

Advection Scheme in CAM-SE, Focus on Stabilization

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Outline

Spectral Element Method (SEM) and stabilization

CAM-SE model for atmosphere

Variable resolutions

Hyper-viscosity for stabilization

- New tensor hyper-viscosity

- CFL condition

Shallow water tests

- Refined highly distorted meshes

- Convergence and performance

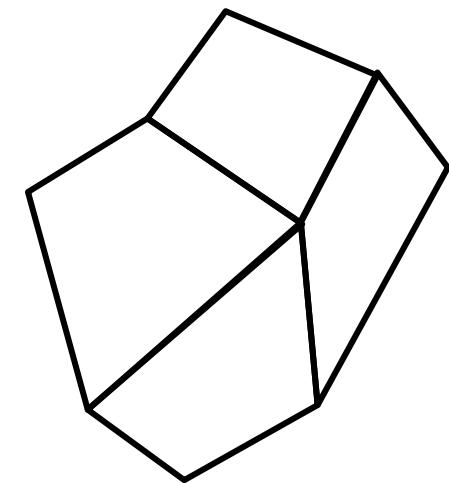
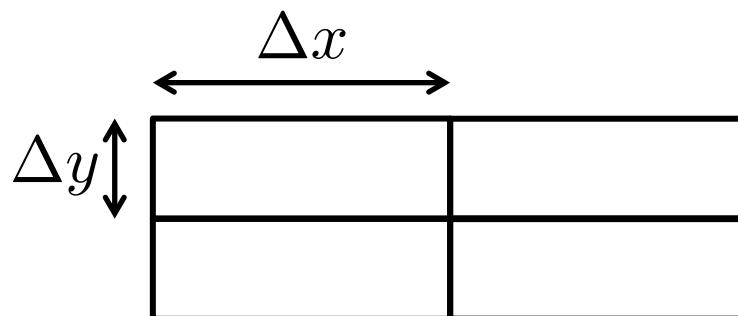
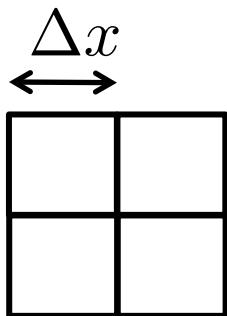
Spectral Element Method and Stabilization

SEM

- Continuous Galerkin finite element method with diagonal mass matrix and Gauss quadrature => highly scalable
- Mimetic properties
- Requires stabilization => hyperviscosity with a coefficient, $C(\Delta x)^4 \Delta^2$

Hyper-viscosity coefficient

$\Delta x?$ $\Delta y???$

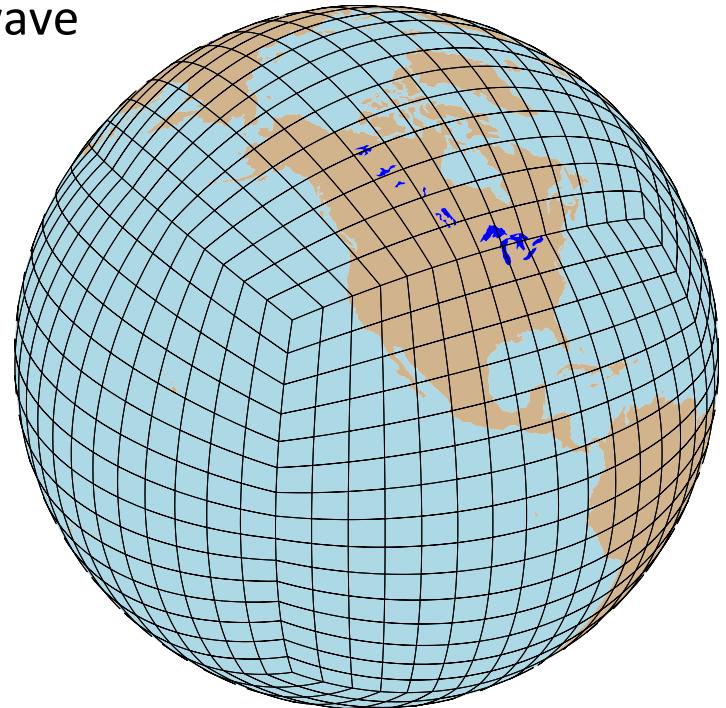
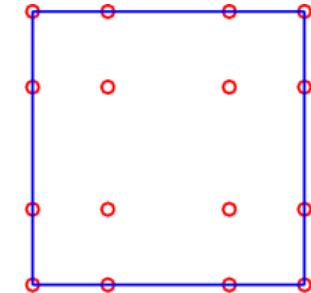


