

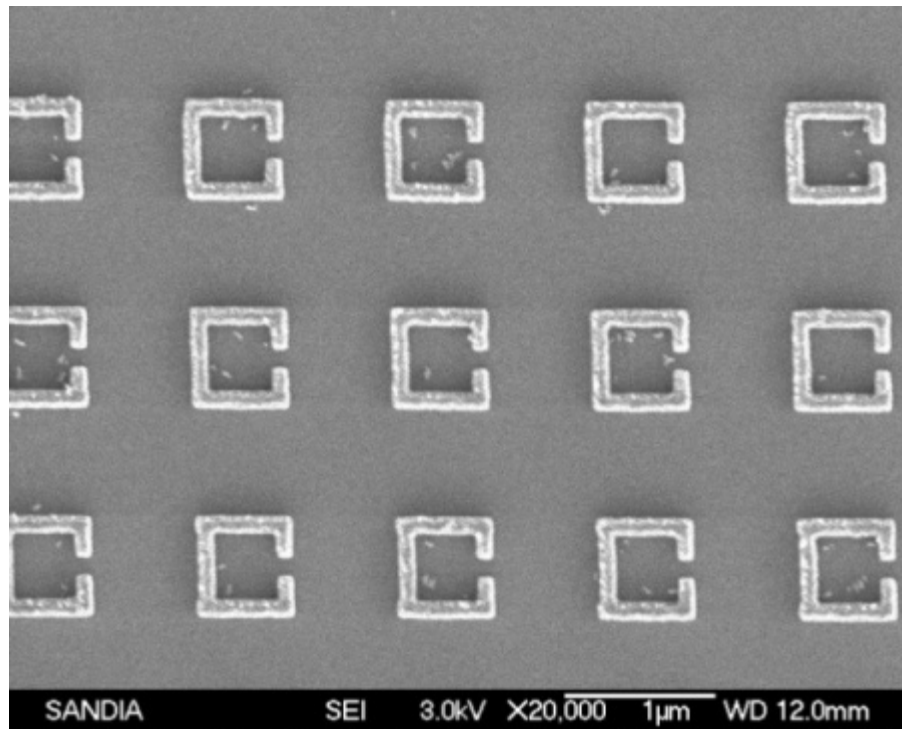
Subcell Models with Application to Split-Ring Resonators in the Infrared

2011 IEEE International Symposium on Antennas and
Propagation and USNC/URSI National Radio
Science Meeting

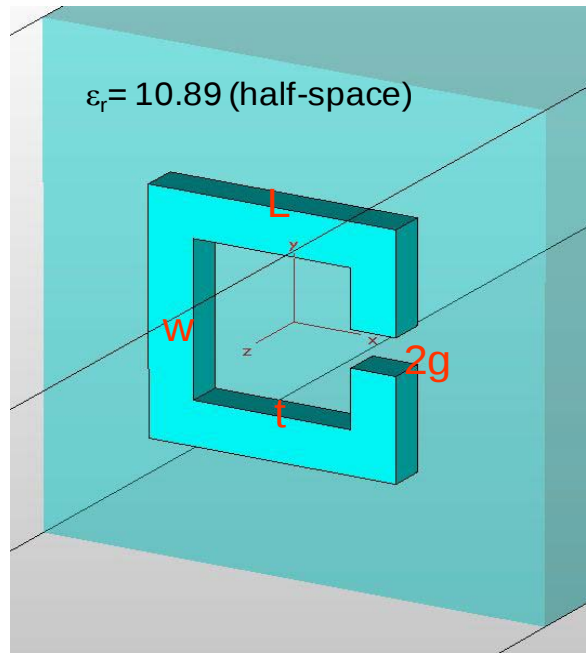
7/04/2011

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William L. Langston, and Michael B. Sinclair

A rectangular lattice of gold split-ring resonators on top of a GaAs half-space



A single gold split-ring resonator on top of a thick GaAs half-space



The dimensions of the SRR are $2g=0.10 \mu\text{m}$, $L=0.66 \mu\text{m}$, $t=0.1 \mu\text{m}$, $w=0.12 \mu\text{m}$.
The relative permittivity of the substrate is $\epsilon_r = 10.89$



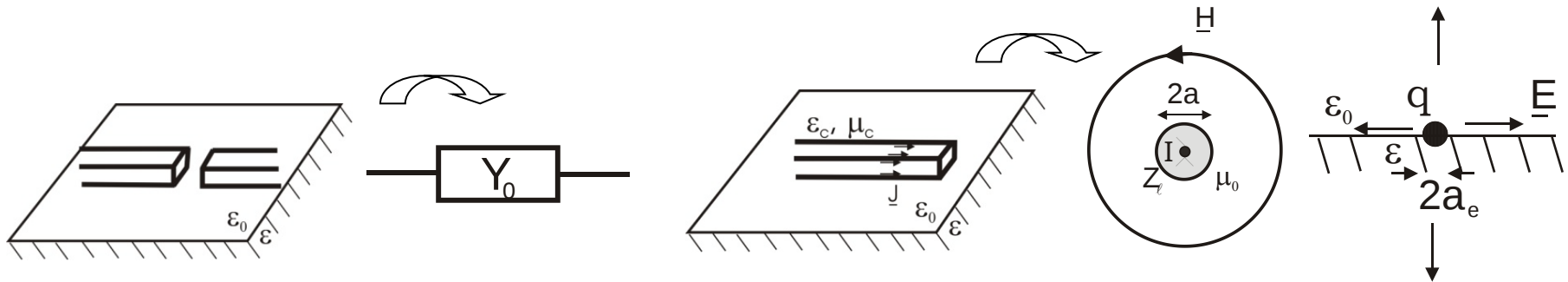
Outline

- ❑ Subcell Models
 - capacitive corrections
 - internal impedance correction
- ❑ Comparison of Subcell Models and Explicit-Mesh Simulations
- ❑ Applications and HPC Subcell Calculations

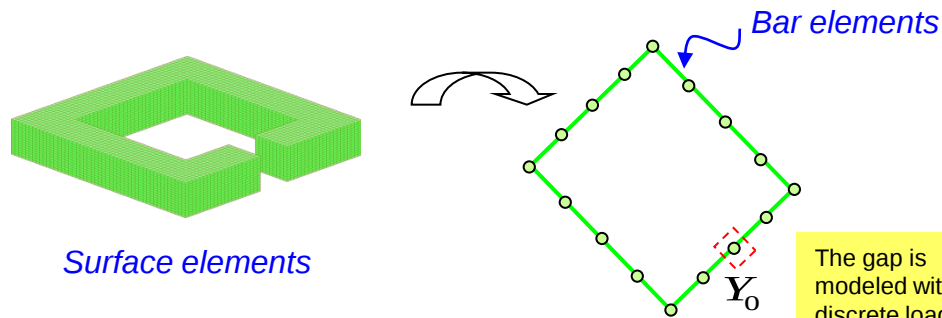
Subcell Models

❖ Local descriptions

- Equivalent radius (Hallen)
- Equivalent radius on dielectric half space
- Impedance per unit length expansion (Cockcroft, Vainshstein, Zhurav, Warne, Holloway)
- Internal admittance per unit length (negligible effect for metals)
- Gap, fringe, and transition capacitance



Rectangular SRR Example



The gap is modeled with a discrete load.

