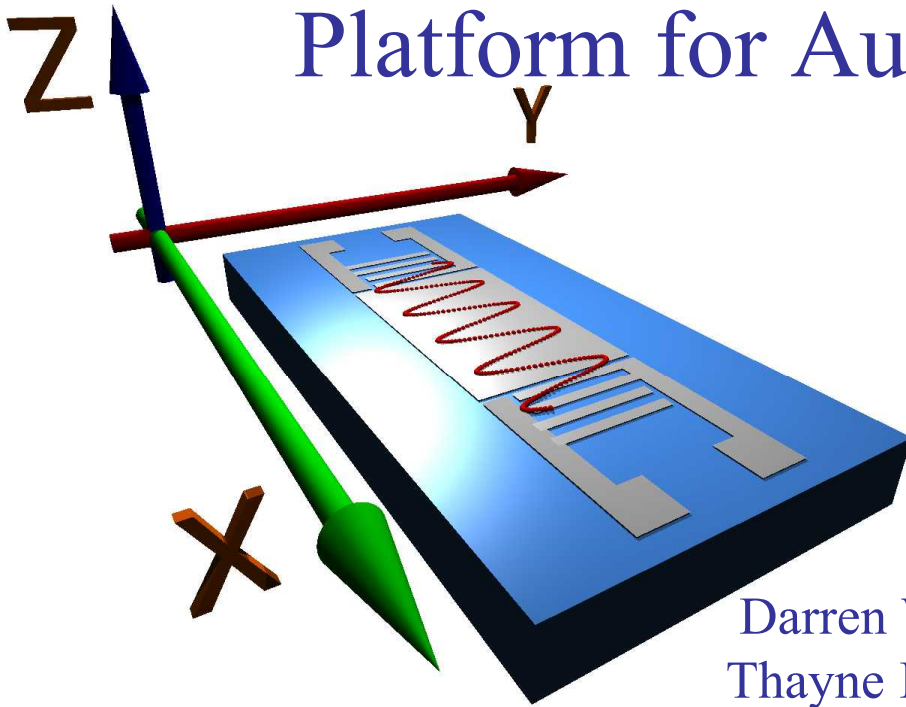


Love Wave Acoustic Array Biosensor Platform for Autonomous Detection



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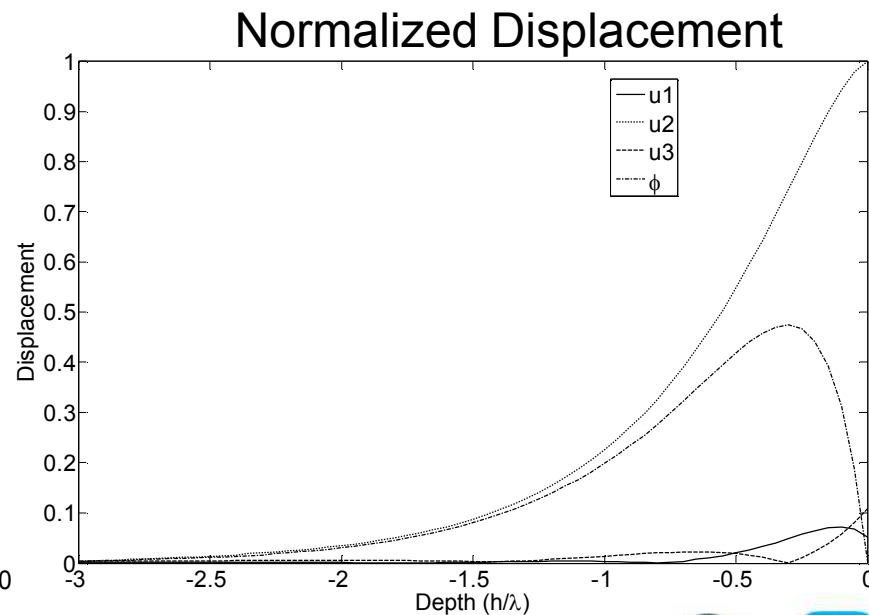
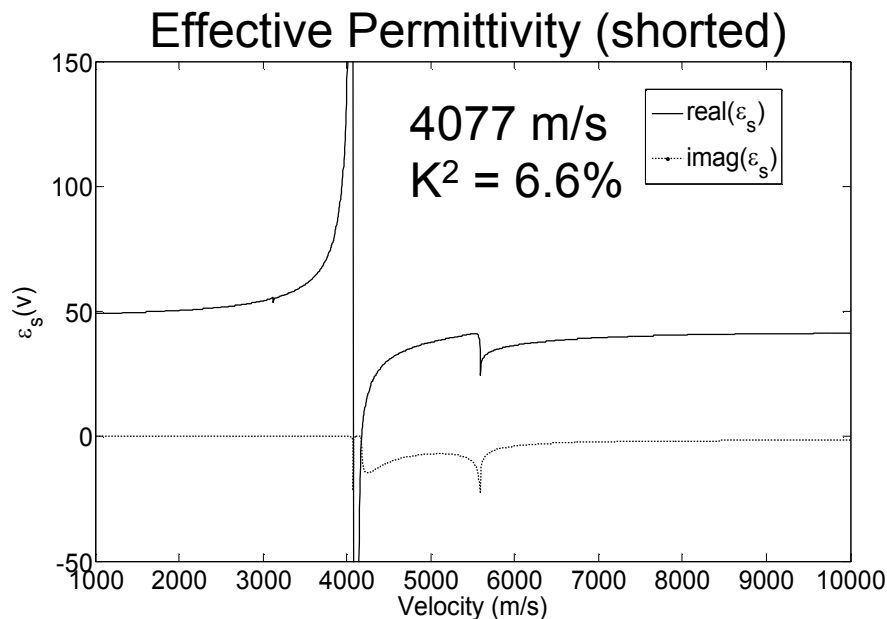


