

Atoms-to-Continuum (AtC) user package for LAMMPS

**Jonathan Zimmerman, Reese Jones,
Jeremy Templeton, Gregory Wagner
Sandia National Laboratories**

Objectives for User Package

- **Calculation of continuum mechanical variables from atomistic simulation data using the Hardy's Eulerian formulation and our Lagrangian formulation.**
- **Coupling of atomistic (molecular statics / dynamics) and continuum (finite element) regions for rigorous thermal and mechanical boundary conditions.**
- **Coupling to emulate electronic temperature effects in metals via the two temperature model (TTM).**

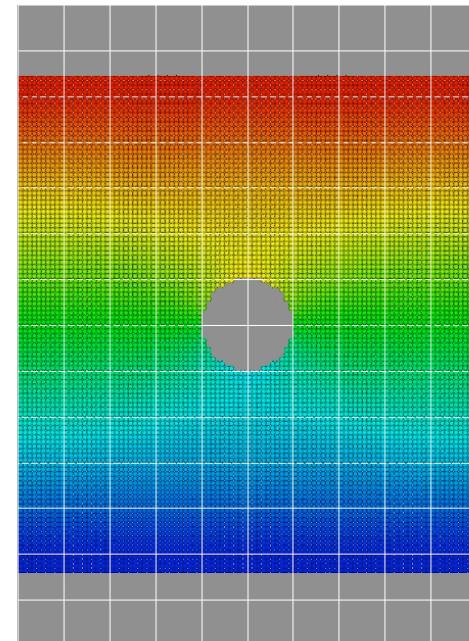
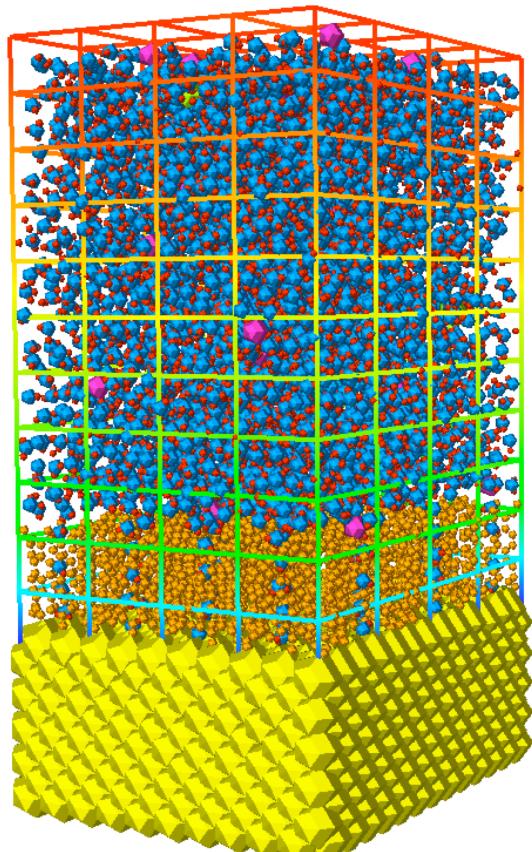
fix atc

fix ID groupID atc type paramfile

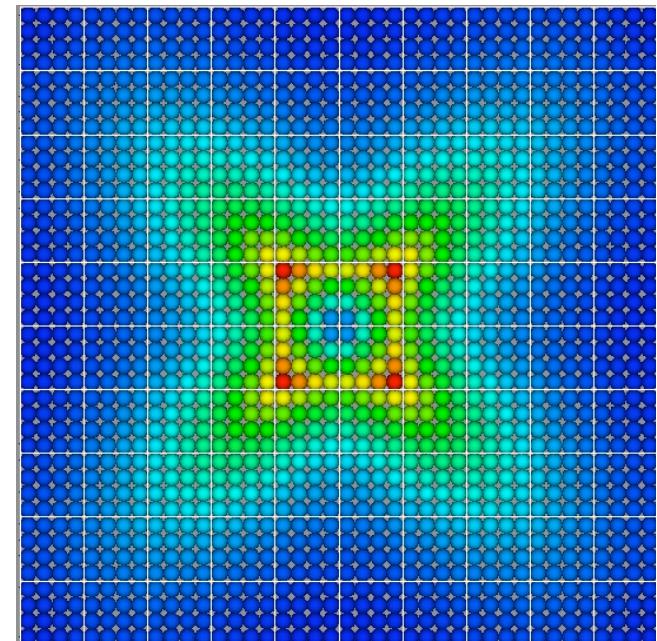
- ID, group-ID are documented in fix command
- **type** = *thermal* or *two_temperature* or *hardy*
 - *thermal* = thermal coupling with field: temperature
 - *two_temperature* = electron-phonon coupling with field, temperature and electron_temperature
 - *hardy* = Hardy on-the-fly post-processing
- **paramfile** = file with material parameters (not specified for *hardy* type)

