



Generating and Performing Experiments Within the In-Drift Environments Anticipated in the Proposed Yucca Mountain Repository

New Orleans, Louisiana

March 18th, 2008

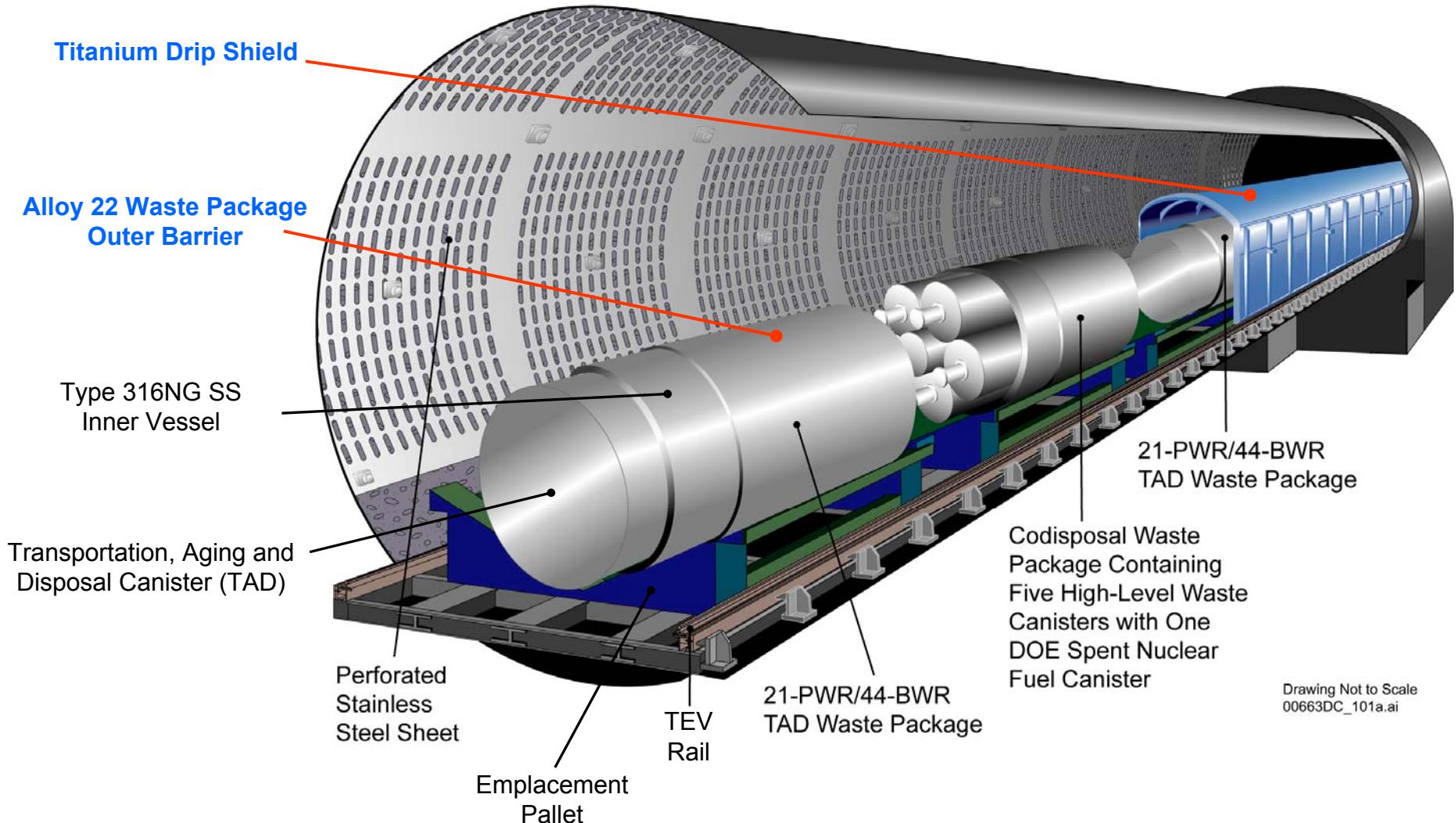
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Principal Member Technical Staff
Yucca Mountain Project

