



DEVELOPMENT OF A 6.25 MV LASER TRIGGERED GAS SWITCH FOR THE REFURBISHED Z DRIVER

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**K.R. LeChien, M.E. Savage, W.A. Stygar, P.E. Wakeland, V. Anaya, D.
Artery, D.E. Bliss, J.P. Corley, A.S. Downie, J.A. Lott, J.J. Lynch,
S.D. Ploor, J.R. Woodworth**

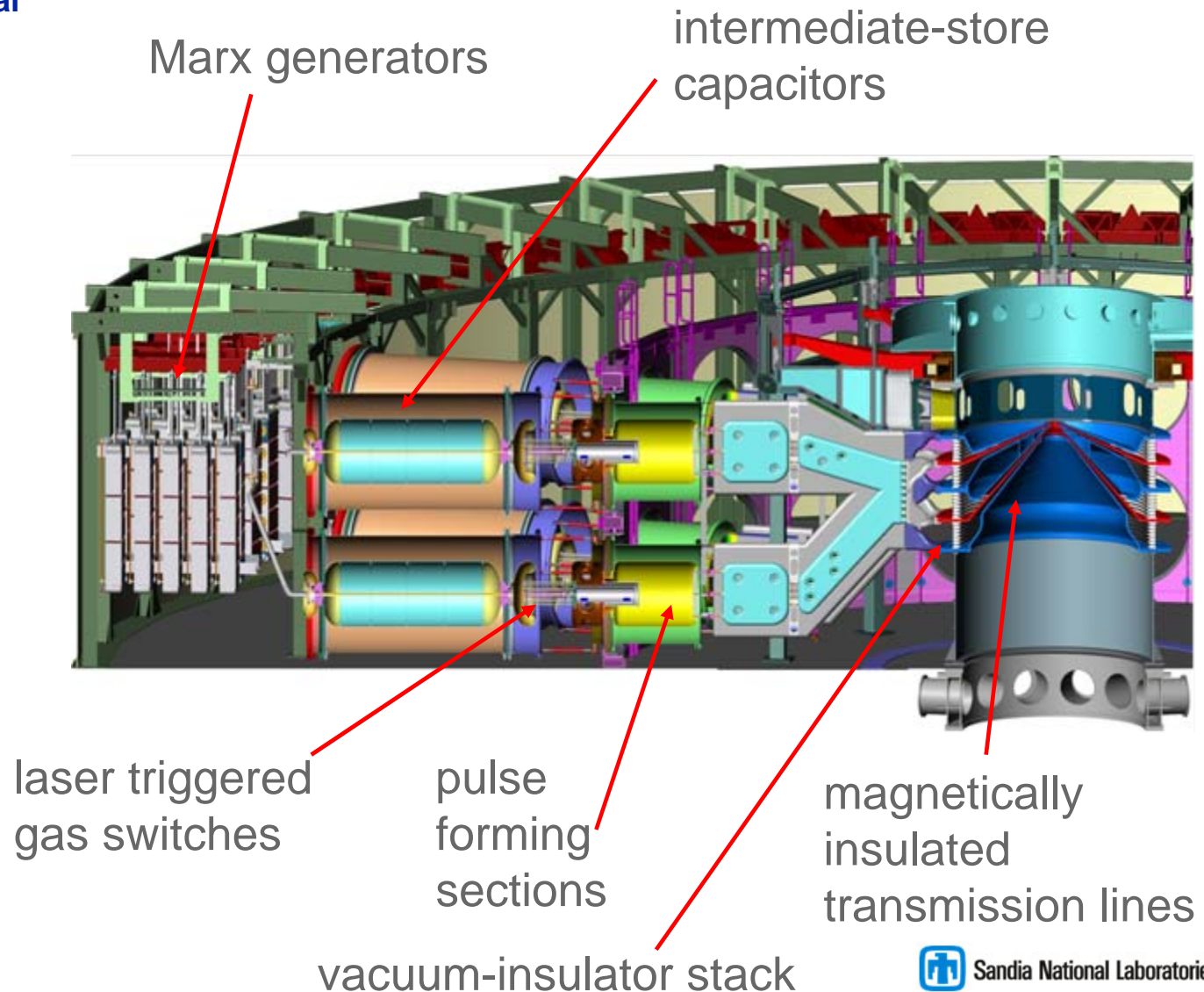


The thirty-six module Z pulsed power system applies 9 MJ of forward going energy in ~ 100 ns with nanosecond accuracy

All Z pulsed power components were replaced between July 2006 and September 2007

A Z shot begins with a 5V signal from the control system:

- A system of trigger generators amplify the trigger pulse to 600 kV
- The Marx generators are discharged in $1.2 \mu\text{s}$, charging the intermediate storage water capacitors
- The laser-triggered gas switches control discharge of the intermediate store capacitors with ~ 5 ns accuracy
- The water switches discharge the pulse-forming line in 115 ns with 2 ns accuracy
- Load current rises in 115 ns to 26 MA





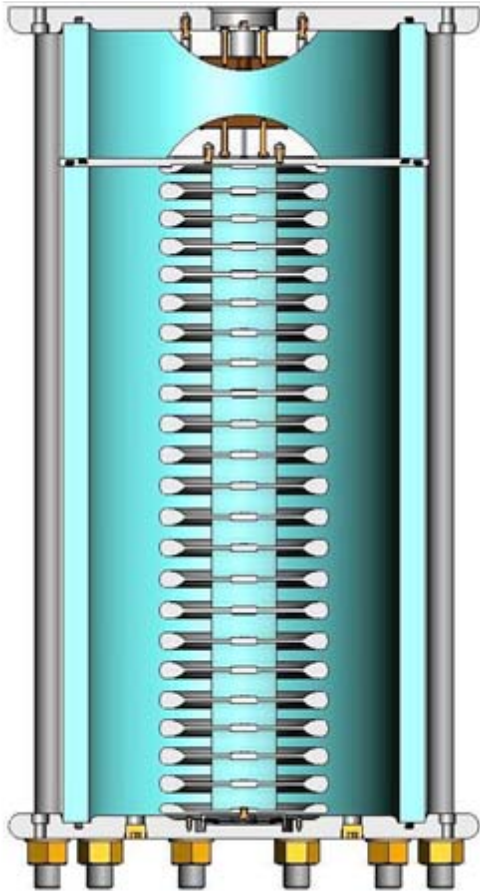
System performance is highly dependant on gas switch operation

- **Forward going wave jitter < 1 ns and repeatability of peak current of $\pm 1\%$**
 - Implies less than 6 ns jitter for an individual switch
- **System reliability of 98%**
 - Implies less than a 0.03% probability of individual switch prefire or late fire
- **To obtain 26 MA in 115 ns (wire array load of 20 mm radius, 20 mm long)**
 - Switch voltage: 6.1 MV
 - Switch current: ~ 800 kA
- **Desired maintenance interval: > 150 shots**

A three-year research effort led to the development of gas switches that meet system performance goals