Outline

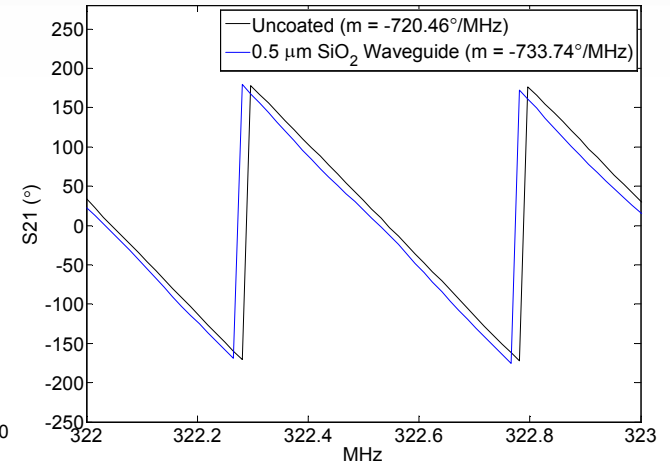
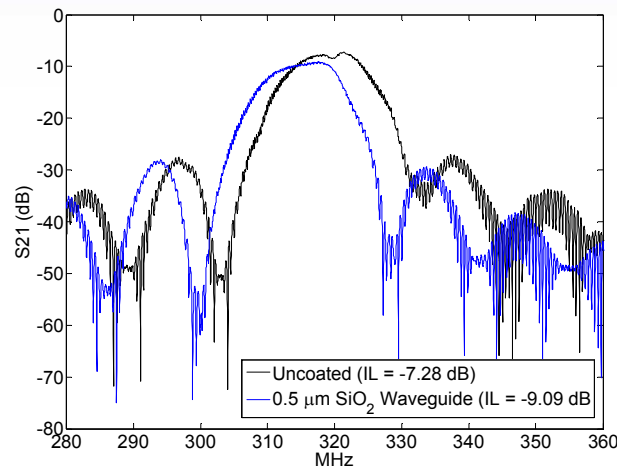
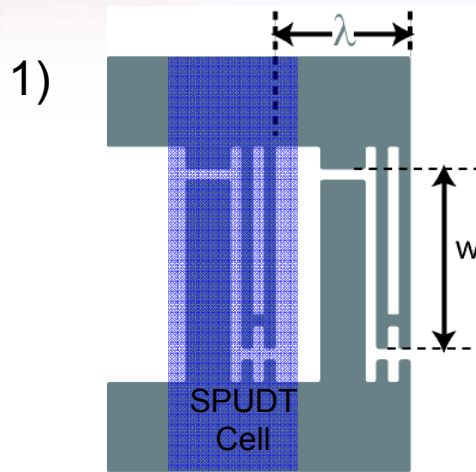
- Sensor System Approach
- Sensor IDT Design
- Waveguide
- Sensitivity and Temperature Analysis
- Detection System
- Sensitivity to Mass Density
- Multi-Analyte Biodetection
- Conclusions

Sensor System Approach

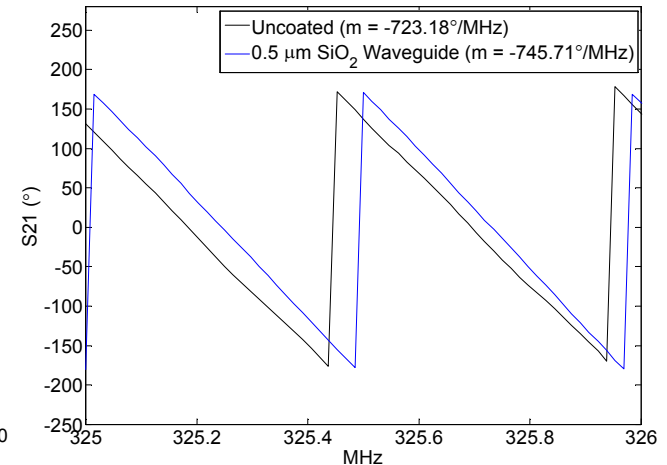
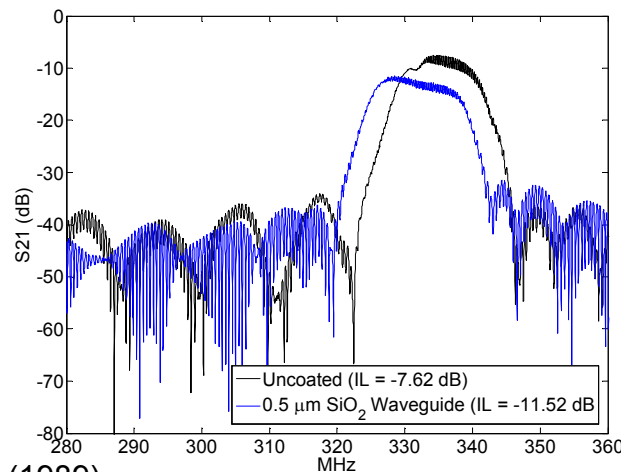
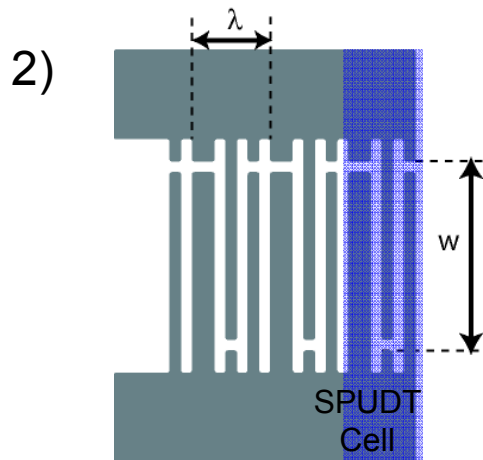
- Design Criteria:
 - High frequency (> 300 MHz)
 - Good phase linearity
 - Low insertion loss
 - Large phase slope
 - Small footprint
 - Challenges for 36° YX Lithium Tantalate $x(0, -54^\circ, 0)$ substrate
- ➔ IDT design is highly critical



Sensor IDT Design



Based on Hartmann, C. S. and B. P. Abbott (1989).

