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*Title:* Solid-Solid Phase Transition Kinetics

*Author(s):* Laura Smilowitz  
Bryan Henson

*Intended for:* Energetic Materials Workshop  
Institute for Shock Physics  
Imperial College  
London, UK



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## Solid – Solid Phase Transition Kinetics

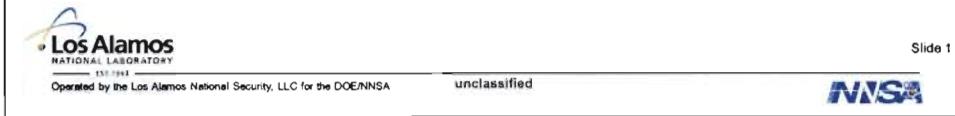
Laura Smilowitz and Bryan Henson  
*Chemistry Division, Los Alamos National Laboratory*

We will give a joint presentation by video teleconference to the Institute for Shock Physics, Imperial College, London. The presentation will cover experimental work unifying the kinetics of the beta-delta phase transition in HMX. We will also present theoretical work concerning the temperature dependence of the rate of transformation, which led to the publication of the virtual melt model of solid –solid phase transformation in 2004.

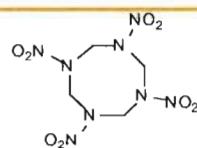
## Solid-solid phase transition kinetics

Laura Smilowitz, Bryan Henson,

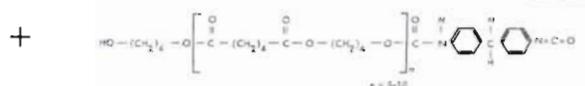
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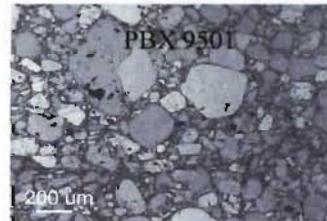
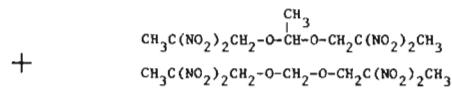
## PBX 9501 - Plastic Bonded Explosive



HMX (95%)



### Estane (2.5%)





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## Outline

- Introduction to Thermal Explosion
  - Pre-ignition thermal decomposition
    - HMX Polymorphs
  - Transition to ignition
  - Ignition
  - Post-ignition burn propagation
- Experimental tools
  - SHG, Raman, DSC
  - comparison of observables
- Kinetics results
- Model of phase transition

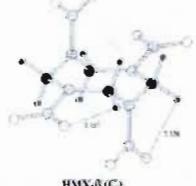
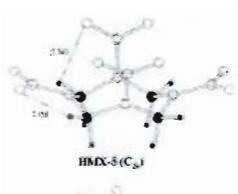


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## HMX Polymorphs



Optimized geometries of HMX- $\alpha$  and  $\beta$  form.

Chakraborty et al. (2001) *J. Phys. Chem. A*

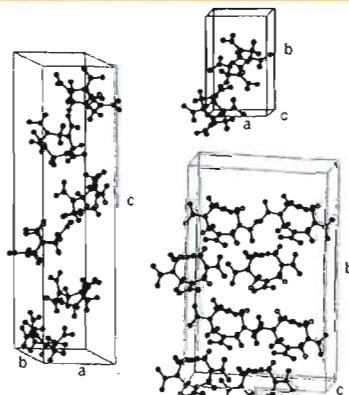


Figure 1. Unit cells for HMX polymorphs. Clockwise from top:  $\beta$ ,  $\alpha$ , and  $\delta$ .

D. Bedrov et al. (2004) *Journal of Computer Aided Materials Design*, 8, 77-85.



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## HMX Polymorphs: $\beta$ , $\alpha$ , $\delta$

Thermodynamics- which phase is stable, not how to get there

Kinetics- how to get there- needs to return thermodynamic phase diagram

Phase	$\beta$	$\alpha$	$\delta$
Sensitivity (drop hammer)	35cm	12cm	7cm
Volume change	0	$\beta +4\%$	$\beta +7\%$
Temperature stability	<105	103-160	>160

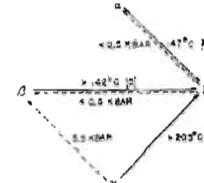


Figure 5. A summary of the temperature- and pressure-induced phase transitions of the  $\alpha$ ,  $\beta$ ,  $\gamma$ , and  $\delta$ -polymorphs of HMX. The solid lines are transitions with slow heating (ref 1) and the dashed lines are transitions with pressure. (R) indicates reversibility with cooling.

Reference: LAMS-2652Studies on the polymorphs of HMX

Author: Cady, H.H., Smith, Louis C., LANL, Oct. 18, 1961.



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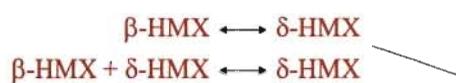
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Reference: Brill, JCP 24 Aug 1978; vol.82, no.17, p.1912-1917

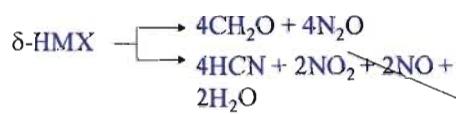
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## Chemical Kinetic Model for Decomposition of HMX



L. Smilowitz (Los Alamos)



R. Behrens (SNL)



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## Focus on 1<sup>st</sup> step: solid-solid phase transition

- What we've done:

- Developed SHG probe as an instantaneous measure of the solid state fraction of beta and delta
- Used SHG in an imaging mode (SHG microscope) to make ansatz about mechanism of phase change: nucleation and growth
- Used integral SHG signal as measure of delta fraction
- Compare SHG observable to other observables: Raman, X-ray, DSC

- Results:

A nucleation and growth model for the solid state phase transition with growth kinetics determined by thermodynamic properties of HMX and the nucleation kinetics empirically fit



