

Plasma Power Station

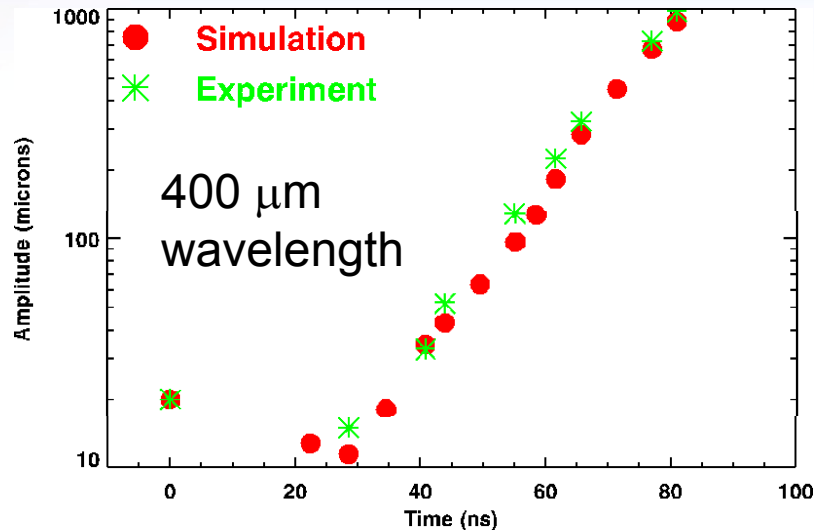
Quasi Spherical Direct Drive Capsule for Fusion Yield
Inverse Diode for Driver-Target Standoff
Magnetically Insulated Linear Transformer Drivers

J. P. VanDevender^{1,2},
M. E. Cuneo², S. A. Slutz², M. Herrmann²,
R. A. Vesey², D. B. Sinars², D. B. Seidel², L. X. Schneider²,
K. A. Mikkelsen², V. J. Harper-Slaboszewicz², B. P. Peyton³,
A. B. Sefkow², and M. K. Matzen²

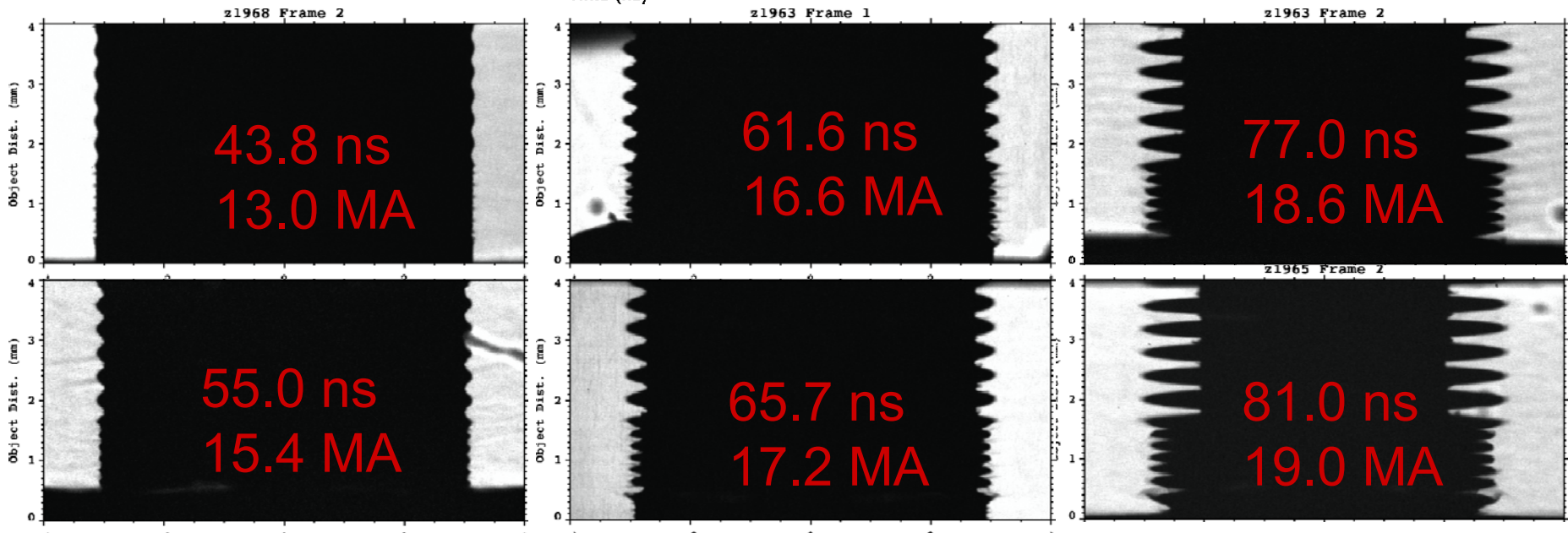
¹*VanDevender Enterprises*, ²*Sandia National Laboratories*, ³*Ktech Corp.*