Subcell: Gap and Fringe Capacitance

Capacitance Correction of thin wire:

$$\Delta C \approx \frac{1}{\pi} (\varepsilon + \varepsilon_0) (w + t) \left[\ln(2a_e / g) - .5772 - \frac{2}{15} \right]$$

$$C_{pp} = \varepsilon_0 \frac{wt}{2g}$$

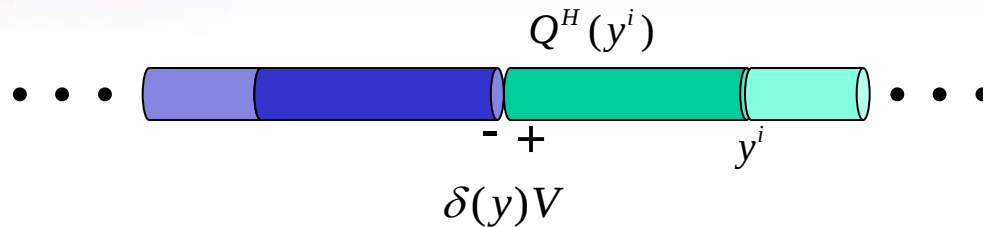
$$a_e \approx 0.036 \mu\text{m} \text{ (GaAs half-space)}$$

$$a_e = a \approx 0.065 \mu\text{m} \text{ (air)}$$

$$\Delta C + C_{pp} = (-2.5206 + 1.0625) \text{ aF} = -1.4581 \text{ aF (GaAs half-space)}$$

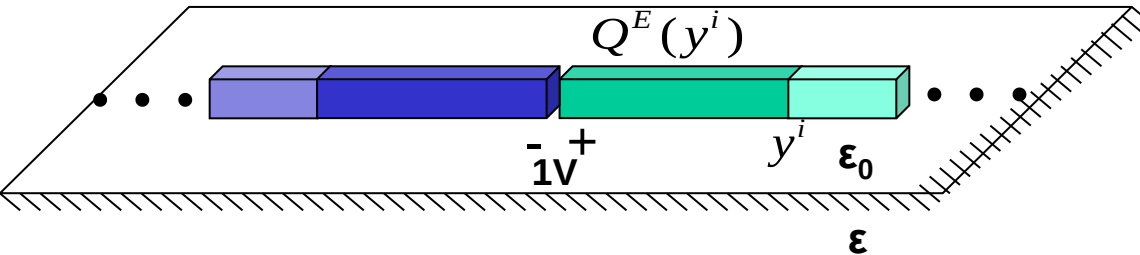
$$\Delta C + C_{pp} = (0.3011 + 1.0625) \text{ aF} = 1.3636 \text{ aF (air)}$$

Subcell Capacitance Corrections: Hallen and EIGER facet 4



$$C^H(y^i) = \frac{\varepsilon + \varepsilon_0}{2\varepsilon_0} Q^H(y^i)$$

$$C^H(y^i) = 63.727 \text{ aF}, 12.960 \text{ aF}$$



$$C_E^i = Q^E(y^i) = \sum_{l=1}^i q_E^l$$

$$Q^E(y^i) = 61.321 \text{ aF}, 13.960 \text{ aF}$$

$$C_t = -0.947214 \text{ aF}, -0.36345 \text{ aF}$$

$$C_t = C_E^i - C^H - (\Delta C + C_{pp})$$

$$\Delta C_f = 2a_e (\varepsilon + \varepsilon_0) \left[\ln(4(3.4)a_e / s_0) - \gamma - \frac{1}{9} \right]$$

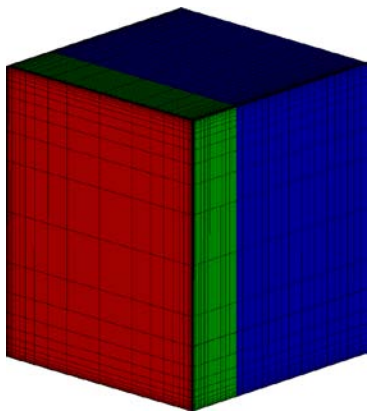
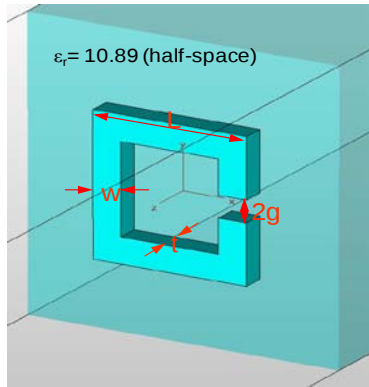
$$\Delta C_f = 9.875 \text{ aF}, 2.7308 \text{ aF}$$

$$C_{Load} = \Delta C + C_{pp} + C_t - \Delta C_f$$

$$C_{Load}^{magneta} = -12.3 \text{ aF}, -1.73 \text{ aF}$$

Electrostatic simulations for improvement of the analytical capacitances

Charge calculations for 1V across the gap and the SRRs arms extended



Index	Color	Top y μm	Length μm	GaAs q/ϵ_0 nCm/F	Air q/ϵ_0 nCm/F
1	red	0.050	0.000	186.6973	168.0576
2	green	0.075	0.025	643.5120	139.8804
3	blue	0.150	0.075	844.6347	191.9064
4	white	0.375	0.225	1663.647	355.1039
5	magenta	1.050	0.675	3587.186	721.7294
6	orange	3.075	2.025	8260.145	1593.920
7	cyan	9.150	6.075	20000.92	3754.312
8	pink	27.375	18.225	50244.16	9255.789
9	light blue	82.050	54.675	129717.3	23578.98
10	black	246.075	164.025	342439.5	61636.23
11	gold	738.150	492.075	925501.6	165389.4
12	grey blue	2214.37	1476.225	2672127.	476384.1

Subcell: impedance per unit length

$$a \approx \frac{1.18(w+t)}{4} \approx .065 \mu m$$

$$Z_s = \frac{\omega \mu_0}{k} \quad (w, t > 4\delta)$$

f (THz)	ϵ_r	k (μm^{-1})	δ (nm)	Z ($\Omega/\mu m$)
31.6	-3753.8 -j1242.7	6.6197 -j41.059	24.3	3.667 +j19.40
63.1	-1051.5 -j185.33	3.7648 -j43.04	23.2	3.829 +j37.62

Near square cross-section:

$$Z \approx \frac{2Z_s}{\pi(w+t)} \left[1 - 0.102 \left(\frac{-4j}{k(w+t)} \right) - \frac{2jZ_s}{\omega \mu_0 (w+t)} \right]$$

