

Dispersion of Polymer-Grafted Nanorods in Polymer Films

Amalie L. Frischknecht

Sandia National Laboratories

Michael J. A. Hore and Russell J. Composto

University of Pennsylvania

APS March Meeting
March 19, 2013



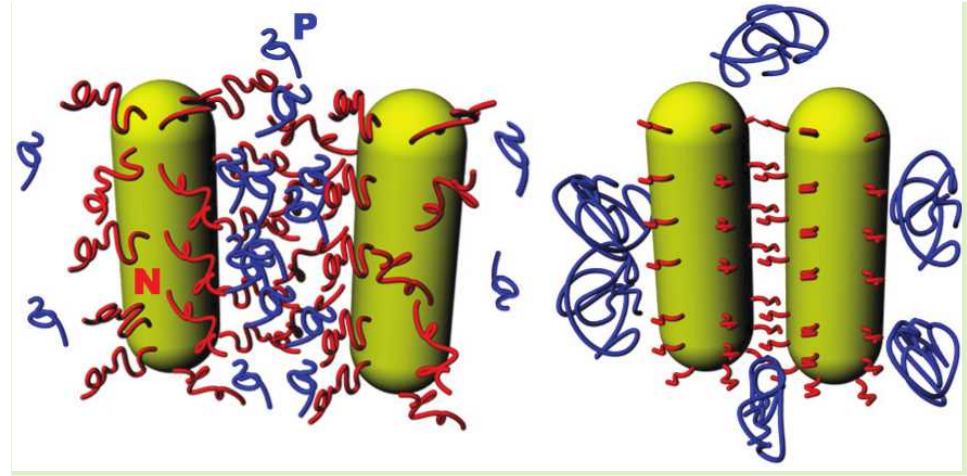
*Exceptional
service
in the
national
interest*



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Experimental System

- gold nanorods
- polymer brush coating
- 5% rods in polymer thin film
 - rods confined in the plane of the film



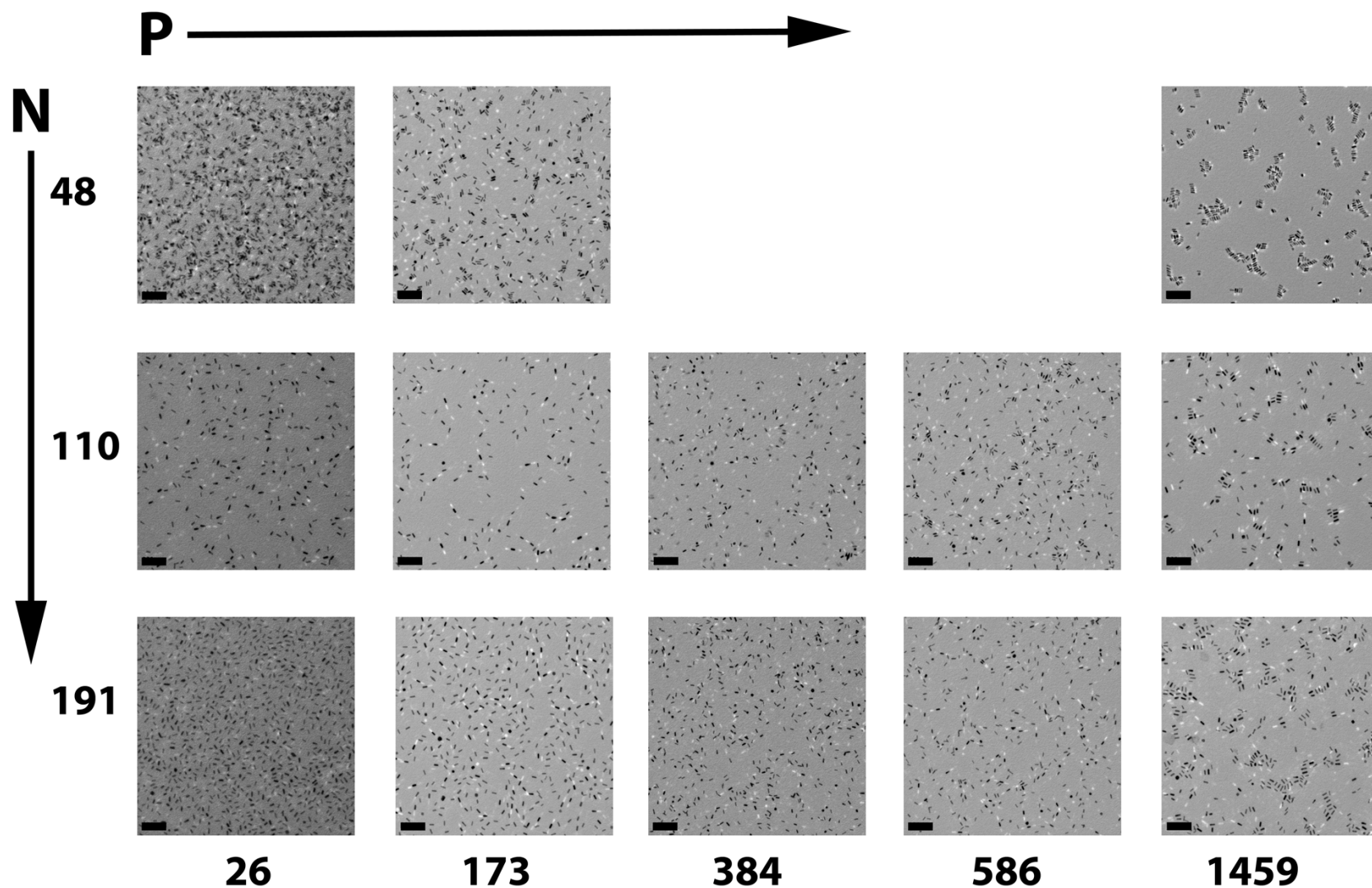
athermal systems:

PS brush in PS

PEO brush in PEO

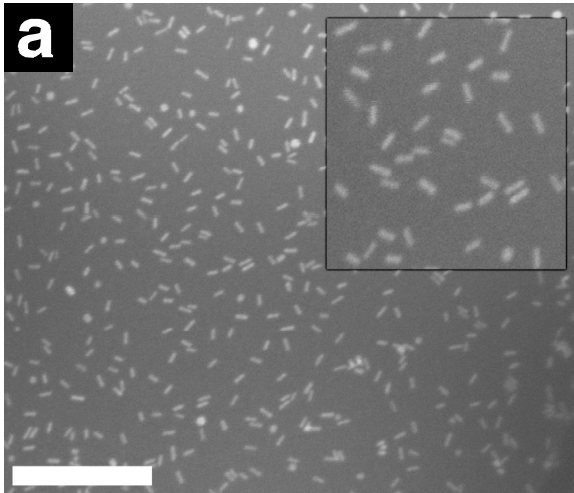
What controls nanorod dispersion/aggregation?

Nanorods: PS-Au(N):PS(P)

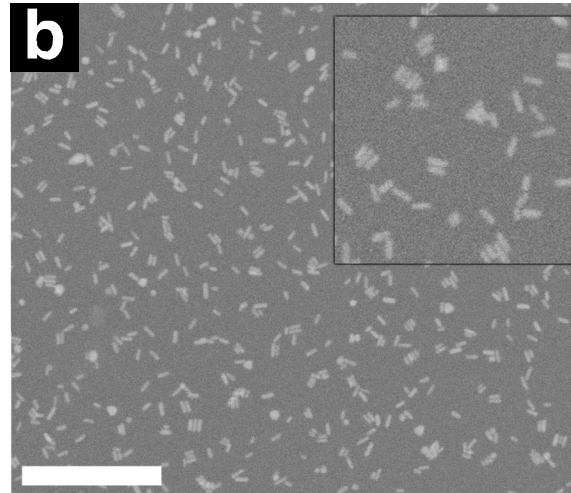


Hore, M. J. A., Frischknecht, A. L., & Composto, R. J. (2012), *ACS Macro Letters*, 1, 115–121.

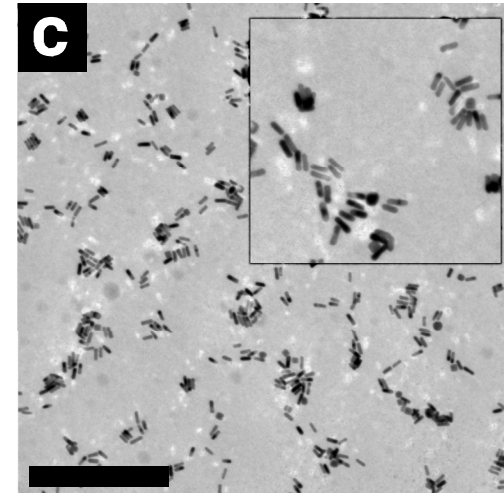
PEO-Au(*N*):PEO(*P*)



