



VHF and UHF Mechanically Coupled AlN MEMS Filters

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Outline

- Background and Motivation
 - *MEMS Filter Motivation*
 - *Mechanically Coupled Filter Architecture*
 - *Low Impedance Piezoelectric Transduction*
- VHF Mechanically Coupled Ring Resonator Filters
 - *100 MHz Mechanically Coupled Filter Measurements*
 - *Filter Temperature Sensitivity and Compensation*
- UHF Overtone Mechanically Coupled Ring Resonator Filters
 - *Filter Design and Measured Results*
 - *Performance Discussion*
- Conclusions and Acknowledgements



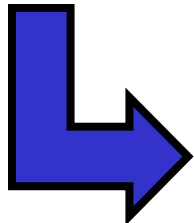
Piezoelectric MEMS Filter Research

- MEMS Filters

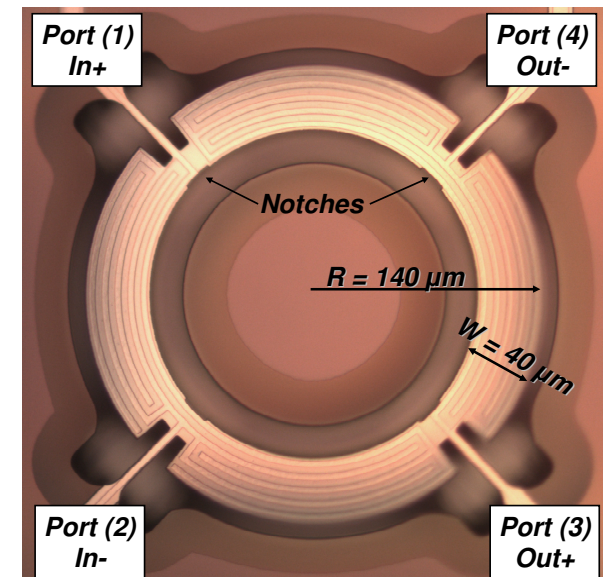
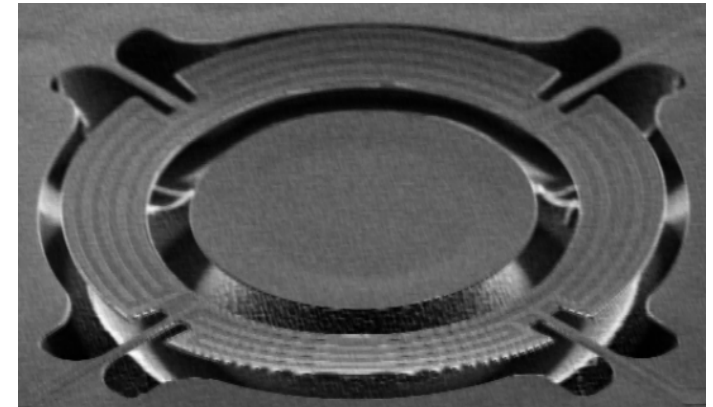
- Small
- Many Frequencies on a Single Chip
- Greater Coupling per Area for the VHF and a Portion of the UHF Band

- Miniature High-Selectivity Filters and Filter Banks not Available in Commodity Driven Wireless Market

- RF Filters in Non-Commercial Bands
- Miniature SAW IF Filter Replacement
- **Filter Banks for Spectrum Analysis and Cognitive Radios**



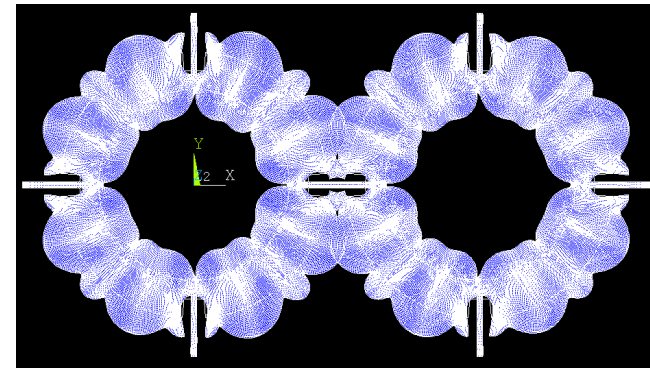
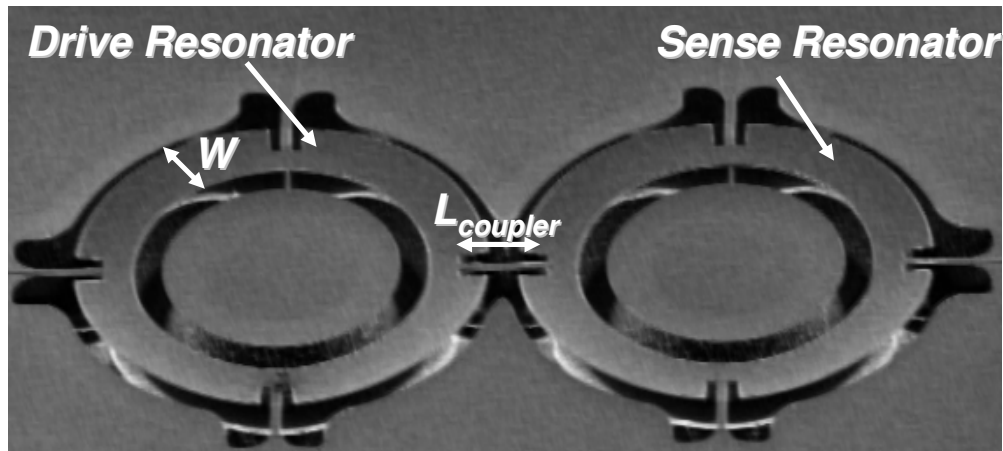
- Electrically Coupled Filters
- Dual Mode Filters
- **Mechanically Coupled Filters**



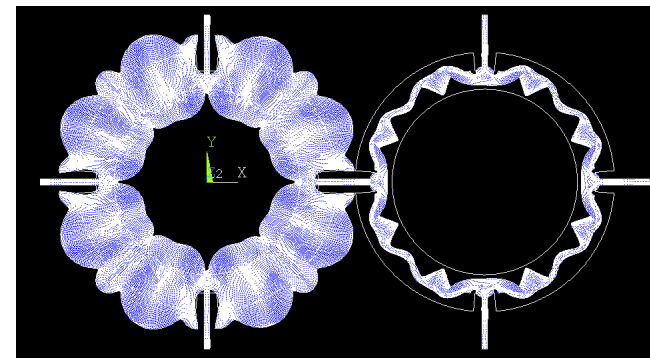
5th Overtone Dual Mode Filter Images



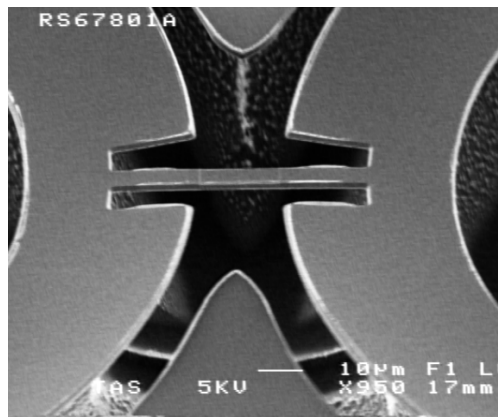
Filter Architecture and Design



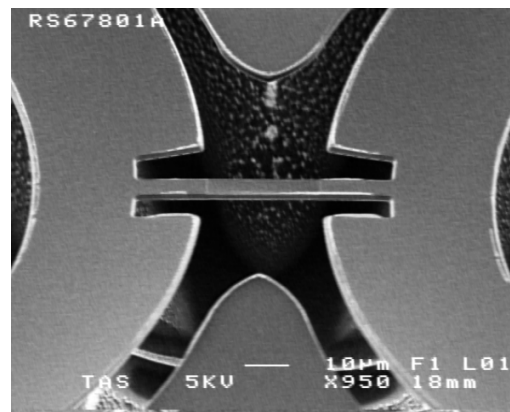
f_{mode0}



f_{mode1}



Narrowest
Bandwidth when
Coupled at Ring
Center



Increase
Bandwidth by
Moving to Higher
Velocity Coupling

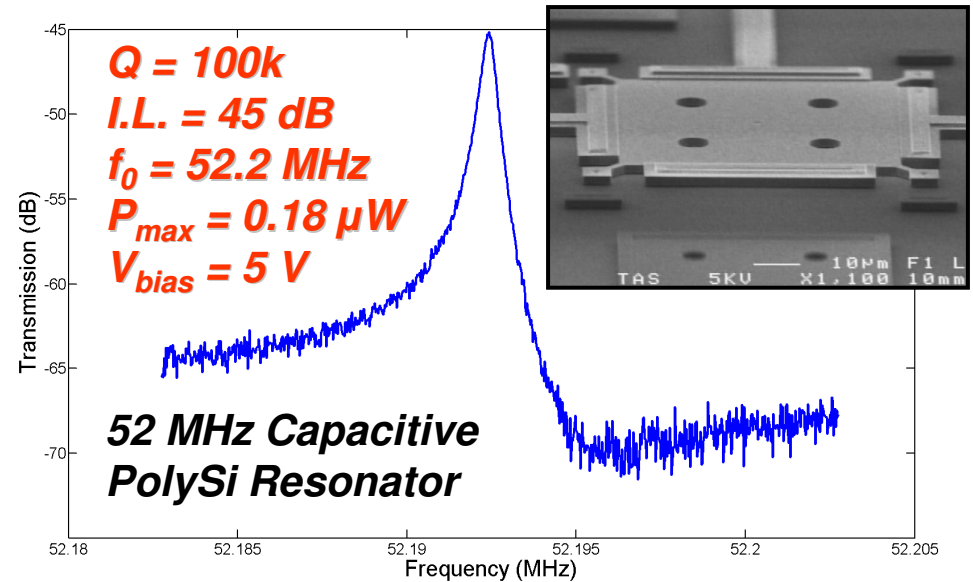
**Narrow Bandwidth MEMS
Filter Architecture 1st
Reported in PolySi by Li et al,
Ultrasonics Symposium 2005**