CAM-SE

Both dynamics and tracer advection use
vertical Lagrangian remap => 2D only

Scalability, mimetic properties

Stabilization needed for both damping of 2dx wave
and modeling enstrophy cascade

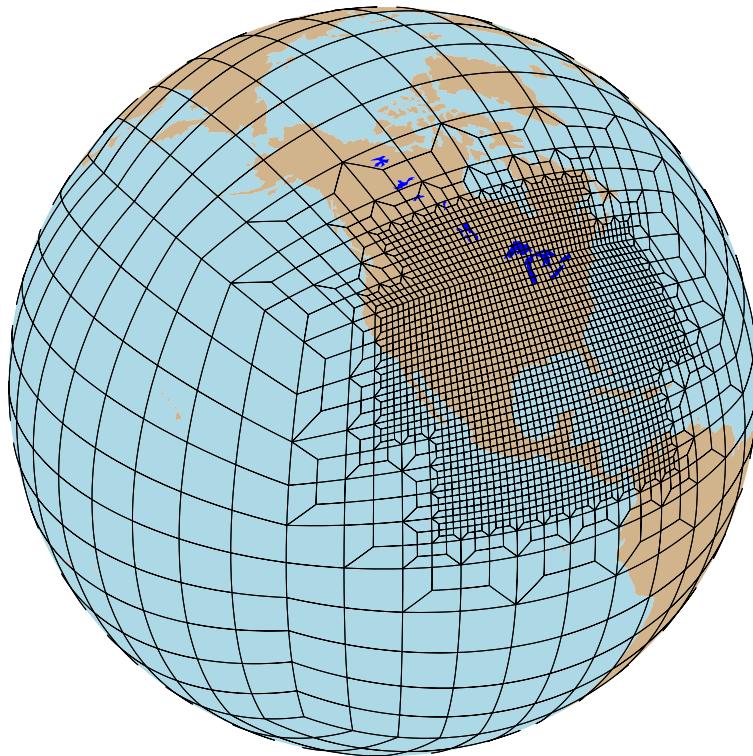


Why variable meshes for climate community

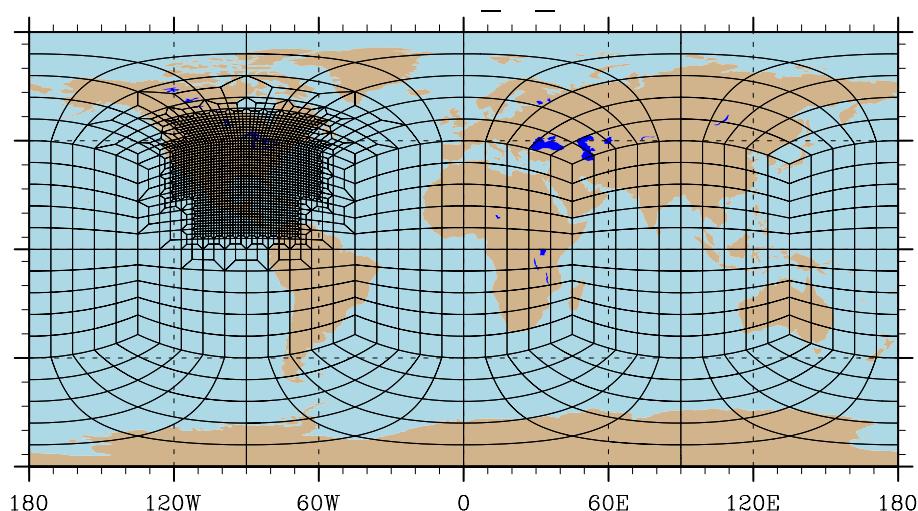
Goals: resolve fine scales with not-so-high cost to calibrate parametrizations, developing parametrizations, forecast, etc.

Example: Variable resolution runs are 10-100 times faster, hundreds of runs are needed. For the mesh below, approximately 46 times less DOFs.

Mesh refined 8 times, from 333 km to 42 km



(a) orthographic



(b) stereographic

Hyper-viscosity (HV)

Stabilization technique for tracers is $\nu \Delta^2 q$ and for vector fields $\nu \Delta^2 \vec{u}$
Coefficient ν scales like $(\Delta x)^{-p}$ with $p = 4$ or $p = 3.2$

Works well. Problem is highly-distorted elements with uneven scales.

