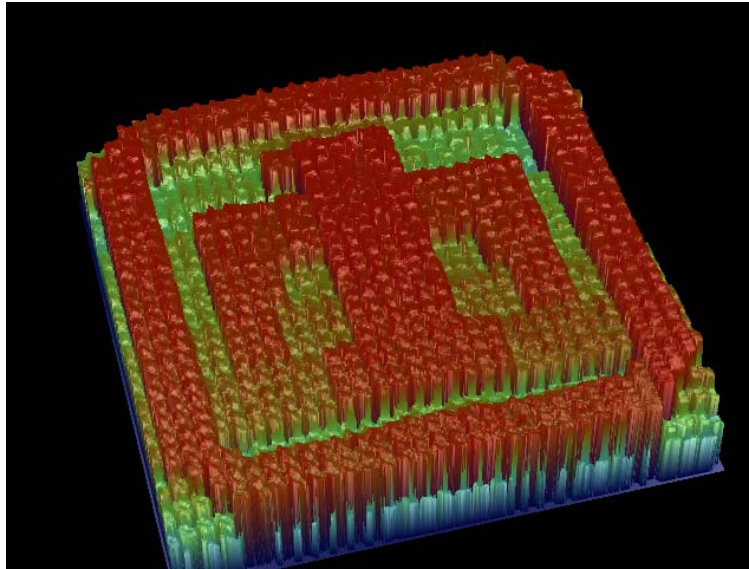




MEMS Active Optics Update

**William D. Cowan, Olga B. Spahn,
Brett E. Bagwell, David V. Wick
and Grant D. Grossetete***

Sandia is a multiprogram laboratory operated by Sandia Corporation, a Lockheed Martin Company,
for the United States Department of Energy's National Nuclear Security Administration
under contract DE-AC04-94AL85000.

*L&M Technologies



Overview

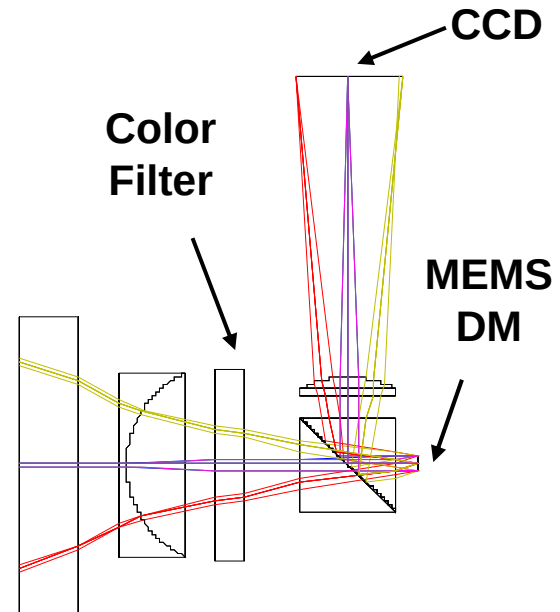
- **Applications and 2007 Focus**
- **SUMMiT™ Technology**
- **Beam Steering Mirrors**
- **High Stroke Mirror Arrays & Results**
- **SFET - SUMMiT™ with Co-fabricated FETs**
- **Latest SFET OMEMS Results**
- **Summary**



Applications

- **Agile Imaging Systems**
 - Non-mechanical Zoom
 - Foveated imaging
- **Beam Steering and Beam Switching**
 - Novel imaging approaches
 - Fast scanning/tracking
- **Gimbal Replacement**
 - MEMS steering speed can overcome angle limitations for some applications
 - Potentially large cost reduction

Foveated Imaging



- **Increase resolution in a selected area of FOV**
 - Extremely wide FOV and low $f/\#$
 - Smaller, more compact than conventional imaging systems
 - Eliminates gimbals (cost, weight, speed limitations, etc.)
 - Multiple threat detection enabled by fast (msec), high resolution tracking of area of interest within the wide FOV
 - Single MEM-DM reduces system aberration

Non-mechanical Zoom



- **Decrease FOV and increase resolution**
 - Optical magnification
 - NO macroscopic moving parts
 - Very fast (20 Hz – 1 kHz)
 - Broadband – Visible to LWIR (if MEMS are used)
 - Two moving optical elements
 - 2 MEM-DMs or macroscopic mirror & MEM-DM



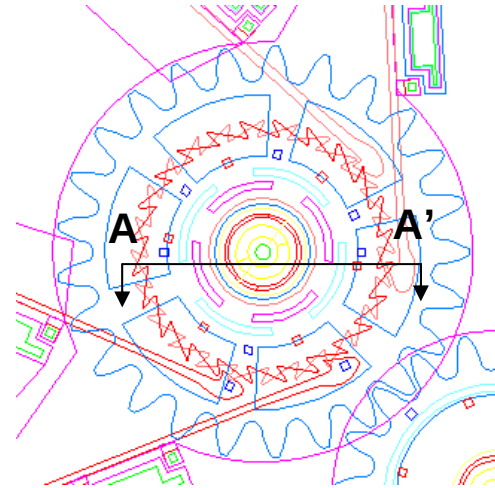
2007 Focus Across Several Efforts

- **Improve**
 - Position repeatability
 - Uniformity and yield
 - Mirror flatness
 - Mirror dynamic behavior
 - Optical power handling
- **Larger aperture DMs**
 - W/o addressing scale-up issues
 - Speed less important
- **Demonstrate scale-up using SFET**

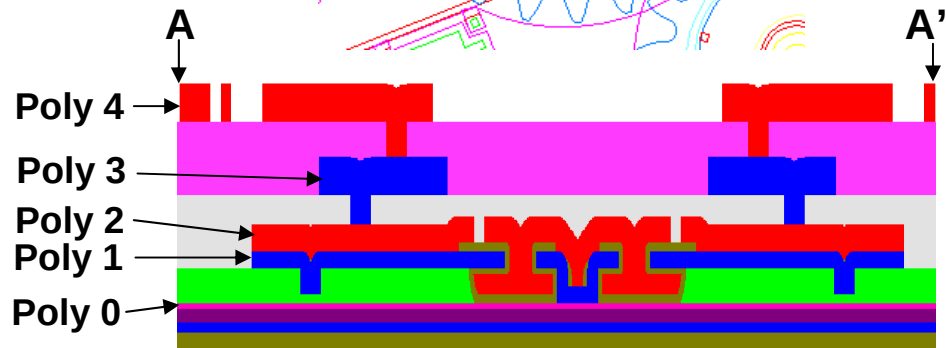
SUMMiT V™ MEMS Technology

Process Features

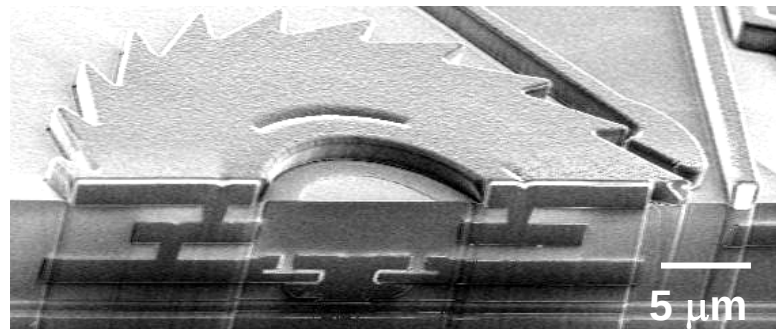
- Polycrystalline silicon (Poly)
- Low stress (< 5 MPa)
- Conformal depositions
- High fracture strength (~ 3 GPa)
- Ground plane layer (Poly 0)
- 4 structural levels (Poly 1- 4)
- Chemical Mechanical Planarization (CMP)
- 1 μm design rules
- Technology accessible through SUMMiT foundry (SAMPLES)
- OMEMS specific BEOL processes
 - Metallization
 - Packaging



Design layout



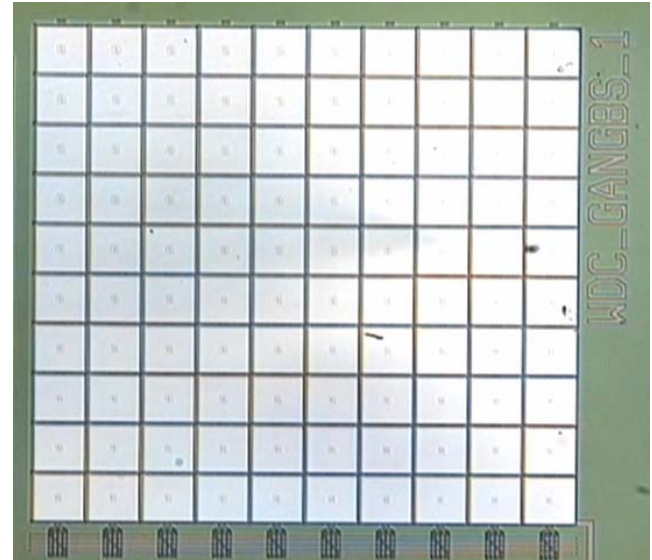
Cross-section drawing



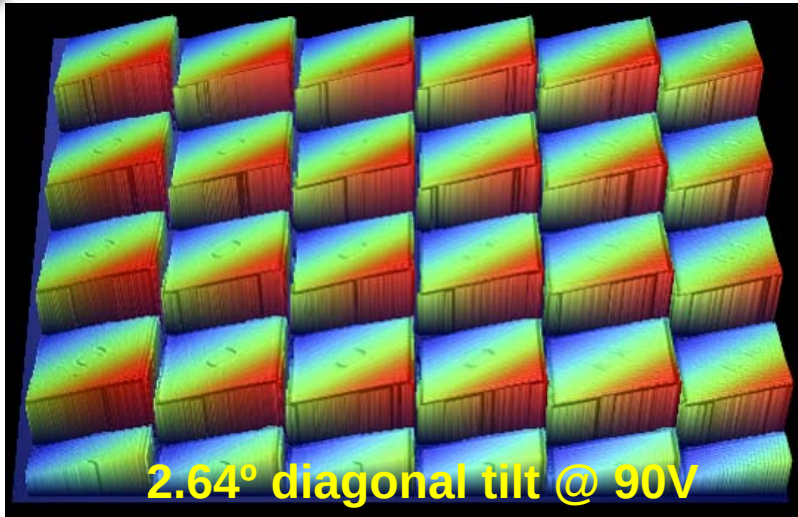
FIB cross-section

Beam Steering Mirrors

- **100 μ m mirrors**
 - 4 electrodes per mirror with analog position control
 - All like electrodes in arrays are tied together – “ganged” – by surface wiring
 - 10x10 array prototypes=1mm
- **Pros**
 - Small size allows large steering angle, speed, easy to keep flat
 - No scale-up problem due to wiring or pin out
- **Cons**
 - Incoherent steering only
 - No calibration, so deflection uniformity is critical

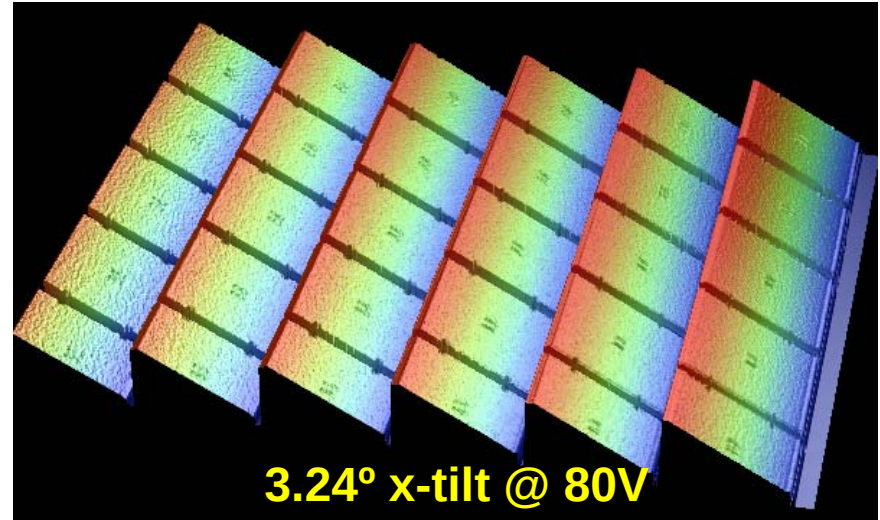


Ganged Arrays



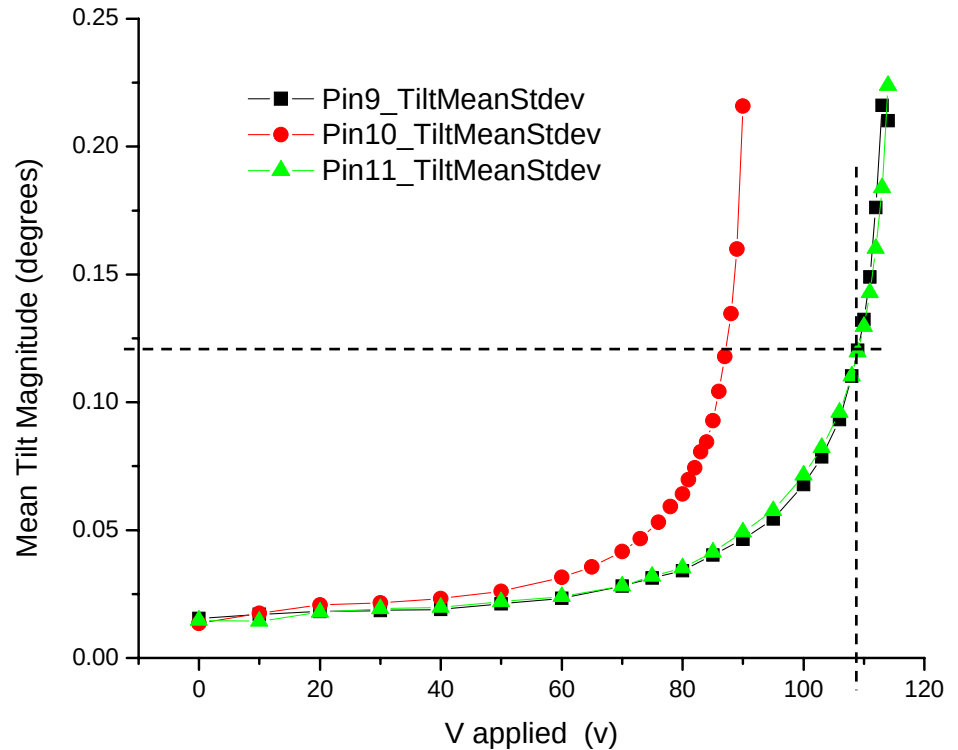
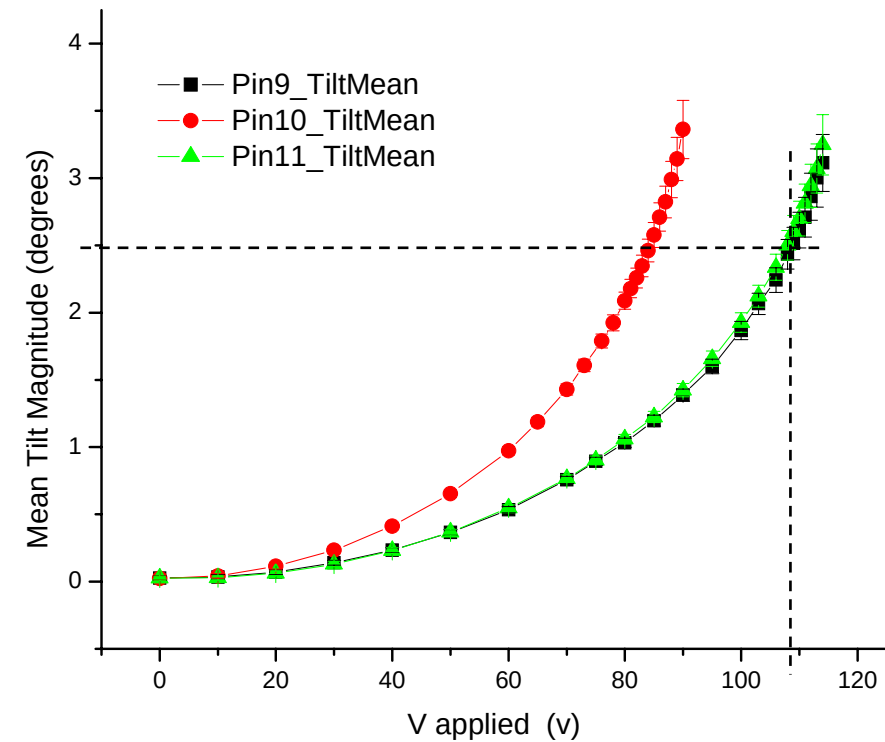
- Ganged Beam Steering
 - Four electrodes per mirror
- Currently in a bench top beam steering demo w/ $\sim 10^\circ$ FOR

- Fast – switching speeds $< 10\mu\text{sec}$, analog position control
- Applications: scanning sensors, missile seekers (gimbal replacement), novel imaging



