

Dual Wavelength Pumped 1.550 μ m High Power Optical Parametric Chirped-Pulsed Amplifier System

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Motivation

■ Objective:

- Develop high power ultra-short pulse tunable laser (USPL) sources in the NIR/MWIR.

■ Key Challenges:

- Standard CPA methods do not work well in this regime due to lack of conventional laser gain media in these spectral regions.
- COTS high power technology exists only at 800nm.
- OPCPA Technology is less mature (TRL 2-3).

WHY OPCPA?

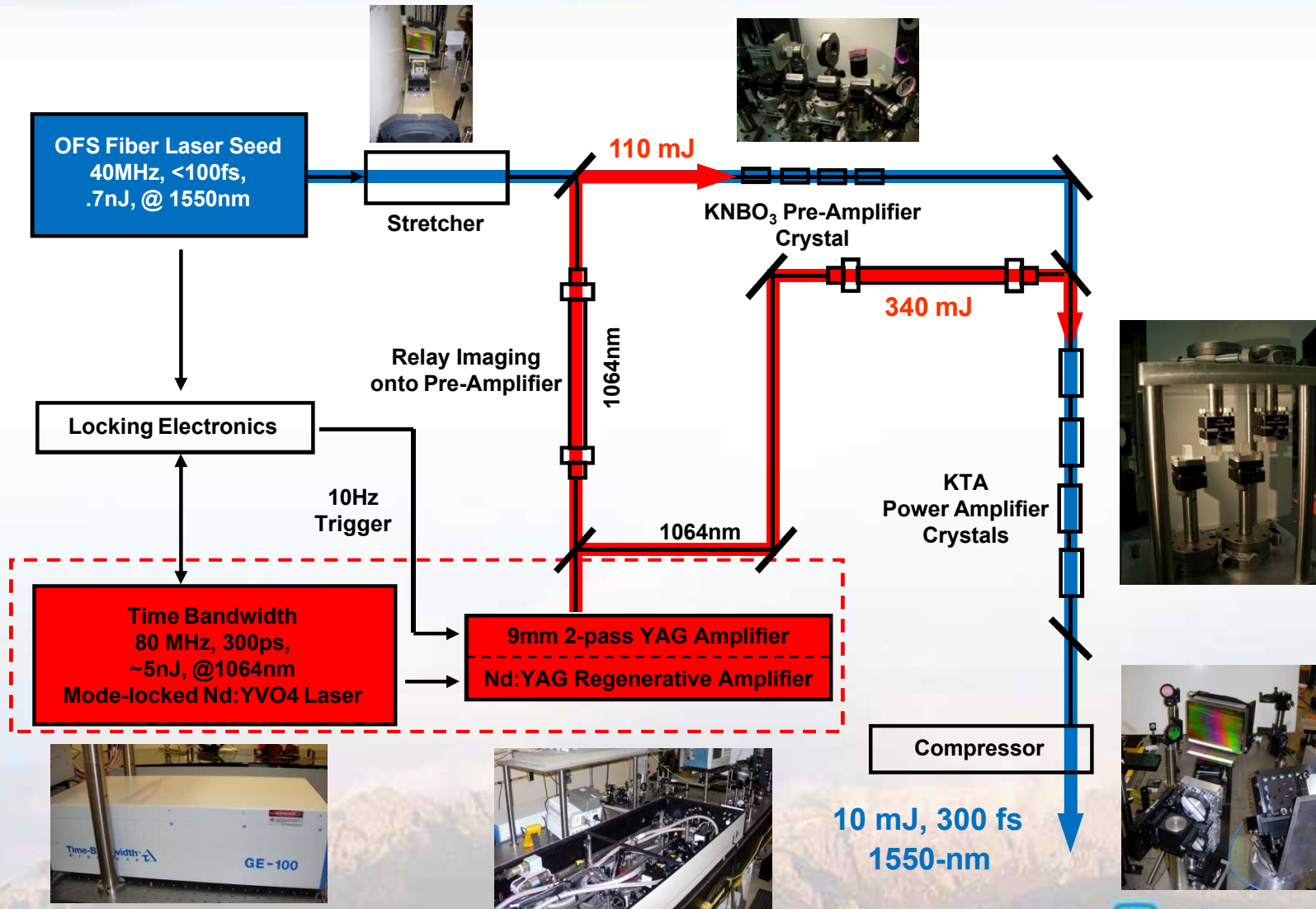
■ Advantages to OPCPA:

- Can support large bandwidths
- Tunable over large frequency range
- Large single-pass gain is possible
- Can result in undistorted signal phase
- Reduced thermal effects in amplifier crystal

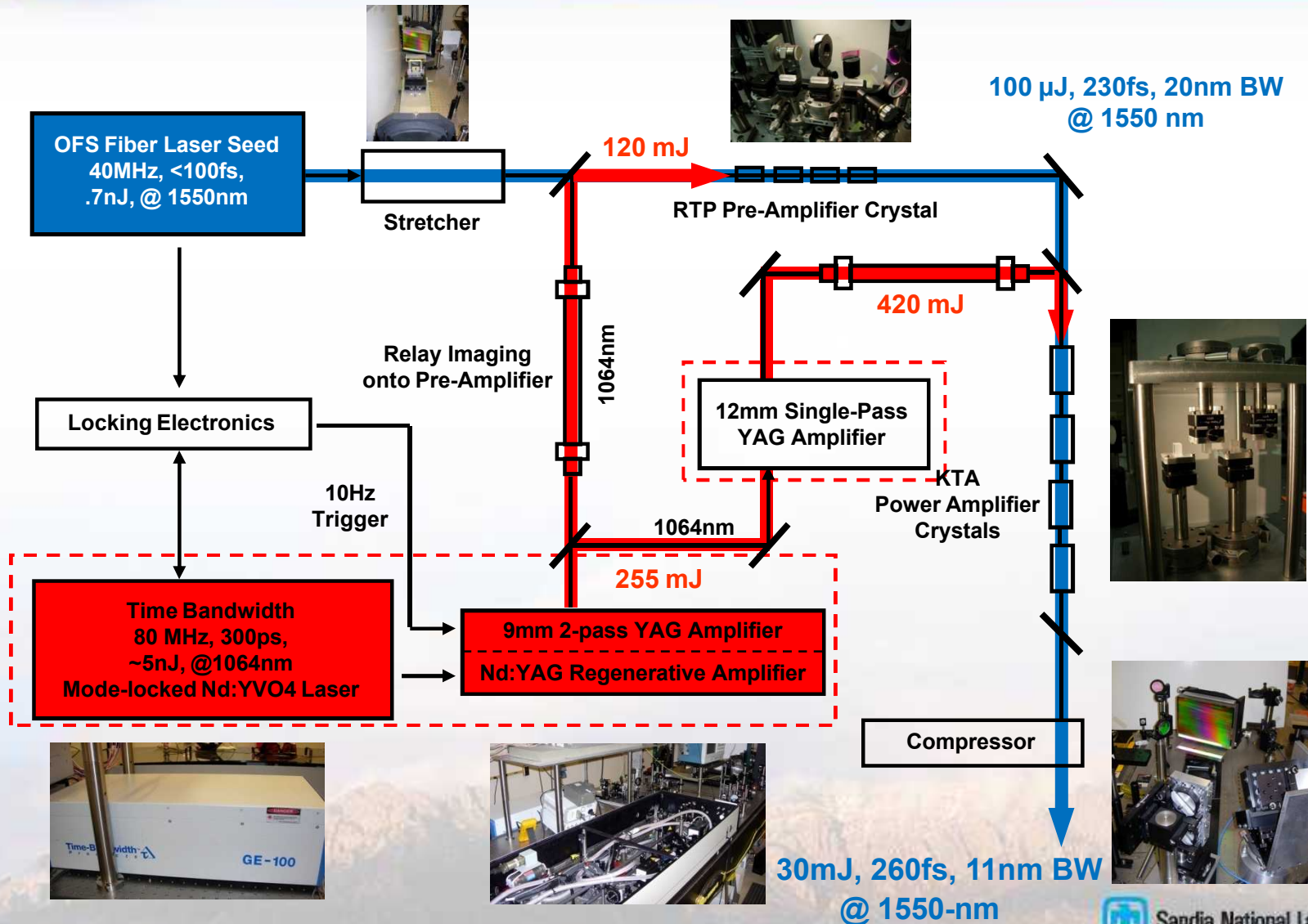
■ Disadvantages:

- Requires phase matching
- Requires temporal alignment
- Gain dependent on intensity

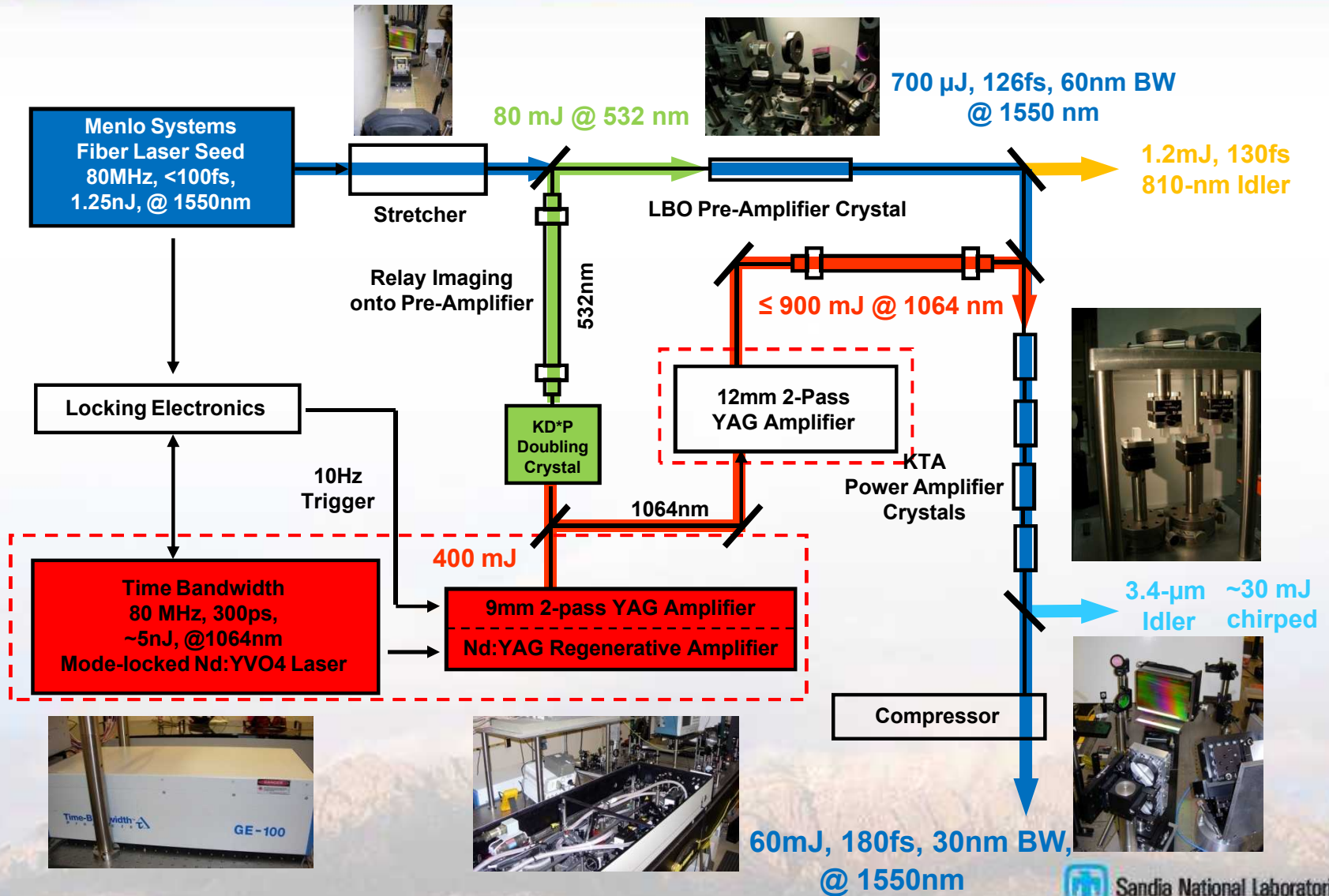
Sandia Gen 1 OPCPA System



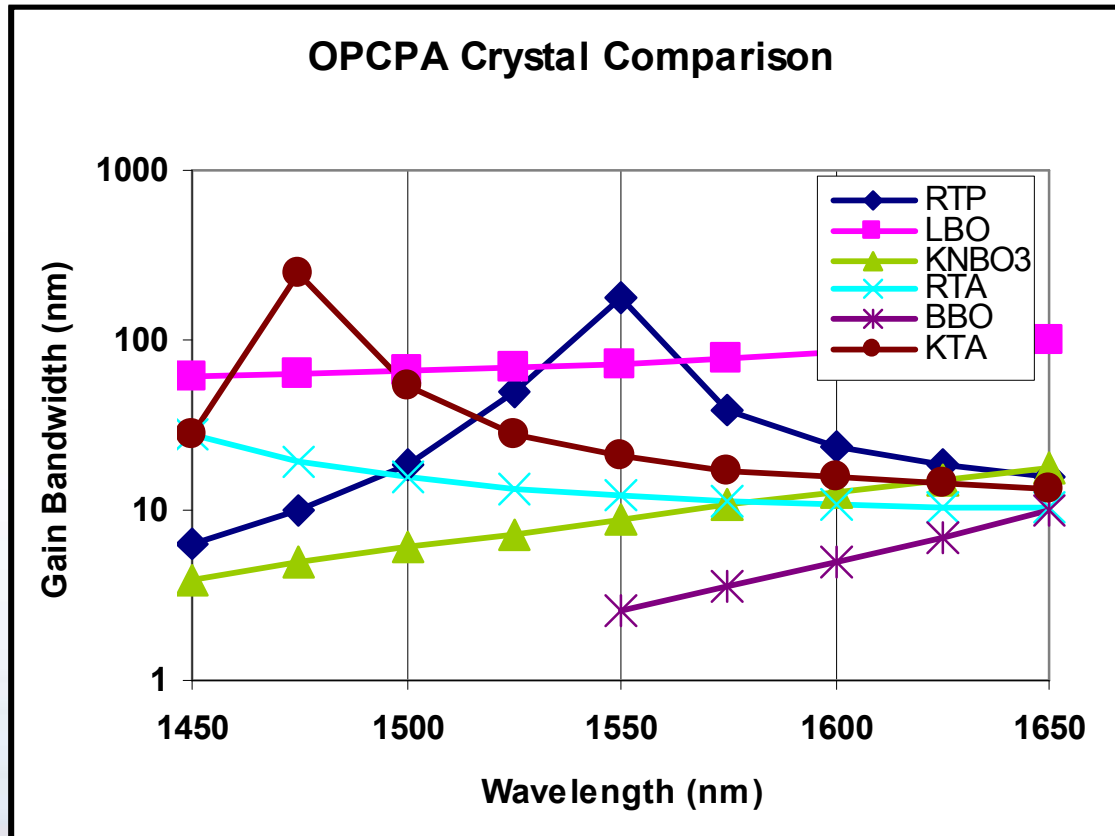
Sandia Gen 2 OPCPA System



Sandia Gen 3 OPCPA System



Non-linear crystal comparison



Damage threshold

LBO – 25 J/cm²

KTA – 15 J/cm²

RTP – 15 J/cm²

RTA – 15 J/cm²

BBO – 13 J/cm²

KNBO₃ – 1.7 J/cm²



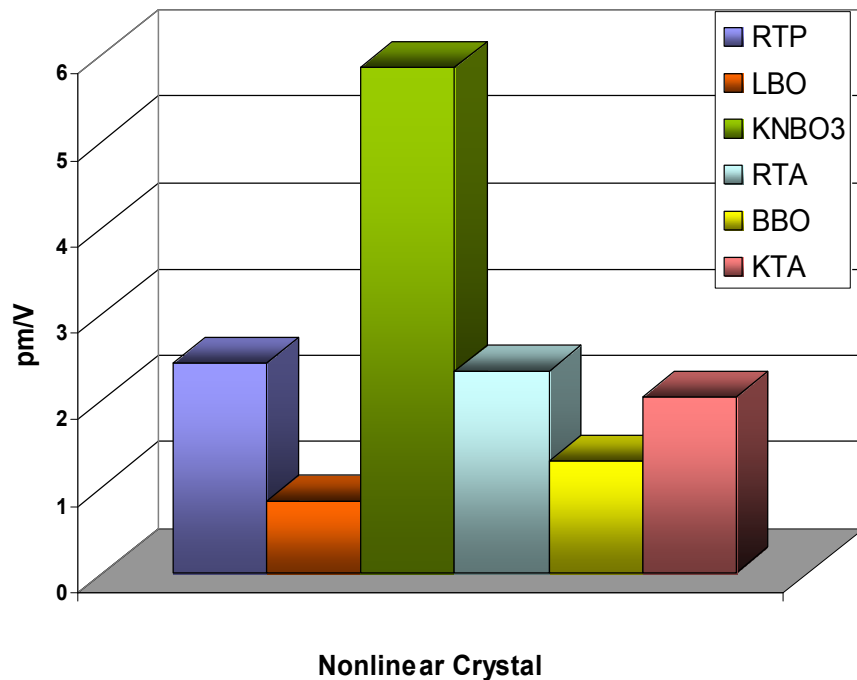
* Results from SNLO nonlinear optics code available from A.V. Smith, AS-Photonics



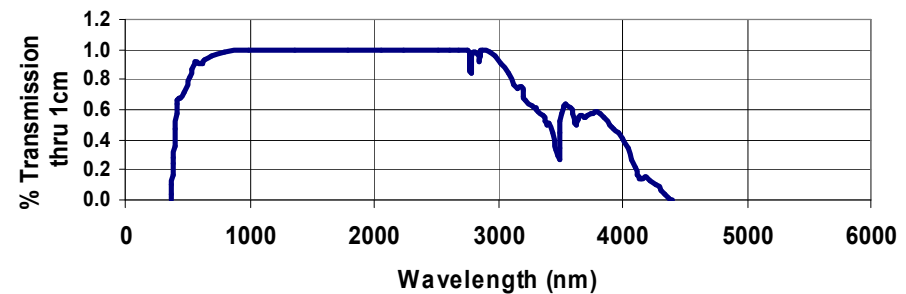
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Non-linear crystal comparison

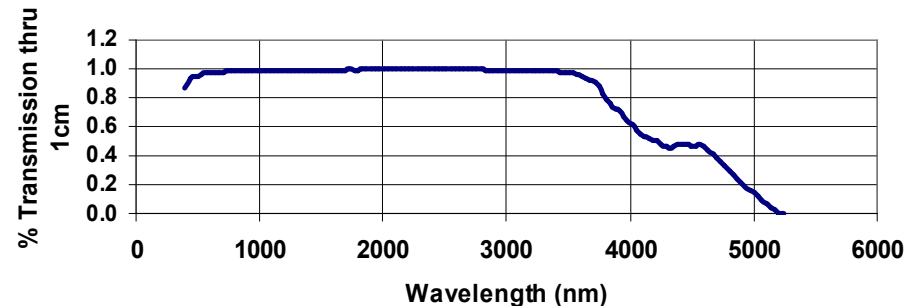