$P/N = 0.43$

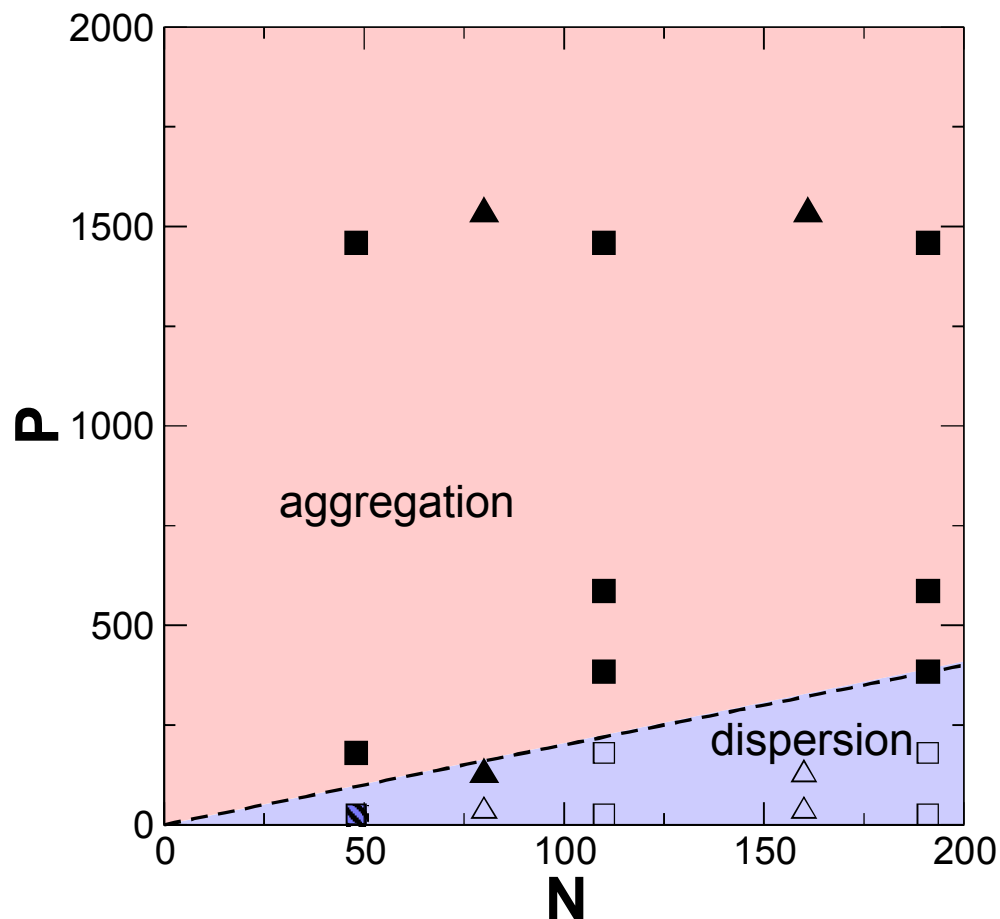


$P/N = 1.58$



$P/N = 19.2$

Dispersion “Map” for NRs



dispersion for $P < 2N$

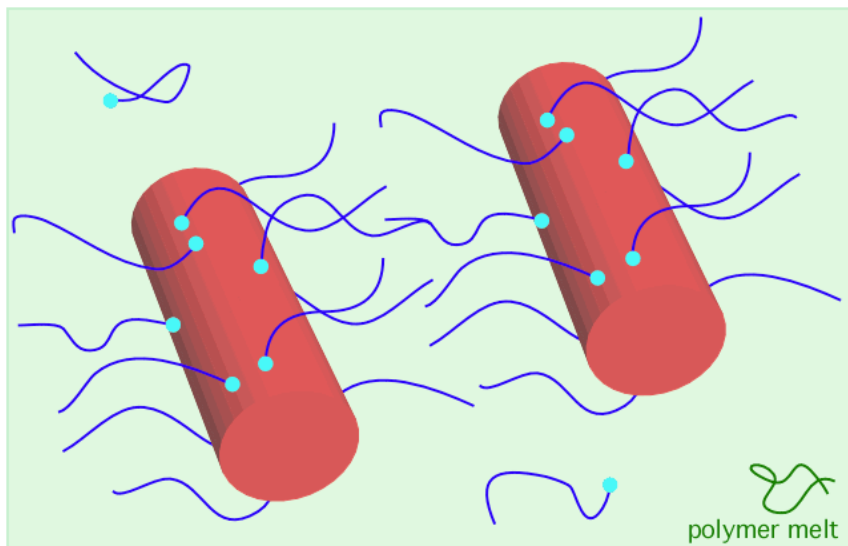
ignores possible effects of:

- rod curvature
- grafting density
- rod length

squares: PS

triangles: PEO

Modeling



classical DFT and SCFT

- brush chains length N
- matrix chains length P
- athermal ($\chi = 0$)
- nanorods with radius R_{rod}
- grafting density σ

goal: calculate polymer-mediated interaction free energy

variables: $\alpha = P/N$

$$R_{rod}/R_g$$

$$\sigma^* \equiv \frac{\sqrt{6}\sigma N^{1/2}}{a\rho_0}$$

experimental ranges:

$$\alpha = P/N = 0.15 - 30$$

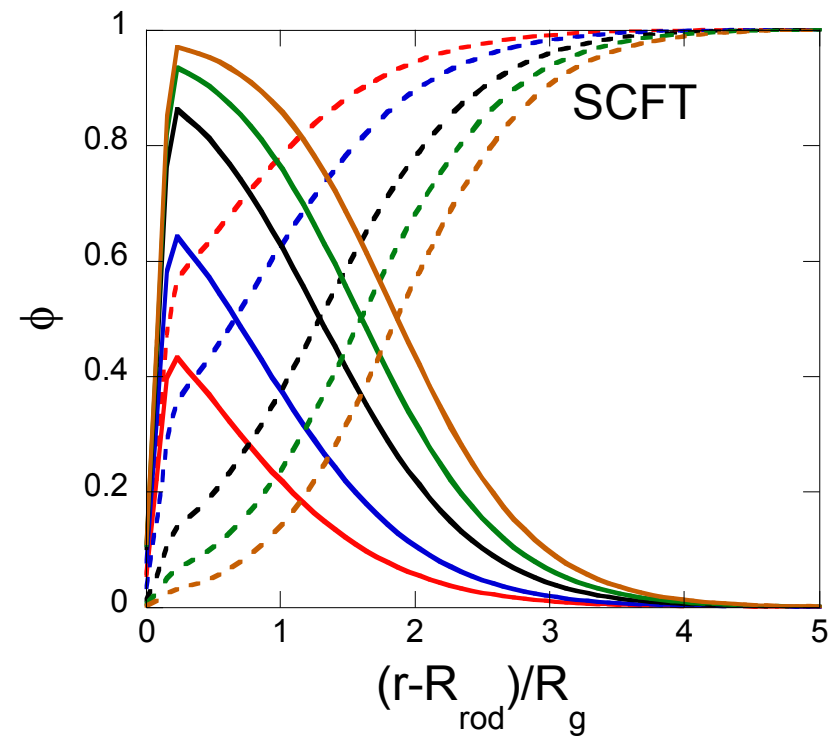
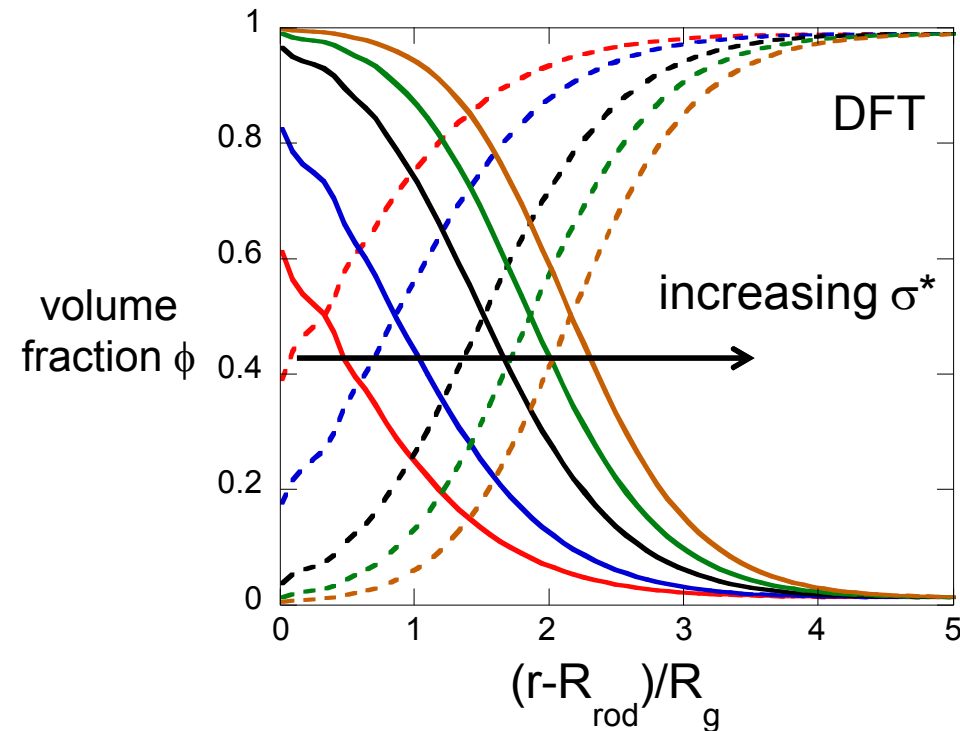
$$R_{rod}/R_g = 1.5-3.2$$

$$\sigma^* = 0.95-2.38$$

earlier work: Frischknecht, J. Chem. Phys., **128**, 224902 (2008)

