

# MEASUREMENT OF SYSTEM DYNAMIC RANGE IN THE TIME DOMAIN

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# Outline

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- Introduction
- Simple design considerations
- Demonstration of signal-dependent noise
- Causes of diminished time-domain dynamic range
- Understanding and diagnosing deficiencies
- Summary



# Introduction

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- Time-domain radar-cross-section response of a target is often utilized to evaluate objects comprised of both small and large scatterers
- To do so requires a large dynamic range in the time domain
- Wideband frequency-domain measurements are often used to determine time-domain response
  - Collect complex frequency-domain data
  - Apply correlation operation to the data to produce a processed time-domain response
- Of interest for our application is a PNA based measurement system that uses a frequency-stepped source, and a fast Fourier transform algorithm to produce the time-domain response



# Time-Domain Dynamic Range

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- **Important:** the instantaneous dynamic range associated with frequency-domain measurements *is not* the same as the time-domain dynamic range
- The coherent integration inherent in the correlation process serves to enhance the time-domain dynamic range, while gain compression, phase noise in the source, quantization noise, calibration errors, and other noise sources serve to degrade the dynamic range
- Time-domain dynamic-range specification for a radar is the range of signal-levels between the noise+clutter level and the response of the large target that corresponds to the top of the linear-response region of the radar



