



# ***VHF and UHF Mechanically Coupled AlN MEMS Filters***

***Roy H. Olsson III, Cody Washburn, James E.  
Stevens, Melanie R. Tuck and Christopher  
Nordquist***

**Sandia National Laboratories, Albuquerque NM**



# Outline

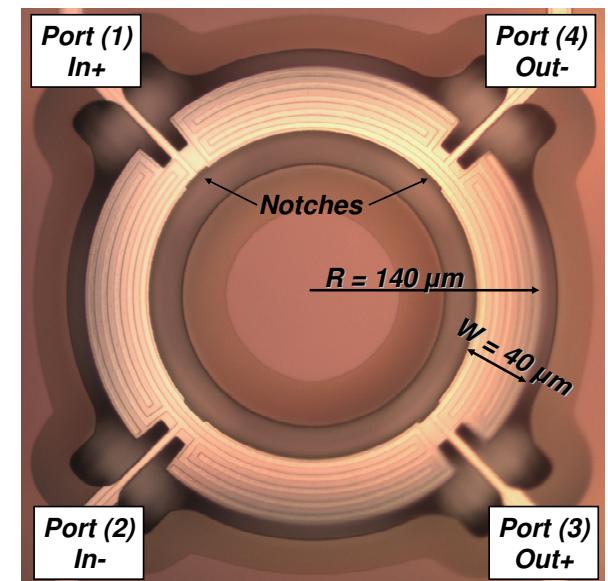
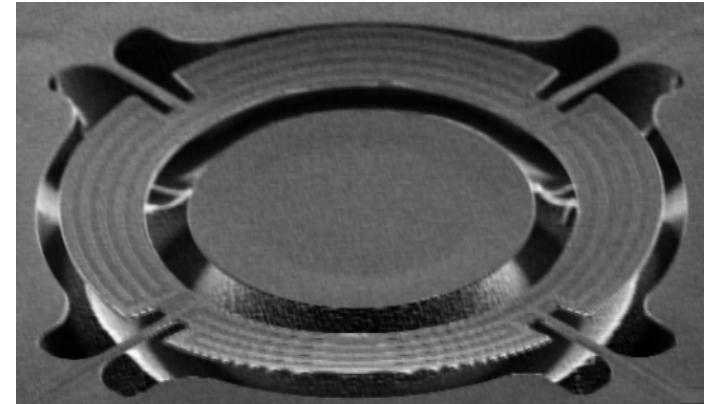
---

- Background and Motivation
  - *MEMS Filter Motivation*
  - *Mechanically Coupled Filter Architecture*
  - *Low Impedance Piezoelectric Transduction*
- VHF Mechanically Coupled Ring Resonator Filters
  - *100 MHz Mechanically Coupled Filter Measurements*
  - *Filter Temperature Sensitivity and Compensation*
- UHF Overtone Mechanically Coupled Ring Resonator Filters
  - *Filter Design and Measured Results*
  - *Performance Discussion*
- Conclusions and Acknowledgements



# Piezoelectric MEMS Filter Research

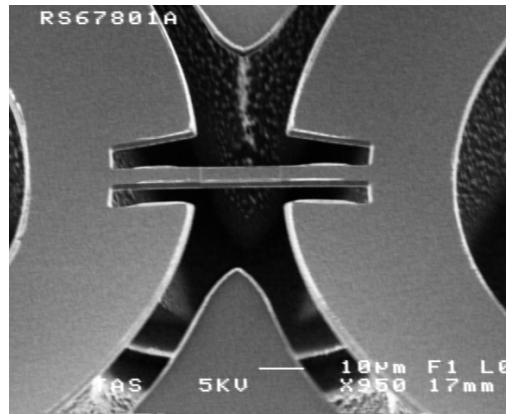
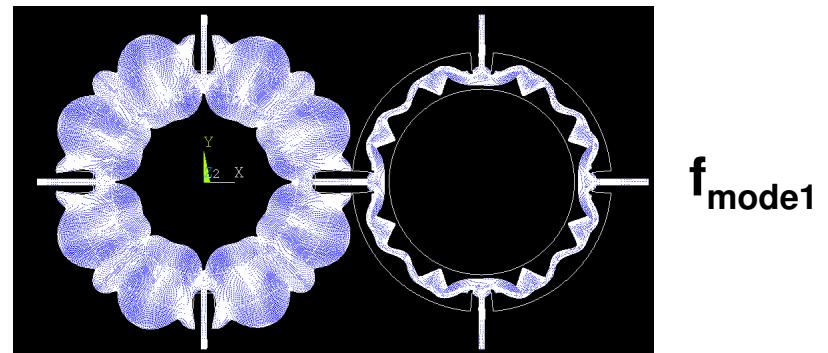
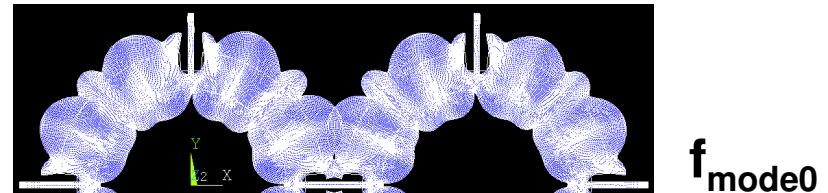
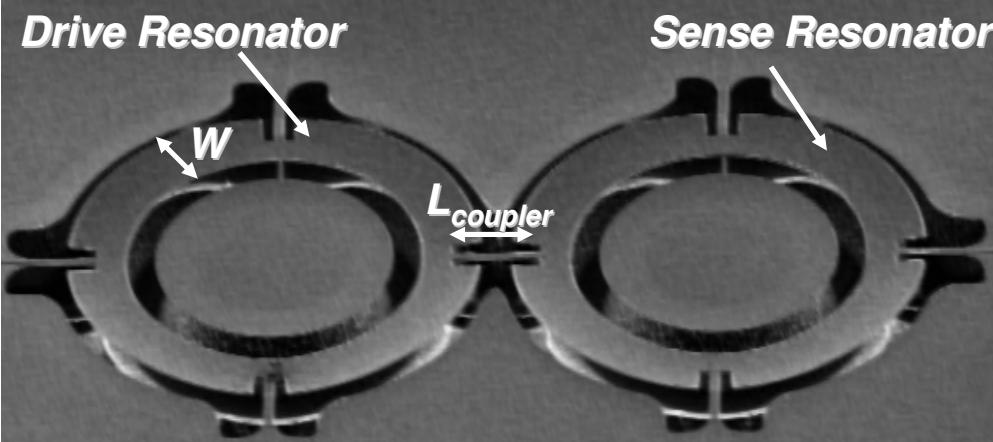
- MEMS Filters
  - *Small*
  - *Many Frequencies on a Single Chip*
  - *Greater Coupling per Area for the VHF and a Portion of the UHF Band*
- Miniature High-Selectivity Filters and Filter Banks not Available in Commodity Driven Wireless Market
  - *RF Filters in Non-Commercial Bands*
  - *Miniature SAW IF Filter Replacement*
  - ***Filter Banks for Spectrum Analysis and Cognitive Radios***
    - Electrically Coupled Filters
    - Dual Mode Filters
    - **Mechanically Coupled Filters**



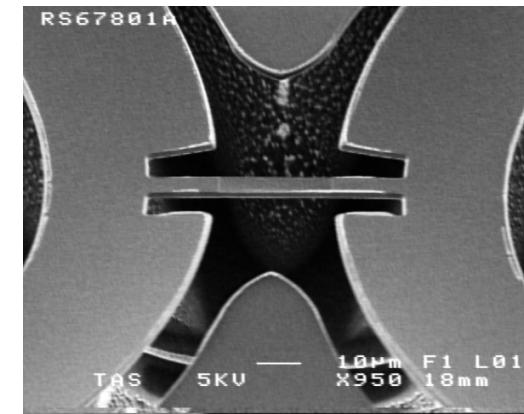
5<sup>th</sup> Overtone Dual Mode Filter Images



# Filter Architecture and Design



Narrowest  
Bandwidth when  
Coupled at Ring  
Center



Increase  
Bandwidth by  
Moving to Higher  
Velocity Coupling

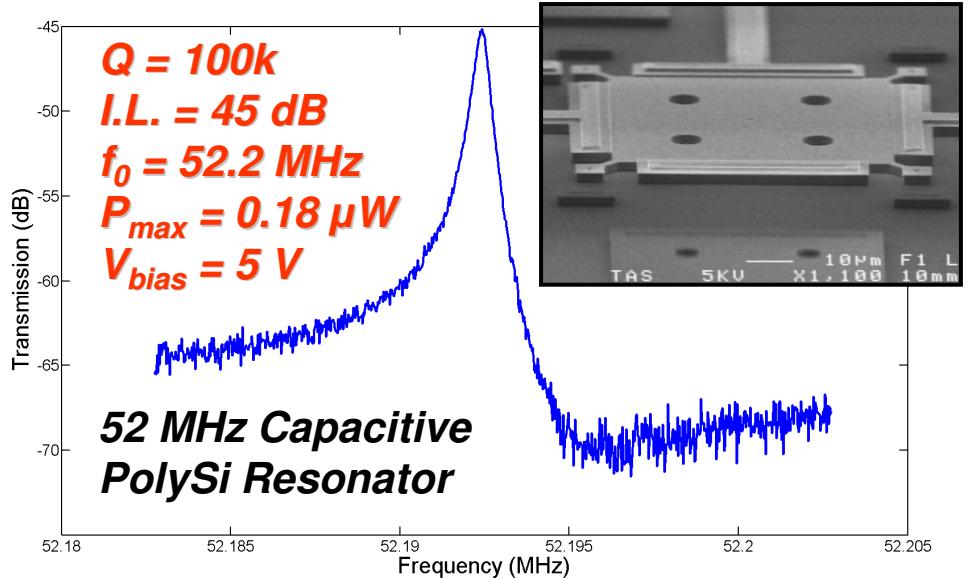
**Narrow Bandwidth MEMS  
Filter Architecture 1<sup>st</sup>  
Reported in PolySi by Li et al,  
Ultrasonics Symposium 2005**