Single Nanorod: Brush Profiles

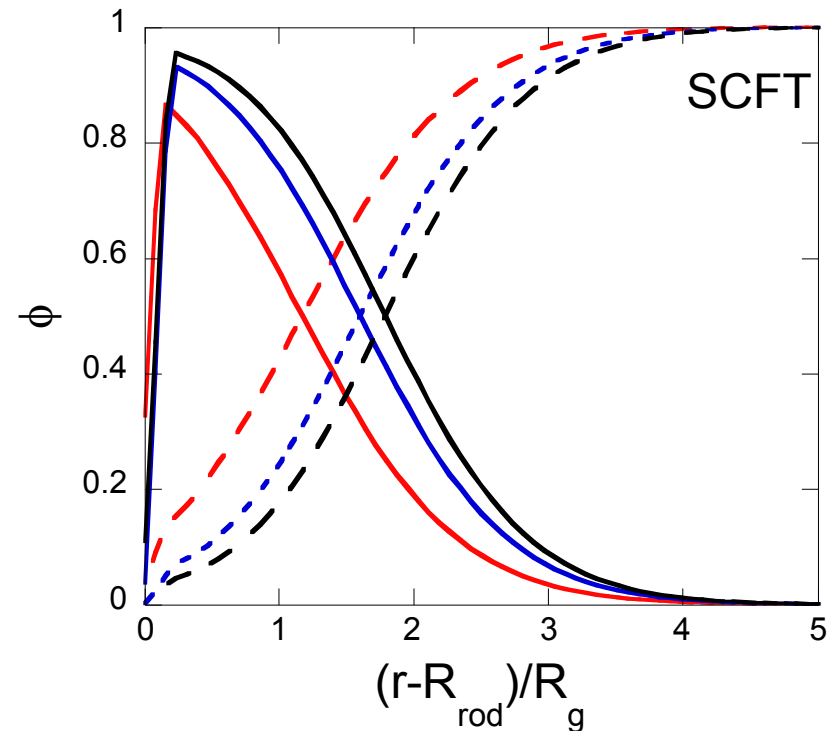
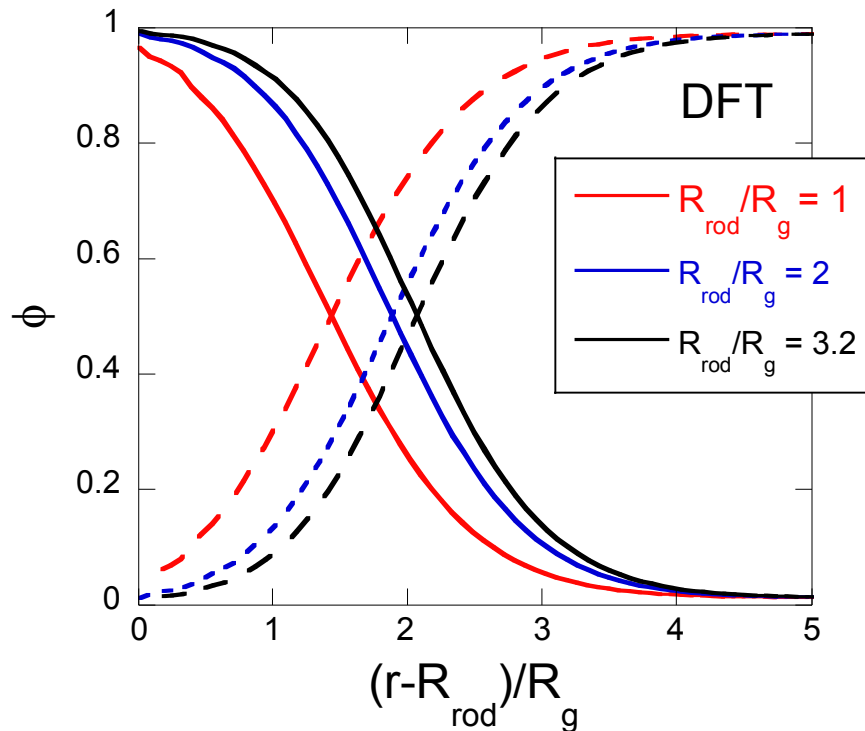
$$R_{\text{rod}}/R_g = 3.2, P/N = \alpha = 3$$



grafting density important

Single Nanorod: Brush Profiles

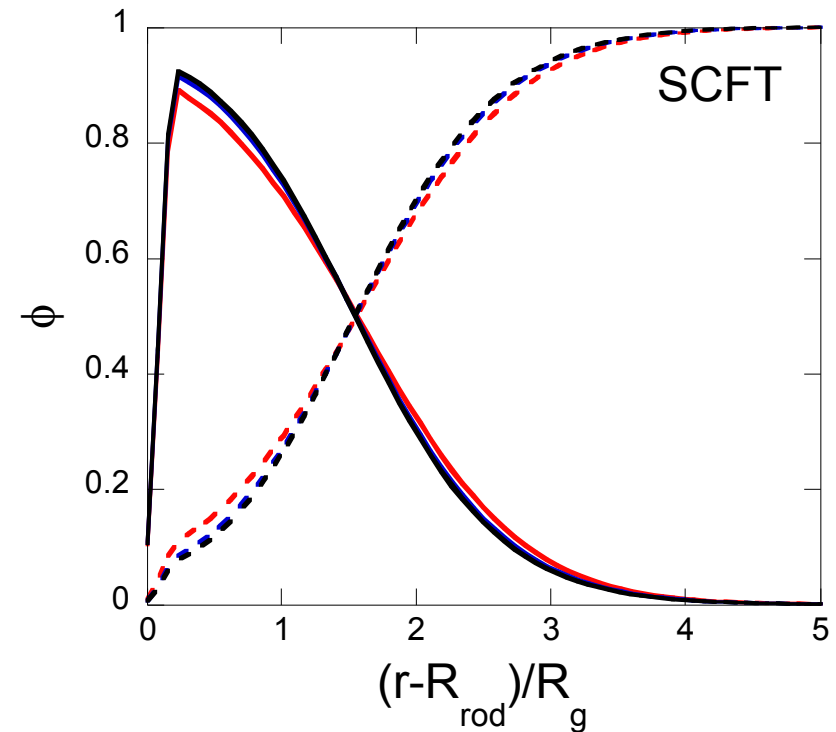
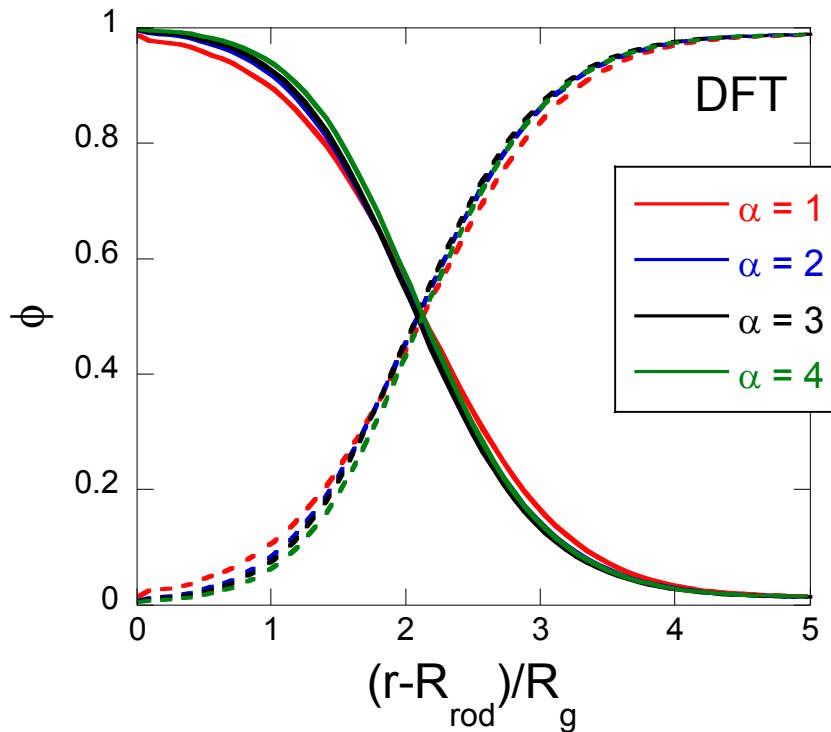
$$\alpha = 2, \sigma^* = 2.38$$