Nonlinear Crystal d_{eff} Values



RTP Transmission Curve



KTA Transmission Curve

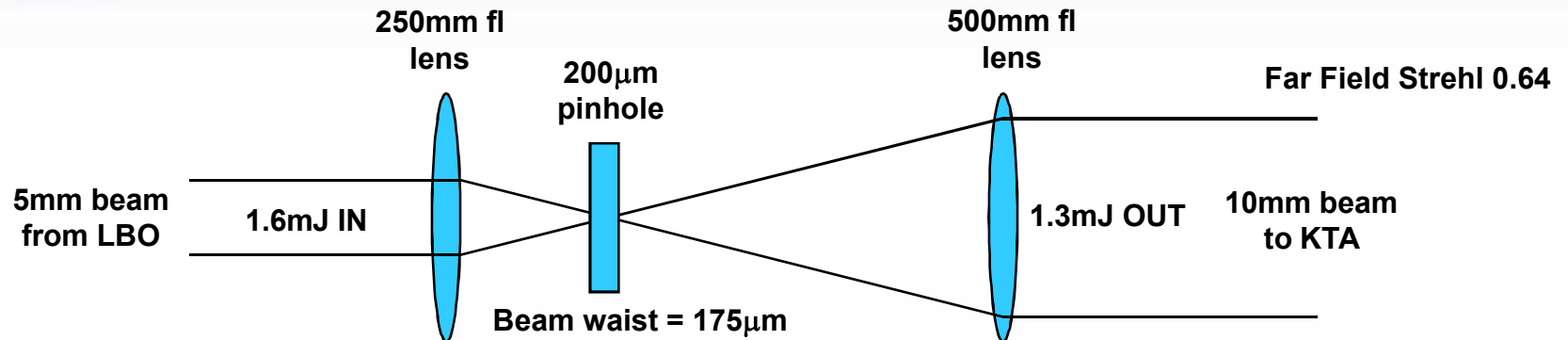


* Results from SNLO nonlinear optics code available from A.V. Smith, AS-Photonics



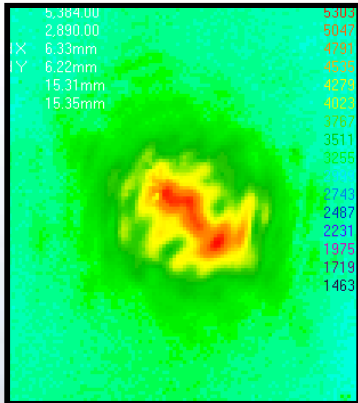
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Interstage Spatial/OPG Filter

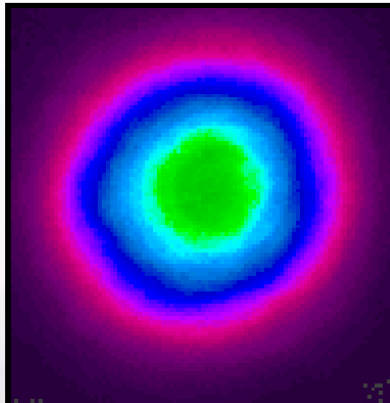


LBO Pre Amplifier Output

Pre SF = 1.6mJ uncomp. / Post SF = 1.3mJ uncomp.



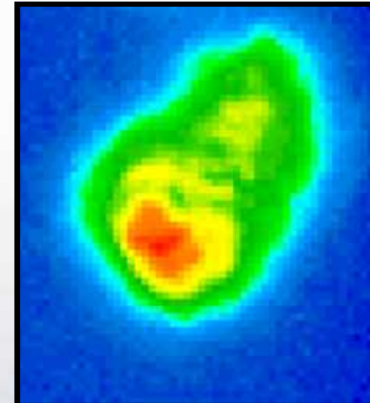
1st stage amplified beam before SF installed



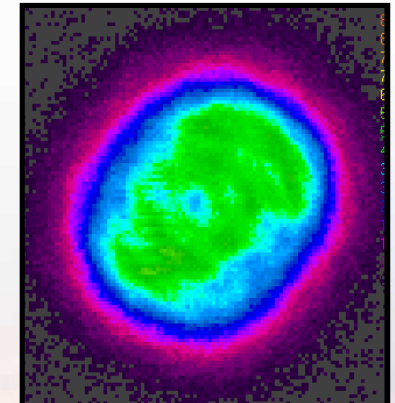
1st stage amplified beam after SF installed

KTA Amplifier Output

Pre SF = 35mJ comp. / Post SF = 45mJ comp.