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## Experimental suite for solid-solid phase transition studies:

- SHG microscope
- Integrated SHG
- Raman (in situ, post mortem)
- FTIR (post mortem)
- DSC (differential scanning calorimetry)
- Temperature



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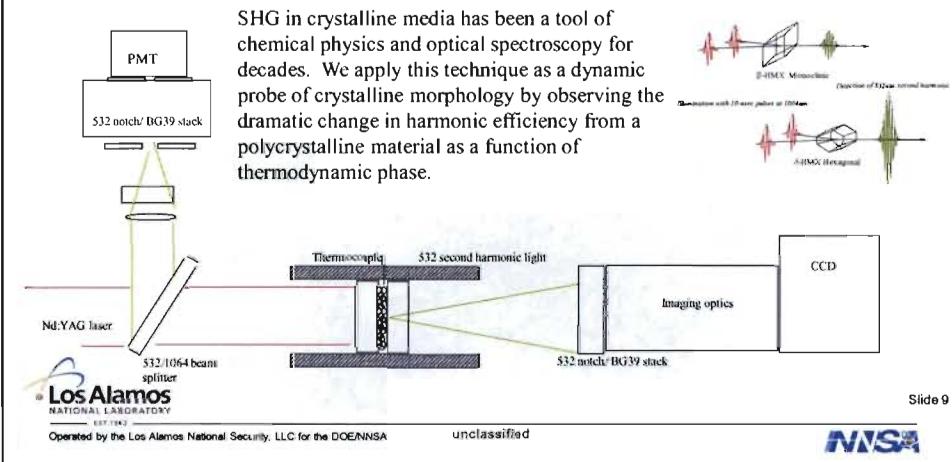
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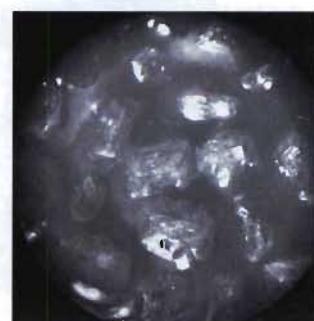


## Detailed study of initial thermal decomposition steps via dynamic SHG microscopy of $\beta$ - $\delta$ transition

SHG microscope developed in C-PCS images with contrast is generated by the SHG symmetry selection rules (only generated from noncentrosymmetric systems).



## Crystal bed photos



Beta vs delta phase: white light images



K31-1342

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## Multi HMX crystal isothermal SHG microscopy



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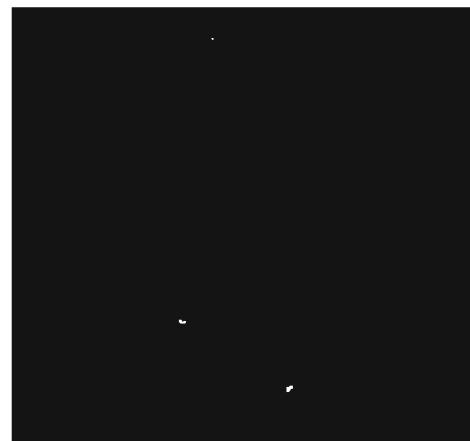
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## Multi HMX crystal isothermal SHG microscopy



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## White light hot stage microscopy



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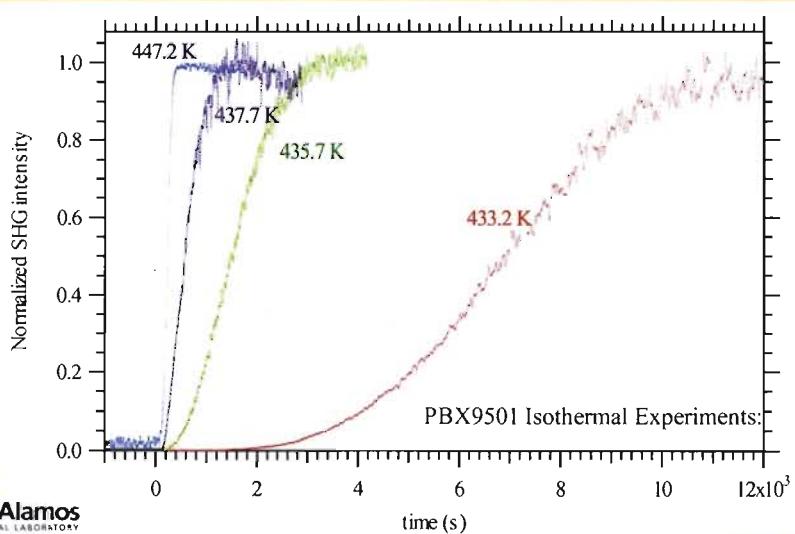
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## Integrated SHG Results



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## Conclusions on comparison of observables

- All are in agreement, *assuming* that the observable probes a representative volume element
- Relative advantages/disadvantages of each:
  - SHG- sensitivity, but it's a relative measure
  - Raman- lose sensitivity when do spatial integration, but can distinguish non-centrosymmetric phases. Hard to use as an absolute measure (baseline fluorescence, change in optical properties)
  - DSC- not an integral measure, so less sensitive and rate dependent, but best for use as an absolute measure. There is a minimum conversion rate needed for observation (dependent on baseline thermal stability)

Smilowitz, L.; Henson, B. F.; Romero, J. J., Intercomparison of Calorimetry, Raman Spectroscopy, and Second Harmonic Generation Applied to Solid-Solid Phase Transitions. *JOURNAL OF PHYSICAL CHEMISTRY A* 2009, 113, (35), 9650-9657.



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## Kinetic Model Summary

Rate controlled by an activation energy which is equivalent to the heat of fusion.