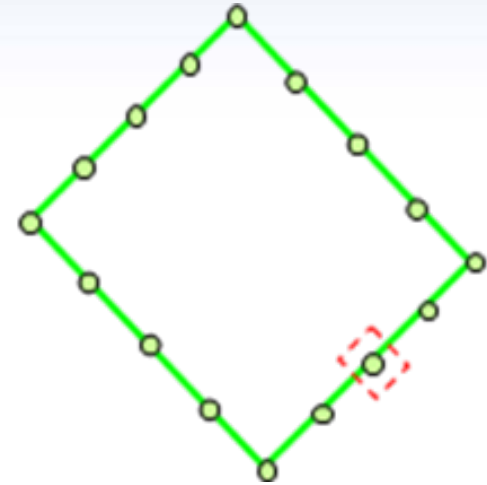
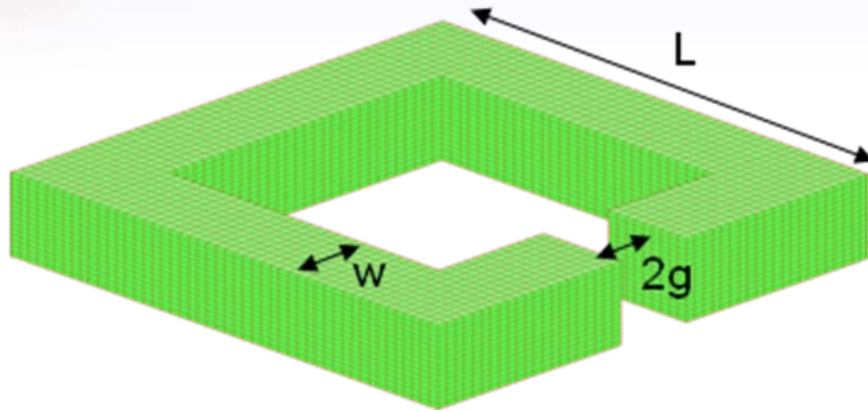
$$\Delta Z_L = Z + \frac{j\omega \mu_0}{2\pi} \ln(a_e / a)$$

$$\Delta Z_C = 0$$

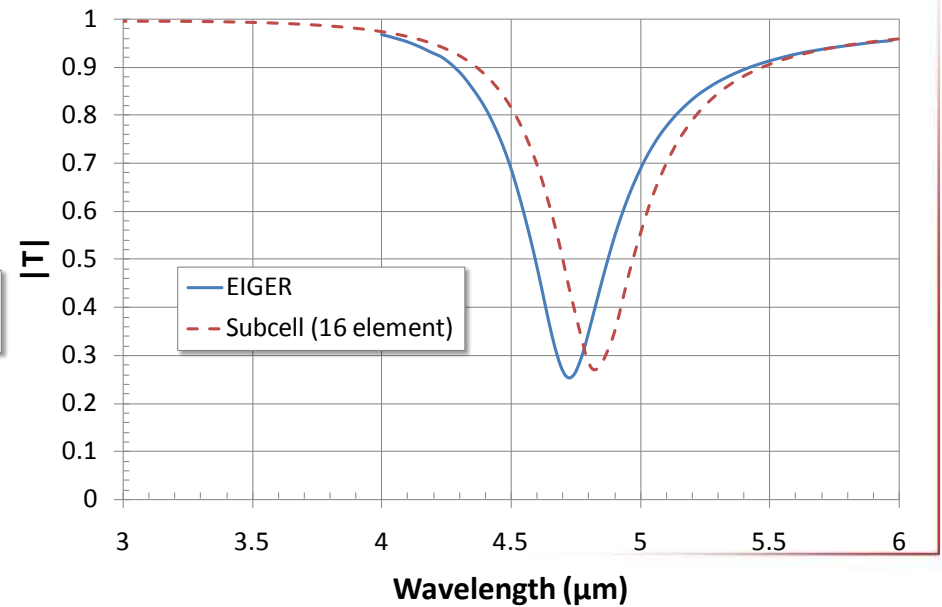
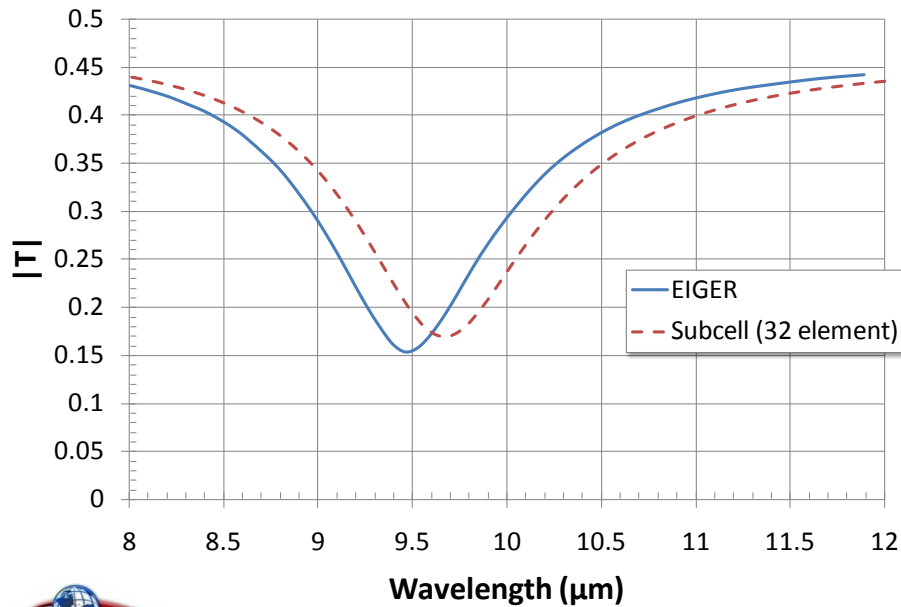
Gold properties at the first resonances of the SRRs **above the GaAs half-space** and **in air**

$$E_s(a_e, s) + \Delta Z_c \frac{d^2}{ds^2} I_s(s) - \Delta Z_L I_s(s) = -E_s^{inc}(s)$$

Comparison of EIGER and Subcell Simulations



1000 to 1 reduction in unknowns and runtime!



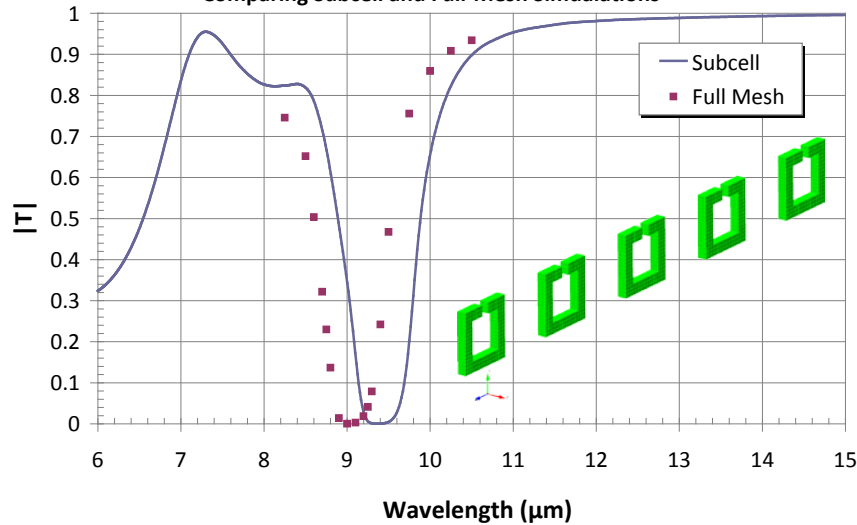


HPC Simulations Subcell Simulations

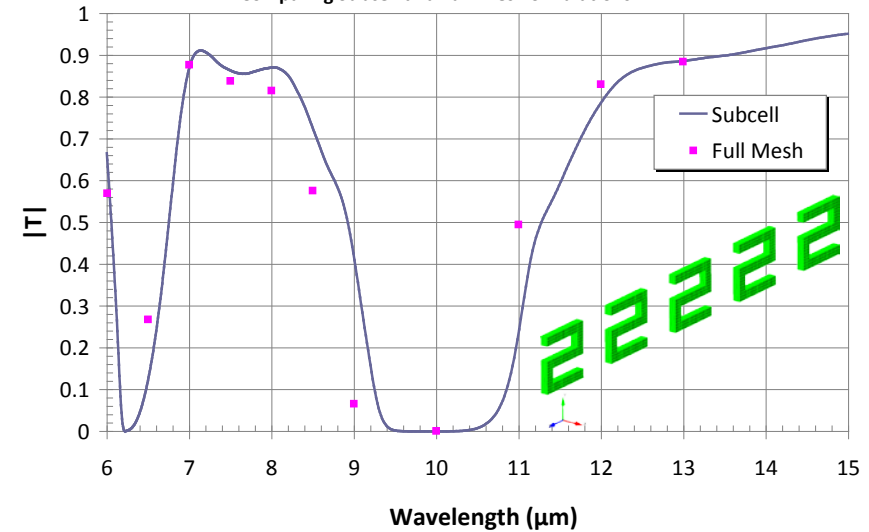
Subcell Models Can be Used For Various Metal Designs