- Slat Mirror Arrays
 - Two electrodes per mirror
 - Two arrays and auxiliary mirror required for 2-D steering

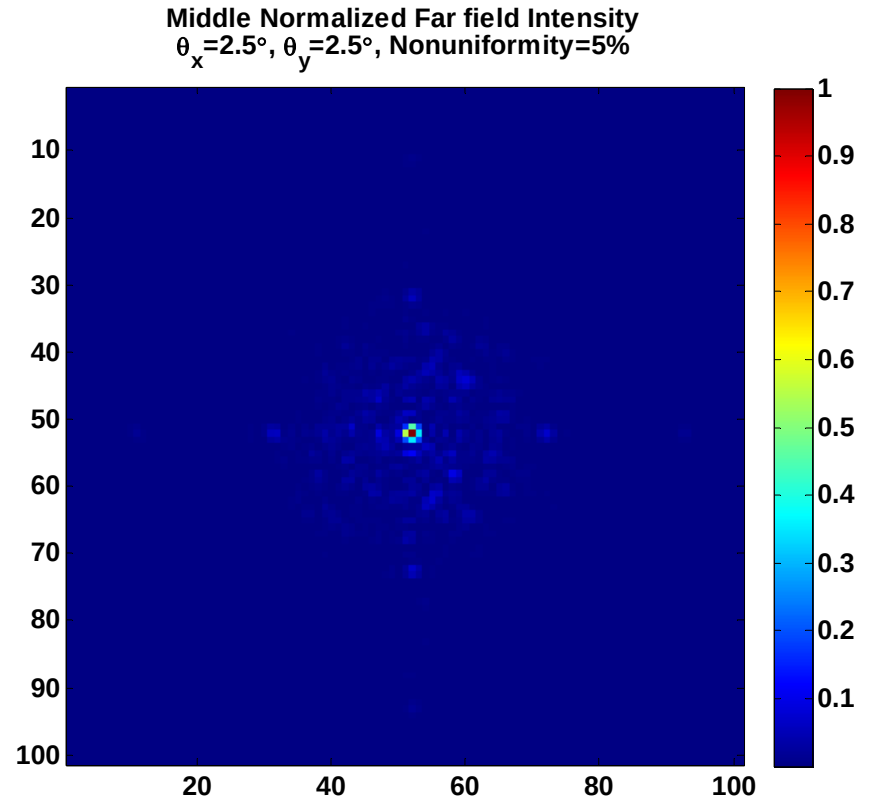
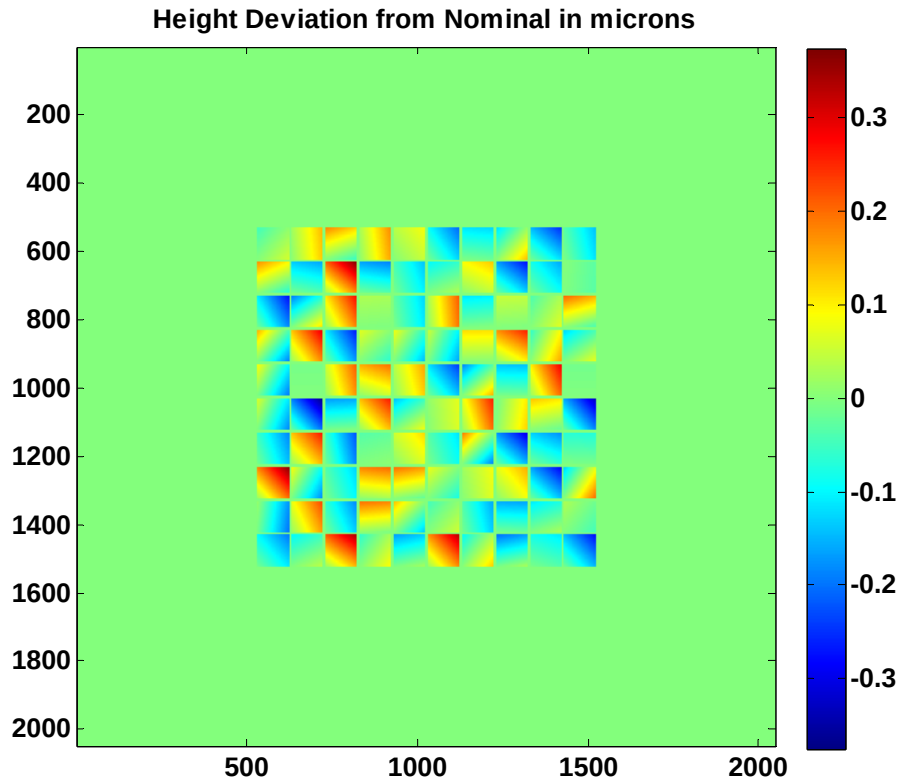
Ganged mirror array - Tilt magnitude and standard deviation vs. applied voltage



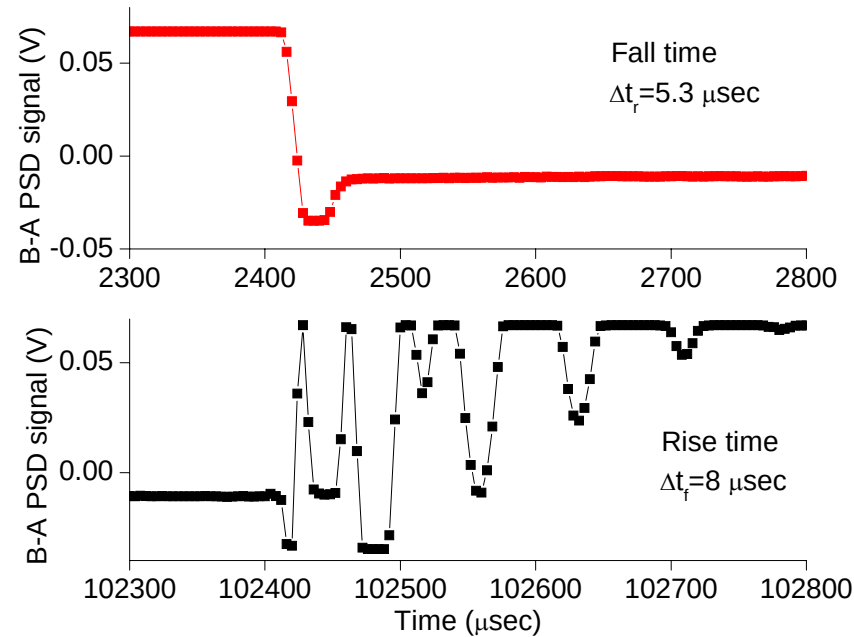
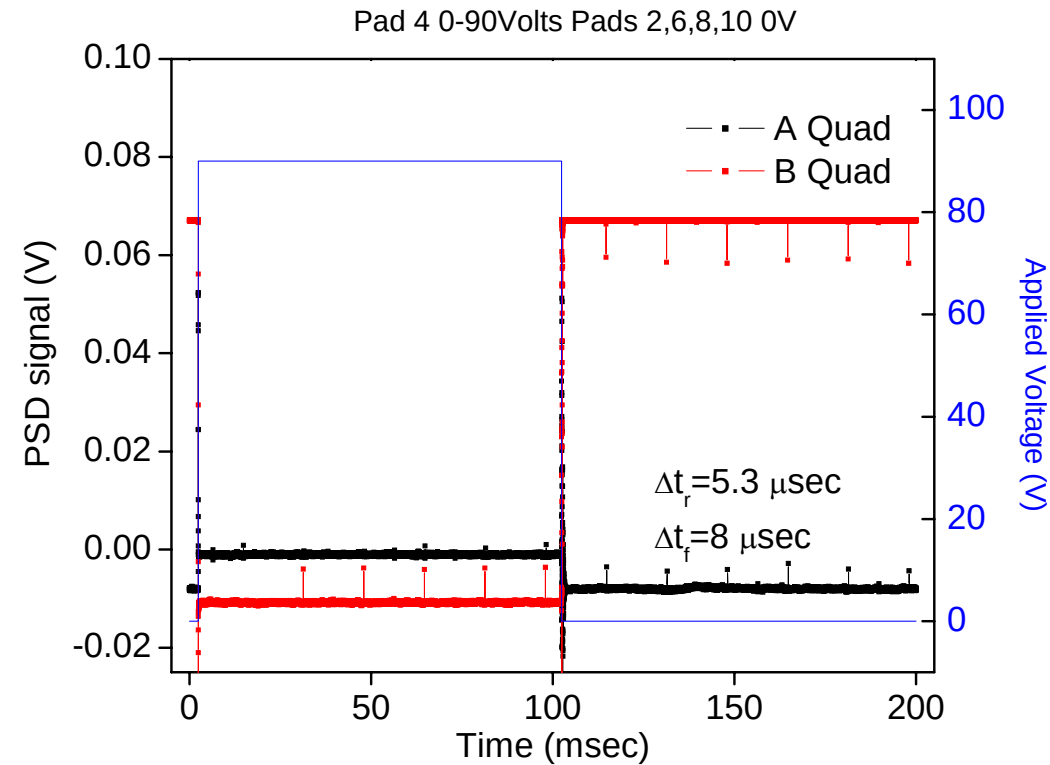
Deviation $\sim 0.125^\circ$ at 2.5° deflection $\Rightarrow \sim 5\%$

Impact of Angle Non-uniformity

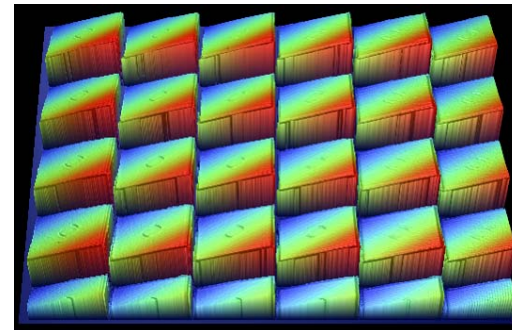
Matlab Model, $\theta_x = \theta_y = 2.5^\circ$, Nonuniformity=5%, $\lambda = 532\text{nm}$



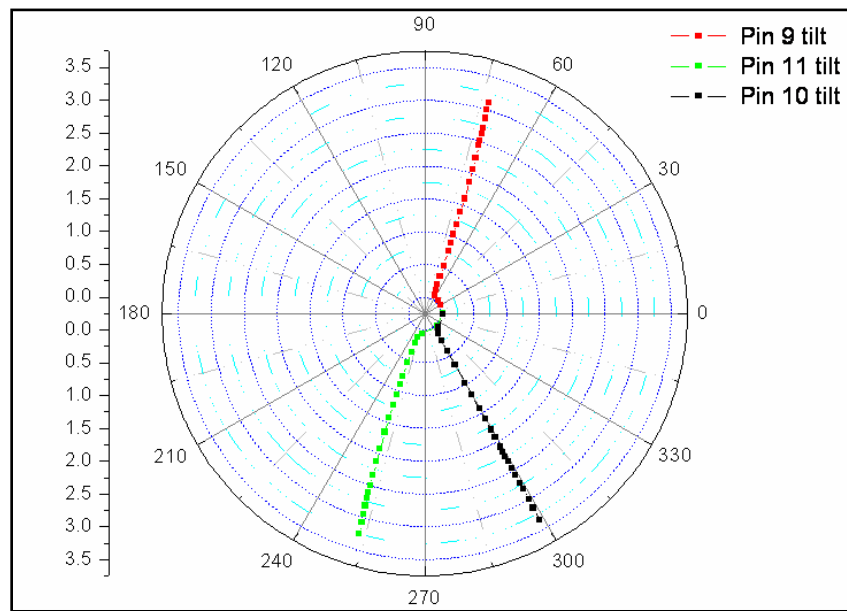
Dynamic Behavior of Ganged Arrays



GANGBS_1A 90V, 2.64° diagonal tilt

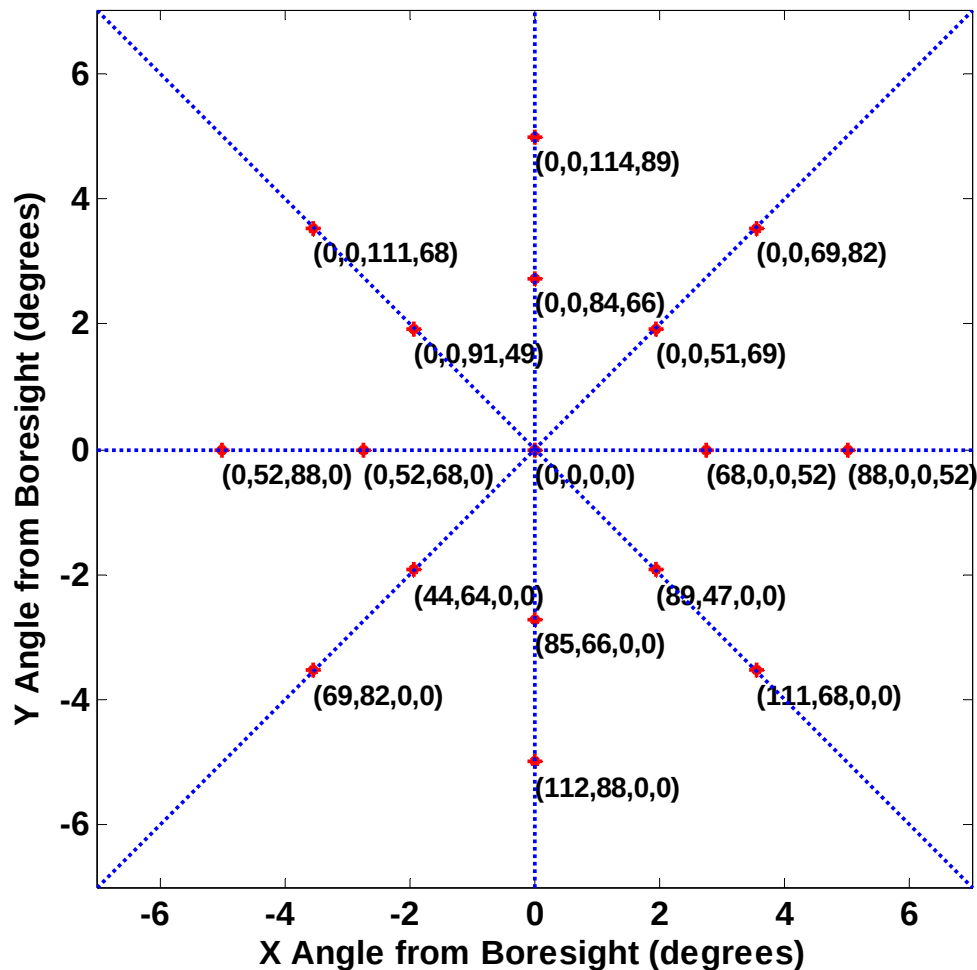


Beam Steering Demo



Mechanical Angle, Single Electrode Drive

Beam Position vs Drive Voltage (SE,SW,NW,NE)



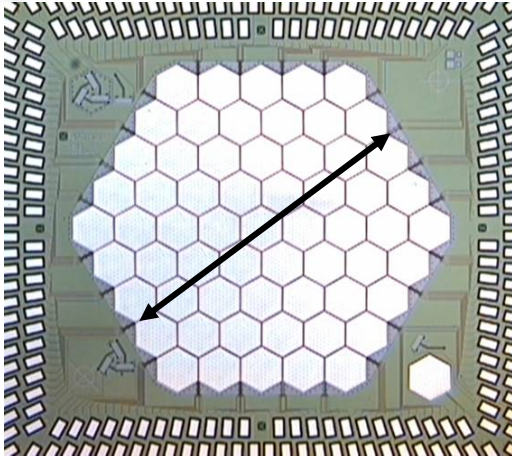


MEM-DM Requirements

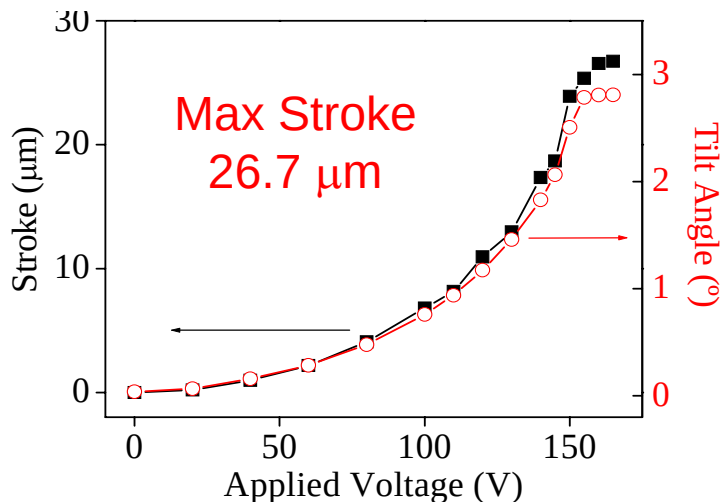
- In addition to the usual requirements of mirror quality, high fill-factor, good reflectivity, etc.
- Large stroke
 - Foveated imaging
 - Greater stroke allows greater degree of uncompensated aberration
 - Greater aberration = greater steering angle
 - Non-mechanical zoom
 - More stroke = more optical magnification
- Larger apertures required for practical systems
 - Larger pixels or more actuators
 - Larger pixels conducive to larger stroke BUT...
 - Speed and mirror flatness get more difficult
 - More actuators requires addressing the pin-out problem
- Currently working all the angles