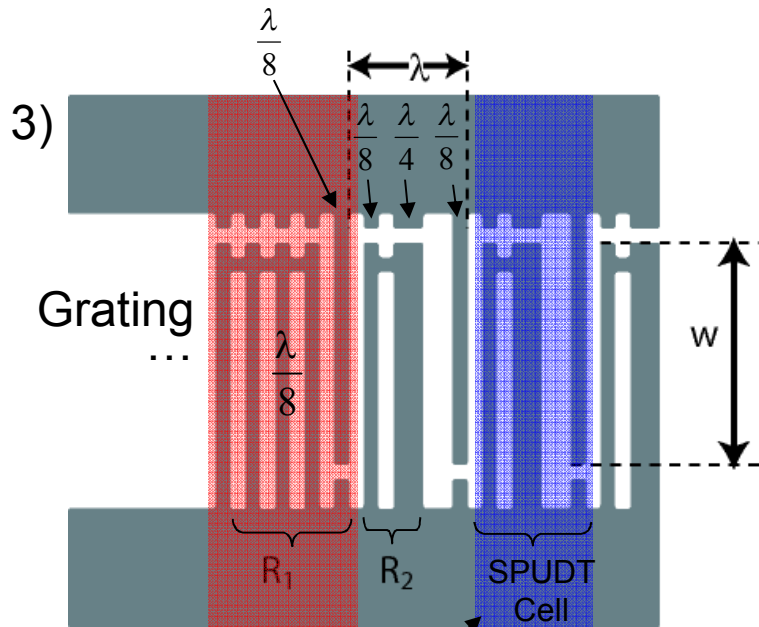


Hartmann, C. S. and B. P. Abbott (1989).
Nakagomi, S., H. Asano, et al. (2003).

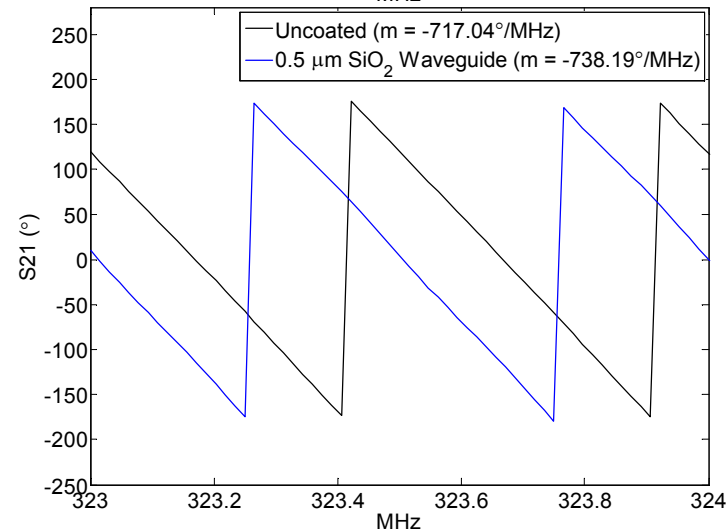
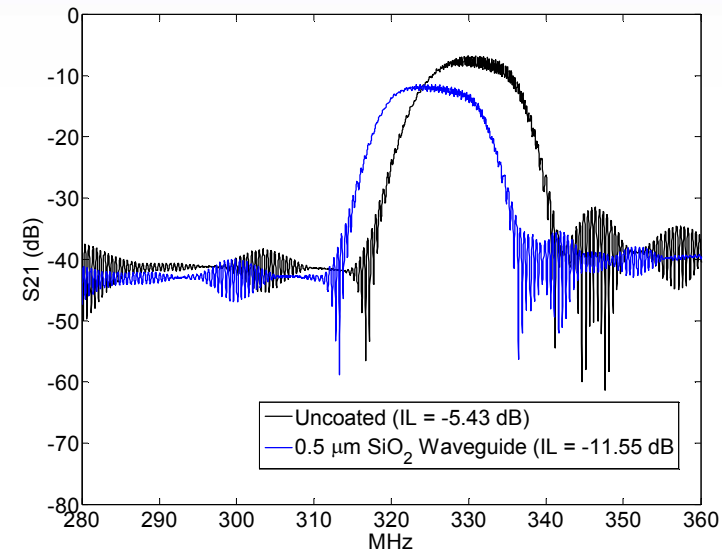
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Sensor IDT Design

Grating plus one SPUDT cell type:

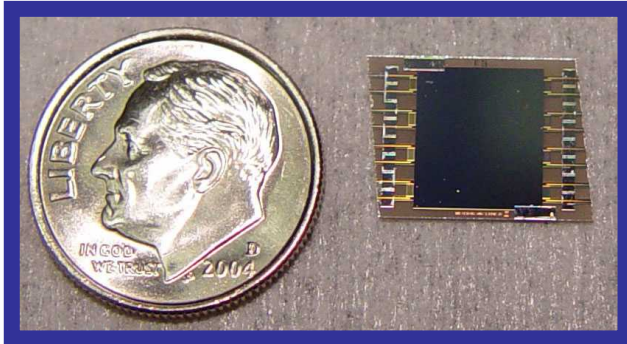


Experimentally tuned SPUDT cell for best response



Four Channel Love Wave Array

Four Channels per Die



Each Channel:
8.1 mm x 0.75 mm

$$\delta = \sqrt{\frac{\eta}{\pi \rho \nu}}$$

Wave penetration depth (δ):
31 nm @ 330 MHz in water
($\eta = 1 \text{ cP}$, $\rho = 1 \text{ g/cm}^3$)