nanorod curvature important

Single Nanorod: Brush Profiles

$$R_{\text{rod}}/R_g = 3.2, \sigma^* = 2.38$$

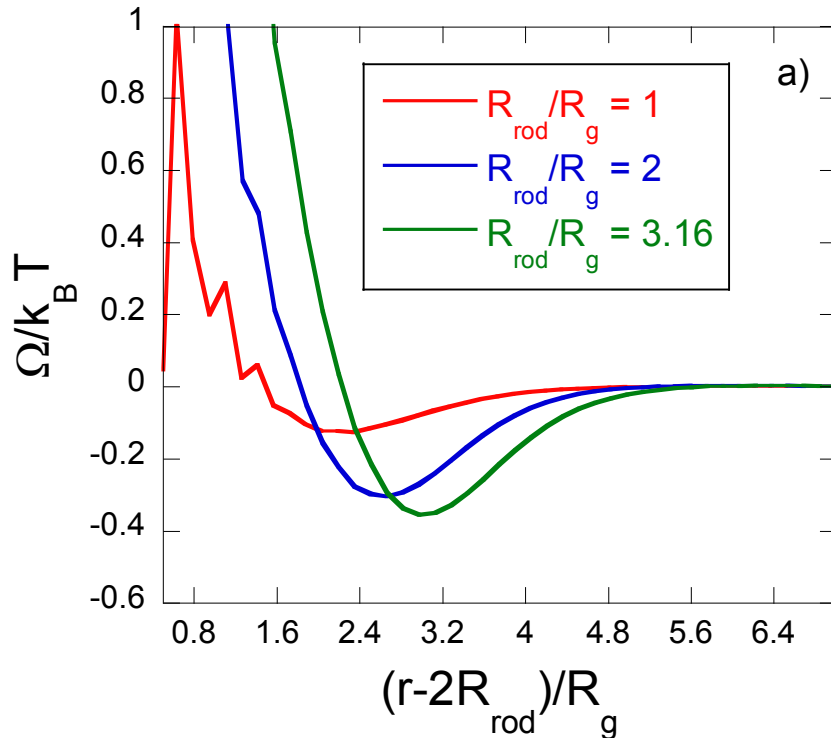


matrix chain length doesn't affect brush profiles much

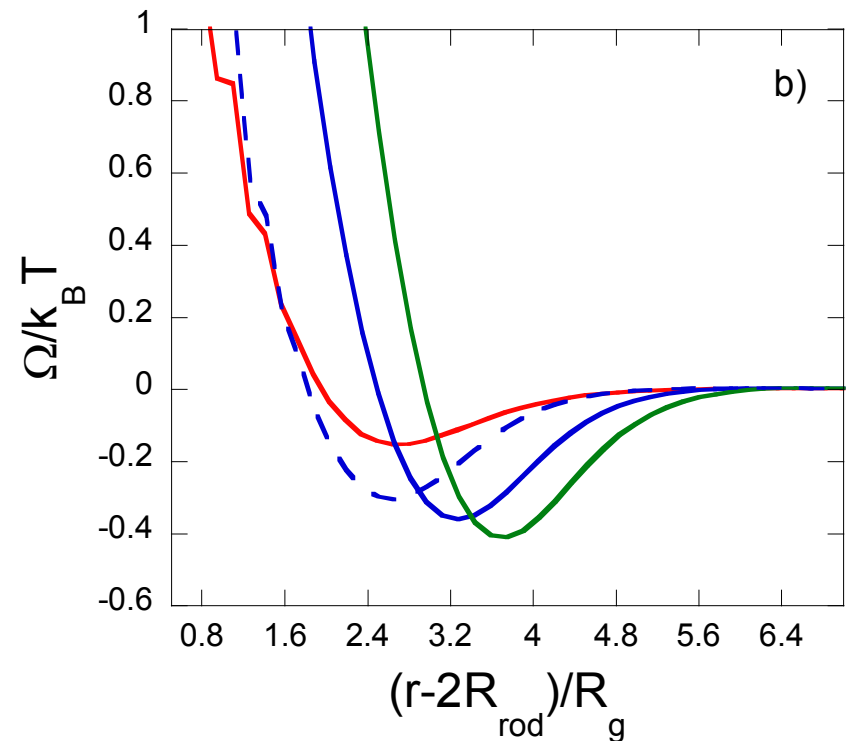
Rod-rod interaction energy

$$P/N = \alpha = 3$$

$$\sigma^* = 1.9$$



$$\sigma^* = 2.4$$

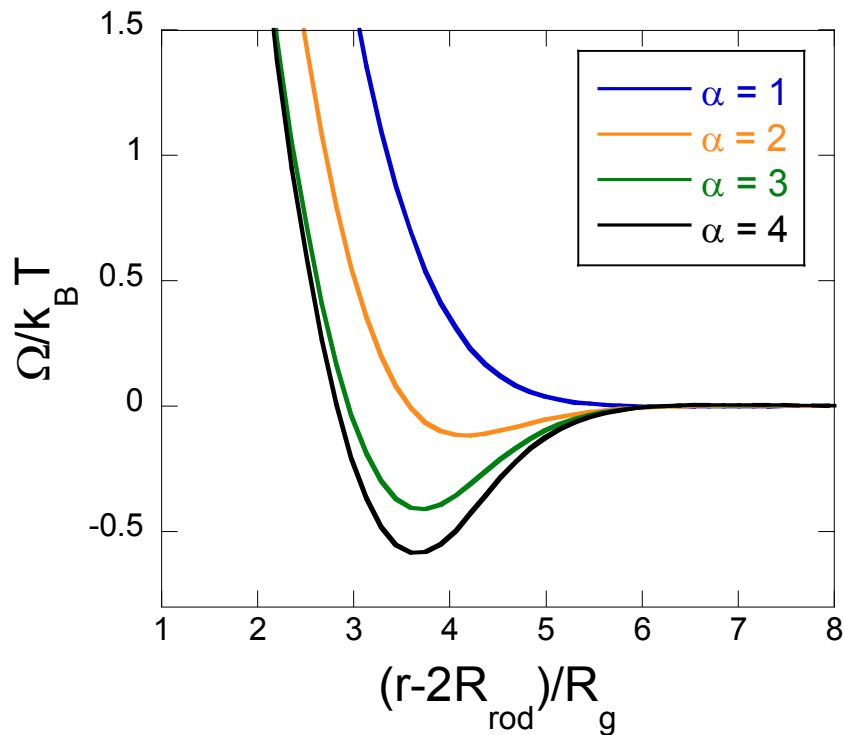


deeper attractive well as:
grafting density increases
 R_{rod} increases

Rod-rod interaction energy

$$R_{\text{rod}}/R_g = 3.2, \sigma^* = 2.4$$

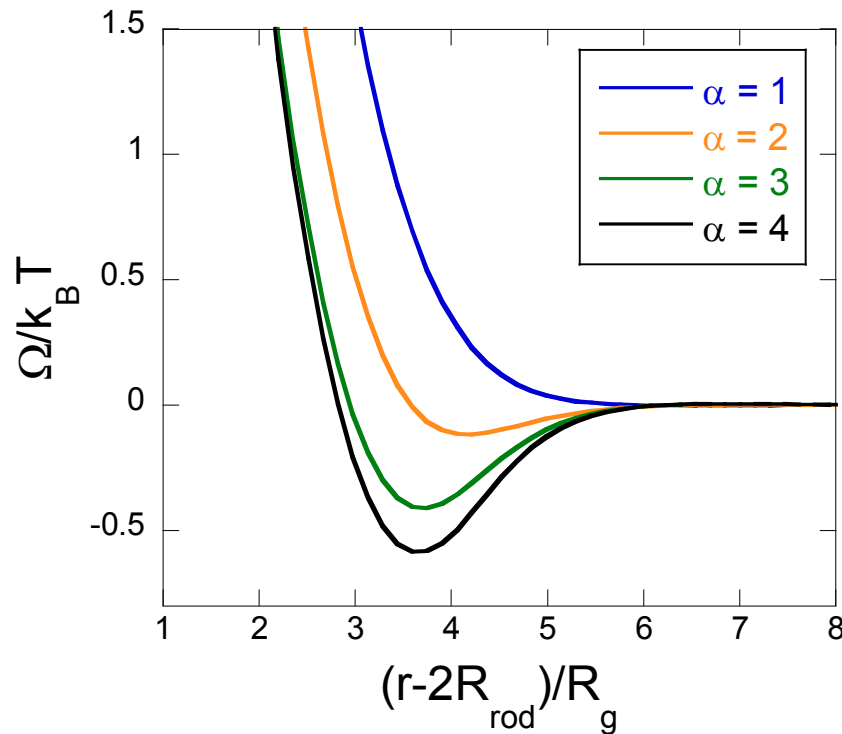
matrix chain length crucial!



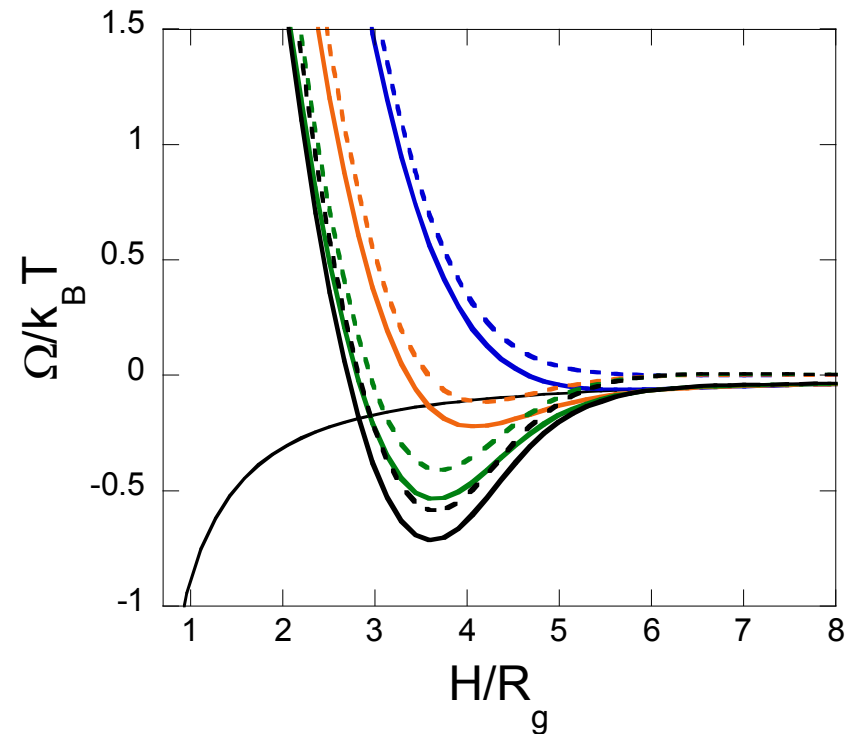
Rod-rod interaction energy

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matrix chain length crucial!

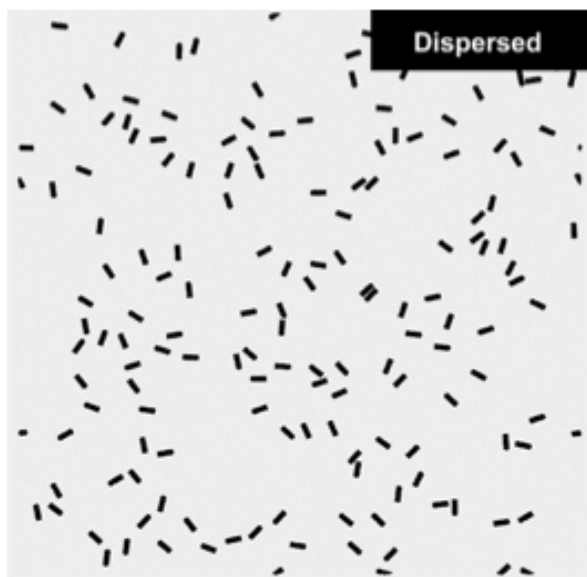


include van der Waals between Au rods: $W = -\frac{ALR_{\text{rod}}^{1/2}}{24H^{3/2}}$

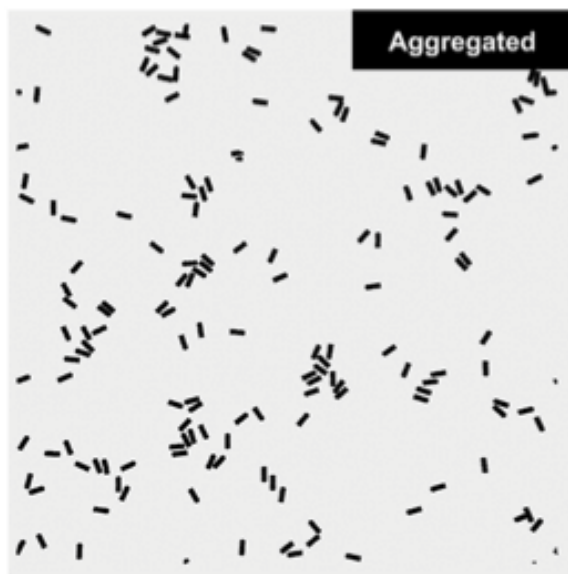


Criterion for Aggregation?