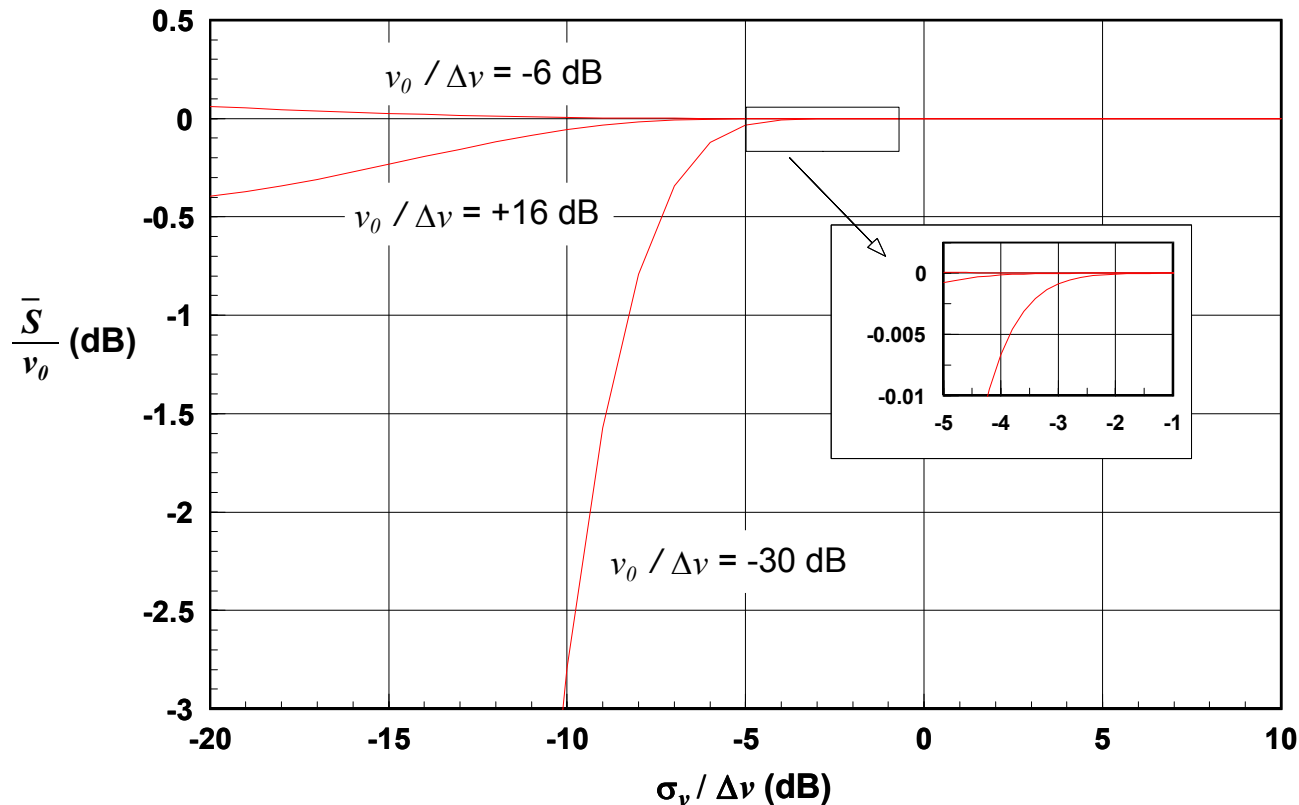
# Simple Design Considerations

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- The maximum instantaneous dynamic range of the system is determined by the number of bits in the A/D when the system gain is adjusted for proper noise level
- The system dynamic range can be extended downward below the least-significant bit through coherent digital signal processing
- The process of quantizing a continuous signal introduces quantization error that is additive noise
- The analog-to-digital converter has a finite number of bits that limits the maximum signal that can be accommodated
- The noise level at the input to the analog-to-digital converter must be adjusted properly for the mean signal to be determined to higher precision than the least-significant bit of the quantizer

# Simple Design Considerations

- For the mean output of the A/D to be a linear function of the input signal, the noise level must satisfy  $\sigma_v / \Delta v \geq -4$  dB