# Piezoelectric Transduction

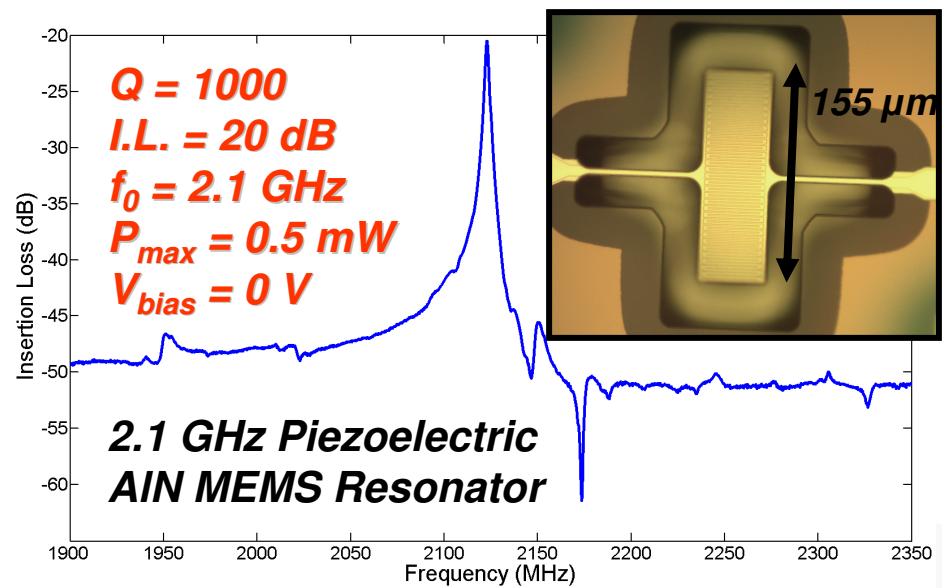
## • Capacitive Resonators

- High Impedance ( $20 \text{ k}\Omega$ )
- High-Q (100k)
- Force  $\approx V^2$
- Low Power Handling ( $0.2 \mu\text{W}$ )
- PolySi not Post-CMOS Compatible (High Temp.)



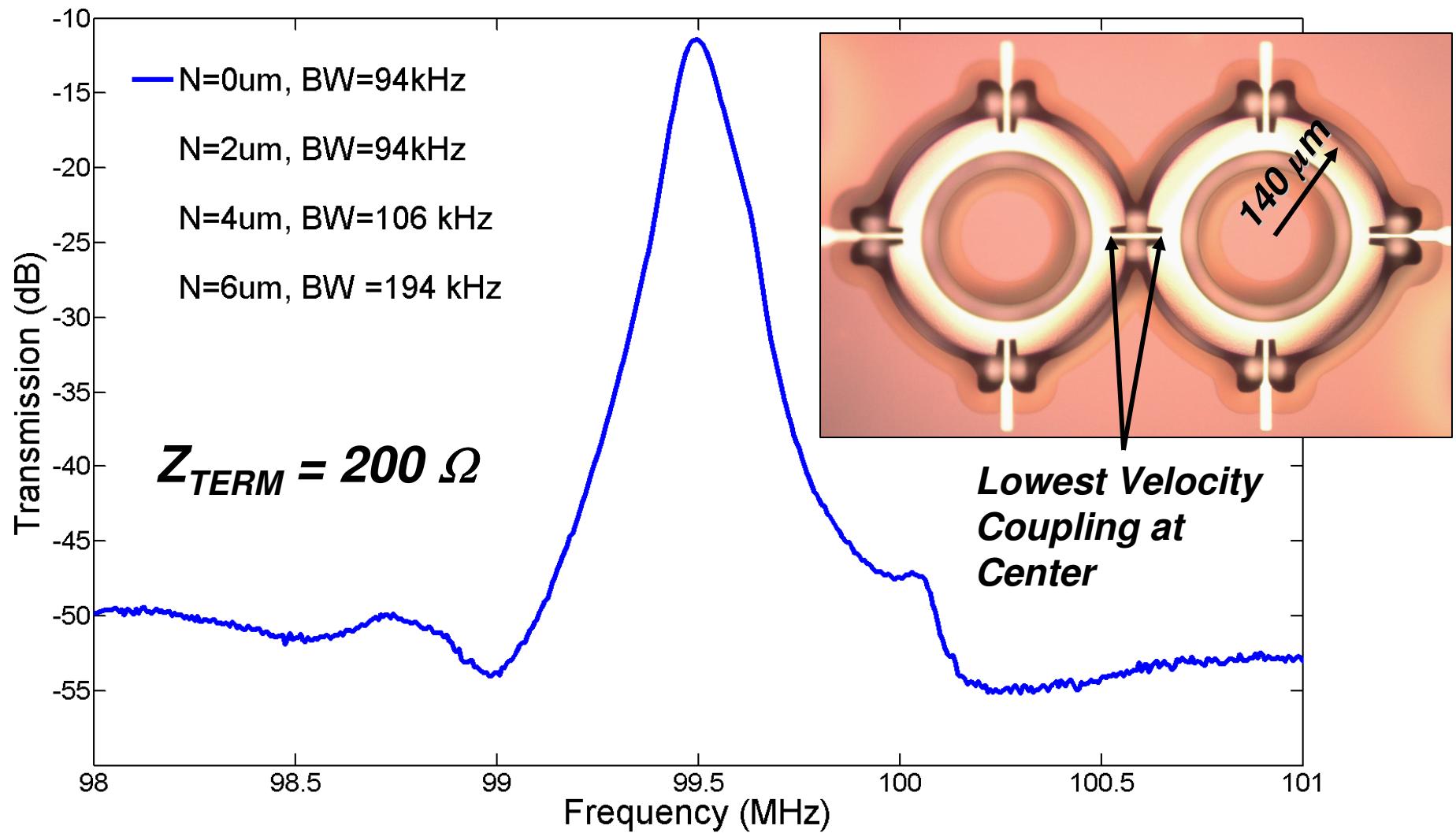
## • Piezoelectric Resonators

- Low Impedance ( $1 \text{ k}\Omega$ )
- Lower Q (1000)
- Force  $\approx V$
- High Power Handling ( $0.5 \text{ mW}$ )
- AlN Post-CMOS Compatible