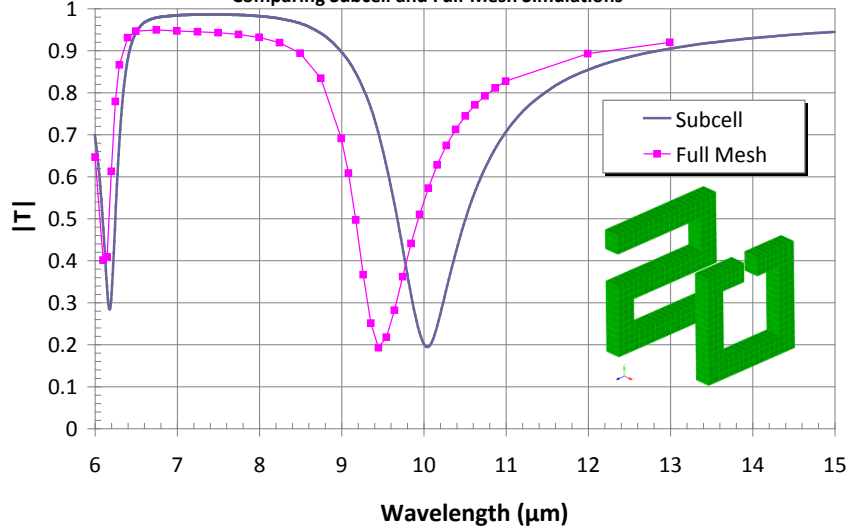
SRR Design B (IR): 5-layers, period=2.82 μm
Comparing Subcell and Full-Mesh Simulations



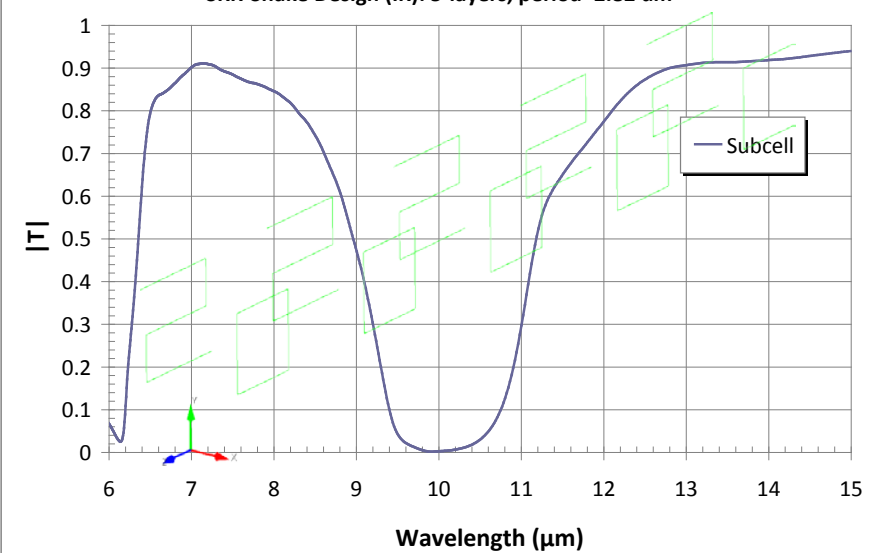
Snake Dipole Design: 5 layers, period=2.82 μm
Comparing Subcell and Full-Mesh Simulations



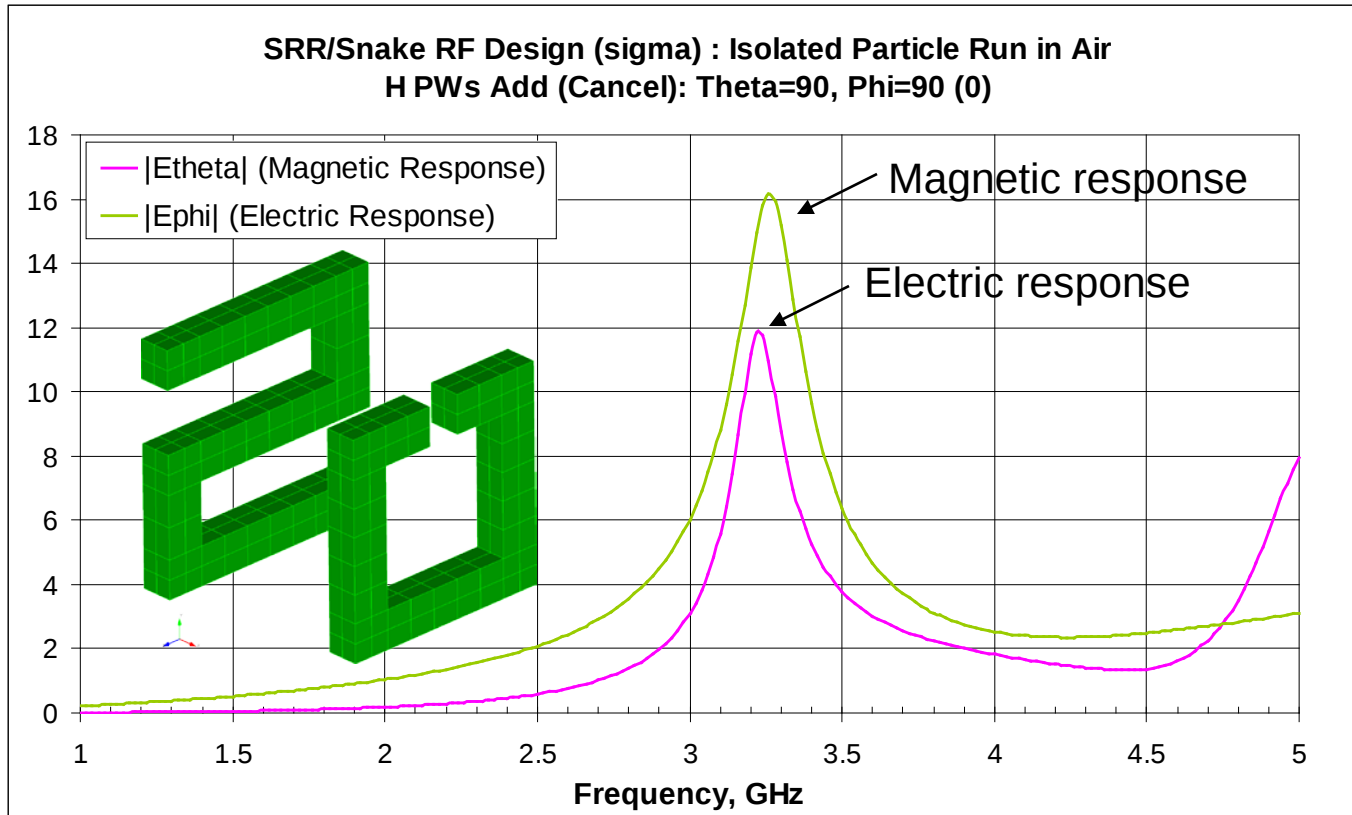
SRR-Snake Design: 1 layer, period=2.82 μm
Comparing Subcell and Full-Mesh Simulations



