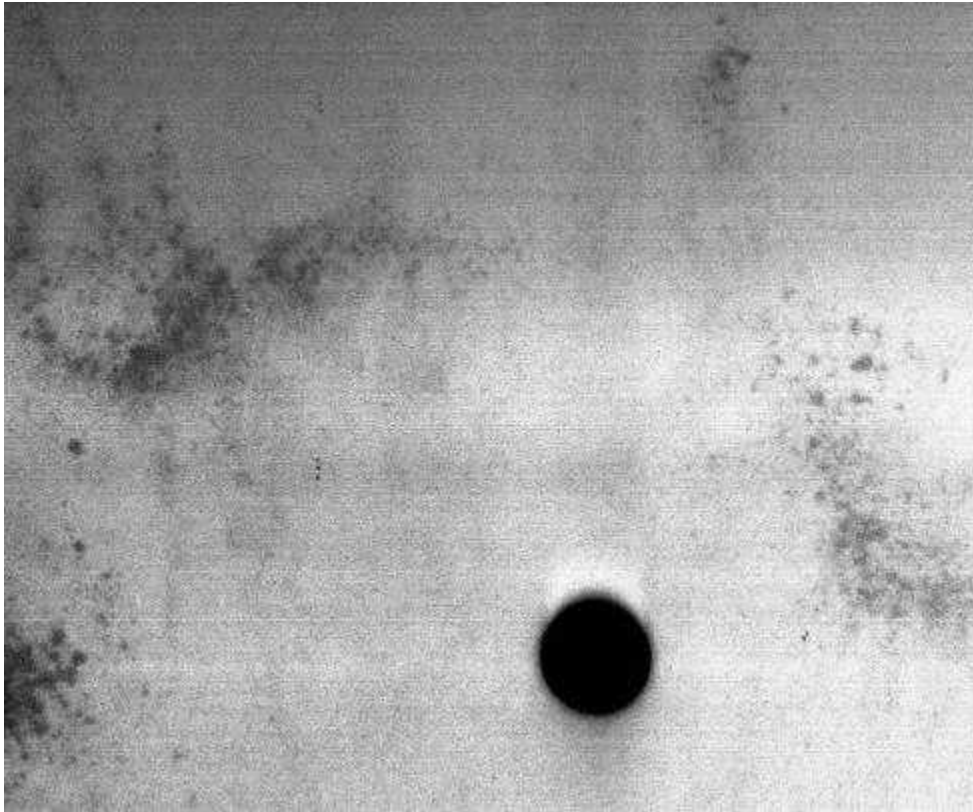


Jet top



Jet bottom

## Expanded view CsCl geometry 2 (**pressed pellet 2.7 g/cm<sup>3</sup>**)



### **Preliminary CsCl pressed pellet conclusion**

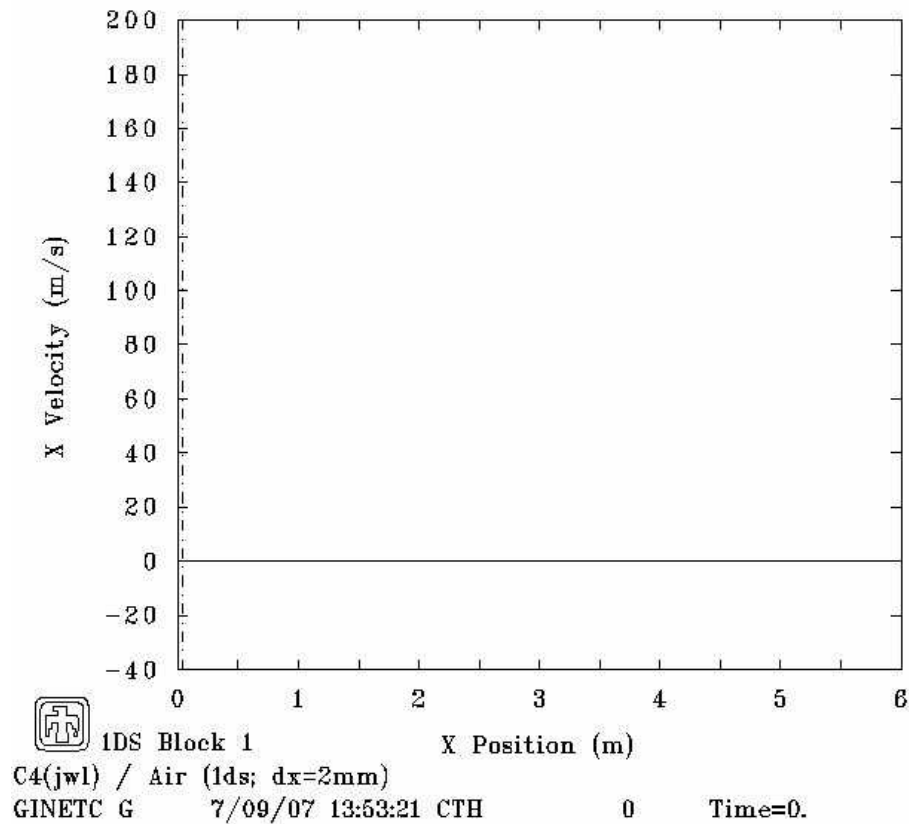
Many large particles ( $> 100 \mu\text{m}$ )

In order to get a pressed density of 2.7, it was necessary to grind CsCl granules (originally of a size  $300 - 400 \mu\text{m}$ ) to a size of about  $5 \mu\text{m}$  prior to cold pressing)