SH-SAW Design Summary (no waveguide)

	(1)	(2)	(3)
Center Frequency	320 MHz	332 MHz	330 MHz
Insertion Loss	-7.28 dB	-7.62 dB	-5.43 dB
3 dB Bandwidth	9 MHz	10 MHz	7 MHz
Amplitude Ripple	0.8 dB P-P	3.9 dB P-P	2.5 dB P-P
Phase Ripple	2° P-P	4.4° P-P	2.8° P-P
Impedance near f_c	45.5 + j4.6 Ω	-	49 + j1.2 Ω
Cross Talk	38 dB	38 dB	39 dB
Phase Slope (uncoated)	-720.46°/MHz	-723.18°/MHz	-717.04°/MHz

Waveguide

Piezoelectric Model:
Green's function method

$$\overline{kG(s)} = \begin{bmatrix} \overline{u_1^{(1)}} & \overline{u_1^{(2)}} & \overline{u_1^{(3)}} & \overline{u_1^{(4)}} \\ \overline{u_2^{(1)}} & \overline{u_2^{(2)}} & \overline{u_2^{(3)}} & \overline{u_2^{(4)}} \\ \overline{u_3^{(1)}} & \overline{u_3^{(2)}} & \overline{u_3^{(3)}} & \overline{u_3^{(4)}} \\ 1 & 1 & 1 & 1 \end{bmatrix} \begin{bmatrix} \overline{T_{13}^{(1)}} & \overline{T_{13}^{(2)}} & \overline{T_{13}^{(3)}} & \overline{T_{13}^{(4)}} \\ \overline{T_{23}^{(1)}} & \overline{T_{23}^{(2)}} & \overline{T_{23}^{(3)}} & \overline{T_{23}^{(4)}} \\ \overline{T_{33}^{(1)}} & \overline{T_{33}^{(2)}} & \overline{T_{33}^{(3)}} & \overline{T_{33}^{(4)}} \\ \overline{D_3^{(1)'}} & \overline{D_3^{(2)'}} & \overline{D_3^{(3)'}} & \overline{D_3^{(4)'}} \end{bmatrix}^{-1}$$

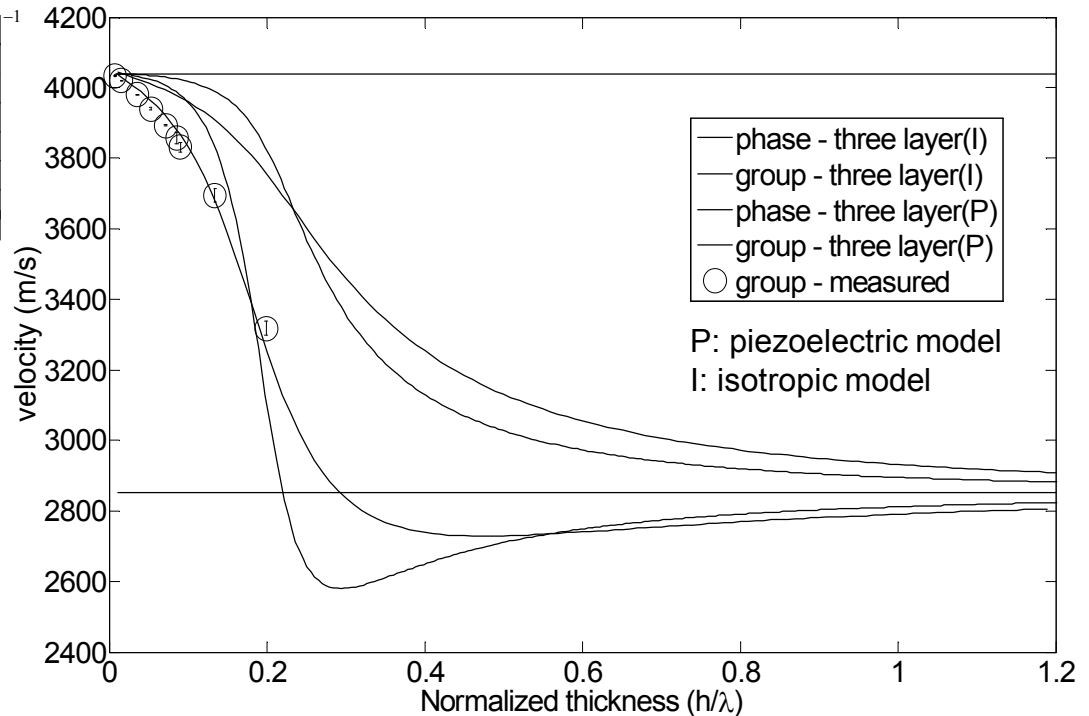
Qiao, D., W. Liu, et al. (1999)