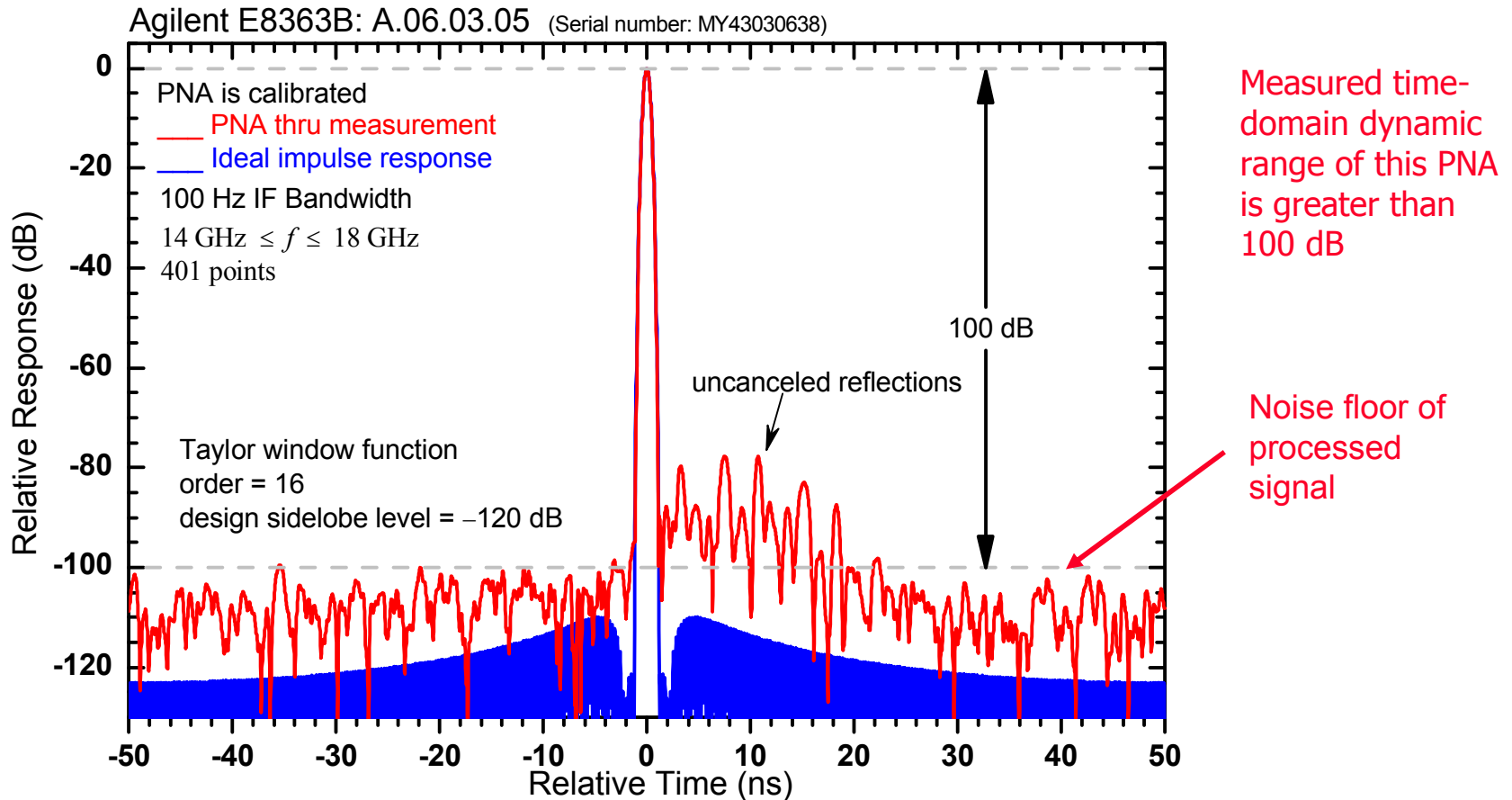
$\bar{S}$  = normalized mean output

$\sigma_v$  = rms noise voltage