# Varied particle sizes – so what

- Localized concentrated shine problem – bad for first responders
- or
- Dilute cleanup problem (low level inhalation problem) – bad for EPA
- Will treat respirable and intermediate transport with traditional aerosol transport codes and large particles and fragments with ballistic models (based on experimental observations)

# Velocity of air behind shock (1 lb C4)





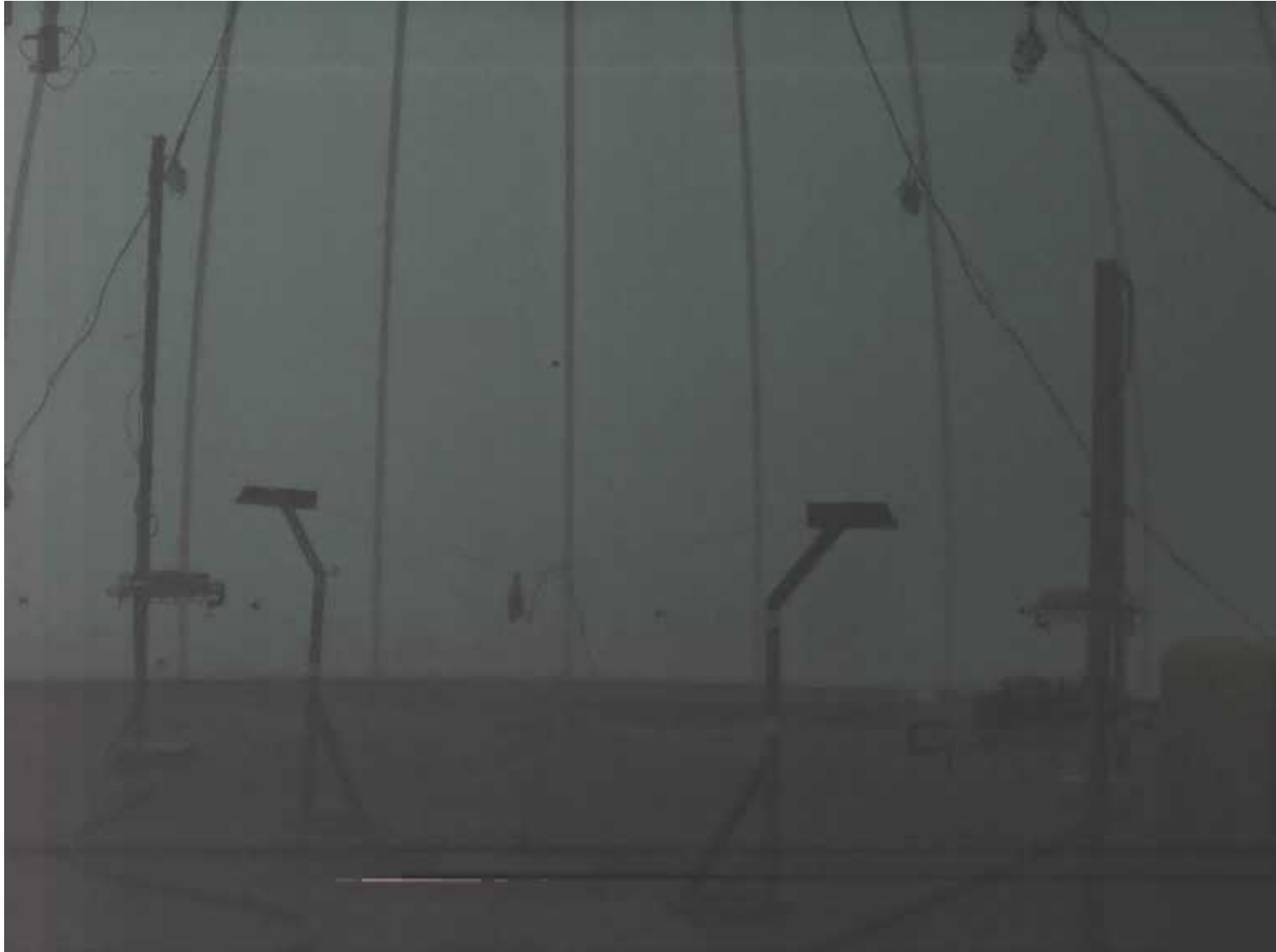
# 100 $\mu\text{m}$ (aero) WC – Geometry 1