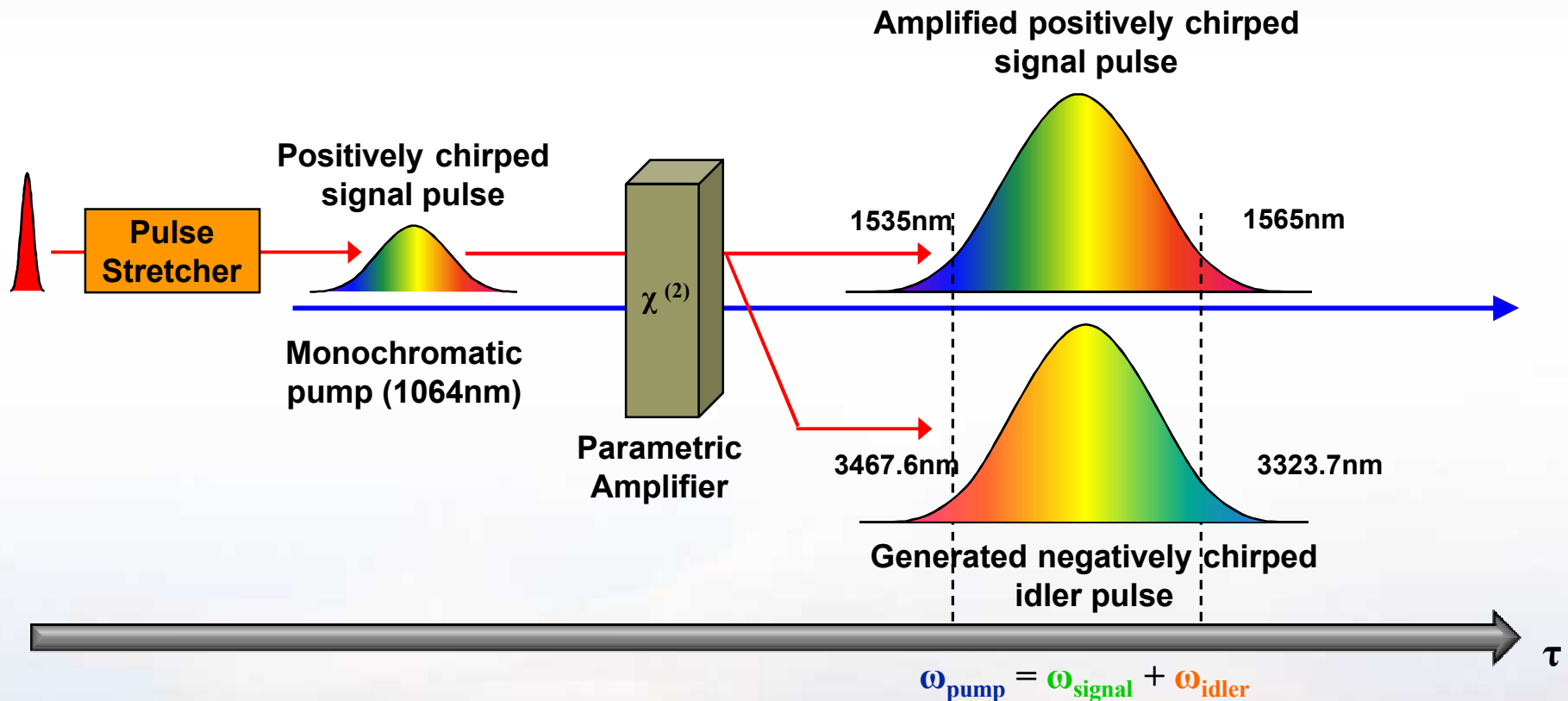
2nd stage amplified beam before SF installed



2nd stage amplified beam after SF installed

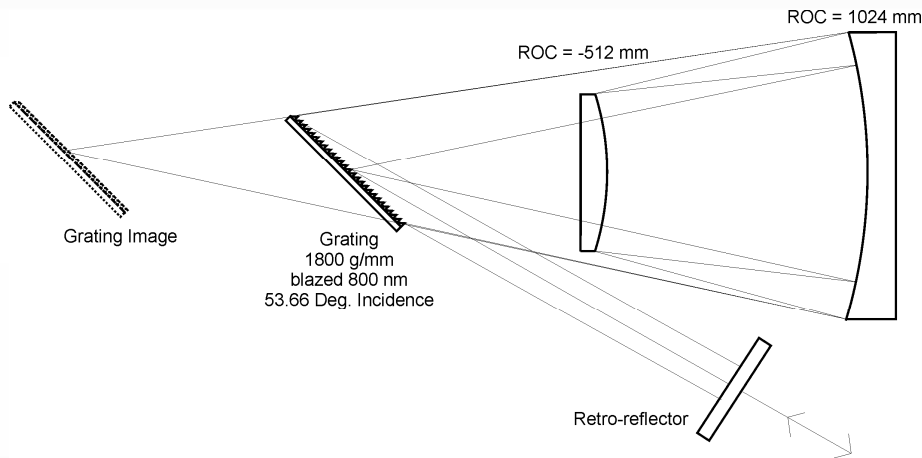


Signal/Idler Compression

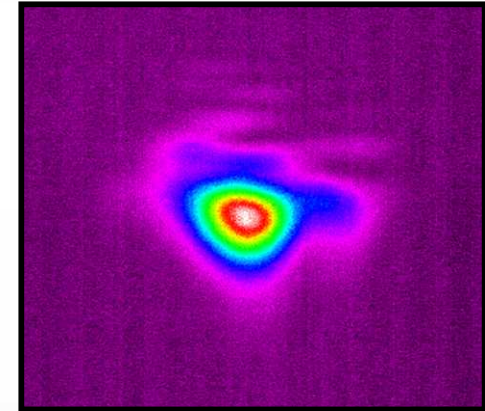


Ex. $\omega(1064\text{nm}) = 2.8176 \times 10^{14}$; $\omega(1535\text{nm}) = 1.953 \times 10^{14}$; $2.8176 \times 10^{14} - 1.953 \times 10^{14} = 8.646 \times 10^{13}$; $C / 8.646 \times 10^{13} = 3467.4\text{nm}$
 $\omega(1064\text{nm}) = 2.8176 \times 10^{14}$; $\omega(1565\text{nm}) = 1.9156 \times 10^{14}$; $2.8176 \times 10^{14} - 1.9156 \times 10^{14} = 9.02 \times 10^{13}$; $C / 9.02 \times 10^{13} = 3323.7\text{nm}$

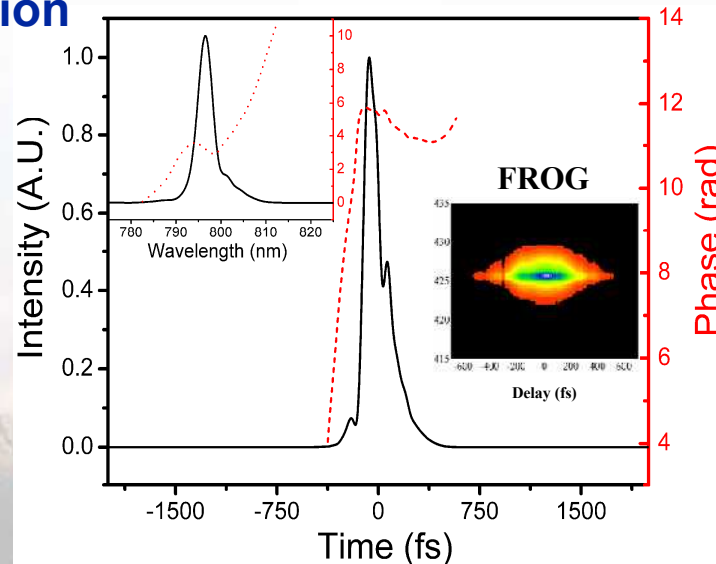
800-nm Idler Pulse from Pre-Amplifier



Beam Profile



- 1.2-mJ energy, ~130-fs duration
- 75% beyond transform limit
- ~7.5 GW peak power