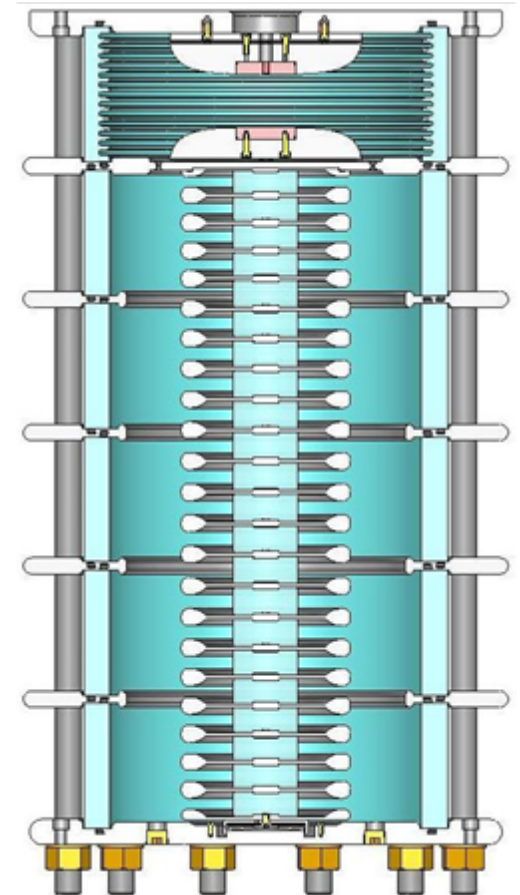


Reducing shot-dependant failure modes has been the biggest challenge to providing a suitable switch



June 2005

- **Flashover of insulators**
 - Erosion of electrodes
 - Insulator design
 - Cleaning procedures
- **Prefires/no-fires due to limited life components**
 - Enhancements due to erosion
 - Optic degradation

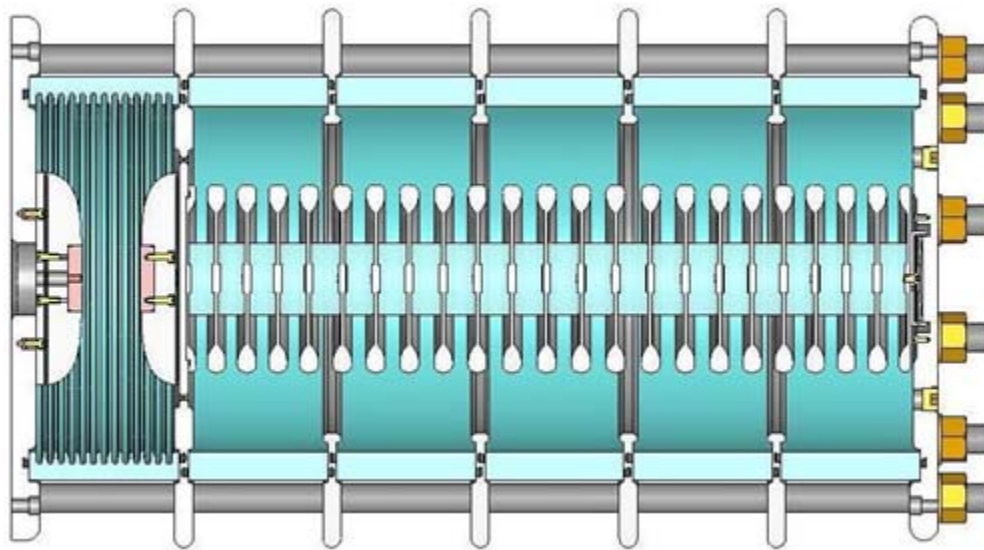


June 2008



The present gas switch design will meet near term Z performance goals

performance parameter	original ZR gas switch (5.0 - 6.25 MV)	ZR-A-3 gas switch (6.25 MV)
prefire rate	7%	< 0.1%
jitter	13 ns	5 ns
flashover rate	5%	< 1%
replacement interval	< 30 shots	~120 shots