The atc picture: mesh, box and atoms

*Saltwater-electrode-CNT
system: mesh overlaps exactly
with water-CNT atom region*



*Circular hole in plate:
mesh overlaps exactly
with box, but atom region
is subset*



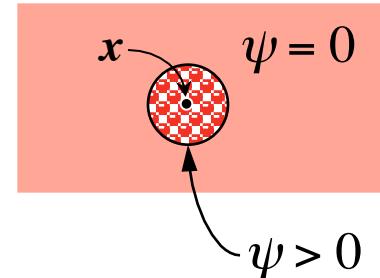
*Elastic inclusion problem:
mesh overlaps exactly
with box and atoms*

Hardy on-the-fly post-processing

$$\sigma(\mathbf{x}, t) = - \left\{ \frac{1}{2} \sum_{\alpha=1}^N \sum_{\beta \neq \alpha}^N \mathbf{x}^{\alpha\beta} \otimes \mathbf{f}^{\alpha\beta} B^{\alpha\beta}(\mathbf{x}) + \sum_{\alpha=1}^N m^\alpha \hat{\mathbf{v}}^\alpha \otimes \hat{\mathbf{v}}^\alpha \psi(\mathbf{x}^\alpha - \mathbf{x}) \right\}$$

$$\mathbf{P}(\mathbf{X}, t) = - \frac{1}{2} \sum_{\alpha=1}^N \sum_{\beta \neq \alpha}^N \mathbf{f}^{\alpha\beta} \otimes \mathbf{X}^{\alpha\beta} B^{\alpha\beta}(\mathbf{X})$$

$$\mathbf{q}(\mathbf{x}, t) = - \sum_{\alpha=1}^N \sum_{\beta \neq \alpha}^N \frac{\mathbf{x}^{\alpha\beta}}{x^{\alpha\beta}} \frac{\partial \phi_\beta}{\partial x^{\alpha\beta}} (\mathbf{x}^{\alpha\beta} \cdot \hat{\mathbf{v}}^\alpha) B^{\alpha\beta}(\mathbf{x}) + \sum_{\alpha=1}^N \left\{ \frac{1}{2} m^\alpha (\hat{v}^\alpha)^2 + \phi^\alpha \right\} \hat{\mathbf{v}}^\alpha \psi(\mathbf{x}^\alpha - \mathbf{x})$$



```

# ...create and initialize the MD system
fix AtC internal atc hardy
fix_modify AtC fem create mesh 1 1 1 box p p p
fix_modify AtC atom_element_map eulerian 100
fix_modify AtC transfer fields none
fix_modify AtC transfer fields add density energy
    stress temperature
fix_modify AtC transfer output nvtFE 100 text
run 1000

```

Common fix_modify commands for atc-hardy

Setup:

```
fix_modify AtC fem create mesh  
fix_modify AtC transfer internal
```

Control and time filtering:

```
fix_modify AtC transfer filter  
fix_modify AtC transfer filter scale  
fix_modify AtC transfer atom_element_map  
fix_modify AtC transfer neighbor_reset_frequency  
fix_modify AtC transfer kernel
```