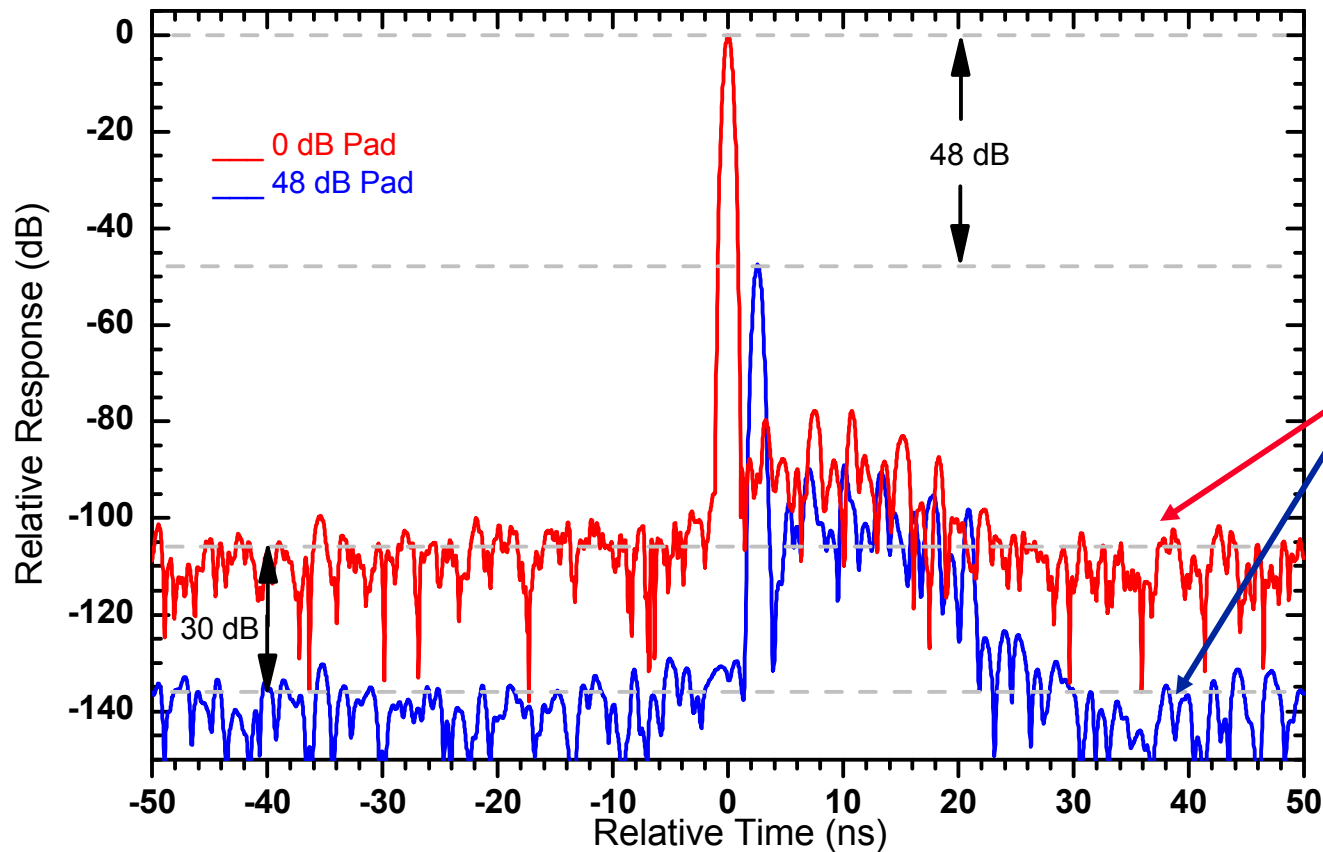
$\Delta v$  = voltage corresponding to the least significant bit