Not LSN Relevant

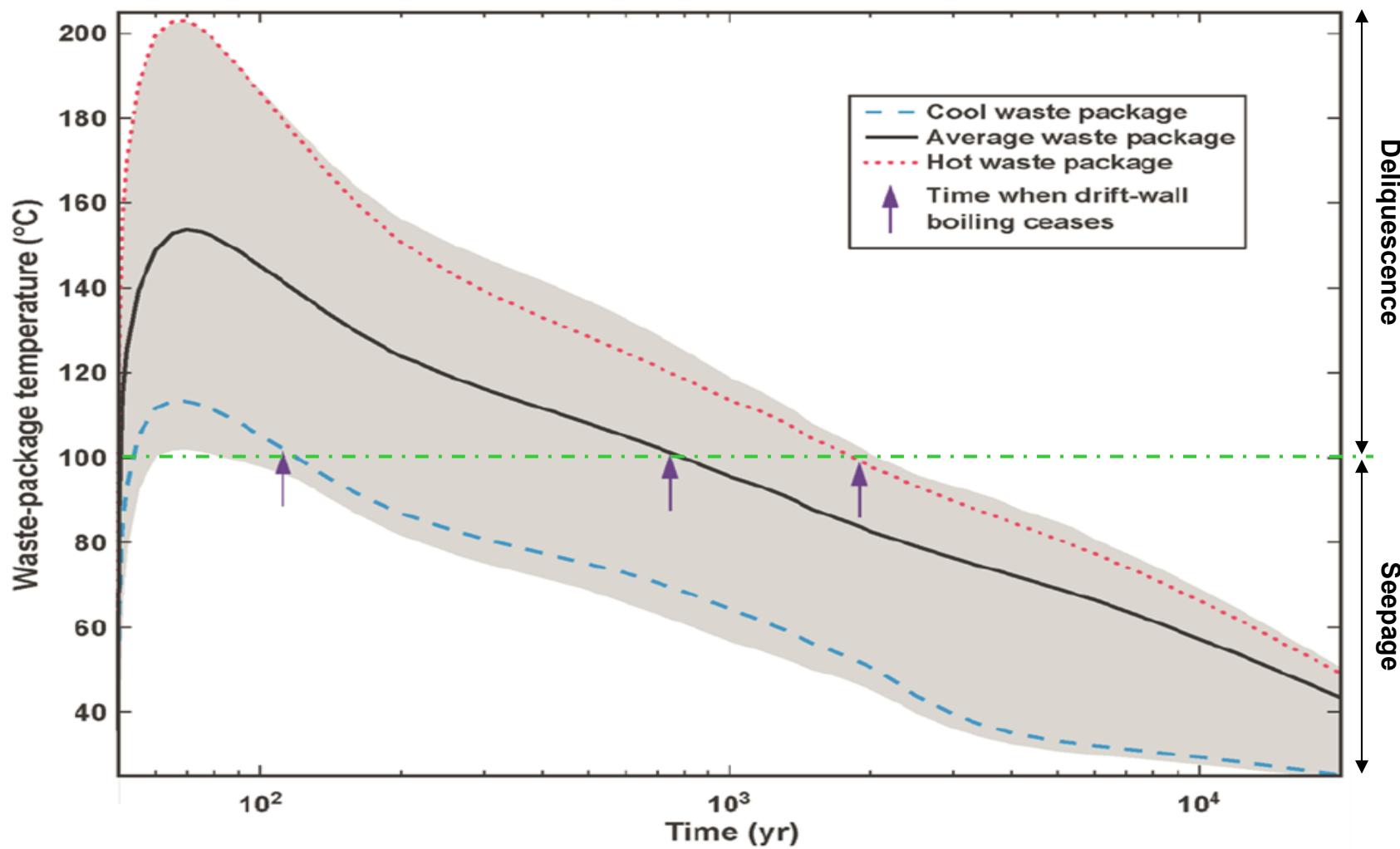
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The Engineered Barrier System



Evolution of Temperature/RH on the Waste Package Surface



Two Types of Chemical Environments

Deliquescence

- Soluble salts deposited on the WP during pre-closure
- Drip shields control post-closure dust accumulation
- Multi-salt assemblages control deliquescence at higher temperatures
- Brine compositions become dilute as T decreases RH increases
- Amount of brine contacting metal surfaces is limited
- Chemistry is moderated by contact with rock-forming minerals in dust
- Brines change with time due to degassing, deliquescence

Seepage

- Seepage may occur after cooldown ($T_{WP} < 105^{\circ}C$)
- WP outer barrier is protected by the drip shields
- Residence time (equilibrium with T, RH at WP surface) controls the corrosion environment
- Chemical conditions (pH, Cl^- , NO_3^- , NO_3^-/Cl^-) are potentially corrosive early during cooldown
- Chemical fractionation may occur during transport

