

# **Packaging of a MEMS Optical Switch For Developmental Testing**

## **Ceramic Interconnect and Ceramic Microsystem Technologies (CICMT 2009)**

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# Outline

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- **Motivation**
- **Description of our MEMS (micro electro-mechanical system)-based optical switch**
- **Package requirements for concept testing**
- **Issues in design and assembly of packages**
- **A ceramist's solution to stiction**
- **Conclusions**



# Motivation

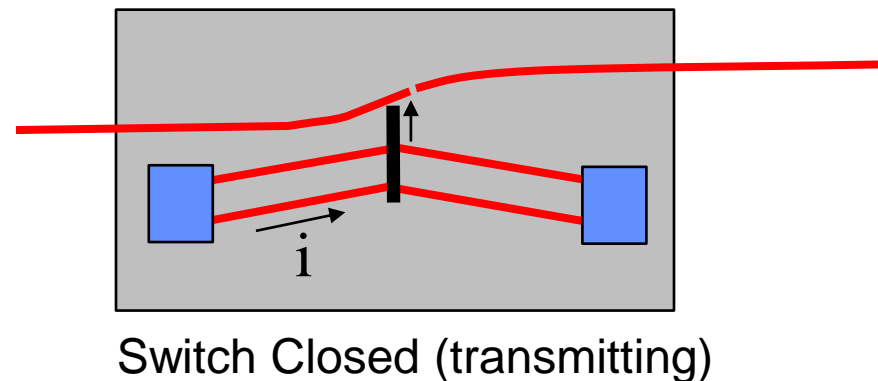
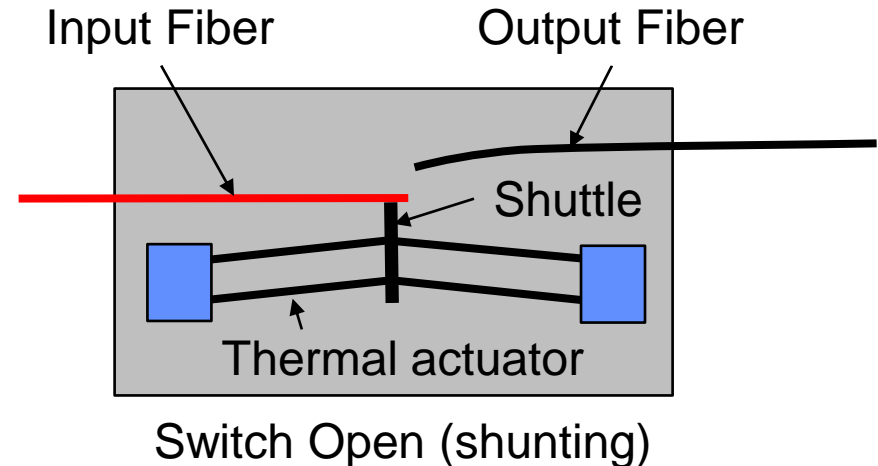
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- **Microelectronic systems** – Concept often proven using a probe station at the wafer scale or with bare die
- **MEMS** – Due to required mechanical, fluidic, or optical interaction, must often be tested in a package to prove concept

**We discuss the prototype packaging of MEMS-based optical fiber switch for developmental testing**

# MEMS Optical Switch Concept

1. Current flowing through actuator causes localized Joule heating
2. Shallow-angle chevron-shaped actuator expands between fixed anchors
3. Small expansion of beam length **relative** to anchor spacing causes large displacement of shuttle
4. Shuttle on actuator moves a fibers into alignment, closing switch
5. Latch (not shown) keeps fibers in alignment until reset