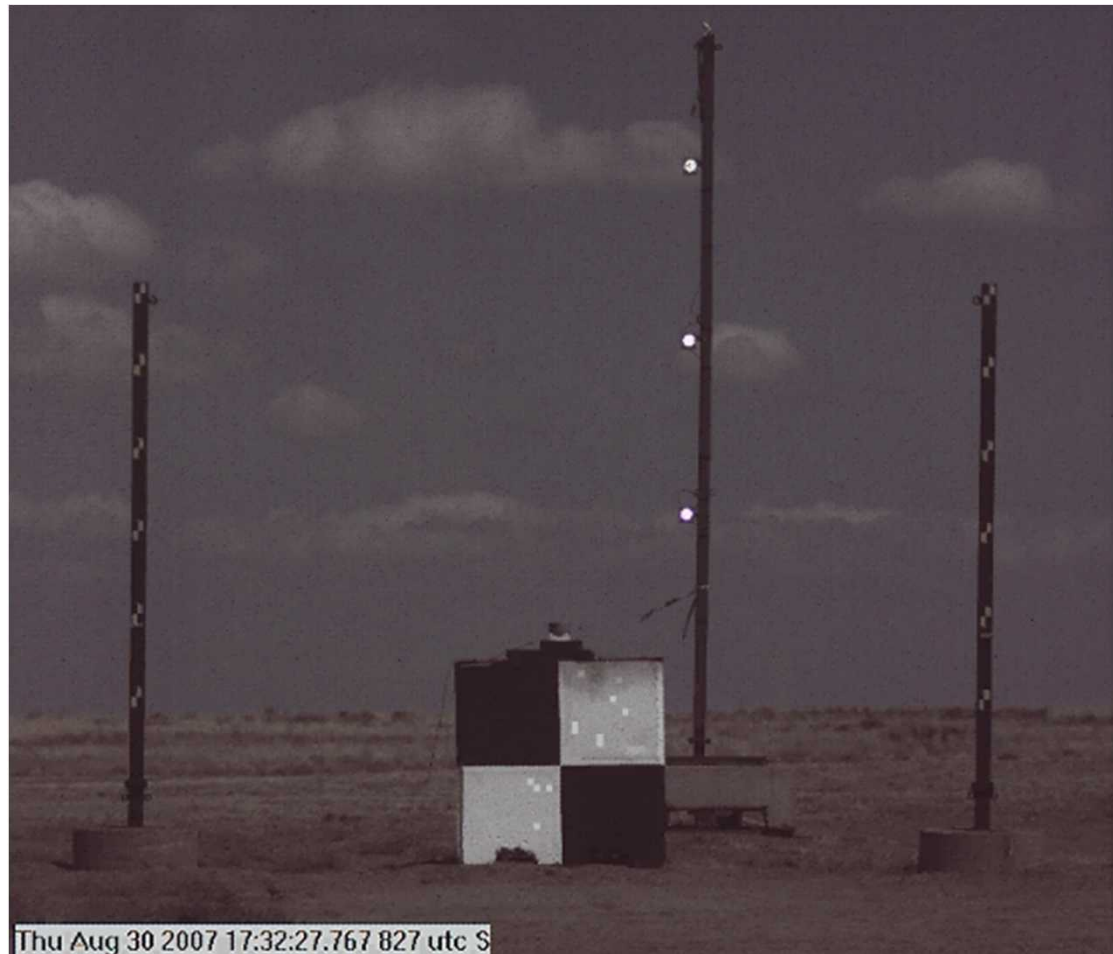
**Large particle/frag velocity at 4 m – 725 m/s,  
at 10 m 400 m/s, at 23 m 145**



## 100 $\mu\text{m}$ (aero) WC – geometry 2



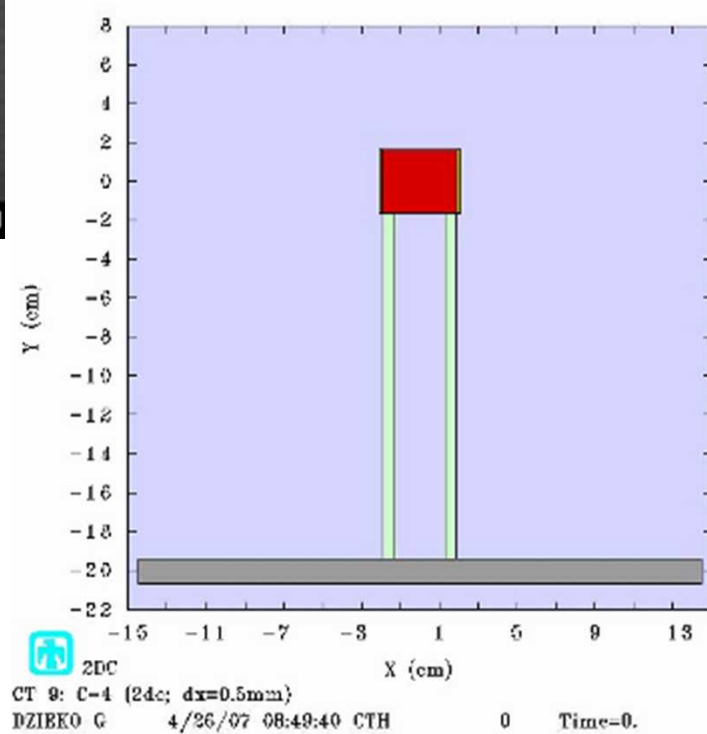
# Larger particles can penetrate the air shock in diverging devices