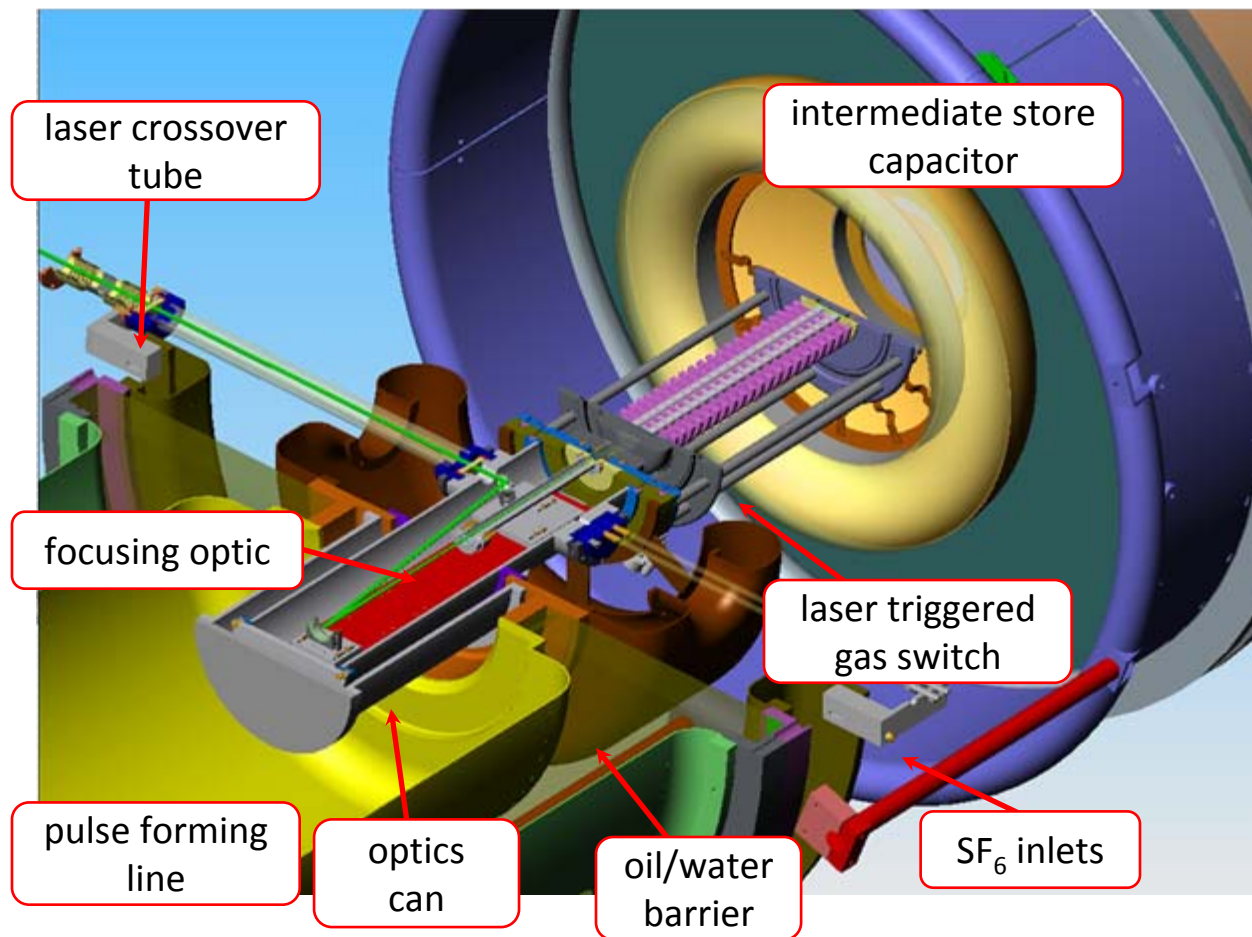


ZR-A-3
laser-triggered
gas switch



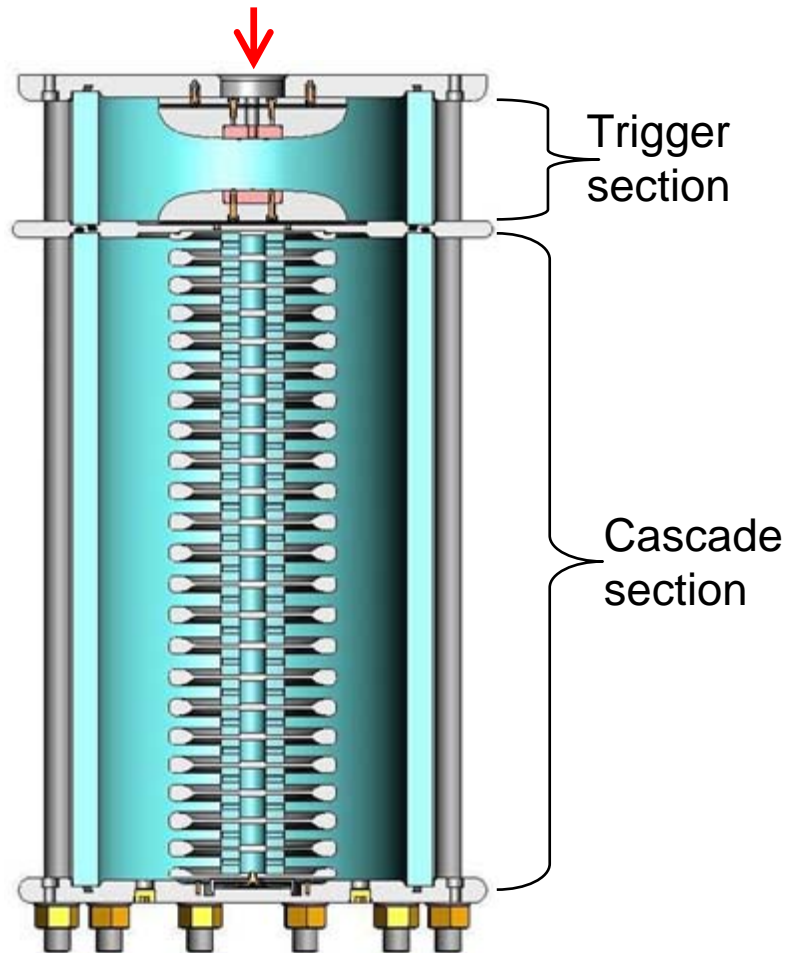
The laser triggered gas switch is the last command fired component in the system

- Each switch has a dedicated laser
 - Nd:YAG
 - $E = 35 \text{ mJ}$
 - $\lambda = 266 \text{ nm}$
 - $t = 4 \text{ ns FWHM}$
- Optical train
 - 6 mirrors, 3 windows, 1 lens
 - 11 m total optical path length





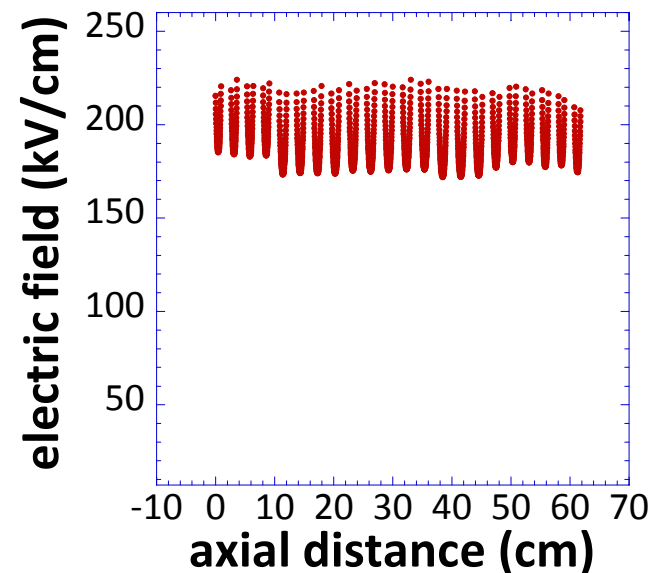
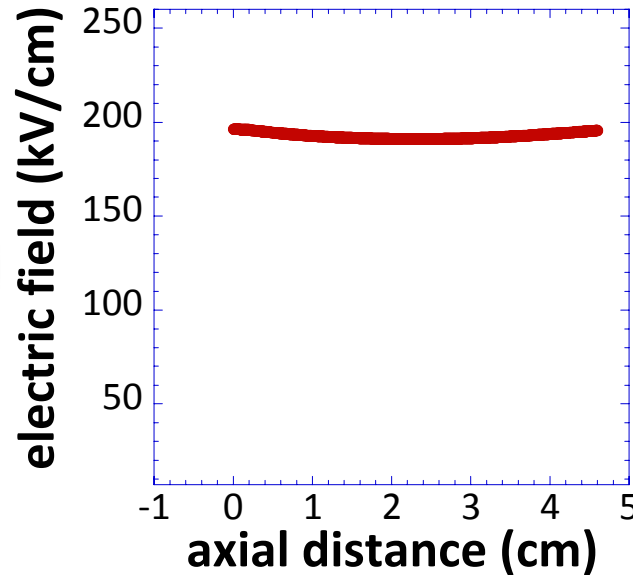
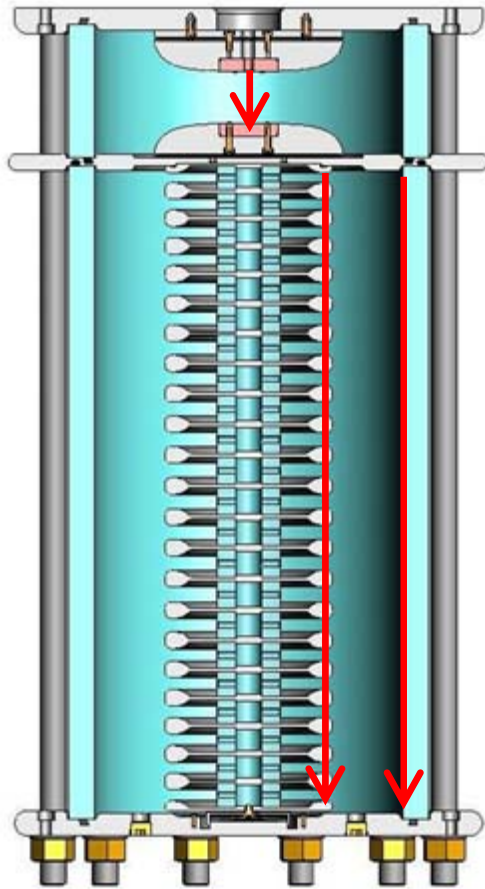
The gas switch is comprised of two series switches; One laser triggered and one electrically overstressed