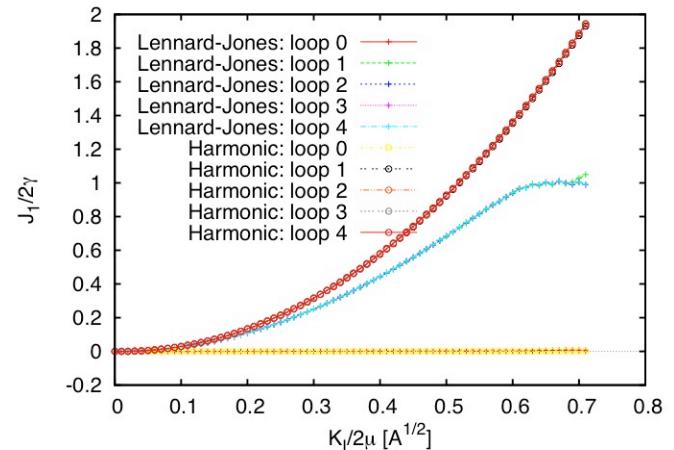
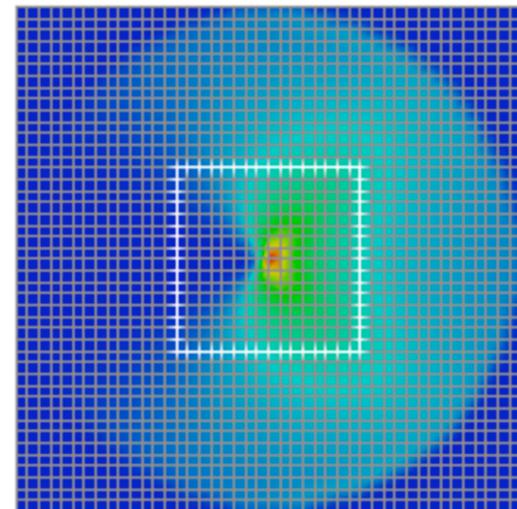
Output: text and EnSight

```
fix_modify AtC transfer output  
fix_modify AtC transfer atomic_output  
fix_modify AtC mesh output
```

Common fix_modify commands for atc-hardy

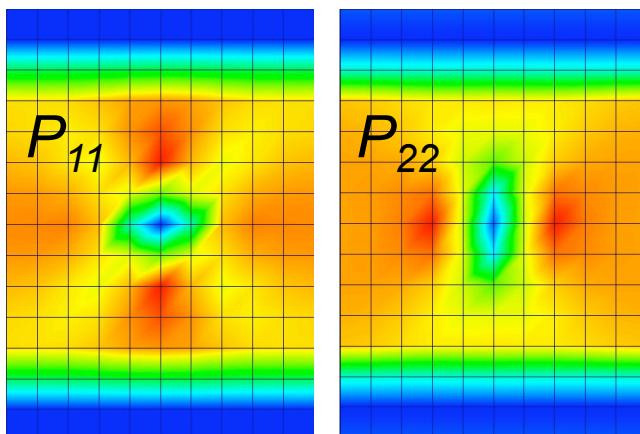
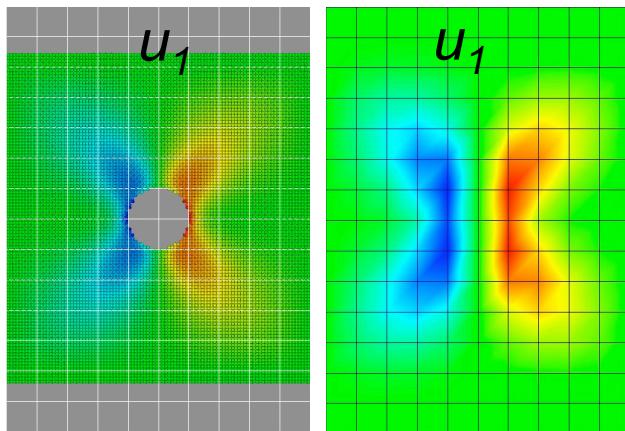
Computation of fields:

```
fix_modify AtC transfer fields
fix_modify AtC transfer gradients
fix_modify AtC transfer rates
fix_modify AtC transfer computes
fix_modify AtC transfer on_the_fly
fix_modify AtC boundary_integral
fix_modify AtC contour_integral
```