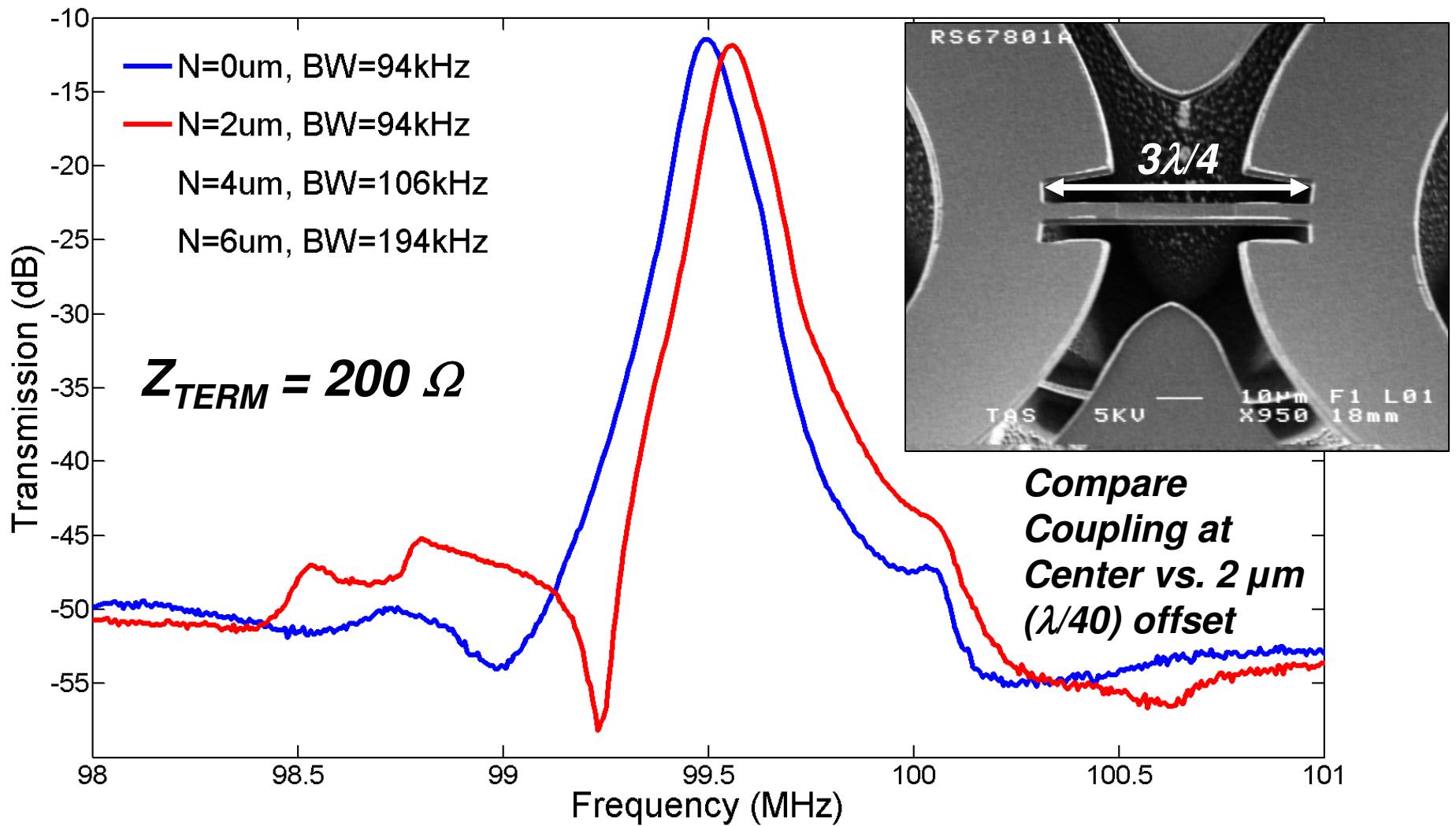


# Measured Results



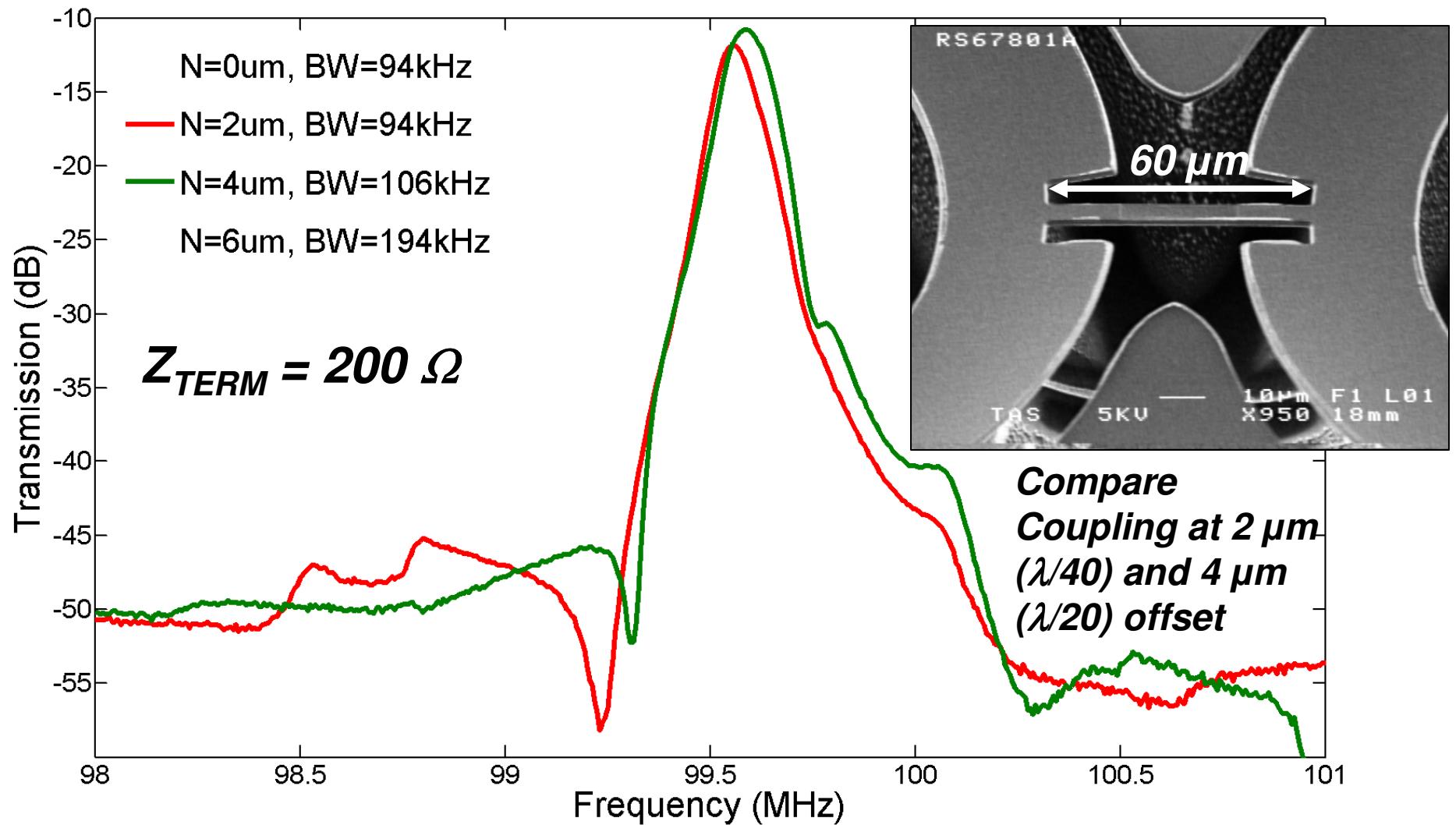


# Measured Results



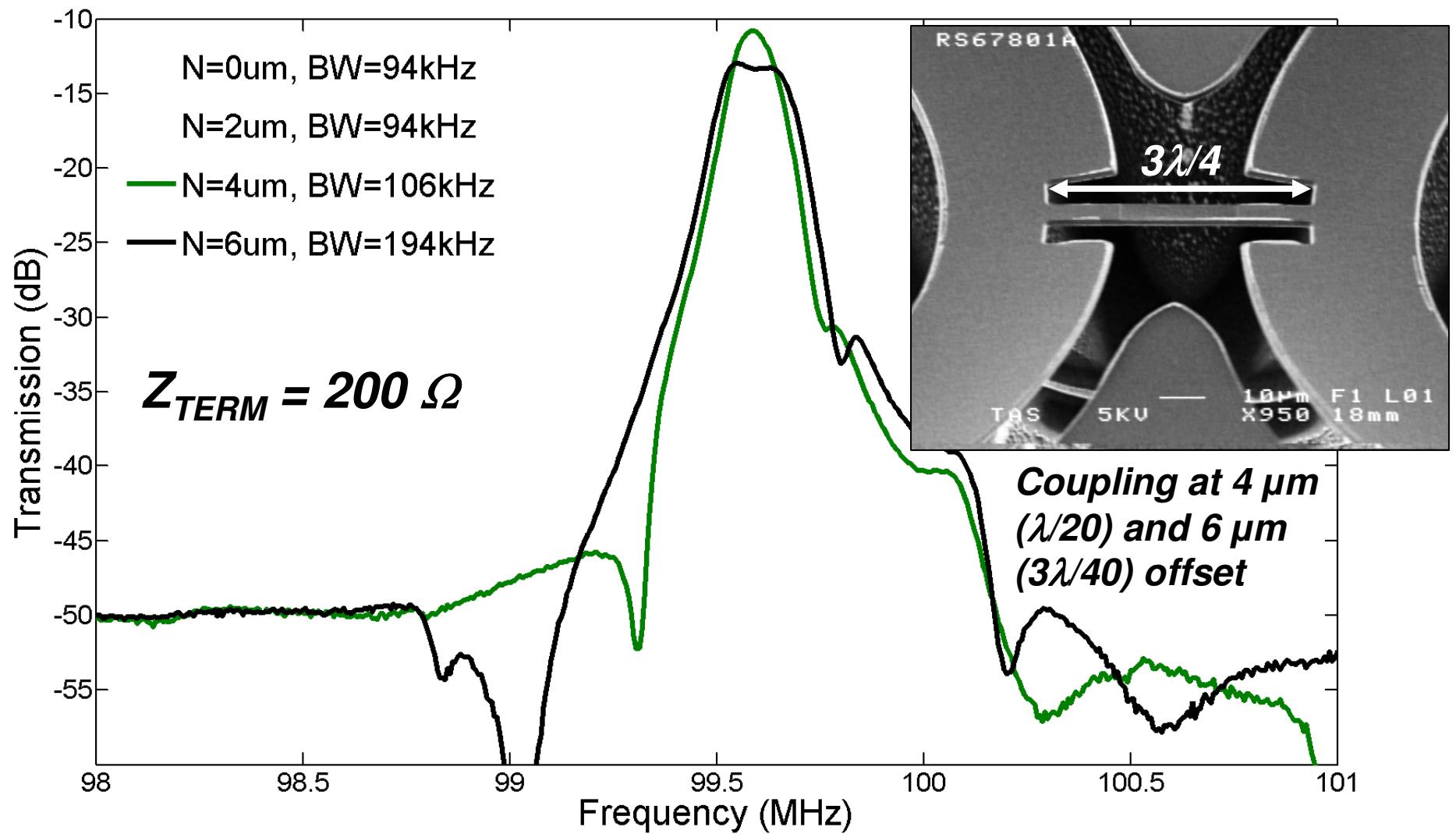


# Measured Results



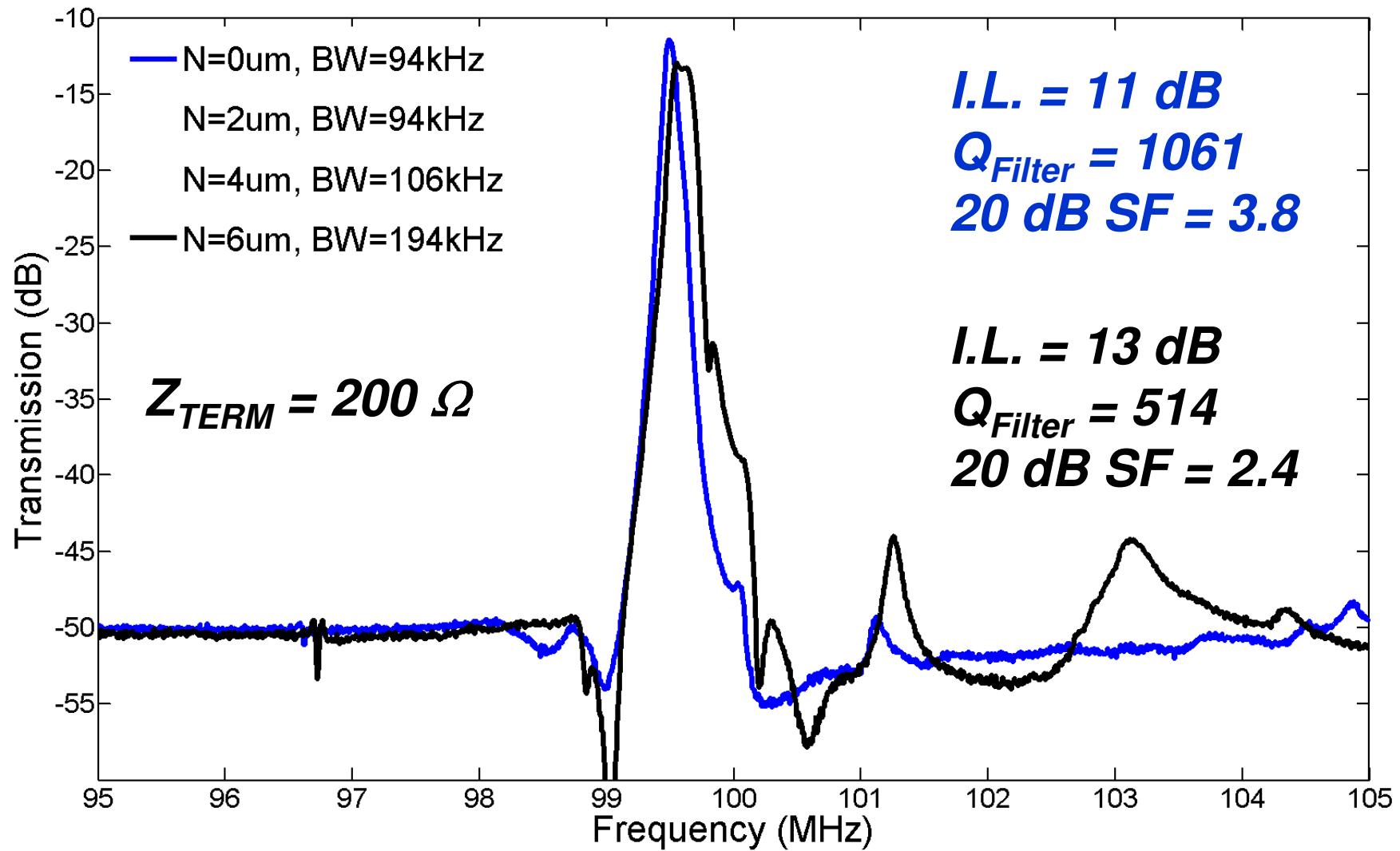


# Measured Results



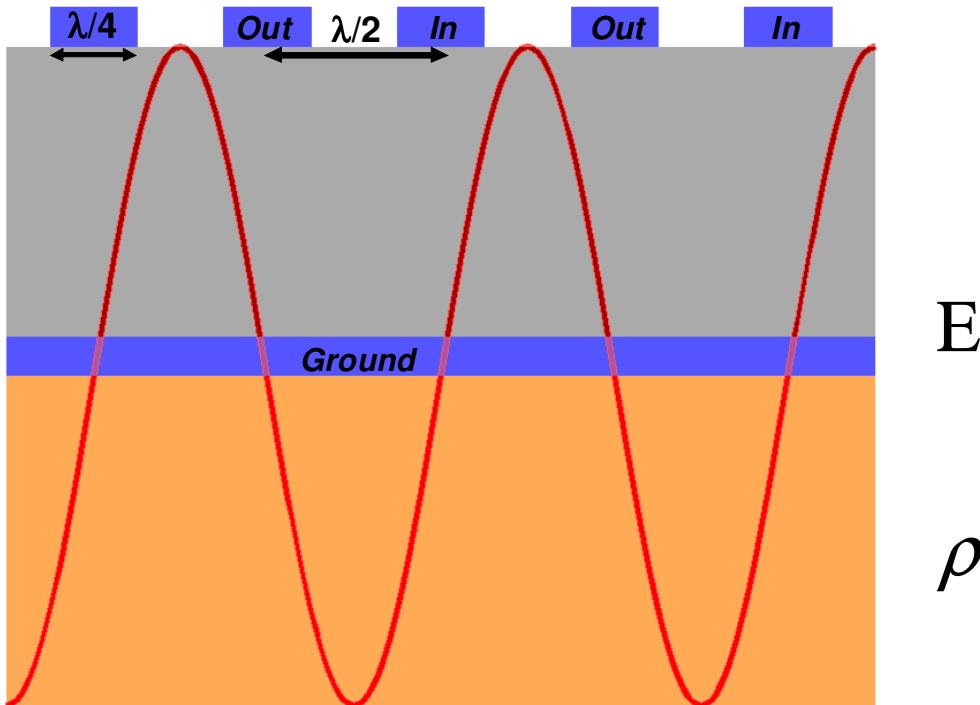


# Wideband Measured Results





# Filter Temperature Stability and Compensation



Metal Electrodes      Aluminum Nitride  