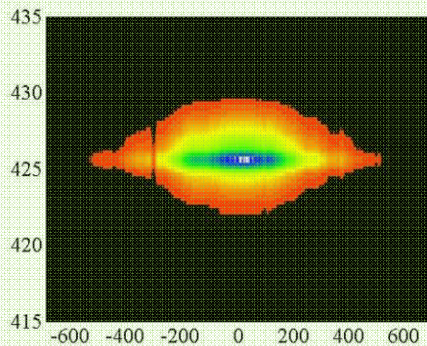
Continuum in Glass



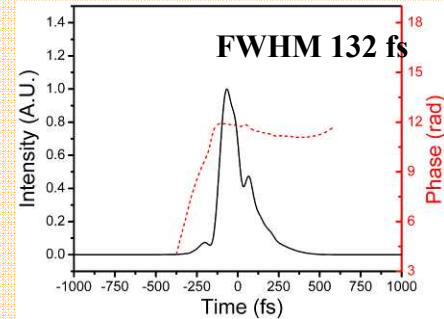
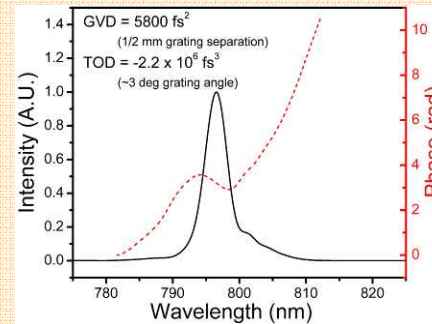
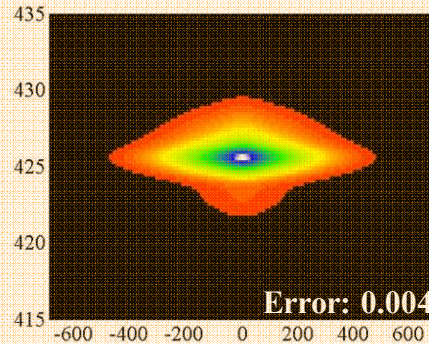
Simultaneous Signal/Idler Compression from Pre-amplifier

800-nm Idler

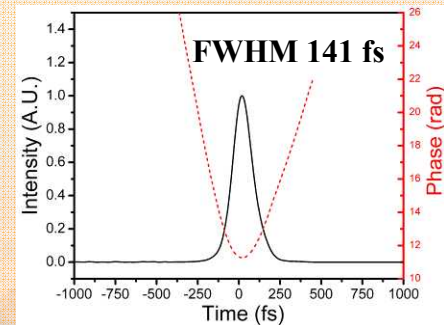
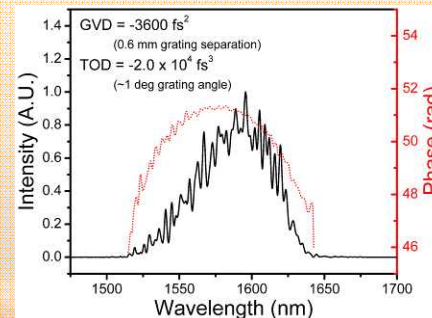
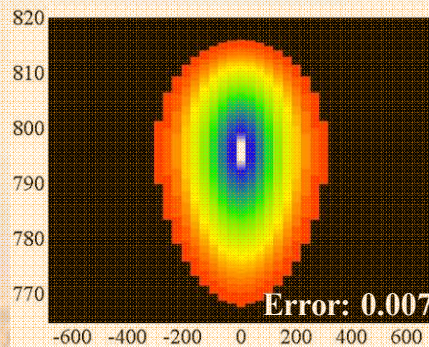
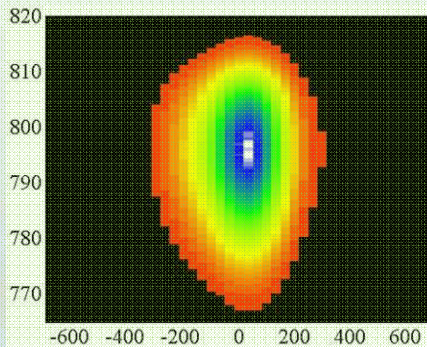
Measured



Retrieved



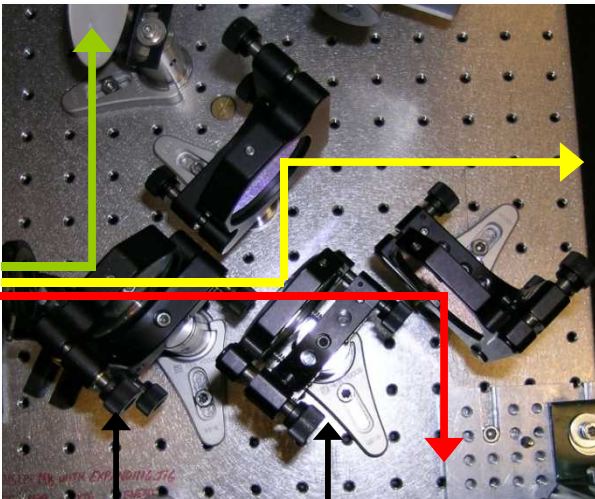
1600-nm Signal



Delay (fs)



3.4- μm Idler Pulse from Power Amplifier



IR Separator Installation

Optic #1
R > 99% @ 1064nm (S)

T > 99% @ 1520-1580nm (P)
& 3300-3500nm (S)

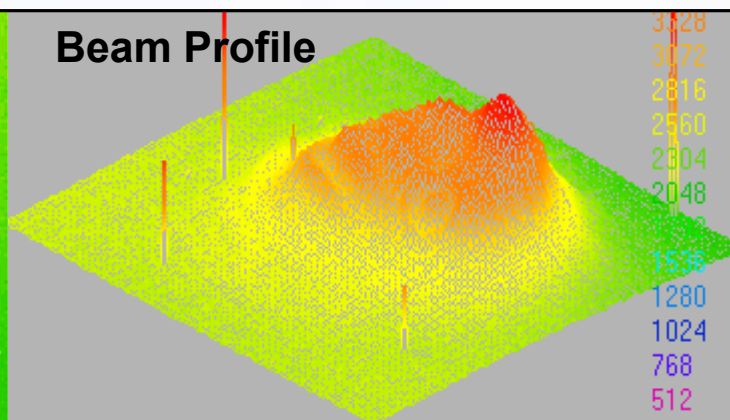
Optic #2
R > 99% @ 1520-1580nm (P)

T > 99% @ 3300-3500nm (S)

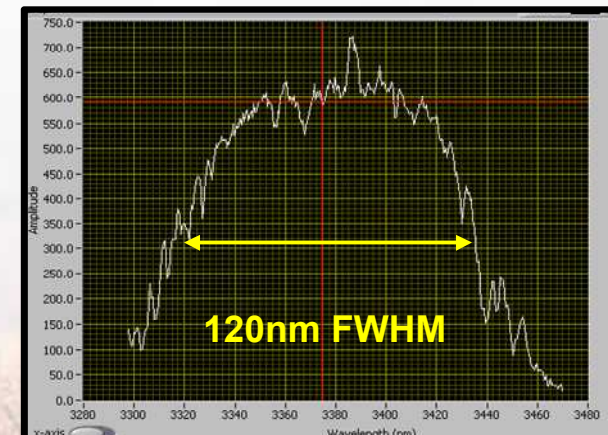
Optic #1 Optic #2

- 25mJ before compression (measured)
- Expect ~50% compressor efficiency
12 mJ @ 3.4 μm (210fs)
- $P_{\text{estimated}} \sim 57 \text{ GW}$ (up from 30GW)