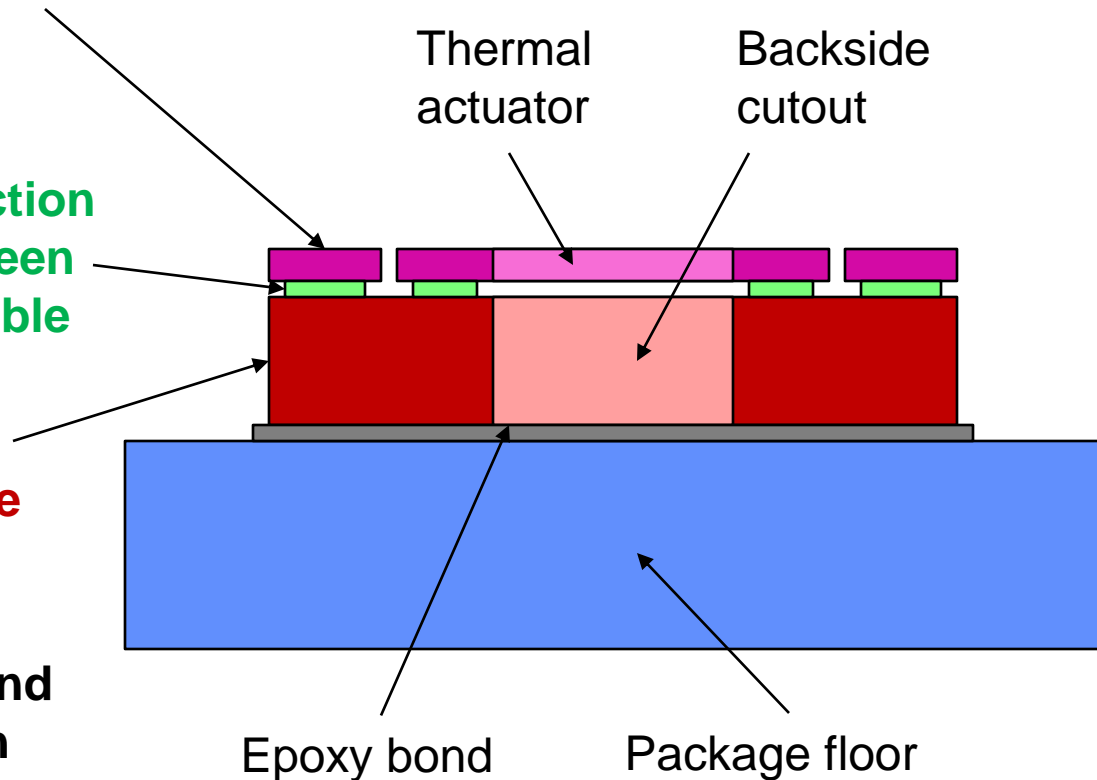


# Layers in MEMS Device

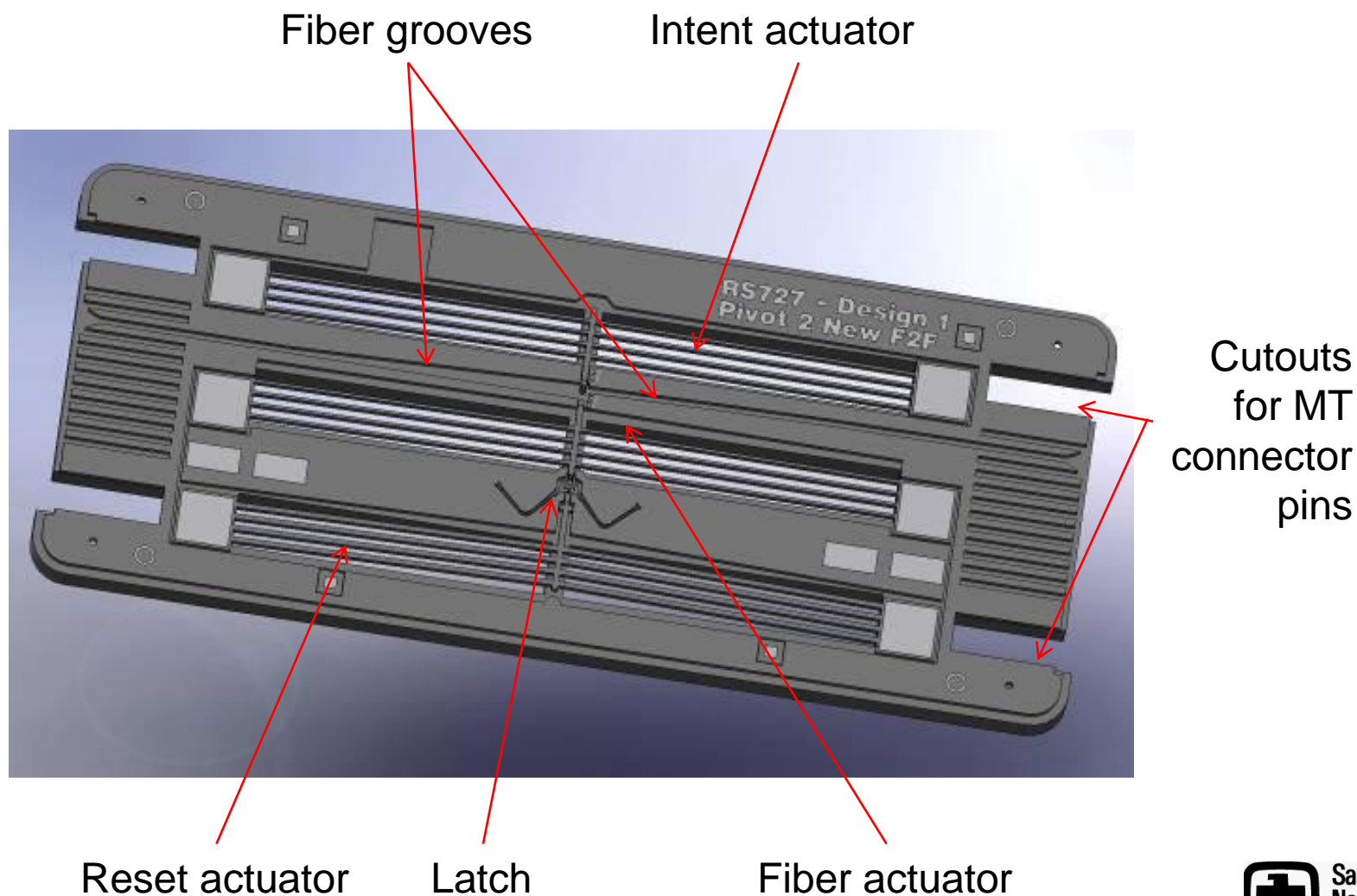
## SOI (silicon on insulator)

- 125  $\mu\text{m}$  device layer that includes thermal actuators and other movable elements
- 2  $\mu\text{m}$  buried oxide (BOX) provides mechanical connection and electrical isolation between layers, removed under movable elements
- 500  $\mu\text{m}$  handle layer with backside cutouts to minimize heat loss

Features are deep reactive ion etched (DRIE) from both front and back with BOX doubling as etch stop



# Layout of MEMS Device





# Device in Operation

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- **Scene 1: whole switch**
- **Scene 2: fiber actuator, optical fiber and latch**
- **Scene 3: optical fiber switching and transmitting light**

# Package For Bench Testing

## Requirements:

- Electrical connectivity to MEMS die
- Support for optical fibers
- Avoid residual stress in die that could cause actuator displacement