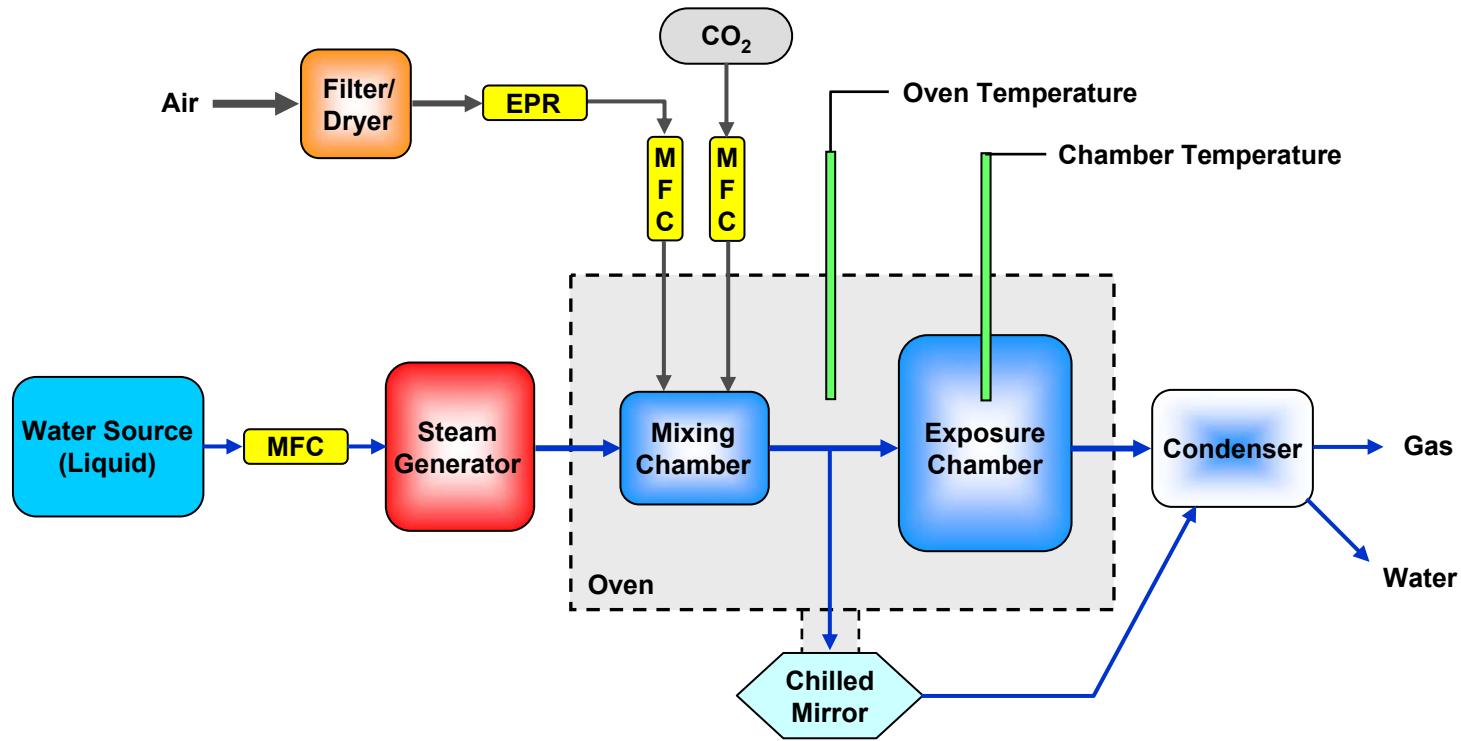
Current Area of Interest

- Bulk of work conducted to date focused on seepage environments
- Deliquescent conditions have been addressed to a limited extent
 - Project data – Thin film experiments, Autoclave experiment
 - CNWRA – corrosion performance in bulk brines
- Focus of this work – behavior of engineered barrier materials under deliquescent conditions
 - Environmental conditions
 - Corrosion performance



Generation of a High Dewpoint Environment (95°C+) at Atmospheric Pressure

- Schematic of High-T, controlled moisture content system



EPR = Electronic Pressure Regulator and MFC = Mass flow controller

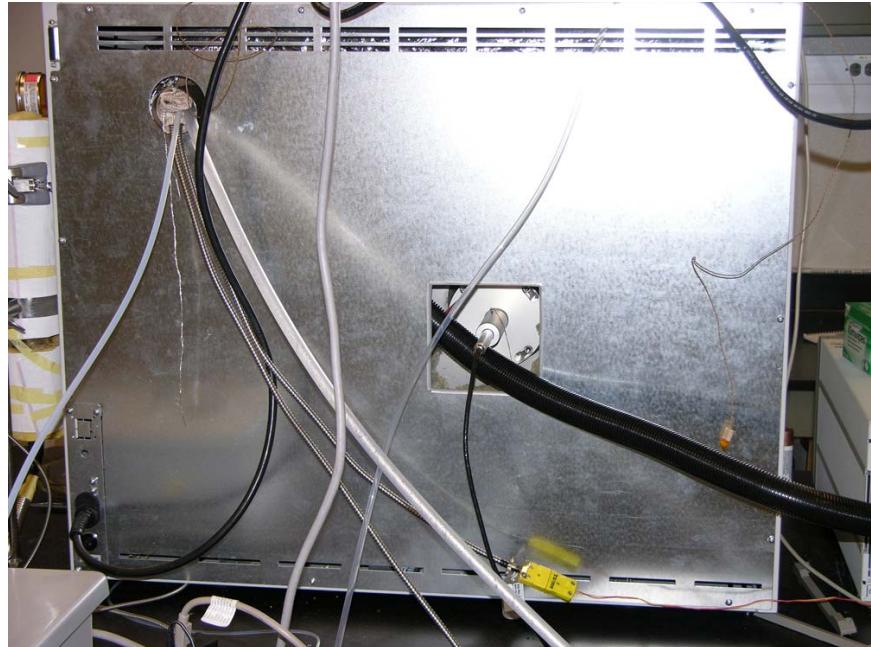
High Temperature, Controlled Dewpoint System