**Large particle/frag velocity at 2 m – 900 m/s, at 10 m  
700 m/s, no dropoff in  $v$  when air shock penetrated**



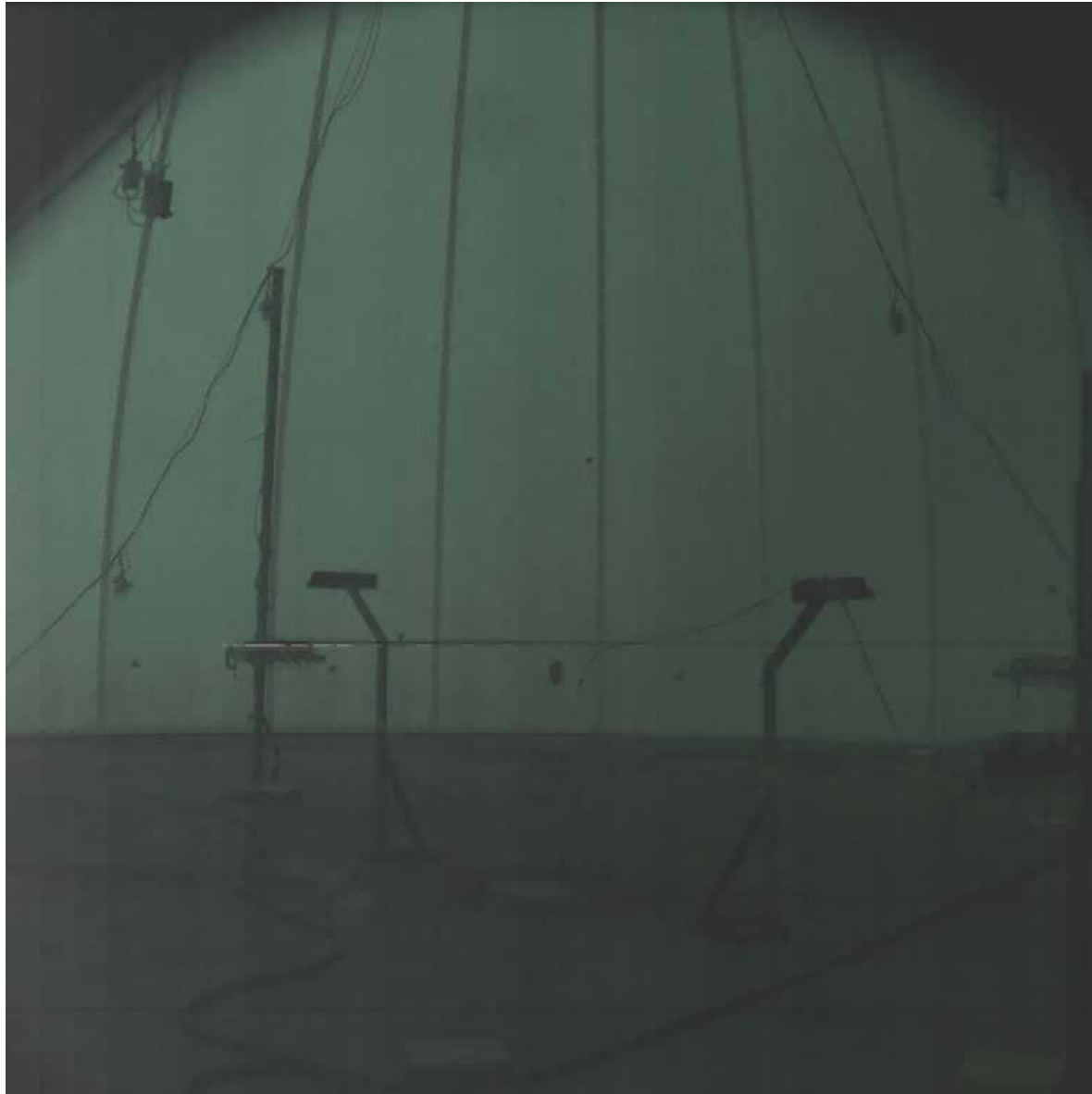
Thu Aug 30 2007 17:32:27.767 841 utc S



# 100 $\mu\text{m}$ (aero) WC – hemispherical wave geometry



**CsCl – 2 & 400  $\mu\text{m}$  (aero)**

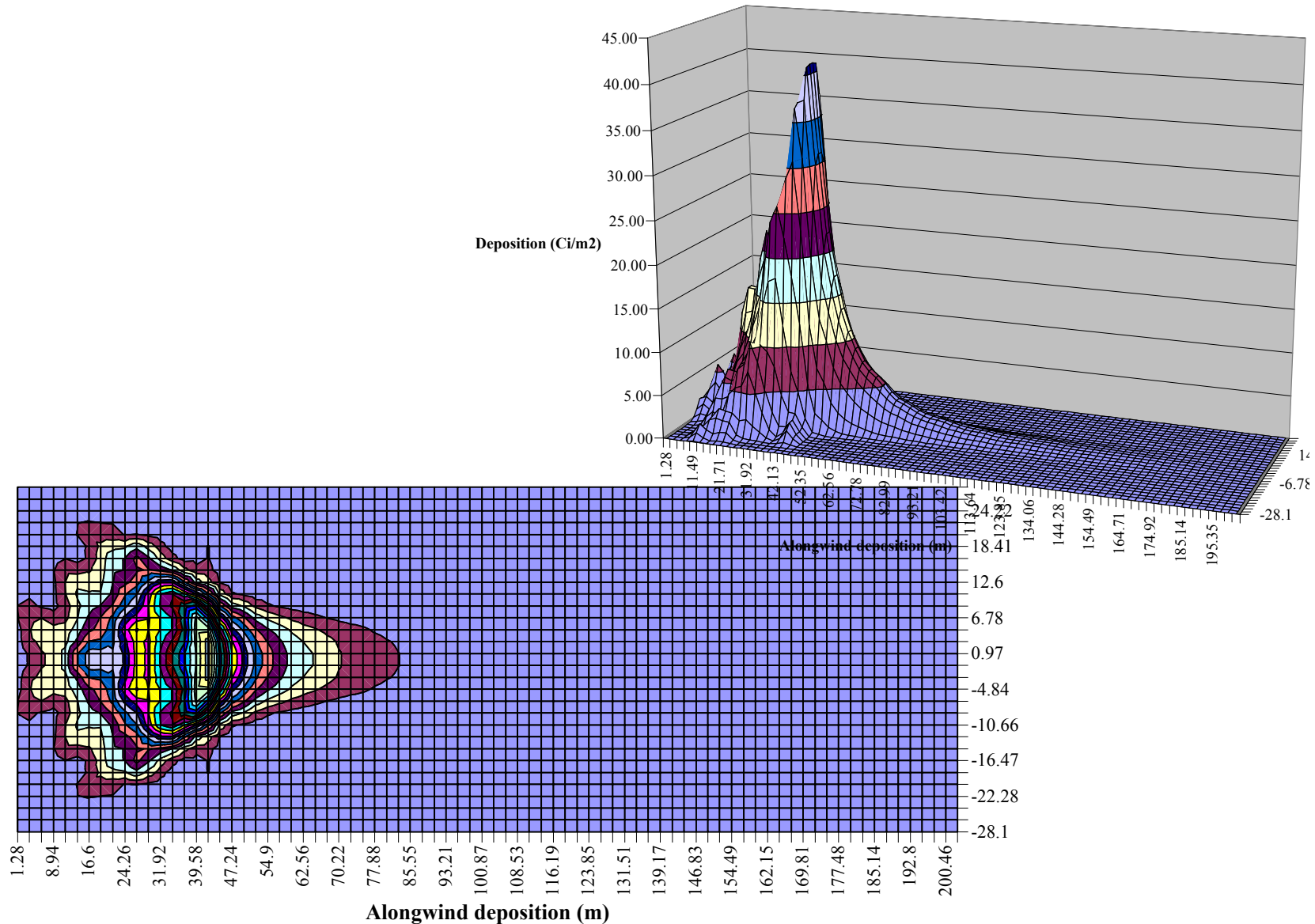




**CsCl – mostly 2  $\mu\text{m}$  (aero)**



# Example of ground deposition from explosive dispersal of ceramic large particles ( $> 100 \mu\text{m}$ , $< 500 \mu\text{m}$ ) – 2D and 3D representations – Scatterme



# Realistic RDD Hazard Boundaries for Varying Device Designs

## (Areas of highest concern for early response)

		<b>Int. Size Source, Basic Eng'g</b>	<b>Very Large Source, Basic Eng'g</b>