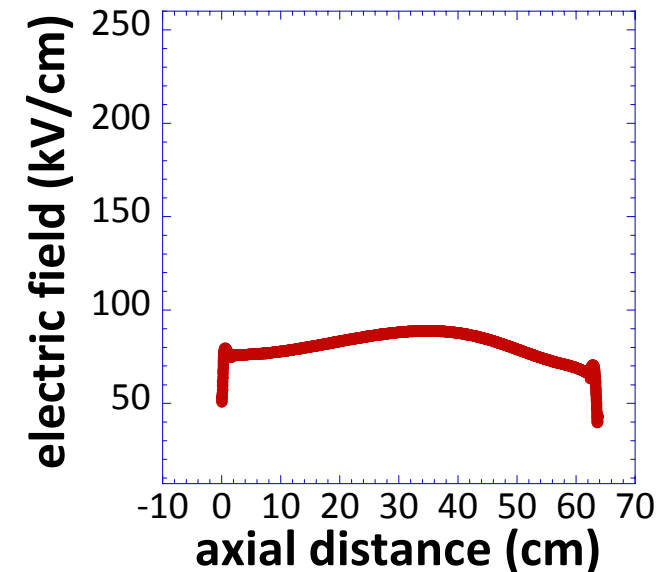
- ~15% of the total voltage is imparted to the trigger gap (~940 kV at 6.25 MV switch voltage)
- Cascade section closure relies on the overstress from the trigger gap
- Cascade section “multi-channels”
- Trigger section and cascade section share a common gas volume



The peak electric field is matched between the trigger and cascade sections before closure

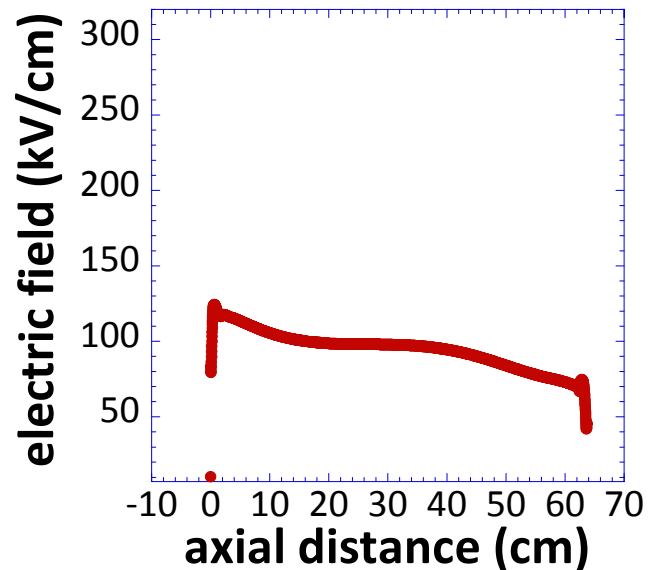
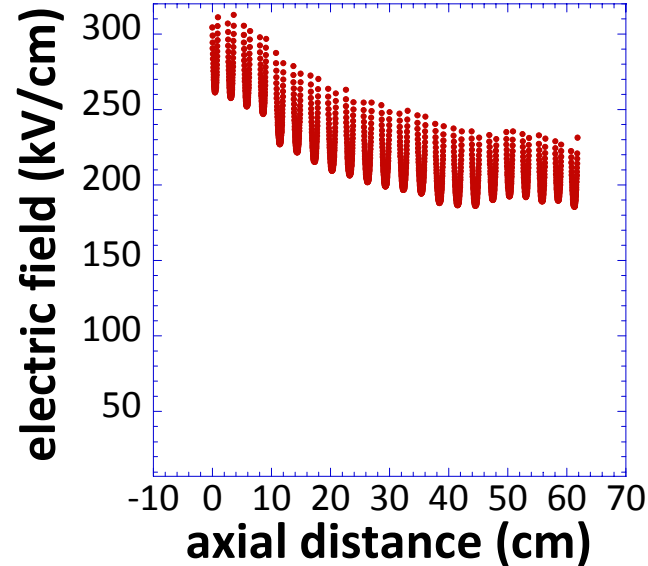
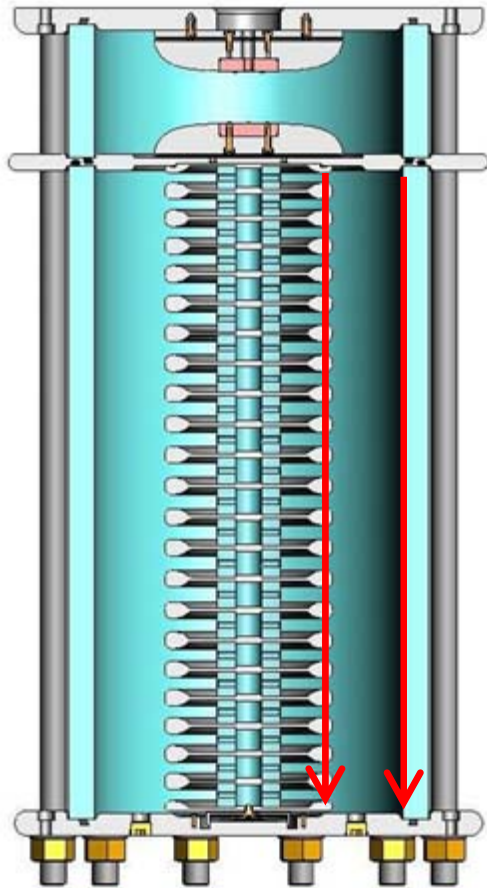


- Trigger gap field is uniform
- Cascade field is uniform
- Cascade insulator field is ~ 0.5 gap field





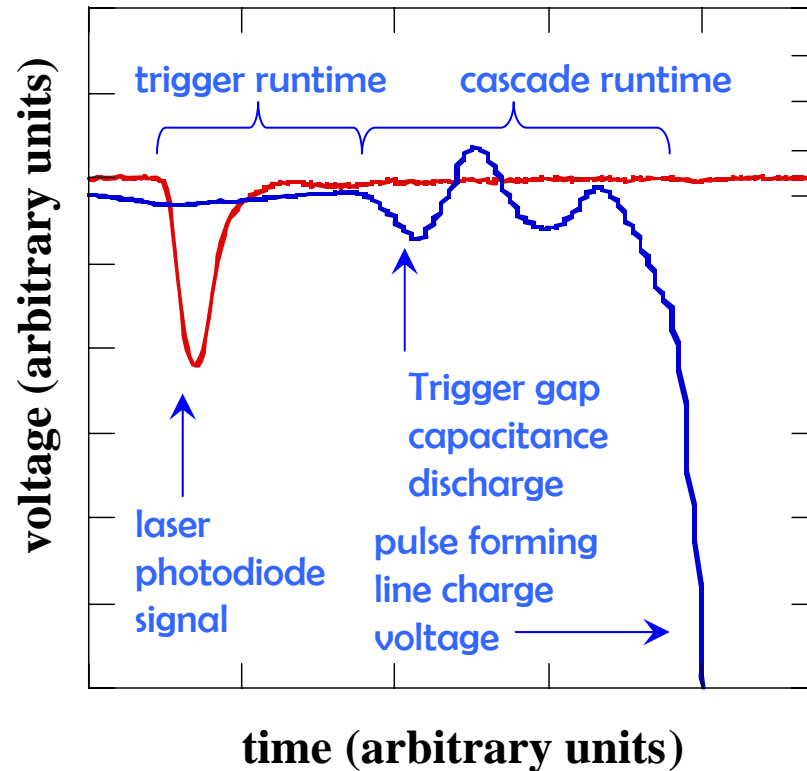
The peak electric field increases throughout the cascade section upon trigger closure



- Electric field magnitude increases approximately 45% when triggered
- Overstress wave is partially impressed on 18 of the 22 gaps