In CAM-SE, HV is implemented by

$$\int_{sphere} \phi_i q_t = \int_{sphere} \phi_i \Delta q = - \int_{sphere} \nabla \phi_i \cdot \nabla q$$

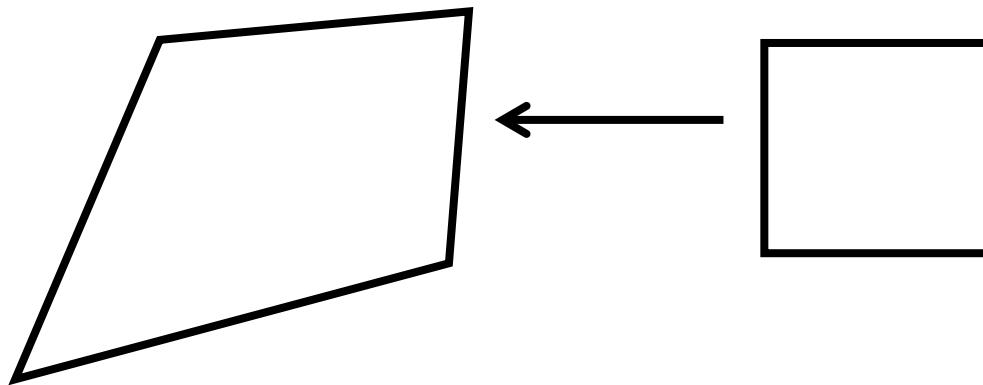
We focus on a local part:

$$\int_{element} \nabla \phi_i \cdot \nabla q$$

Elements in Physical and Reference Spaces

Transform:

$$x(\xi, \eta), y(\xi, \eta) \quad \xi, \eta \in [-1, 1] \times [-1, 1]$$



$$\begin{aligned} & \int_{element} \nabla_{xy} \phi_i \cdot \nabla_{xy} q \\ &= \int_{[-1,1] \times [-1,1]} D^{-T} \nabla_{\xi\eta} \phi_i \cdot D^{-T} \nabla_{\xi\eta} q \quad D = \begin{pmatrix} \frac{\partial x}{\partial \xi} & \frac{\partial y}{\partial \xi} \\ \frac{\partial x}{\partial \eta} & \frac{\partial y}{\partial \eta} \end{pmatrix} \\ &= \int_{[-1,1] \times [-1,1]} \nabla_{\xi\eta} \phi_i \cdot D^{-1} D^{-T} \nabla_{\xi\eta} q \end{aligned}$$

Dimensions from Metric Tensors

Focus on an inverse metric tensor

$$D^{-1}D^{-T} = (D^T D)^{-1} = E\Lambda E^T$$

$$E\Lambda E^T = E \begin{pmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{pmatrix} E^T = E \begin{pmatrix} \left(\frac{2}{\Delta x}\right)^2 & 0 \\ 0 & \left(\frac{2}{\Delta y}\right)^2 \end{pmatrix} E^T$$

$\Delta x, \Delta y$ are interpreted as dimensions of an element

Tensor hyper-viscosity:

Instead of $\nabla_{\xi\eta} \phi_i \cdot D^{-1}D^{-T} \nabla_{\xi\eta} q$ take

$$\nabla_{\xi\eta} \phi_i \cdot D^{-1} \mathbf{V} D^{-T} \nabla_{\xi\eta} q$$

$$\mathbf{V} = DE \begin{pmatrix} \left(\frac{2}{\Delta x}\right)^{2-p} & 0 \\ 0 & \left(\frac{2}{\Delta y}\right)^{2-p} \end{pmatrix} E^T D^T$$

Tensor hyper-viscosity, motivation

In case of uniform elements, $(\Delta x)^p \Delta q$ leads to

$$\nabla_{\xi\eta} \phi_i \cdot E \begin{pmatrix} \left(\frac{1}{\Delta x}\right)^{2-p} & 0 \\ 0 & \left(\frac{1}{\Delta x}\right)^{2-p} \end{pmatrix} E^T \nabla_{\xi\eta} q$$