$v_0$  = input voltage

# Demonstration of Signal-Dependent Noise



# Add 48 dB Attenuation to Signal Path

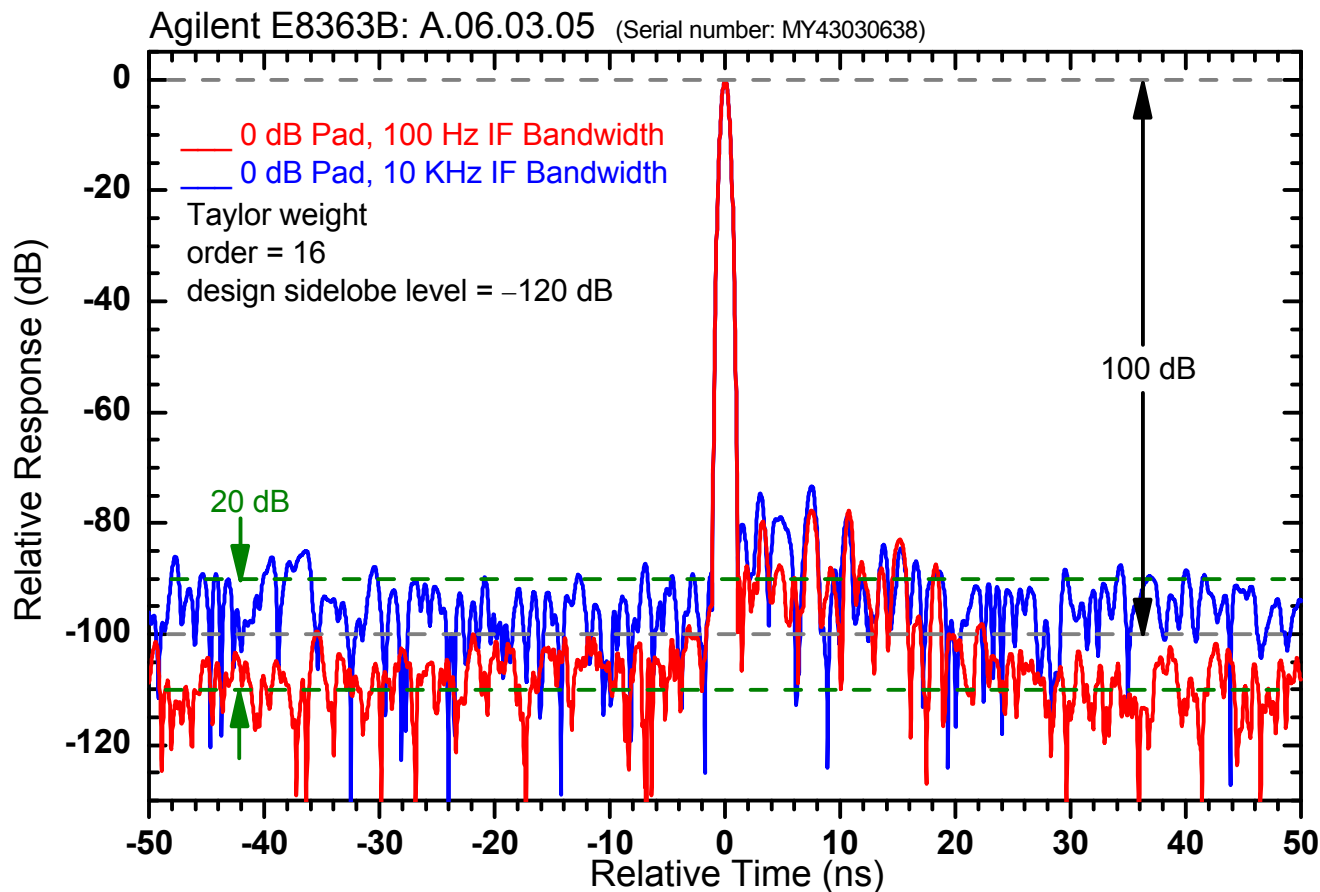


Noise floor depends on the amplitude of the signal

Decreasing signal by 48 dB decreases noise floor by 30 dB.



# Increase IF Bandwidth from 100Hz to 10KHz



Noise level  
increases by ratio  
of IF bandwidths  
or 20 dB



# Causes of Diminished Time-Domain Dynamic Range

1. Gain compression and non-linear response
2. Inadequate signal-to-(noise+clutter) for calibration
3. Improper gain distribution throughout the system
4. Excessive numerical error in characterization of calibration target
5. Excessive phase noise in the RF source
6. Timing jitter



# Gain Compression and Nonlinear Response

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- In a nonlinear system, thermal noise can be mixed with the signal, becoming a multiplicative factor, and leading to a noise component whose amplitude is a function of the signal
- Consider a system with a voltage gain  $g[V]$ . For an input signal  $s$  with noise  $n$ , the output would be

$$s_{out} = (s + n)g[s + n] = g_0(s + n) + g_2(s + n)^3 + \dots$$

- To first order in input noise, the output noise is

$$n_{out} = n(g_0 + 3g_2s^2 + 5g_4s^4 + \dots)$$

- If the signal is large enough that  $g_0 < 3g_2s^2$ , then the noise will be dominated by the signal-dependent component
- Maximizing the linearity of the entire system over the range of expected signals will reduce the hardware's contribution to signal-dependent noise



# Inadequate Signal/(Noise+Clutter) at Calibration

- Calibrated RCS measurement can be written:

$$\gamma_{tgt} = \left( s_{tgt} + \varepsilon_{tgt} \right) \frac{\gamma_{cal}}{s_{cal} + \varepsilon_{cal}}$$

- Using a binomial expansion for the denominator

$$\gamma_{tgt} = \left( s_{tgt} + \varepsilon_{tgt} \right) \frac{\gamma_{cal}}{s_{cal}} \left( 1 - \frac{\varepsilon_{cal}}{s_{cal}} + \frac{\varepsilon_{cal}^2}{s_{cal}^2} - \dots \right)$$

- The term  $s_{tgt} \frac{\gamma_{cal}}{s_{cal}} \frac{\varepsilon_{cal}}{s_{cal}}$  is signal dependent noise+clutter

brought in from the calibration

- Maximizing the signal-to-noise ratio,  $s_{cal} / \varepsilon_{cal}$ , during calibration measurement will reduce the calibration contribution to signal-dependent noise and clutter

# Time-Domain Response of Two 5/16" Spheres

File: 2 Spheres\_8-

Calibrated Using a Sphere

Pregates Disabled

User Gate disabled

Date: 04-Jul-07 Time: 23:29 Operator:

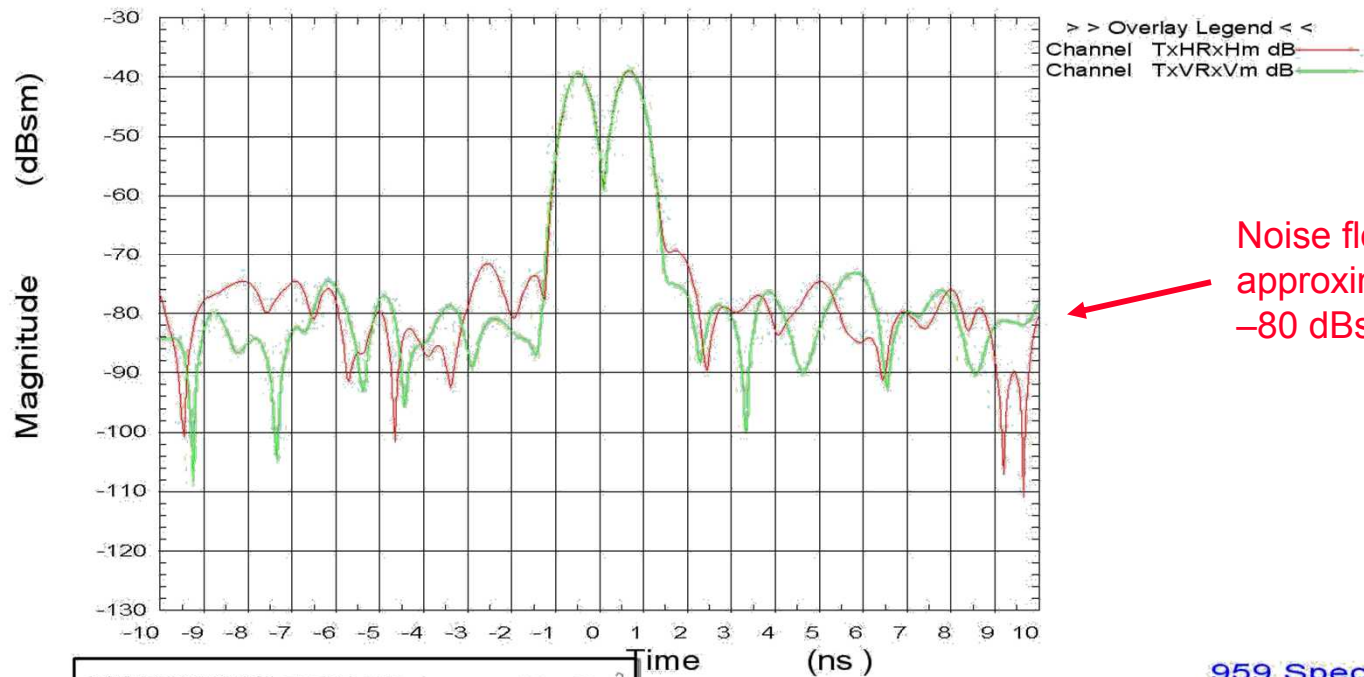
Ref. Target Dim: 20.00 in N/A in

401 Freqs: Start: \*\*\*\*\*

Stop: 10.000 GHz

Azimuth : -6.00 Degs

2 Spheres .3125 inch separated 6 inches

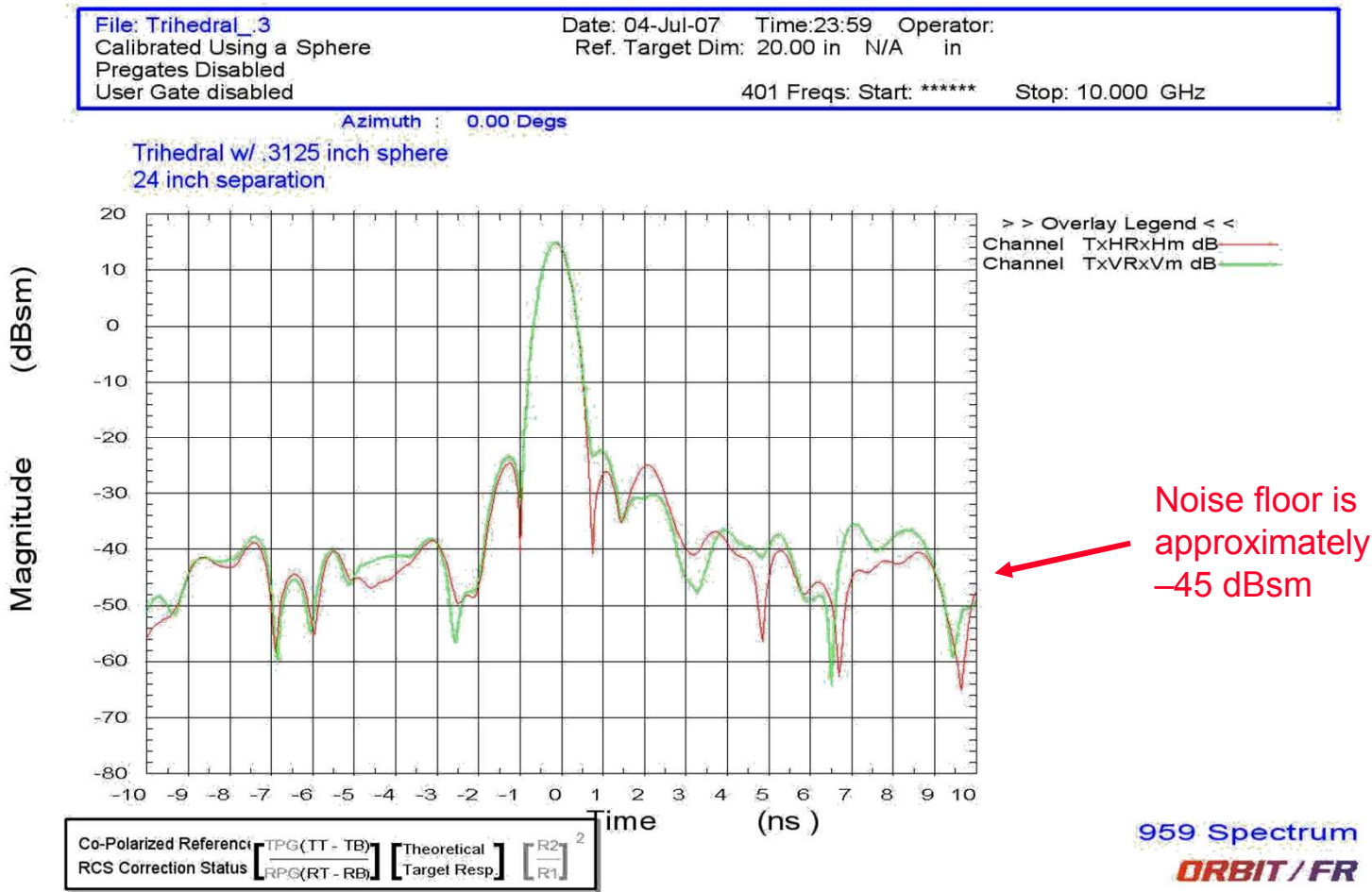


Co-Polarized Reference  $\left[ \frac{TPG(TT - TB)}{RPG(RT - RB)} \right] \left[ \frac{\text{Theoretical Target Resp.}}{R1} \right]^2$

959 Spectrum

ORBIT / FR

# Time-Domain Response of a Large Trihedral





# Improper Gain Distribution

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- Gain must be distributed properly throughout the system to minimize the thermal noise at the output of the system
- Adequate gain early in the receiver chain is required
  - Low noise amplifiers as close as possible to the antenna ports
- Gain carefully distributed throughout the system to overcome losses introduced by switches, cables, etc. and minimize the effect of additional thermal-noise contributions
- The result will maximize the dynamic range and minimize the signal-dependent noise



# Inaccurate characterization of calibration target

- Suppose the calibration target is not characterized accurately
- Error in the computation will introduce signal-dependent noise
- Replace the term  $\gamma_{cal}$  with  $\gamma_{cal} + \varepsilon_{comp}$  in the earlier equation introduces a new signal-dependent term

$$s_{tgt} \frac{\varepsilon_{comp}}{s_{cal}}$$

- This term can destroy the time-domain dynamic range of a system





# Phase Noise in the RF Source and Timing Jitter

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- Both phase noise in the RF source and timing jitter are another source of signal-dependent noise in the system
- RF-source and timing-clock characteristics will provide an upper limit on the obtainable dynamic range
- It is always good practice to lock all timing signals to a single, stable clock



# Summary

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- Reviewed and discussed design and performance aspects of a measurement radar system relative to time-domain dynamic range
- A qualitative understanding can be extracted from this review that is useful for understanding and evaluating radar performance
- This review serves as a reminder of the numerous opportunities for degradation of time-domain dynamic range