Balance of forward and reverse growth rates defines equilibrium temperature (cusp in half-time curve)

2nd order kinetics- acceleratory behavior due to dependence on interface between  $\beta$ - $\delta$

2<sup>nd</sup> order kinetic component yields a 1<sup>st</sup> order thermodynamic transition

**virtual melt state-** activation energy = **heat of fusion**,

but phase transition is occurring at  $T < T_m$

Theory by V. Levitas based on the lowering of the melt temperature for a region of local tension at the interface – solves many previously reported conundra

Levitas, V. I.; Henson, B. F.; Smilowitz, L. B.; Asay, B. W., Solid-solid phase transformation via virtual melting significantly below the melting temperature. *Physical Review Letters* 2004, 11, (92), 235702-1

Levitas, V. I.; Smilowitz, L. B.; Henson, B. F.; Asay, B. W., Solid-solid phase transformation via internal stress-induced virtual melting:

Additional confirmations. *Applied Physics Letters* 2005, 87, (19), 1-3



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## Comparison of observables

- There are inherent difficulties in observing solid to solid phase transitions- solids are heterogeneous and optically opaque, hindering observation.
- There have been confusing and contradictory reports with different kinetics reported depending on the observable- SHG vs Raman vs DSC vs X-ray vs dilatometry
- The goal of this study was to validate SHG as a probe of  $\delta$  fraction, and understand the contradictions between observables



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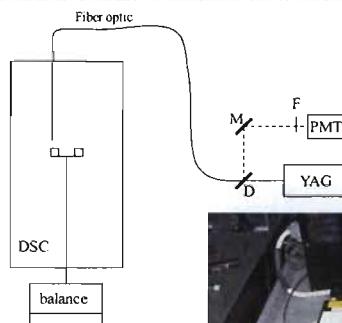
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## Experiment: DSC/TGA/MS: with SHG

Goal- couple existing diagnostics to probe solid state lattice, solid to gas dynamics, and gas phase products simultaneously



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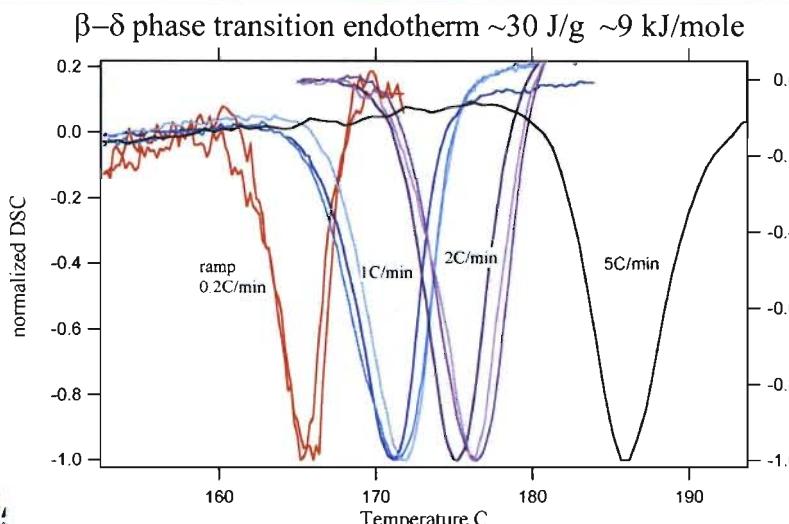
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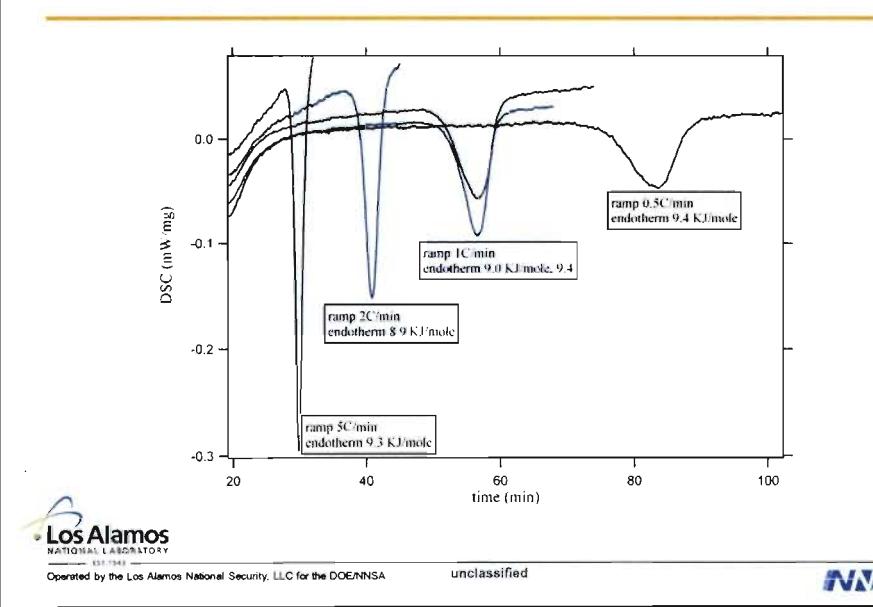
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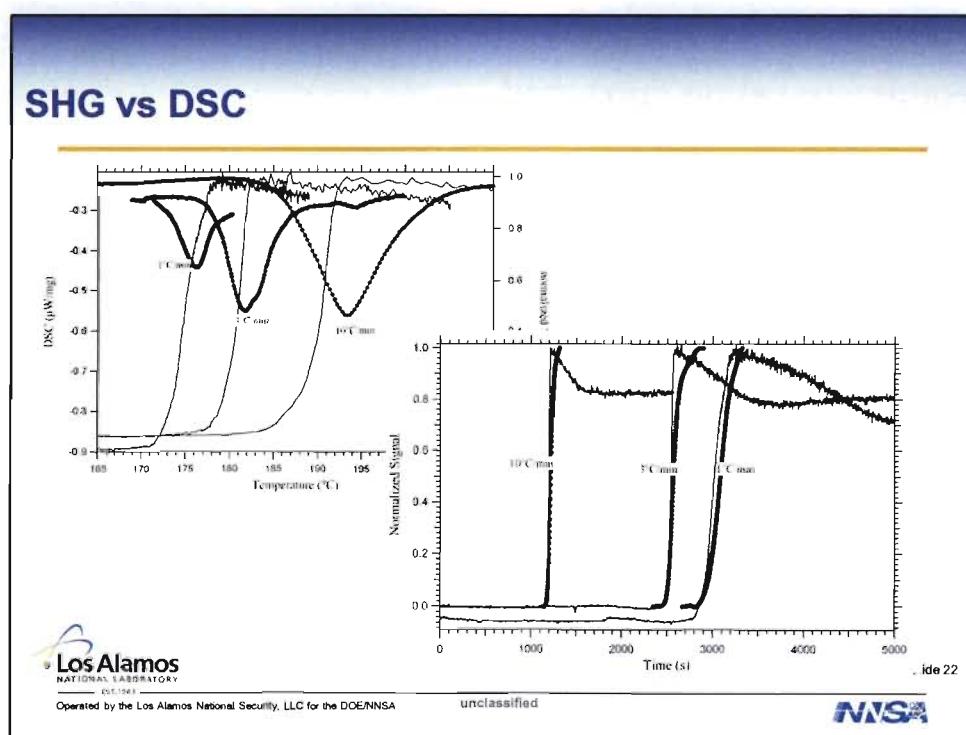
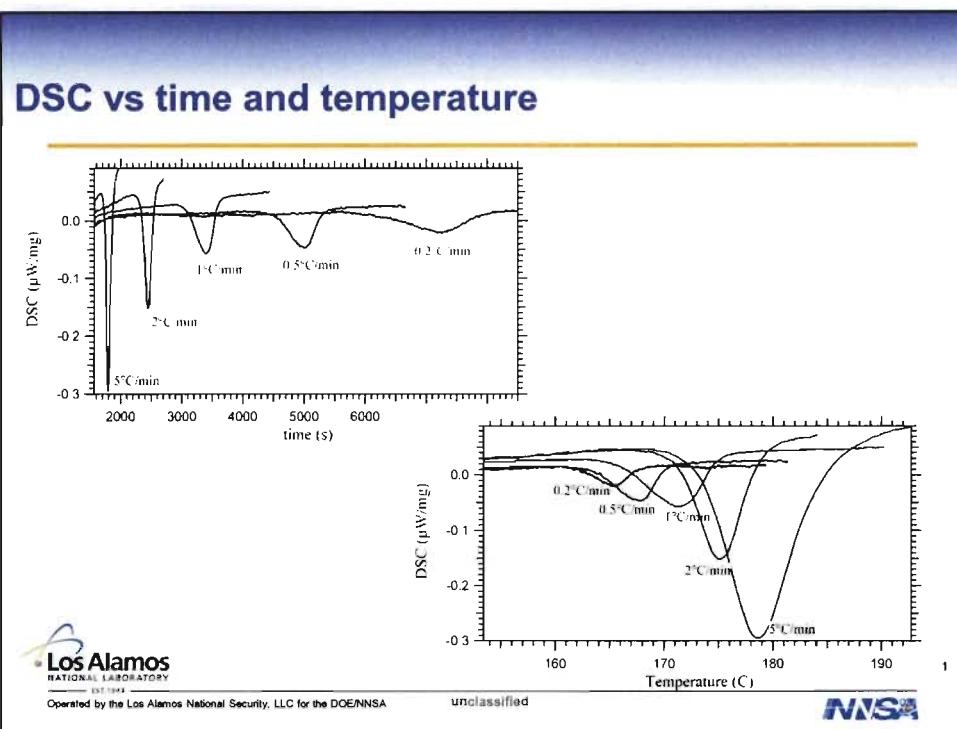