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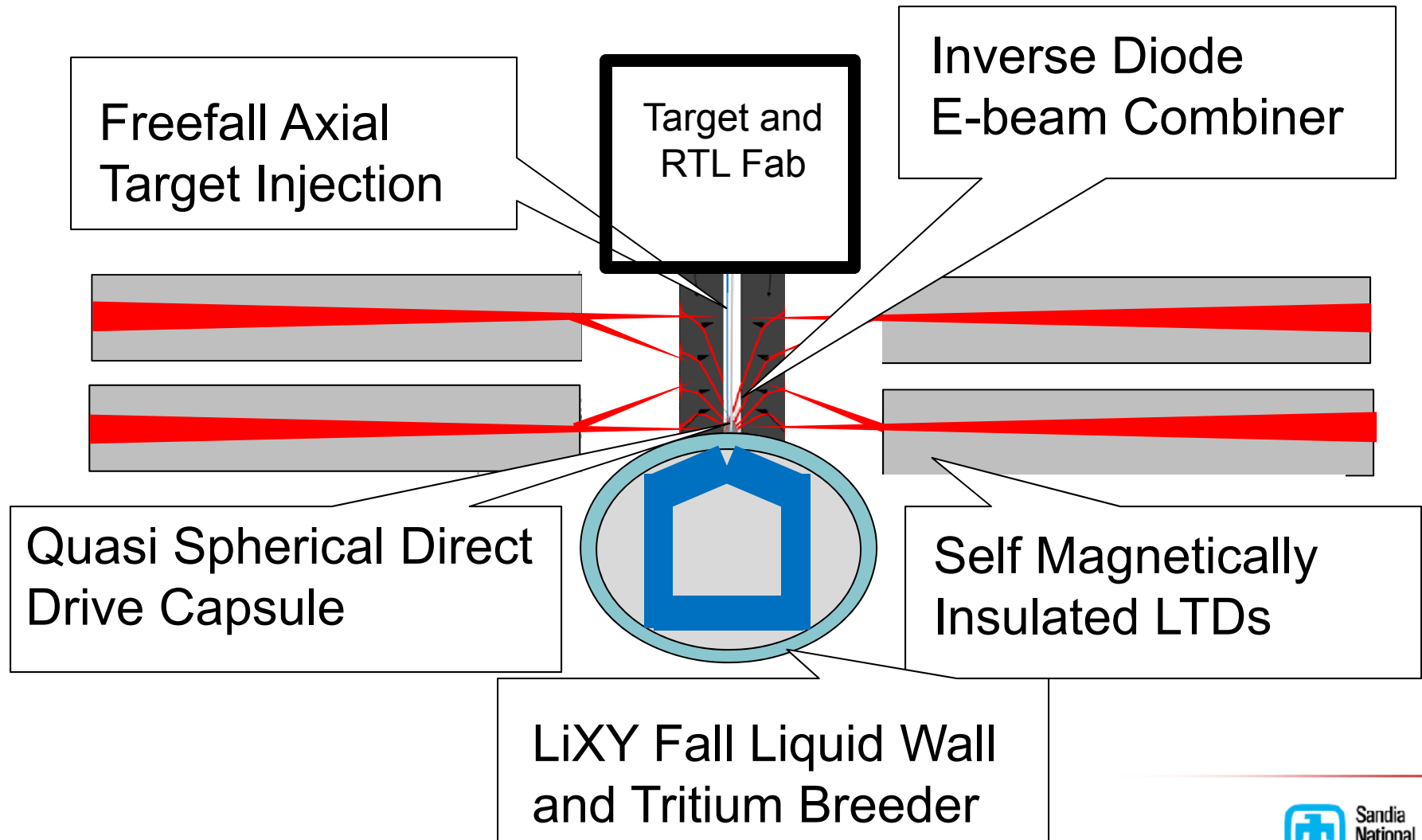
Experiments have validated LASNEX simulations of Magnetic Rayleigh Taylor (MRT) Instability.



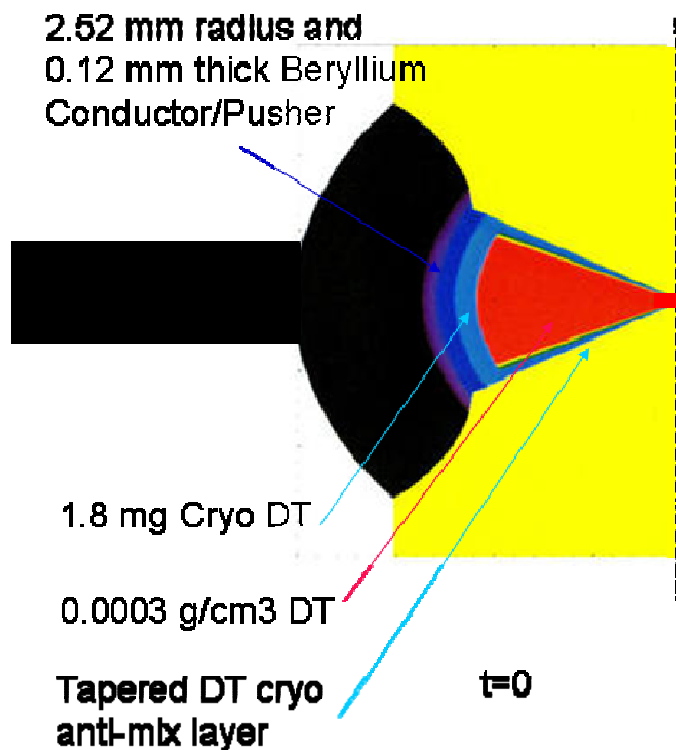
- D. Sinars et al. PRL **105**, 185001 (2010) and Physics of Plasmas **18**, 056301 (2011)
- Longer wavelengths compared well.
- Shorter wavelength growth less than 2D predictions.



**PPS now targets 3 Hz operation to produce power at
Meir-Mohr Model COE of 7.6 cents/kW-hr.**



Quasi Spherical Direct Drive capsule offers 500 MJ yields with 85 MJ energy store.