SRR-Snake Design (IR): 5-layers, period=2.82 μm



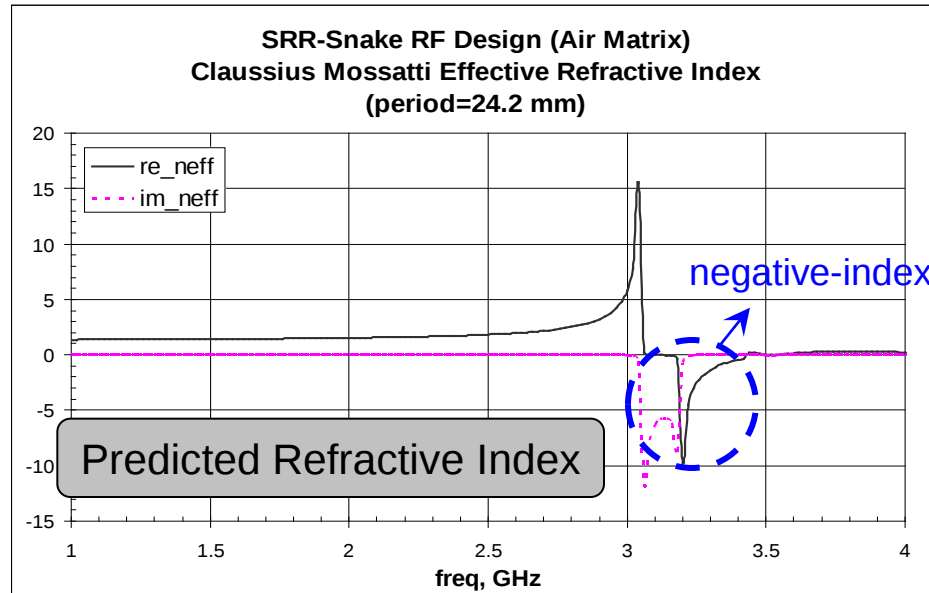
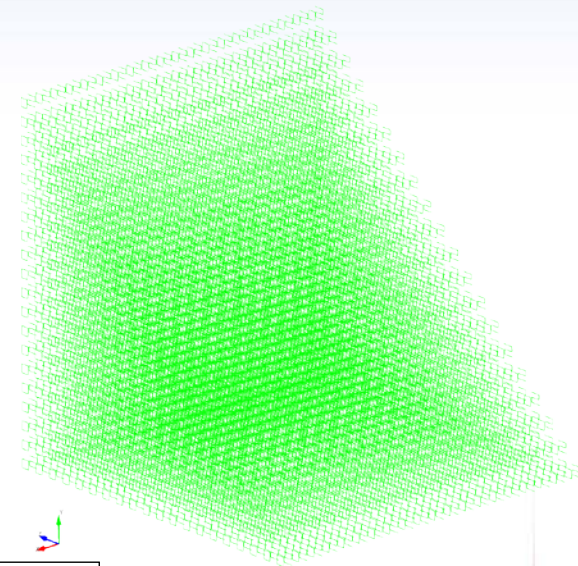
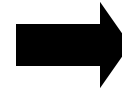
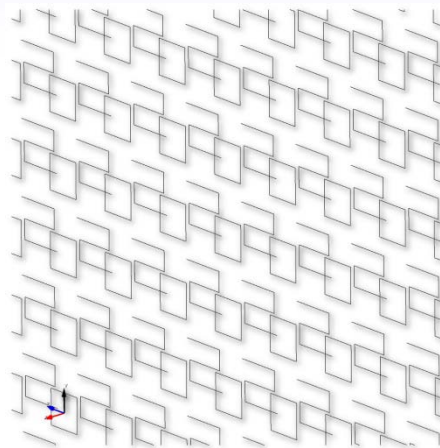
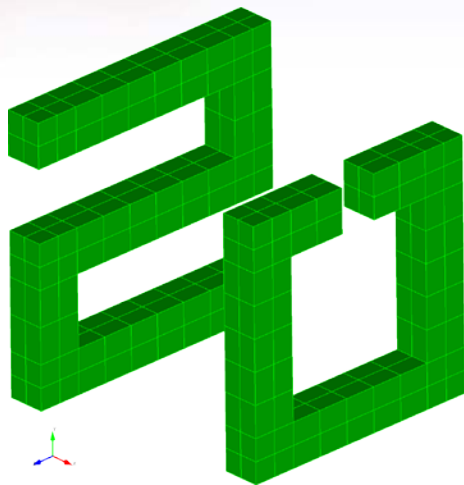
Subcell Models Can Be Used to Model Negative-Index Prisms (3D)