## DSC results overview

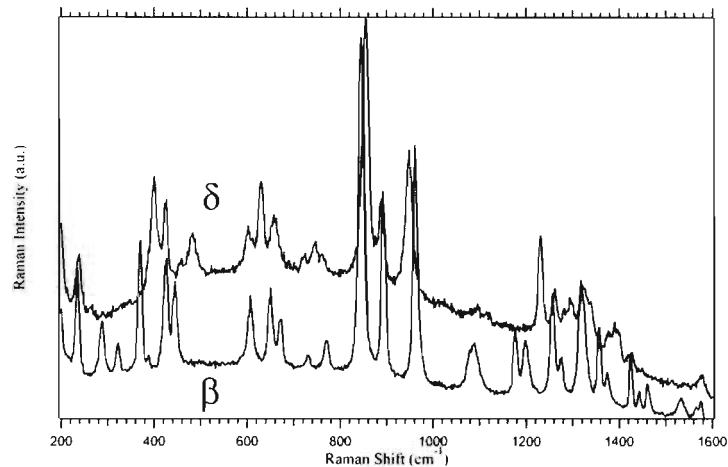


## DSC





## Raman



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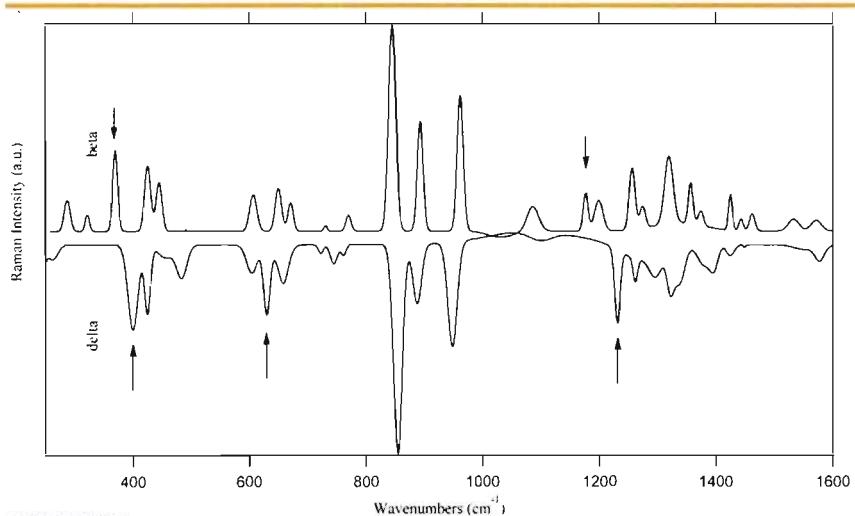
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## Raman baseline corrected