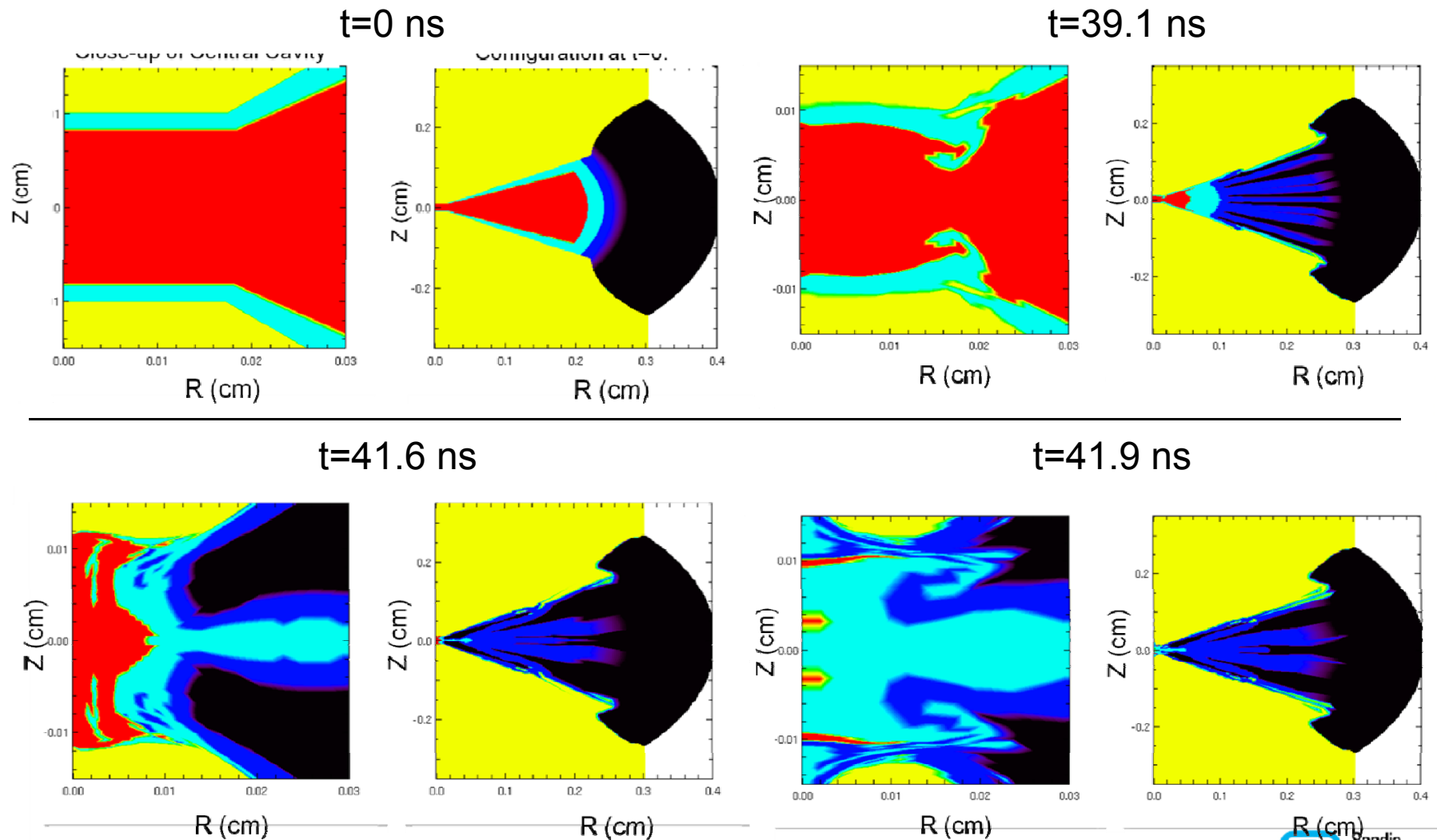


Many issues are mitigated with a higher dl/dt .

- **Uniform Initiation**
- **Less growth of Magnetic Rayleigh Taylor instability**
- **Lower driver energy**
- **Higher ηG**
- **Lower Cost of Electricity**

2D yield is currently limited by a wall instability.
Three possible solutions are being examined with LASNEX.

LASNEX Simulations show MRT Instability is benign for $R_0/\delta_0 = 21$ and 1 MJ yield in 1D and 2D at 38 MA.



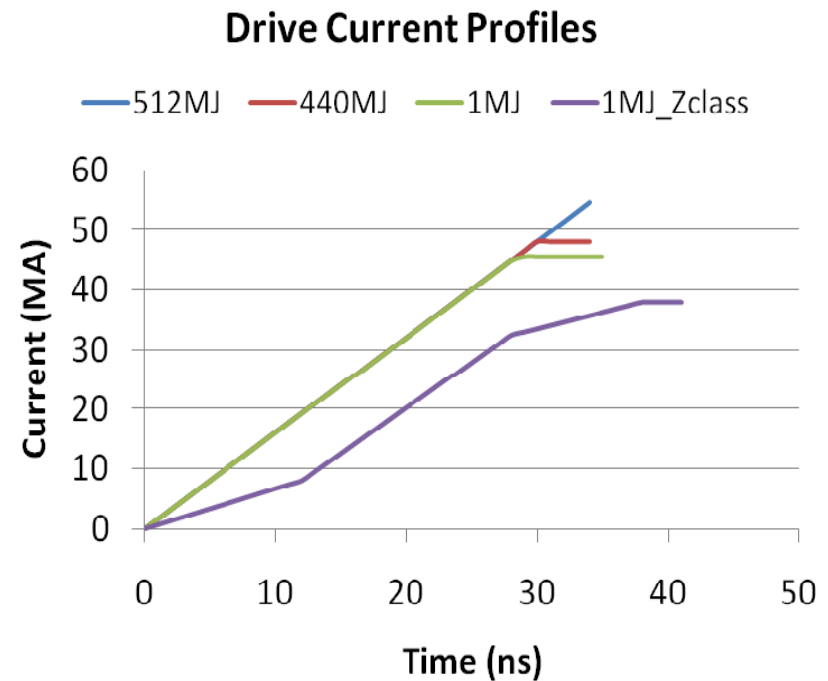
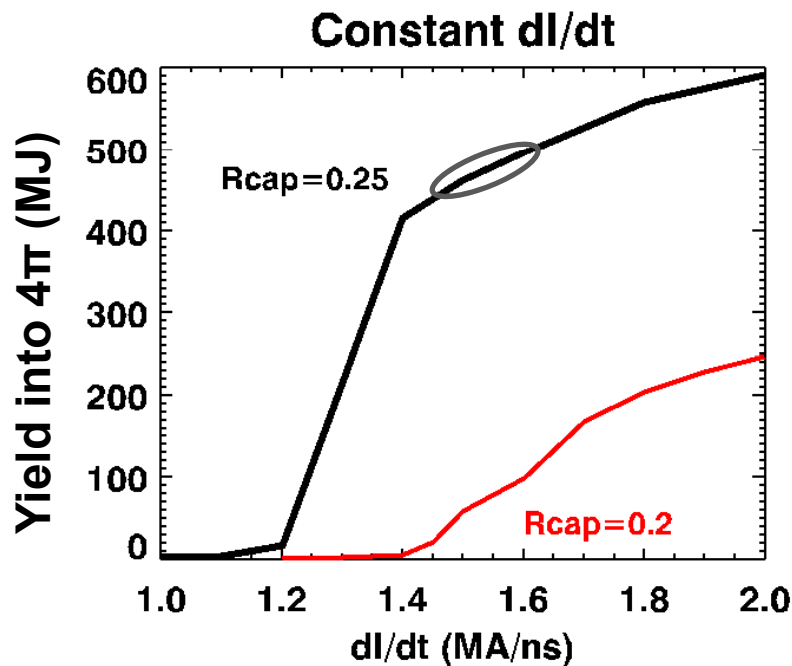