SiO<sub>2</sub> Temperature Compensation Layer      Acoustic Wave Propagation

Resonator Cross-section

$$f_0 \approx \sqrt{\frac{E}{\rho}}$$

$$E_{TOTAL} = \frac{(E_{AlN} t_{AlN} + E_{oxide} t_{oxide})}{t_{AlN} + t_{oxide}}$$

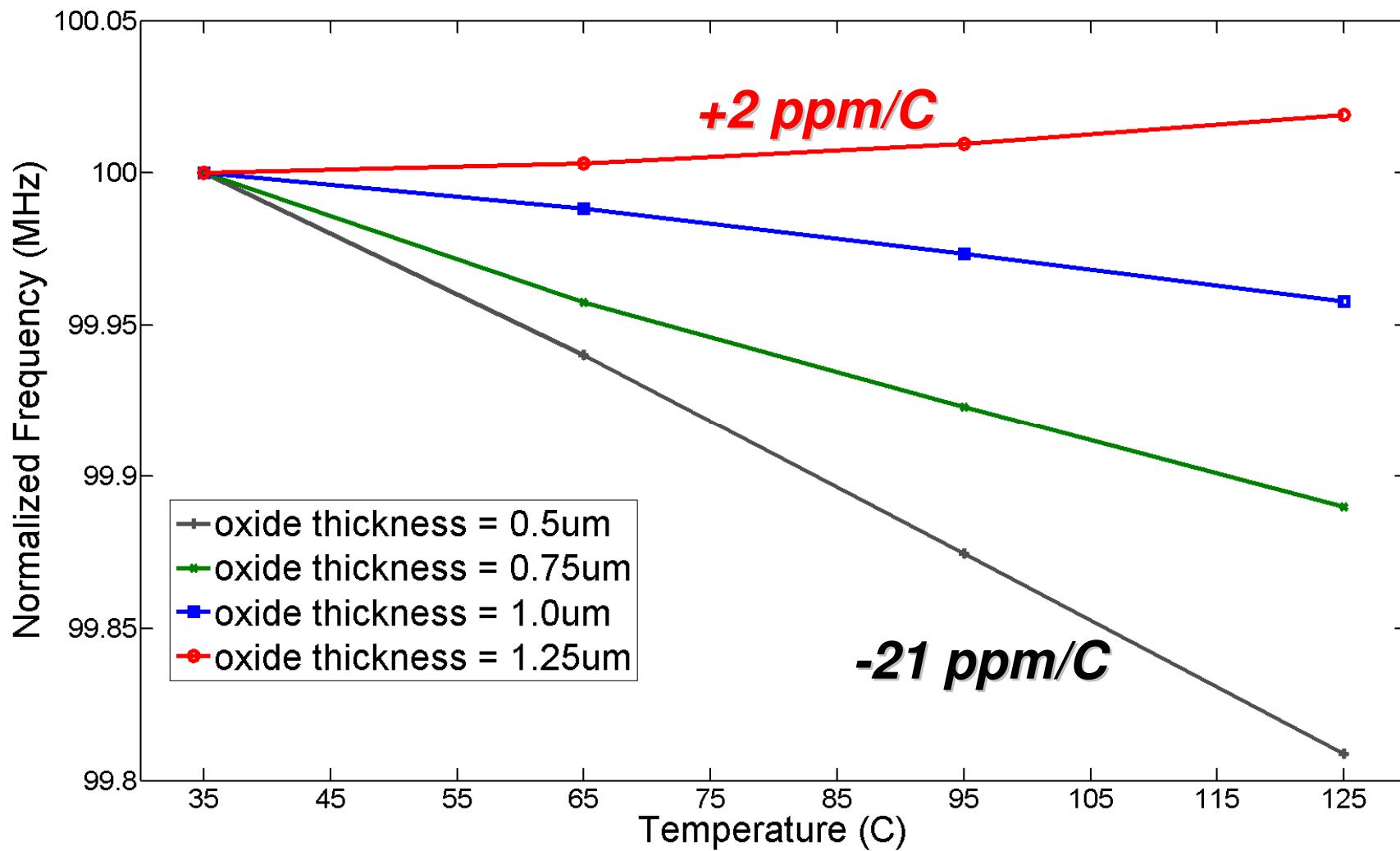
$$\rho_{TOTAL} = \frac{(\rho_{AlN} t_{AlN} + \rho_{oxide} t_{oxide})}{t_{AlN} + t_{oxide}}$$