For distorted elements,

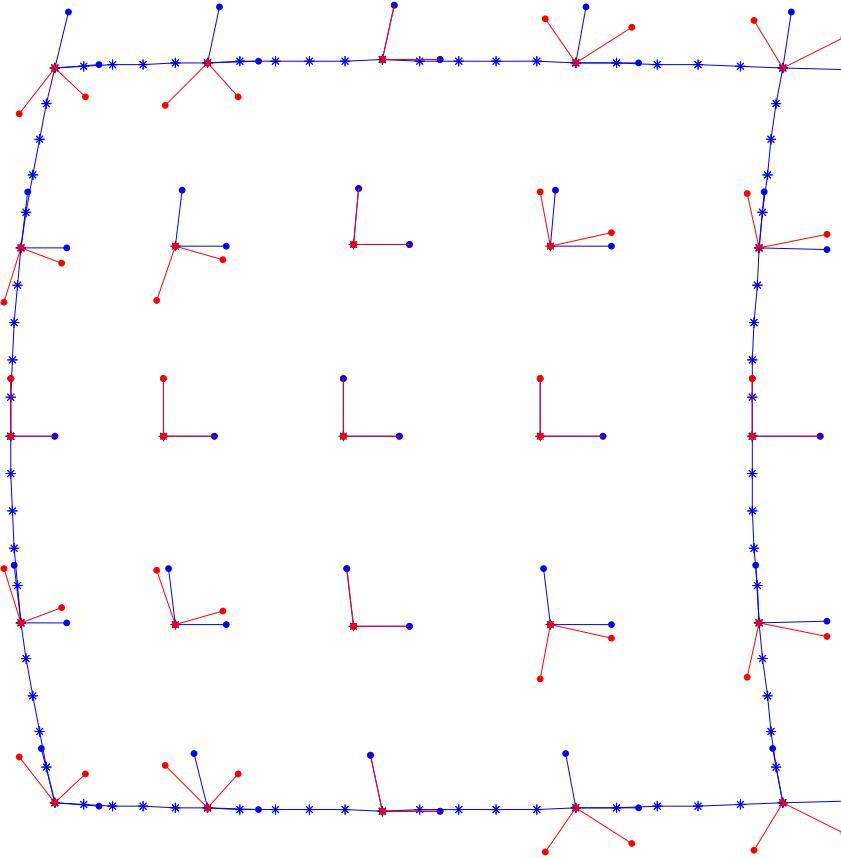
$$\nabla_{\xi\eta} \phi_i \cdot E \begin{pmatrix} \left(\frac{1}{\Delta x}\right)^{2-p} & 0 \\ 0 & \left(\frac{1}{\Delta y}\right)^{2-p} \end{pmatrix} E^T \nabla_{\xi\eta} q$$

Technicalities: we project all 4 elements of \mathbf{V} .
It is well-defined across elements' edges.

CFL, matrix E

CFL estimates follow from 1D analysis.

Columns of matrices E as vectors: ‘uniform’ quad on a sphere, blue segments represent covariant bases, red segments represent columns of matrix E.



Shallow Water Tests

Tests as in Williamson et al. (JCP, 1992)

Test Case #2: Global steady state nonlinear zonal geostrophic flow.

Convergence rates for a numerical scheme are expected to be same as in theory.