Simulations reveal seven features that motivate QSDD.

1. Quantum Molecular Dynamics make design less uncertain than laser plasma interaction, wire initiation, and opacities make x-ray drive.
2. >6 times more energy in the fuel than x-ray drive.
3. Peak magnetic pressure >10 times ablation pressure of x-ray drive.
4. Internal pulse shaping automatically provides hot spot heating and adiabatic compression of main fuel.
5. Metal conductor tamps expansion during burn.
6. >4.5 MA current penetration into fuel gives alpha trapping and reduce p_{ignition} by a factor of 5.
7. Possibility of MJ yields on a 40-ns, Z-class driver.

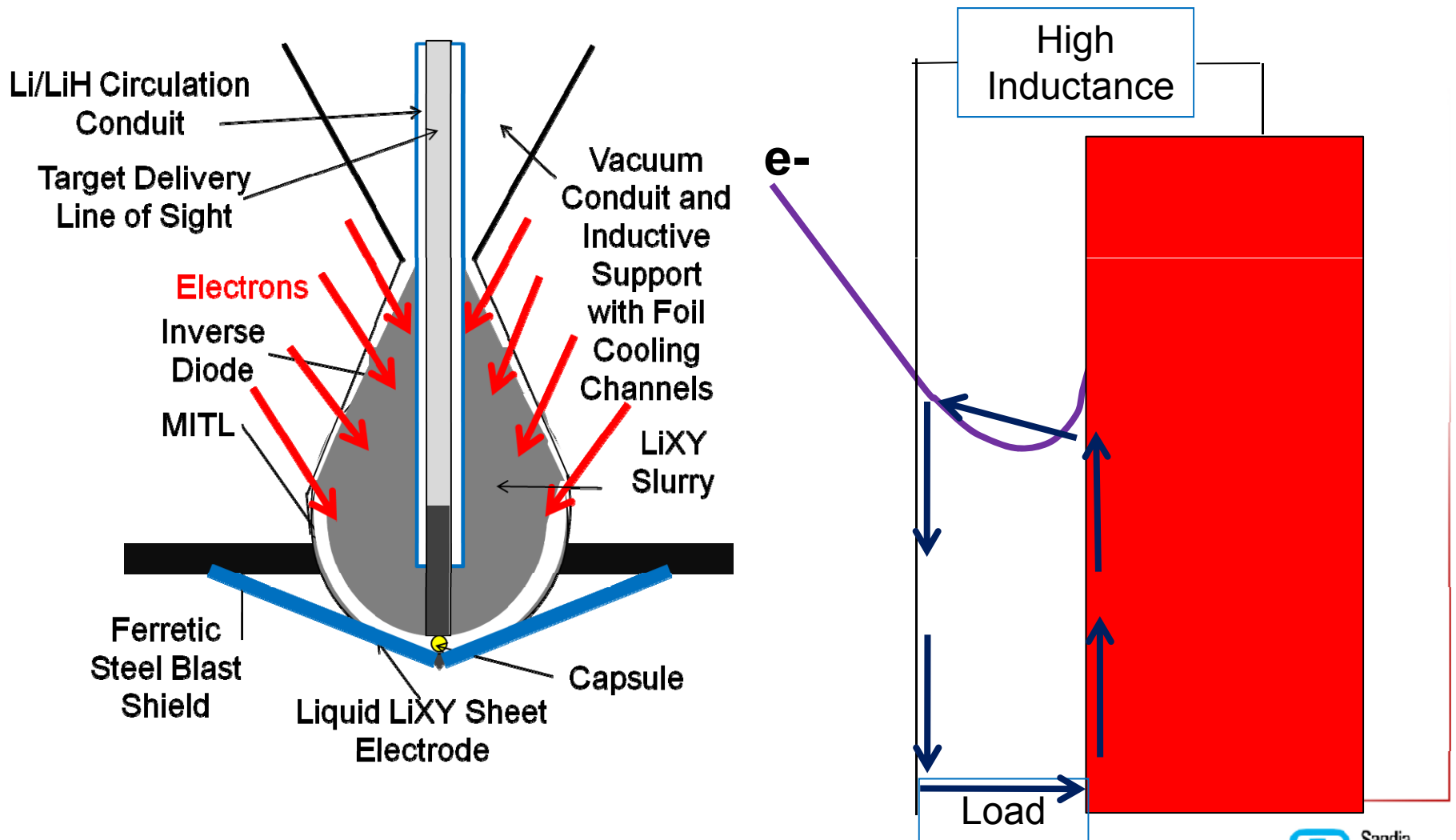
Projected drive current is ~ 38 MA for ignition on Z-class driver and ~48 MA for high-gain on PPS.