***2007 DM focus was on increasing aperture...
...without losing functionality...(and improving
uniformity/repeatability)***

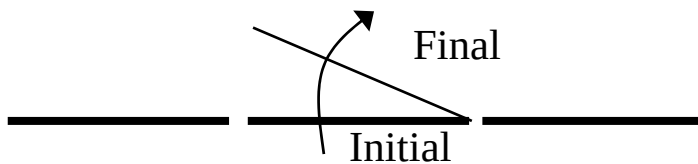
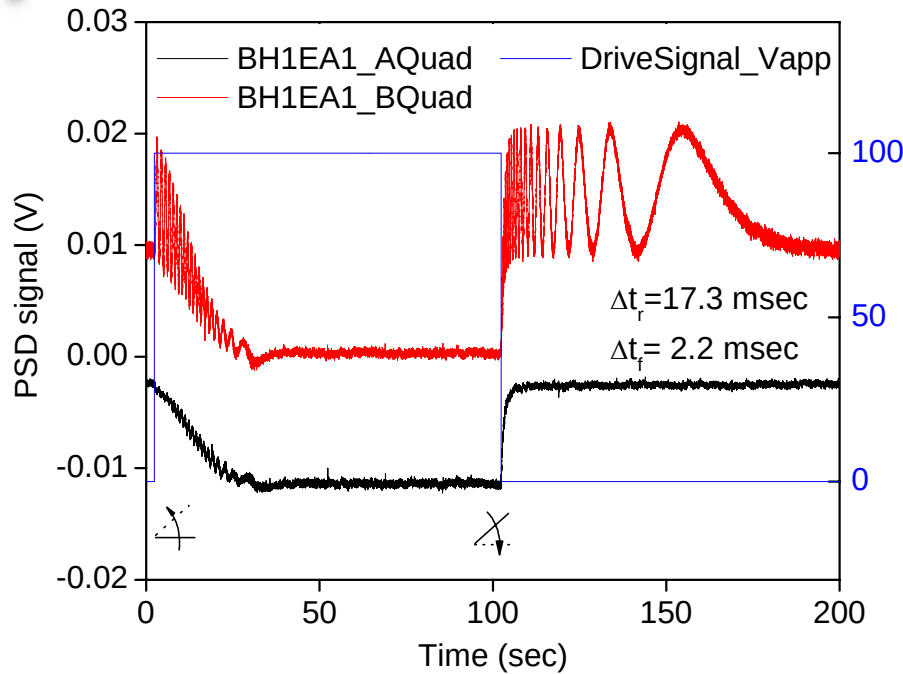
New 500 μ m Piston/Tip/Tilt Mirror Arrays



- Original employed mechanical pivot in actuators
 - Ensured full stroke but bad for uniformity, position repeatability and dynamics
- Revised (BH1_E & _F)
 - No mechanical contact in actuators (except at full deflection)
 - Optimized torsion springs and actuator to mirror plate springs using beam element models
 - BH1_F has slightly longer lever for >stroke

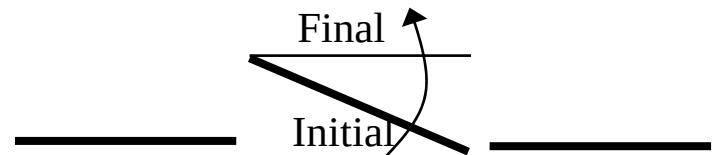
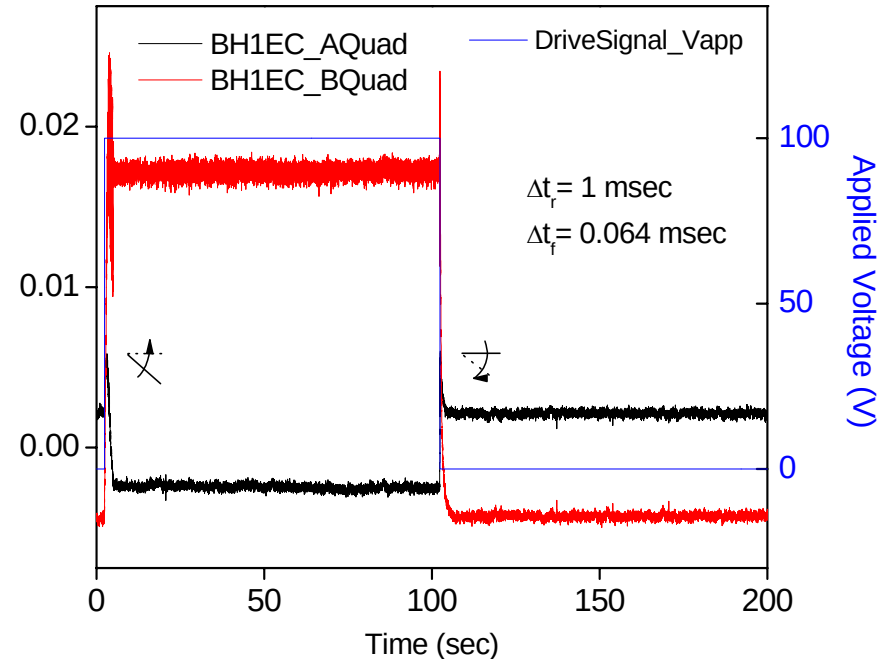


500 μ m Mirror Dynamics (in air)



Profile of mirror position

Air damping and mechanical contact of mirror edge

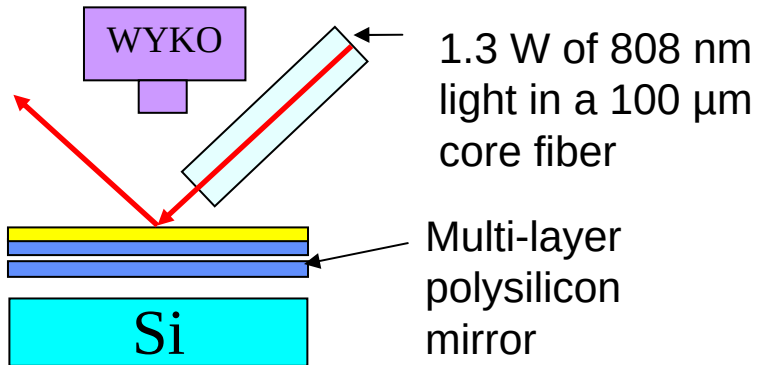


Profile of mirror position

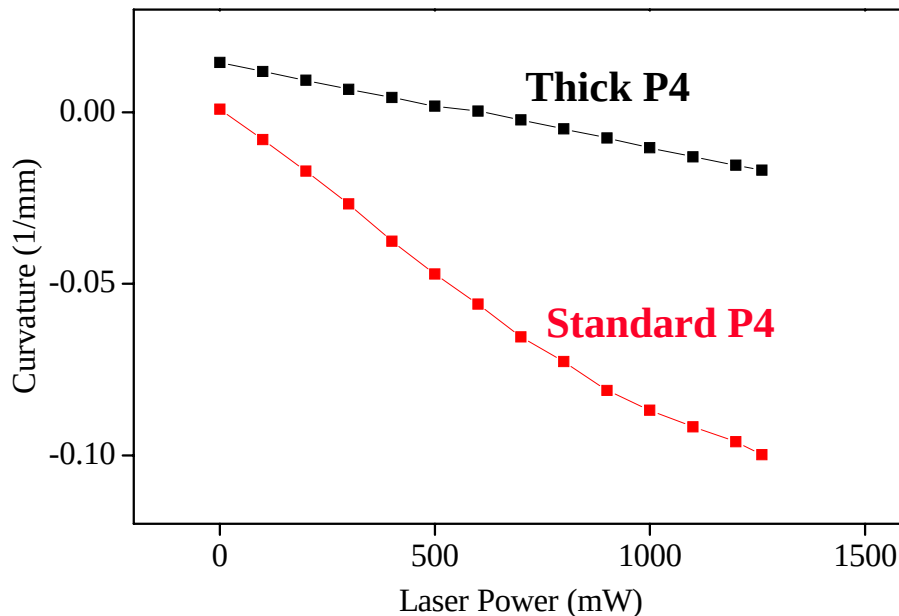
Minimal damping, NO mechanical contact

Improved Optical Power Handling Using Thicker Poly4

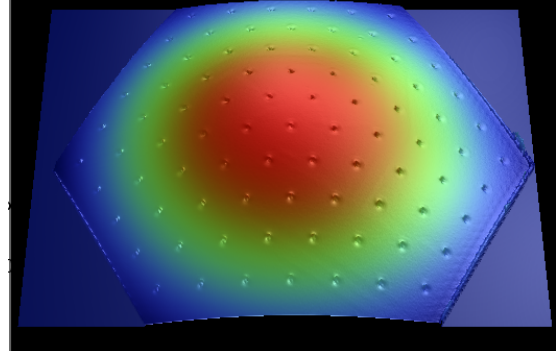
Laser Heating Setup



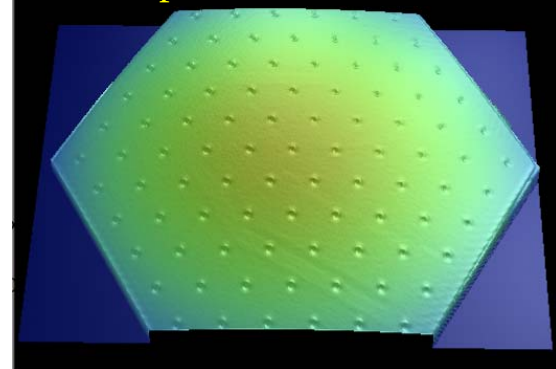
Measured Curvature vs Laser Power



Standard p4



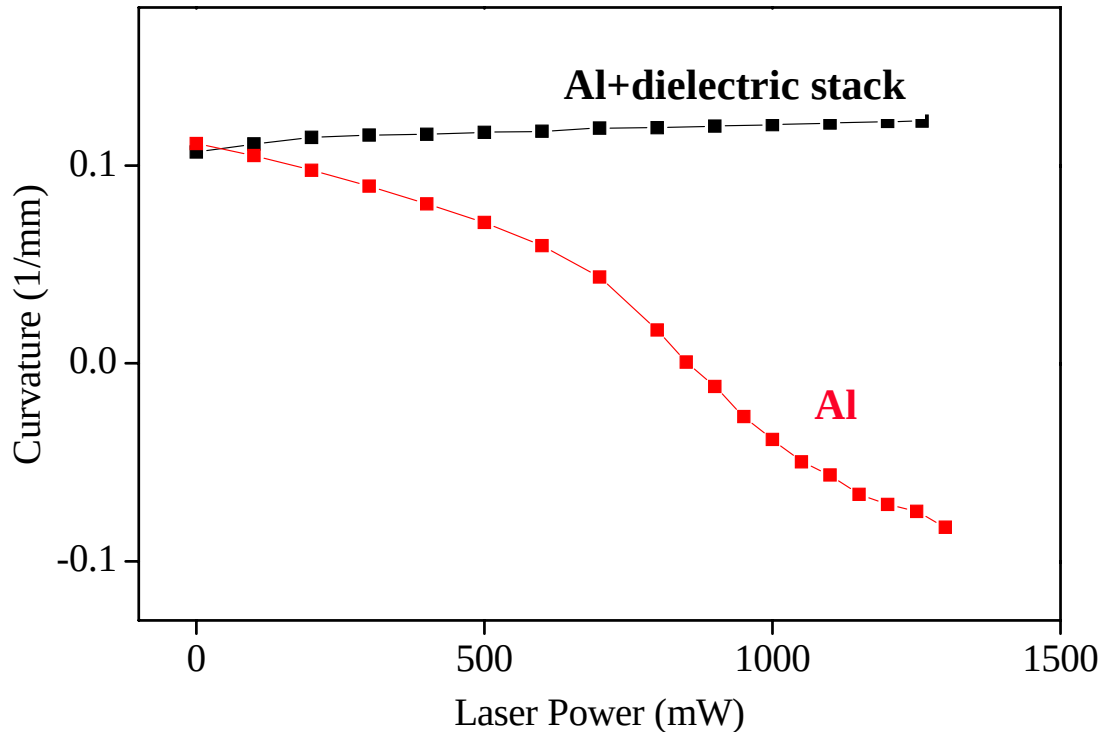
Thick p4



Difference Surfaces
(1.25W – 0W)

Improved Optical Power Handling Using Dielectric “helper” Stack on Metal

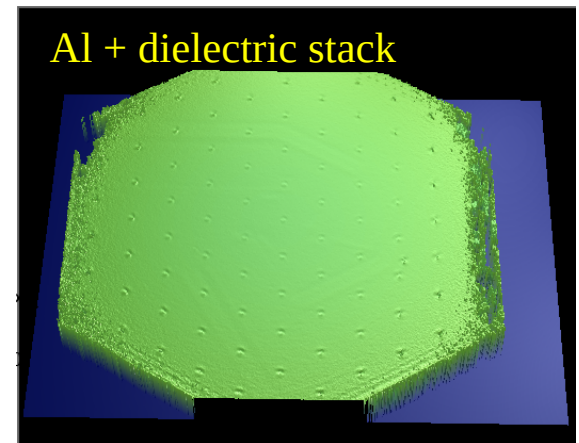
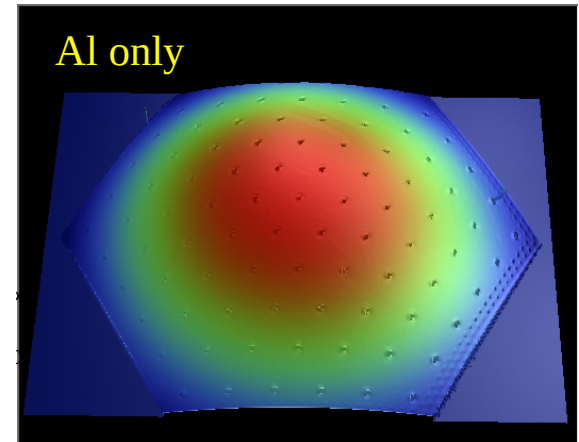
Measured Curvature vs Laser Power



Helper stack=4 pairs SiO₂/HfO₂

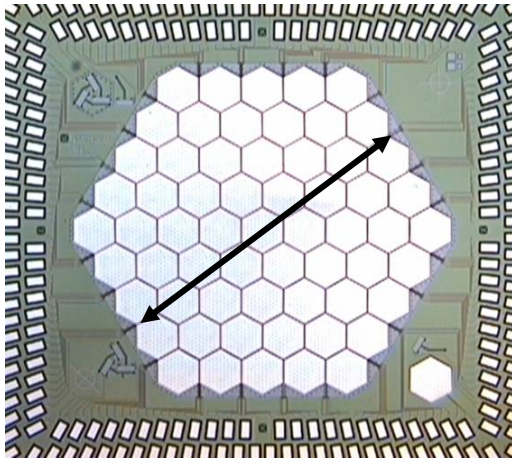
Absorbance at 808 nm = 2.3% for dielectric+Al
(vs. 15.8 % for Al only coated mirrors)