Beam Profile

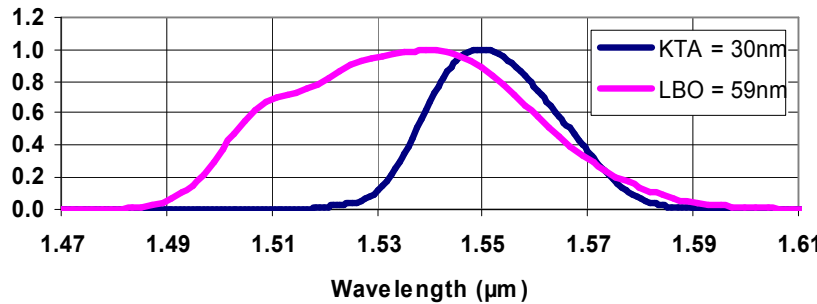


Idler Spectrum

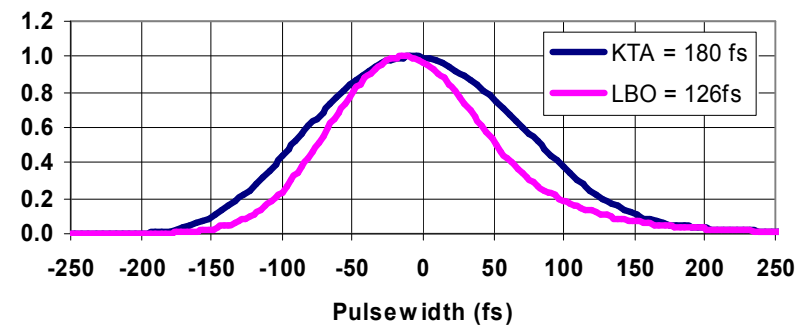


1550-nm Signal from Both Amplifier Stages

Amplified LBO/KTA Bandwidth

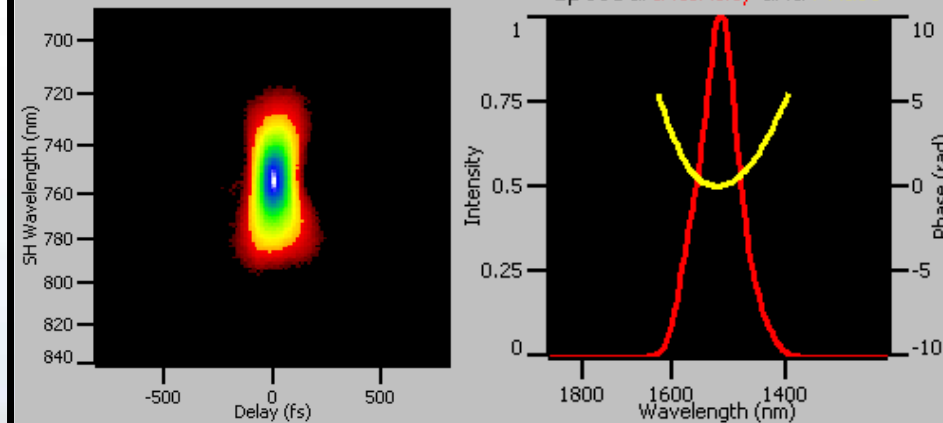


Amplified LBO/KTA Pulsewidth



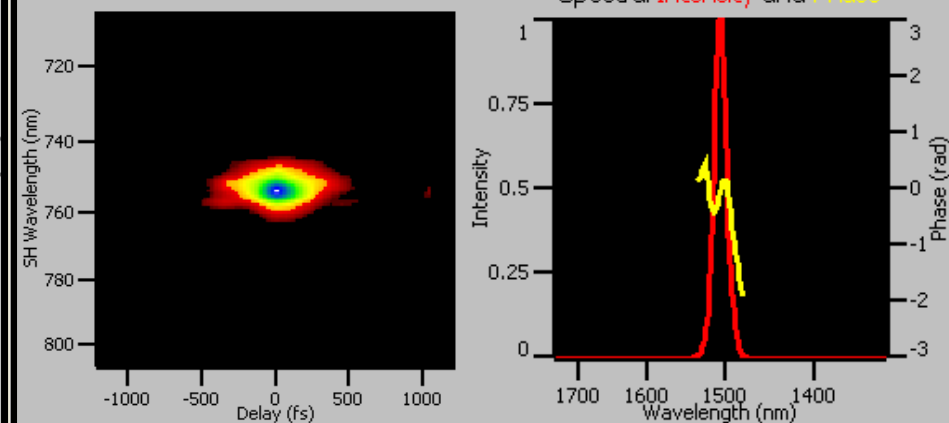
Measured FROG Trace

Spectral Intensity and Phase



Measured FROG Trace

Spectral Intensity and Phase

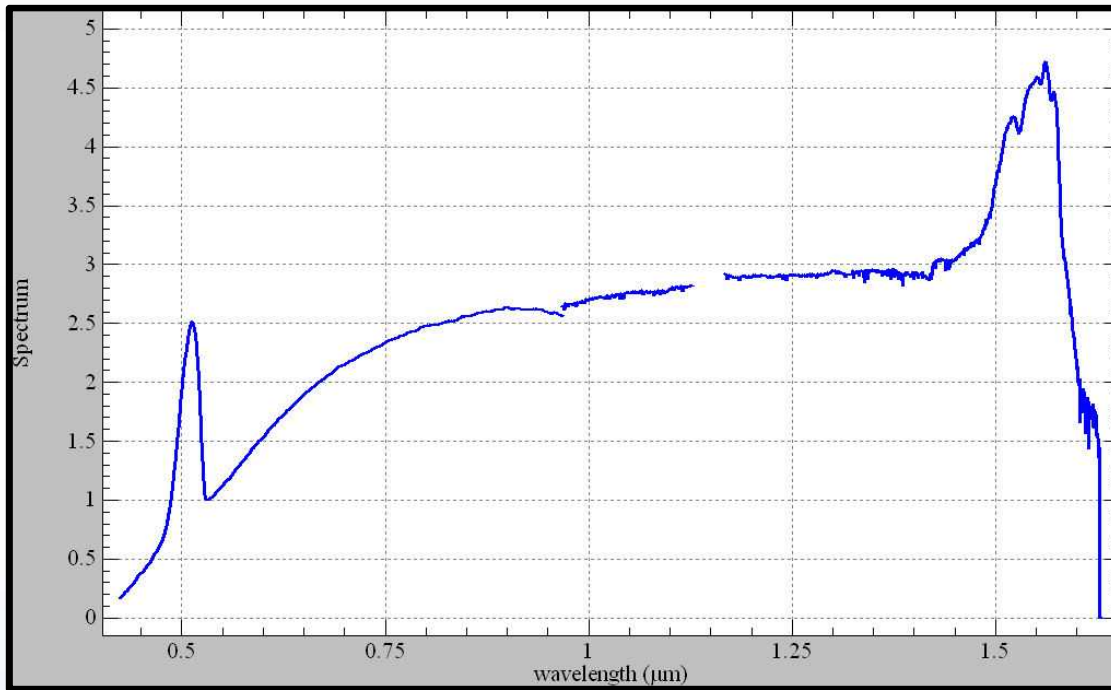


- 1st Stage Peak Power: 7.5 GW
- Energy: 0.7 mJ
- Pulse Width: 126 fs (previous 145fs)
- Amplified Bandwidth: 59 nm

- System Peak Power: 333 GW (previous 160GW)
- Energy: 60 mJ (previous 35mJ)
- Pulse Width: 180 fs (previous 220fs)
- Amplified Bandwidth: 30nm



Continuum and Harmonic Generation in Air



45mJ, 180fs

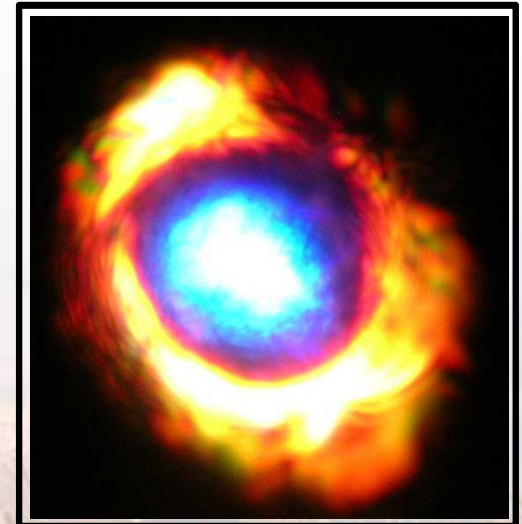
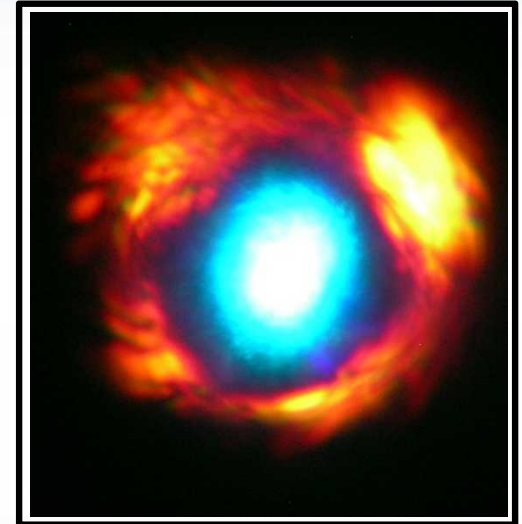
Focused with 30cm lens

Conversion efficiencies to THG (517nm) >1%

Possible nonlinear Raleigh Beacon

Launches NIR (atmospheric propagation more favorable)

Generates green light at target.