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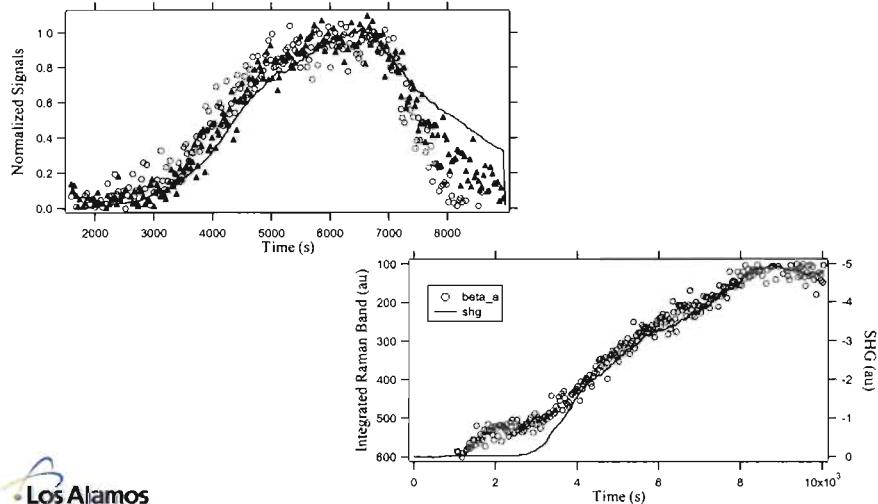
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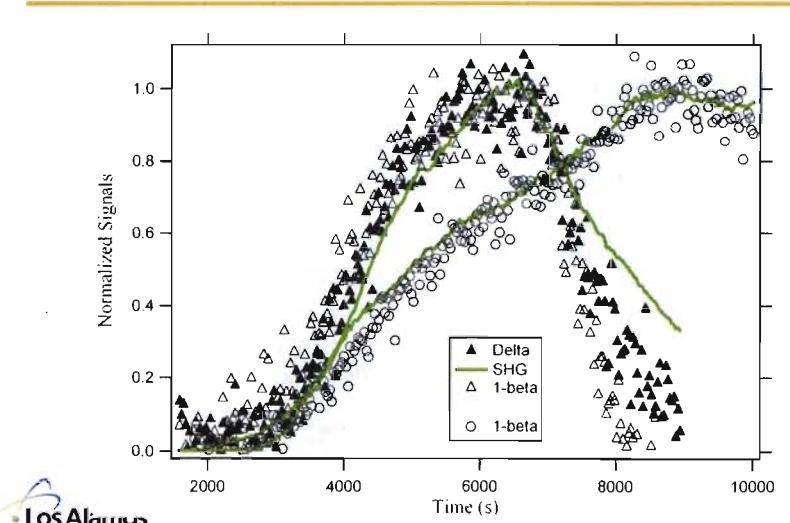


## Raman vs SHG



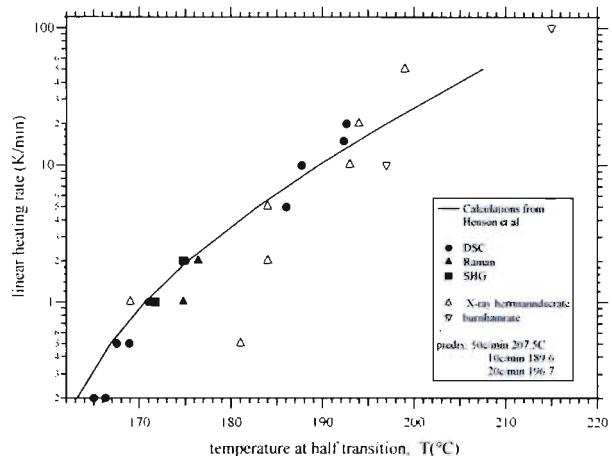
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## Raman/SHG



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## Raman/SHG/DSC vs model



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## Conclusions on comparison of observables

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- Relative advantages/disadvantages of each:
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  - Raman- lose sensitivity when do spatial integration, but can distinguish non-centrosymmetric phases. Hard to use as an absolute measure (baseline florescence, change in optical properties)
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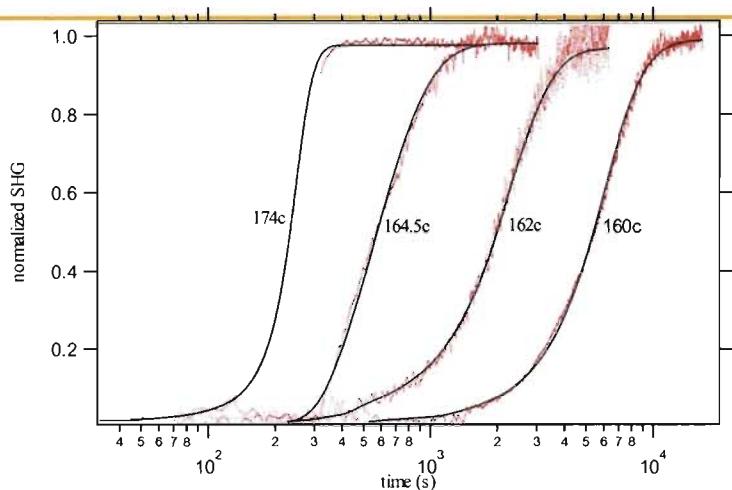
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## Kinetics