## Solution:

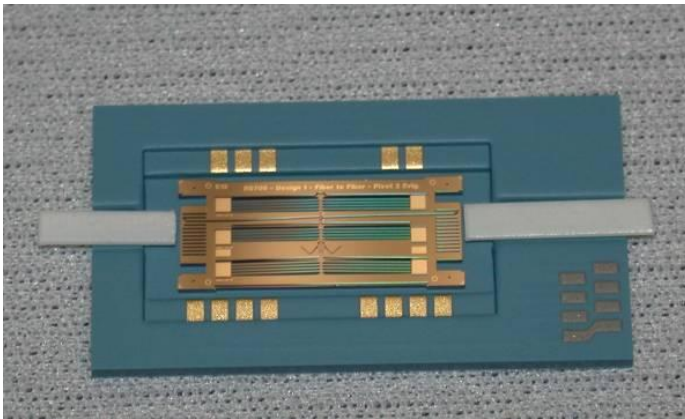
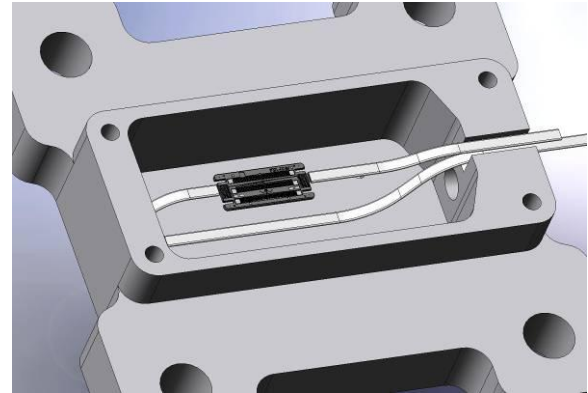
- HTCC “bathtub” DIP (dual in-line package) with ends sawed off, on alumina substrate for fiber support
- Room temperature epoxy die attachment



# Package For Vibration Testing

## Further requirements:

- Small form factor
- Ruggedized fiber attachment
- Withstand potting pressures
- Observation window



## Solution:

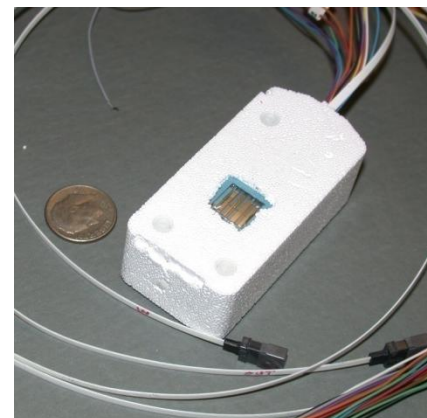
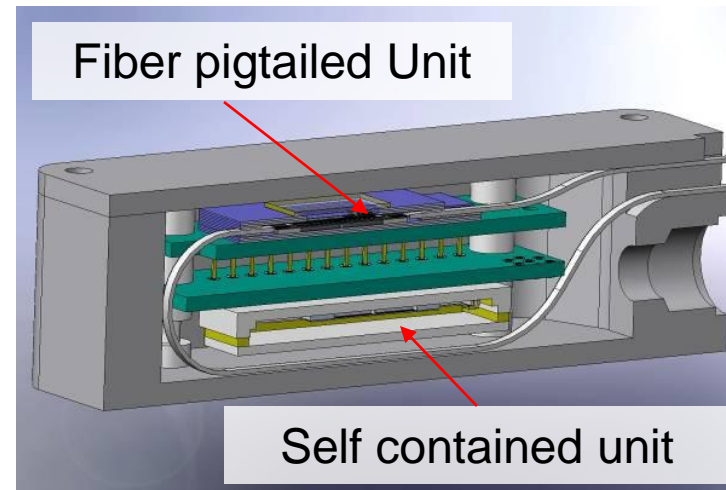
- Custom LTCC package and lid
- Ribbon fiber with unused fiber stubs epoxied into grooves in MEMS die
- Solder pads for direct connection to wiring harness

# System Design for Test

Due to importance of showing success of MEMS concept, two devices were put into test bed

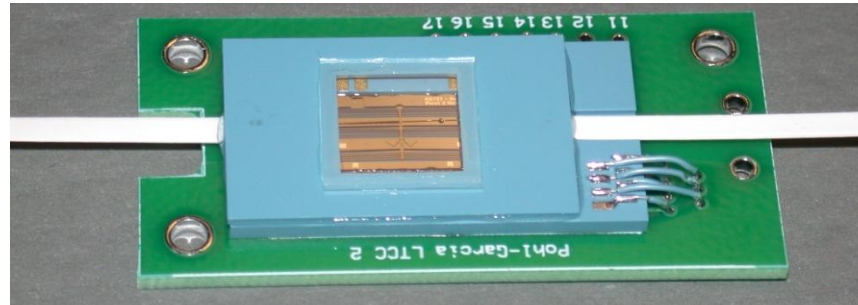
- LTCC package with optical fiber pigtails terminated with MT connectors for external optical testing
- Bathtub DIP consisting LED, switch, photo-detector, and stub fibers for self-contained optical testing

Units were mounted on PCBs, held in cavity using plastic pins, and potted in place using expanded polystyrene beads



Potted assembly removed from cavity with window exposed

# Package Concerns for Fiber-Pigtailed Unit



- Protection of MEMS die during mechanical environments testing
- Survivability of package under potting pressure
- Thermal stresses on MEMS die from die attachment
- Preparation of optical fibers
- Complexity of device assembly
- Bonding of optical fiber to die / package
- Survivability of device under potting temperature

# Mechanical Protection of MEMS Die

**Considered including mechanical stops to protect movable elements in MEMS**

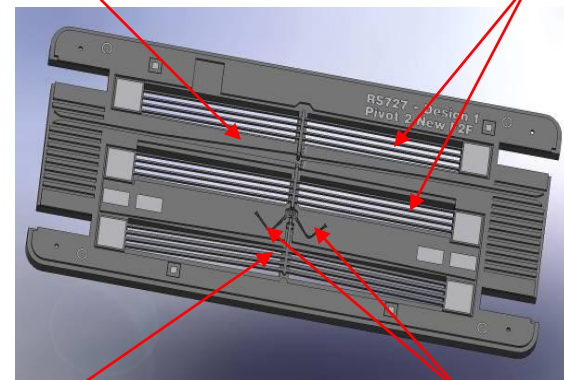
- **FEA modeling indicates that under inertial loading, the movable elements are**
  - stiff – all vibrational modes above 4000 Hz)
  - strong – all factors of safety (FOS) above 6 for 1000g static loading
- **Response to shock loading still unknown**