Summary

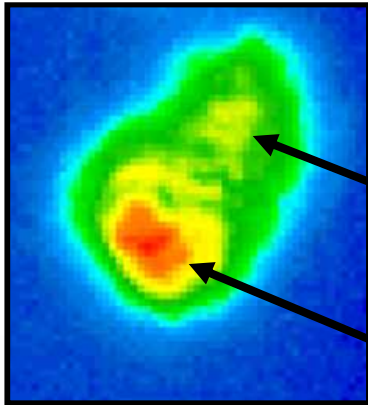
- OPCPA system constructed to generate unprecedented power (>330 GW) at the key wavelength of 1550nm.
- Significant improvement in gain bandwidth, pulsewidth, and output energy (thus peak power) from previous Sandia OPCPA designs.
- High power radiation is also generated at the very useful wavelengths of 810nm and 3393nm in the OPCPA process.
- Improved beam quality (focusability) by a factor of ~ 3 .
- First demonstrated simultaneous compression of signal and idler beams from an OPCPA.
- First demonstrated laser filamentation at $1.6\mu\text{m}$.



*Acknowledgements : Funding provided under CRADA with Lockheed Martin Missile and Fire Control (Orlando, FL).

Beam Quality Issues

Previous beam quality

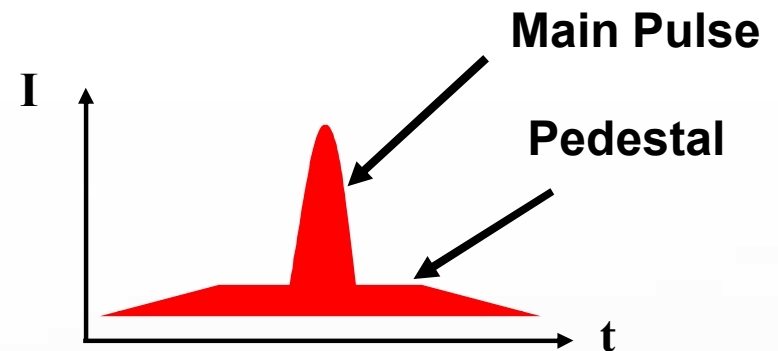


Focus is several X
diffraction limited

Beam or OPG?

Main Beam

Pulse Contrast



- Difficult to characterize beam
- What is the actual “intensity”?
- Hot spots in beam damage components
- Limit overall output energy



OPCPA Evolution

Gen 1 – KNBO₃ pre-amp + KTA power amp (>30GW)

- Final Output = >30mJ uncompressed/10mJ compressed, 300fs, 10nm BW

Gen 2 – RTP pre-amp + KTA power amp (100GW)

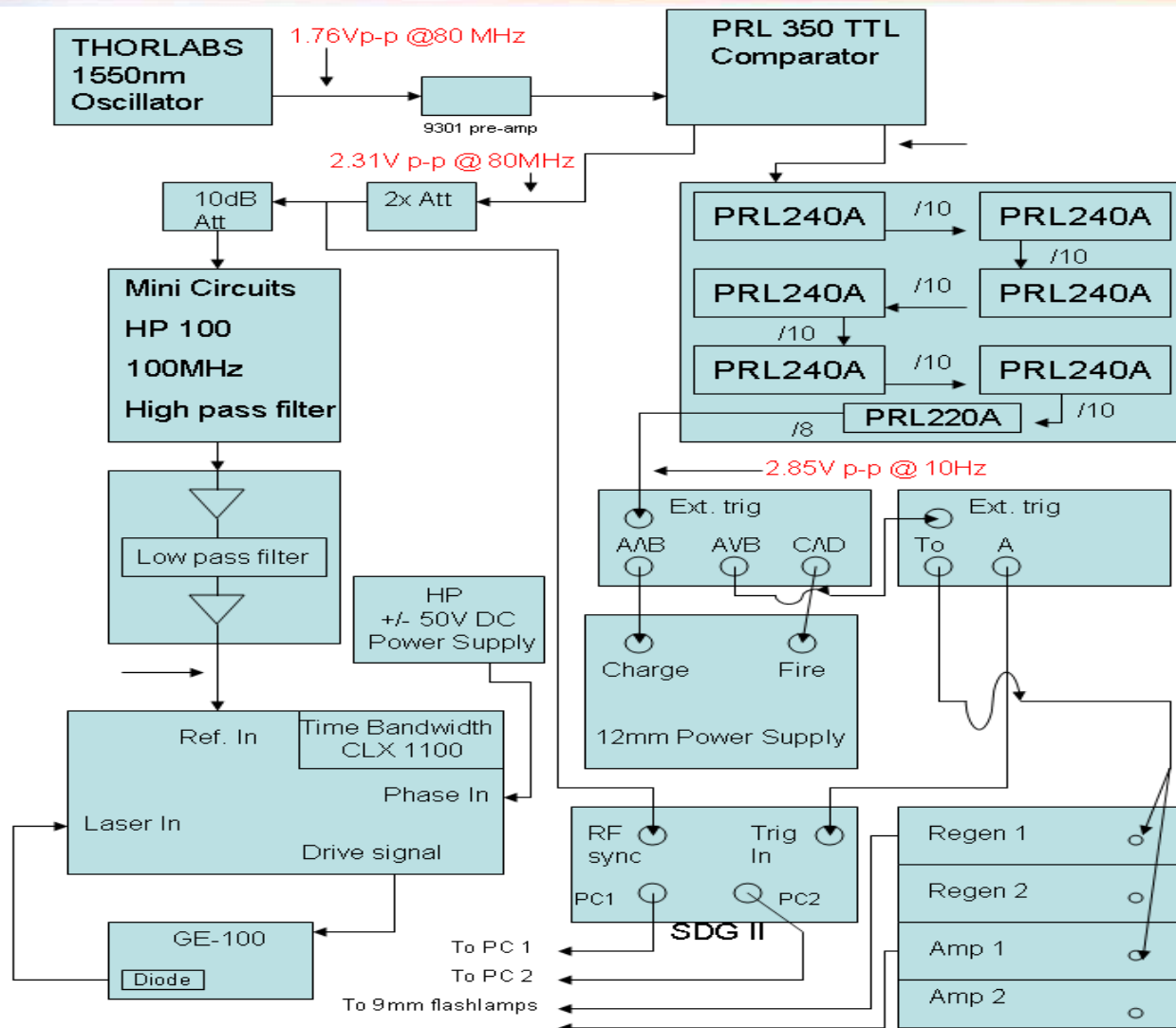
- 1st stage output = 100μJ, 230fs FWHM, 20nm
- 2nd stage output = 66mJ uncompressed/30mJ compressed, 260fs FWHM, 11nm

Gen 3 – LBO pre-amp + KTA power amp (>310GW)