Piezoelectric Transduction

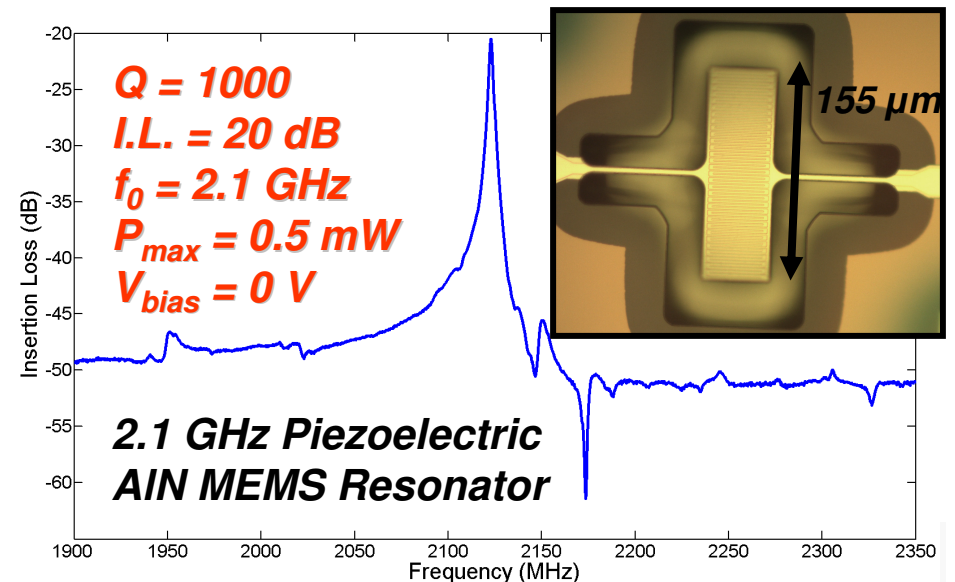
• Capacitive Resonators

- High Impedance (20 k Ω)
- High-Q (100k)
- Force $\approx V^2$
- Low Power Handling (0.2 μ W)
- PolySi not Post-CMOS Compatible (High Temp.)



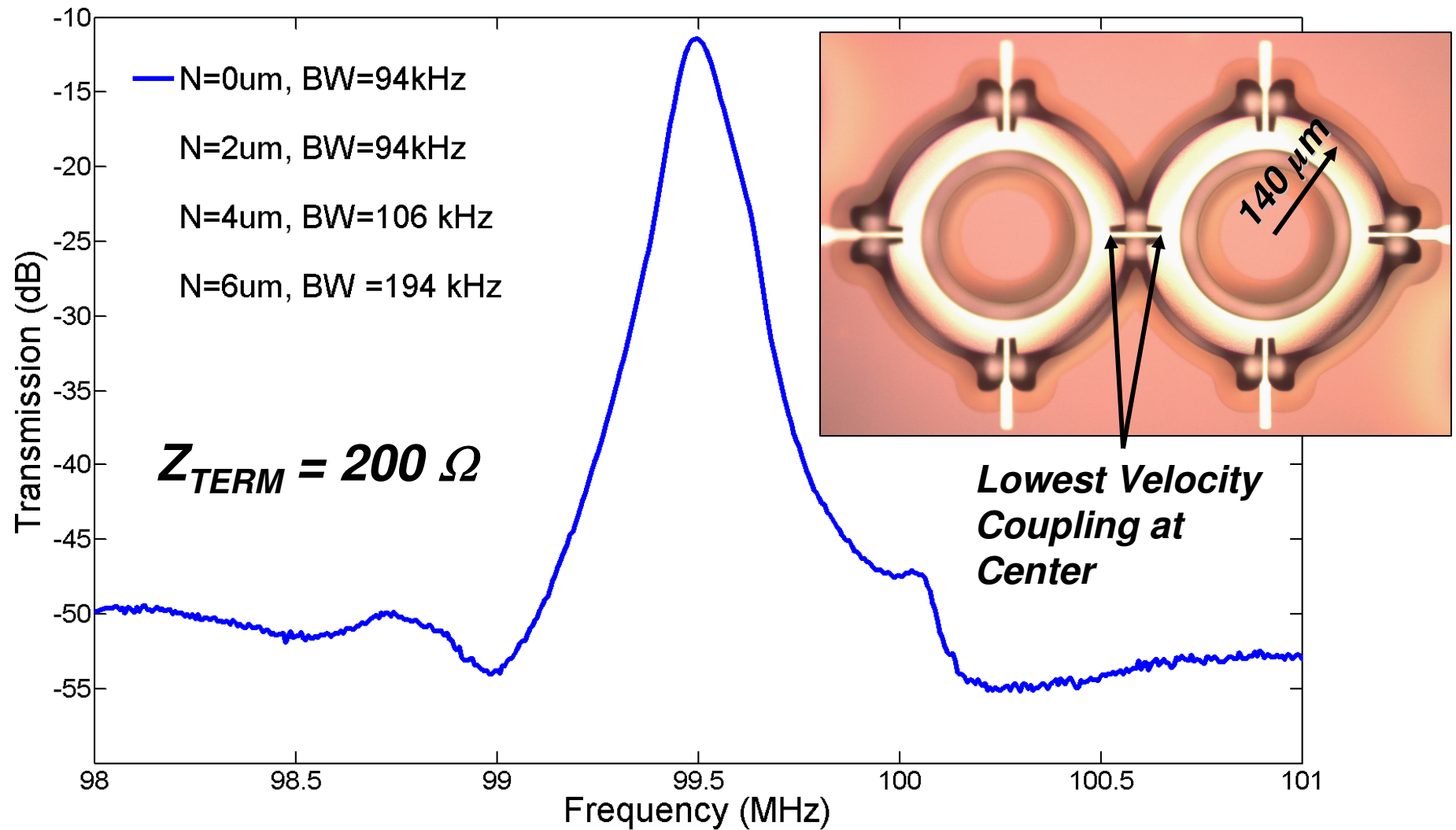
• Piezoelectric Resonators

- Low Impedance (1 k Ω)
- Lower Q (1000)
- Force $\approx V$
- High Power Handling (0.5 mW)
- AlN Post-CMOS Compatible