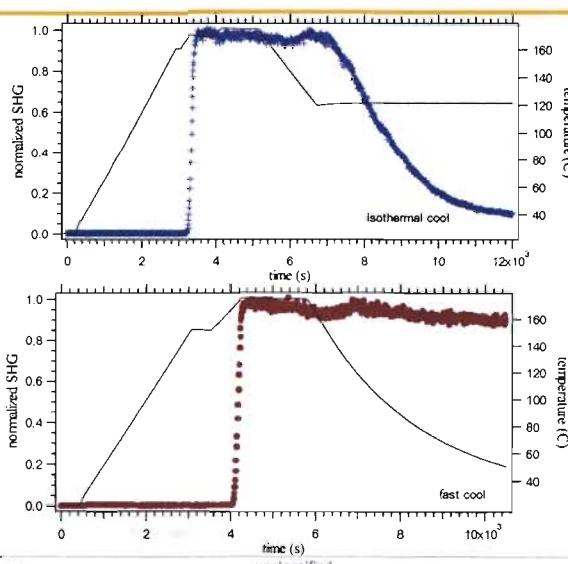
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## Controlling Reversion



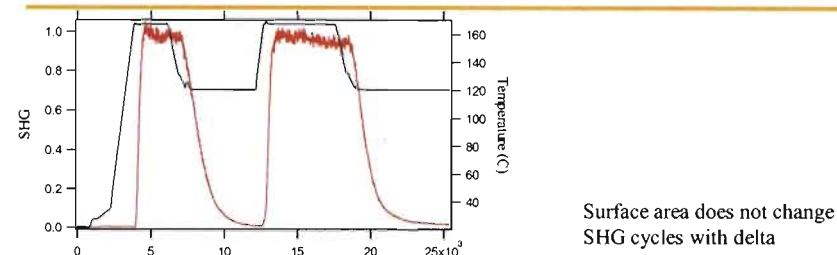
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## Reversibility of phase transition



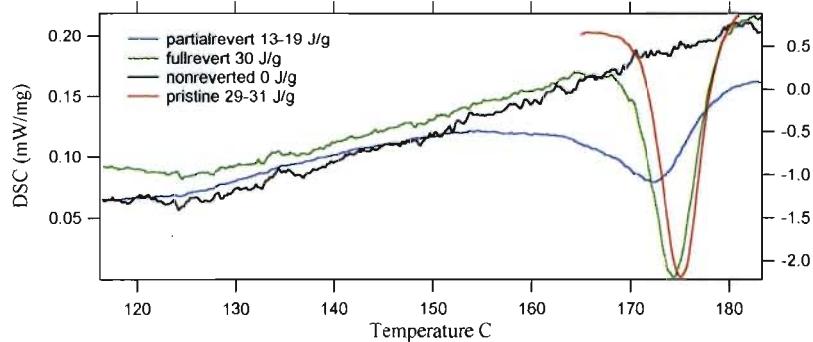
Surface area does not change  
SHG cycles with delta

Implies: not a SA effect  
and, mechanical damage  
does not significantly affect  
kinetics

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## Reversion experiments



Seeded growth  
Fully reverted  $\beta$  – same calorimetry as pristine  $\beta$   
Quenched  $\delta$  – no endotherm

Therefore- we can separate polymorph phase from mechanical damage state

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## Kinetics of PBX9501

- Observe- reversible transition
- Sigmoidal kinetics
- Use reversible nucleation and growth model with Arrhenius rates and transition state for growth step= melt state
  - determine thermodynamic parameters to fit forward reaction rates at different temperatures/ramp rates (feedback into larger scale experiments)



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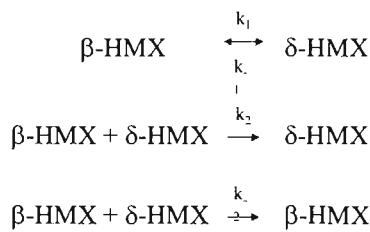
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## Model $\beta$ - $\delta$ phase transition:

Coupled first order nucleation and second order growth



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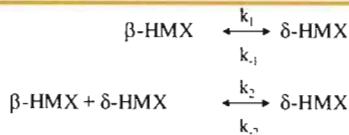
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## Transition kinetics



Nucleation and growth rate law:

$$d\delta/dt = k_1 \beta + k_2 \beta^* \delta - k_{-1} \delta - k_{-2} \beta^* \delta$$

Where:  $k_i(T) = kT/h \exp((T\Delta S^* - \Delta H^*)/RT)$   
 $= kT/h \exp(-\Delta G^*/RT)$

the rate is determined by the thermodynamic parameters of the transition state

Transition state = melt state  
 $\Delta G^* = \Delta G_{\text{fusion}}$



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## Virtual Melt

Valery I. Levitas,\*† Bryan F. Henson,‡ Laura B. Smilowitz,‡ and Blaine W. Asay‡  
*J. Phys. Chem. B* 2006, 110, 10105-10119