Magnetic Rayleigh-Taylor instability allows initial aspect ratio of $R_o/\delta = 21$.



Producing $dl/dt=1.5 \times 10^{15}$ A/s in a 2.5 mm radius capsule requires a new technology.

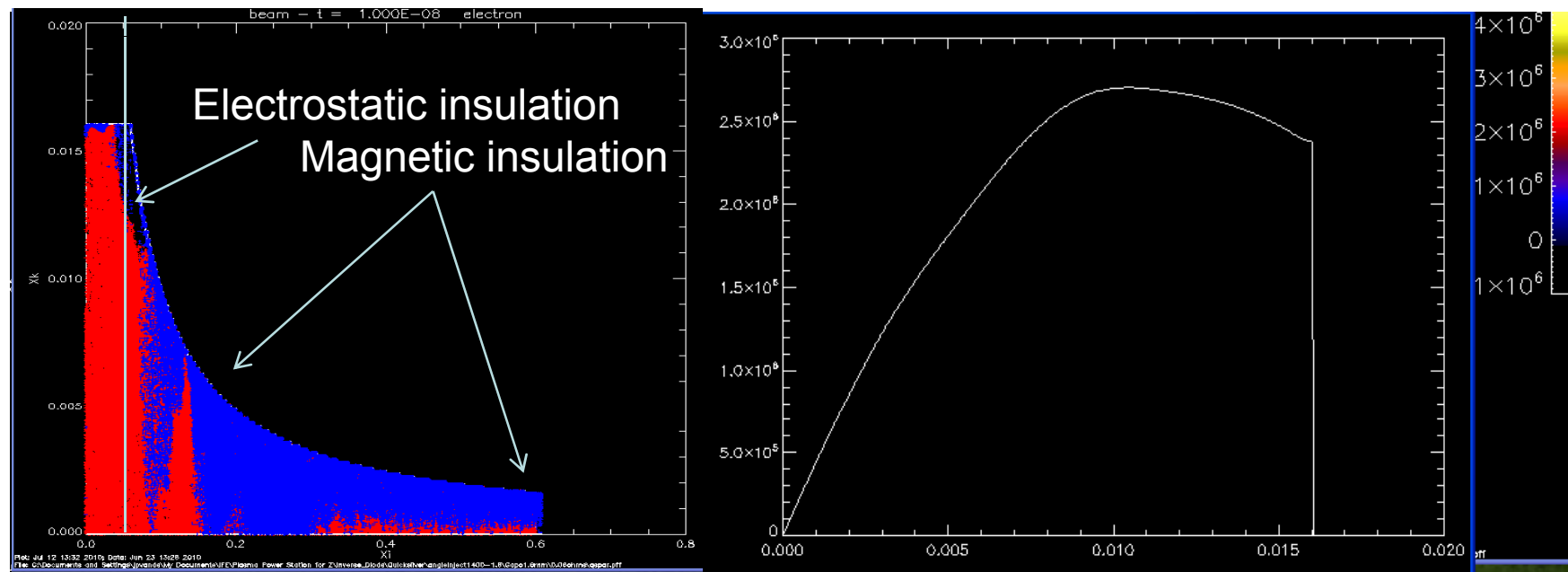
RTL and Inverse Diode couple the capsule to the driver.



Space charge distribution prevents secondary electrons from neutralizing injected current.

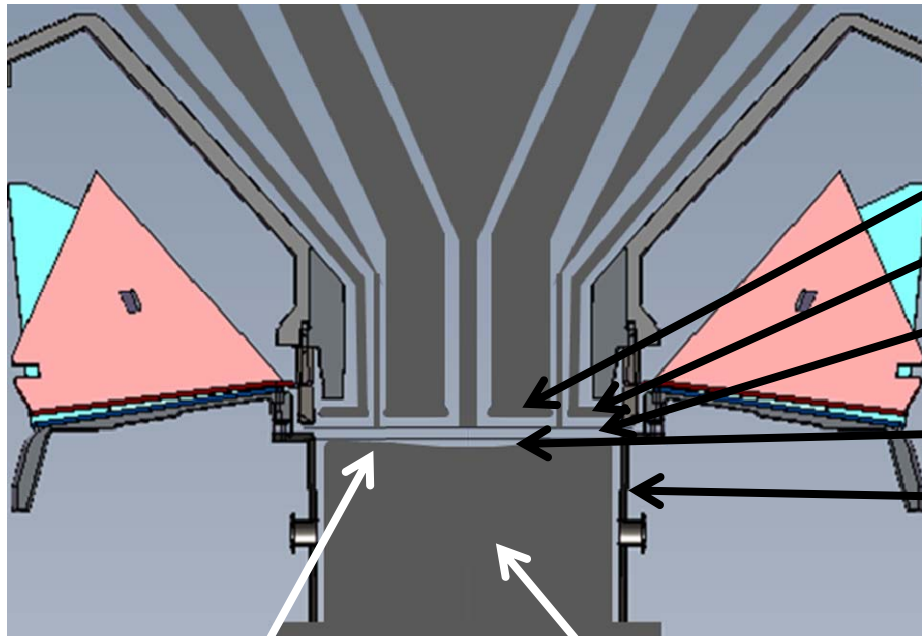
Red: Injected electrons
Blue: Electrons emitted from cathode

Potential distribution across AK gap at $r=0.05$ m shows E-field reversal at cathode.

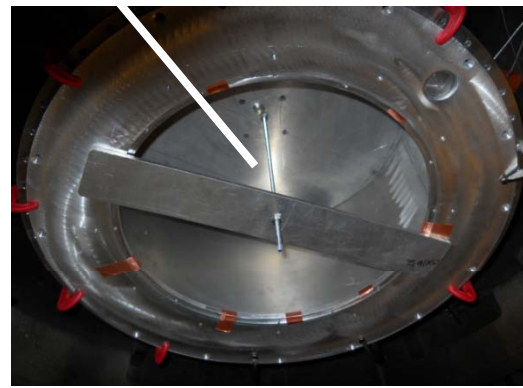


40 MA at 4 MeV injected and 33 MA at 2 MV at load
without optimization

Saturn experiment supports the feasibility of the Inverse Diode for the PPS—in some key parameters.