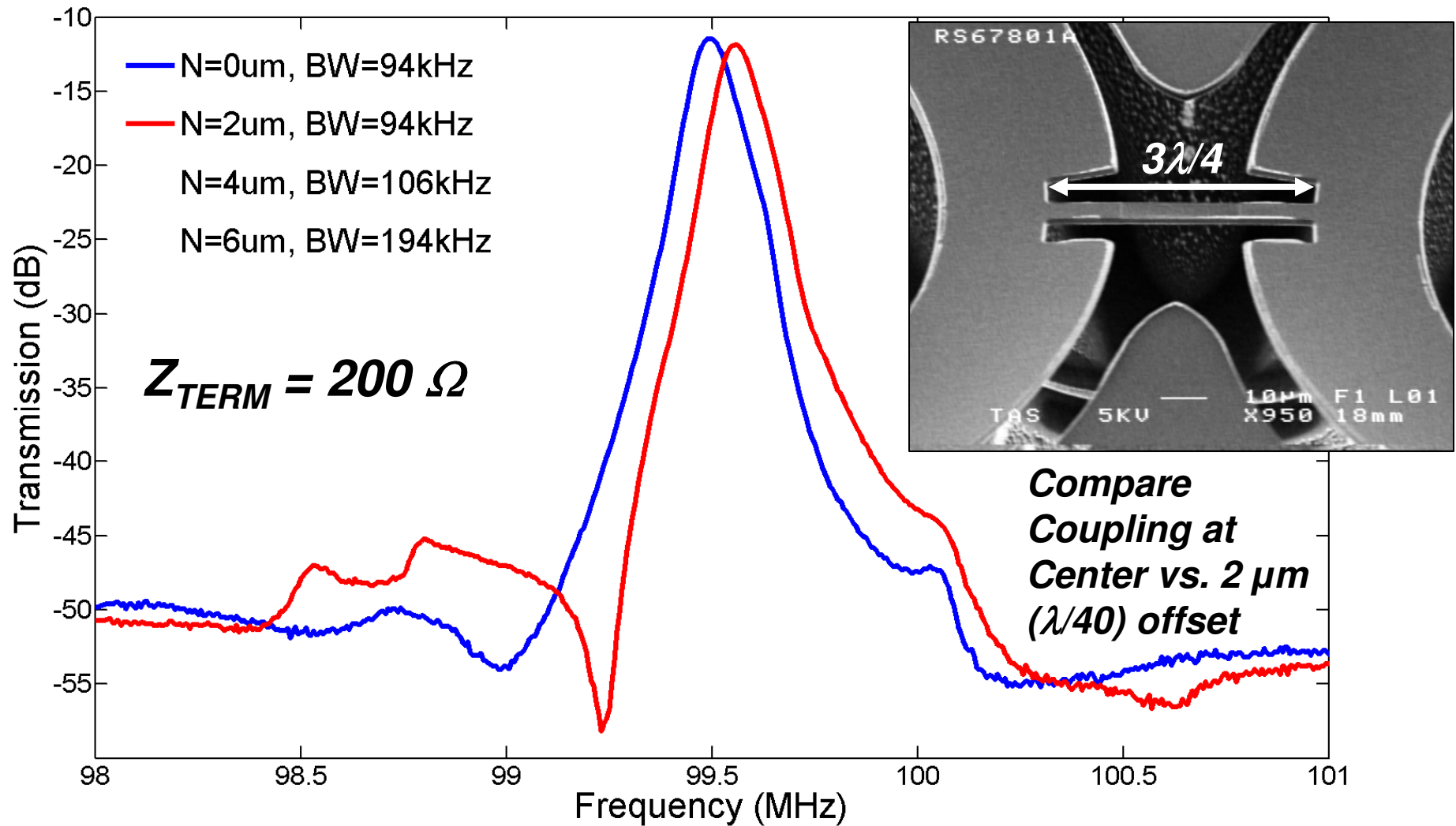


Measured Results



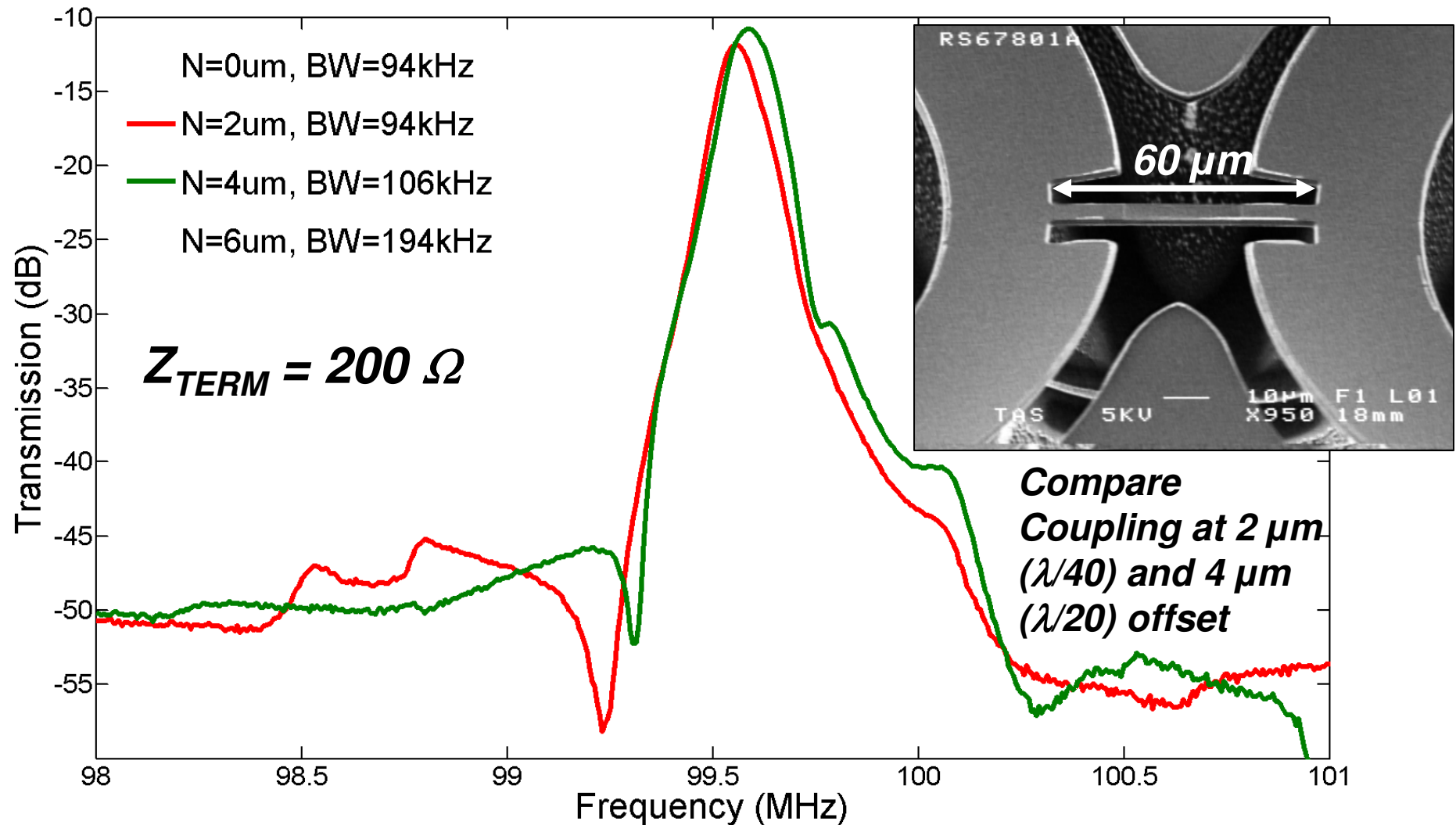


Measured Results



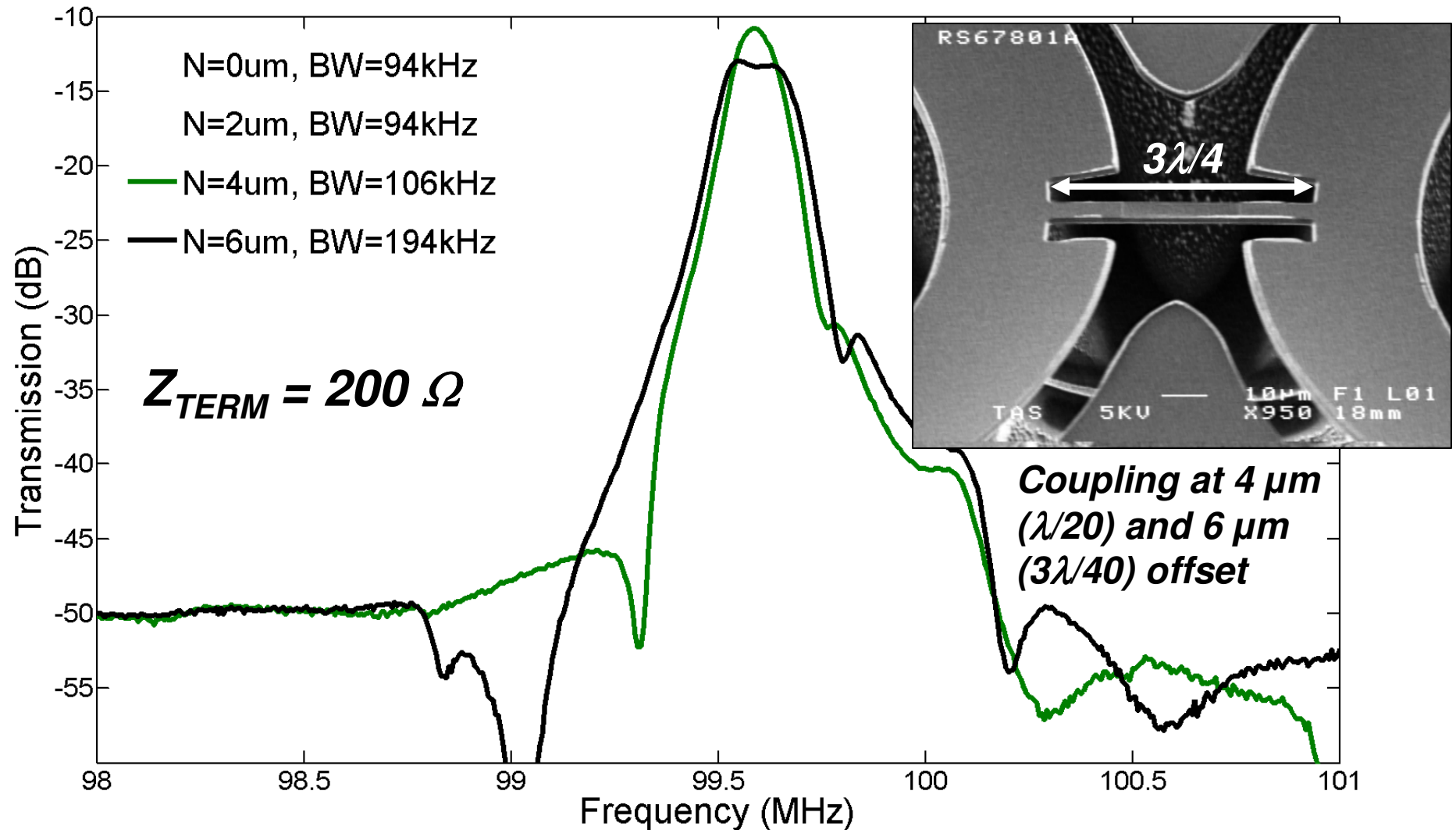


Measured Results



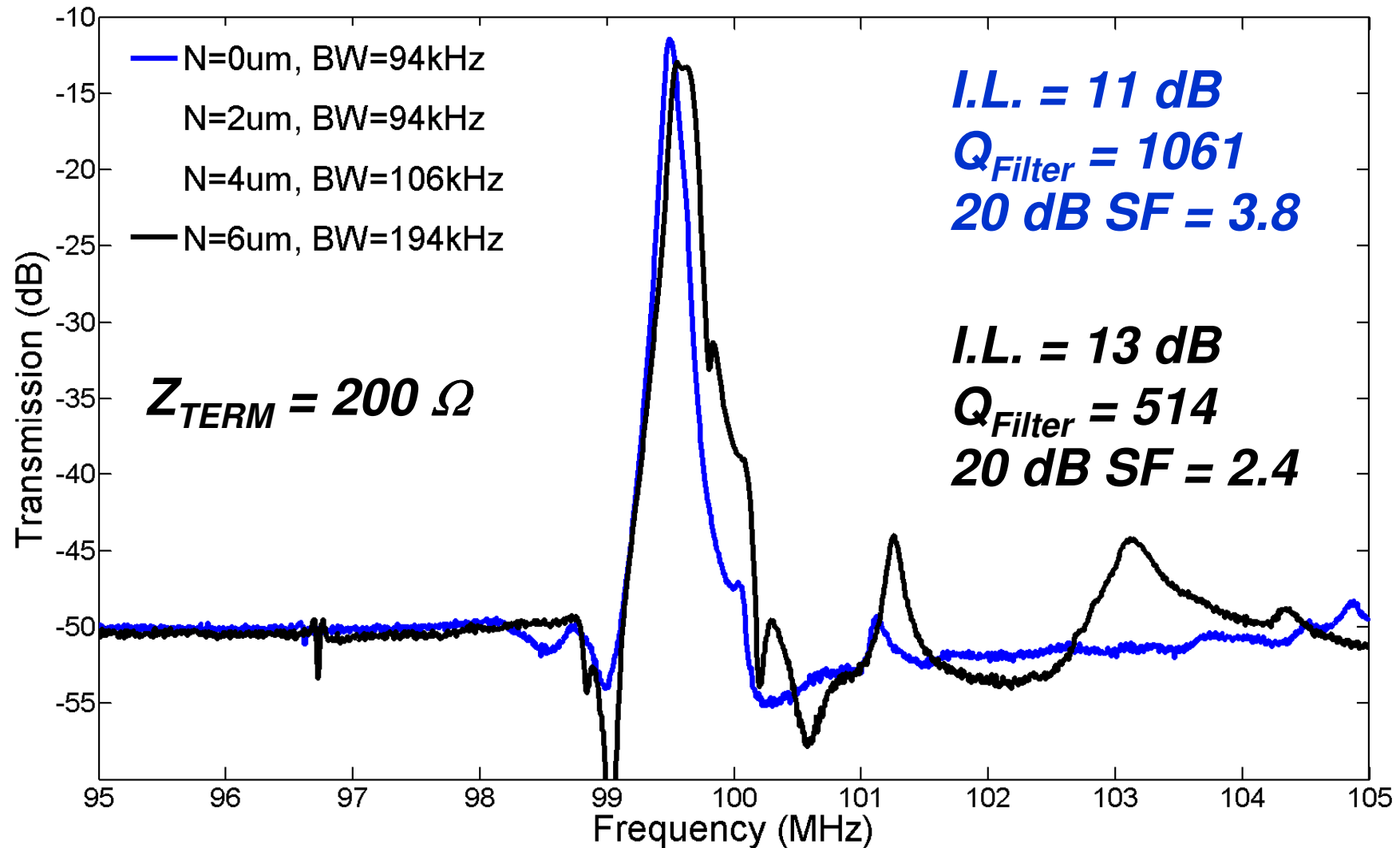


Measured Results



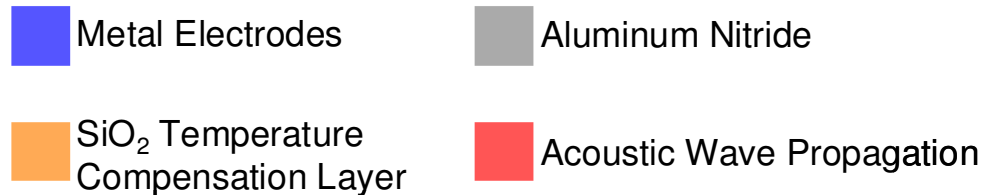