<b>Groundshine dose of 100 rad, 24-hour exposure assumed</b>	Acute groundshine threshold	0	~ 300 m
<b>Inhalation dose of 100 rad to the bone marrow (30-day committed dose)</b>	Acute haematopoietic syndrome threshold	0	0
<b>Inhalation dose of 270 rad to the lung (30-day committed dose)</b>	Acute pneumonitis threshold	0	0
<b>Lifetime inhalation dose of 100 rem (50-year committed dose)</b>	Chronic radiation sickness threshold	0	0
<b>5 rem groundshine dose (5-hour exposure assumed)</b>	Workers can work unrestricted for 5 hours	~ 100 m	~ 600 m
<b>10 * ALI for inhalation</b>	Use of Prussian Blue DTPA highly recommended	0	0

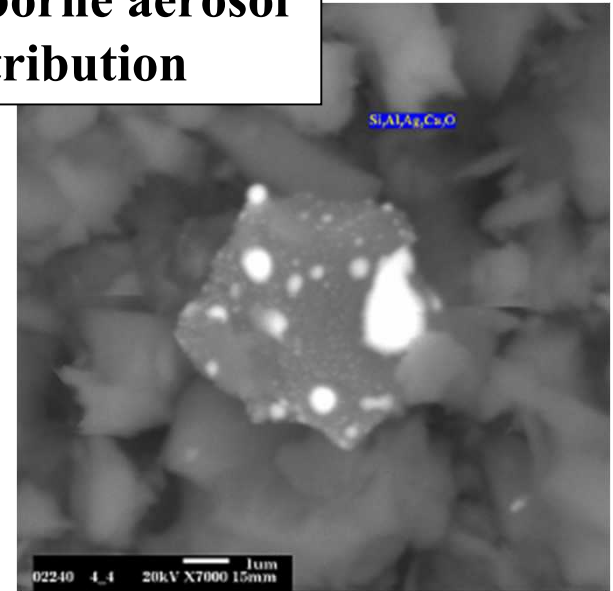
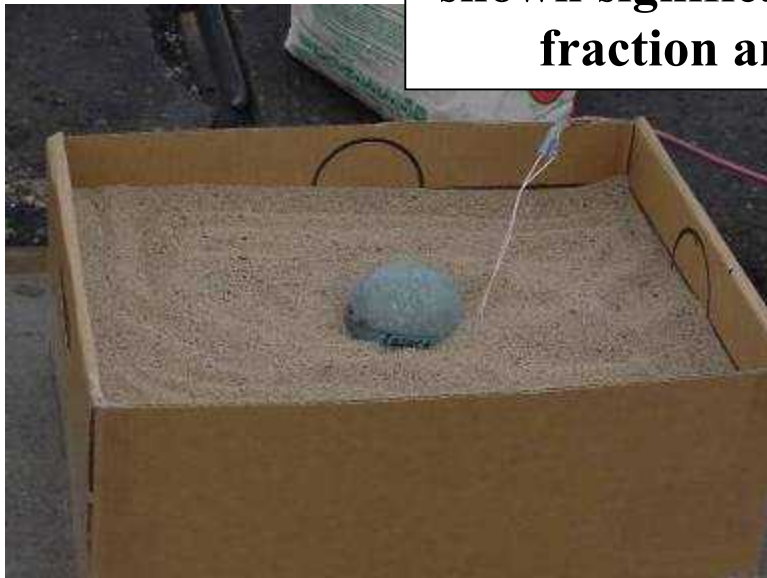
Applications