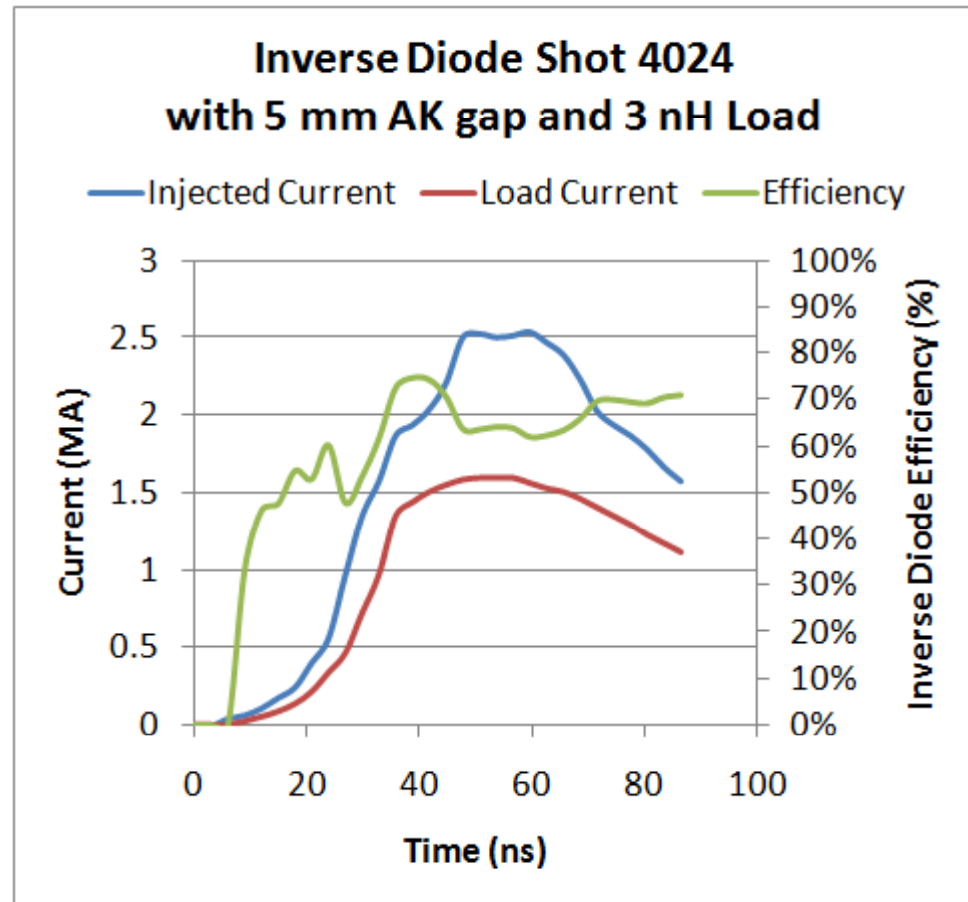


- Inner MITL Cathode
- Outer MITL Cathode
- Post Accelerating Gap (PAG)
- Inverse Diode Gap
- Voltage Monitoring Inductor

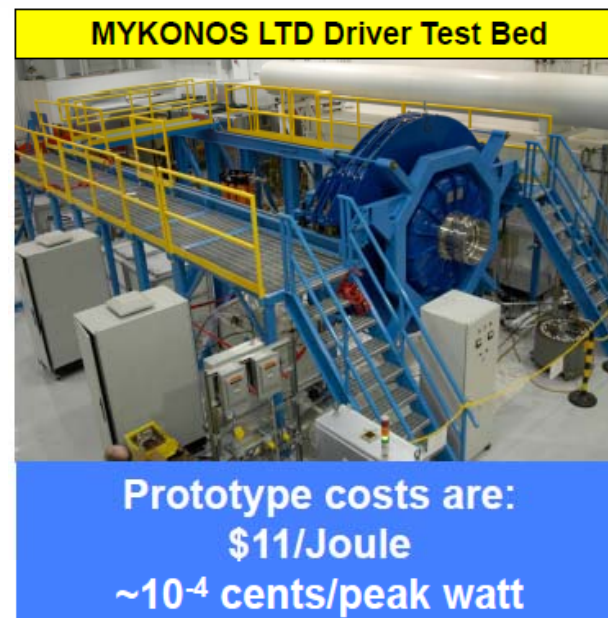
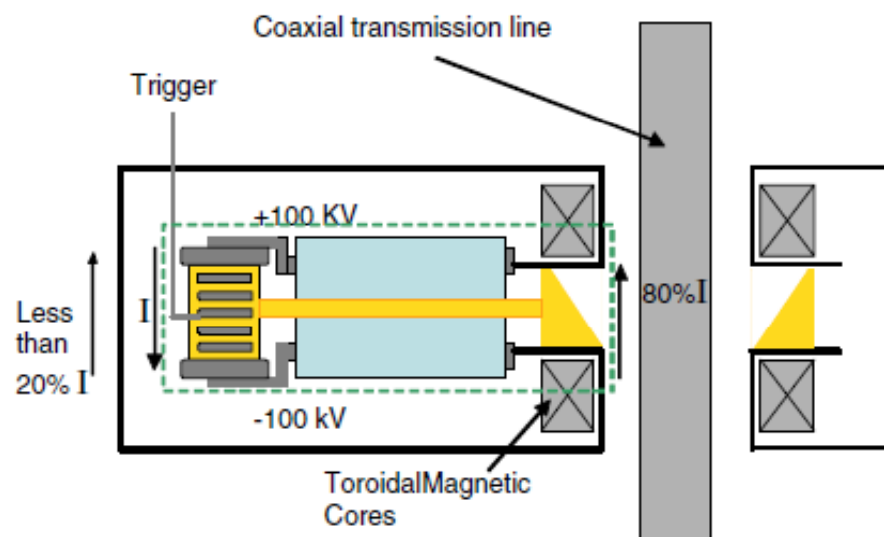


Saturn	PPS
1,3 MV	11 MV
2 kA/cm ²	0.5 kA/cm ²
2.5 MA	50 MA

Unoptimized Inverse Diode had ~65% collection efficiency on Saturn.