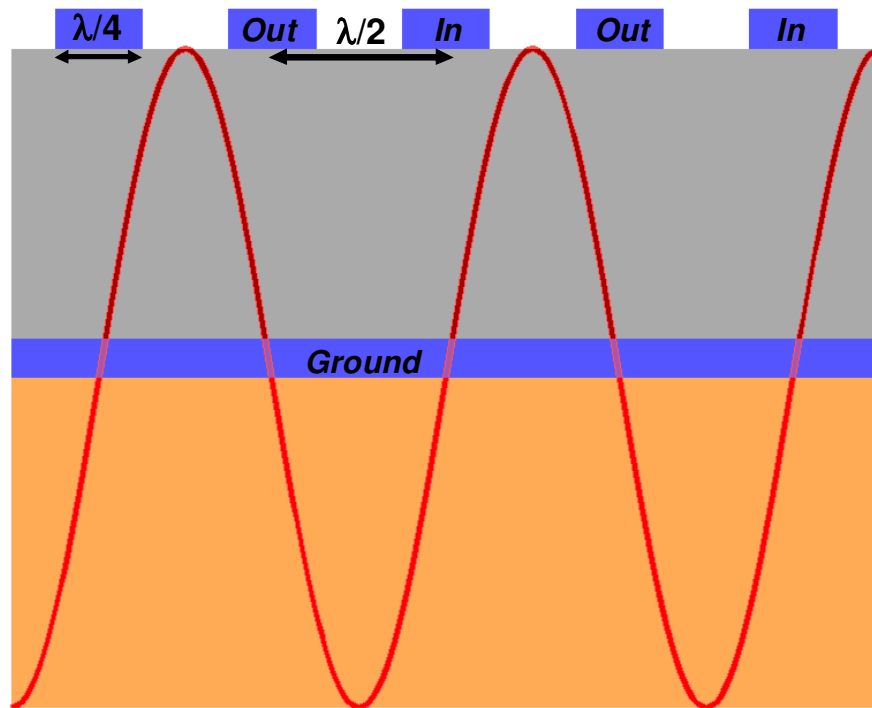


Wideband Measured Results





Filter Temperature Stability and Compensation



Resonator Cross-section

$$f_0 \approx \sqrt{\frac{E}{\rho}}$$

$$E_{TOTAL} = \frac{(E_{AlN}t_{AlN} + E_{oxide}t_{oxide})}{t_{AlN} + t_{oxide}}$$