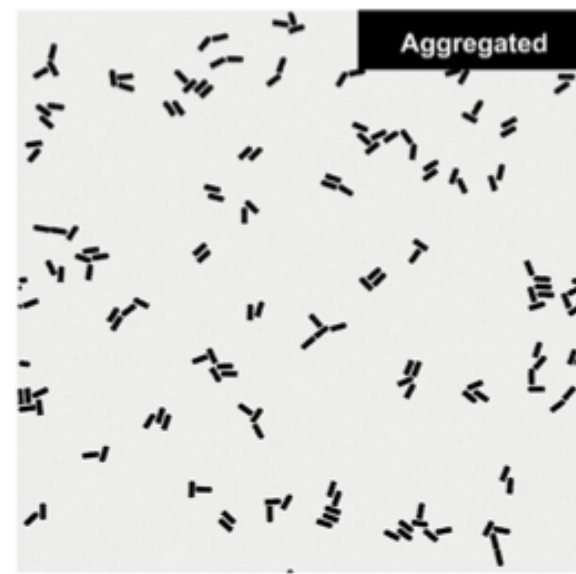
Monte Carlo simulations
square-well potential



0 kT



5 kT

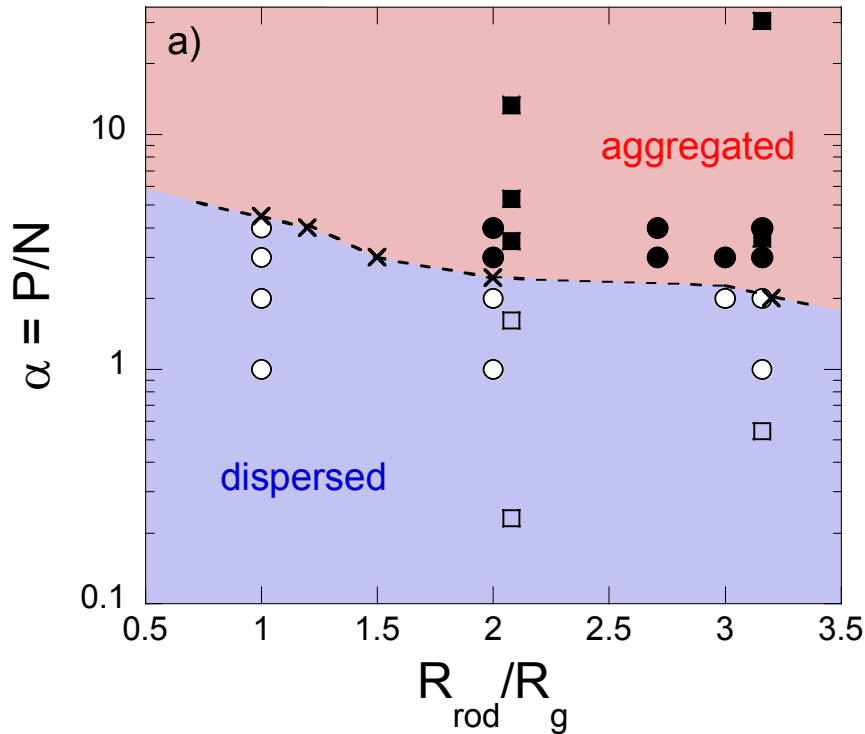


10 kT

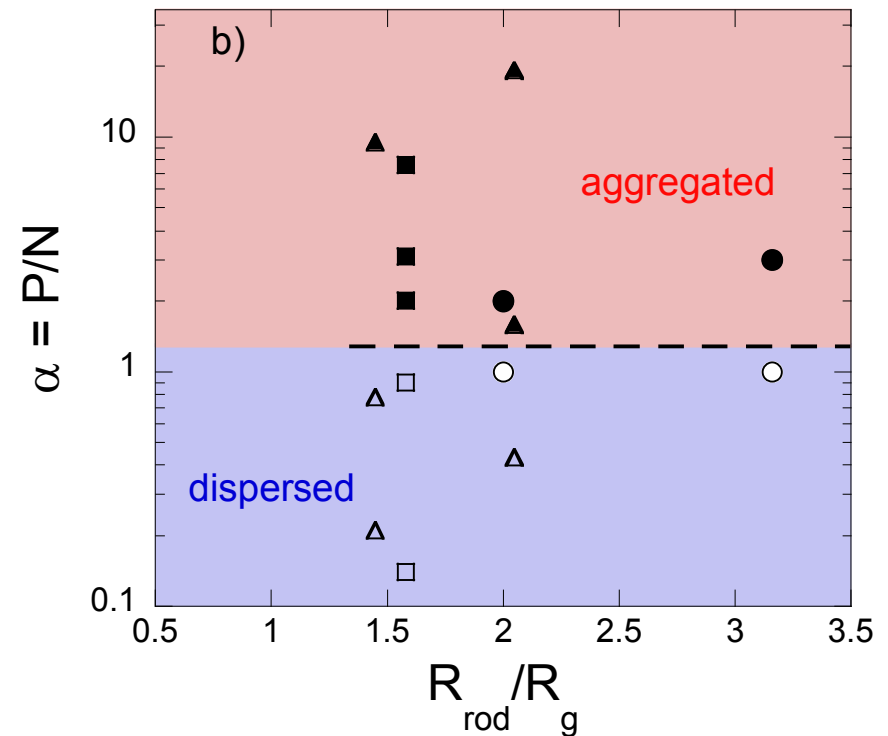
assume aggregation for $E_{\text{tot}} > 5 \text{ kT}$

Comparison with experiment

$$1.9 < \sigma^* < 2.4$$



$$1 < \sigma^* < 1.4$$

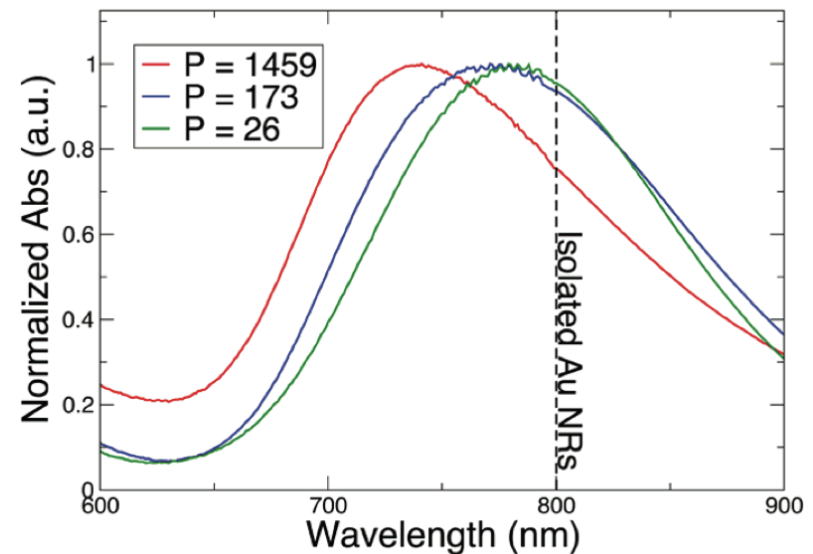
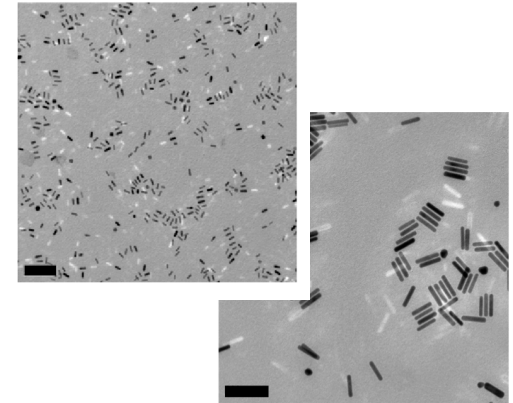


circles = DFT
squares = PS/PS
triangles = PEO/PEO

good overall agreement

Conclusions

- brush profiles remarkably insensitive to α
- interaction energy sensitive to σ^* , R_{rod} , and α
- DFT captures correct trends
 - transition to aggregation near $P/N = 2$
- design: promote dispersion for
 - small σ^* , R_{rod} , or α
 - can potentially control rod spacing in aggregates
 - to control optical properties