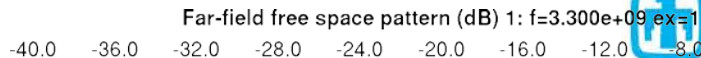
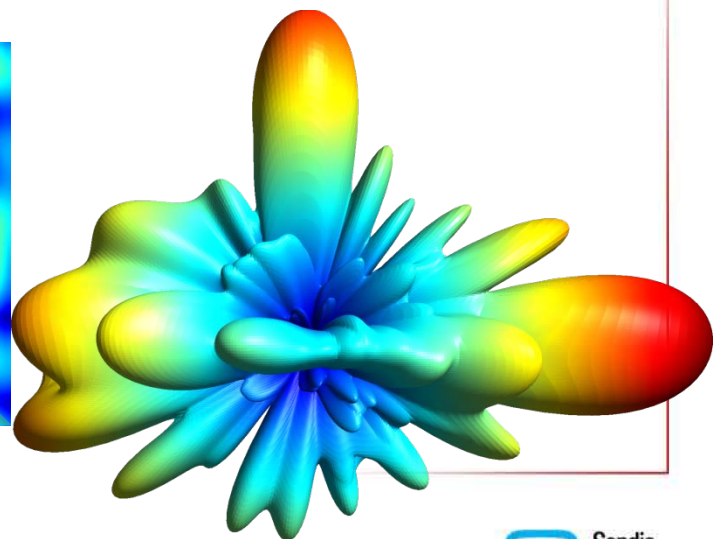
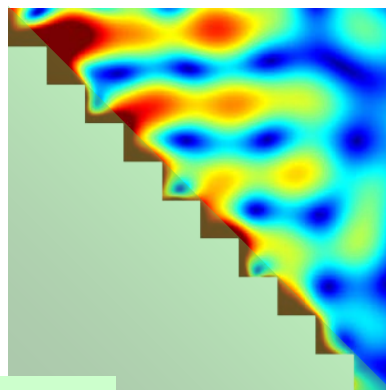
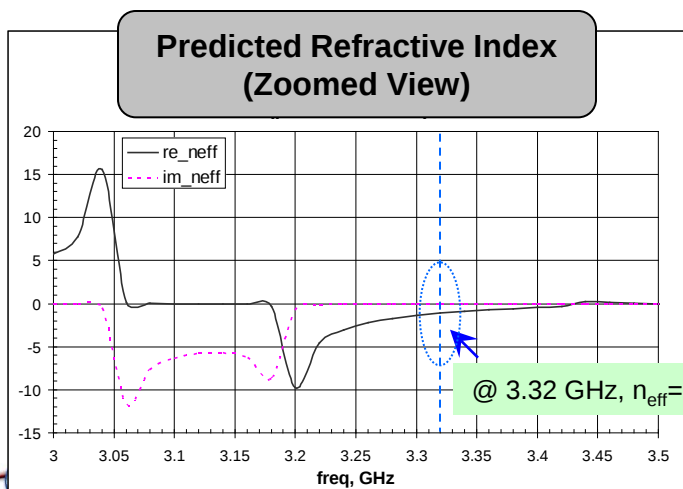
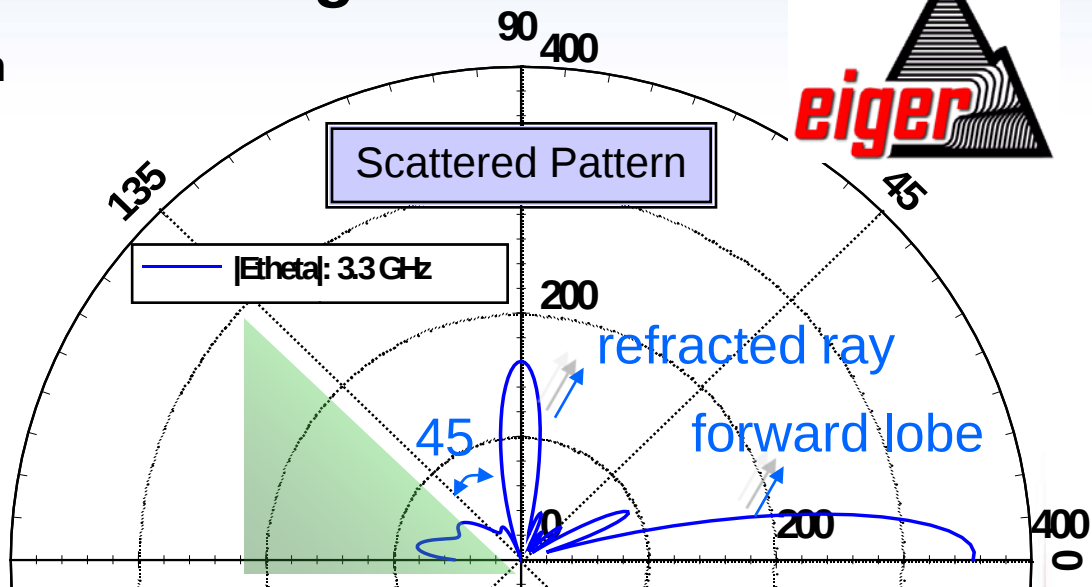
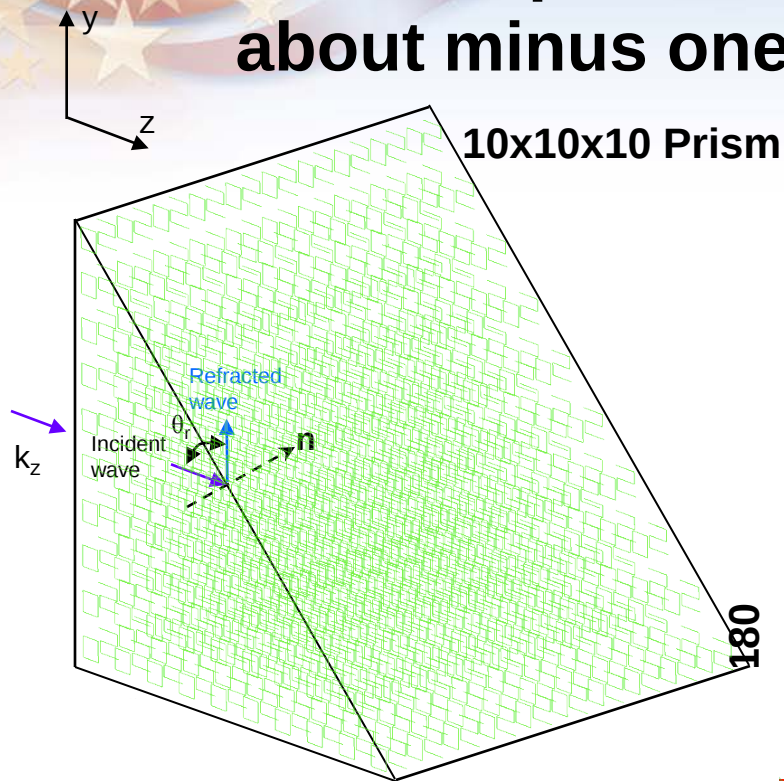
SRR generating magnetic response around 3.2 GHz