**Decided to forego mechanical stops based on promising FEA results**

**Factors of Safety under 1000g static loading**

Optical Fiber: 6.1

Fiber and Intent Actuators: 12

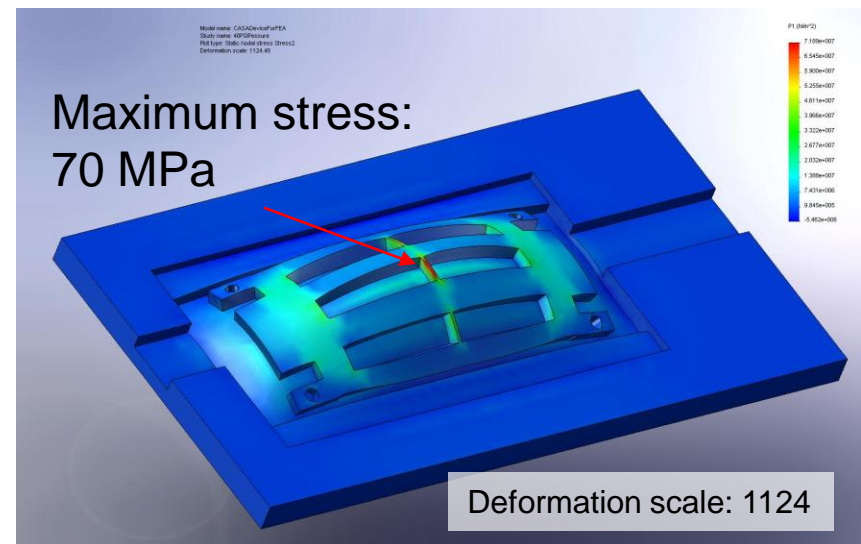
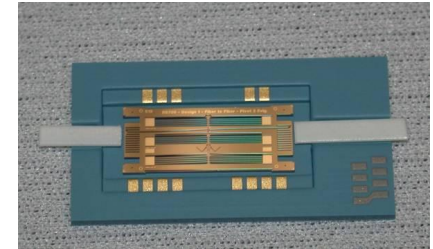


Reset Actuator: 19

Latch Claws: 43

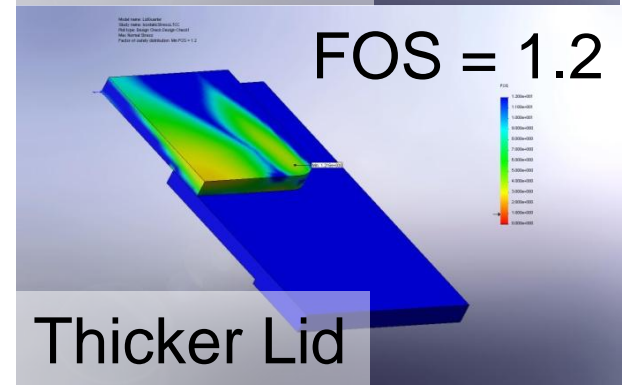
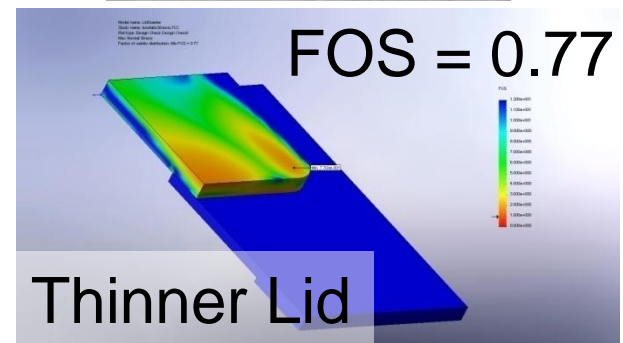
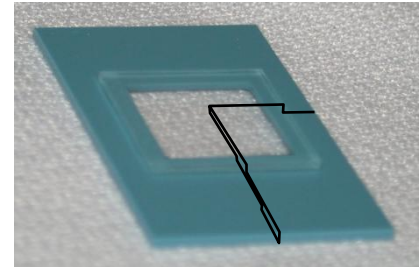
# Analysis of Potting Stresses on Package

- In potting, it was assumed that the pressure could reach 275 kPa (40 psi)
- Modeling predicts package safe, but cavity floor flexure could cause die failure
- Modeling predictions prompted us to strongly bond the LTCC package to the PCB to provide extra backside rigidity



# Analysis of Potting Stresses on Lid

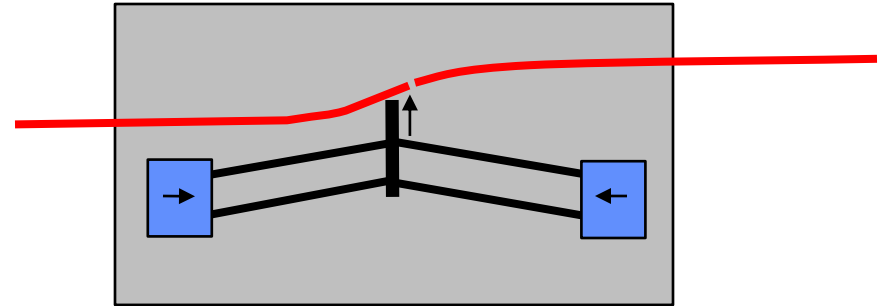
- Under same 275 kPa potting pressure
- Modeling predicts LTCC safe, but glass close to slow crack growth threshold
- Increasing LTCC thickness to reduce flexure of frame had larger impact than increasing glass thickness
- Made the lid thicker in response



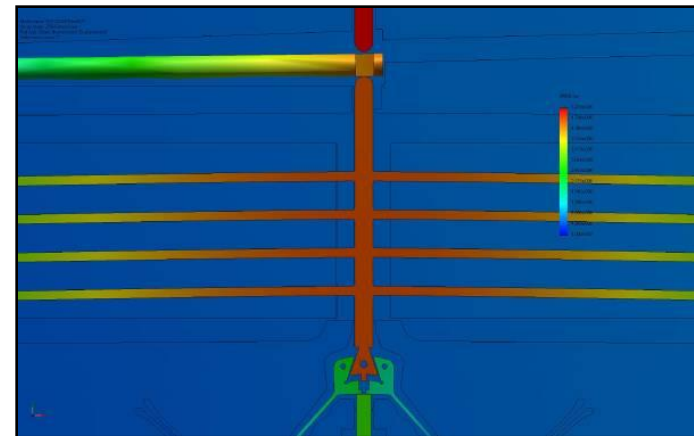
# Need to Avoid Die Attach Thermal Stresses

- Thermal stresses from high-temperature die attachment can result in deflection of actuators with no applied current
- Small contraction of anchor spacing **relative** to actuator beam length causes large displacement of shuttle
- Used a room-temperature-curable epoxy to avoid problem

Model of die on alumina with stress-free temperature of 102 C. Shuttle displacement from nominal (indicated by red color) is 43 $\mu$ m.