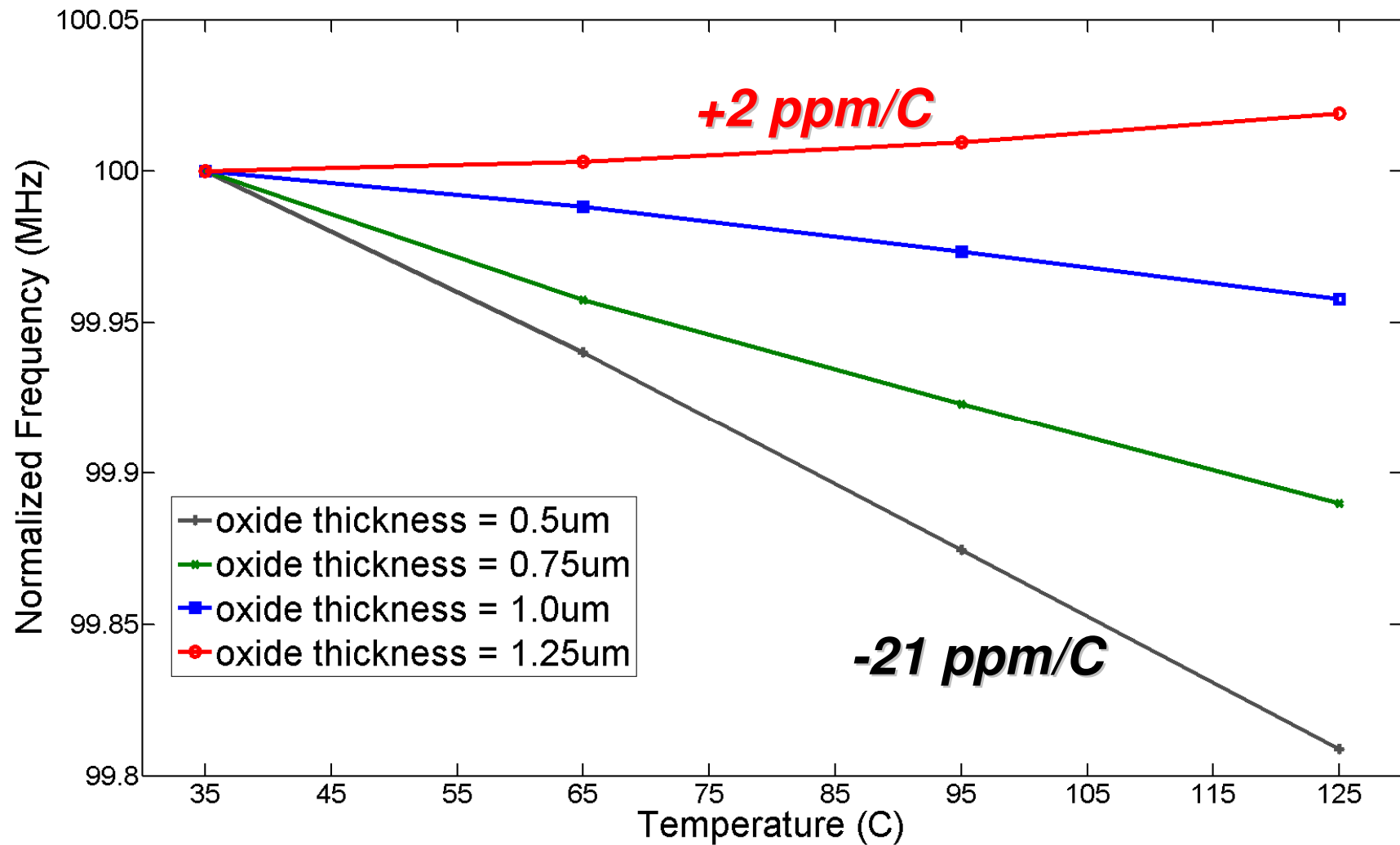
$$\rho_{TOTAL} = \frac{(\rho_{AlN}t_{AlN} + \rho_{oxide}t_{oxide})}{t_{AlN} + t_{oxide}}$$