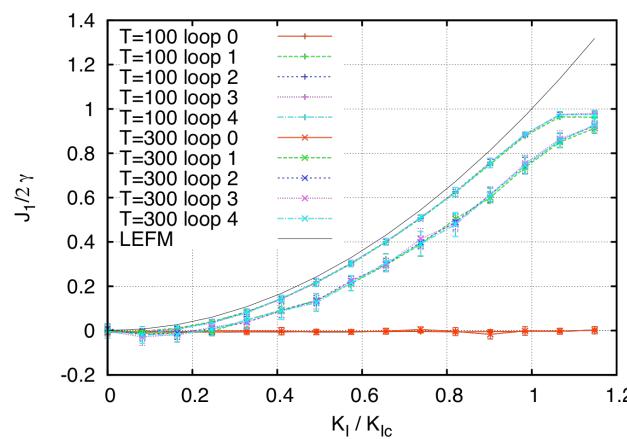
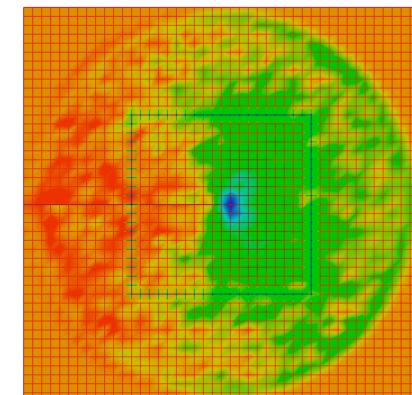
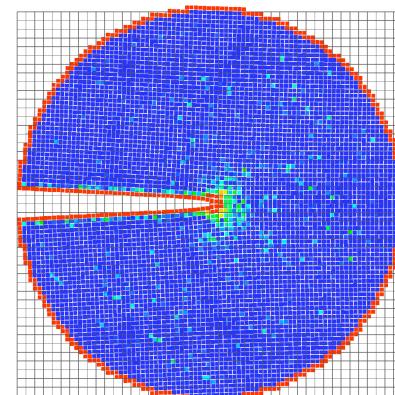


Examples of using atc-hardy

Tensile stretching of plate with circular hole



Compressive stress field for an atomic simulation of shock loading



Calculation of local values of atomic potential energy, Eshelby tensor, and J-integral at finite temperature

TMS 2011

Thermal coupling using atc

- Coupled FEM/MD equations

$$\sum_J M_{IJ} \dot{\theta}_J = \frac{2}{3k_B} \sum_{\alpha} N_{I\alpha} (\mathbf{v}_{\alpha} \cdot \mathbf{f}_{\alpha}) \Delta V_{\alpha} + \sum_J K_{IJ}^{fem} \theta_J$$

$$m_{\alpha} \dot{\mathbf{v}}_{\alpha} = -\frac{\partial U}{\partial \mathbf{x}_{\alpha}} - \sum_I N_{I\alpha} \lambda_I \mathbf{v}_{\alpha}$$

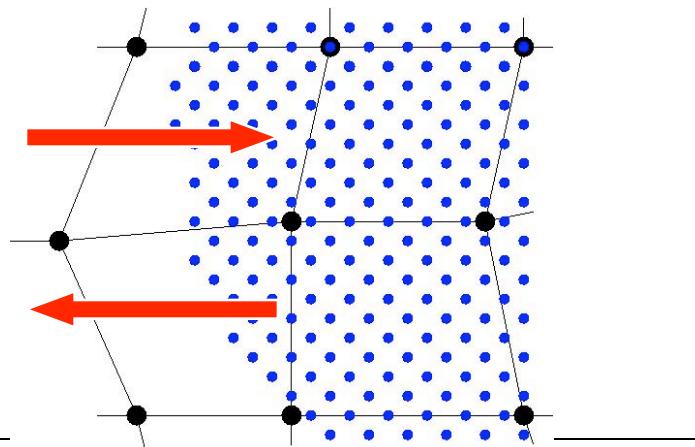
**Coupling parameter
(temperature/flux constraint)**