Partial Actuation Due to Compressive Thermal Stresses in Die



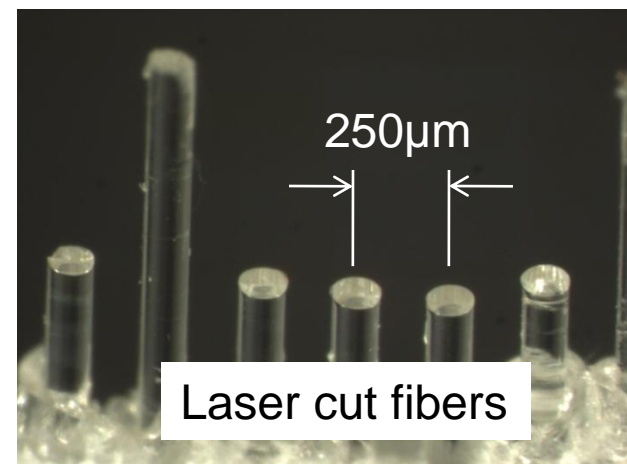
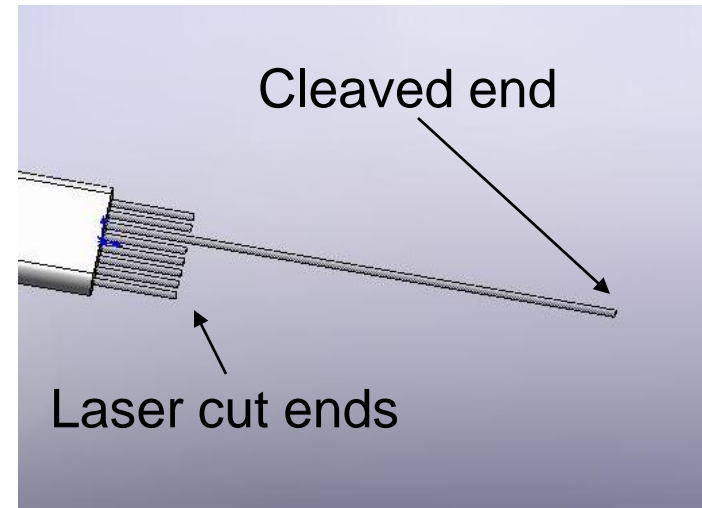
# Preparing Ribbon Fiber For Insertion

Approach is to use multi-fiber ribbon and use passive fibers for mechanical support

- Active fibers must have pristine cleaved ends
- Passive fibers must be cut shorter without damaging active fiber

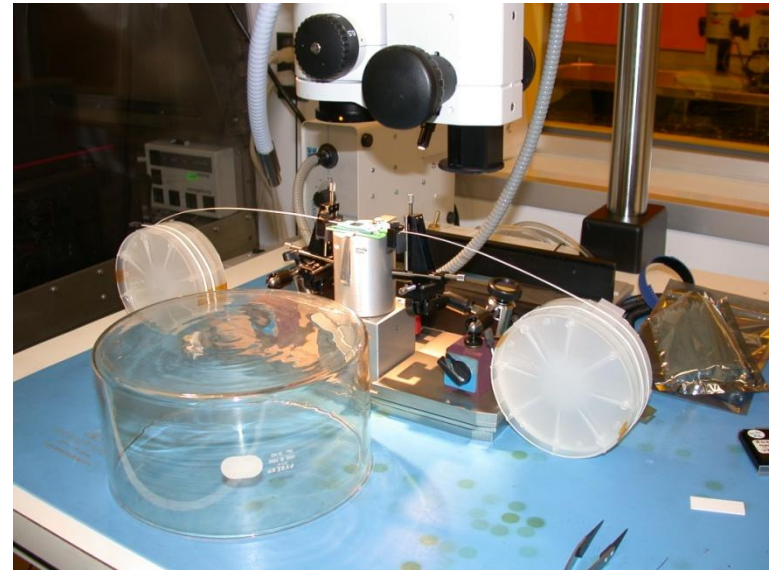
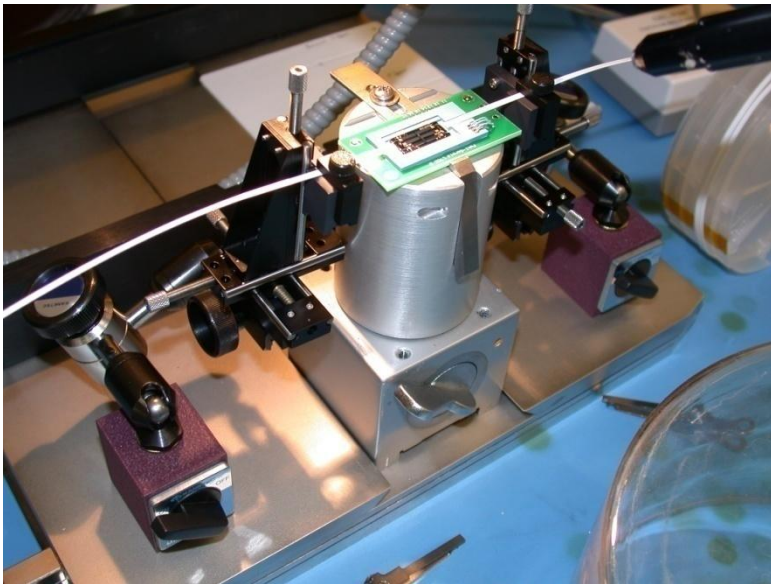
## Process