$$\varepsilon_s(s) = \frac{1}{\varepsilon_o G_{44}(s)}$$

Find all poles and create list of
velocities as thickness increases

Isotropic Case:
Solve dispersion equation for
three layered system

Dispersion Curves:
SiO₂ Waveguide on 36° YX LTO



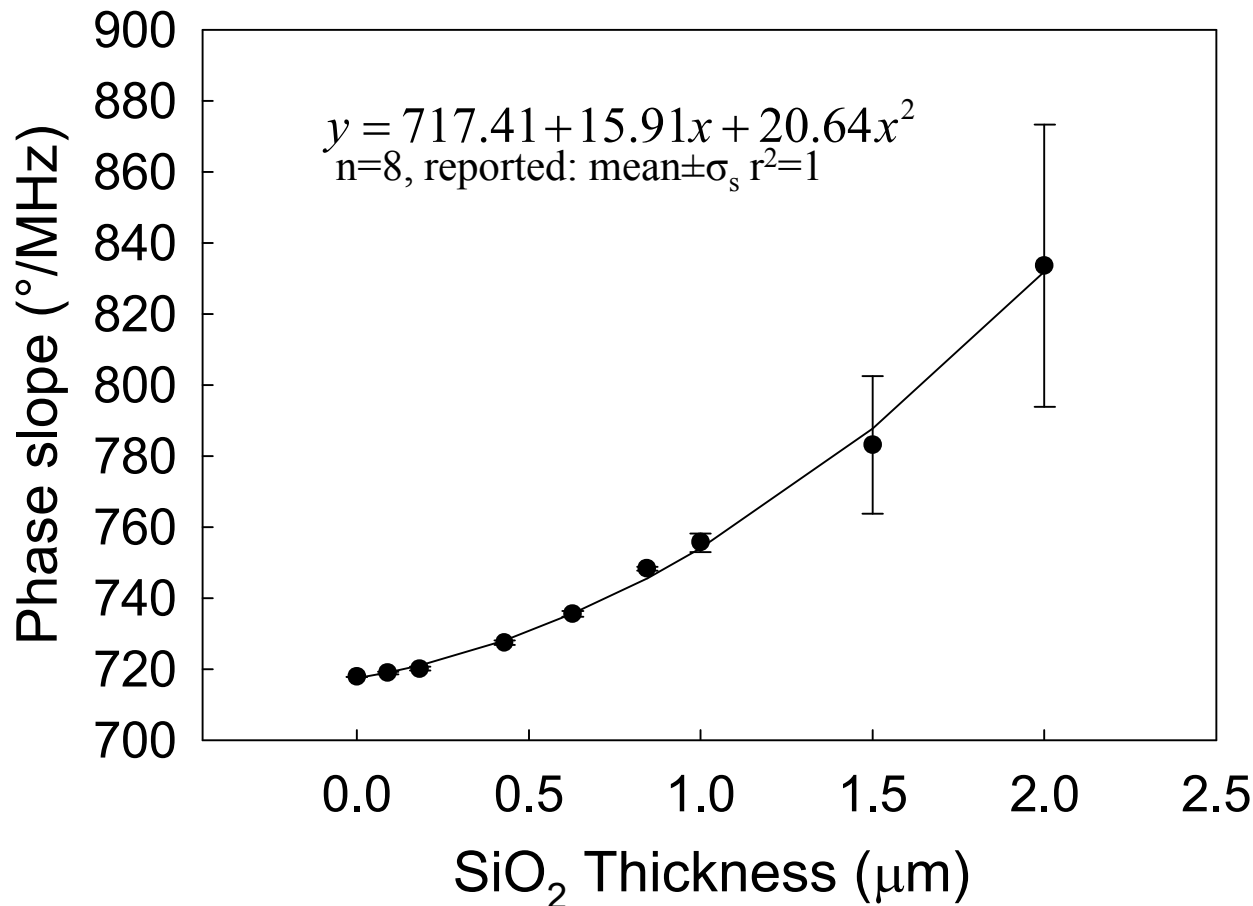
P: piezoelectric model
I: isotropic model

Dispersion for isotropic model differs
significantly from the full piezoelectric model

Waveguide, cont'd

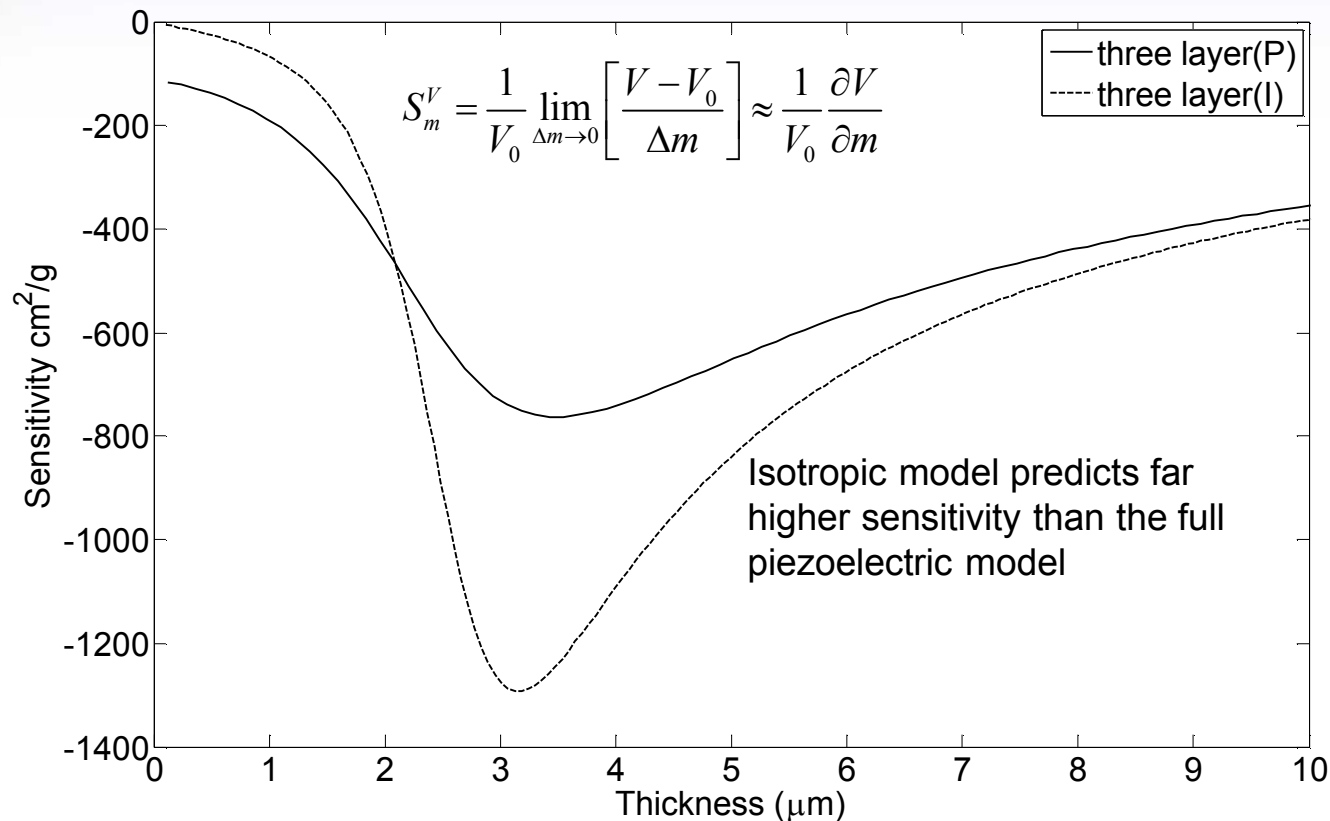
Nondestructive Analysis of Waveguide Sensitivity:

- Phase slope is an indicator of reproducibility for sensitivity
- Indirect measure of sensitivity without performing mass detection experiments



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Sensitivity Analysis



Model	Optimal Thickness		Optimal Frequency	Sensitivity	
	h/λ	h (μm)	f_{opt} (MHz)	$1/\rho_2\lambda$	cm^2/g
Plate mode	-	-	-	-	-1.22
Three layer(P)	0.290	3.55	285.01	-2.05	-761.97
Three layer(I)	0.260	3.19	287.53	-3.48	-1291.81

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Temperature Compensation

TCF:

36° YX LTO = -35 ppm/°C

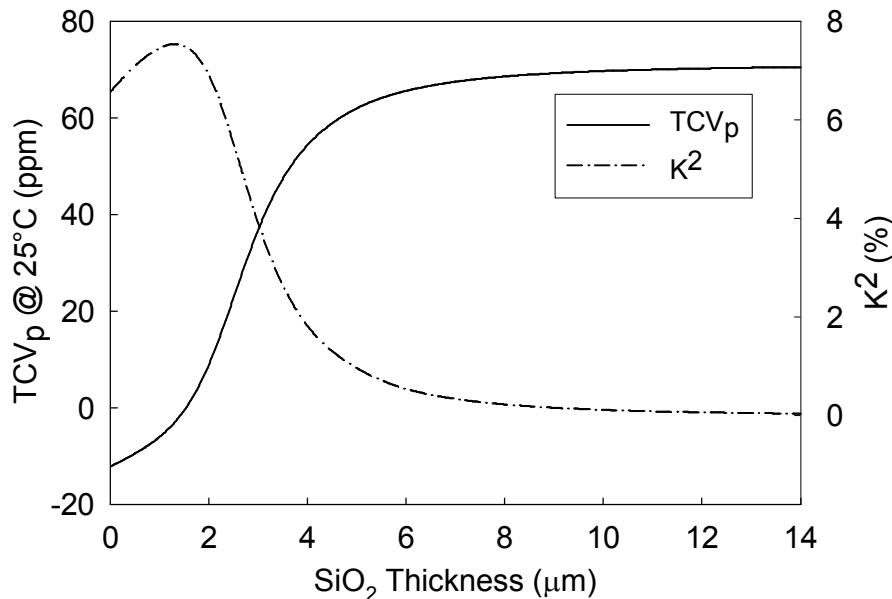
Silicon dioxide = +80 ppm/°C, $\alpha = +9$ ppm

α : Temperature expansion coefficient

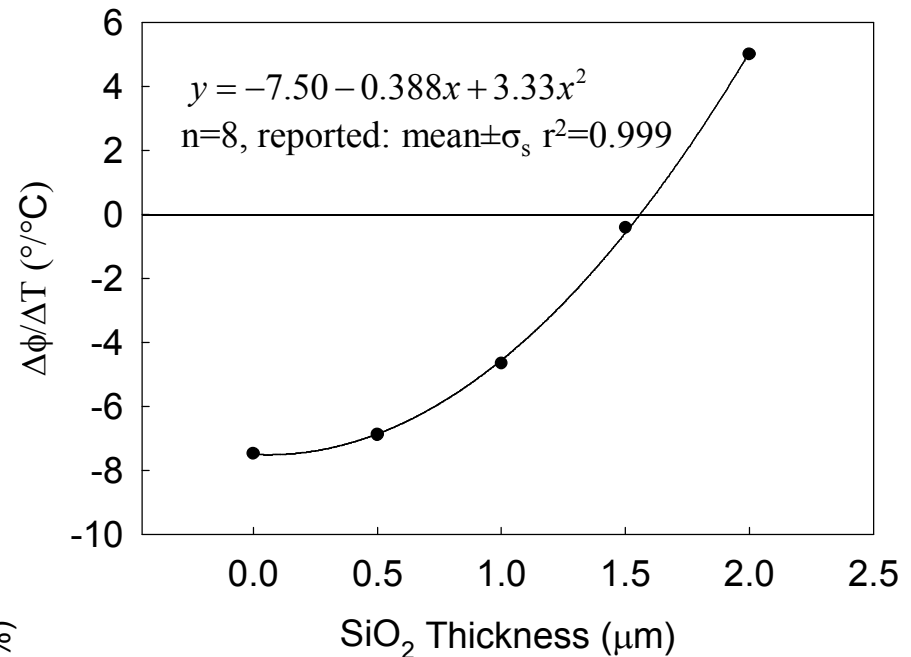
$$TCV_p = \alpha - TCF$$

$$TCV_p = \frac{1}{V(25^\circ\text{C})} \frac{\partial V_p}{\partial T} \approx \frac{1}{V(25^\circ\text{C})} \frac{V(35^\circ\text{C}) - V(25^\circ\text{C})}{10^\circ\text{C}}$$