$$E_{AlN} \approx -65 ppm/K$$

$$E_{oxide} \approx +185 ppm/K$$



Temperature Stability vs. Oxide Thickness





Temperature Compensation Limits

AlN Thickness Control

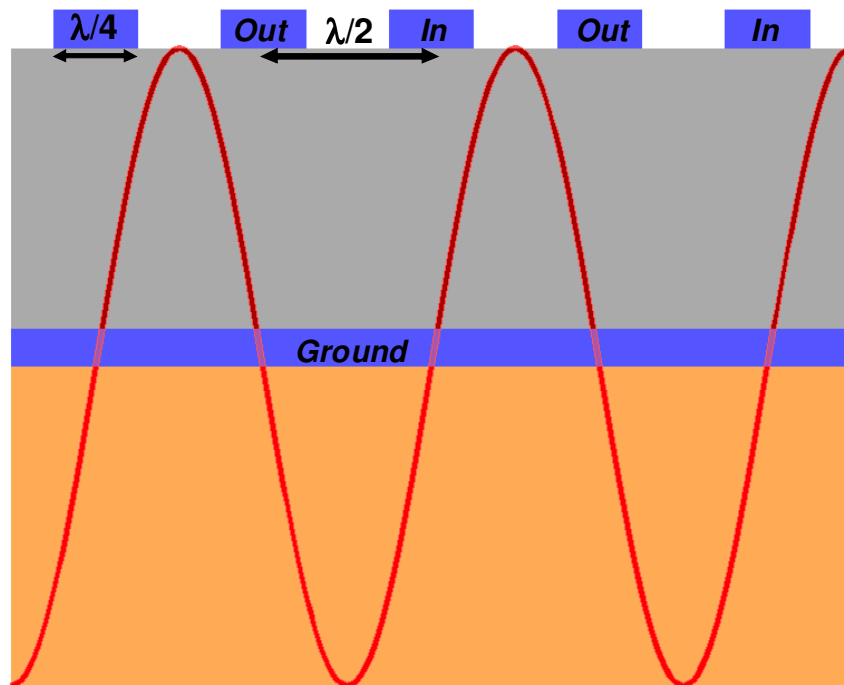
➤ Wafer to Wafer

$$\sigma_{thickness}(AlN) = 0.2\%$$

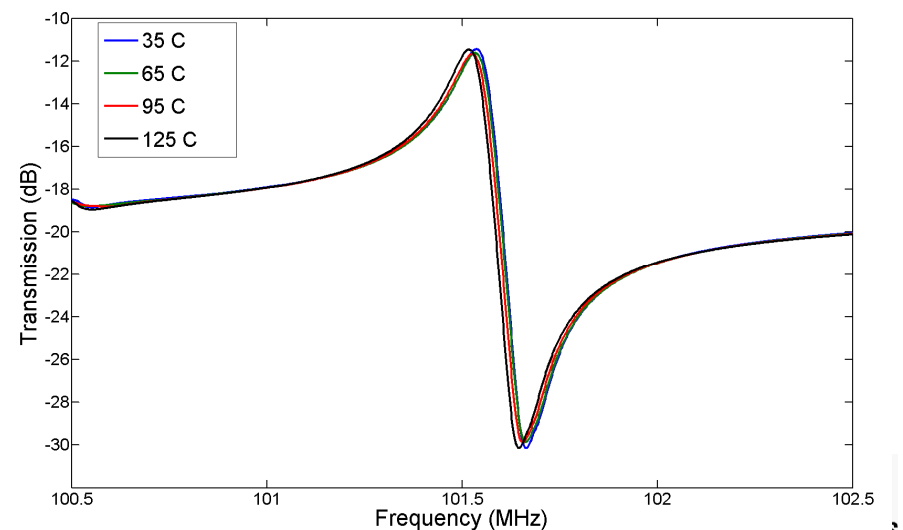
➤ Within Wafer

$$\sigma_{thickness}(AlN) < 1\%$$

❖ $\pm 26 \text{ ppm across } -55 \text{ to } 125 \text{ C}$

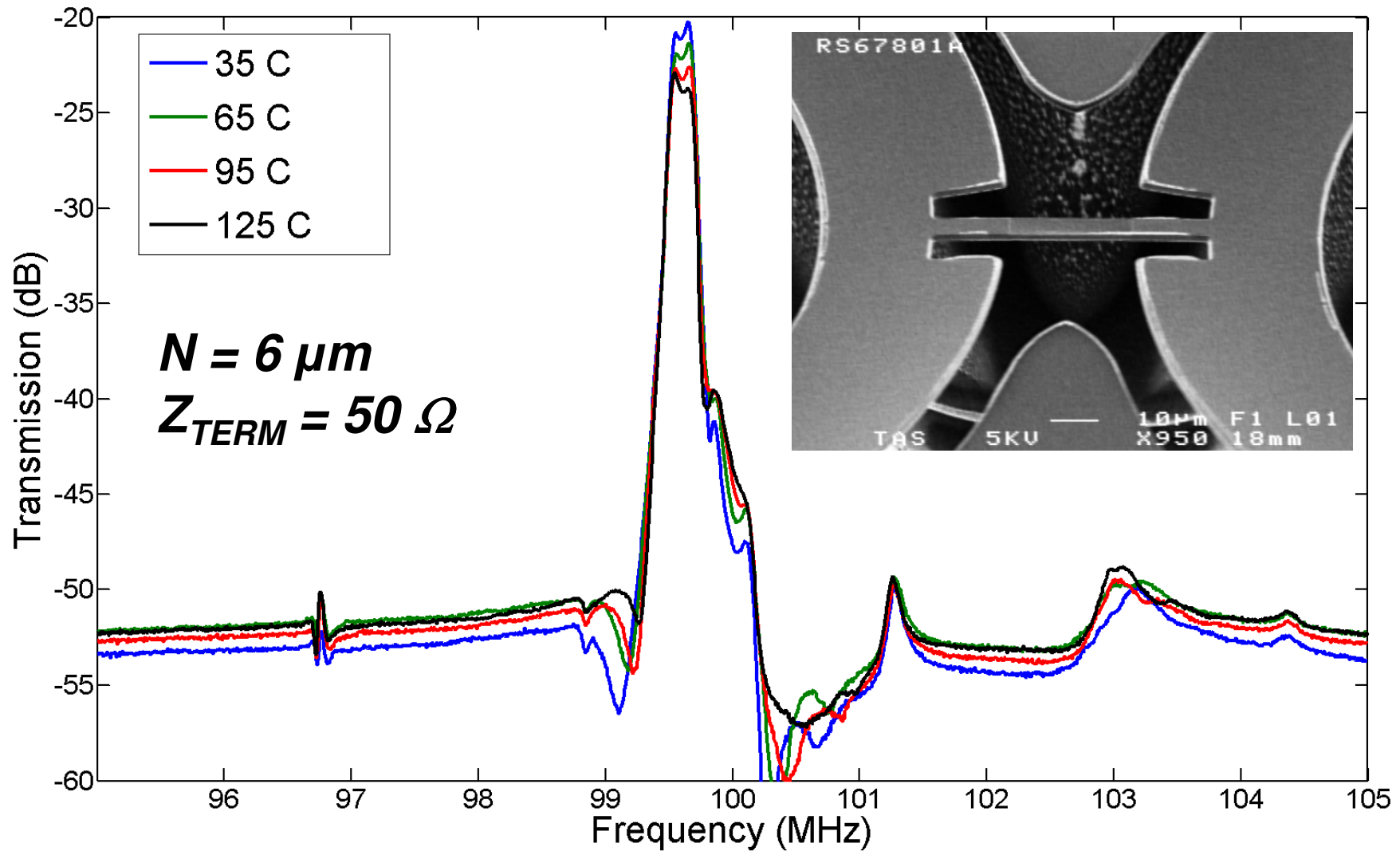


Resonator Cross-section



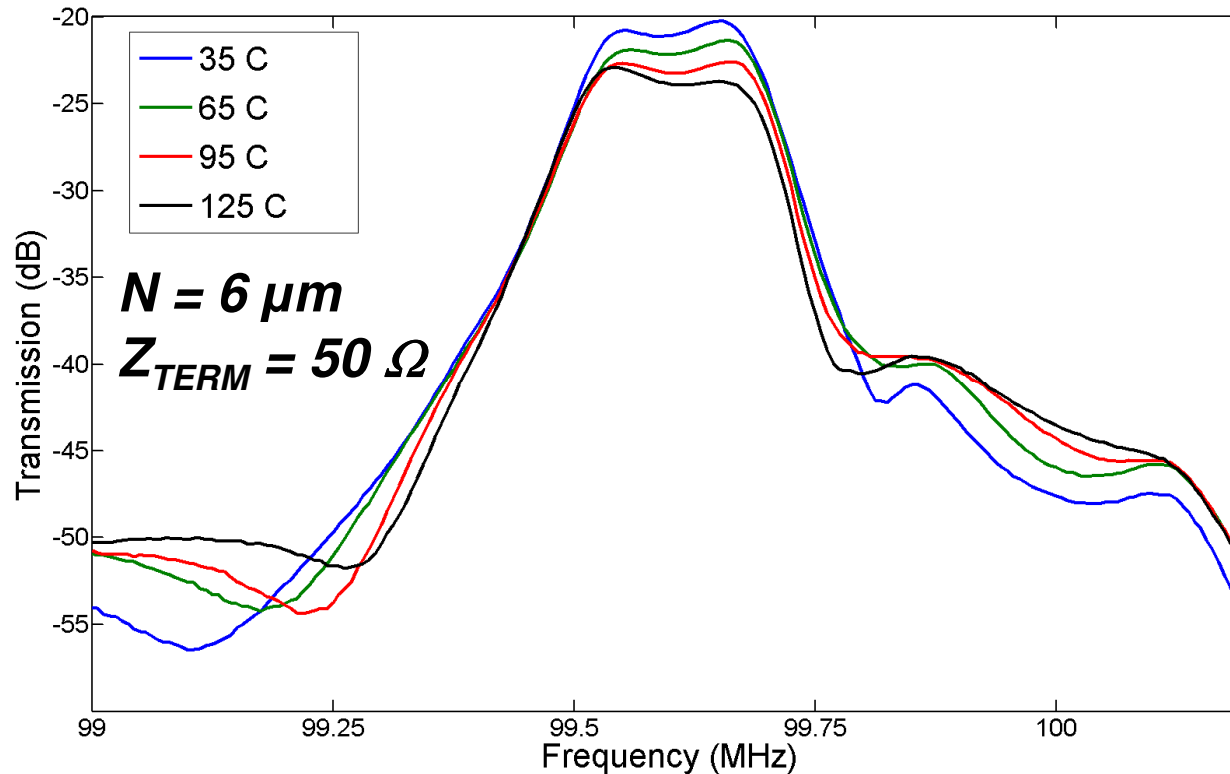


Temperature Stability Filter Impact





Temperature Stability Filter Impact



**Useable 3dB
Bandwidth (35-125 C)
= 181 kHz**

**Max. 3dB Bandwidth
(35-125 C) = 194 kHz**

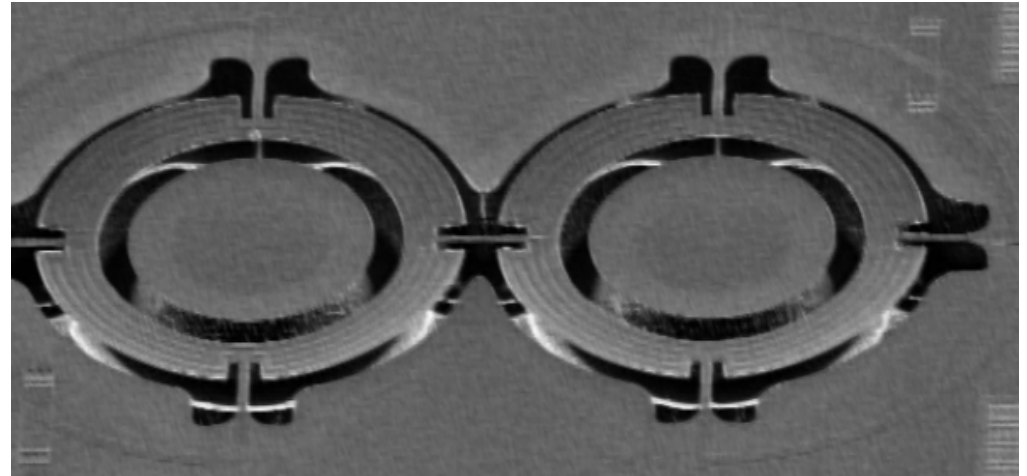
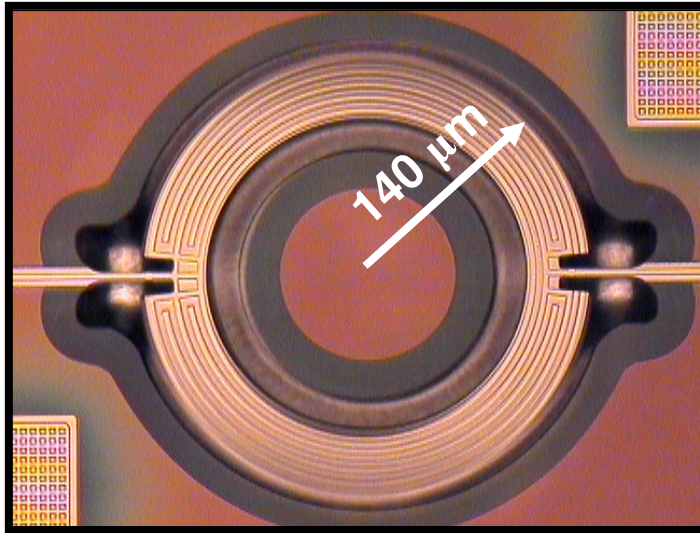
**% Useable Bandwidth
(35-125 C) = 93.3%**

**6.7% Bandwidth
Dedicated to
Temperature Drift**

Oxide Thickness (μm)	$f(-3\text{db})$ min @35 C (MHz)	$f(-3\text{db})$ min @125 C (MHz)	$f(-3\text{db})$ min @35 C (MHz)	$f(-3\text{db})$ max @125 C (MHz)	Useable Band-width
0.5	106.900	106.69796	107.0875	106.8851	0 kHz
1.1	99.5125	99.5000	99.69375	99.69375	181.25 kHz

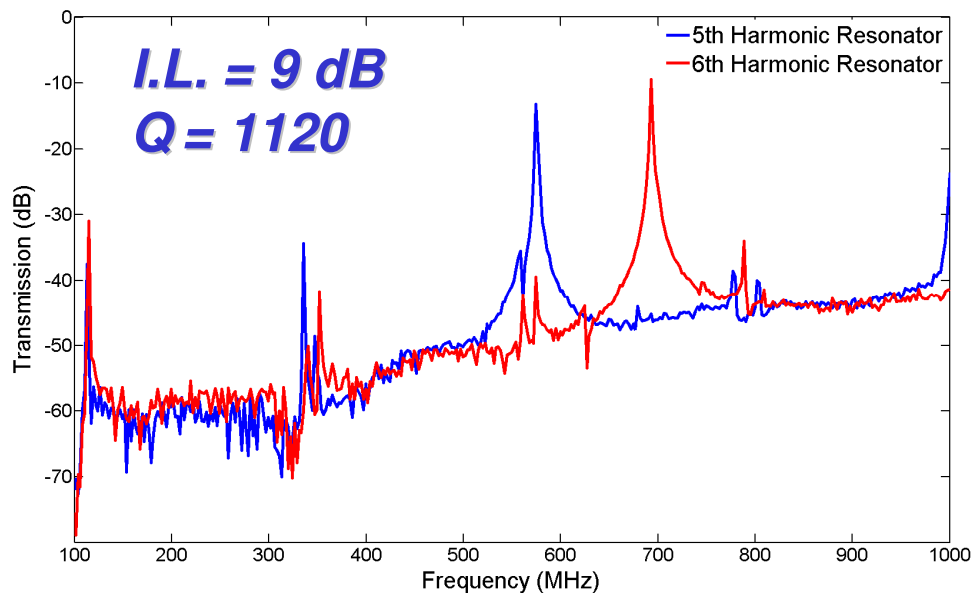


Scaling to Higher Frequency (Overtone Operation)