$$E_{AlN} \approx -65 \text{ ppm/K}$$

$$E_{oxide} \approx +185 \text{ ppm/K}$$

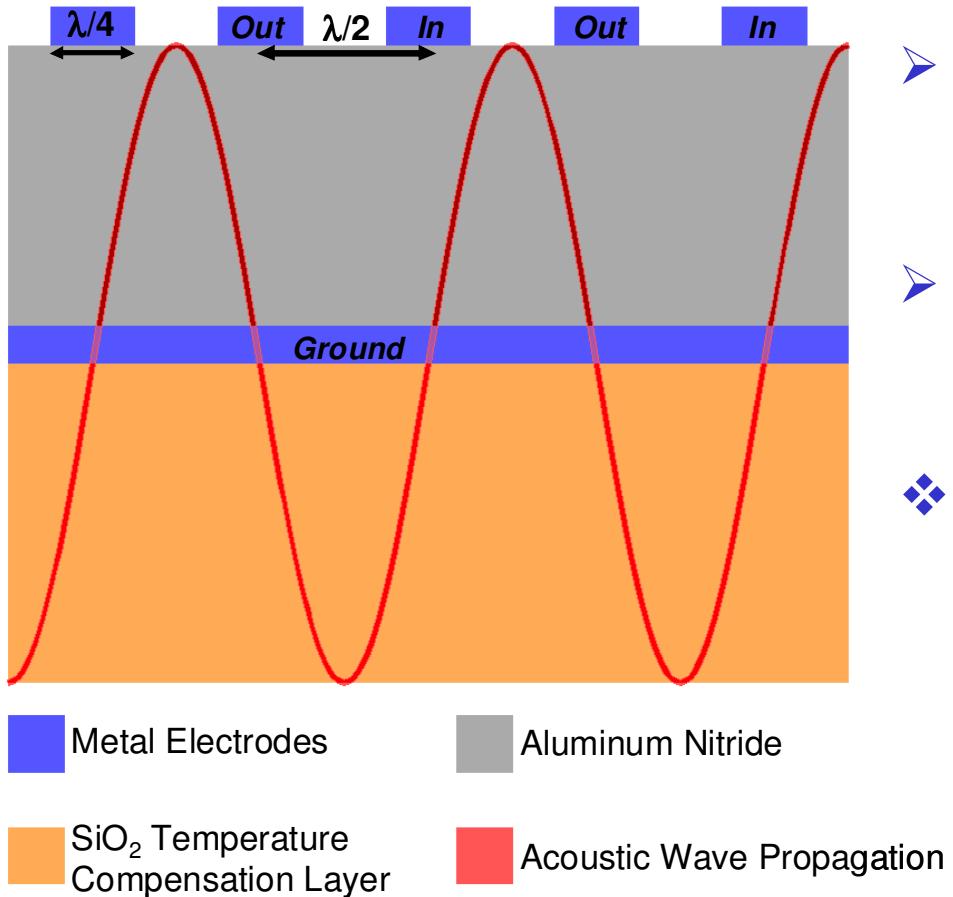


# Temperature Stability vs. Oxide Thickness





# Temperature Compensation Limits



Resonator Cross-section

## AlN Thickness Control

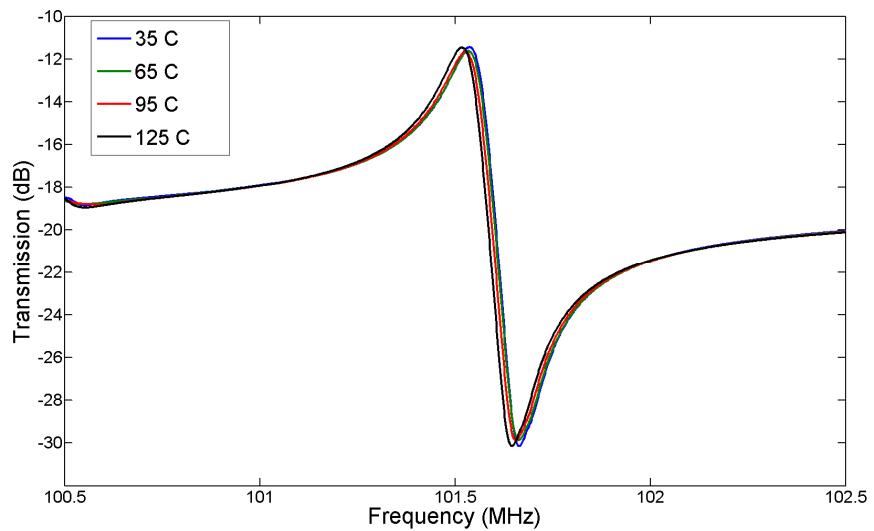
### ➤ Wafer to Wafer

$$\sigma_{\text{thickness}}(\text{AlN}) = 0.2\%$$

### ➤ Within Wafer

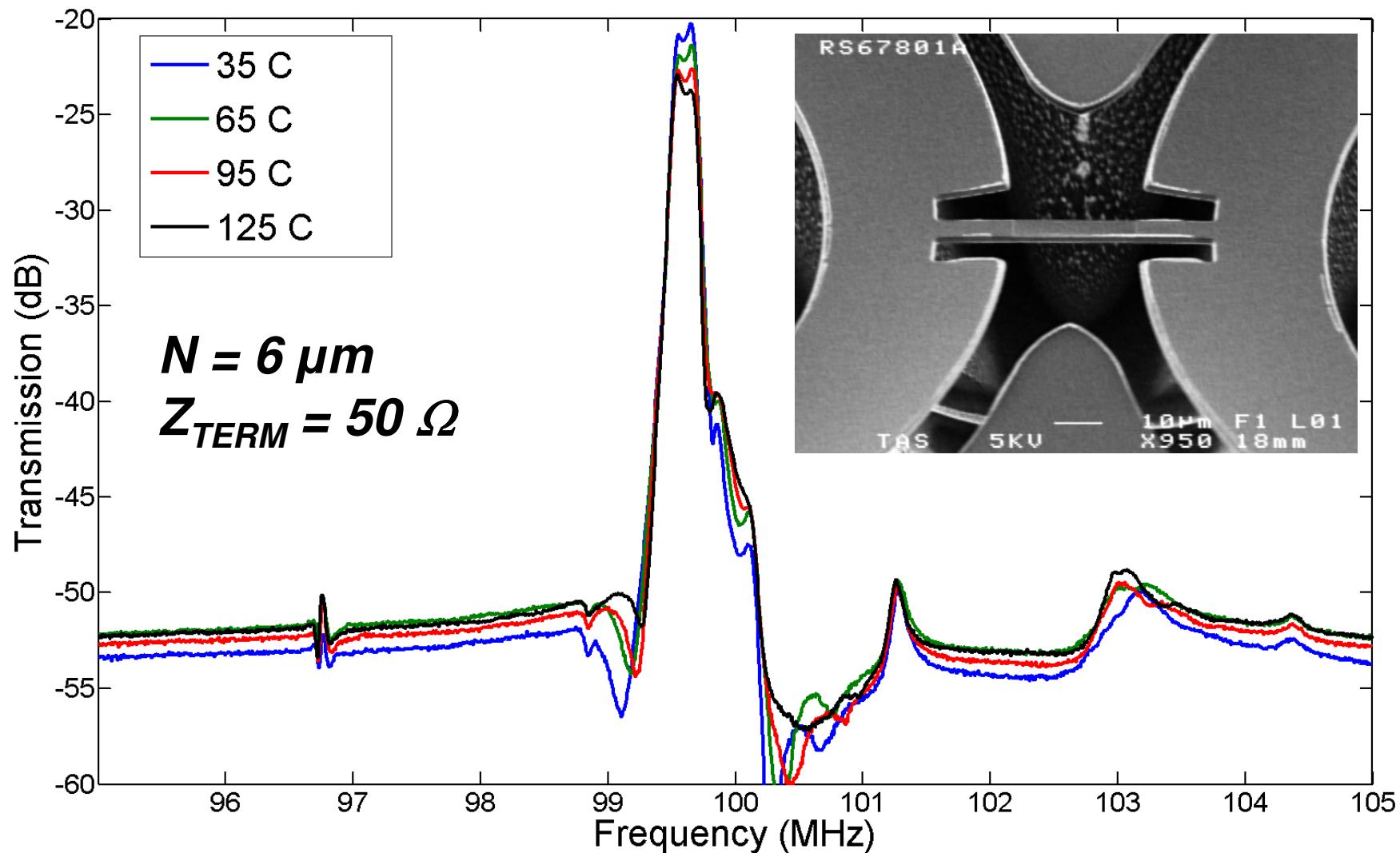
$$\sigma_{\text{thickness}}(\text{AlN}) < 1\%$$