Calculated TCV_p vs. Waveguide Thickness

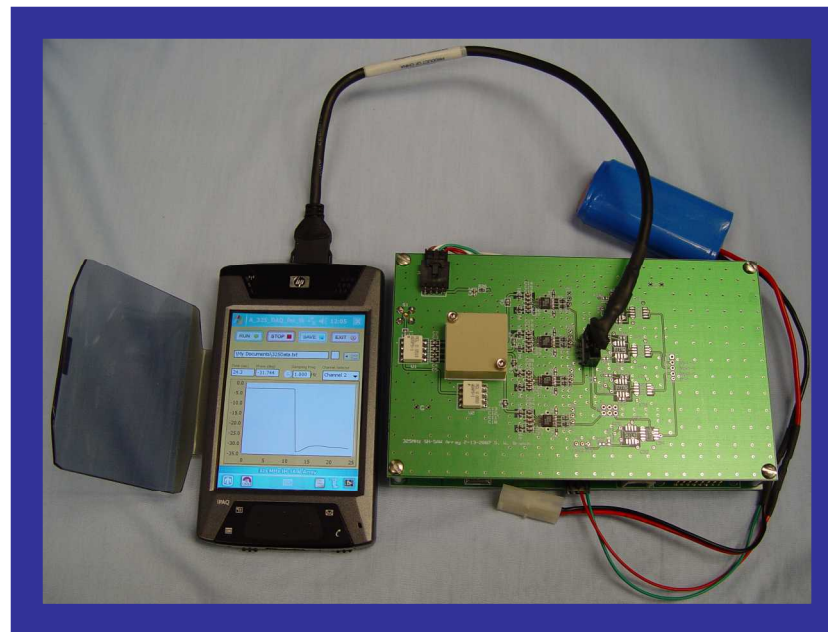
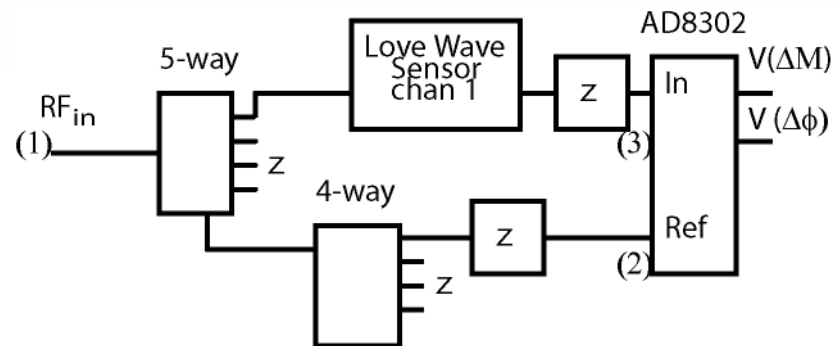


Measured Phase Shift/Temperature Shift
vs. Waveguide Thickness



Phase Based Detection System

- Tunable RF source (310-350 MHz)
 - Multiple frequency analysis
- Signals are split to drive 4 Love Wave sensors
- 5V DC, 20 hr operation
- AD8302
 - Phase difference
 - Magnitude difference
 - Φ resolution of 0.01°
- Labview software for DAQ and Analysis
- PDA or Laptop Readout
- Sample rate: 1k



Sensitivity to Mass Density

Sensitivity due to density/viscosity:

Method: Malavé, A., U. Schlecht, et al. (2006)

$$S_{\phi,\eta} = \sqrt{4\pi\nu} \left(\frac{\Delta\phi}{\sqrt{\rho\eta}} \right)$$

ν : frequency of Love Wave sensor

ρ : fluid density (g cm^{-3})

η : fluid viscosity (Pa s)

ϕ : phase shift ($^\circ$)

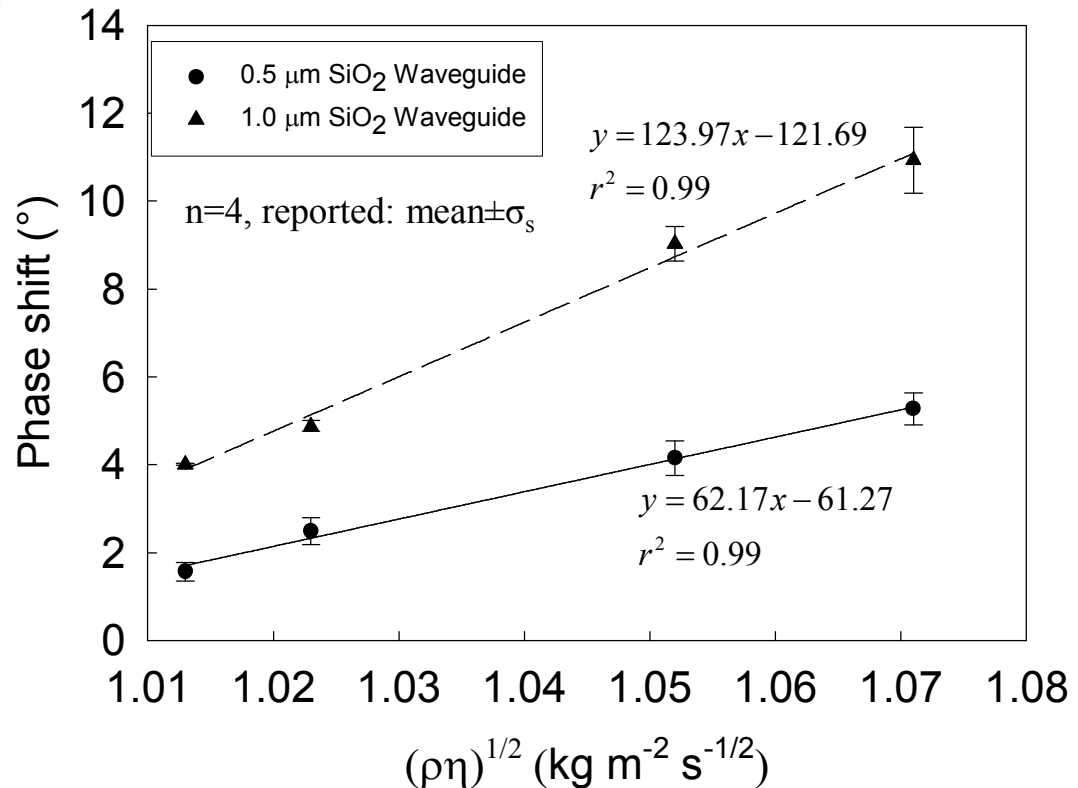
$$\text{Slope: } \frac{\Delta\phi}{\sqrt{\rho\eta}}$$