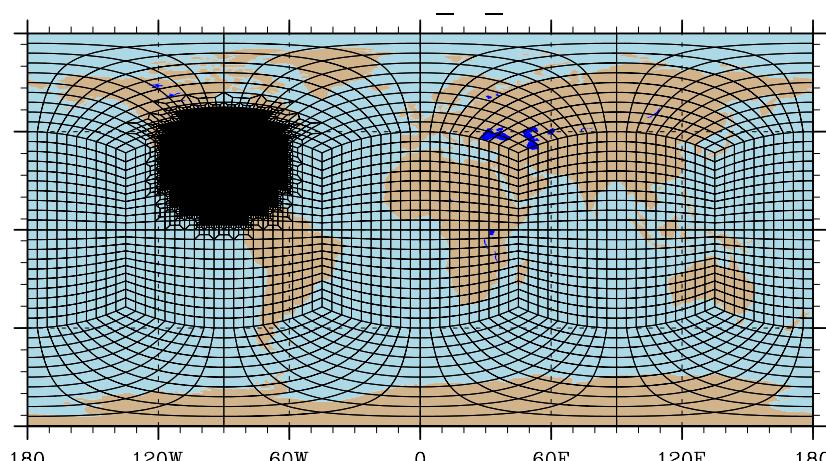
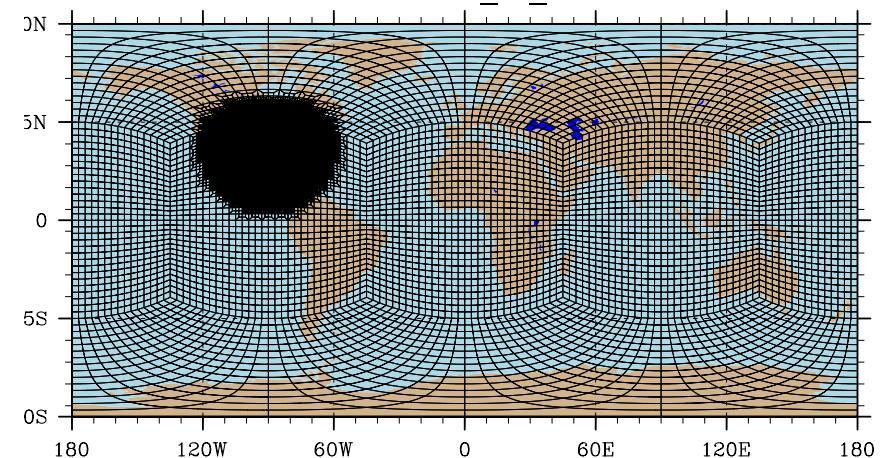
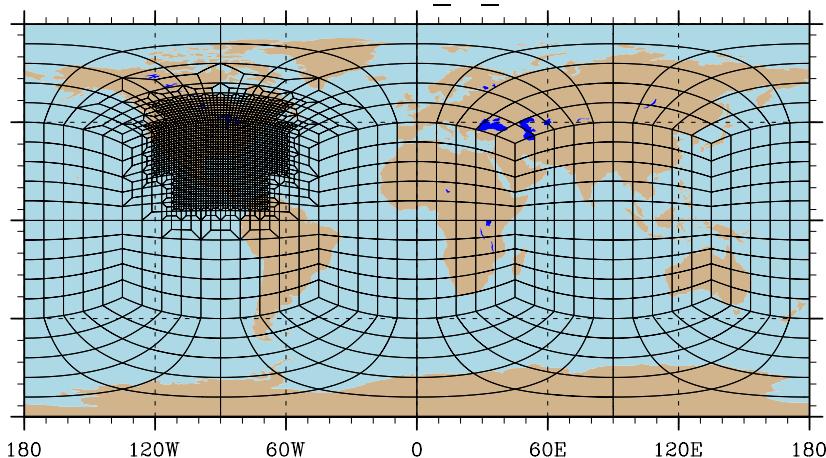
plots

Test Case #5: Zonal flow over a mountain

Analytic solution does not exist. Errors