Mirror mechanical functionality not tested

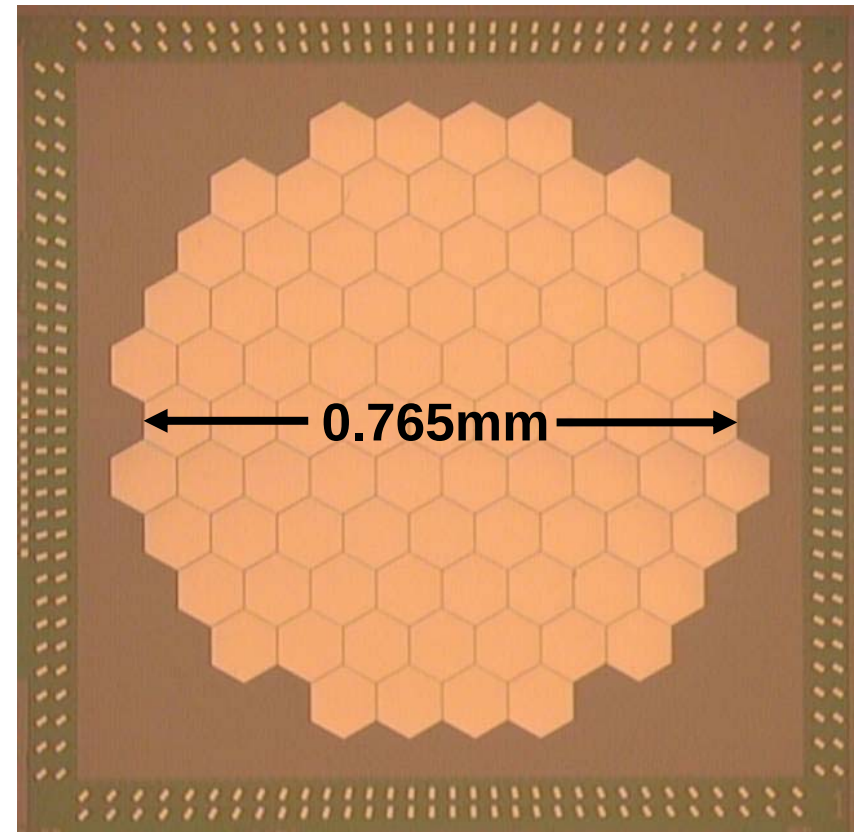
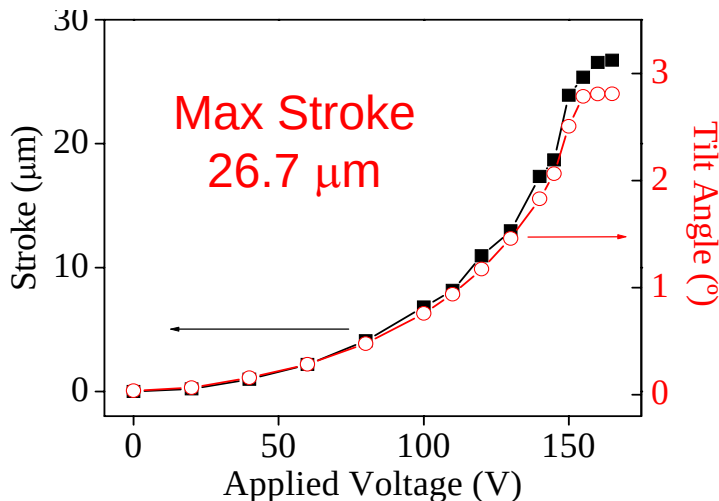


Difference Surfaces
(1.25W – 0W)

~8mm Piston/Tip/Tilt Mirror Arrays



- 61 hex mirrors in hex array
- Mirrors 0.5 mm edge-to-edge
- 3.9 mm array aperture
- 208 pin PGA package

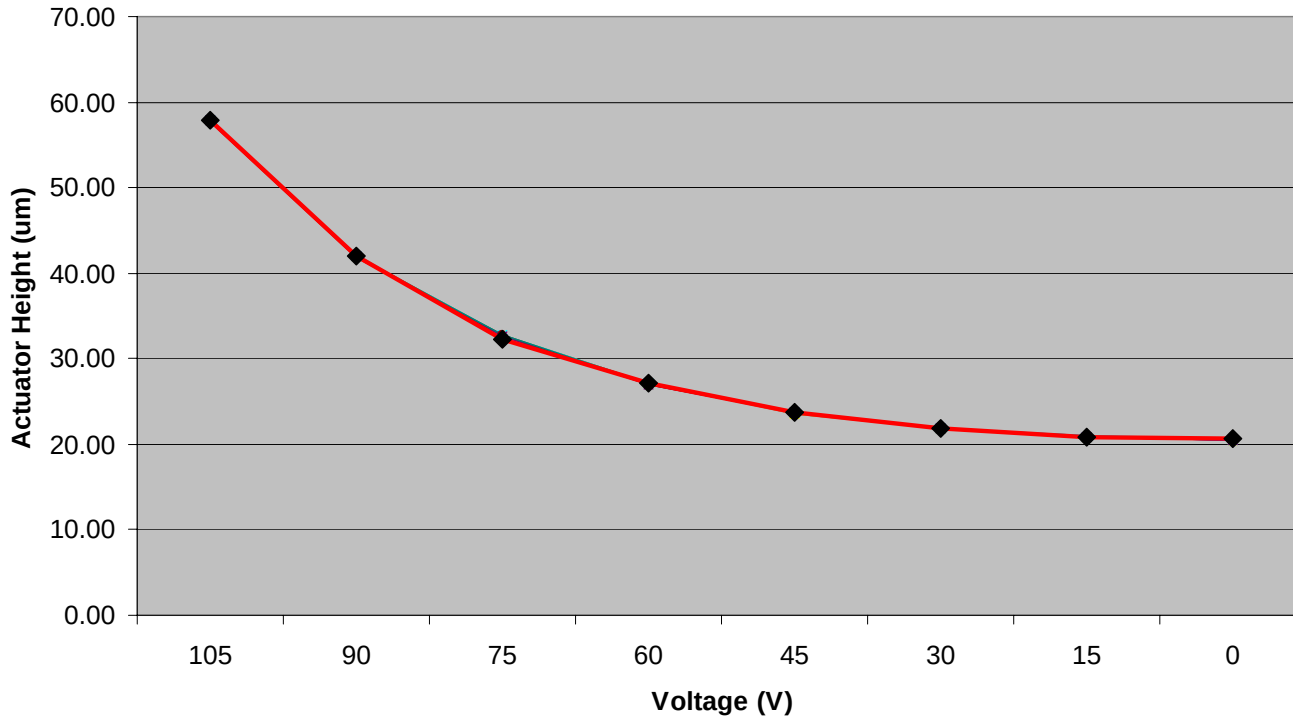


- 85 hex mirrors in hex array
- Mirrors 0.85 mm edge-to-edge
- ~8 mm array aperture
- 256 pin PGA package
- 3 actuator variations

850um Mirror Position Repeatability

Lever 1 Design with 2 Up, 1 Down

Actuator Height vs. Voltage



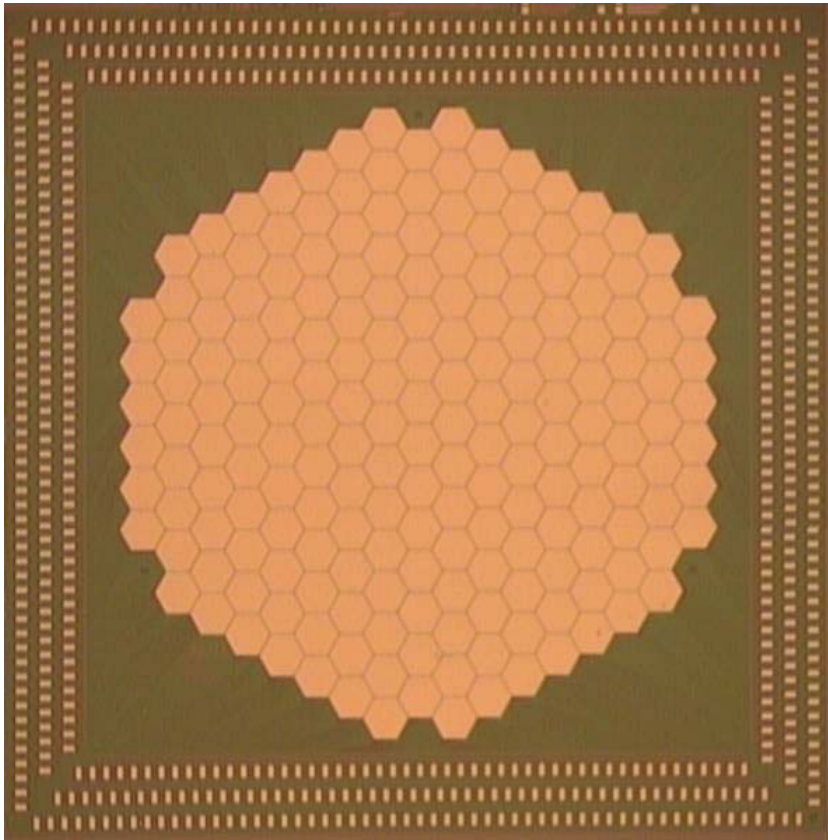
- 10 Iterations
- 2 up → 1 down
- 8 samples across 0-105V
- Average Template Fit = 995/1000

V	Height (um)	σ (um)
105	57.80	3.16E-02
90	41.99	7.97E-02
75	32.54	2.22E-01
60	27.09	5.45E-02
45	23.67	3.14E-02
30	21.84	3.79E-02
15	20.89	3.37E-02
0	20.54	4.22E-02
Avg		6.66E-02

Radius of curvature of 850 L1 (Standard poly4, 50 nm AlCu, wafer center)



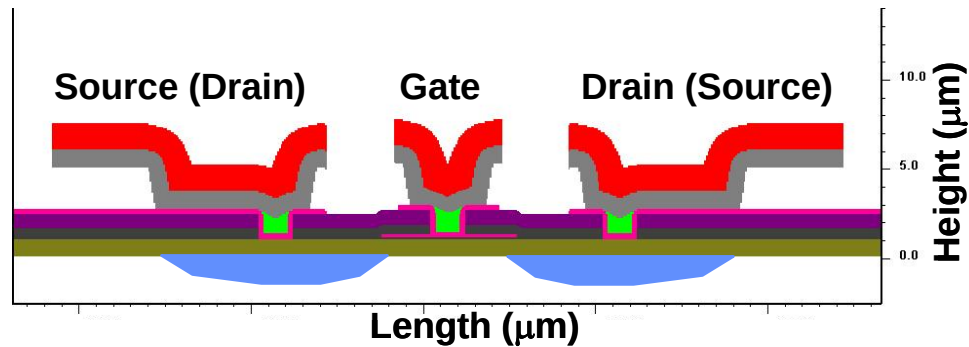
~8mm Aperture, 211-Mirror Array



← 10.5 mm →

- 211-hex mirrors in hex array
- ~8 mm array aperture
- Mirrors 0.5 mm edge-to-edge
- BH1_F design, $>25\mu\text{m}$ stroke
- Status – largely untested
 - BGA packages on hand but no parts packaged yet
 - Mirror flatness OK
 - Visual yield OK (quarter wafer inspection)

SUMMiT™ Field Effect Transistor (SFET) Fabrication

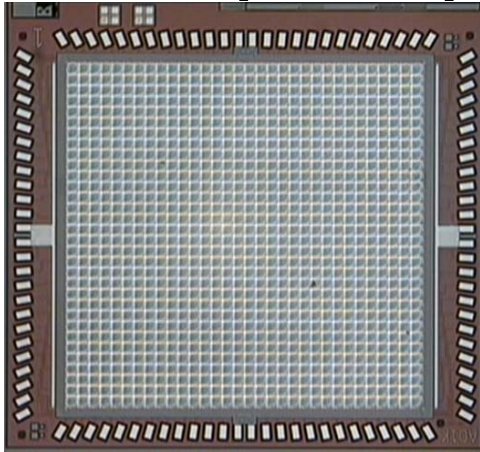


- **SUMMiT™ flow with added gate level for SFET**
 - Gate oxide, 1000Å steam, grown on bare Si p-type substrate
 - Polysilicon gate uses same film *type* as Poly0; deposited immediately after gate is grown
 - Poly12 source/drain contacts doped in-situ with phosphorus
 - Subsequent high temperature anneals (for stress control) diffuse dopant into substrate to form source and drain
- **Remaining fabrication steps identical to SUMMiT™ V**
 - Building on a mature and robust MEMS process
- **Back end processes: 100nm Al metal, release & packaging**

B. L. Draper, M. Okandan, S. S. Mani, and R. S. Bennett, "A Novel Method of Fabricating Integrated FETs for MEMS Applications," *IEEE JMEMS*, Vol. 13, No. 3, pp. 500-504, June 2004.

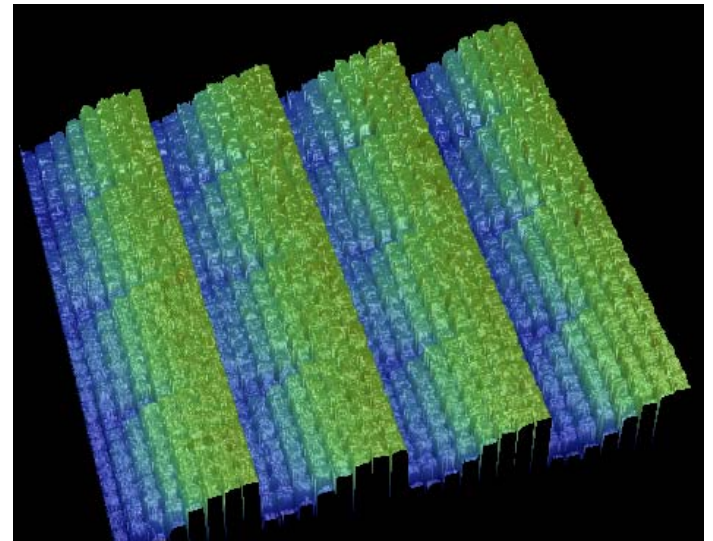
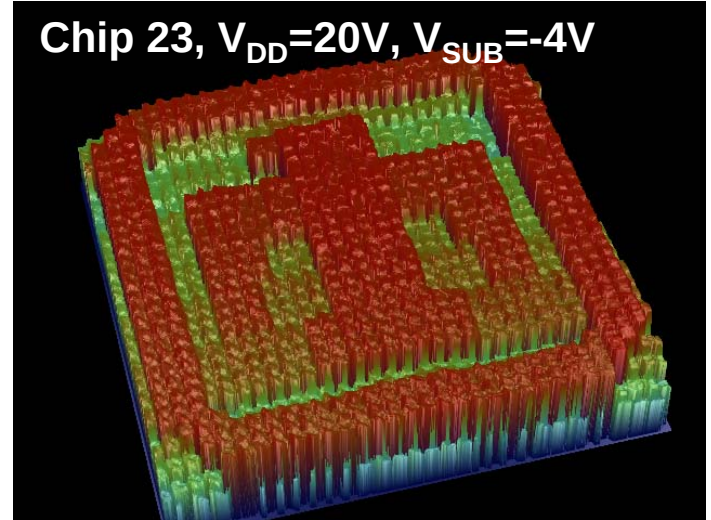
Piston Mirror Array (PW2007)

AO1K (RS562)



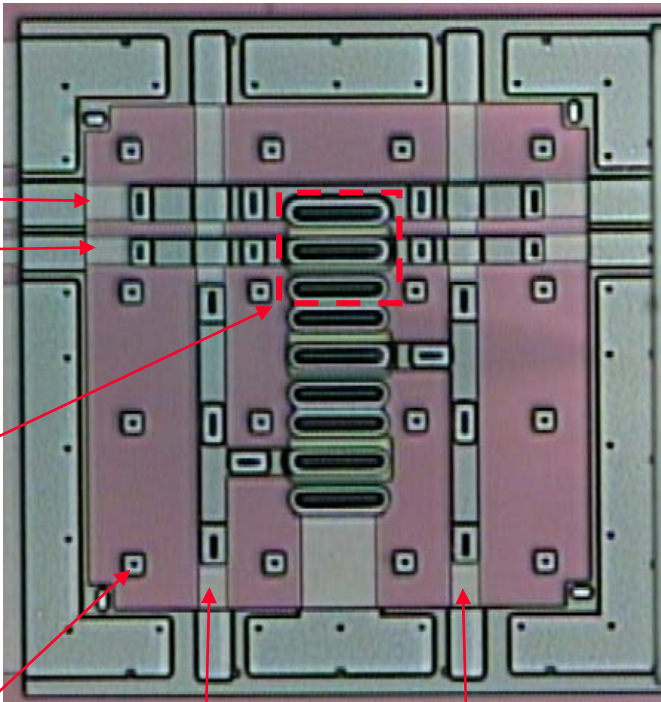
- 1024 Piston-only mirrors
- Mirrors 0.15 mm square
- Maximum stroke: 2 μm
- 4.8 mm array aperture
- 132 pin PGA package
- Applications: laser communications, narrowband/high-speed aberration correction

Chip 23, $V_{DD}=20\text{V}$, $V_{SUB}=-4\text{V}$



AO1K Construction Details

Through Poly2
(No Poly3 or Poly4)

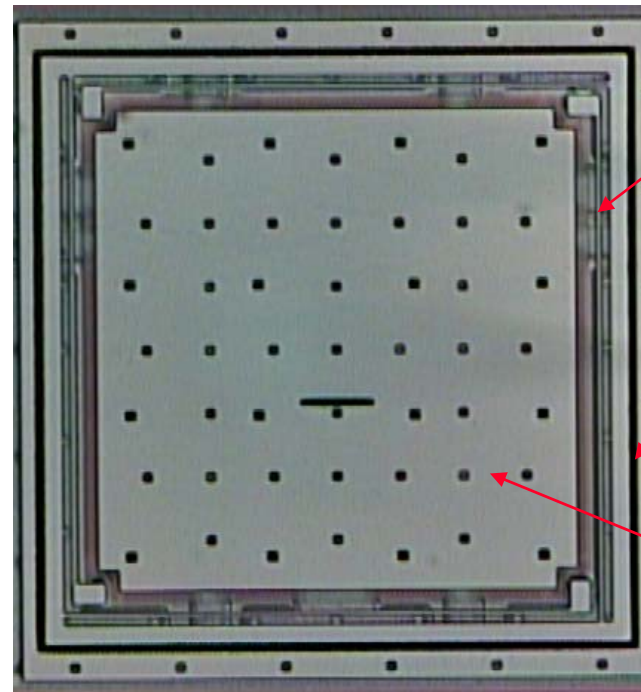


Electrode
support
pillar
(1 of 16)