- Strip jacket
- Mechanically cleave all fibers with multifiber cleaver
- Cut passive fibers to length with CO<sub>2</sub> laser



# Assembly of Fibers Into MEMS Die

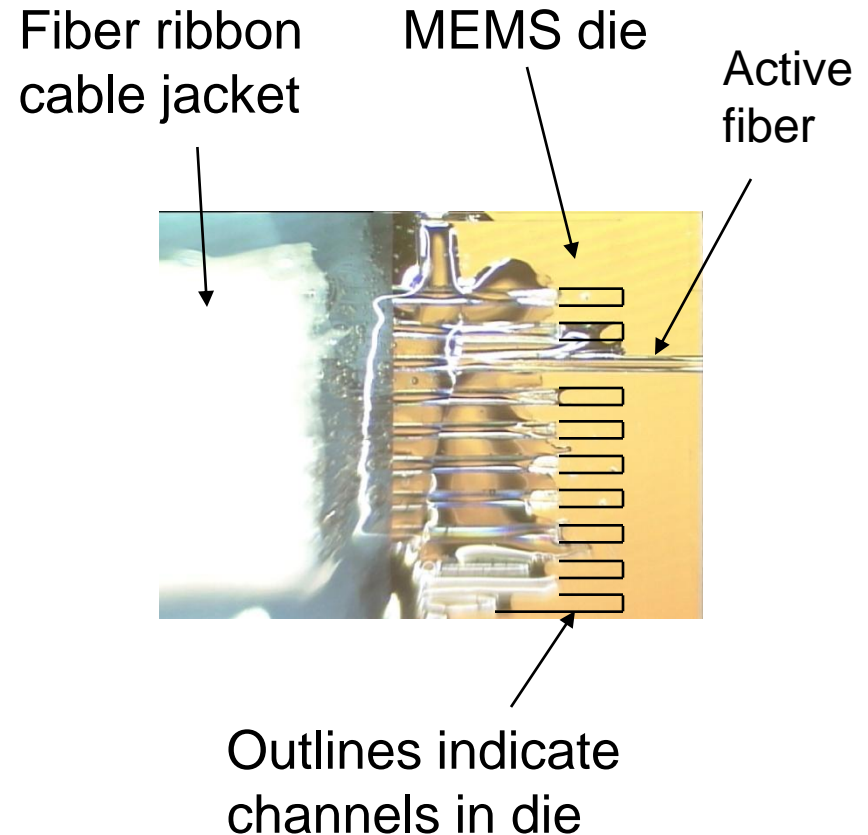
- Tools are two x-y-z rotationally adjustable micromanipulators, a workholder, and a boom mounted microscope



- Use micromanipulators to feed fibers into grooves in die
- Epoxy fiber into place by hand

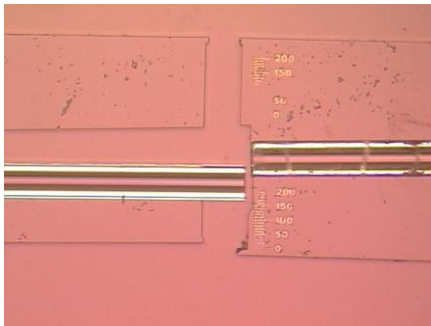
# Bonding Fibers to Die

- **Robust bond is created by epoxying fibers into channels on die over about 1 mm of length**
- **Epoxy extends over edge of die to prevent unprotected fiber from rubbing on die edge**
- **No appreciable bonding to fiber jacket**
- **Package lid prevents fiber from peeling up**

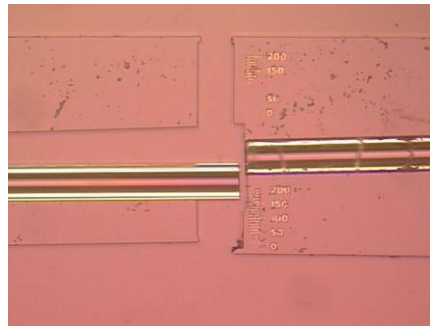


# Testing the Fiber Bond Strength

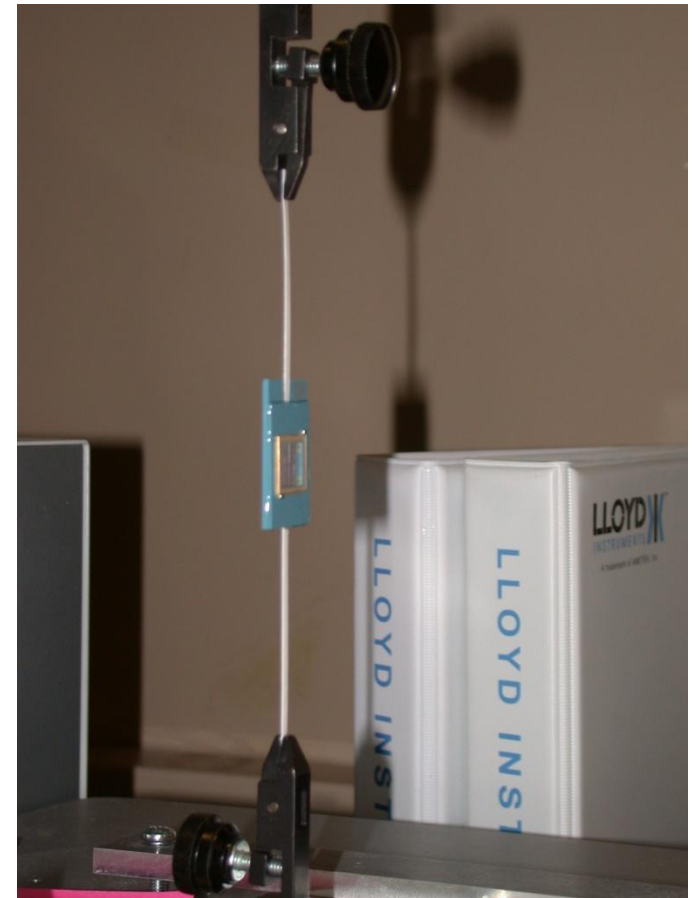
- Pigtailed packaged devices were non-destructively tested on a pull tester with a maximum load of 50 N (11.2 lbs)
- No movement of fiber was detected