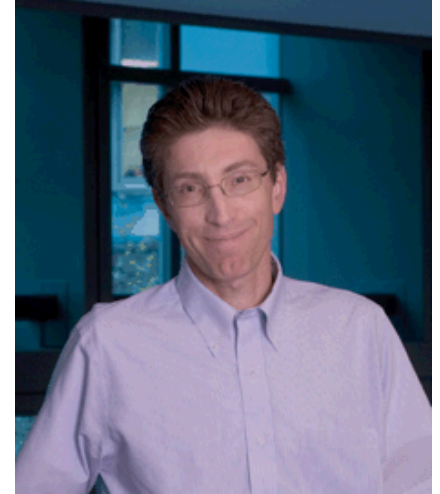


Acknowledgments



Michael J. A. Hore
Russell J. Composto

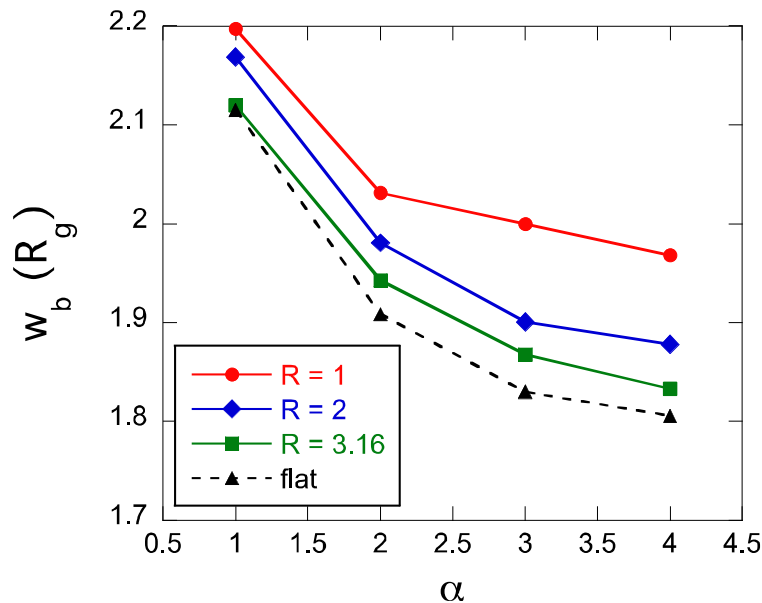
University of Pennsylvania



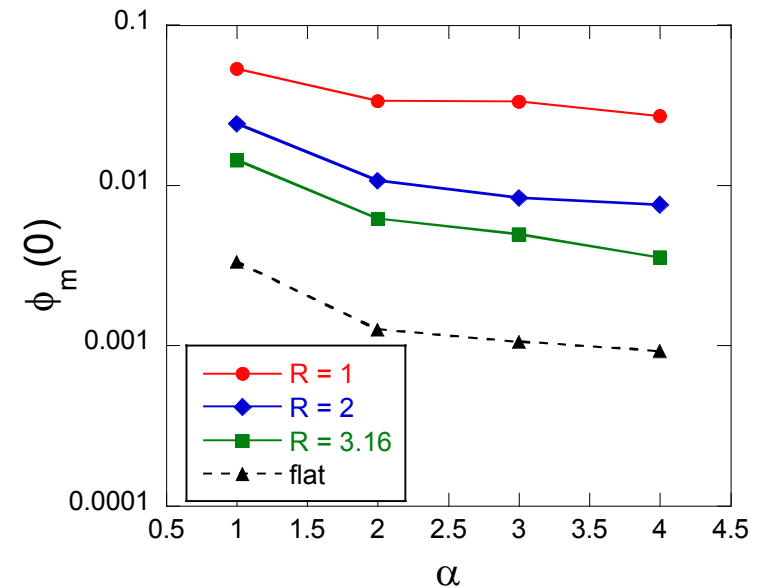
CINT User Program

Brush Characteristics vs α

brush width



volume fraction of matrix chains
at NR surface



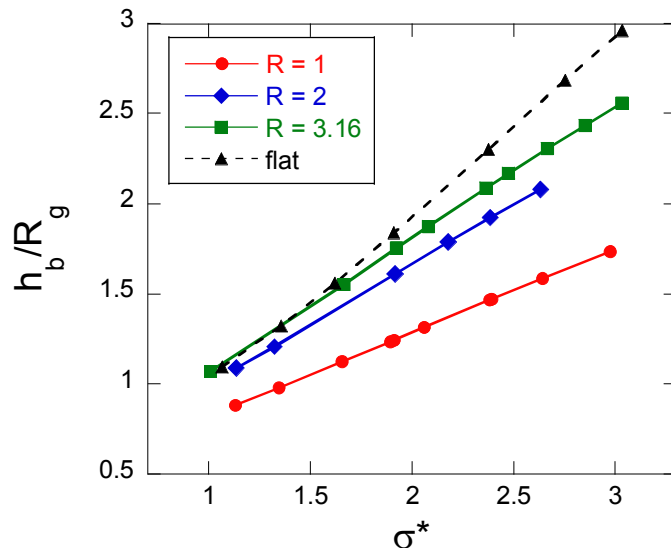
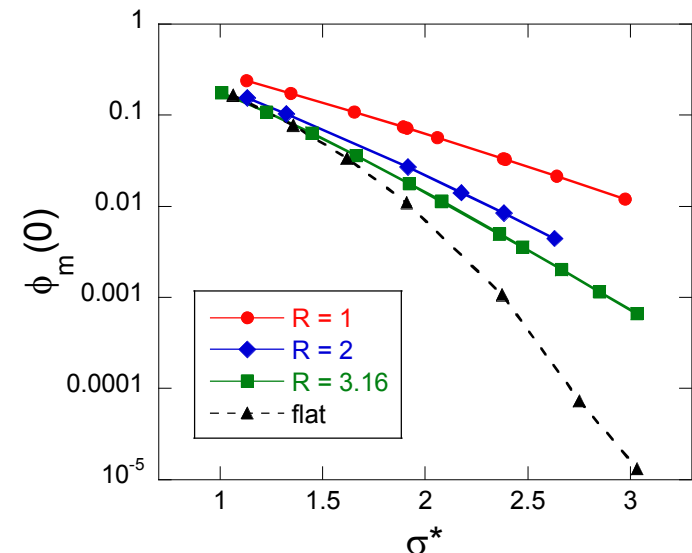
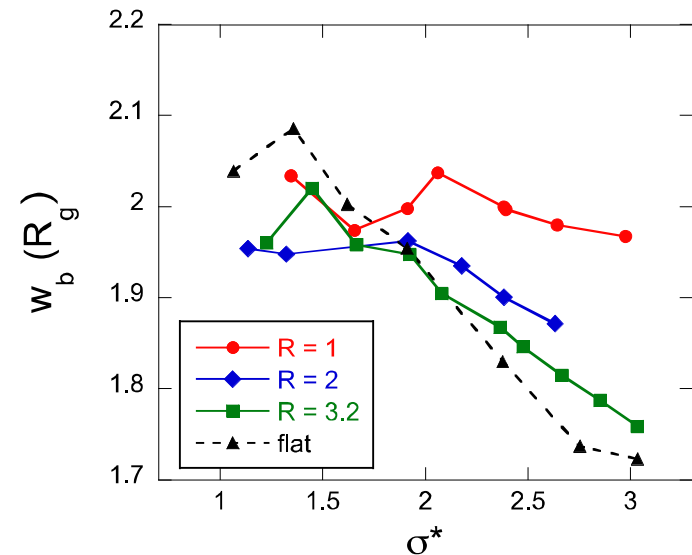
- brush height insensitive to α
- details of interface matter for interactions

Brush Characteristics vs σ^*

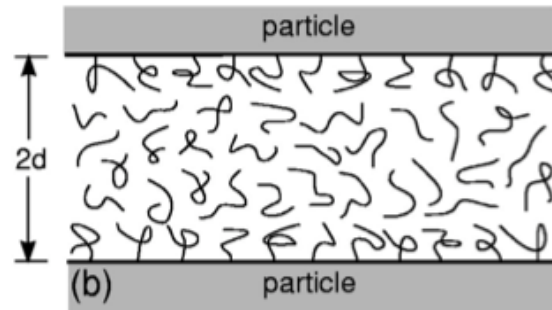
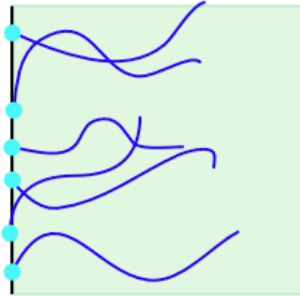
height h_b
(nearly linear) $\phi_b(h_b) = \frac{1}{2}\phi_b(0)$

width w_b $w_b = \frac{\phi_b(0)}{|\phi'_b(h)|}$

matrix fraction
at rod surface $\phi_m(0)$

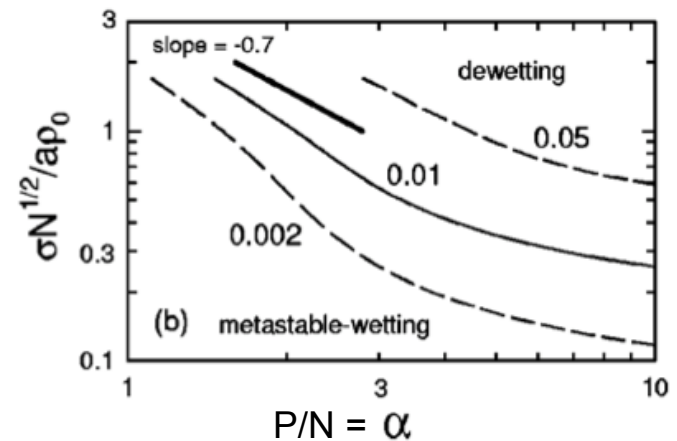
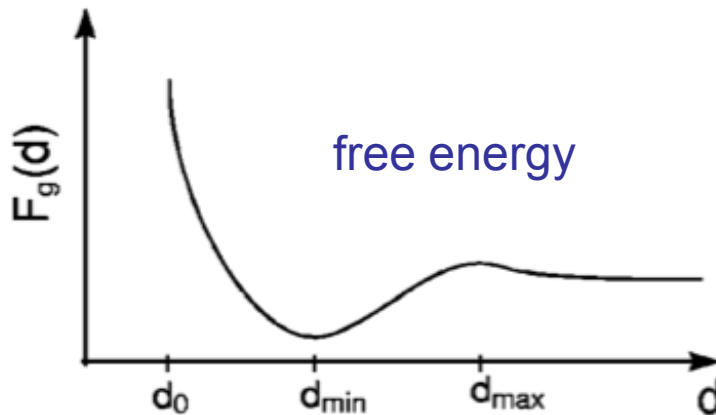


Brush-Brush Interactions

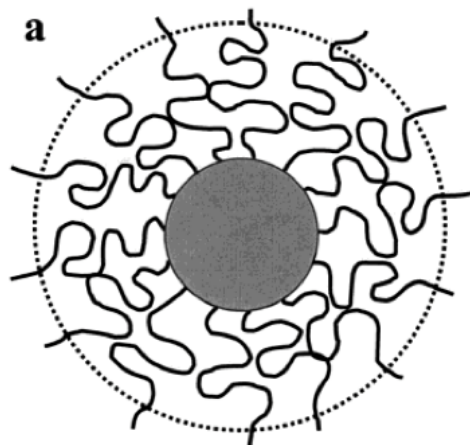


autophobic dewetting:

- entropy cost for matrix chains to enter brush
- leads to positive brush-matrix surface tension
- brushes are attracted