# Supplemental Viewgraphs

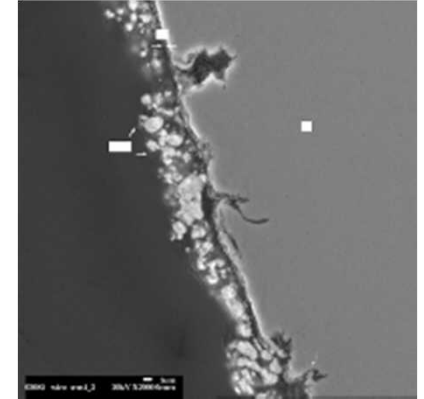
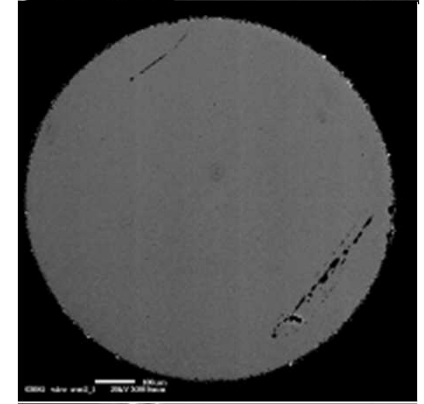
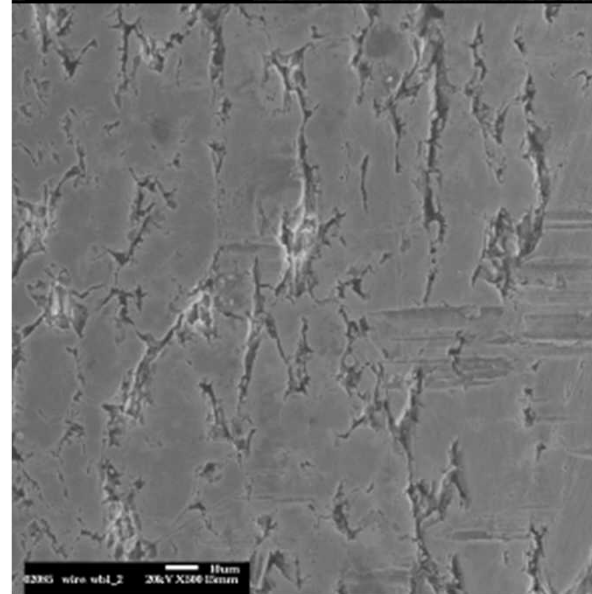
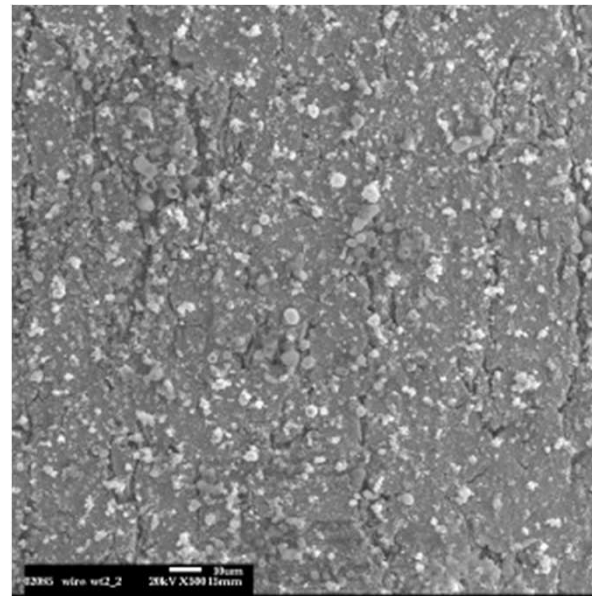
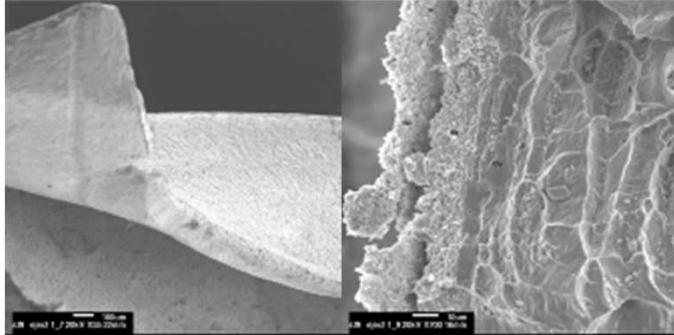
# **Inert material entrained into the fireball can coagulate with respirable particles causing an effective increase in size**

- Material entrained within 100 ms of the blast is most effective
- Efficiency of entrainment depends on the surface type , the elevation, and device geometry
- Nature of the dispersion can be altered drastically

**Agglomeration/condensation studies have shown significant reduction in airborne aerosol fraction and a shift in size distribution**