Pre-test  
picture



After pull tests up  
to 50 N

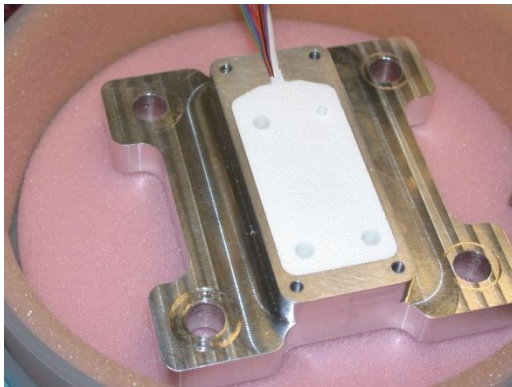


# Potting Process

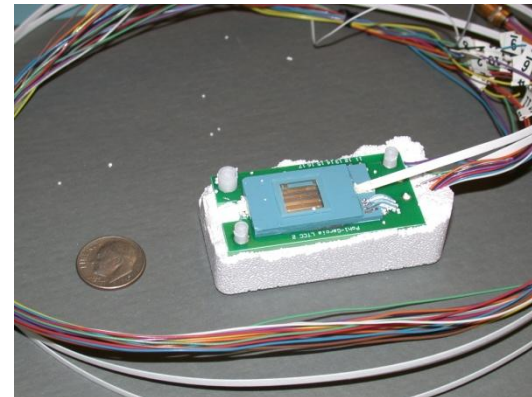
- Expand polystyrene beads in closed cavity containing device
- Temperature up to 100°C, pressure estimated at up to 275 kPa (40 psi)



Putting beads into housing



Fused beads with lid removed



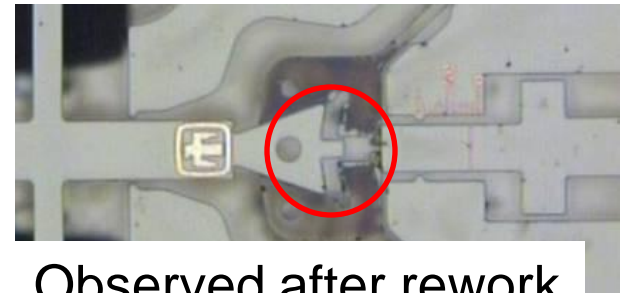
Post-test tear-down

# Thermal Stresses from Post-Cure Thermal Excursion

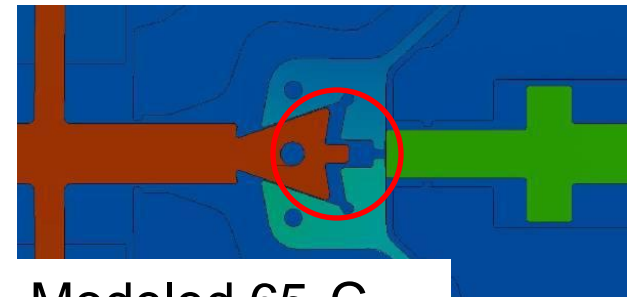
- A self-contained unit (MEMS in an HTCC bathtub DIP) was reworked, requiring heating to  $\sim 180^{\circ}\text{C}$
- Observe fiber actuator displacement at room temperature commensurate with a  $65^{\circ}\text{C}$  stress free temperature (assuming no compliance in epoxy bond)
- **Similar effects are observed after potting**
- **Will have to address in next version of package**