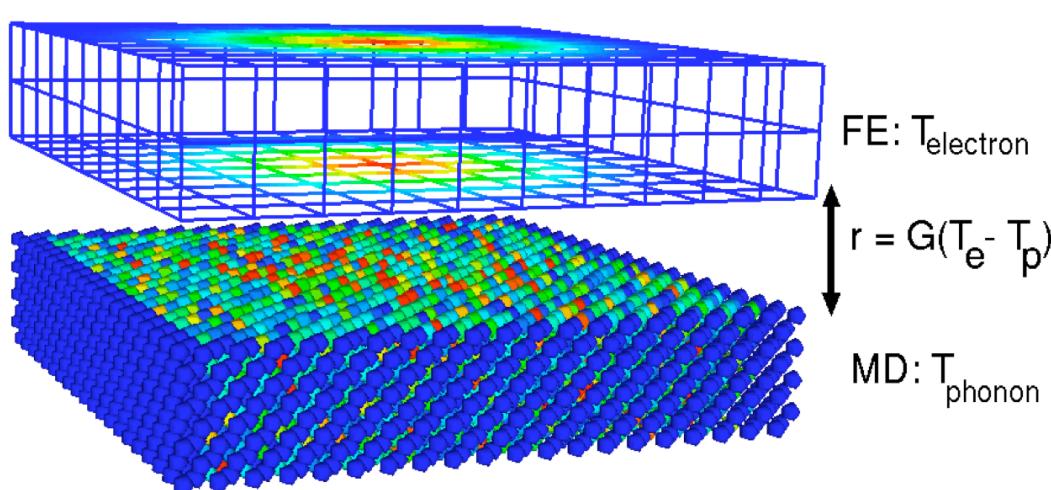
Atoms contribute to nodal heat equation

- Combined MD/FEM system has two-way coupling:

Heat at nodes affects MD energy through thermostat



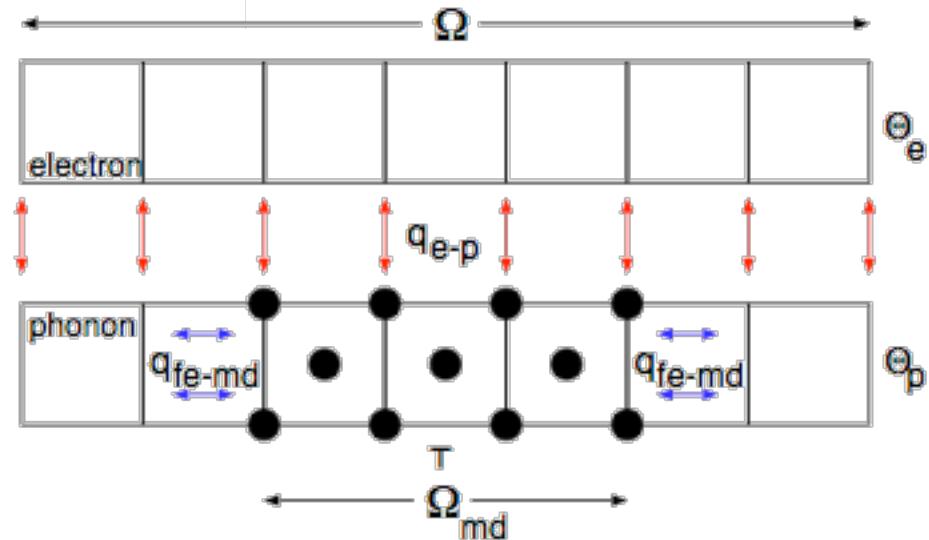
Two-Temperature coupling using atc



Energy exchange handled through thermostats as in the thermal-only problem

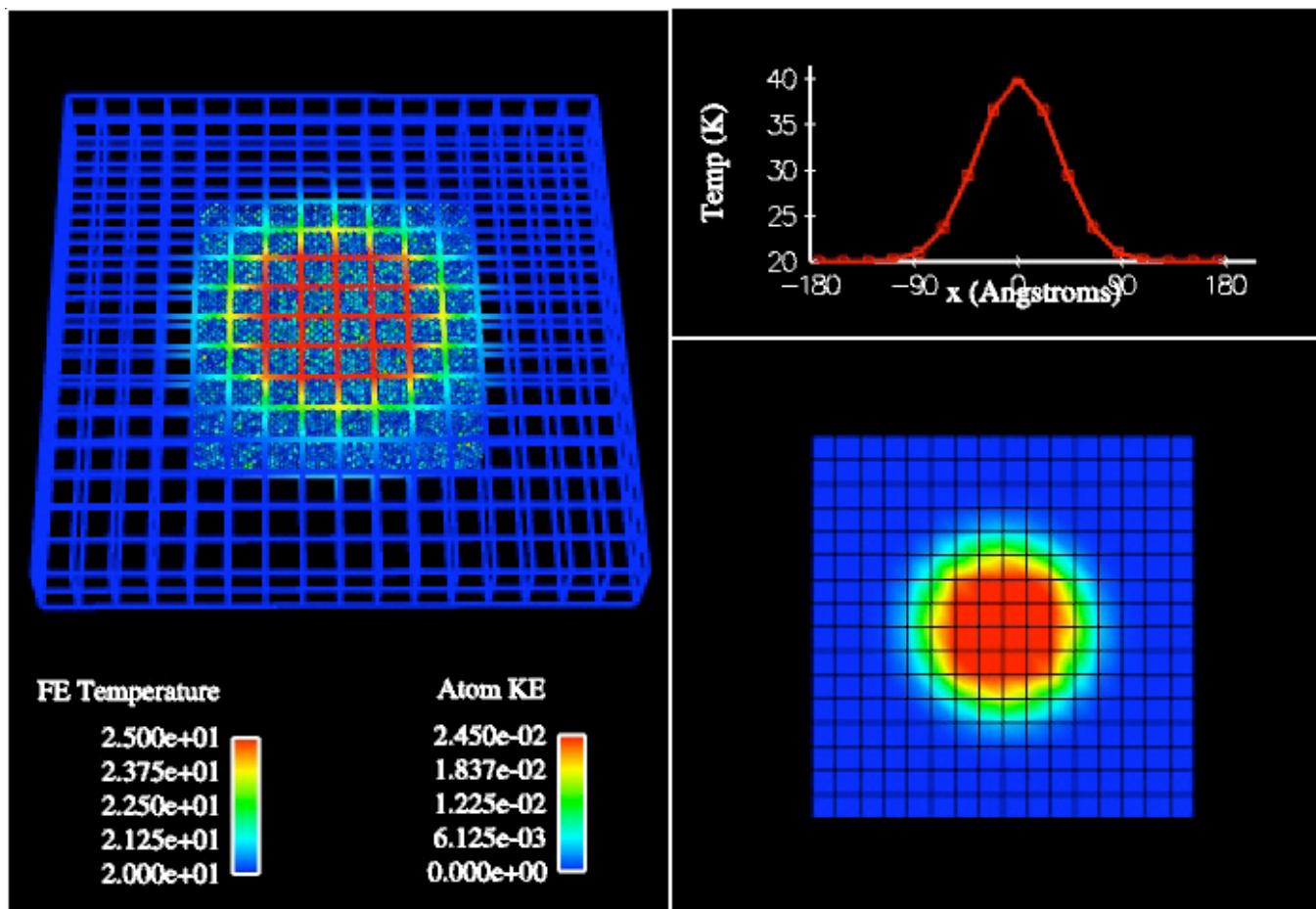
Explicit representation of phonons by MD