Reset

Column

Through Poly3
(No Poly4)



Flexures
(1 of 4)

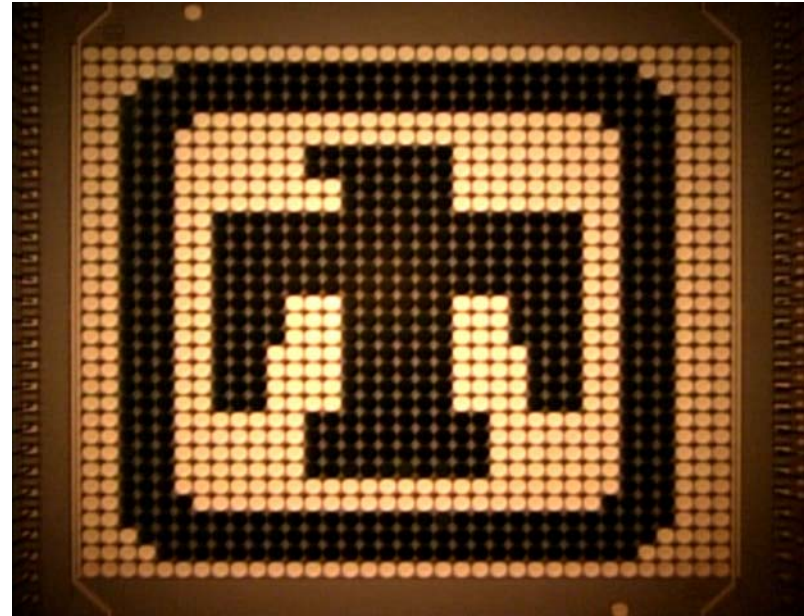
Shielding

Electrode

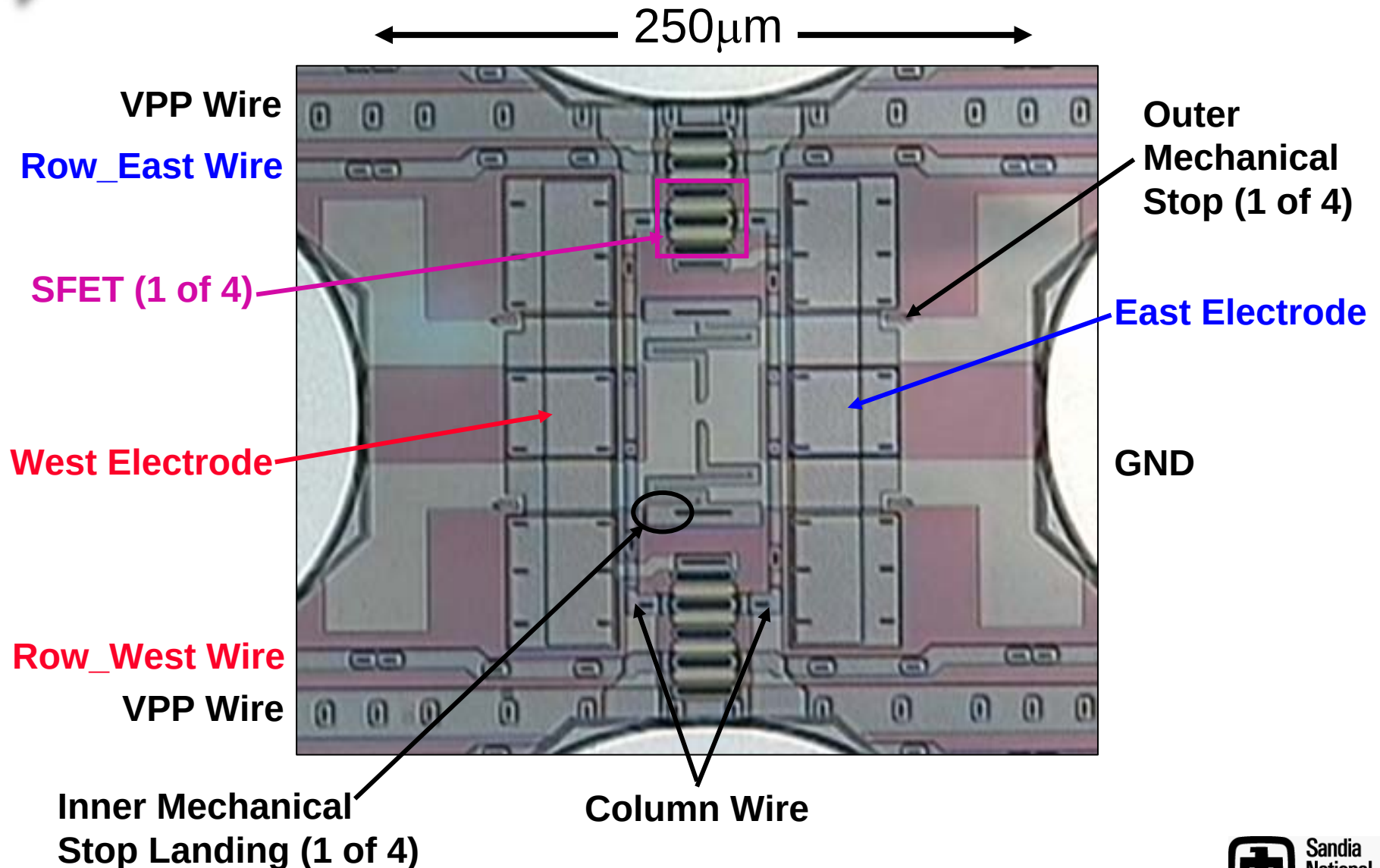
150 μm

SFET Beam Switching Mirror Array

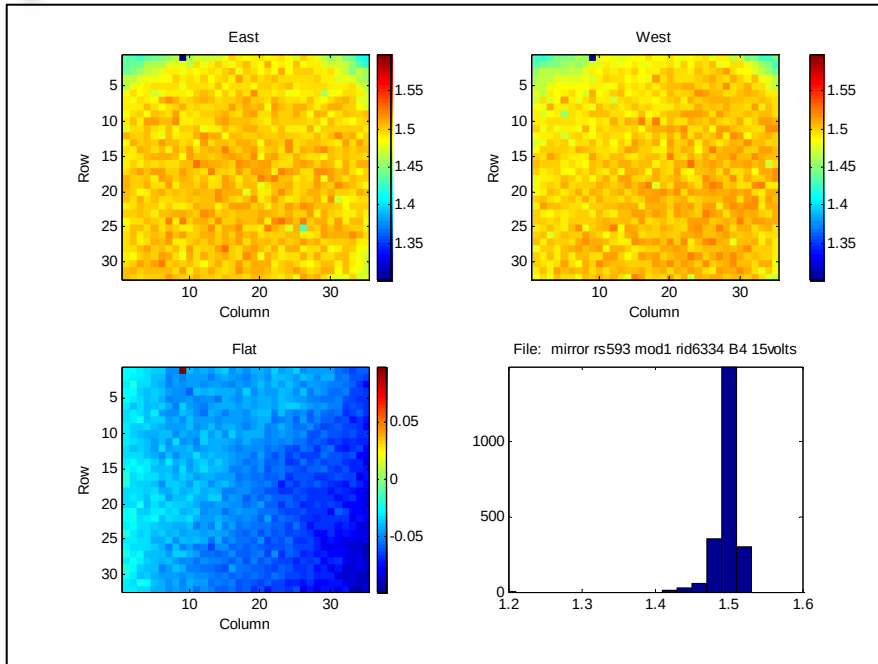
- **Largest SFET-OMEMS devices to date**
 - 1120 mirrors (32-rows x 35-columns)
 - 240 μm diameter mirrors, 250 μm pitch
- **Integrated row/column address electronics**
 - 2240 electrodes (2 per mirror)
 - 4 or 6 transistors per mirror cell
 - Packaged in 120 pin PGA
- **Tri-stable mirrors: $\pm 1.4^\circ$, 0° (flat)**
 - Angle deviation $< 0.1^\circ$
- **Mirror flatness: $< 30\text{nm}$ peak-to valley**
- **Switching speed:**
 - **Mechanical:** $< 150 \mu\text{sec}$ in air
 - **Circuit/transistors:** $> 20\text{MHz}$ (current version of electronics support $\sim 45 \mu\text{sec}$ array update)
- **Functional Mirror Yield: 99-100%**



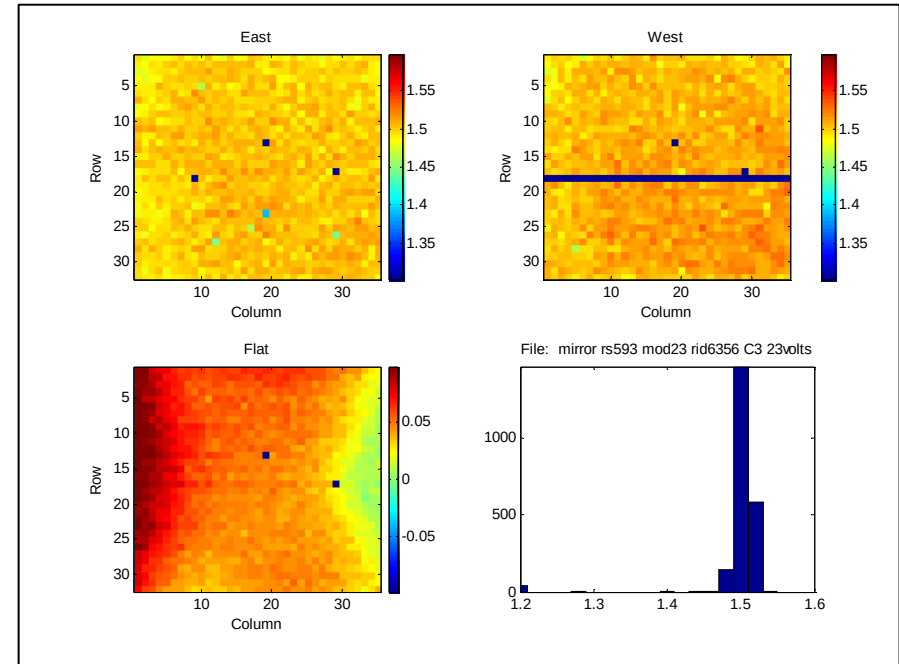
SFET Switching Mirror Detail



Etched vs Backfilled DIMPLE3

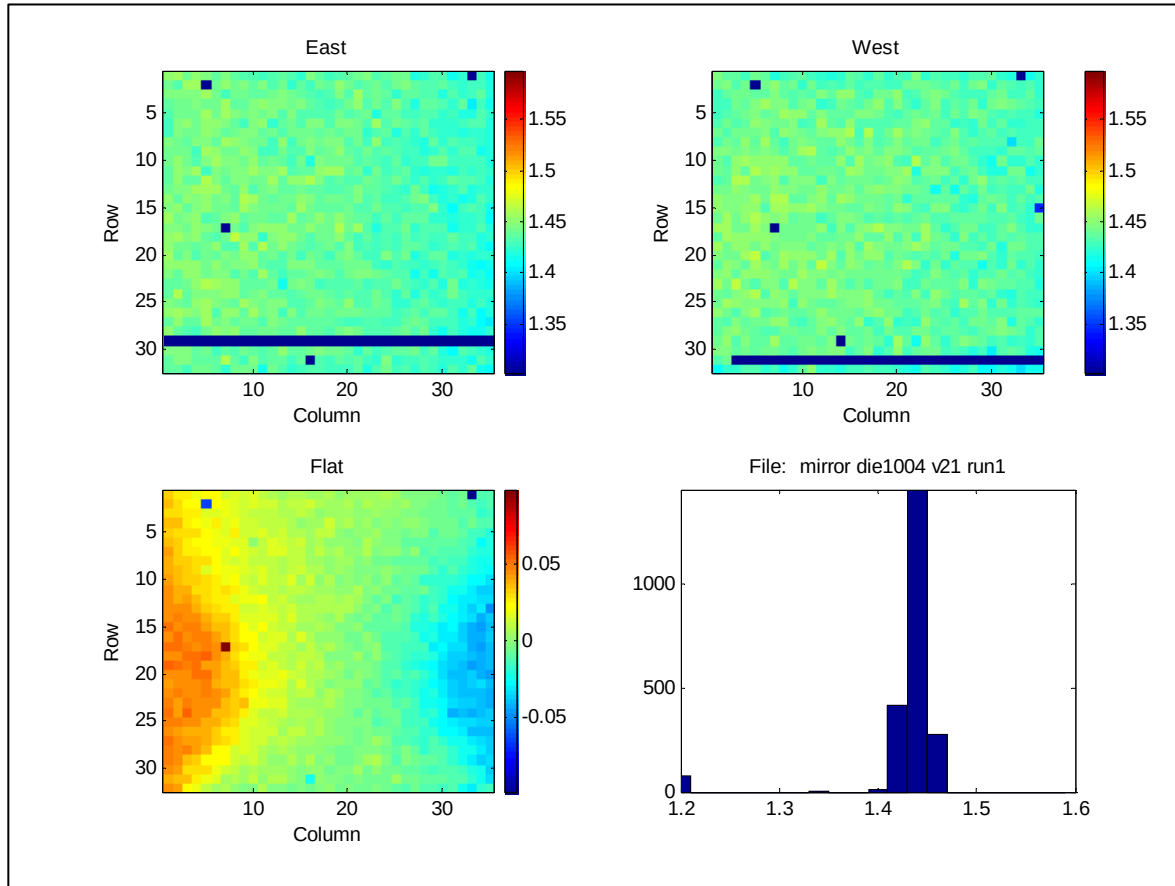


East mean= 1.497 std dev=**0.014**
with 1119 points
West mean= 1.498 std dev=**0.014**
with 1119 points
Combined East/West mean= 1.498
Flat mean= -0.051 std dev=0.014
with 1119 points

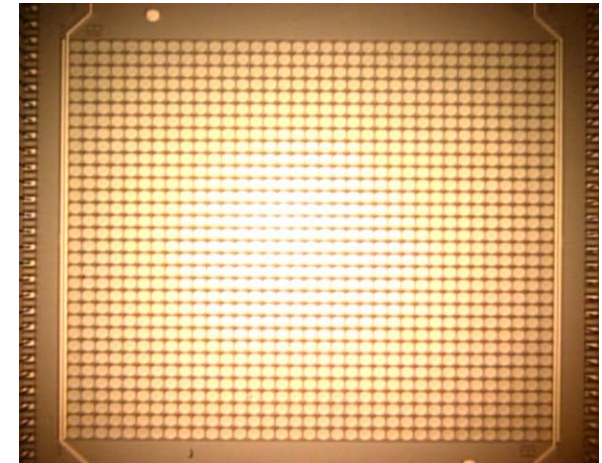


East mean= 1.500 std dev=**0.008**
with 1116 points
West mean= 1.508 std dev=**0.009**
with 1083 points
Combined East/West mean= 1.504
Flat mean= 0.049 std dev=0.020
with 1103 points