are obtained with a hi-res solution.

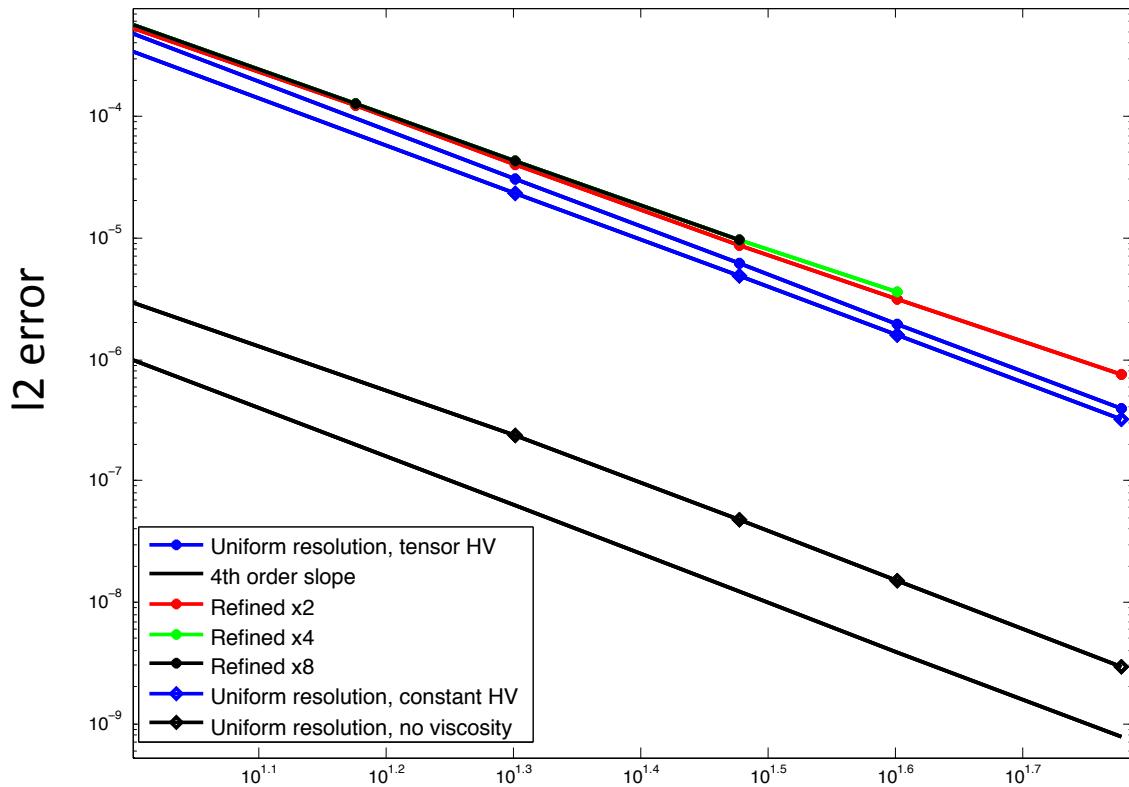
The mountain is given by C0 function. Theoretical convergence rates are not expected; vorticity field is examined for oscillations.