Brushes on Curved Surfaces

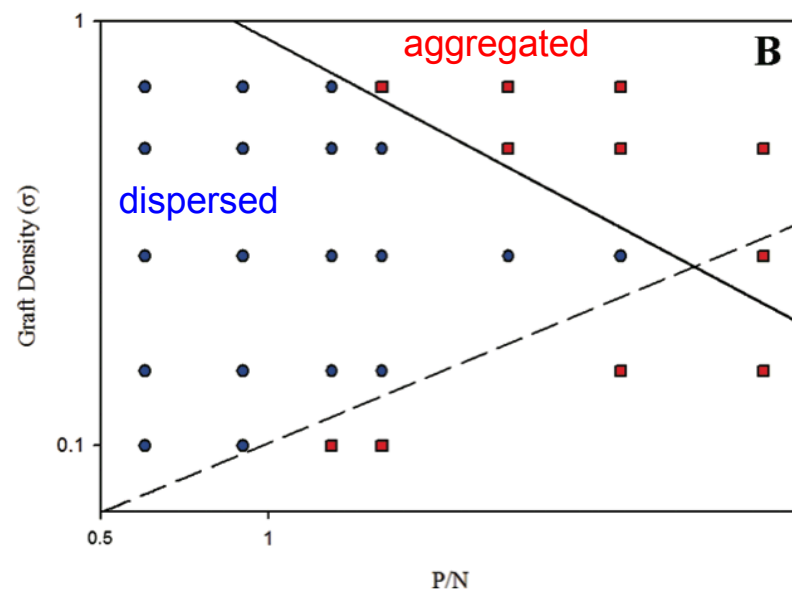
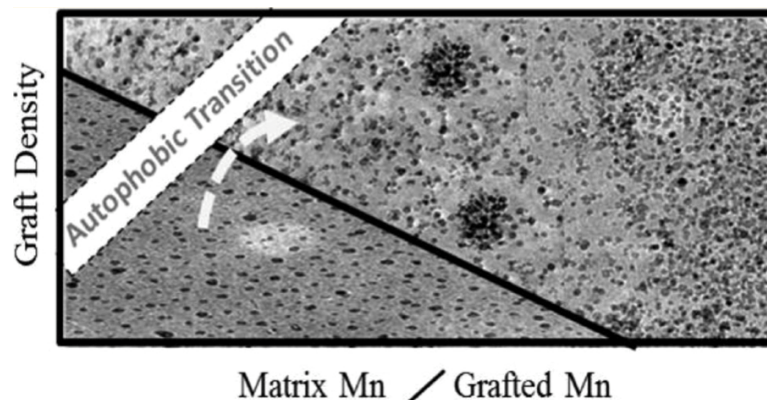


- more volume than on flat surface at same grafting density
- chains splay out more
- brush is less extended

expect wet to dry transition to occur for

- larger grafting densities
- larger P/N

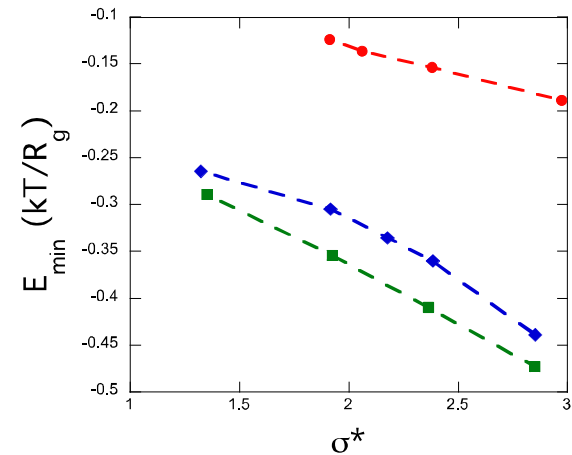
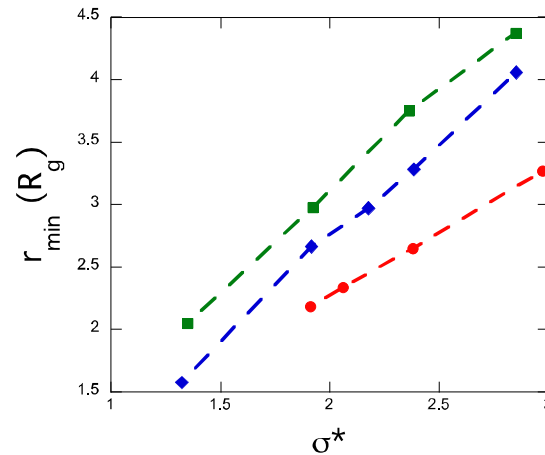
PS-silica in PS



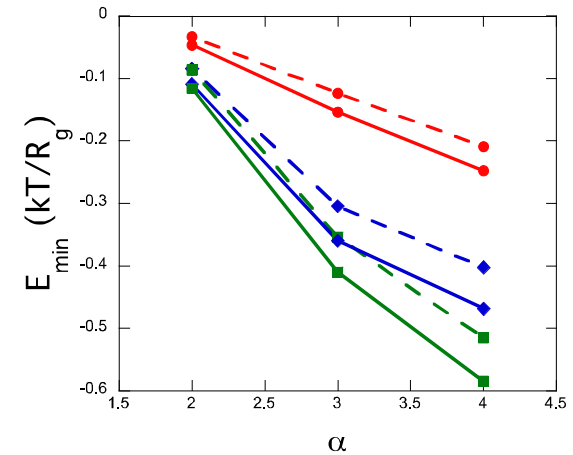
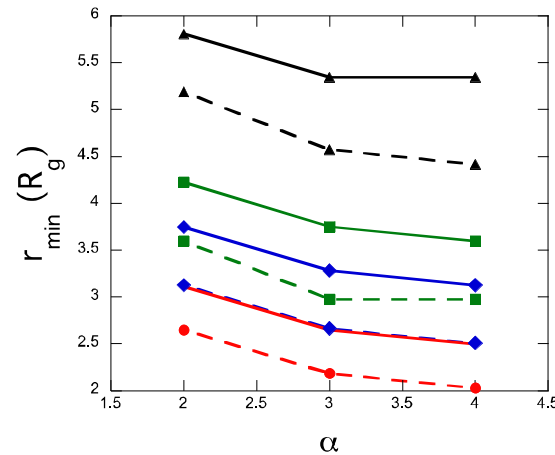
Sunday, D., Ilavsky, J., & Green, D. L. (2012).
Macromolecules, 45, 4007–4011.

Interactions vs σ^* and α

grafting density

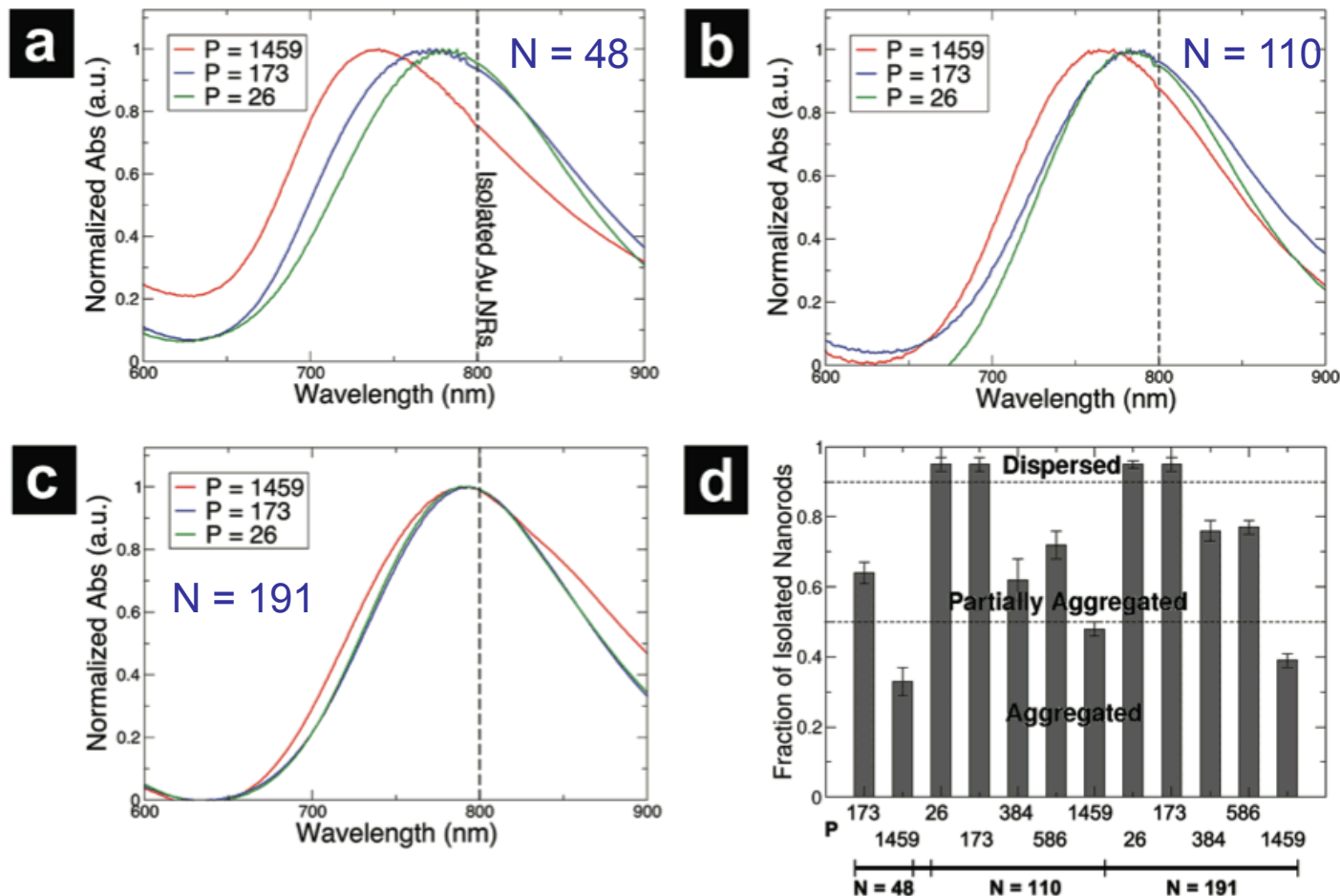


chain ratio



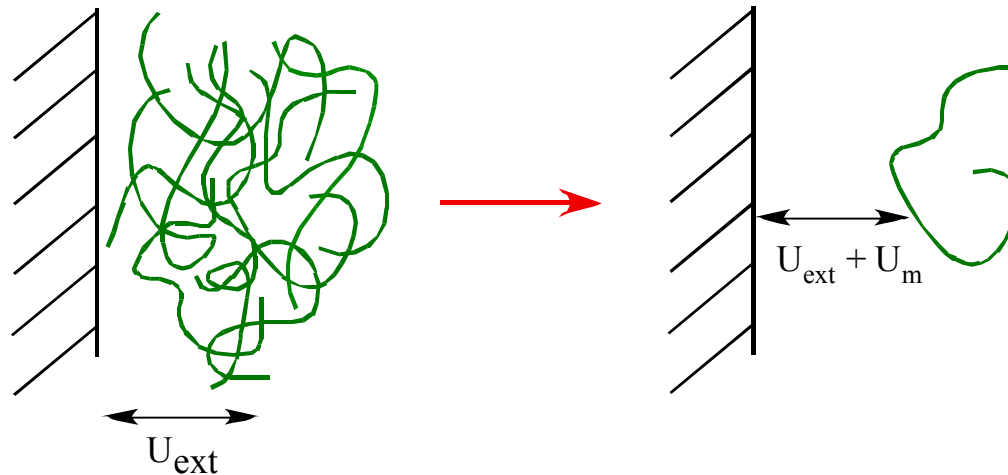
- depth of well decreases with both σ^* , α
- $r_{\min}$ increases with increasing σ^* , decreases with increasing α

Surface Plasmon Resonance



Hore, M. J. A., Frischknecht, A. L., & Composto, R. J. (2012), *ACS Macro Letters*, 1, 115–121.