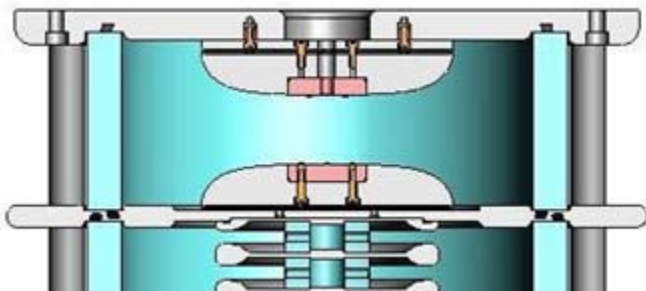
Electrical closure of the switch is monitored by voltage, photomultiplier, and streak camera diagnostics



- Runtime and jitter for the trigger and cascade section are fully identifiable.
- The ability to clearly observe each sections closure has led to major advances in our understanding of laser triggered gas switches in a multi-megavolt environment.
- Trigger section failure modes and cascade section failure modes are separable with these diagnostics



Trigger section



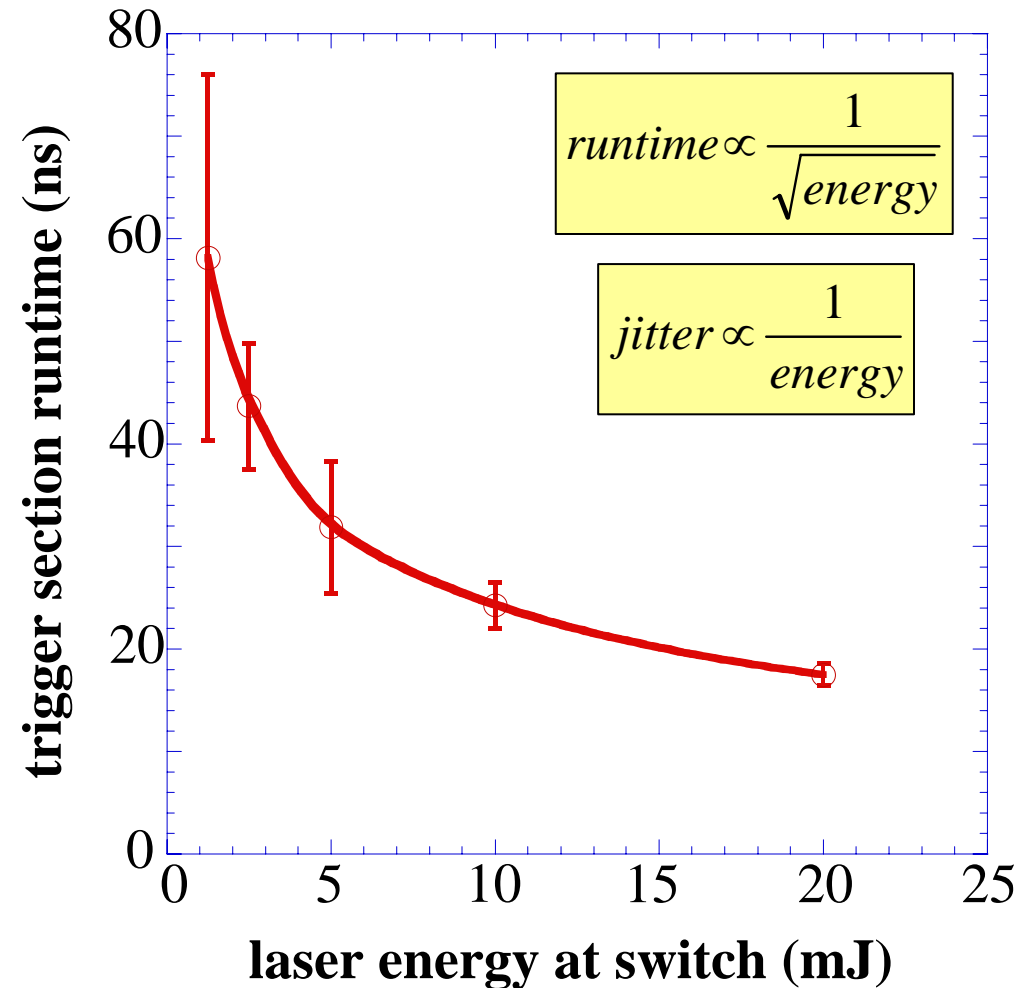
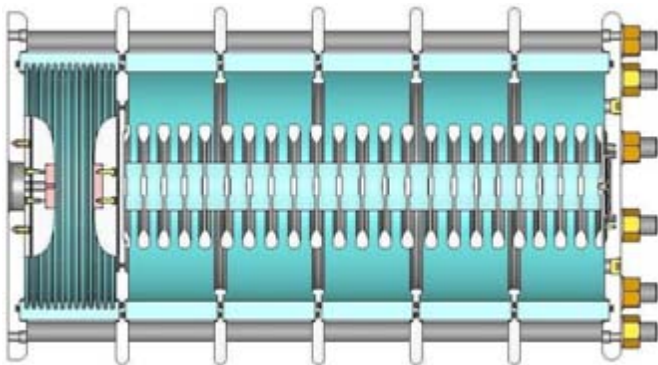
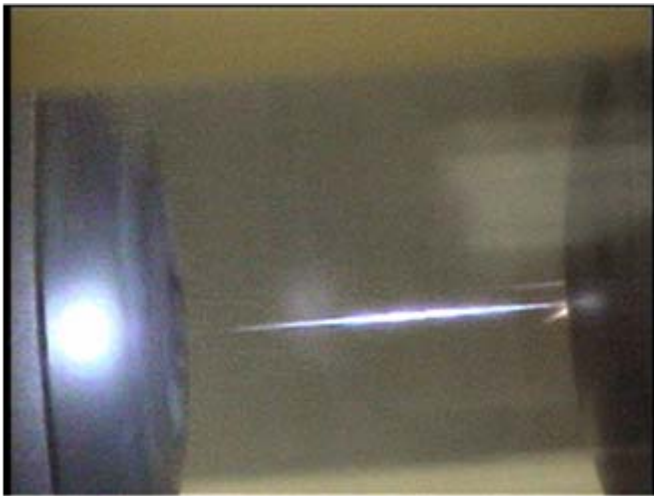
- Laser parameters
- Trigger electrode material (single channel)
- Optic line of sight





The trigger section is designed for sub-nanosecond jitter performance

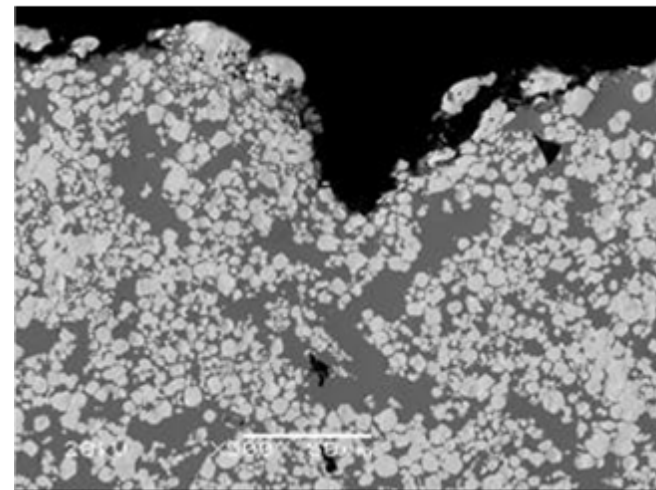
- **Trigger jitter is ~ 1 ns at a gap distance commensurate with a prefire probability of <0.01%**