Angle Uniformity

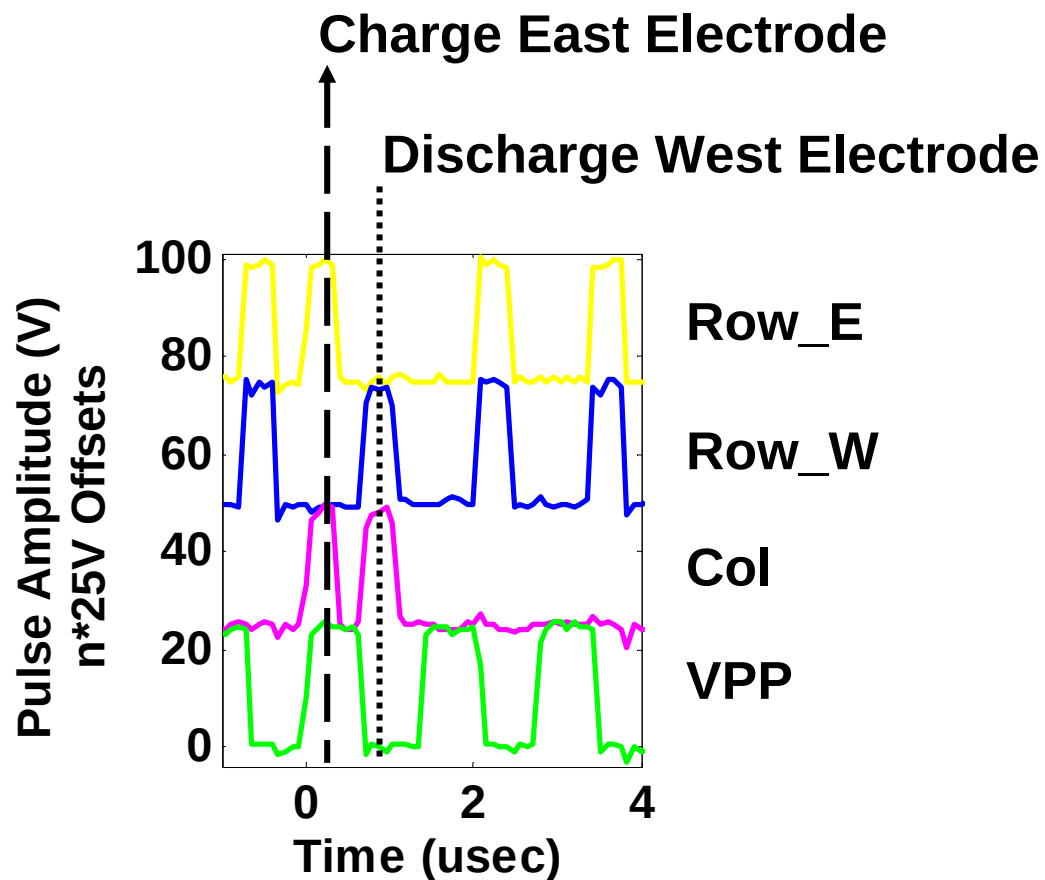
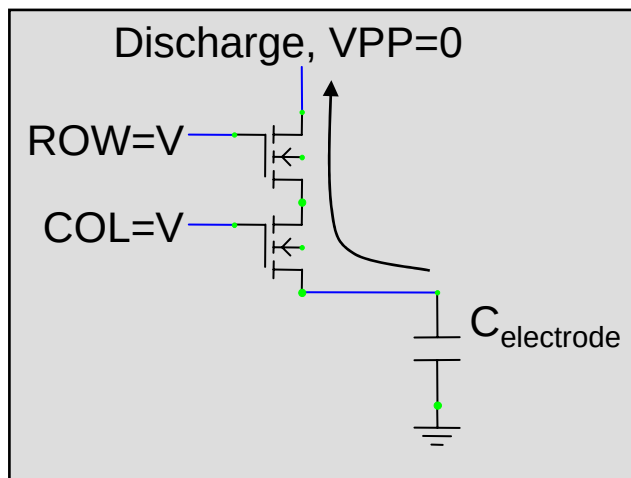
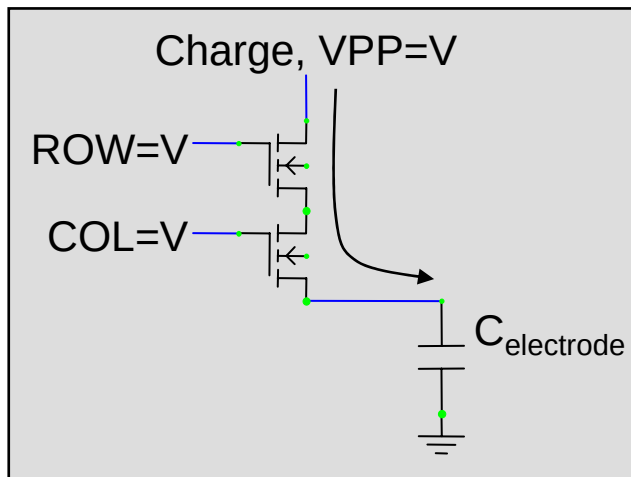


East mean= 1.438, std dev=0.010 with 1081 points
West mean= 1.439, std dev=0.010 with 1082 points
Flat mean= 0.005, std dev=0.022 with 1118 points

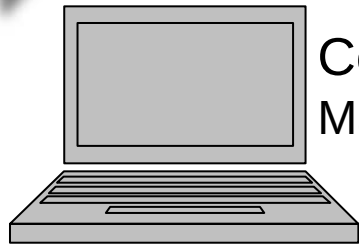


- Video capture of mirrors operating at 8ms/cycle (E-F-W-F)
- Stuck mirrors released by mechanical shock
- Vdd=25V, Vsub-4V

2-Transistor per Electrode Single-ended Drive

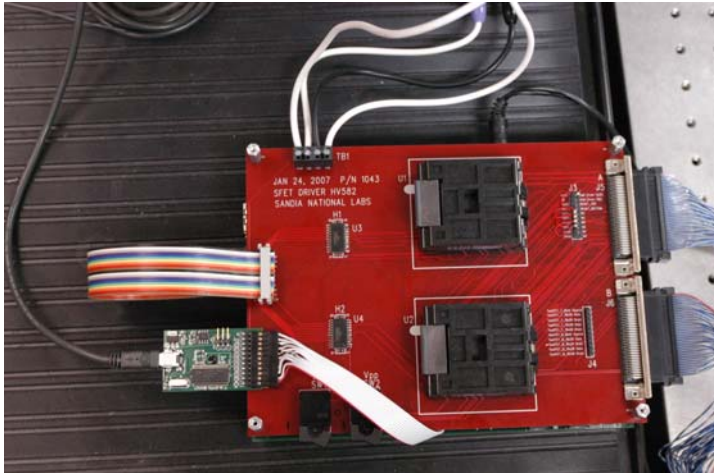


Beam Switching Mirror Demo

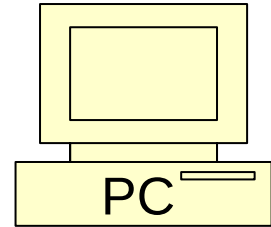


Control PC
Matlab w/USBee Interface

Power Supplies



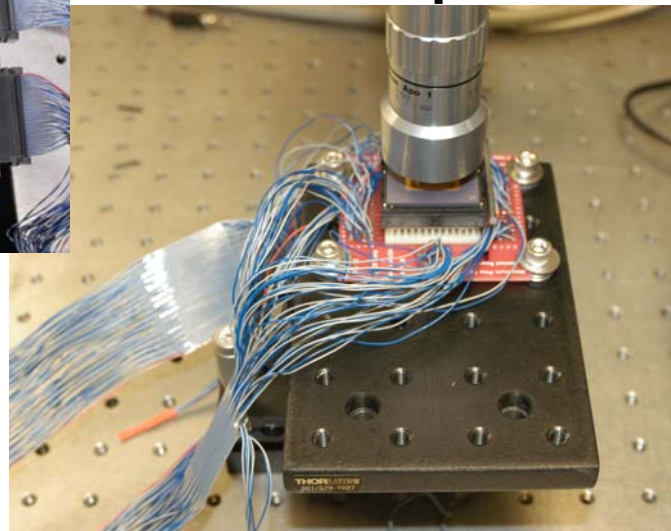
FPGA Demo Board
(not visible) and
Level shift circuitry



PC

Video Capture

Microscope
Camera



SFET Mirror Video





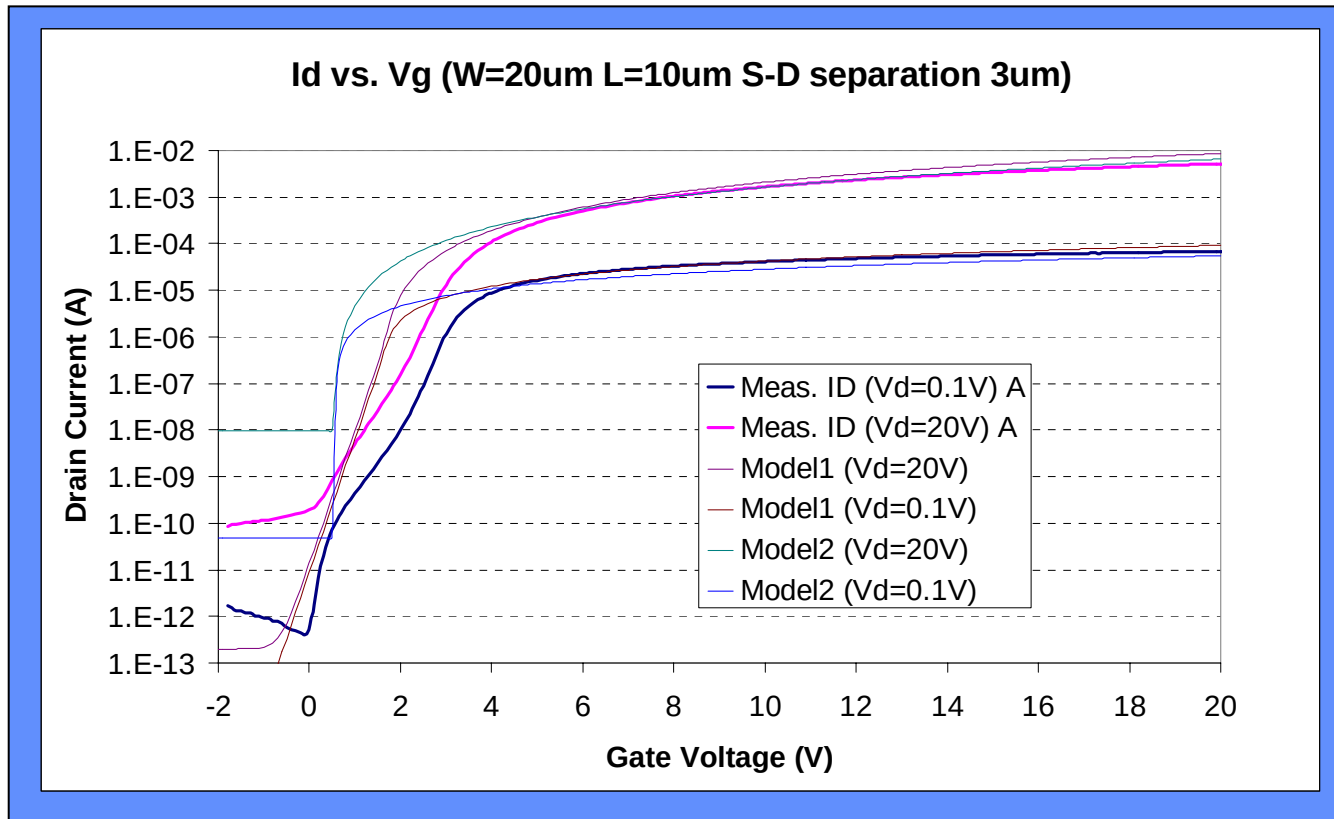
Summary

- **Ganged beam steering mirrors show promise for fast, incoherent beam steering**
 - Initial angle uniformity not bad
 - Improvement expected through device modeling and designs to minimize process-induced variations
- **Position repeatability of lever mirrors improved by eliminating actuator mechanical contact**
- **Improved understanding of large mirror dynamics**
- **Large mirrors w/ acceptable flatness achievable**
 - 850 μ m mirrors across ~8mm aperture demonstrated
- **SFET solves pin-out problem for large scale arrays**



Backup Slides

SFET Characteristics and Model



- Both models OK when transistors are “ON” ($V_g > \sim 5V$)
- “OFF” transistor leakage current is under-predicted by Model1
- “OFF” transistor leakage current is over-predicted by Model2
 - *Used for all SPICE circuit simulations to date*



SFET Design Considerations

- Transistors consume layers up through Poly12
- Transistor size and spacing rules limit the circuit functionality that can be implemented in a given unit cell size
 - Nominal $10\mu\text{m} \times 20\mu\text{m}$ gate SFET area $\sim 576\mu\text{m}^2$
- MEMS electrode and actuator structures must accommodate transistor footprint
- Two approaches for densely packed mirror arrays
 - Transistors under electrodes or beside electrodes
 - Minimum array mirror size $\sim 100\mu\text{m} \times 100\mu\text{m}$
- SFETs are photosensitive – must shield from light in operation
- Only NMOS transistors available limiting circuit configurations
 - *Think 70s era NMOS-only circuitry*
- Despite limitations SFET offers tremendous potential for micromirror array scale up, localized sensing/amplification & novel detectors

Addressing Schemes

Use pulse-width modulation or charge control for pseudo-analog positioning

- Piston mirror examples demonstrate this approach
- Number of mirror positions, array size & switching speed dictate off-chip signal requirements
 - Limited by on-chip switching speed

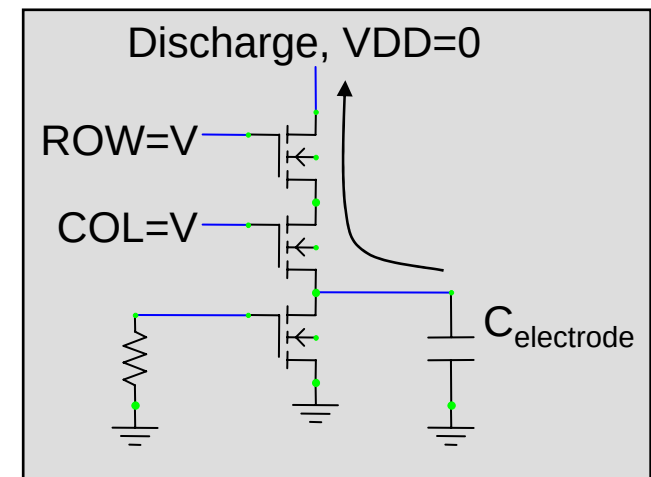
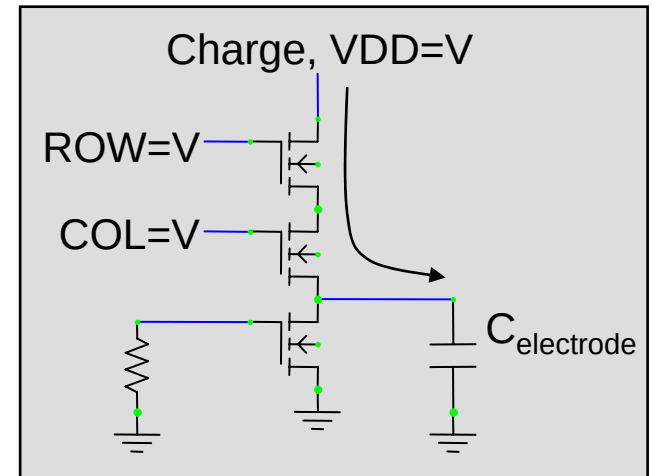
Single-ended drive of On-Off electrodes

- Fill and empty the bucket through the same hose
- VDD a control signal rather than a DC source
 - When $VDD=V$ & ROW & COL electrode charged
 - When $VDD=0$ & ROW & COL electrode discharged
- Demonstrated on 4x5 tri-stable mirror arrays
- SPICE simulation for 35x64 electrodes
- Allows reset transistors to be eliminated

Analog control of ROW (COL) gate signals

- Allows faster update and slower refresh cycle
- Requires sufficient transistor uniformity
- Works in SPICE simulations but untested

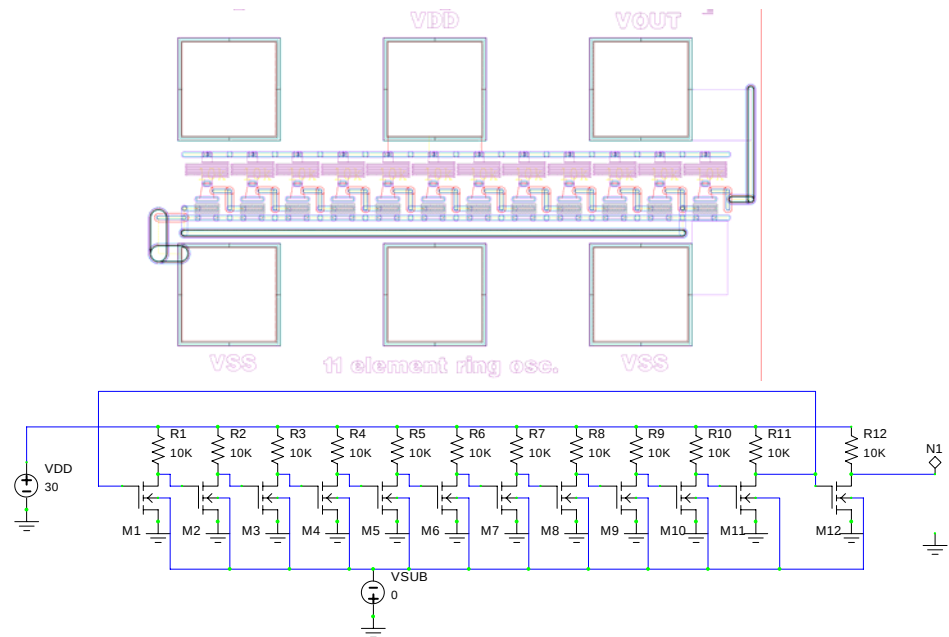
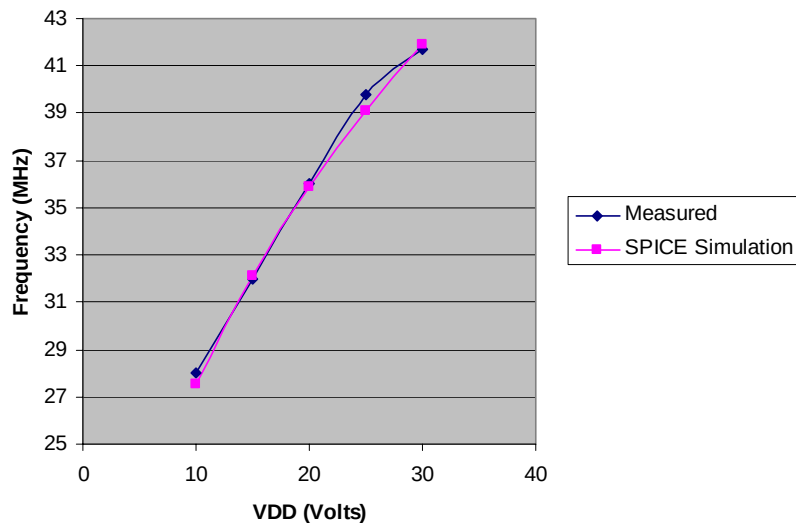
Single-ended Drive