Meshes



**Goal is to show that refined meshes
do ‘no harm’ compared to
uniform meshes of
the same coarse resolution**

Convergence for TC2



~degrees of freedom

Tensor HV, uniform resolution:
4th order

Refinement with x2:
3.7th order

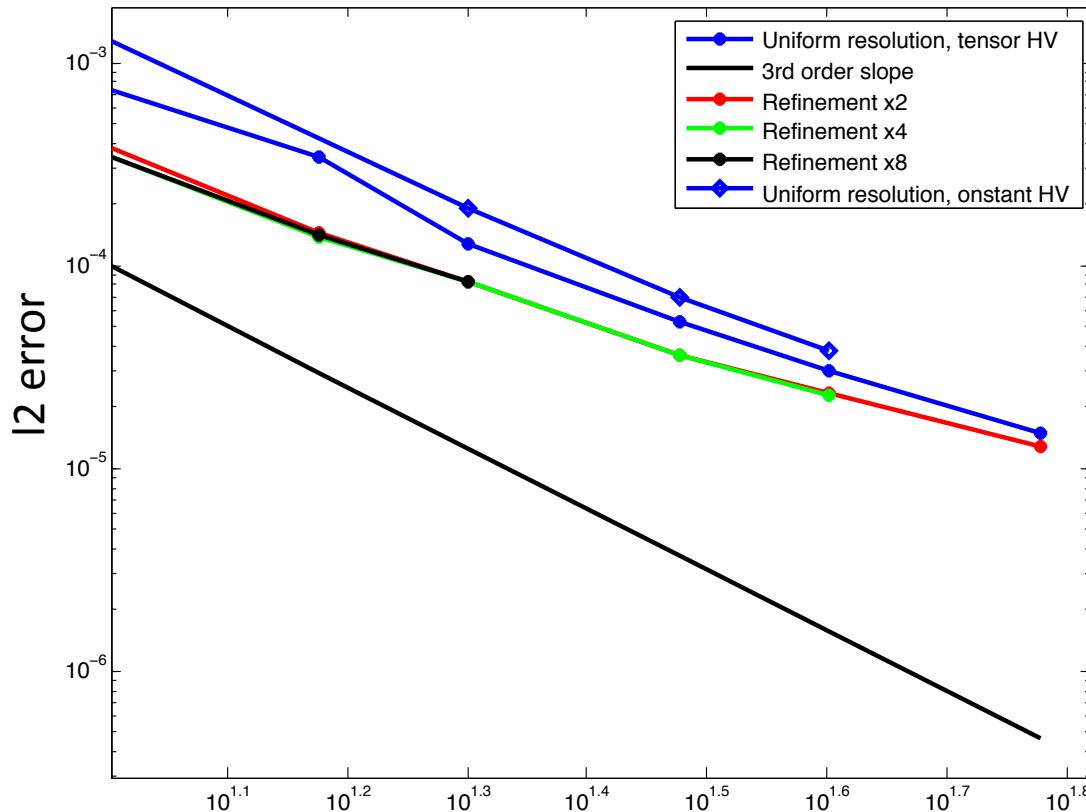
Refinement with x4:
3.7th order

Refinement with x8:
3.7th order

Constant (traditional) HV:
3.9th order

No hyperviscosity:
3.9th order

Performance of TC5

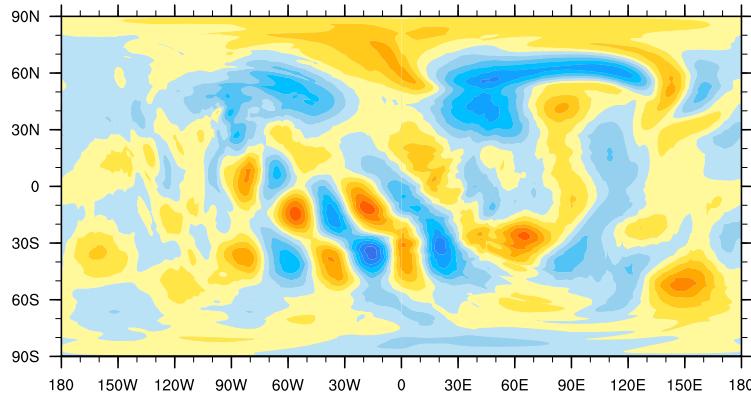


~degrees of freedom

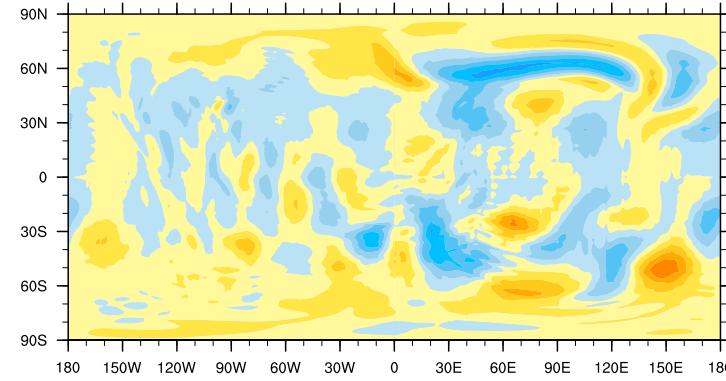
Note that refined regions are over the mountain which improves errors

Performance of TC5 (cont.)