Electron effects solved for on overlaid mesh



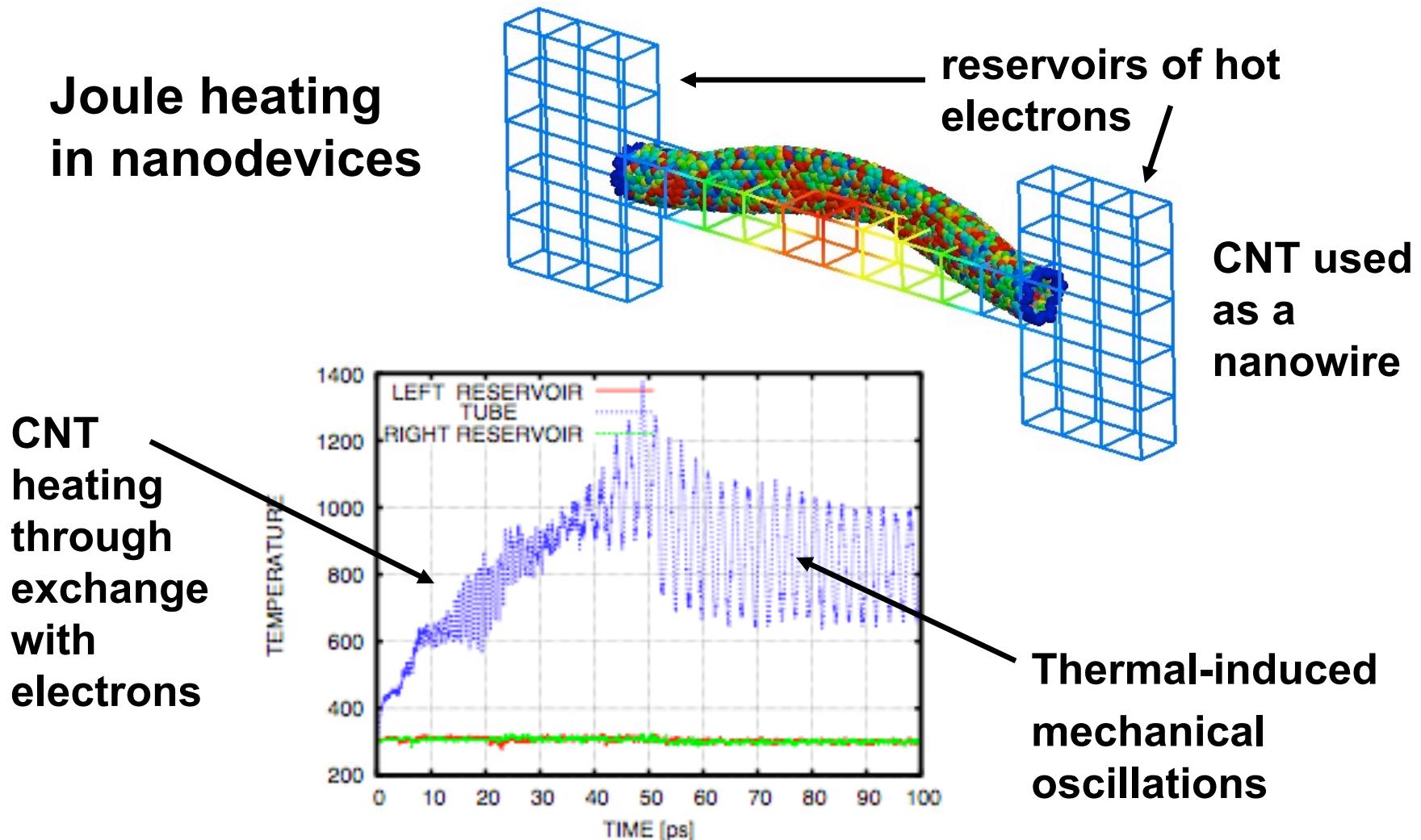
Example of using atc-thermal

2D diffusion problem



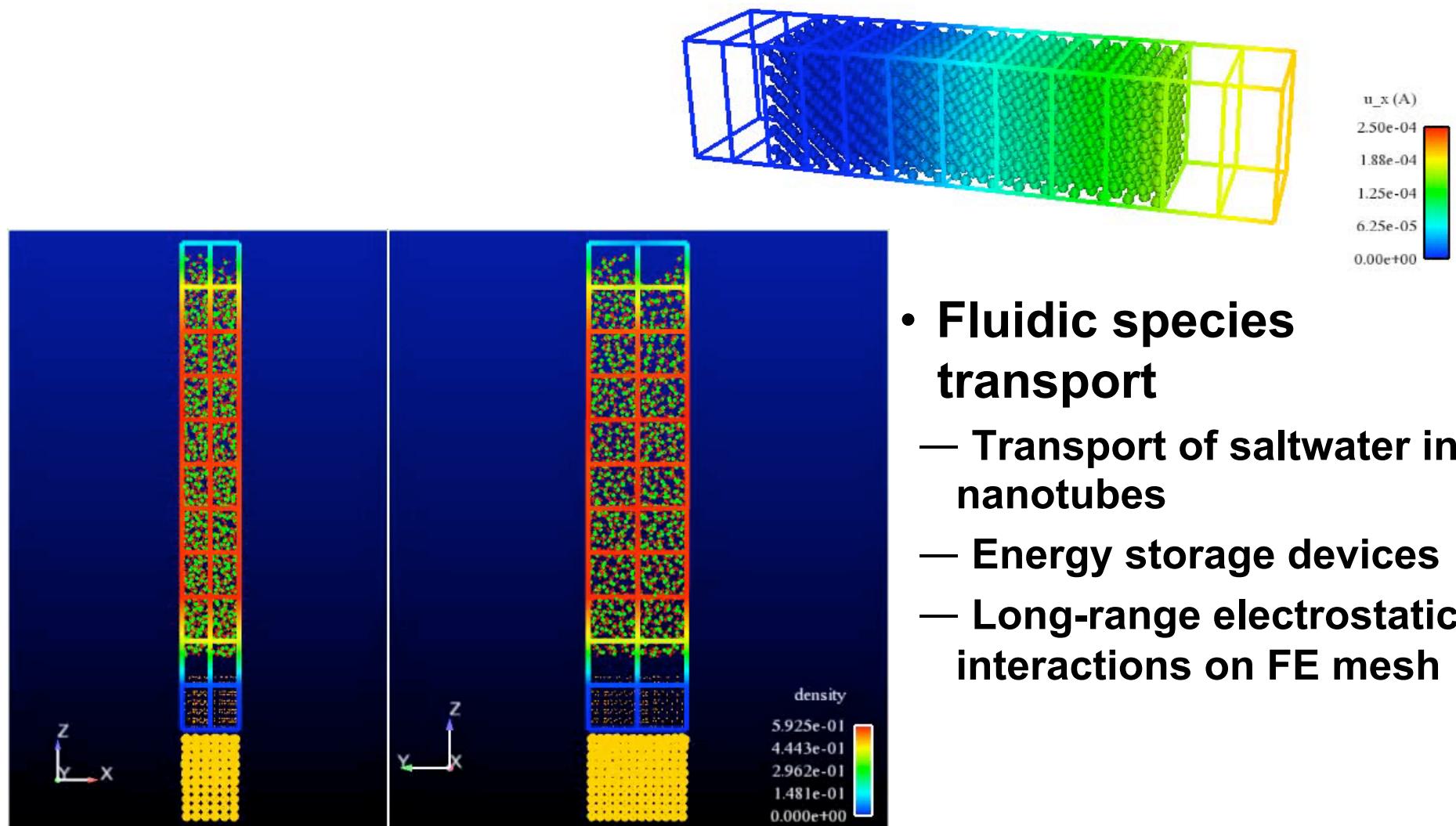
- Plate with embedded MD region (~33,000 atoms)
- Initialized to temperature field with Gaussian profile
- Adiabatic boundary conditions at edges

Example of using atc-two temperature



Future efforts

- Elasto-dynamic response at the nano-scale



Concluding Remarks

- **References:**
 - atc-hardy
 - Zimmerman, Jones and Templeton, *J. Comput. Phys.* (2010)
 - Jones and Zimmerman, *J. Mech. Phys. Solids* (2010)
 - Jones *et al.*, *J. Phys.: Condens. Matter* (2010)
 - atc-thermal
 - Wagner *et al.*, *Comp. Meth. Appl. Mech. Eng.* (2008)
 - Templeton, Jones and Wagner, *Model. Simul. Mater. Sci. Eng* (2010)
 - atc-two temperature
 - Jones *et al.*, *Intl. J. Numer. Meth. Eng.* (2010)
- **Simulations performed with LAMMPS MD code:**
<http://lammps.sandia.gov>

Sandia National Laboratories is a multi-program laboratory managed and operated by Sandia Corporation, a wholly owned subsidiary of Lockheed Martin Corporation, for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000.