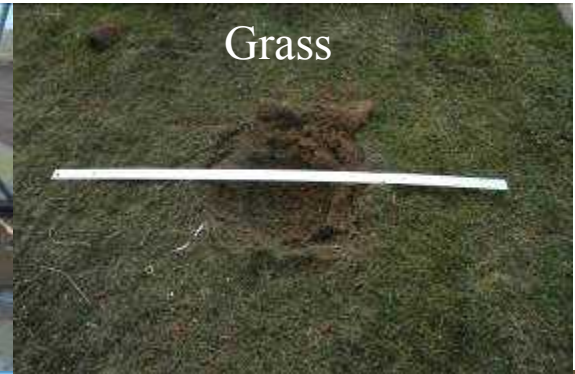


Region of heavy deposition and active agglomeration is smaller than visible fireball





# Dirt entrainment/plume behavior tests performed on several urban surfaces



All craters analyzed

2006-11-02 17:37:08 999000



2006-11-02 17:37:08 999000



# Afterburn and fireball comparisons: 1 lb, det on top, different surface conditions

Steel plate



Grass

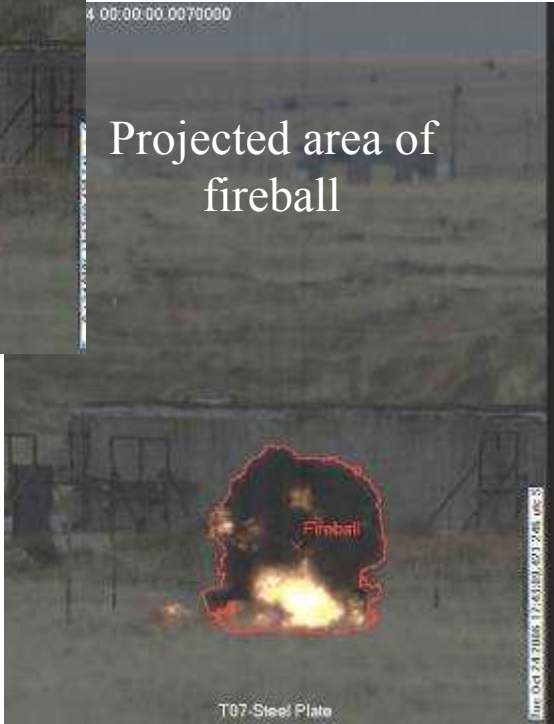
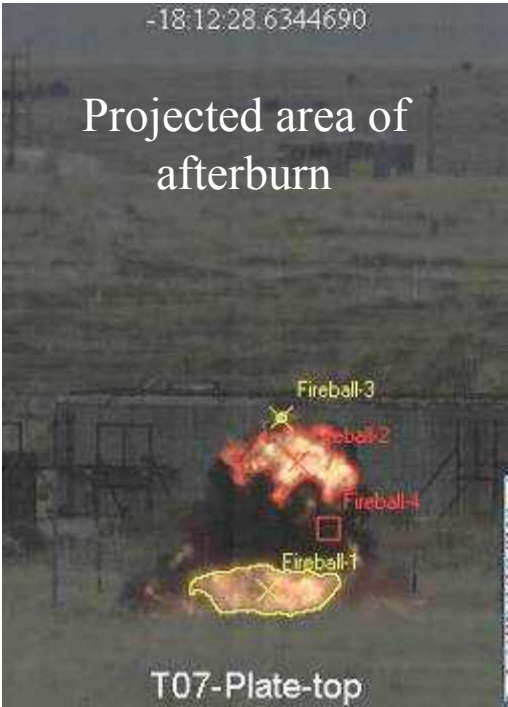


Steel plate, 1 m high



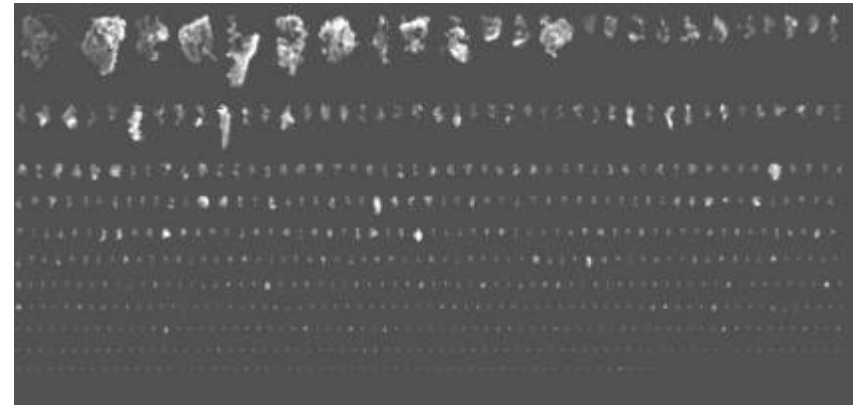
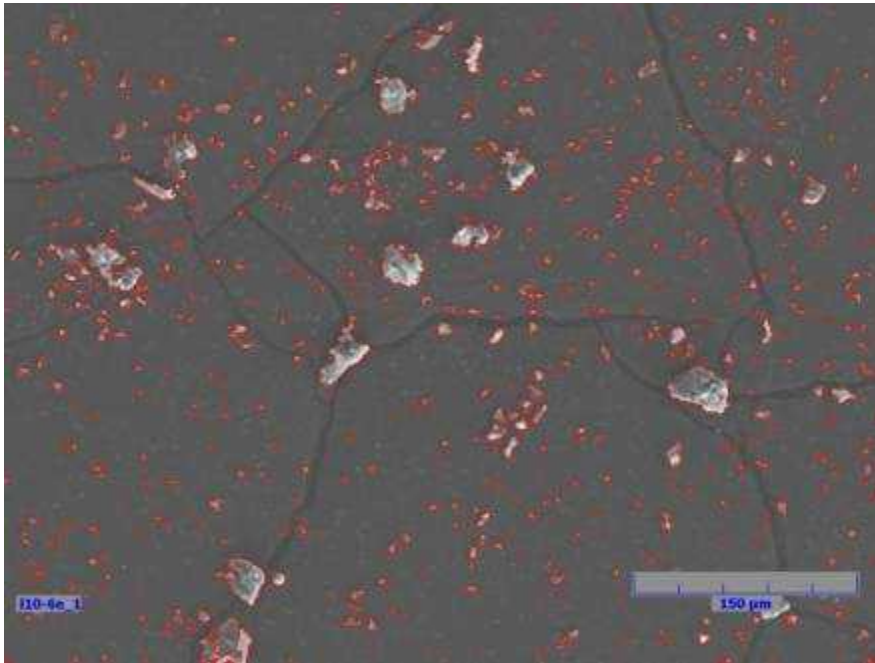
Normalized mass of material in fireball early time