• Overtone MEMS Filters

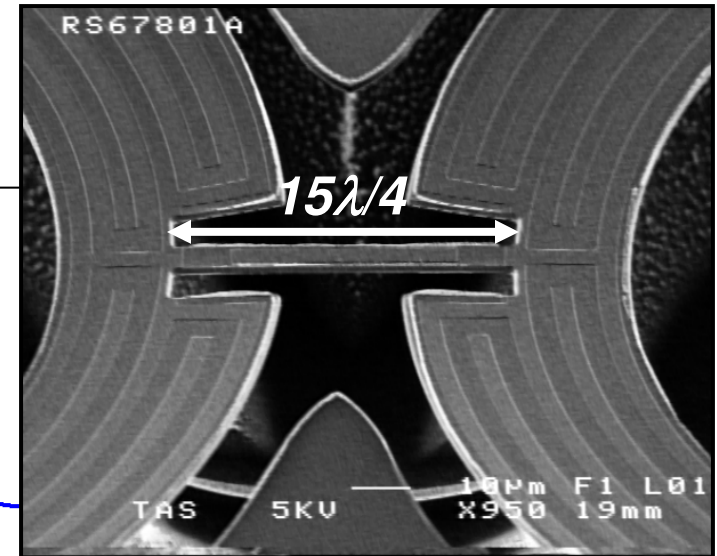
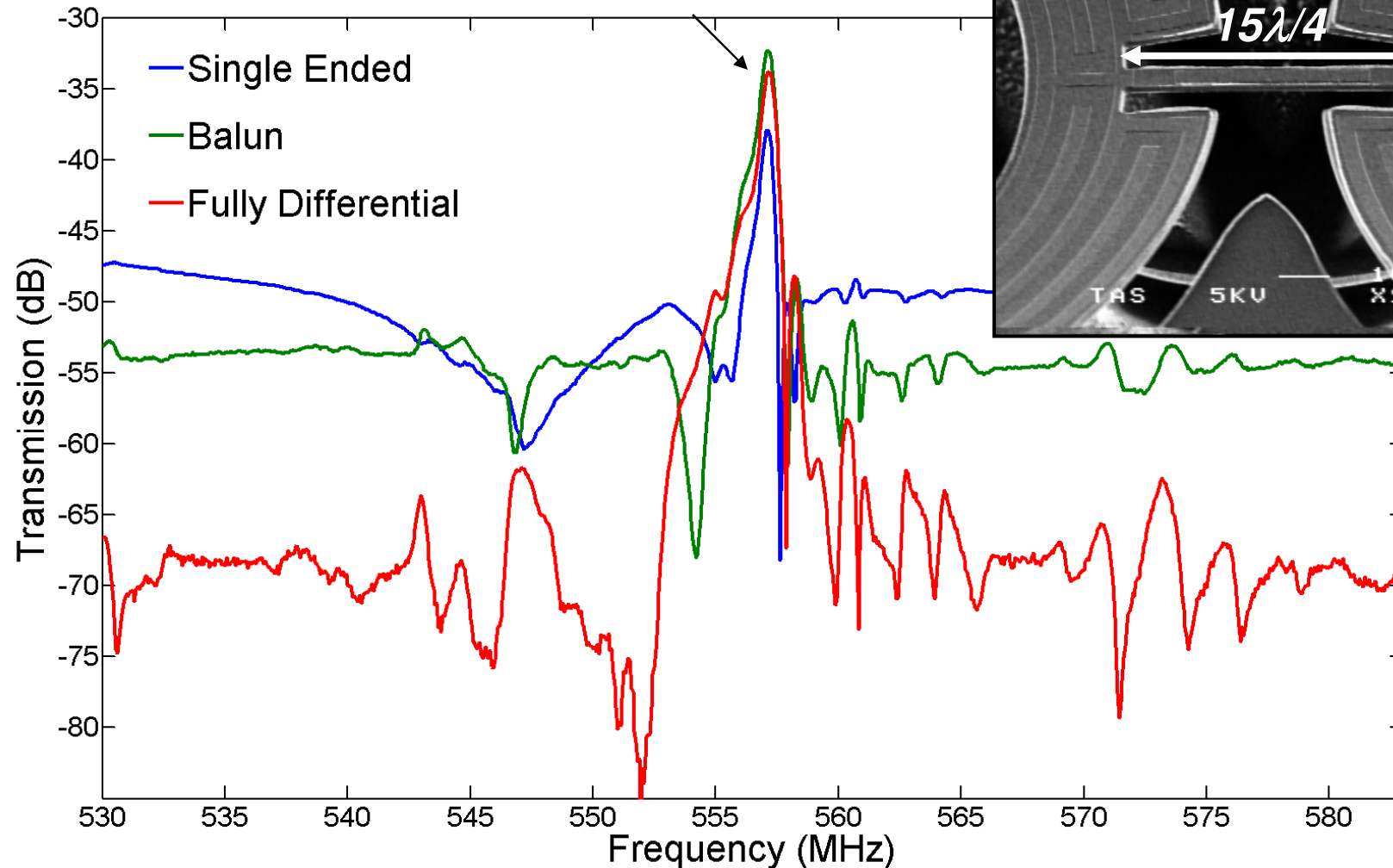
- *Previously scaled resonators to 1 GHz with low insertion loss*
- *Use overtone operation to scale mechanically coupled filters*
- *Allows balun and fully differential operation for improved out-of-band rejection*





5th Overtone Filter Measured Results

**Fully Differential Operation Improves
Stop-Band Rejection by 25 dB**
**Higher Than Expected
Insertion Loss Based
on Previous Results**





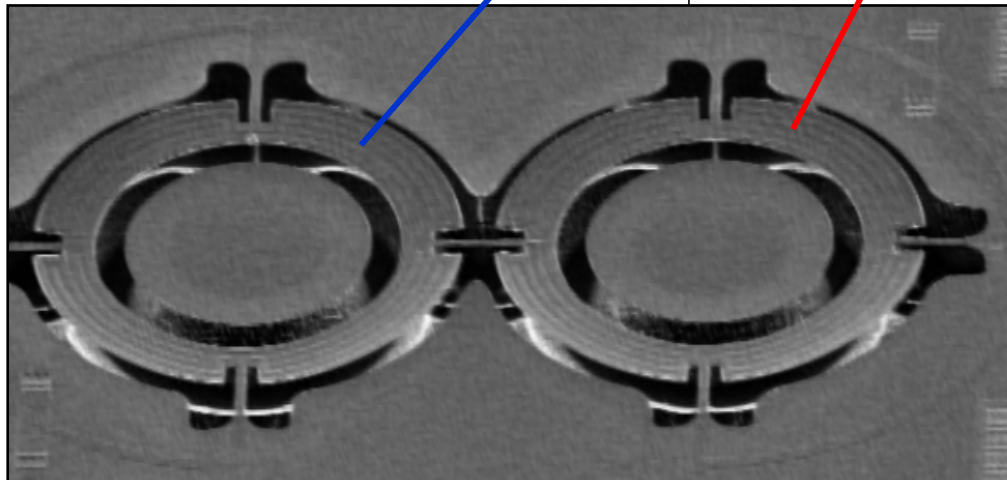
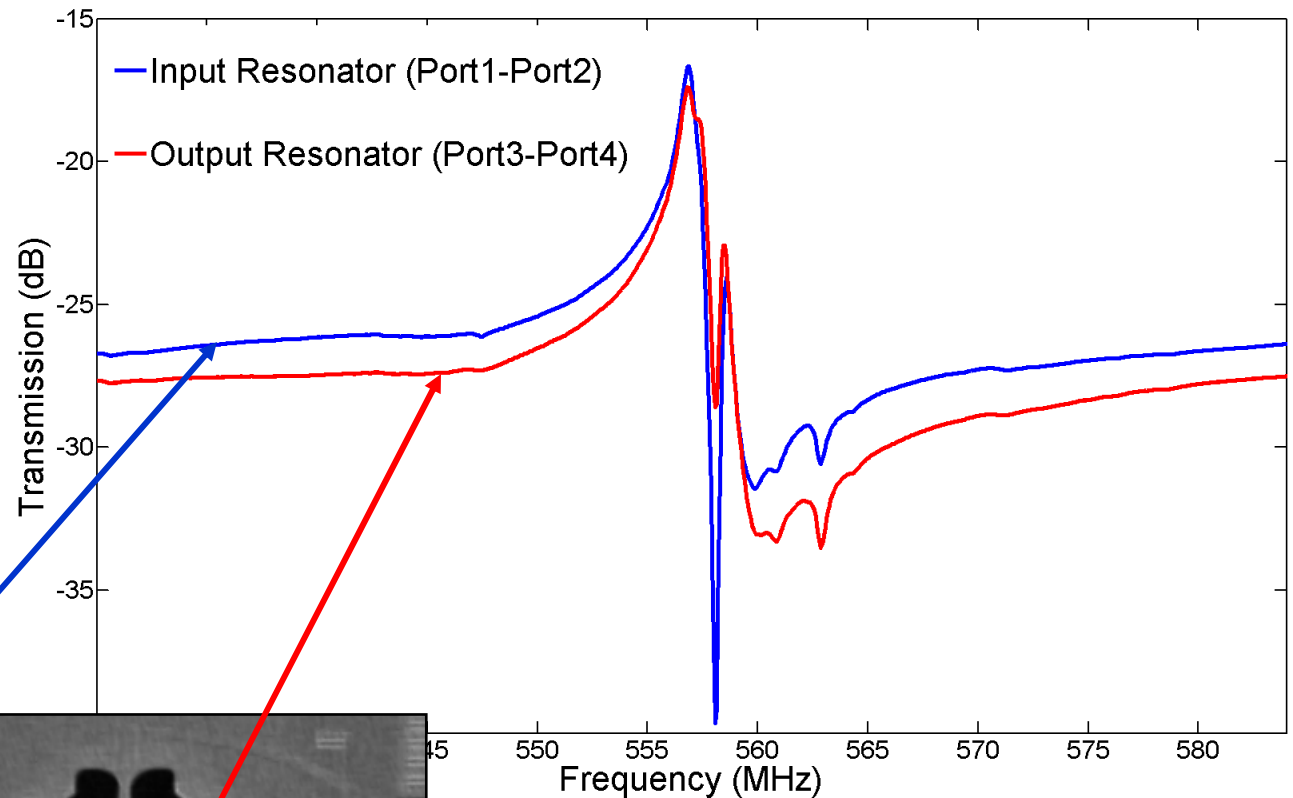
Overtone Filter Discussion