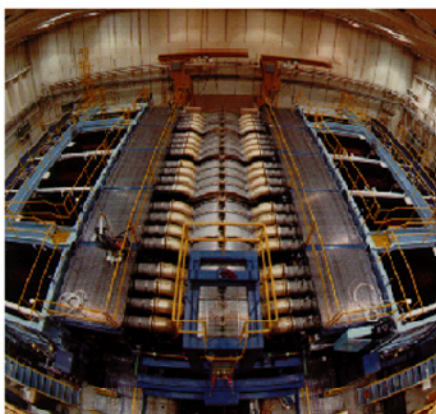
Magnetically Insulated, Linear Transformer Driver (MI-LTD) provides the modular e-beams.



PBFA-I, 2 MV, 12 MA

Hermes III, 18 MV, 0.7 MA

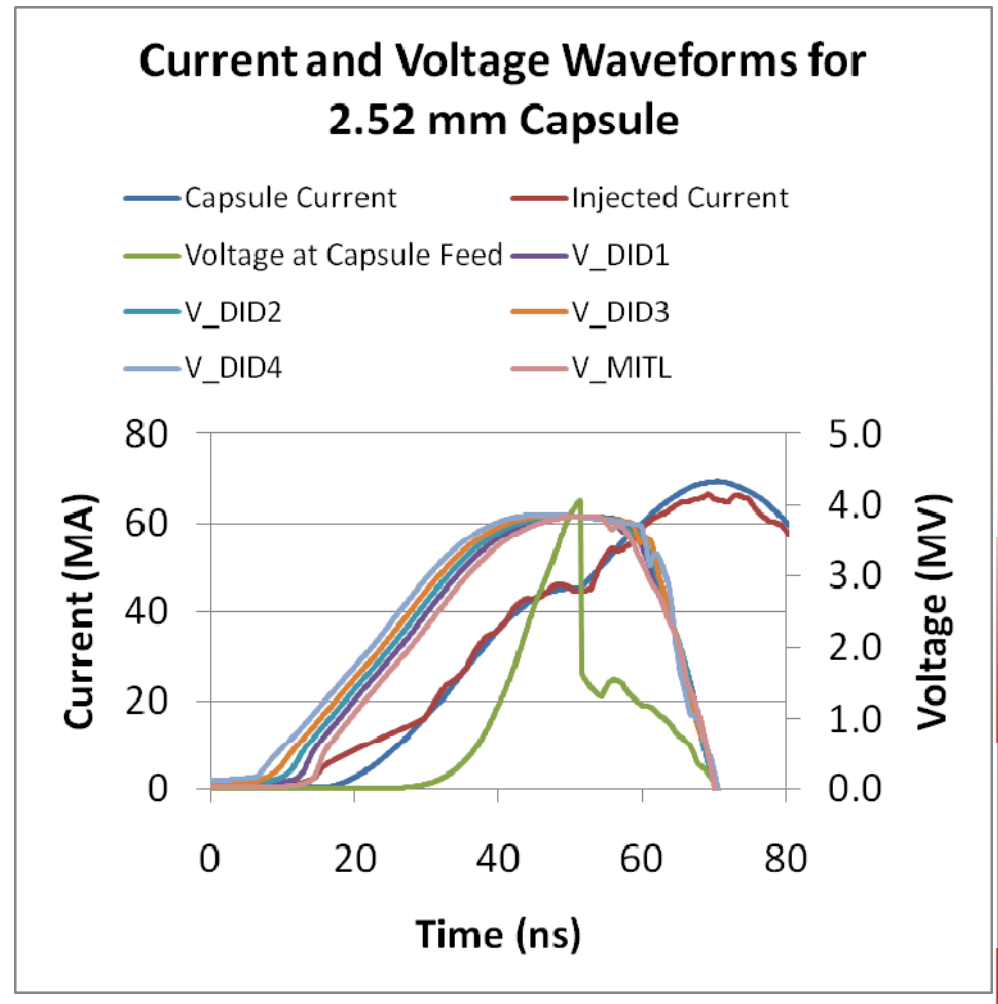
RHEPP II, 120 HZ



45 MA at 1.5×10^{15} A/s in QSDD capsule drives the design of the rest of the PPS.

- Direct Inverse Diode
 - 1 meter radius
 - 560 A/cm^2 injected electrons
 - 1 mm to 2mm minimum AK gap for 7.5 to 15MeV injected electrons
- MITL and Capsule
 - 1mm to 2 mm AK gap
 - 2.5 to 3.5 mm QSDD capsule

MITLs with 1 mm to 2 mm AK gaps must not short out.



PPS targets 3 Hz operation to produce power at Meir-Mohr Model COE of 7.6 cents/kW-hr.

First Units with 10% Cost of Capital and 1.85 MIT 2009 Study Factor to 2007\$ gives 14.9 cents/kw-hr.