Z dipole generating electric response around 3.2 GHz

We assemble a 3D prism of subcells to realize a negative-refractive index

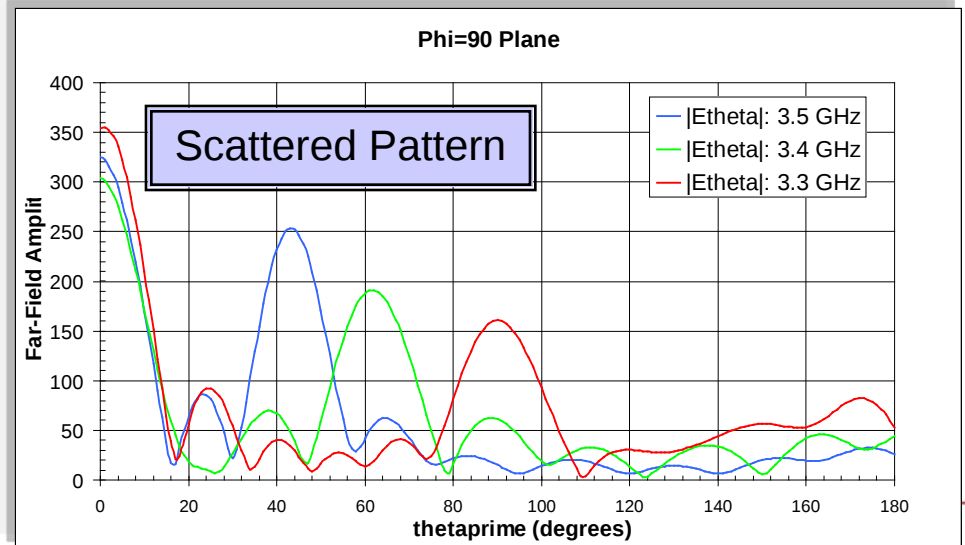
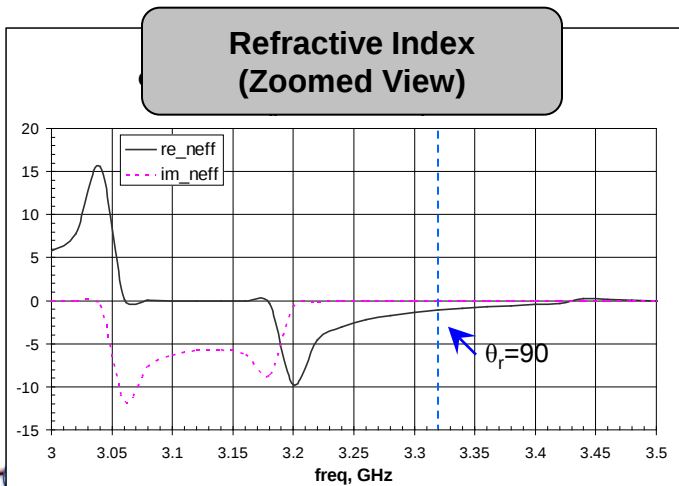
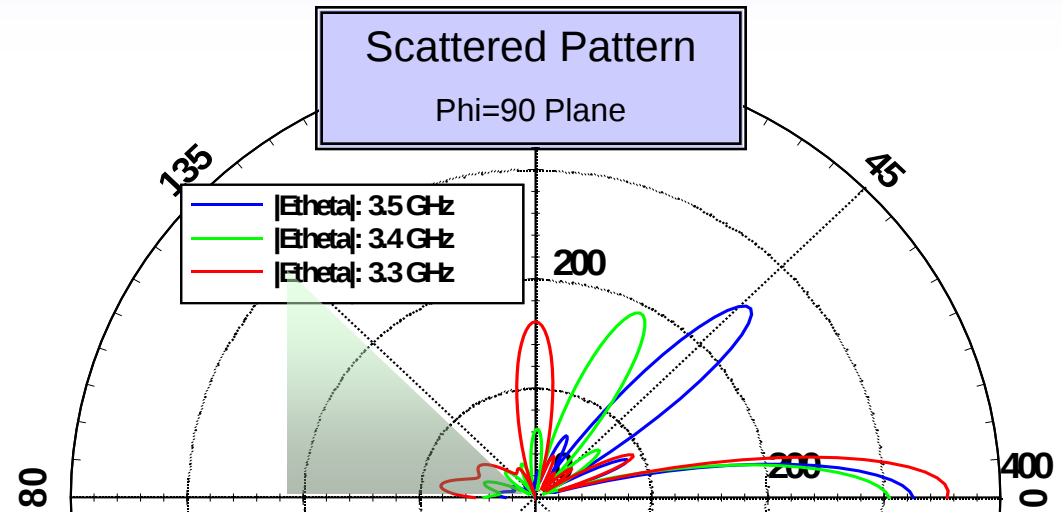
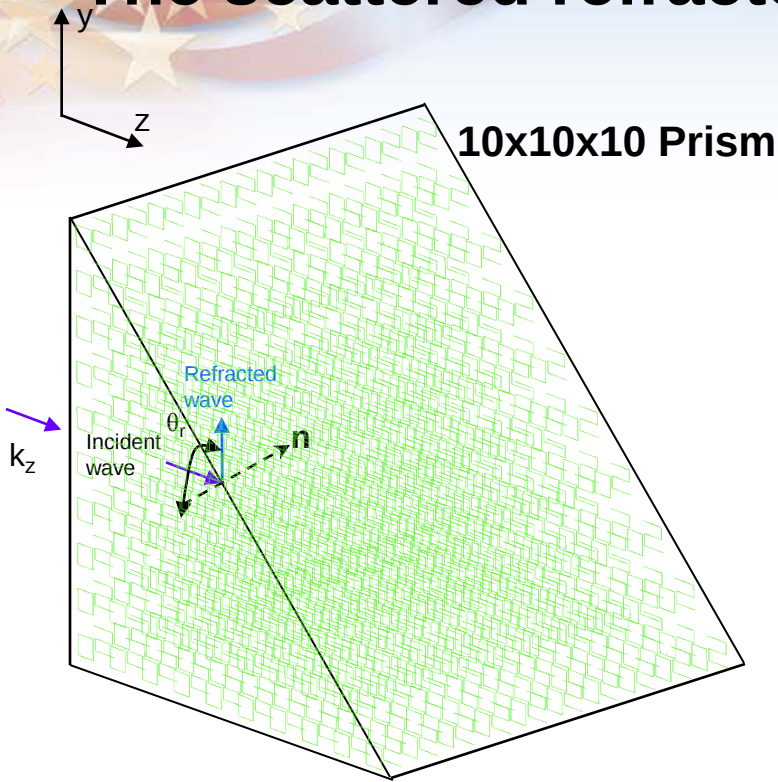


The RF 3D prism run shows a negative index of about minus one occurring around 3.3 GHz