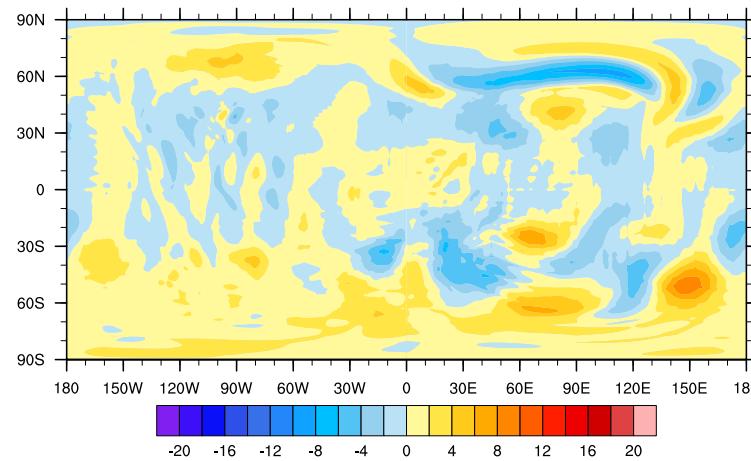
Uniform Mesh



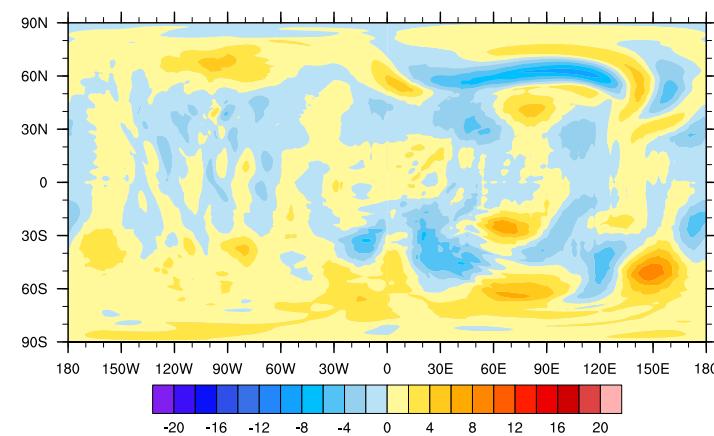
$k=2$ 2x local refinement



$k=4$ 4x local refinement

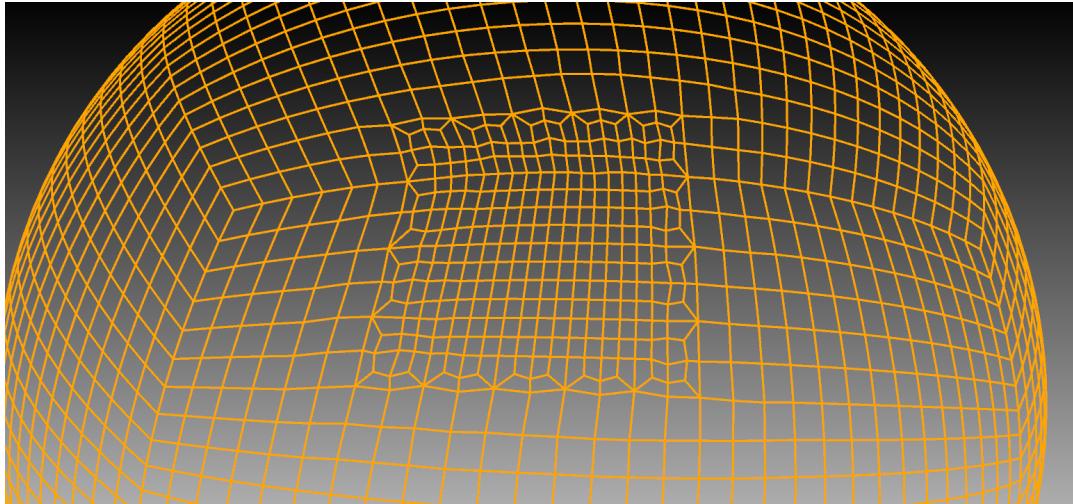


$K=8$ 8x local refinement



- Refinement over mountain has almost zero impact on error
- Local refinement simulations have slightly smaller error – probably due to differences in hyperviscosity operator not mesh refinement (tensor vs. const. coeff)

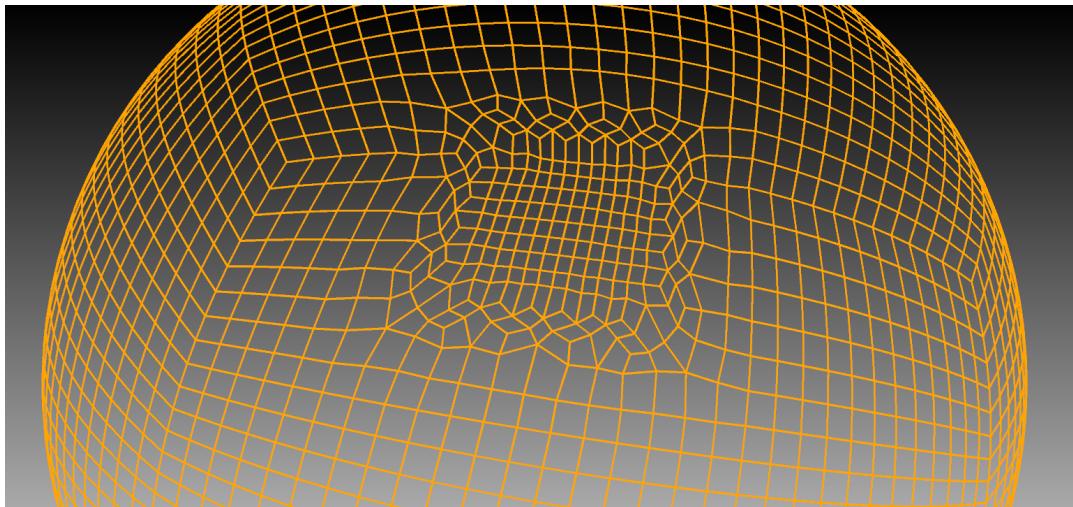
Things To Do



CUBIT refined mesh

Tensor \mathbf{V} smoothness
Is important

Quality of meshes
(less nodal valence,
smoothness) will improve
results further



Refinement 'by hand'