❖ *± 26 ppm across -55 to 125 C*



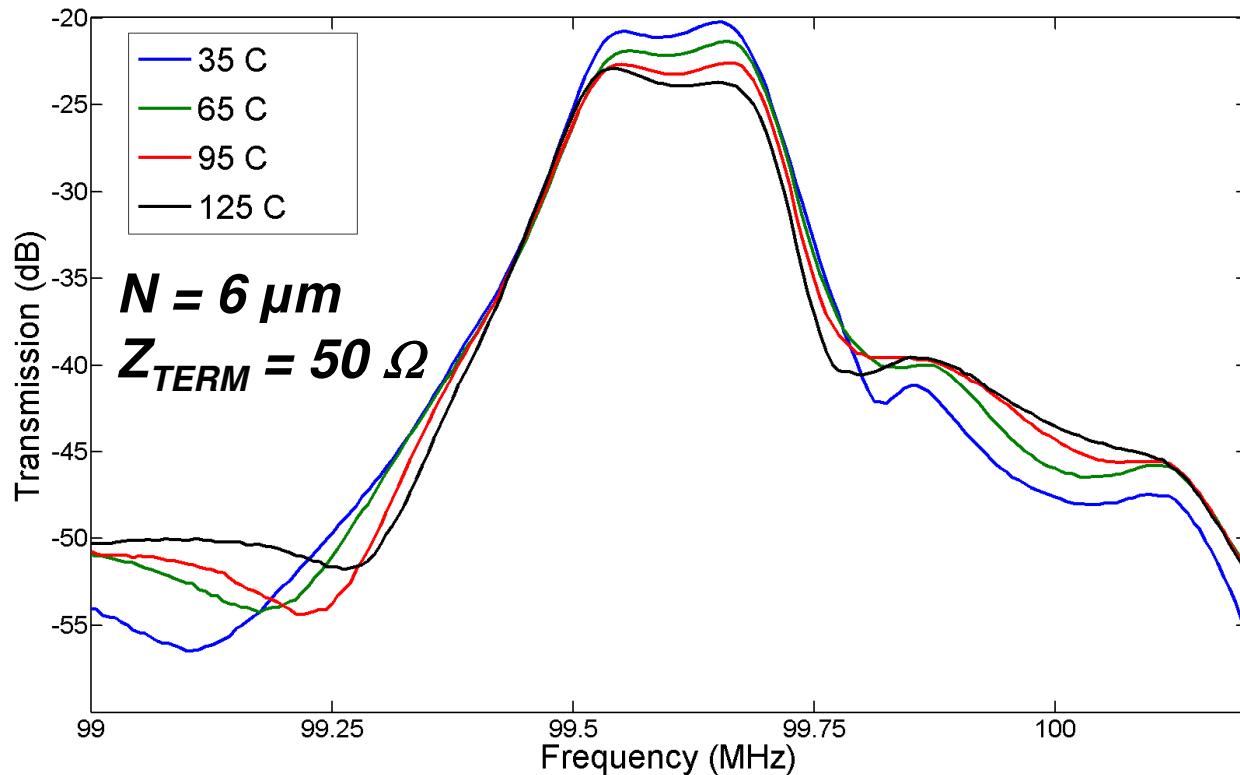


# Temperature Stability Filter Impact





# Temperature Stability Filter Impact



**Useable 3dB Bandwidth (35-125 C) = 181 kHz**

**Max. 3dB Bandwidth (35-125 C) = 194 kHz**

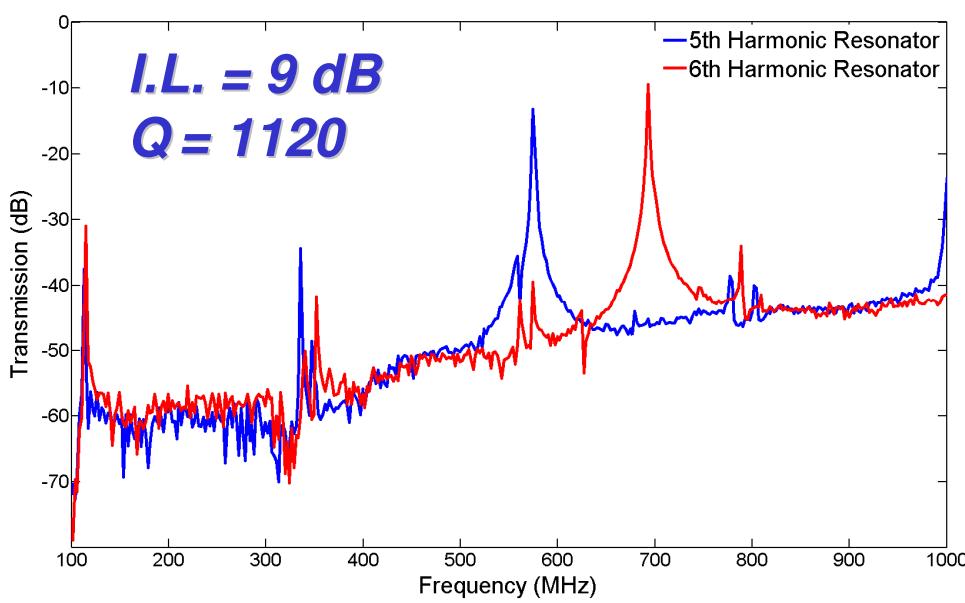
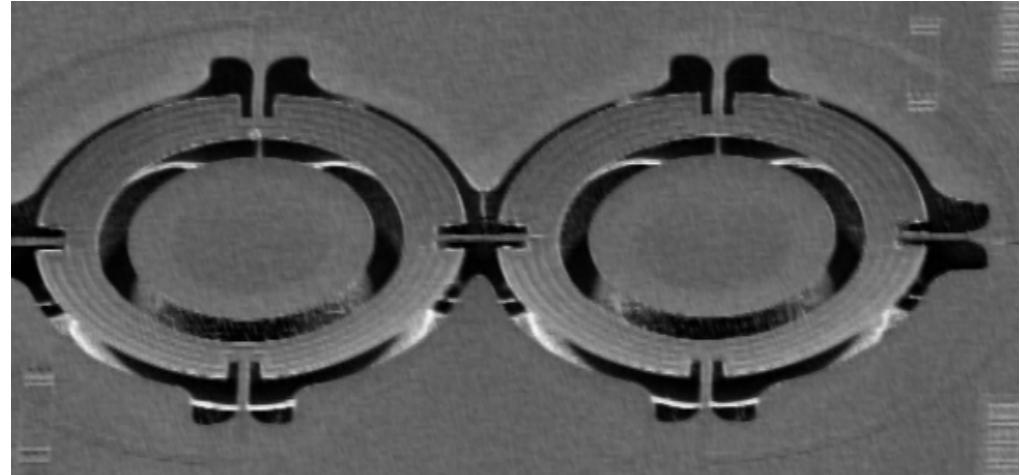
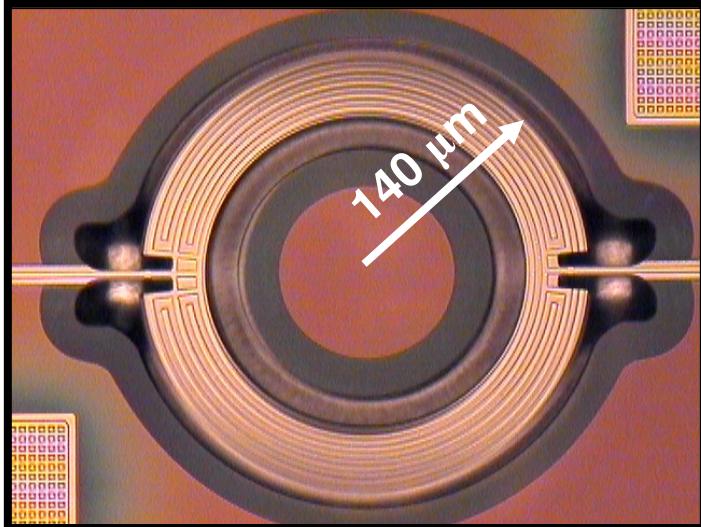
**% Useable Bandwidth (35-125 C) = 93.3%**

**6.7% Bandwidth Dedicated to Temperature Drift**

Oxide Thickness ( $\mu m$ )	$f(-3db) \text{ min } @35 \text{ C (MHz)}$	$f(-3db) \text{ min } @125 \text{ C (MHz)}$	$f(-3db) \text{ min } @35 \text{ C (MHz)}$	$f(-3db) \text{ max } @125 \text{ C (MHz)}$	Useable Bandwidth
0.5	106.900	106.69796	107.0875	106.8851	0 kHz
1.1	99.5125	99.5000	99.69375	99.69375	181.25 kHz