0.5 μm Waveguide ($\nu = 328 \text{ MHz}$):

$$S_{\phi,\eta} = 4.31 \pm 0.33 \text{ } ^\circ \text{ mm}^2 / \text{ng}$$

1.0 μm Waveguide ($\nu = 325 \text{ MHz}$):

$$S_{\phi,\eta} = 7.19 \pm 0.74 \text{ } ^\circ \text{ mm}^2 / \text{ng}$$



Detection limit:

Noise (N): 0.01° , $5N$
 $= 6.71 \pm 0.40 \text{ pg} / \text{mm}^2$

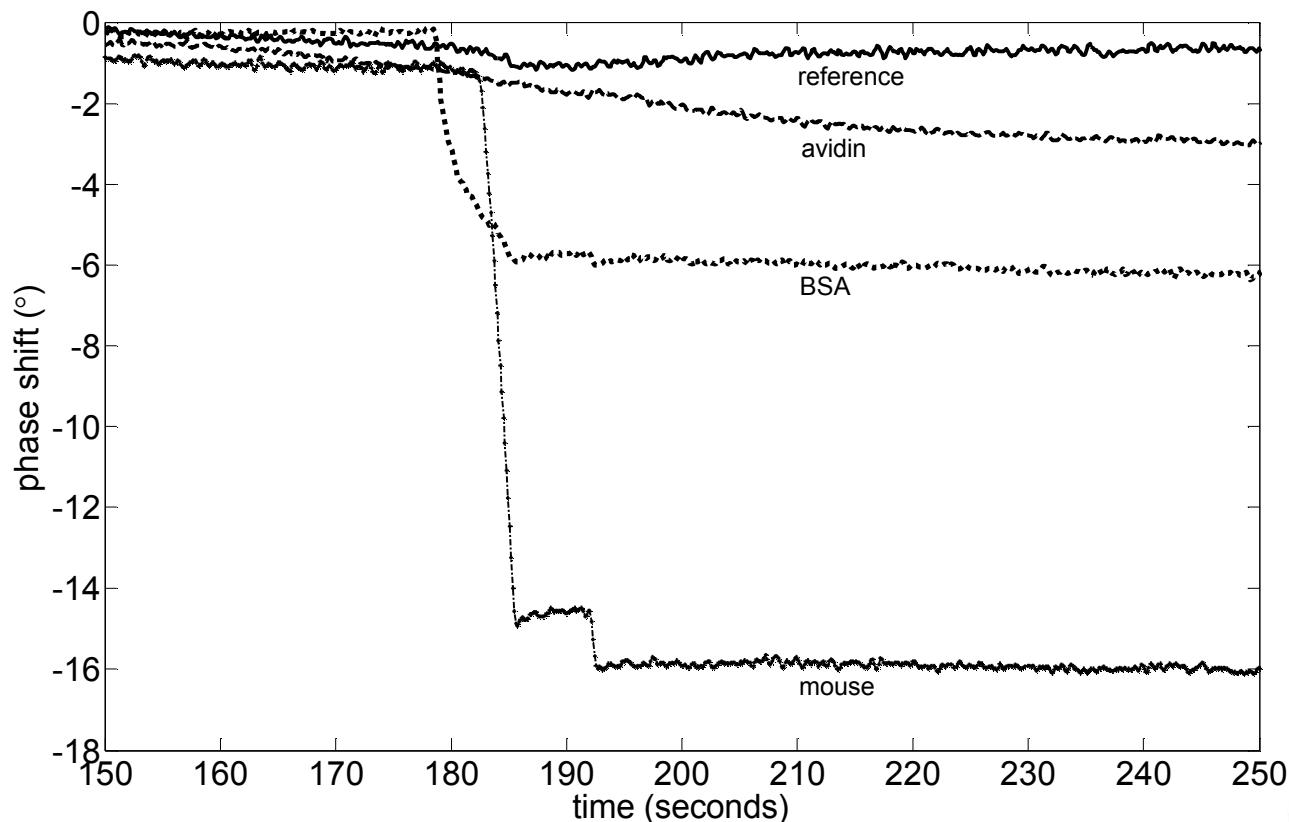
Conservative values



Multi-Analyte Biodetection

Multi-Analyte Detection:

- 1) IgG: Anti-avidin, antigen: avidin
 - 2) IgG: Anti-BSA (albumin), antigen: BSA
 - 3) IgG: Anti-mouse, antigen: (mouse) anti-rabbit
- Antigens combined in a single fluid sample (50 μ l) @ 100 ng/ml each
- Flow cell: 4 μ l
Flow rate: 10 μ l/min, carrier buffer: 10 mM PBS



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Conclusions

- We have developed an IDT suitable for high frequency Love Wave sensors.
- The IDT design has an excellent S21 response, minimal bulk wave interferences, and excellent phase linearity.
- A Love wave array was fabricated with four detection channels.
- A phase detection system was developed to monitor four channels simultaneously.
- Sensitivity results indicate a detection limit of 6.71 ± 0.40 pg / mm² with 0.01° resolution at 5 times the noise level.
- Performed multi-analyte biodetection of a complex sample.