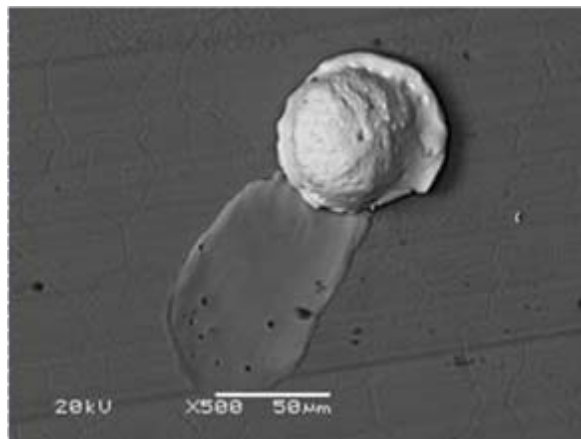


Appropriate selection of trigger electrode material led to suitable performance at 6.25 MV, 800 kA

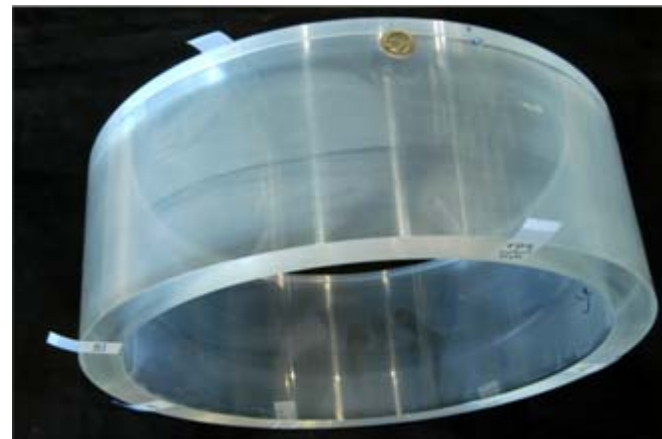
- The flashover rate was reduced an order of magnitude; from 8% with stainless steel to < 1% using Elkonite 50W3
- The lifetime of the final optic was increased by an order of magnitude; from 50 shots with Mallory 1000 to > 200 shots with Elkonite 50W3.



Molybdenum trigger electrodes: byproducts coated insulators and led to flashing (43 shots)



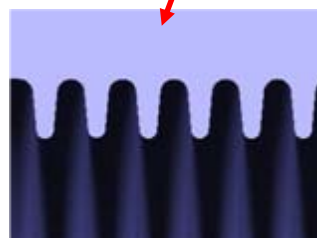
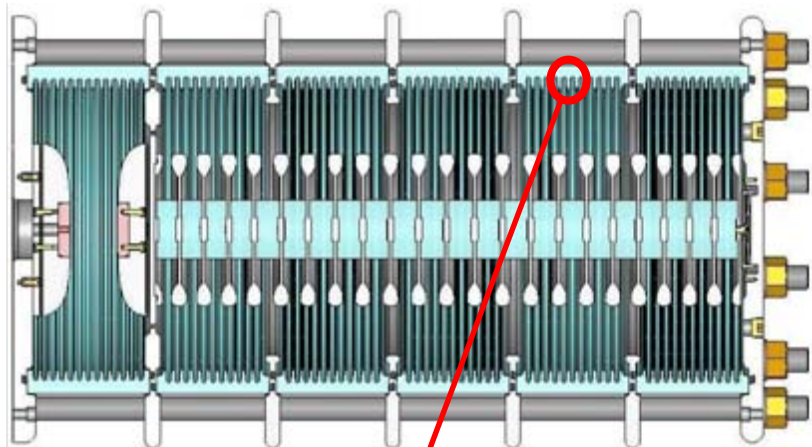
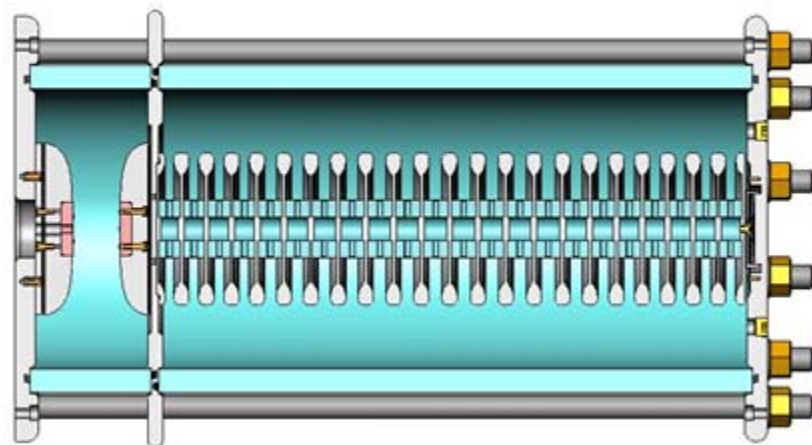
HD-17 Cu-W: electrodes material was deposited in large pieces and led to flashover (40 shots)



Mallory Cu-W: electrode material coated optics and reacted unfavorably with UV (30 shots)

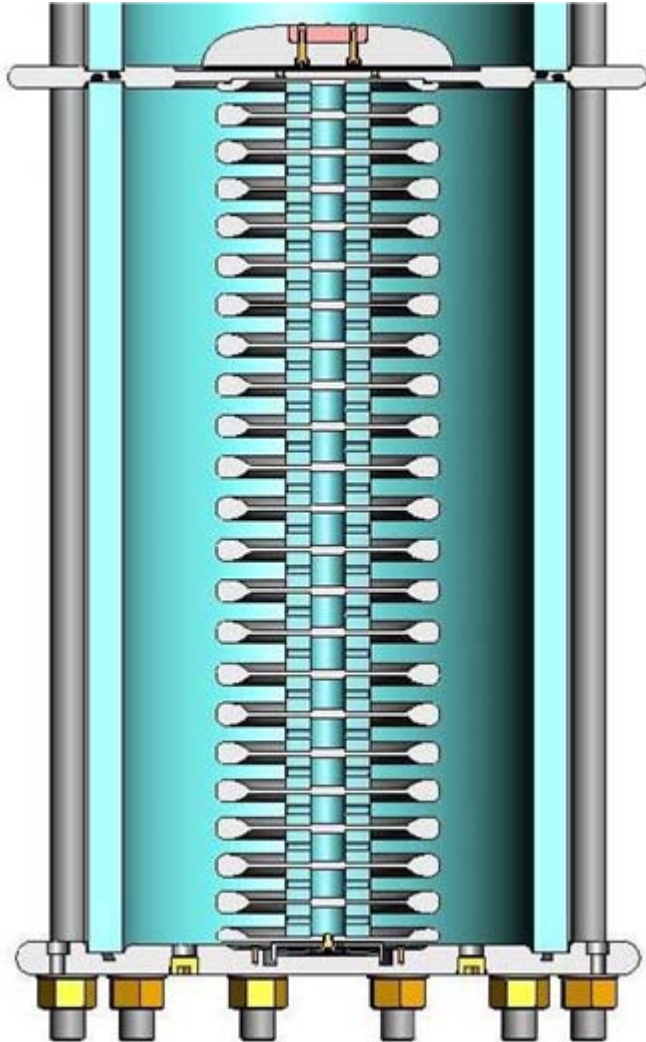


Scalloping and segmenting monolithic insulators increased reliable gas switch performance by two orders of magnitude