Classical (Fluids) Density Functional Theory (DFT)



$$\Omega[\rho_\alpha(\mathbf{r})] = F[\rho_\alpha(\mathbf{r})] + \sum_\alpha \int d\mathbf{r} \rho_\alpha(\mathbf{r}) [V_\alpha(\mathbf{r}) - \mu_\alpha]$$

Helmholtz free energy F : ideal gas term,
monomer interactions, bonding

CMS-DFT
(Chandler, McCoy, Singer)

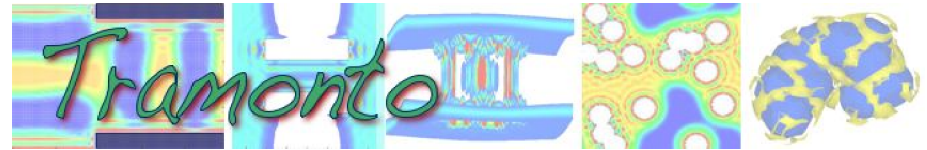
minimize free energy

$$\frac{\delta \Omega}{\delta \rho(\mathbf{r})} = 0 \longrightarrow \text{equations to solve for } \rho(\mathbf{r})$$

Fluids-DFT Implementation

solve nonlinear integral eqtns

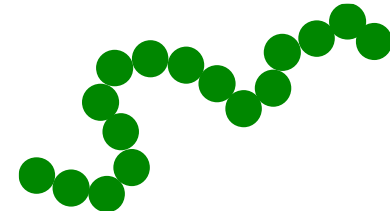
- in 3D, Cartesian grid
- modified Newton solver
- parallel



<http://software.sandia.gov/tramonto>

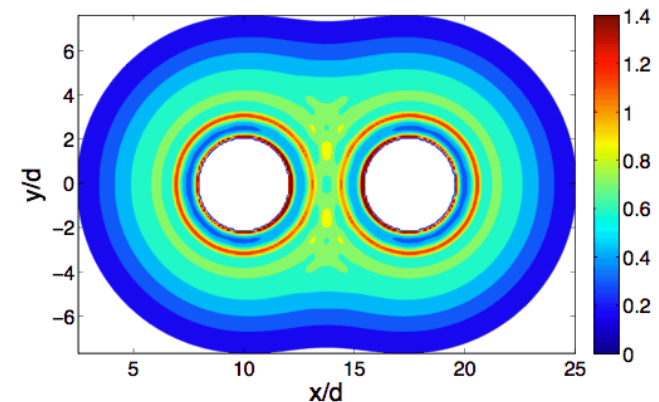
- **inputs**

- model of the fluid
 - freely-jointed tangent chains
 - repulsive LJ interactions
- bulk fluid densities (chemical potentials)
- surface geometry
 - NR exclude polymer
 - sticky ends attracted with LJ energy



- **outputs**

- fluid density profiles
- equilibrium free energy
 - phase diagrams
- adsorption, stress profiles, ...



Our approach: CMS-DFT

- chains are flexible
- 2nd order density expansion

Chandler, McCoy, Singer (1986);
McCoy et al. (1990s)

$$\rho_{\alpha}(r) = \frac{\rho_{\alpha}^b}{N_{\alpha}} \sum_{s=1}^{N_{\alpha}} \frac{G_s(r) G_s^i(r)}{e^{-\beta U_{\alpha}(r)}}$$

Chain density distribution

$$U_{\alpha}(r) = V_{ext}(r) - \sum_{\gamma} \int c_{\alpha\gamma}(r-r') [\rho_{\gamma}(r') - \rho_{\gamma}^b] dr'$$

Unknown field

$$c(r) = c_{rep}(r) - u_{att}(r)$$

PRISM
Theory

RPM
Approx

$$G_s(r) = e^{-\beta U_{\alpha,s}} \int w(r-r') G_{s-1}(r') dr'$$

$$G_s^i(r) = e^{-\beta U_{\alpha,s}} \int w(r-r') G_{s+1}^i(r') dr'$$

$$G_1 = G_N^i = e^{-\beta U(r)}$$

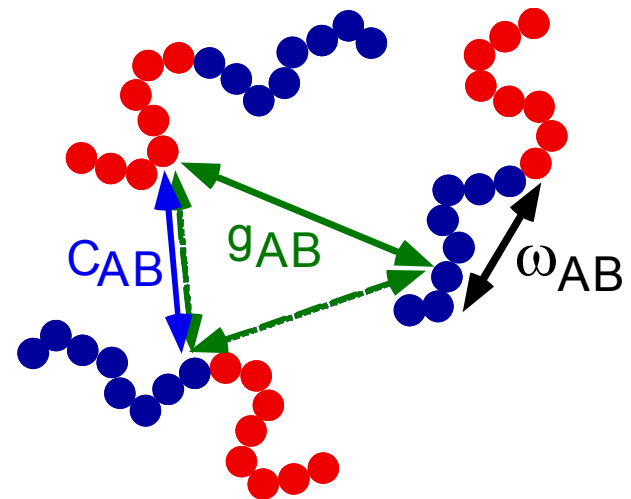
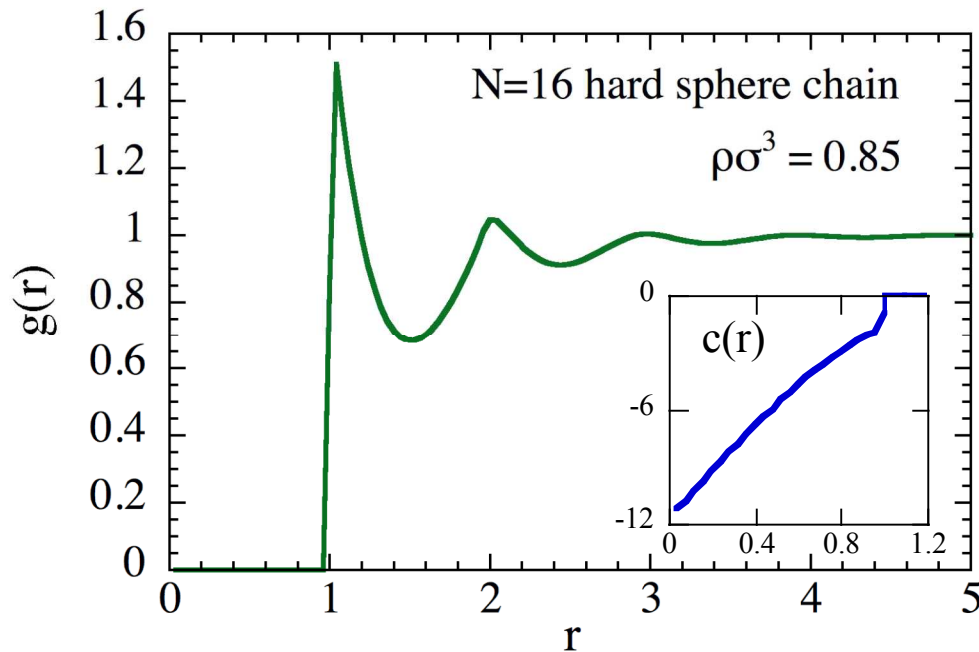
$$w(r) = \frac{1}{4\pi\sigma^2} \delta(|r| - \sigma)$$

Chain Architecture
(freely-jointed chains)

Input to CMS-DFT: PRISM Theory Sandia National Laboratories

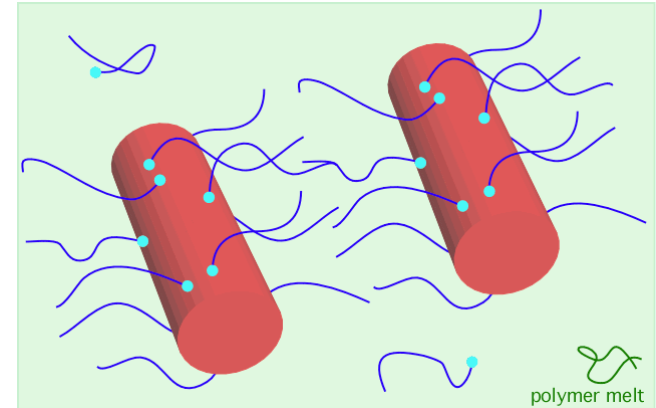
Curro and Schweizer

- Liquid state theory for homogeneous polymer fluids
 - intramolecular correlations ω_{AB}
 - intermolecular correlations $g_{AB}(r)$, $c_{AB}(r)$
- Excellent for repulsive interactions



Calculation Details

- parallel cylinders
- athermal (repulsive interactions)
- adsorbed chains
 - $N = 40$
 - $\rho_b a^3 = 0.01$
- matrix chains
 - $P = 40, 80, 120, 160$
 - $\rho_b a^3 = 0.85$



surface interactions:

- repulsive for matrix chains, all except end on adsorbing chains
- attractive to one end of adsorbing chains, depth ε_e