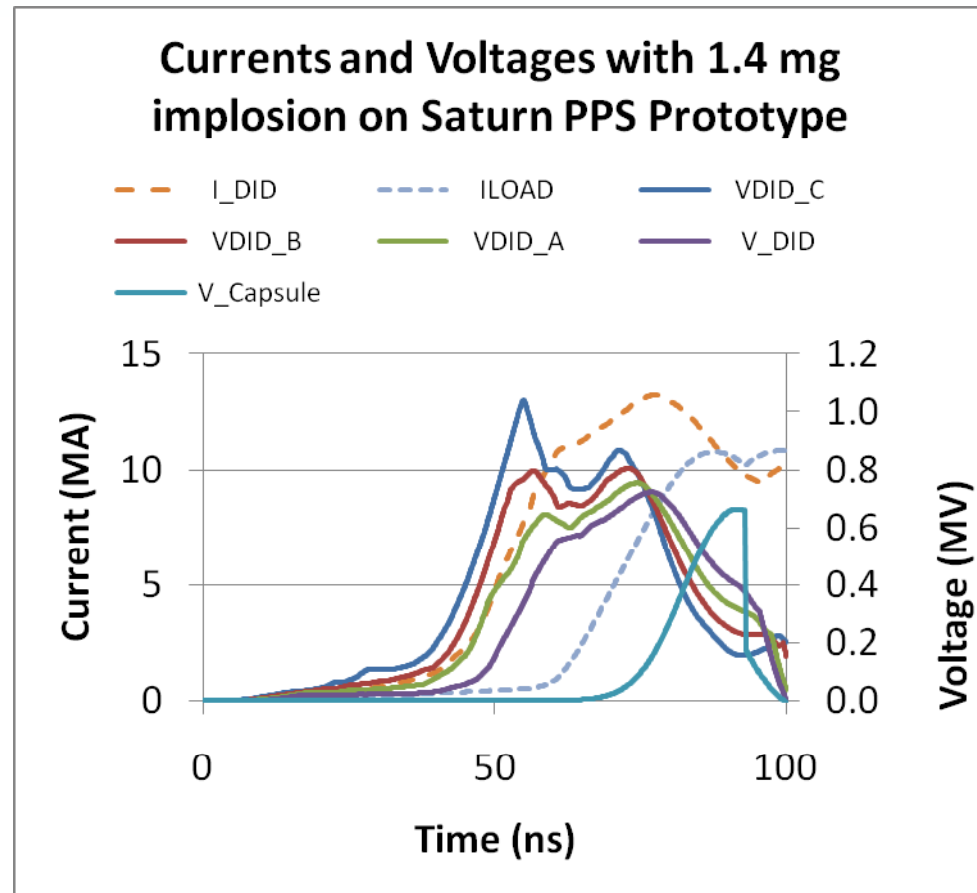
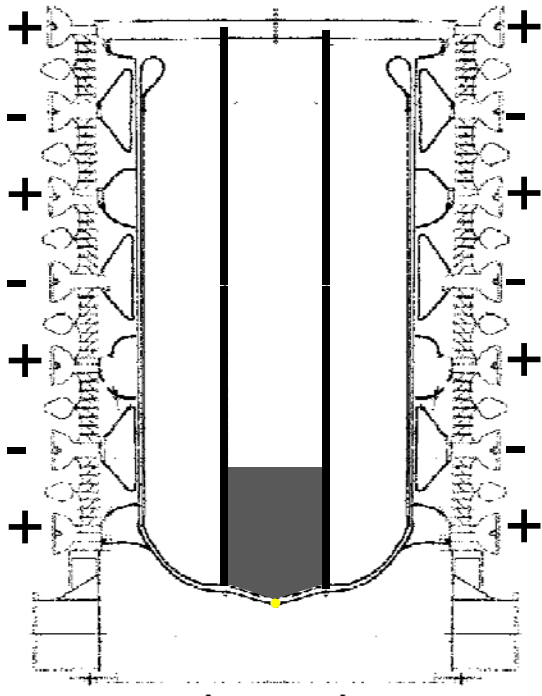
Input: Nc=number of chambers	1.00
Input: RR=rep rate in shots per chamber per second	3.00
Input: Discount or Hurdle Rate for attracting capital	10.00%
MIT Escalation Factor	1.85
Approximation to Pe (MW)	866
Eta=thermal to electrical	0.44
\$/Joule for Bank Energy	2.00
Energy Store (MJ)	85.0
η_{G_bank}	7.5
Net Electrical Power (MW)	651
Output: COE in \$/KWH	0.149
Y(E)=yield per chamber (MJ)	641
M=Energy multiplication factor	1.15
Net Electric Power (MW)	651

Proven Units with 7.8% Cost of Capital and 1.0 MIT 2009 Study Factor to 2007\$ gives 7.6 cents/kw-hr.

Input: Nc=number of chambers	1.00
Input: RR=rep rate in shots per chamber per second	3.00
Input: Discount or Hurdle Rate for attracting capital	7.80%
MIT Escalation Factor	1
Approximation to Pe (MW)	866
Eta=thermal to electrical	0.44
\$/Joule for Bank Energy	2.00
Energy Store (MJ)	85.0
η_{G_bank}	7.5
Net Electrical Power (MW)	651
Output: COE in \$/KWH	0.076
Y(E)=yield per chamber (MJ)	641
M=Energy multiplication factor	1.15
Net Electric Power (MW)	651

QSDD Capsule, Cylindrical RTL, Survivable Inverse Diode,
Magnetically Insulated LTD.

Saturn could prototype the PPS Inverse Diode, RTL, and QSDD Capsule.



QSDD baseline with 17.5 mg mass has 4 cm/ μ s velocity.
QSDD surrogate with 1.4 mg mass has 22 cm/ μ s velocity.



Many issues need to be addressed.

- Better mitigation of wall instability
- Experimental demonstration of QSDD performance
- High-resolution Gorgon, LASNEX, or Hydra simulations at 500 MJ yield with $di/dt \sim 1.5 \times 10^{15}$ A/s
- Experimental demonstration of $> 90\%$ current efficiency with Direct Inverse Diode (DID)
- Survivable anode at 560 A/cm^2 electron injection
- 2D simulations of blast and radius for survivability
- Simulation of chamber recovery for 3 Hz operation
- LiXY working fluid with $< 3 \times 10^{-5}$ Torr vapor pressure at 400°C
- Liquid metal MITL anode
- Ignition on short pulse modification of Z