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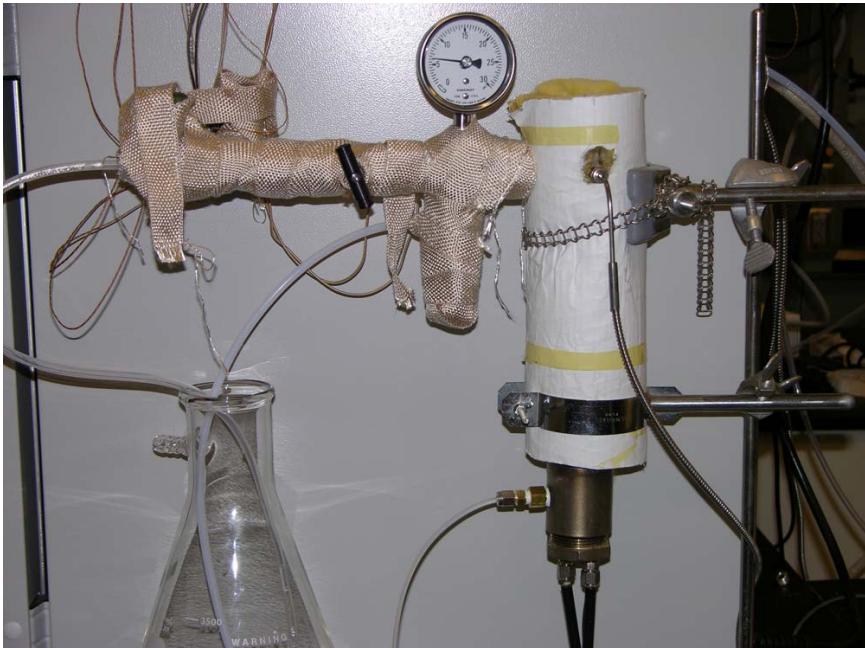
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High Temperature, Controlled Dewpoint System



- **Preheaters within the oven as well as heated lines required to prevent condensation**

High Temperature, Controlled Dewpoint System



- **Steam delivery system allows precise mass control of water delivery to the exposure chamber**

Relevant Dust Sources and Composition

Current model is based on two sources of dust:

- Yucca Mountain tunnel dusts
 - Dominantly rock powder, <1% highly soluble salts (Peterman et al., 2003, *IHLRWM Conf. Proceedings*)
 - Important deliquescent mineral assemblages:
 - NaCl-KNO₃
 - NaCl-KNO₃-NaNO₃
 - NaCl-KNO₃-NaNO₃-Ca(NO₃)₂
- Atmospheric dust
 - Site-specific data, 6 locations near YM (Reheis and Kihl, *JGR*, 1995)
 - Highly soluble salt load—10.5% (avg)
 - Carbonate content—9.5% (avg)
 - Solubles—National Atmospheric Deposition Program (NADP) regional precipitation (rain-out) data

Sample #	Ca mg/L	Mg mg/L	K mg/L	Na mg/L	NH ₄ ⁺ mg/L	NO ₃ ⁻ mg/L	Cl ⁻ mg/L	SO ₄ ²⁻ mg/L	NO ₃ ⁻ /Cl ⁻
NV00-2002	0.48	0.044	0.013	0.059	0.26	1.14	0.09	0.46	7.3
NV00-2001	0.66	0.068	0.042	0.113	0.69	2.15	0.16	1.01	7.7
NV00-2000	1.21	0.137	0.055	0.263	1.01	3.24	0.36	1.35	5.2

NADP/NTN 2000, Part 2.; NADP/NTN 2001, Part 2.; NADP/NTN 2002, Part 2.



Brine Evolution in a Thin Dust Layer

- **Quantity of salts is low in the brine layer**
 - $1.8 \mu\text{L}/\text{cm}^2$ (18 μm thick layer) at 120°C – decreasing with increasing temperature
- **Numerous processes which may alter the composition of the brine**
 - Acid degassing
 - Reaction with other material in the dust
 - Dilution due to changes in atmospheric dewpoint
- **Relevant brine composition will be a function of the initial salt chemistry in the dust, but will not necessarily be identical to the initial chemistry.**



Processes Affecting Brine on the Waste Package Surface

- Acid degassing — $\text{H}^+_{(\text{aq})} + \text{Cl}^-_{(\text{aq})} \leftrightarrow \text{HCl}_{(\text{aq})} \leftrightarrow \text{HCl}_{(\text{g})}$
 - Ca-chloride brines degas and dry out (TGA experiments)
 - Multiple-salt assemblages can deliquesce at higher temp:
 - Acid-degassing may occur initially, but less as pH increases
 - Brines may not degas sufficiently to dry out
 - NO_3/Cl minimum ratio is controlled by temperature
- Reactions with silicate minerals in dust
 - Silicate dissolution buffers pH
 - Ca, Mg removed from brine as silicate phases
 - Deliquescence RH generally increases (brines may dry out)
 - Possible consumption of chloride by silicates
 - Scapolite-, cancrinite-, sodalite-, prehnite-group minerals
 - Clays (exchange for hydroxides)
- Dilution with decreasing temperature, increasing humidity