# Scaling to Higher Frequency (Overtone Operation)



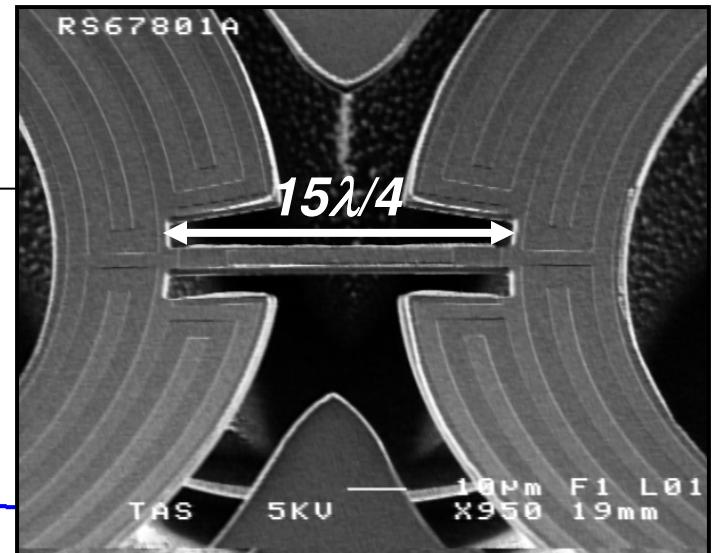
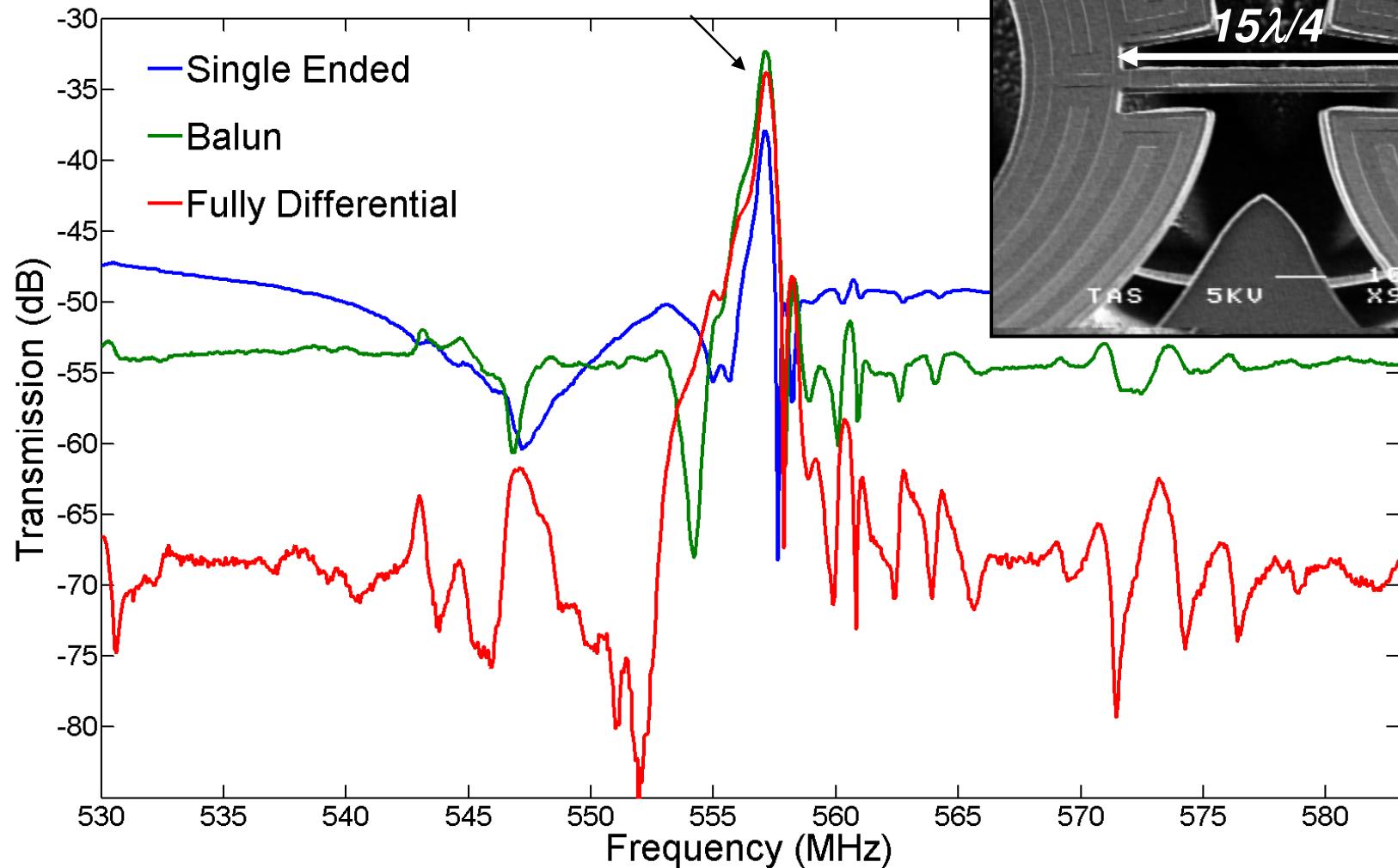
- Overtone MEMS Filters

- Previously scaled resonators to 1 GHz with low insertion loss
- Use overtone operation to scale mechanically coupled filters
- Allows balun and fully differential operation for improved out-of-band rejection



# 5<sup>th</sup> Overtone Filter Measured Results

*Fully Differential Operation Improves  
Stop-Band Rejection by 25 dB  
on Previous Results*





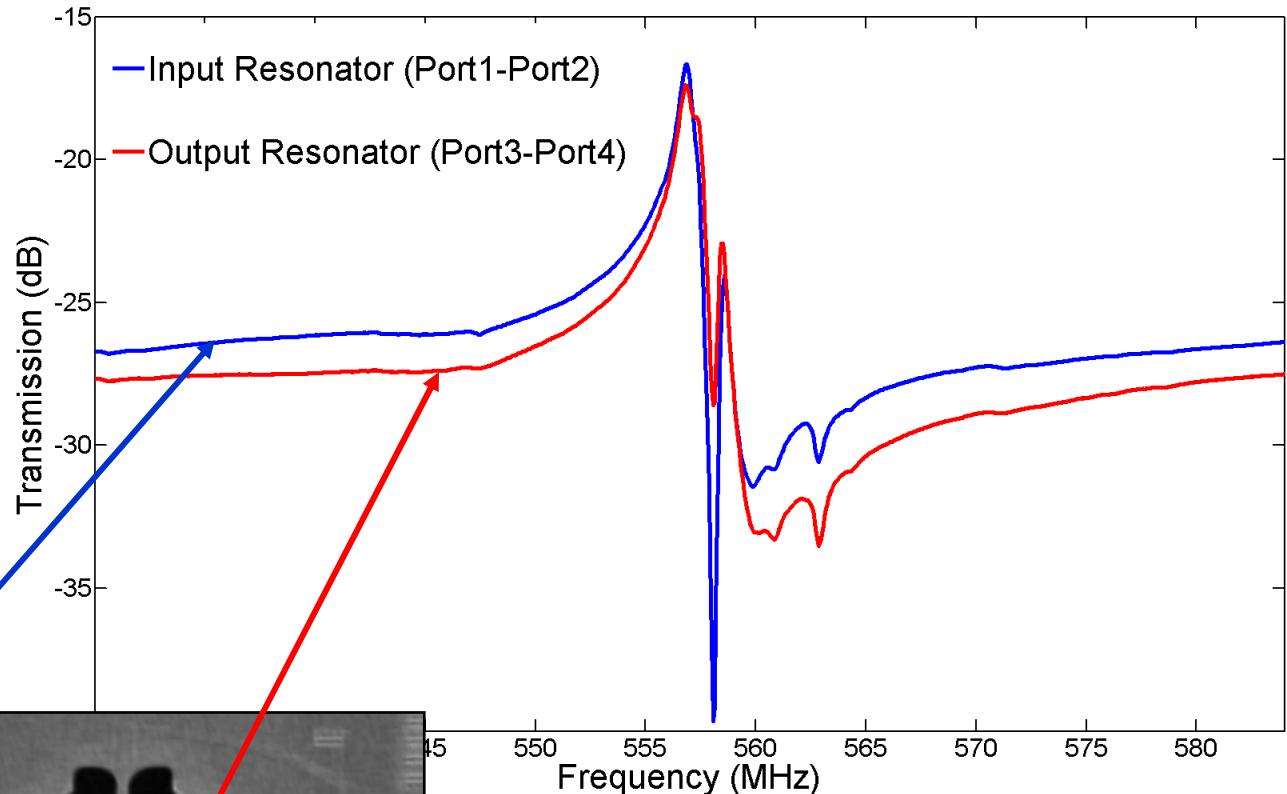
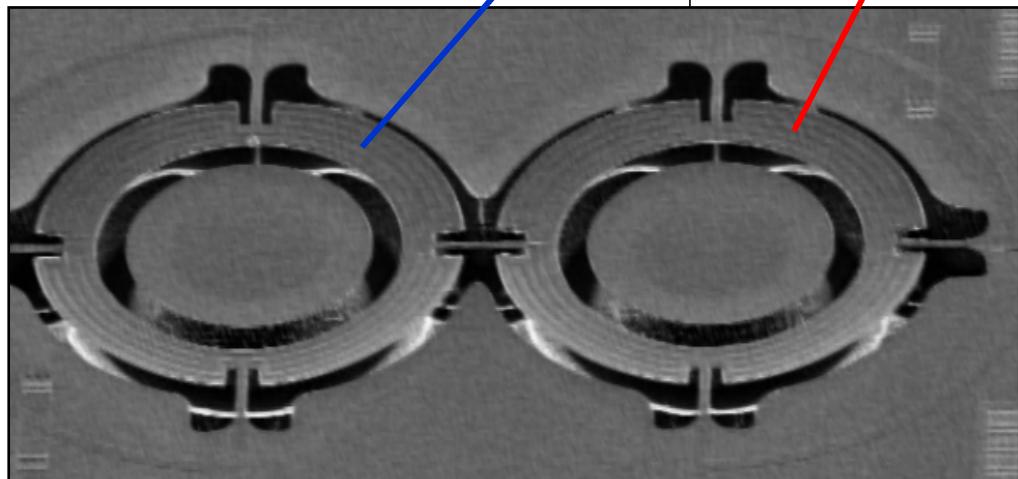
# Overtone Filter Discussion