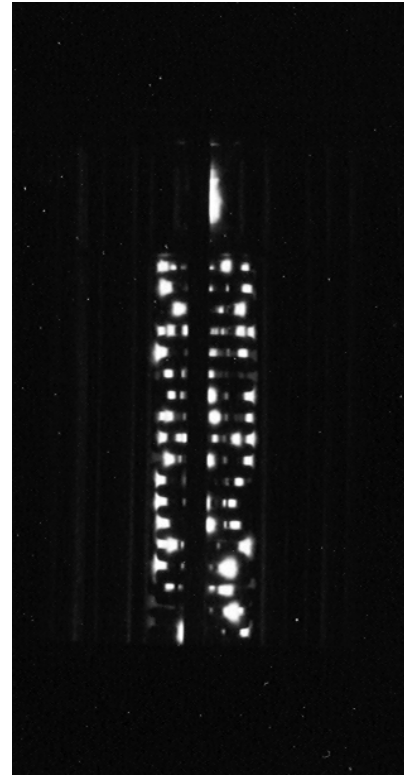




Cascade section

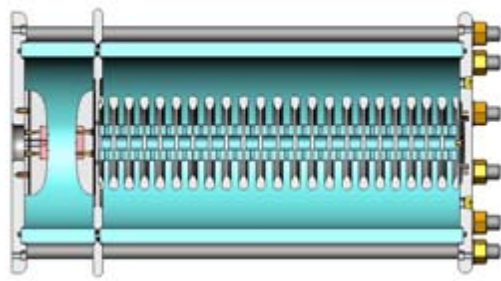
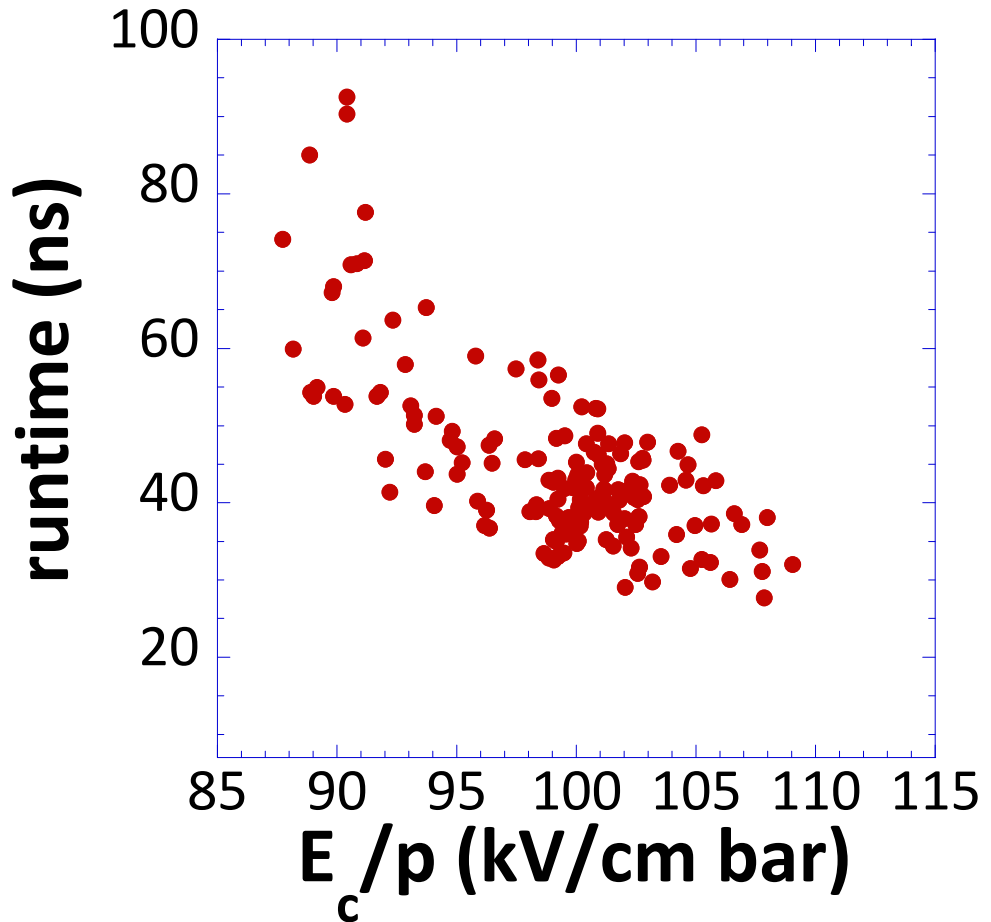
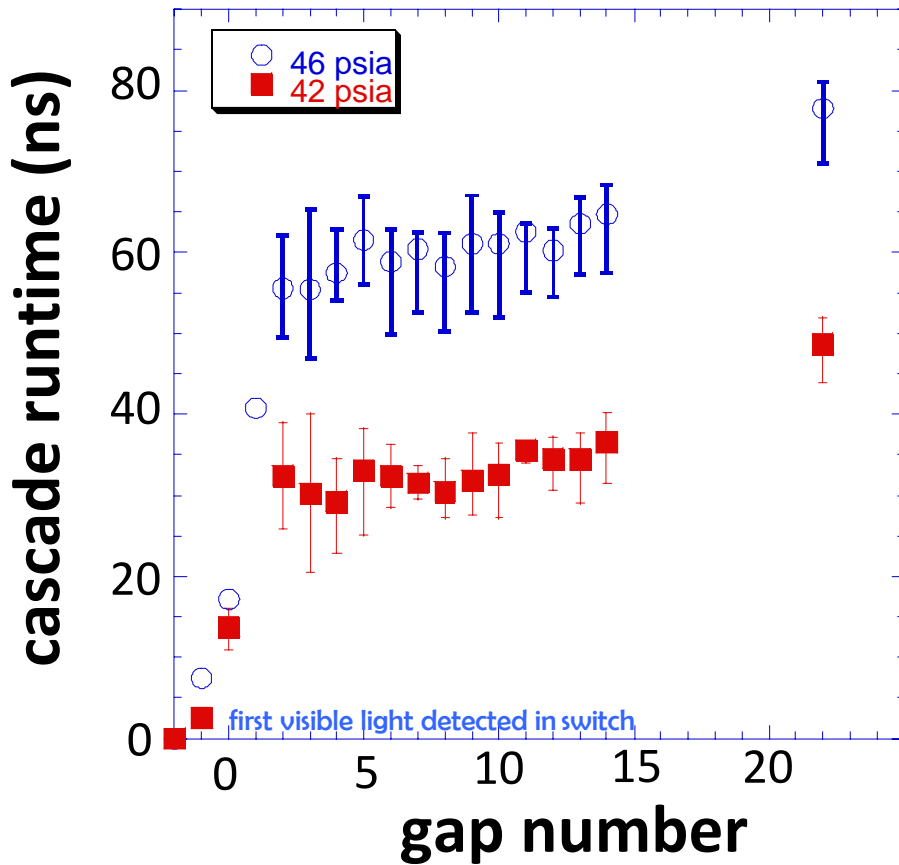