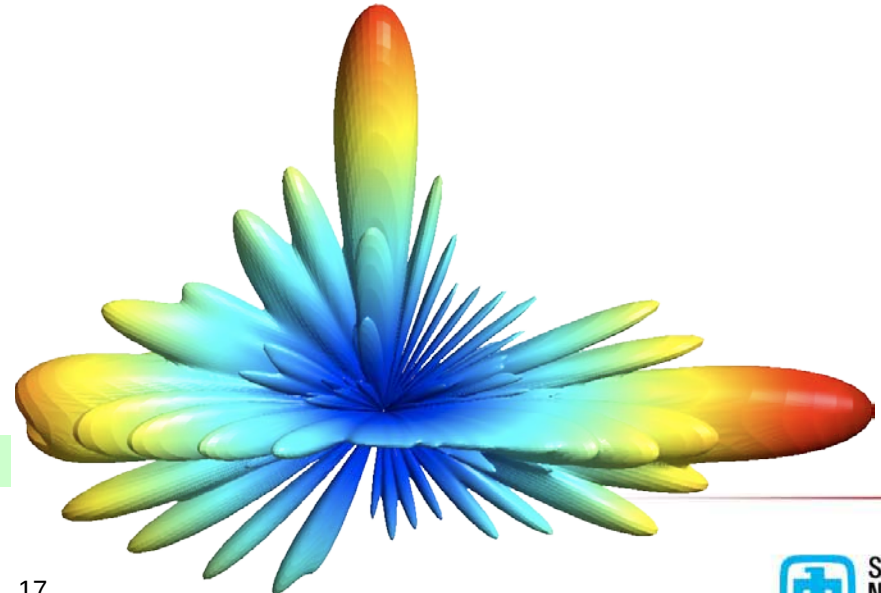
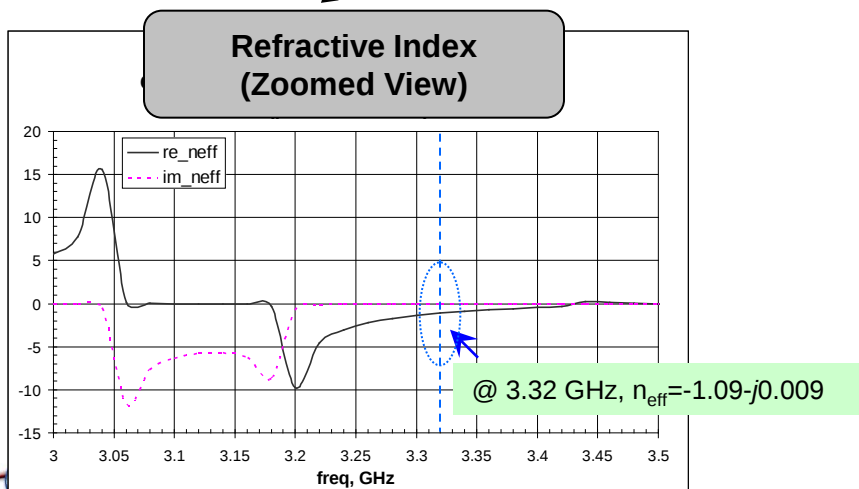
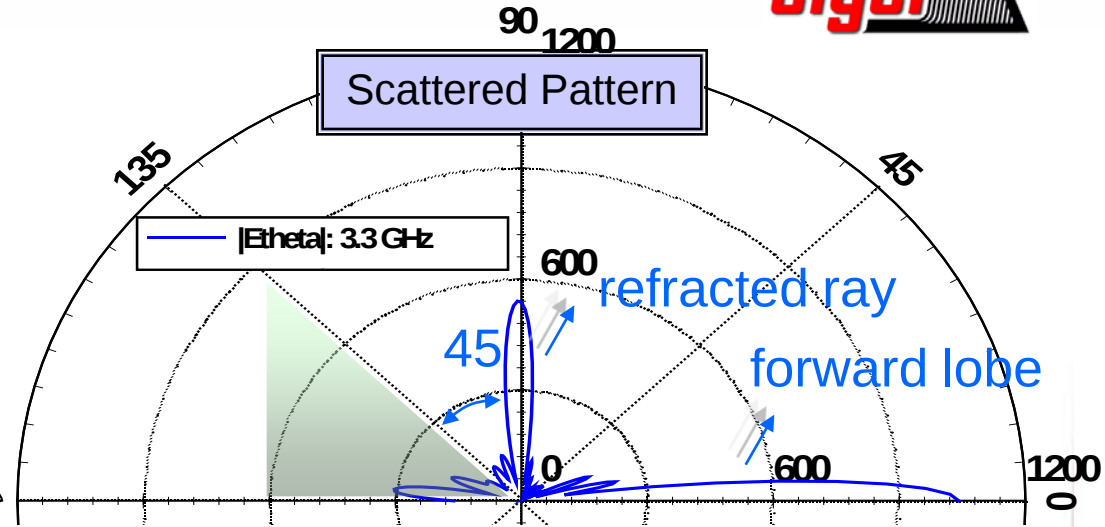
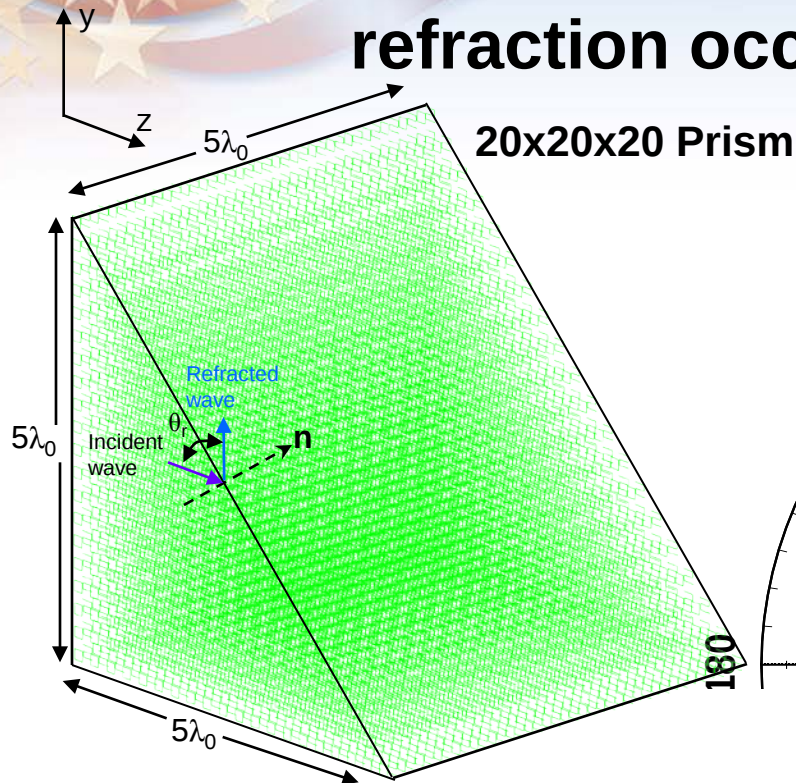


Sandia National Laboratories

The scattered refracted beam scans with frequency



The results of the RF 3D prism run show negative refraction occurring around 3.3 GHz



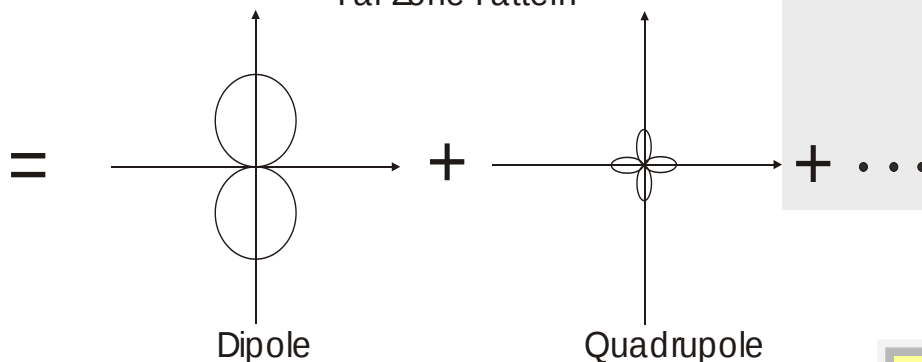
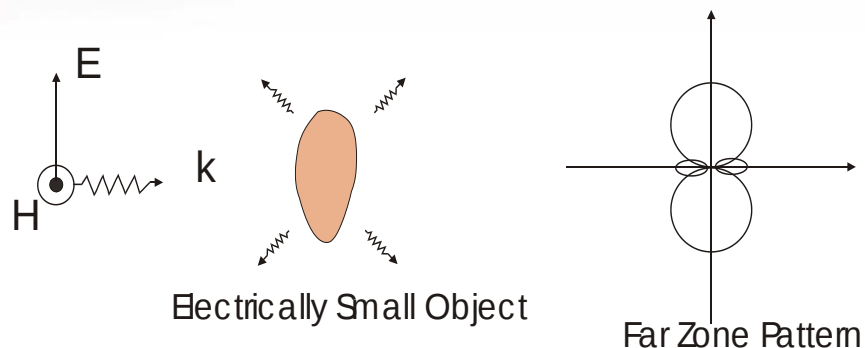
Acknowledgements



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This tool has been very valuable in carrying out this work.

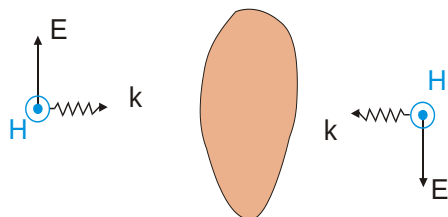
A dual-plane wave excitation of a single resonator simplifies interpretation of effective-media results



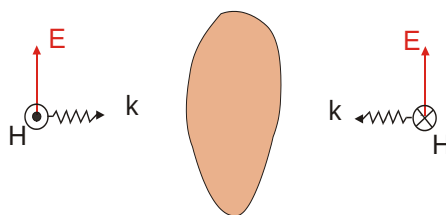
- separate electric and magnetic responses
- far-field amplitudes yield *spectral positions of resonances*
- far-field patterns yield polarizabilities and *type of response*
 - electric vs. magnetic
 - dipole vs. quadrupole
 - effective media parameters (with removal of radiation damping)

Design Procedure: Isolated Particle Simulation and Moments

Magnetic Field Drive



Electric Field Drive



IPSaM