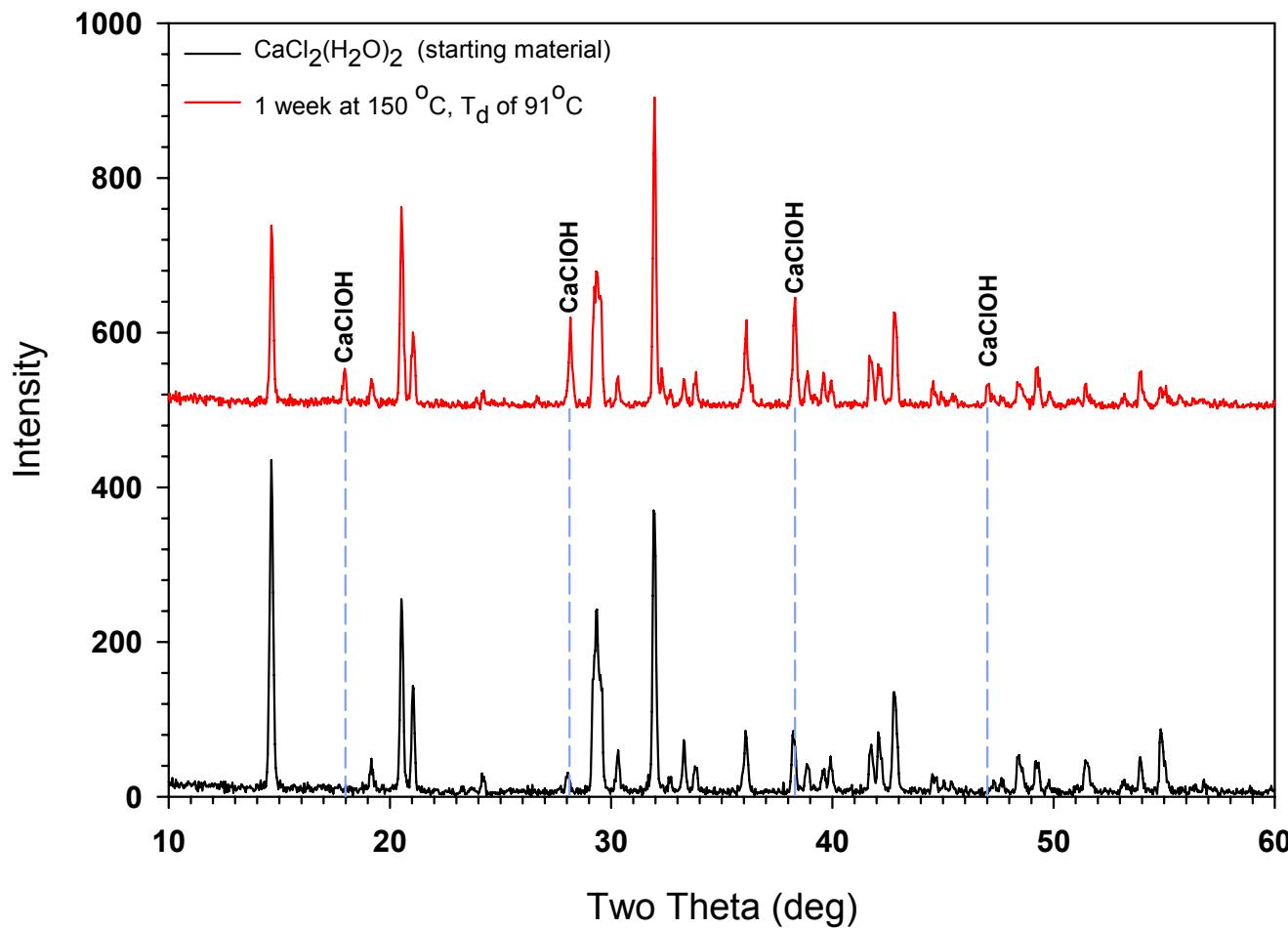
Acid Degassing Example: Calcium Chloride

- 1 week exposure at 150°C with a T_d of 91°C



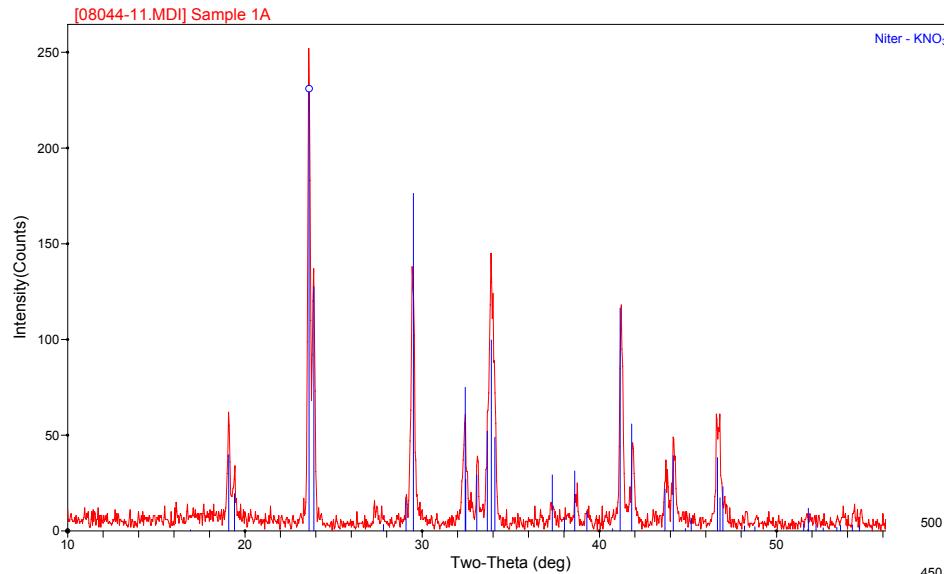
- Salt deliquesced then dried out (at least macroscopically)