- Electrically overstressed
- Multi-channeling





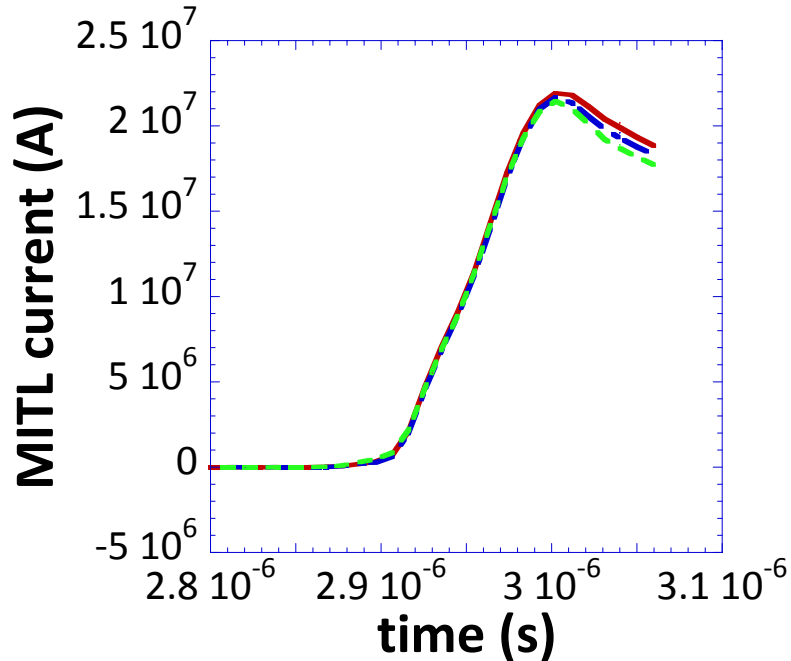
The magnitude of the overstress and the geometry of the switch determines the operation of the cascade section



- Cascade jitter is < 5 ns at a pressure commensurate with a prefire probability of $< 0.1\%$ at 6.25 MV

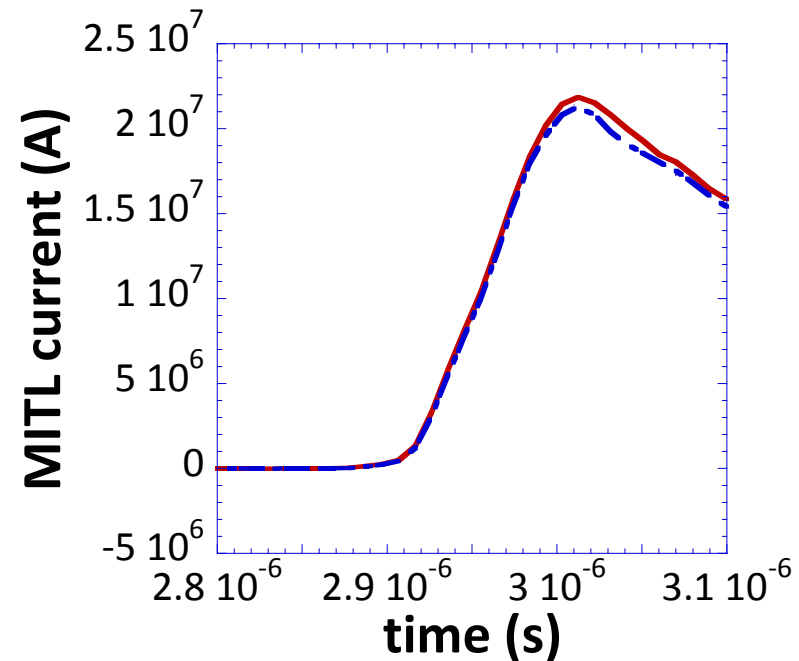


The MITL current jitter is of order 1 ns with the present gas switch design



$$\sigma = 0.401 \text{ ns}$$

- $V = 5.2 \text{ MV}$
- $P = 39 \text{ psia}$
- $E_c/p = 99 - 108 \text{ kV/cm bar}$



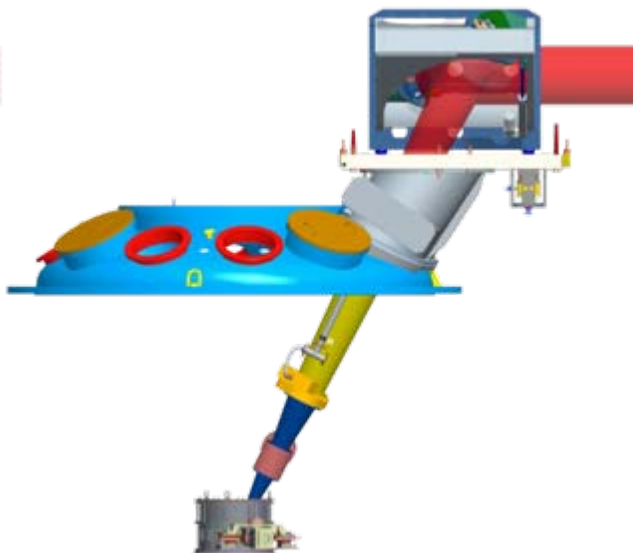
$$\sigma = 0.308 \text{ ns}$$

- $V = 5.2 \text{ MV}$
- $P = 39 - 42 \text{ psia}$
- $E_c/p = 100 \text{ kV/cm bar}$

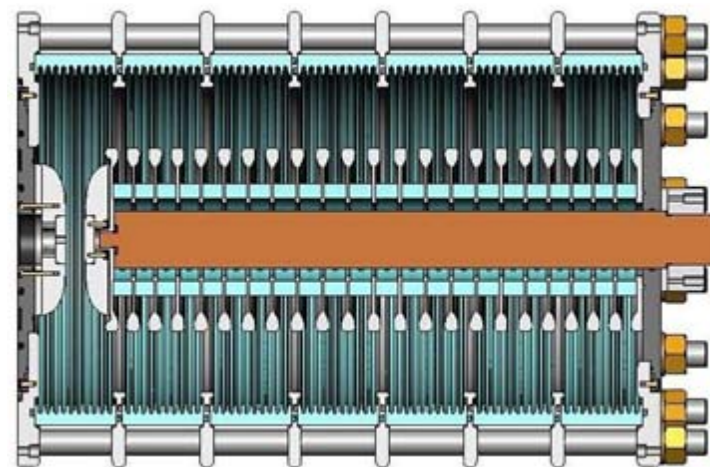
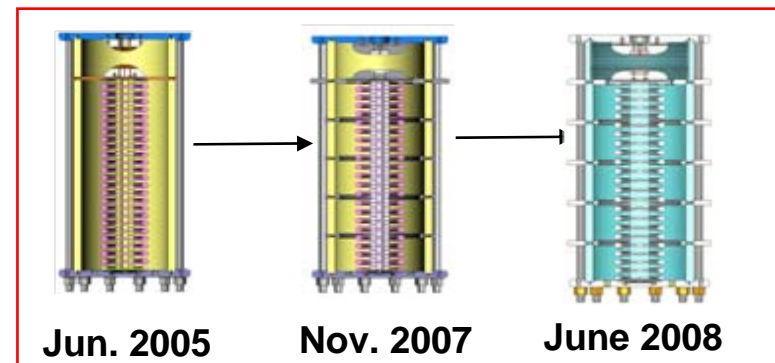


Summary

- A reduction of single switch jitter of less than 3 ns is required to obtain precise radiographs using Z-Petawatt and increases backlighting accuracy for Z-Beamlet



- Requires a different topology
 - Testing beginning June 1



January 2009