- Filter Insertion Loss

- *Input/Output Resonators Show Strong Coupling and Matched Frequencies*

- $Q_{Filter} = 1000$
but

- $Q_{Resonator} = 495$



- ❖ *Degraded resonator Q from additional anchors*
- ❖ *Coupling occurs only over 1/5th of low velocity coupling locations*



Conclusions

➤ MEMS Filter Motivation

- *Small Size, Strong Coupling per Area*
- *Many Frequencies per Wafer*
- *Narrow Band Operation*
- *Filter Banks for Spectrum Analysis and Cognitive Radio*

➤ VHF Mechanically Coupled Filters

- *Filter Architecture and Design*
- *Bandwidth Control*
- *Temperature Drift Reduced for Narrow Bandwidth Filters*

➤ UHF Overtone Mechanically Coupled Filters

- *Filter Topology Scaled to 550 MHz*
- *Unexpected Insertion Loss*
 - Resonator Q degraded by additional anchors (anchor loss limited)
- *Additional Work Needed to Evaluate Overtone Mechanical Coupling Efficiency*

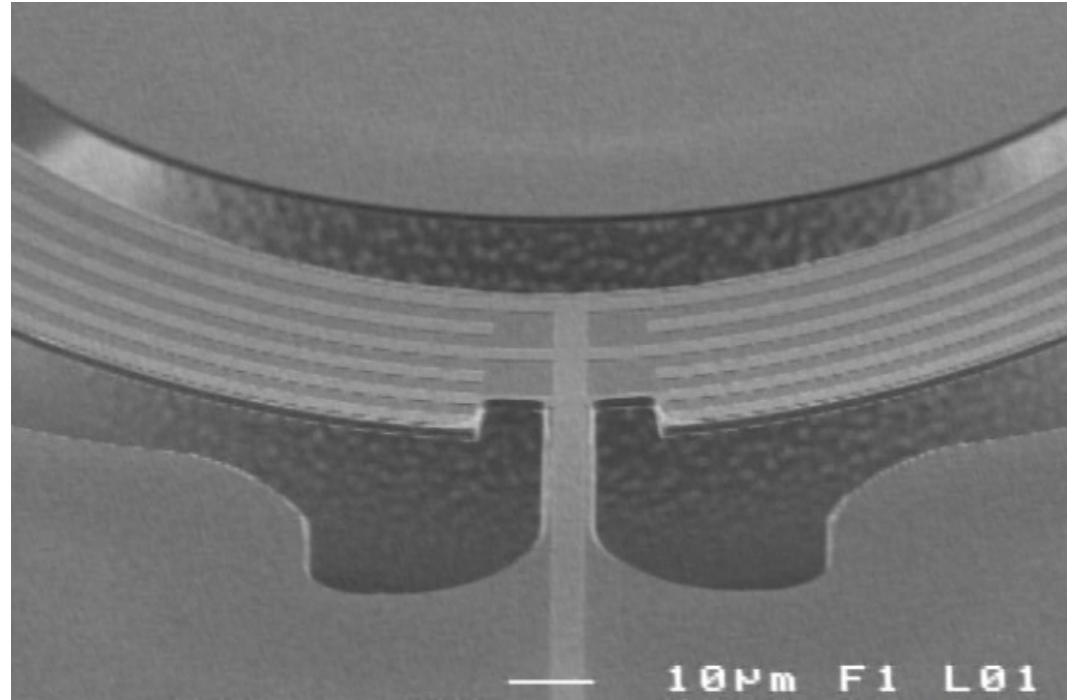


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Contact Information

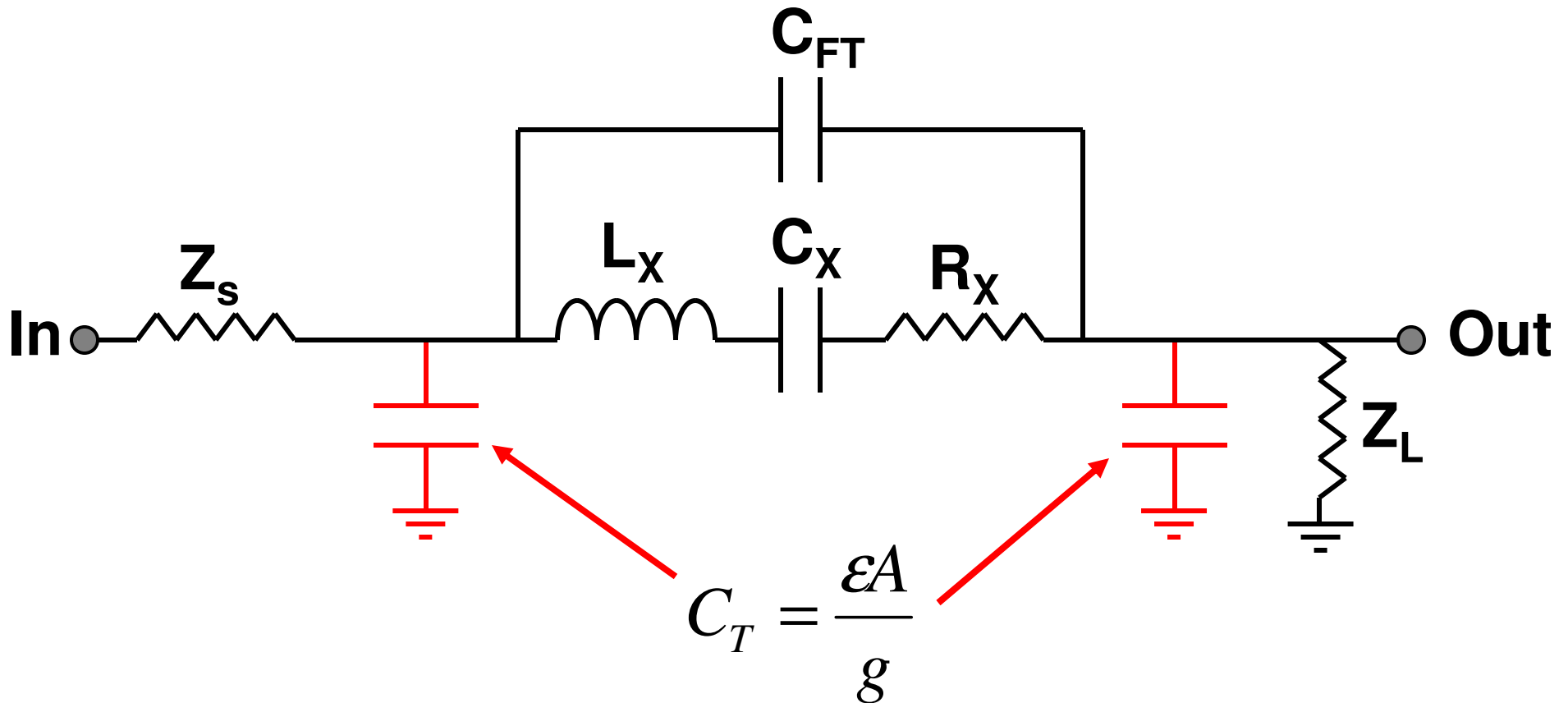
Roy Olsson (rholsso@sandia.gov)



Backup Slides



Transducer Capacitance



In most capacitively transduced devices,

$Z(C_T) \ll R_x$ above a few 100 MHz

$$R_x = \frac{Z(C_T) k_{\text{beam}}^4}{\omega_0 Q V_P^2 (\epsilon A)^2}$$

Increase Overlap Area,
Dielectric