Calcium Chloride Degassing at 150°C with a T_d of 91°C



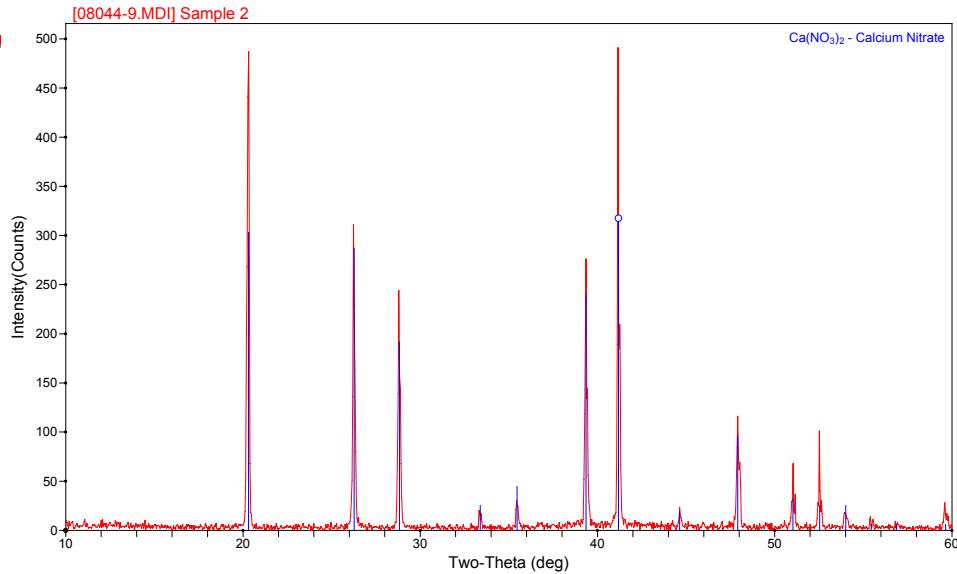
- **CaClOH formed, presumably accompanied by chloride loss as $\text{HCl}_{(\text{g})}$**

Multi-Salt Assemblage Behavior



KNO₃
1.5 wks at T=180C, Tdew=94.5C
No changes observed

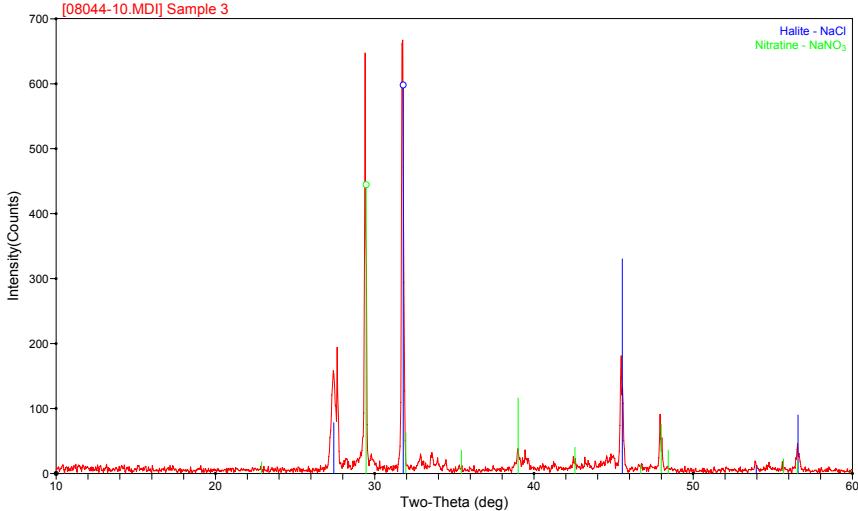
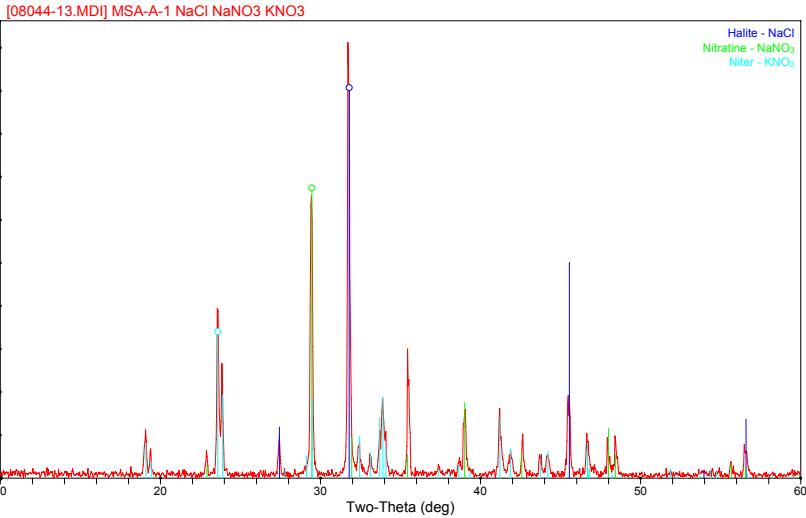
$\text{Ca}(\text{NO}_3)_2 \cdot 3\text{H}_2\text{O}$
1.5 wks at T=180C, Tdew=94.5C
Water removed, but material otherwise unchanged



Multi-Salt Assemblage Behavior

Three salt mixture ($\text{NaCl} + \text{KNO}_3 + \text{NaNO}_3$)