Surface	Mass of inert material in Fireball (kg)
Mixed sand	1
Loose dirt	1
Concrete	0.08
Grass	0.07
Packed dirt	0.03
Asphalt	0.02 (Late burn)
Steel plate	0





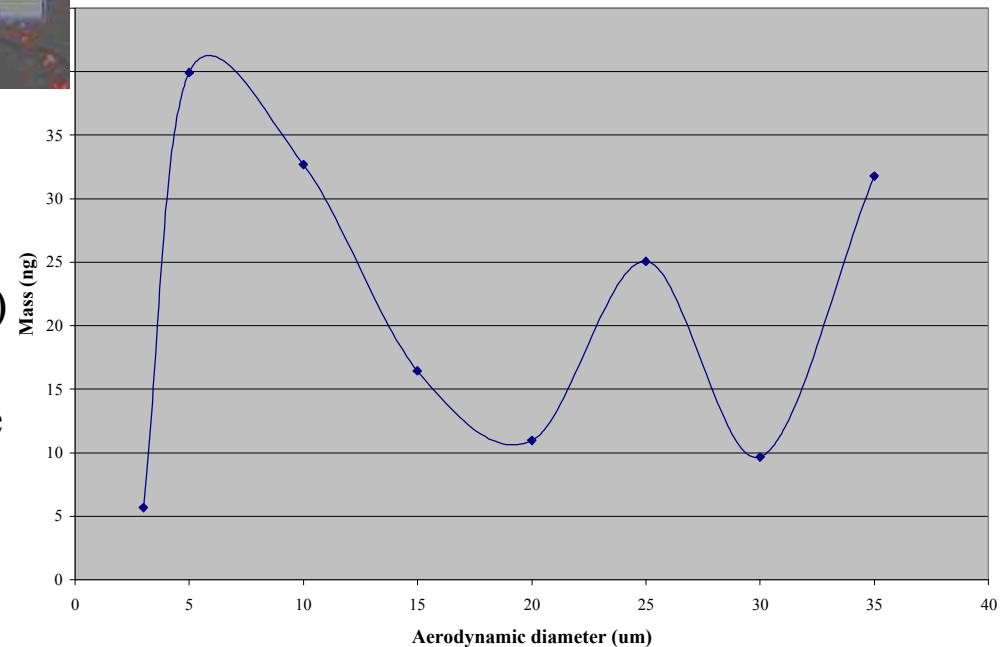
# Dirt entrainment particle size analysis



Mass vs aerodynamic diameter (from electromicrograph field of view)

Consistent with bimodal size observations  
From Pinnick, Fernandez, and Hinds  
(Explosion dust particle size measurements)

Observed peaks at 7 and 70 μm irrespective  
of soil or explosive type  
(Clay soil from LA, sandy clay soil from  
AL, and sandy soil from NM)



# Some Simple Fireball Physics

- Det wave in explosive
- Shock wave in particles ( $\Delta P$  acceleration of particles)
- Expansion of det products (acceleration of particles by det products)
- Stagnation when det products reach atmospheric pressure (drag – deceleration of particles)
- Particles  $> ? \mu\text{m}$  escape influence of fireball and det products – inertia  $>$  drag (simple calculations and experimental observations show that escape velocities achieved for particles  $> 100 \mu\text{m}$  aero)
- Shock wave in air, influence of neighbor particles (reduced drag)
- Afterburn if  $\text{O}_2$  available, Temperature not suppressed, soot and CO available
- C4 and TNT produce a lot of soot and CO
- TNT has an  $\text{O}_2$  balance of  $-74 \%$ , while HMX and RDX have an oxygen balance of about  $-20 \%$  (more energy in initial detonation, less in afterburn)
- More than half of the energy from TNT comes from the afterburn if the products burn to completion
- Shape of fireball dependent on det location, shape of explosive, material interactions



# Additional Basics Needed Here

- Settling Velocity
  - 1  $\mu\text{m}$  – .0035 cm/s
  - 10  $\mu\text{m}$  – .31 cm/s
  - 100  $\mu\text{m}$  – 24.8 cm/s
  - 1000  $\mu\text{m}$  – 386 cm/s
- Force of Drag  $F_D = C_D \frac{\pi}{8} \rho_g d^2 V^2$
- Aerodynamic diameter  $d_a = d_{phys} \rho_p^{1/2}$

$$\text{Re} = \frac{\rho_g V d}{\eta_g} \quad (\text{or in cgs units}) \quad \text{Re} = 6.6 V d$$