SFET Ring Oscillator

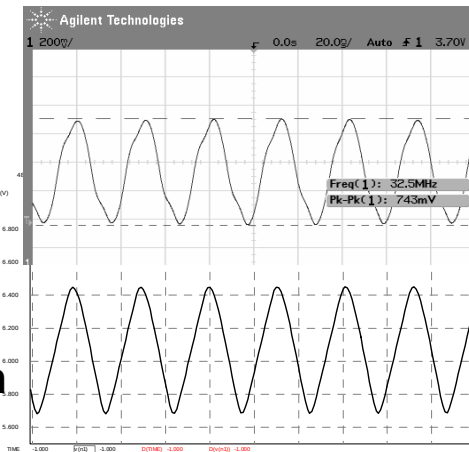
- 11 stage ring oscillator
 - Nominal 10x20 SFETs
 - 10KOhm pull-up resistors
- Measured data shows >40MHz switching at 30V
- Results used to tweak SFET model
 - Increasing C_{gdo} and C_{gso} from 700pf to 1600pf provided good simulation match to data

11-Stage Ring Oscillator Measured vs Simulated



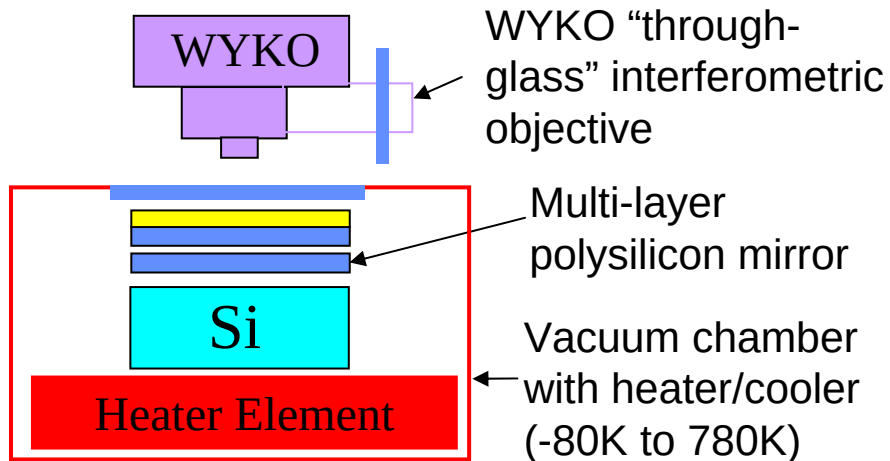
Data

SPICE
Simulation

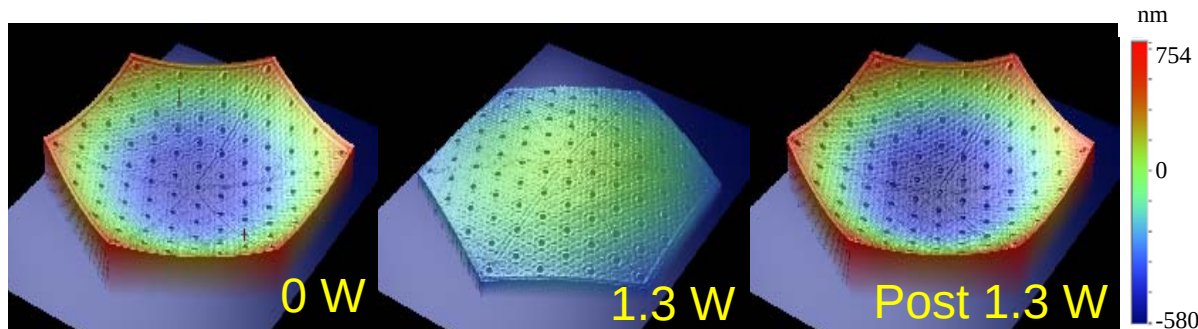
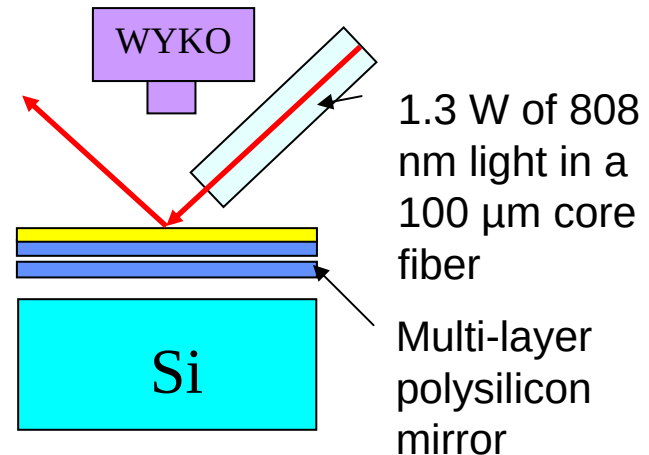


Temperature & High Optical Power Effects

Ambient



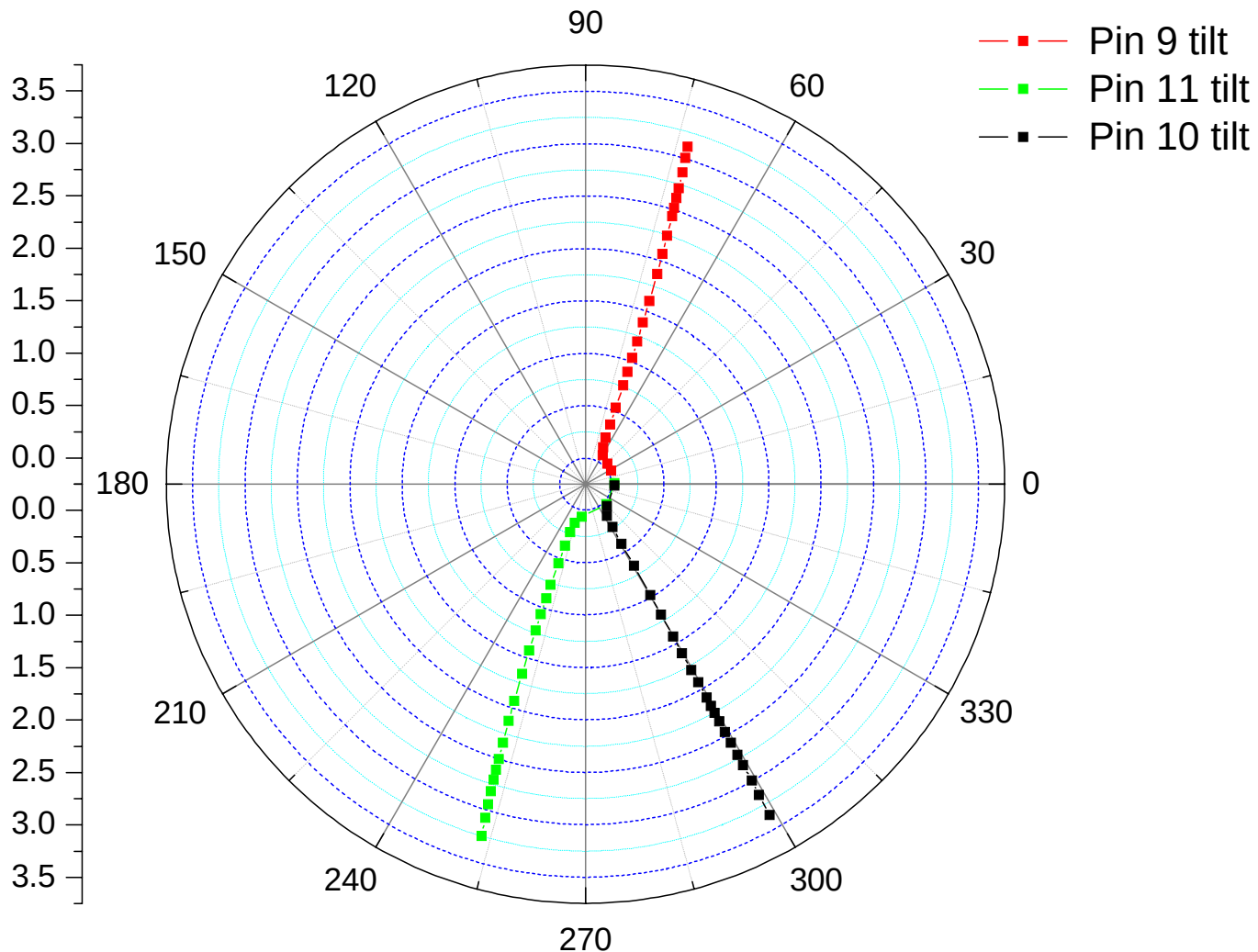
Laser Heating



Laser heating results for 1.3 W (2.8 kW/cm^2)

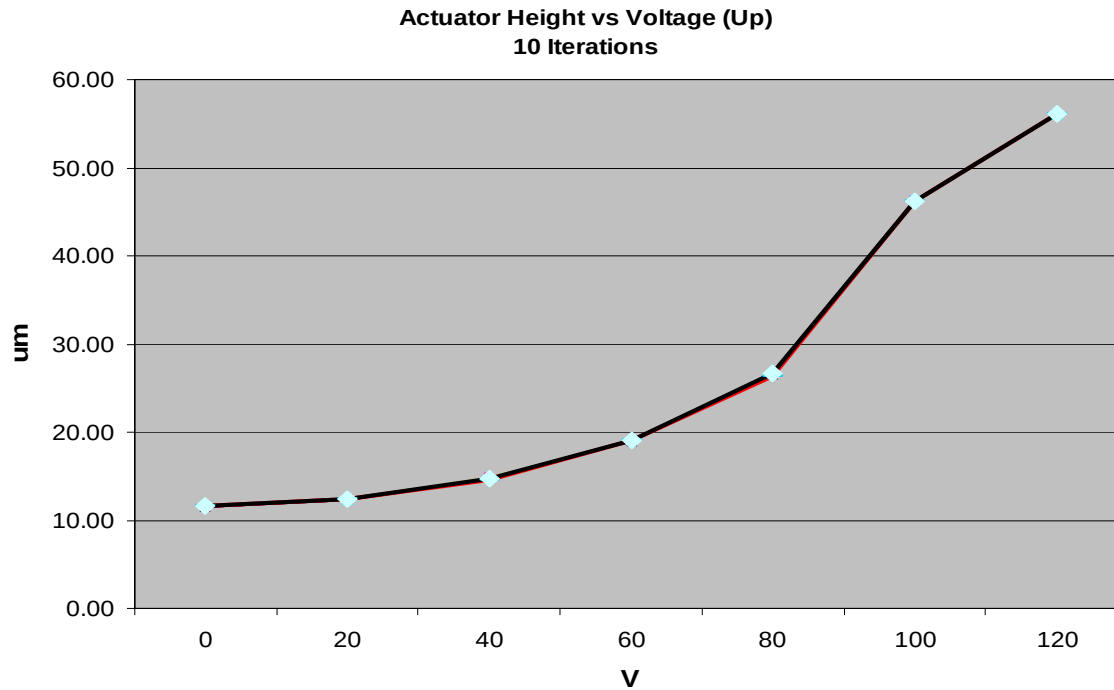
*Permanent deformations have been observed
for both gold and aluminum mirrors*

Diagonal tilt of ganged mirror array – polar representation



Repeatability: 1 Up

L1



Voltage	σ
0	6.77E-02
20	6.30E-02
40	8.06E-02
60	5.36E-02
80	6.13E-02
100	6.26E-02
120	7.69E-02

Avg = 6.65E-02 um

- 10 Iterations
- 2 down → 1 up
- 6 samples across 0-120V

RMS roughness (w/curvature)



Mag: 5.2 X

Mode: PSI

Surface Data

Surface Statistics:

Ra: 23.79 nm

Rq: 29.73 nm

Rz: 211.83 nm

Rt: 226.07 nm

Set-up Parameters:

Size: 736 X 480

Sampling: 1.62 um

Processed Options:

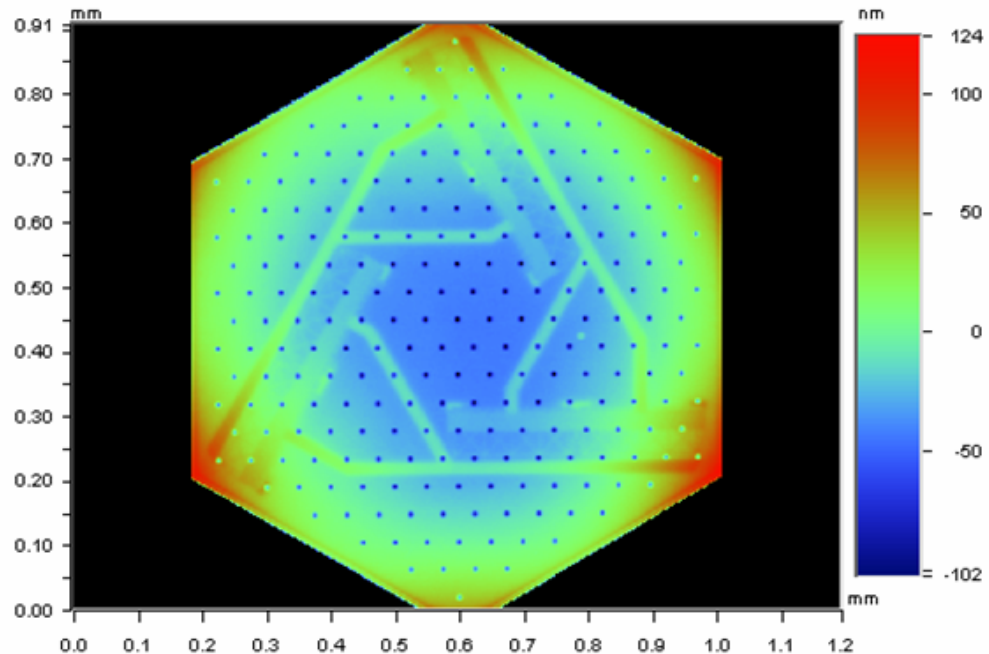
Terms Removed:

Tilt

Filtering:

None

rms
roughness
(includes
ROC)



Title: H850_L1 ctr Al

Note: id6436 std P4

RMS roughness (w/o curvature)



Mag: 5.2 X
Mode: PSI

Surface Data

rms
roughness
(curvature
removed) —
Remaining
major
contributor is
print through
(~23 nm
peak-to-
valley)

Surface Statistics:

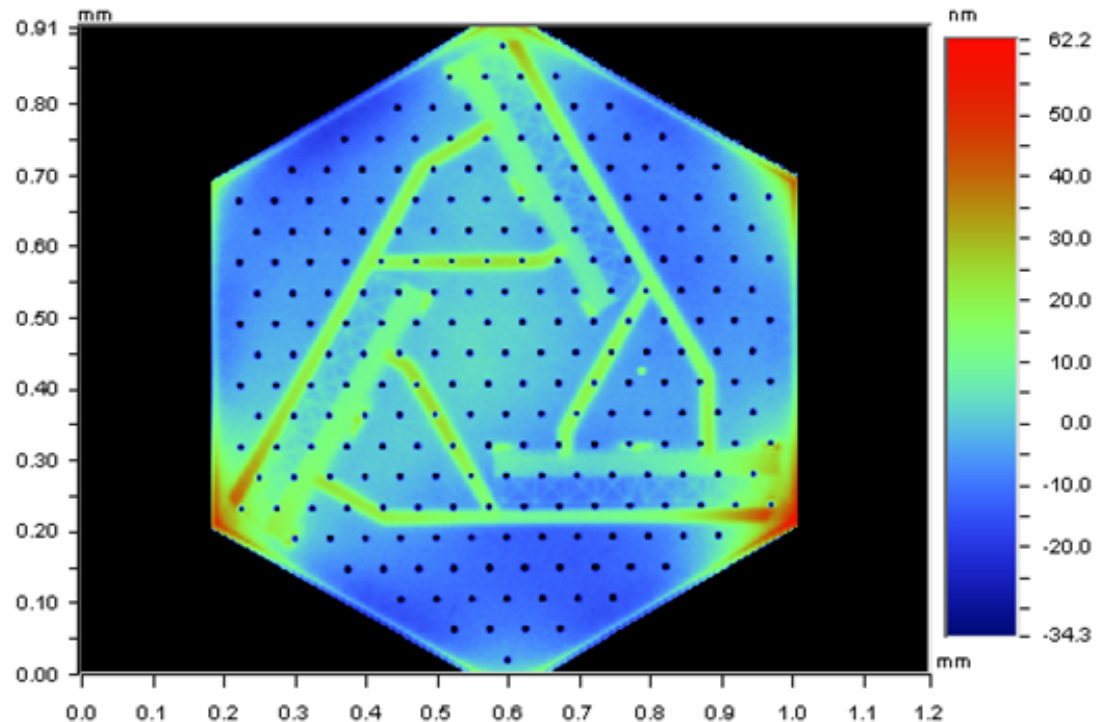
Ra: 7.96 nm
Rq: 10.55 nm
Rz: 86.13 nm
Rt: 96.49 nm