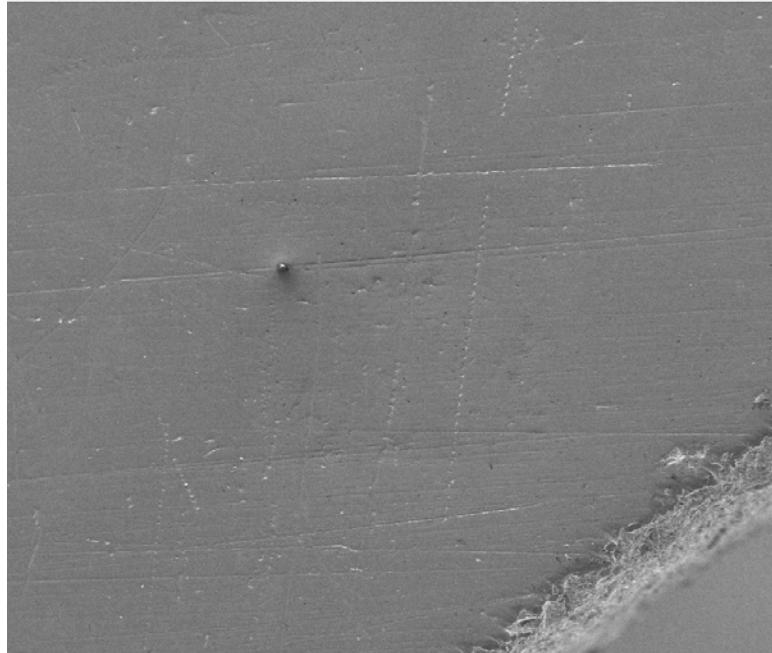
- 1.5 wks at $T=180^\circ\text{C}$, $T_{\text{dew}}=94.5^\circ\text{C}$



Transformation evident in long term thin film experiments - Insoluble particle formed from 4-salt mixture after 50 days at 180°C , pure steam

Alloys 22 and 825 under Deliquescent Conditions

- Samples exposed to 180°C, $T_d \approx 100^\circ\text{C}$ for 50 days
- Samples had a $\text{NaCl} + \text{NaNO}_3 + \text{KNO}_3$ or $\text{NaCl} + \text{NaNO}_3 + \text{KNO}_3 + \text{Ca}(\text{NO}_3)_2$ thin salt film



Mag | Spot | WD | VacMode | HV | Det | Pressure | 400.0 μm
200x | 3.5 | 10.3 mm | High vacuum | 10.0 kV | ETD | --- | C09_crevice



Mag | Spot | WD | VacMode | HV | Det | Pressure | 400.0 μm
200x | 3.5 | 10.3 mm | High vacuum | 10.0 kV | ETD | --- | E09_f-crevice-a

- Neither the Alloy 22 nor the 825 Samples exhibited crevice corrosion
- Note that the 825 sample pictured has not been cleaned – deposits from the salt film are still present

Work performed by R.Rebak, T.Lian, J.Rard, and K.Evans at LLNL



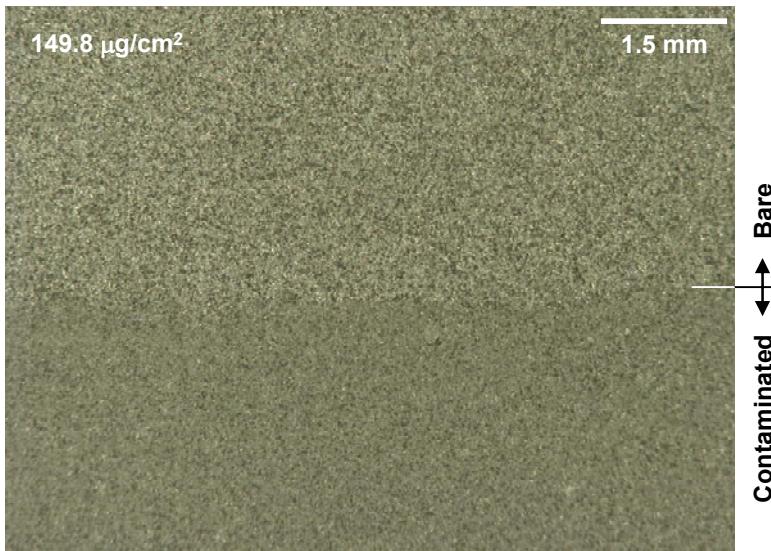
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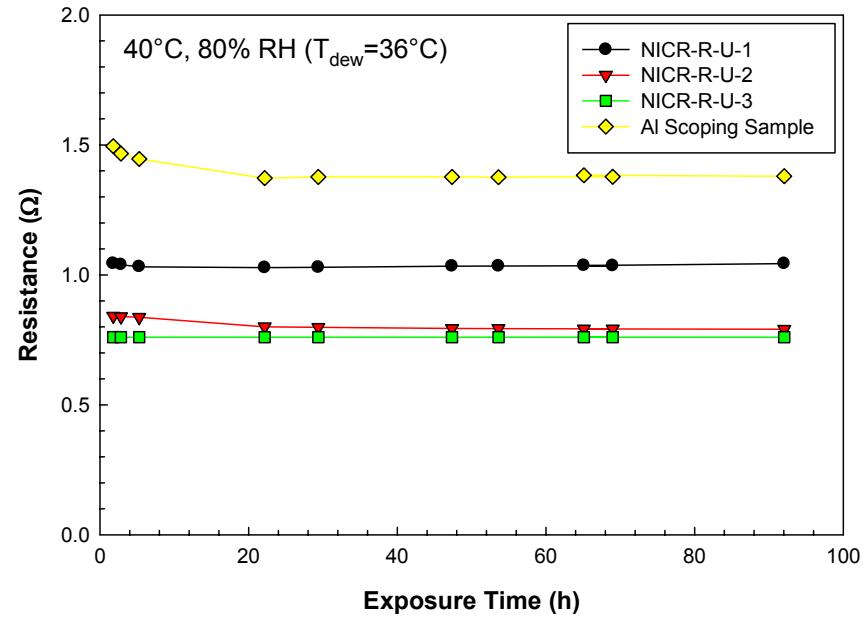
Monitoring Corrosion Under Thin Dust Layer