- Filter Insertion Loss

- *Input/Output Resonators Show Strong Coupling and Matched Frequencies*

- $Q_{Filter} = 1000$  but

- $Q_{Resonator} = 495$



- ❖ *Degraded resonator Q from additional anchors*
- ❖ *Coupling occurs only over 1/5<sup>th</sup> of low velocity coupling locations*



# Conclusions

---

## ➤ MEMS Filter Motivation

- *Small Size, Strong Coupling per Area*
- *Many Frequencies per Wafer*
- *Narrow Band Operation*
- *Filter Banks for Spectrum Analysis and Cognitive Radio*

## ➤ VHF Mechanically Coupled Filters

- *Filter Architecture and Design*
- *Bandwidth Control*
- *Temperature Drift Reduced for Narrow Bandwidth Filters*

## ➤ UHF Overtone Mechanically Coupled Filters

- *Filter Topology Scaled to 550 MHz*
- *Unexpected Insertion Loss*
  - Resonator Q degraded by additional anchors (anchor loss limited)
- *Additional Work Needed to Evaluate Overtone Mechanical Coupling Efficiency*



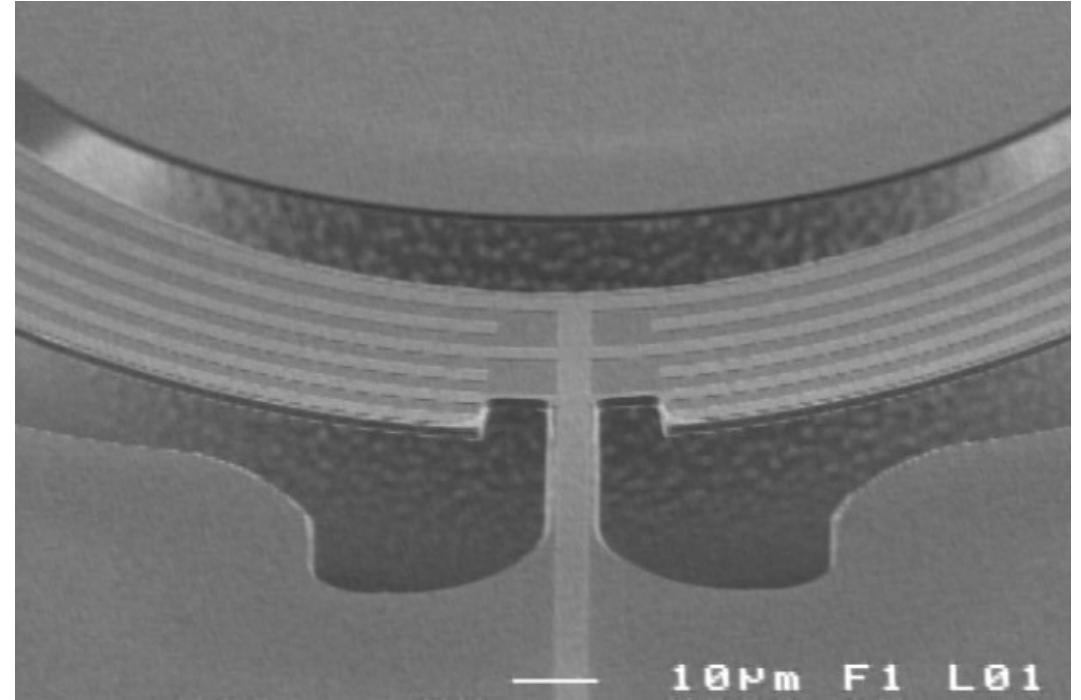
# *Acknowledgments*

---

## Acknowledgement

Microelectronics Development  
Laboratory Staff at Sandia  
National Laboratories

Research Supported by Sandia  
National Laboratories Research  
and Development Program  
(LDRD)



## Contact Information

Roy Olsson ([rholss@sandia.gov](mailto:rholss@sandia.gov))

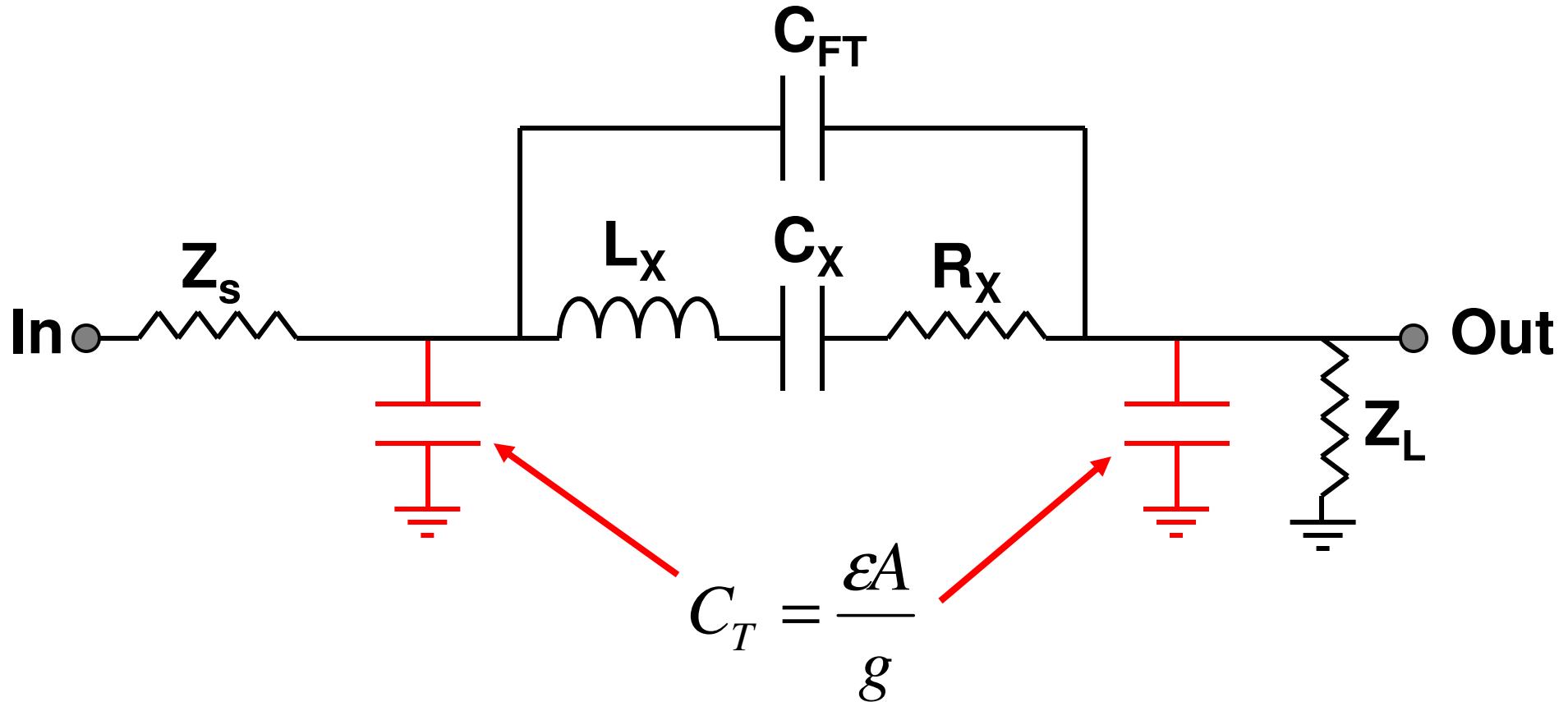


---

# *Backup Slides*



# Transducer Capacitance



In most capacitively transduced devices,

$Z(C_T) \ll R_x$  above a few 100 MHz

increase Overlap Area,  
Dielectric

$$R_x = \frac{k_{beam}^4}{\omega_0^2 Q V_p^2 (\epsilon A)^2}$$