Set-up Parameters:

Size: 736 X 480
Sampling: 1.62 μm

Processed Options:

Terms Removed:
Curvature & Tilt
Filtering:
None



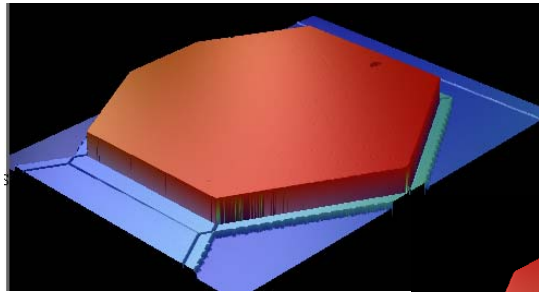
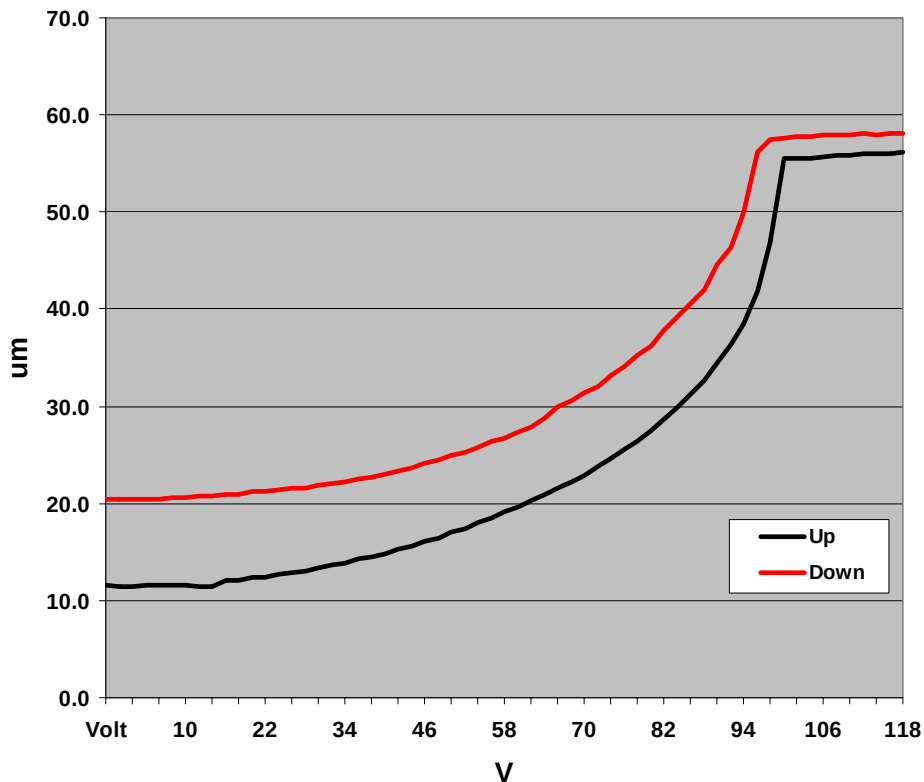
Title: H850_L1 ctr Al
Note: id6436 std P4



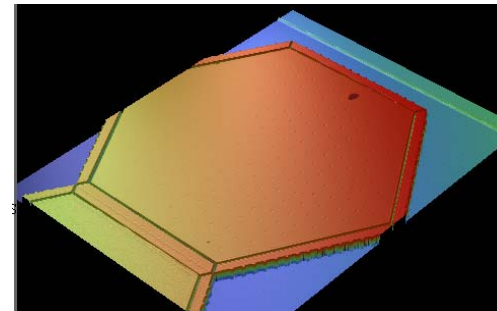
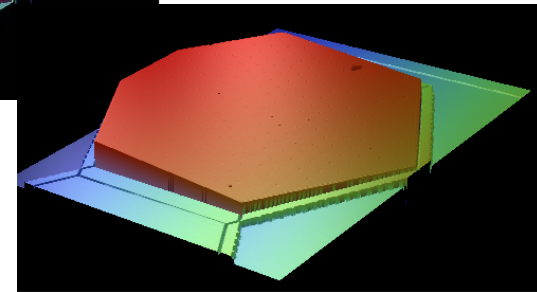
Voltage vs Deflection

*Single (varying) actuator.
 Δ is indicative of mech.
Interference.*

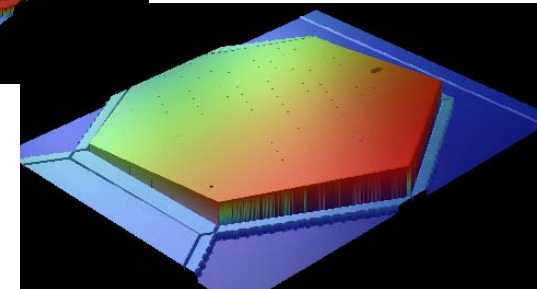
Actuator Height vs. Voltage



Up $\rightarrow$ Down
 $\Delta = 370\text{m}$

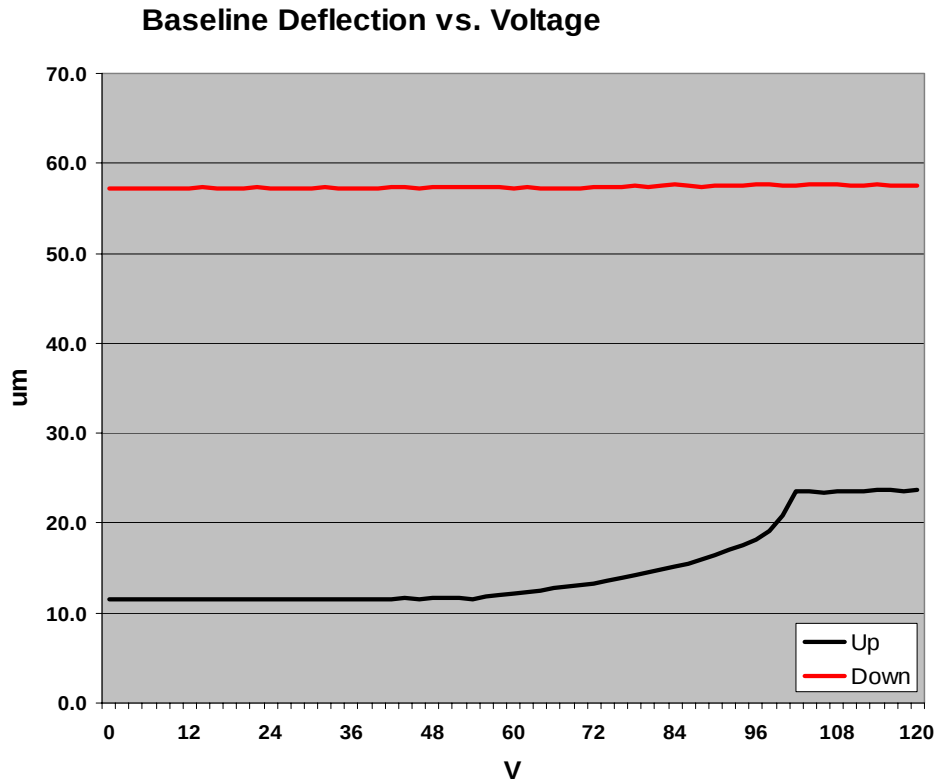


Down $\rightarrow$ Up
 $\Delta = 440\text{m}$



Mechanical Interference

L1



← Actuators Up

← Actuators Down

Repeatability: Static

- N = 10 measurements. Manual (lateral) displacement between measurements.
- Results are a quantitative measurement of our ability to infer height over an array. → Not good, but not a problem for right now...

Max

R01	R02	R03
14.09	24.82	25.39
12.2	186	160

Min

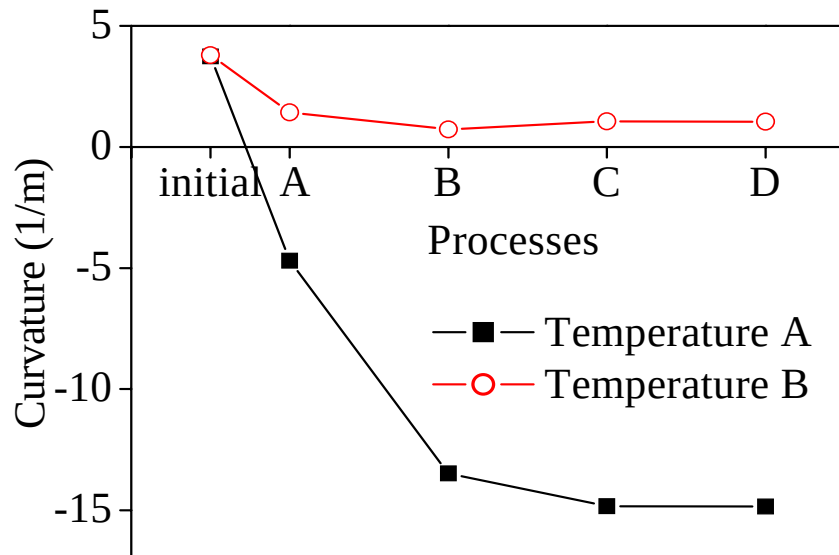
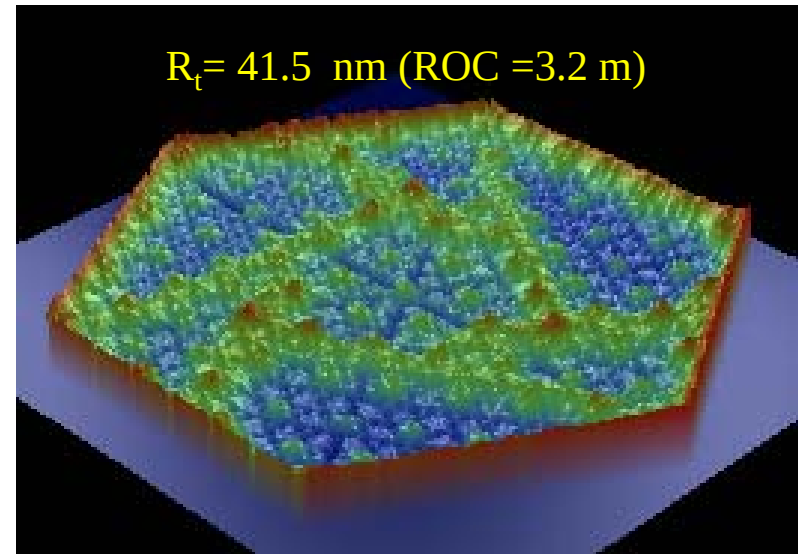
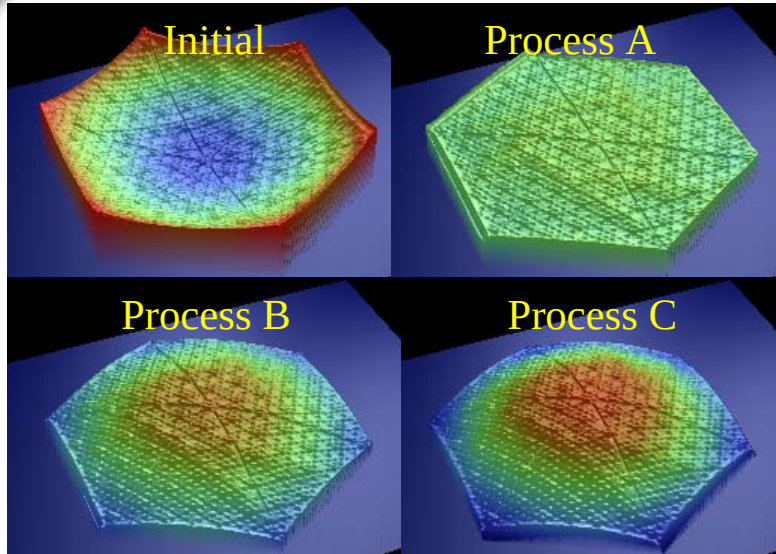
R01	R02	R03
13.2	12.31	12.53
470	470	480

Act #

Avg
(μm)

σ
(nm)

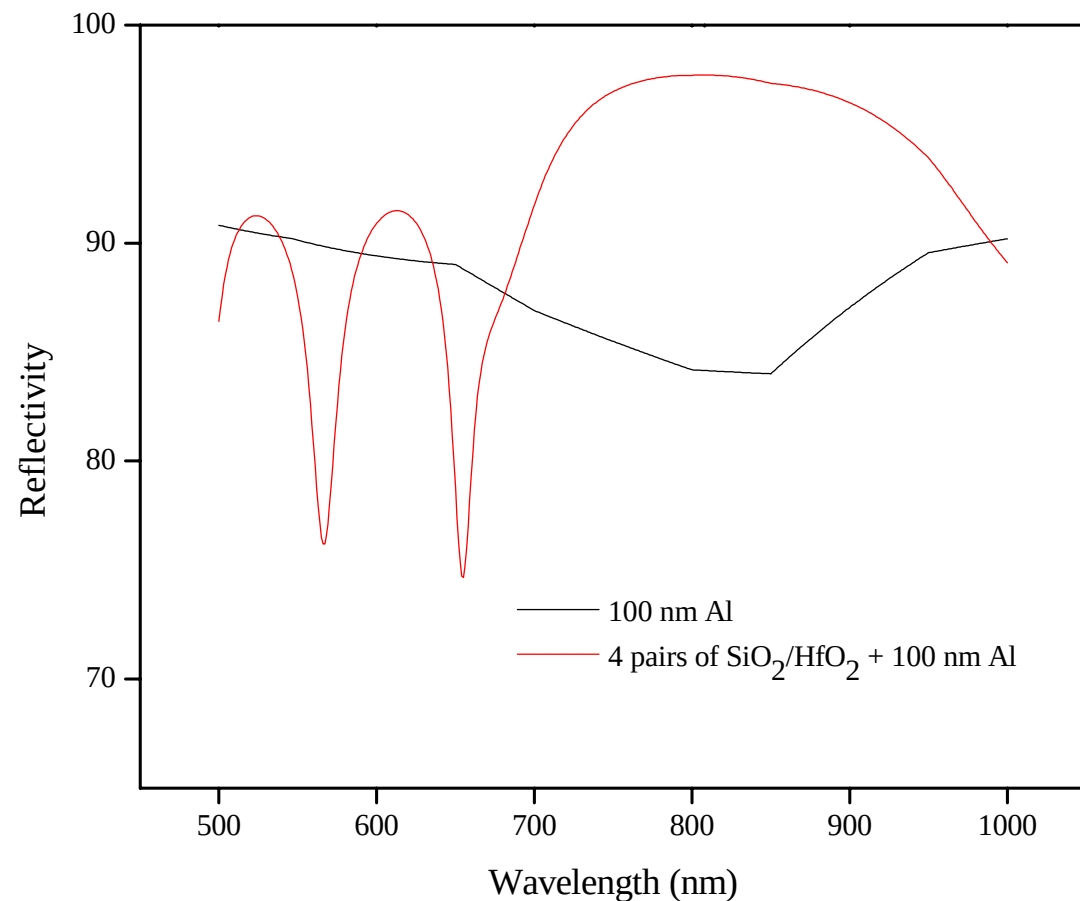
RTA Improves Mirror Surface Quality



Reinforced Mirror, Flattened by Process A

- Process A
 - Pre-release RTA
 - Five 30-sec cycles @ 1100C
- Results shown w/o metal
 - Drive convex with RTA
 - Allow tensile metal to flatten
- Transfer to fab pending

Reflectivity of metallized (Al) MEMS mirror with and without dielectric layers



Absorbance at 808 nm = 2.3 %
for dielectric + Al coated mirrors
vs. 15.8 % for Al only coated
mirrors