We theoretically predict a new phenomenon, namely, that a solid-solid phase transformation (PT) with a large transformation strain can occur via internal stress-induced virtual melting along the interface at temperatures significantly (more than 100 K) below the melting temperature. We show that the energy of elastic stresses, induced by transformation strain, increases the driving force for melting and reduces the melting temperature. Immediately after melting, stresses relax and the unstable melt solidifies. Fast solidification in a thin layer leads to nanoscale cracking which does not affect the thermodynamics or kinetics of the solid-solid transformation. Thus, virtual melting represents a new mechanism of solid-solid PT, stress relaxation, and loss of coherence at a moving solid-solid interface. ... Sixteen theoretical predictions are in qualitative and quantitative agreement with experiments conducted on the PTs in the energetic crystal HMX. In particular, (a) the energy of internal stresses is sufficient to reduce the melting temperature from 551 to 430 K for the  $\bar{\alpha}$  phase during the  $\bar{\alpha} \rightleftharpoons \bar{\beta}$  PT and from 520 to 400 K for the  $\bar{\beta}$  phase during the  $\bar{\beta} \rightleftharpoons \bar{\alpha}$  PT; (b) predicted activation energies for direct and reverse PTs coincide with corresponding melting energies of the  $\bar{\alpha}$  and  $\bar{\beta}$  phases and with the experimental values; (c) the temperature dependence of the rate constant is determined by the heat of fusion, for both direct and reverse PTs; results b and c are obtained both for overall kinetics and for interface propagation; (d) considerable nanocracking, homogeneously distributed in the transformed material, accompanies the PT, as predicted by theory; (e) the nanocracking does not change the PT thermodynamics or kinetics appreciably for the first and the second  $\bar{\alpha} \rightleftharpoons \bar{\beta}$  cycles, as predicted by theory; (f)  $\bar{\alpha} \rightleftharpoons \bar{\beta}$  PTs start at a very small driving force (in contrast to all known solid-solid transformations with large transformation strain), that is, elastic energy and athermal interface friction must be negligible; (g)  $\bar{\alpha} \rightleftharpoons \bar{\beta}$  and  $\bar{\beta} \rightleftharpoons \bar{\alpha}$  PTs, which are thermodynamically possible in the temperature range  $382.4 < \delta < 430$  K and below 382.4 K, respectively, do not occur.

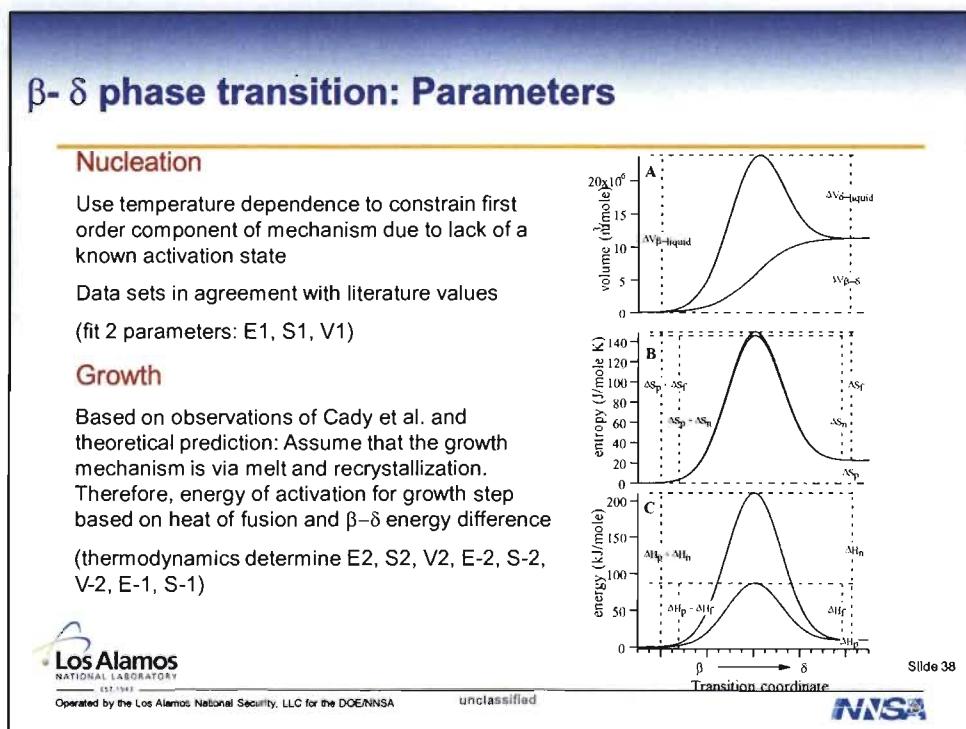
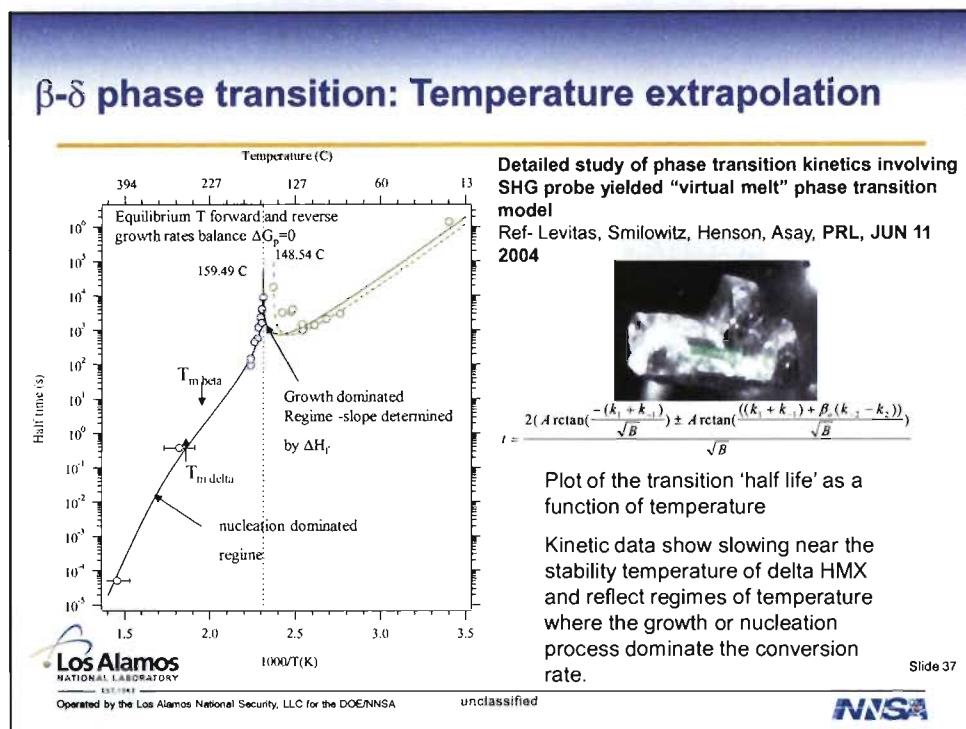
- Levit, V. I.; Henson, B. F.; Smilowitz, L. B.; Asay, B. W., Solid-solid phase transformation via virtual melting significantly below the melting temperature. *Physical Review Letters* 2004, 11, (92), 235702-1
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$$\frac{\partial x}{\partial t} = k_1(1-x) - k_{-1}x + \beta_o(k_2 - k_{-2})x(1-x)$$