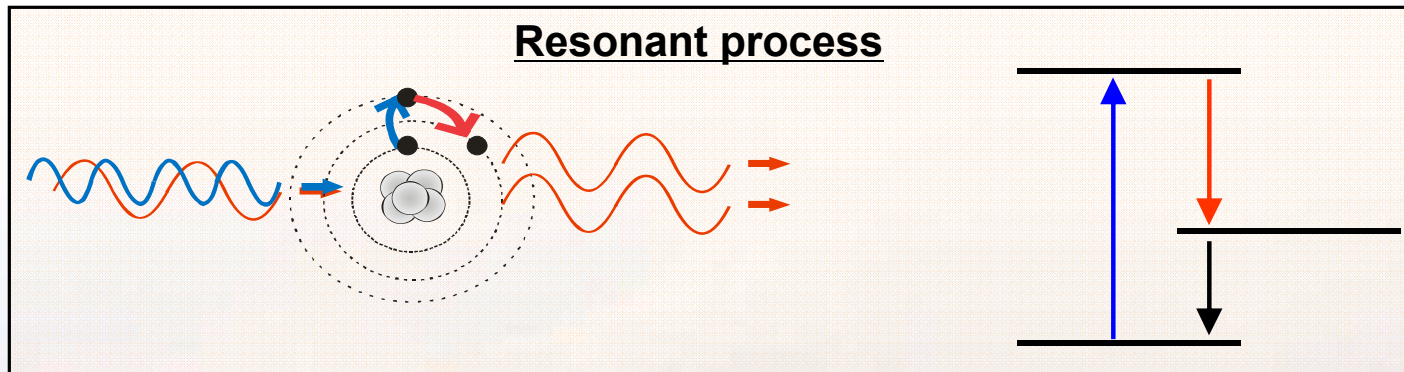
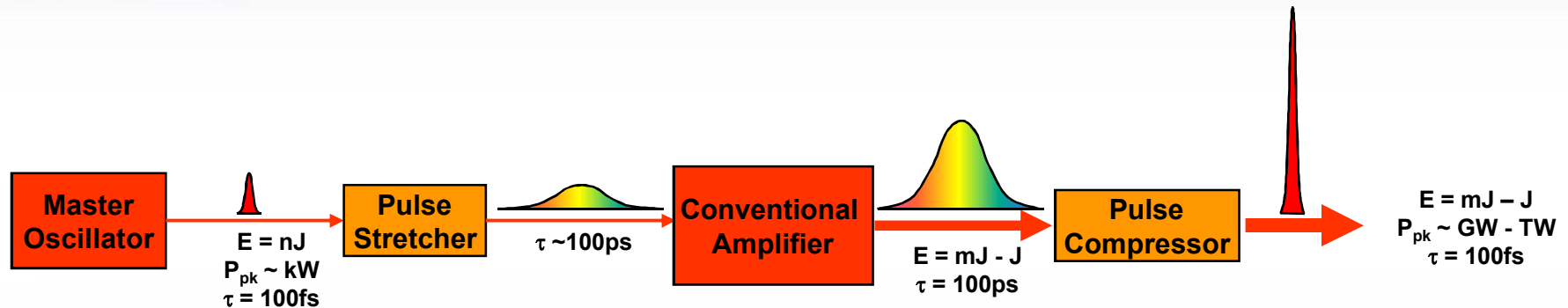
- 1st stage output = 700μJ, 126fs FWHM, 60nm BW
- 2nd stage output = 60mJ compressed, 180fs FWHM, 30nm



Menlo/Timing diagram slide?



Conventional Chirped Pulse Amplification (CPA)



Advantages

- Relatively simple setup
- Well-known physics

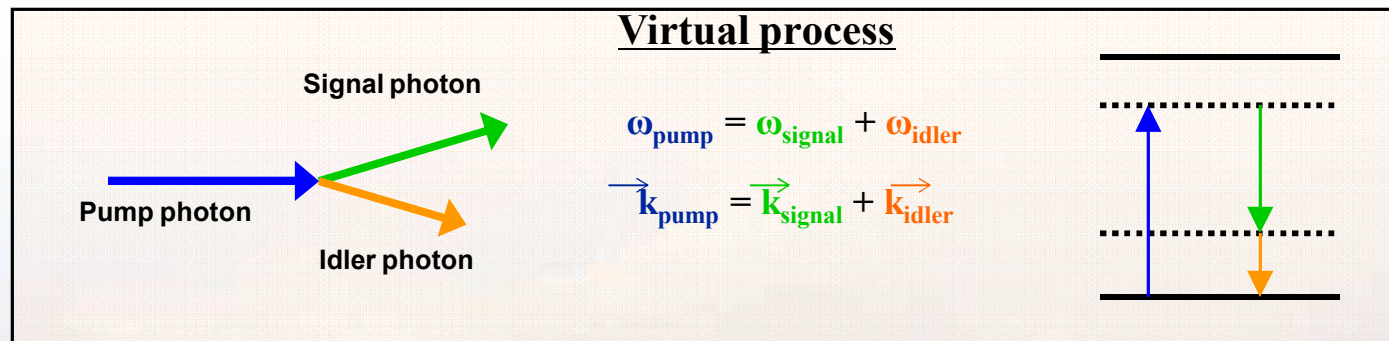
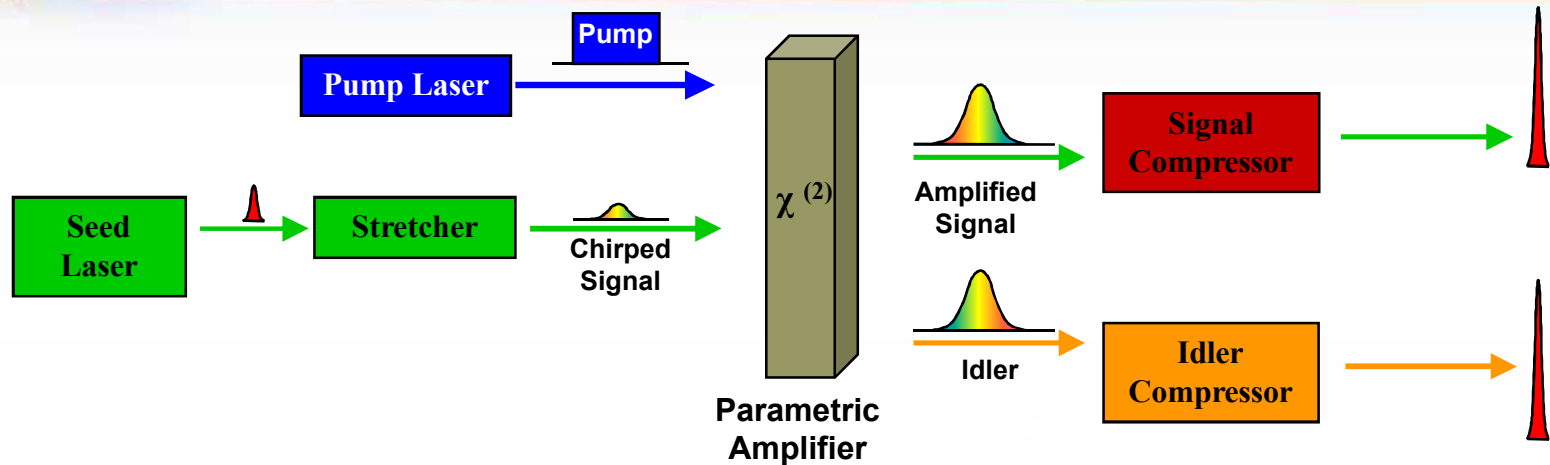
Disadvantages

- Finite lifetime and spectral bandwidth
- Wavelengths restricted to available laser gain media
- Gain limited by amplified spontaneous emission (ASE)
- Prone to parasitic losses such as thermal recombination



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Optical Parametric Chirped Pulse Amplification (OPCPA)



Advantages

- Can support large bandwidths
- Tunable over large frequency range
- Large single-pass gain possible
- Reduced nonlinear effects (B-integral)
- Can result in undistorted signal phase

Disadvantages

- Gain dependent on intensity (need pulses)
- Requires temporal alignment
- Requires phase matching





Transform limited bandwidth for Gaussian pulses

<u>Pulsewidth</u>	<u>Center λ</u>	<u>Bandwidth if pulse is transform limited (nm)</u>
2.5000E-14	1.5500E-06	141.0442
5.9000E-14	1.5500E-06	59.7645
1.1753E-13	1.5500E-06	30.0018
1.8000E-13	1.5500E-06	19.5895
3.5250E-14	1.5500E-06	100.0314