Stress Free

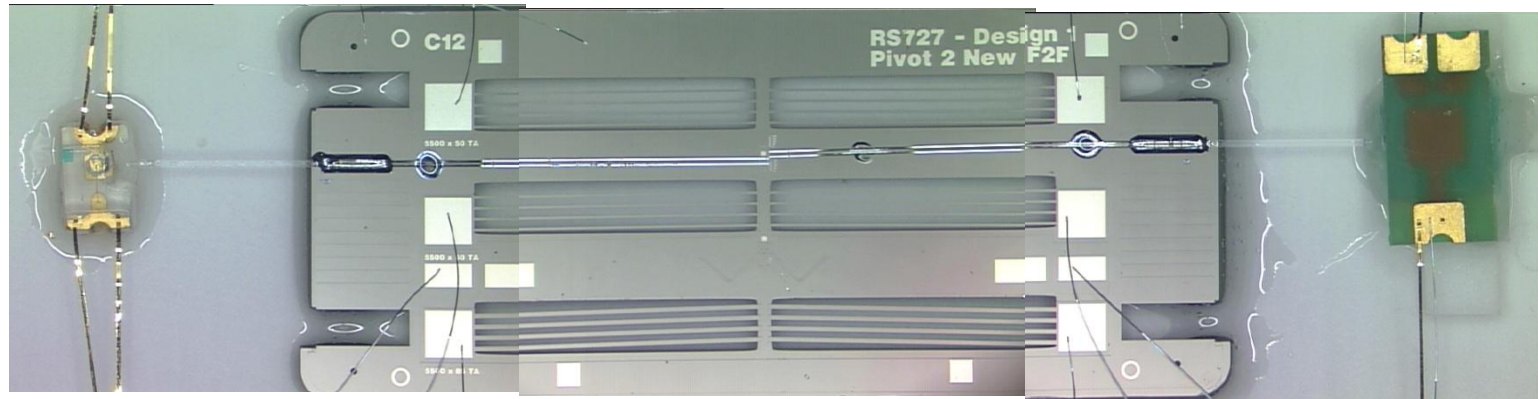


Observed after rework



Modeled 65 C  
stress free temp

# Self Contained Unit

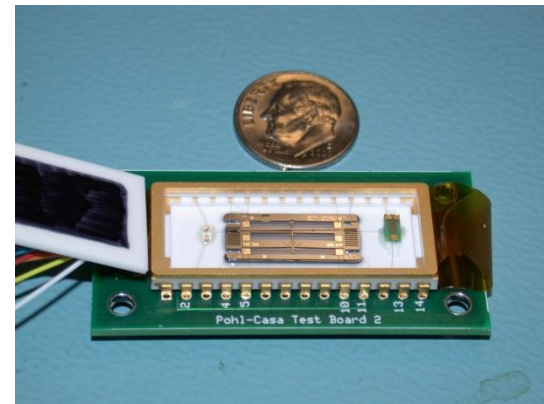


LED

MEMS Switch

Photodiode

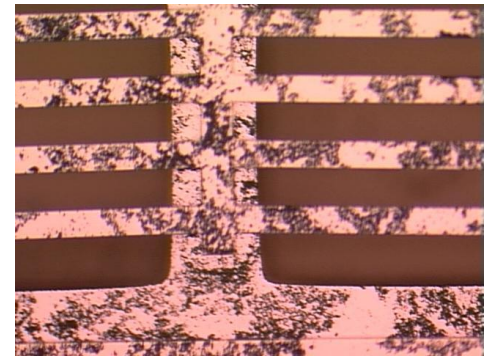
- Much simpler because we don't have to worry about external loads on fiber, aligning end of long fiber



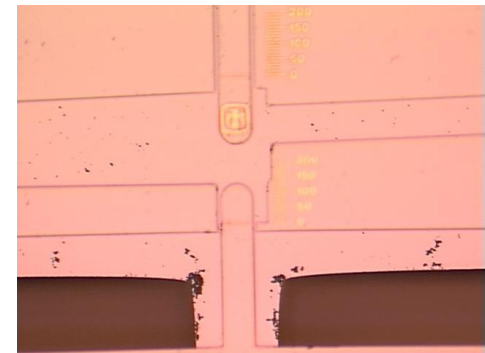
# Solving Stiction Problems

**Are particles in MEMS devices always bad?**

- **Large area, smooth, clean surfaces separated by  $2\mu\text{m}$  gap between device and handle layers would stick if brought into contact.**
- **Used  $1\mu\text{m}$  alumina particles delivered in water / isopropanol suspension to ensure separation of surfaces**
- **Approach effective even though process not perfected. Ideally, use few particles that get drawn into small gaps where needed.**



Too many particles, but device worked



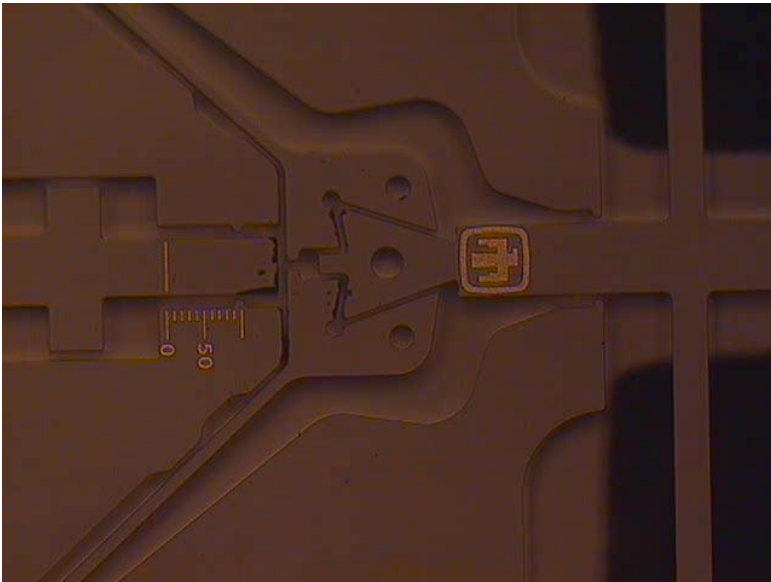
Fewer particles, but still effective



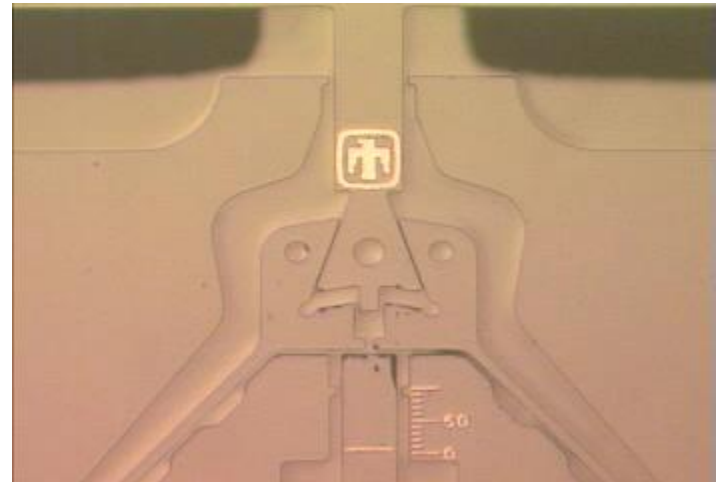
# Results

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- Device survived testing
- Stresses from thermal excursion during potting caused displacement of actuators



Pre-test movie



Post-test movie



# Future Package

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- **Will have to be hermetic**
- **Avoid use of organics**
- **Need to solve CTE mismatch issues**
- **Manufacturability will have to be improved**



## Conclusions

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- **LTCC technology allows for rapid fabrication (2 weeks for us) of prototype packages for MEMS development for environmental testing of MEMS devices**
- **FEA design tools are valuable in analyzing the likely response of the packaged system before fabrication and test**



# Acknowledgements

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- **Dennis De Smet** - LTCC fabrication, device assembly, and testing
- **Gayle Schwartz** – Assembly
- **Howard Arris** – Potting