Proof of concept experimentation

- Fixture capable of operating in low and high temperature chambers
- Samples decorated with $\sim 150 \mu\text{g}/\text{cm}^2$ of 4 salt mixture ($\text{NaCl} + \text{NaNO}_3 + \text{KNO}_3 + \text{Ca}(\text{NO}_3)_2$)



(Alloy 22 coupon shown – rougher surface finish than ribbons)



Summary

- Environmental chamber has been designed and assembled which allows precise control of the dewpoint at elevated temperatures
 - T_{dew} up to $T_{boiling}$ and $T_{chamber}$ in excess of 250°C.
 - Access to all anticipated in-drift conditions during the thermal pulse.
- Brine evolution is a key aspect to assessing corrosion performance during the deliquescent period.
- Electrical techniques aimed at observing corrosion under aggressive conditions are under development.

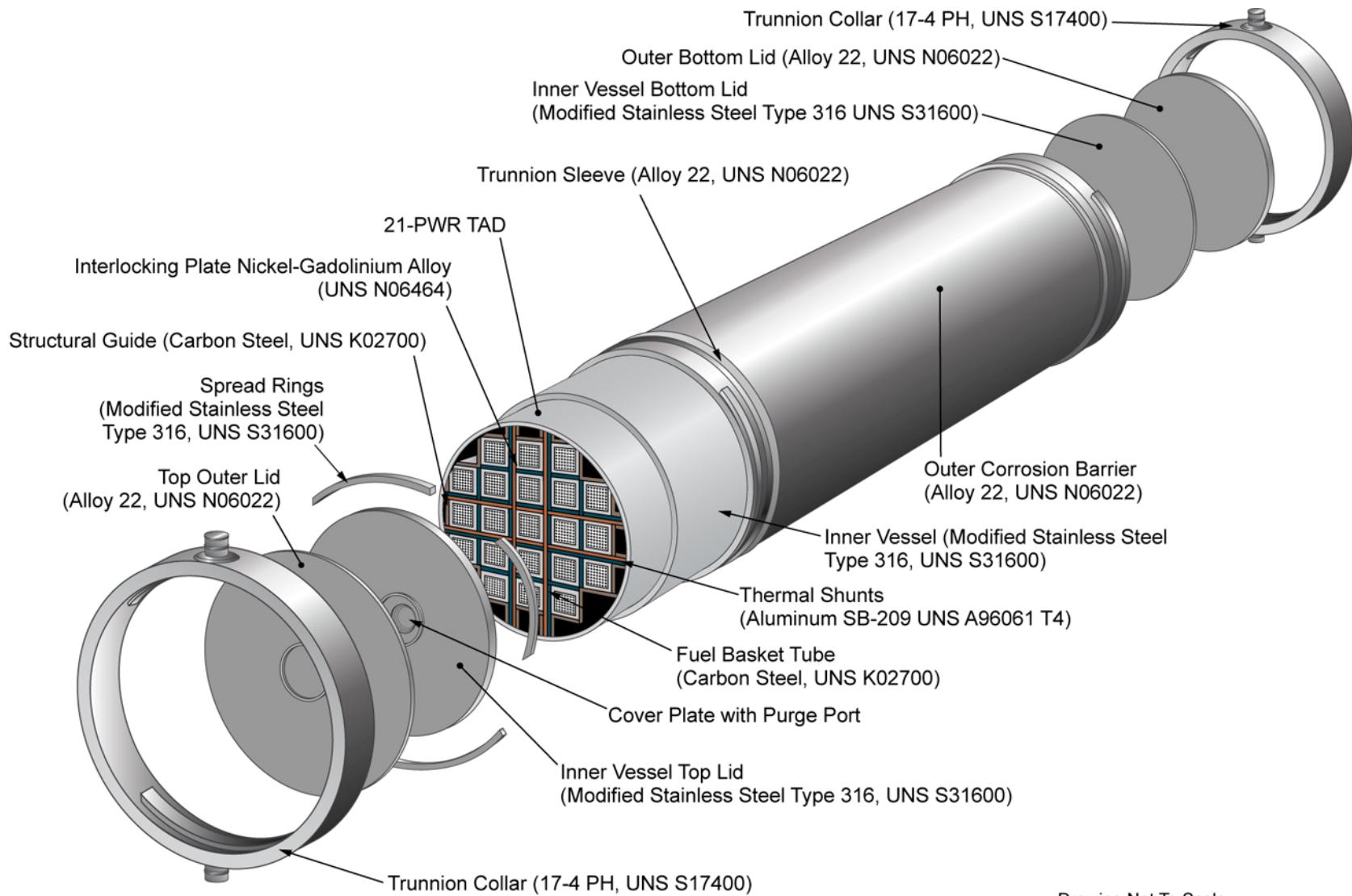
Backup Material



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Schematic of a Waste Package



Drawing Not To Scale
00688DC_020a.ai



The Natural and Engineered Barrier System