<p>First order kinetics</p> $\frac{\partial x}{\partial t} = k_1(1-x) - k_{-1}x$ $x_e = \frac{k_1}{k_1 + k_{-1}}$ $\frac{k_1}{k_1 + k_{-1}} = \frac{\exp\left(-\frac{\Delta G_{phase}}{RT}\right)}{\left(1 + \exp\left(-\frac{\Delta G_{phase}}{RT}\right)\right)}$ $x_e = \frac{\exp\left(-\frac{G_\delta}{RT}\right)}{\exp\left(-\frac{G_\delta}{RT}\right) + \exp\left(-\frac{G_\beta}{RT}\right)}$	<p>Second order kinetics</p> $\frac{\partial x}{\partial t} = \beta_o(k_2 - k_{-2})x(1-x)$ $\beta_o(k_2 - k_{-2}) = 0$ $k_2(T) - k_{-2}(T) = \frac{k_b T}{h} Q \exp\left(-\frac{\Delta G_{fusion}}{RT}\right) \left(1 - \exp\left(-\frac{\Delta G_{phase}}{RT}\right)\right)$ $\Delta G_{phase} = \Delta H_{phase} - T\Delta S_{phase} = 0$ $T = T_{phase}$
--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------	-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------

Second order thermodynamics

First order thermodynamics

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## Thermodynamics vs. kinetics

- Thermodynamics typically determines *whether* something will happen, not how *fast*
  - However, equilibrium is not static
  - Simple TST theory of sublimation

kinetic order

$\nu[X_e^{area}] = [\rho_{solid}] \frac{k_b T}{h} \frac{[q_{area}^{rea}]}{[q_{solution}]} \exp\left(-\frac{\Delta H_{sub}^*}{RT}\right)$

$\frac{\partial n}{\partial t} = \nu \exp\left(-\frac{\Delta G^*}{RT}\right) \int A(n) dA$

$\frac{\partial n}{\partial A \partial t} = \nu \exp\left(\frac{\Delta S_{sub}^* T - \Delta H_{sub}^*}{RT}\right)$

$\frac{\partial n}{\partial A \partial t} = \frac{1}{\sqrt{2\pi mkT}} P$

▪ kinetic rate (Hertz-Knudsen)

$\frac{\partial n}{\partial t} = -kn^0$

$\frac{\partial n}{\partial t} = -kn^{2/3}$

$\frac{\partial n}{\partial t} = -kn^1$

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## Kinetic Model Summary

Rate controlled by an activation energy which is equivalent to the heat of fusion.  
Balance of forward and reverse growth rates defines equilibrium temperature (cusp in half-time curve)  
2nd order kinetics- acceleratory behavior due to dependence on interface between  $\beta$ - $\delta$   
2nd order kinetic component yields a 1st order thermodynamic transition  
**virtual melt state**- activation energy = heat of fusion,  
but phase transition is occurring at  $T < T_m$   
Theory by V. Levitas based on the lowering of the melt temperature for a region of local tension at the interface – solves many previously reported conundra

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## Summary

- $\beta$ - $\delta$  phase transition in HMX occurs via 2nd order nucleation and growth mechanism
- The rate of growth is controlled by the heat of fusion at a temperature 100C below the thermodynamically stable melt
- A virtual melt mechanism has been developed which explains this phenomenon
- SHG as a viable tool for studying solid state phase transitions has been validated against DSC
- Previously reported inconsistencies between various observables have been explained.



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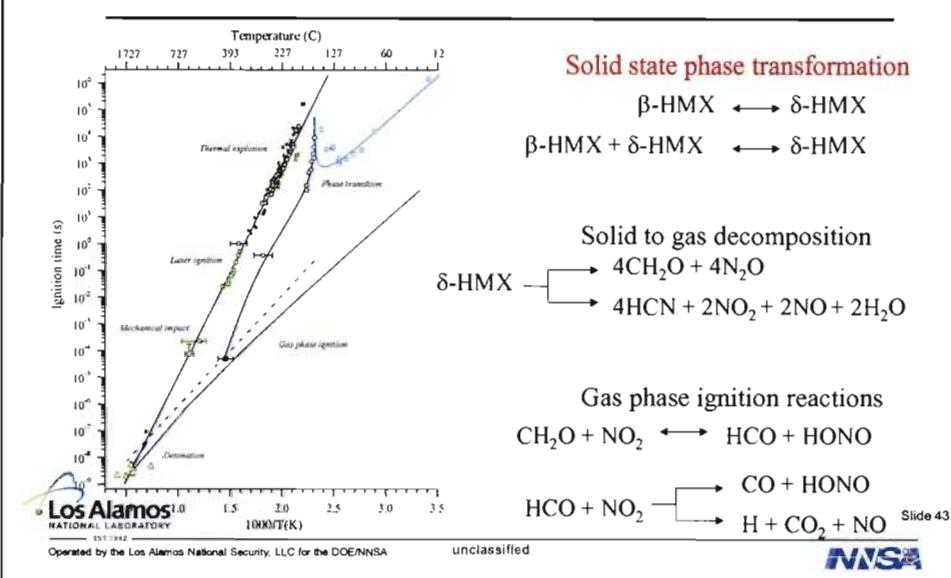
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## The phase transition and chemical decomposition



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