

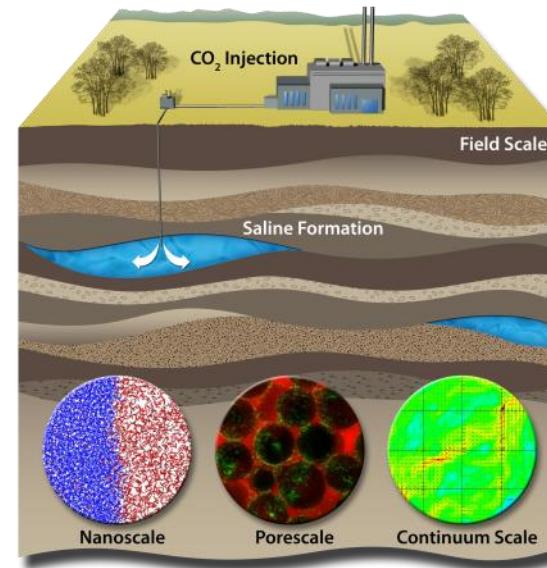
# Upscaling of reaction rates in reactive transport using pore-scale reactive transport model

Hongkyu Yoon

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Collaborators:

Thomas Dewers, Bill Arnold (SNL)  
Jon Major, Peter Eichhubl (UT)



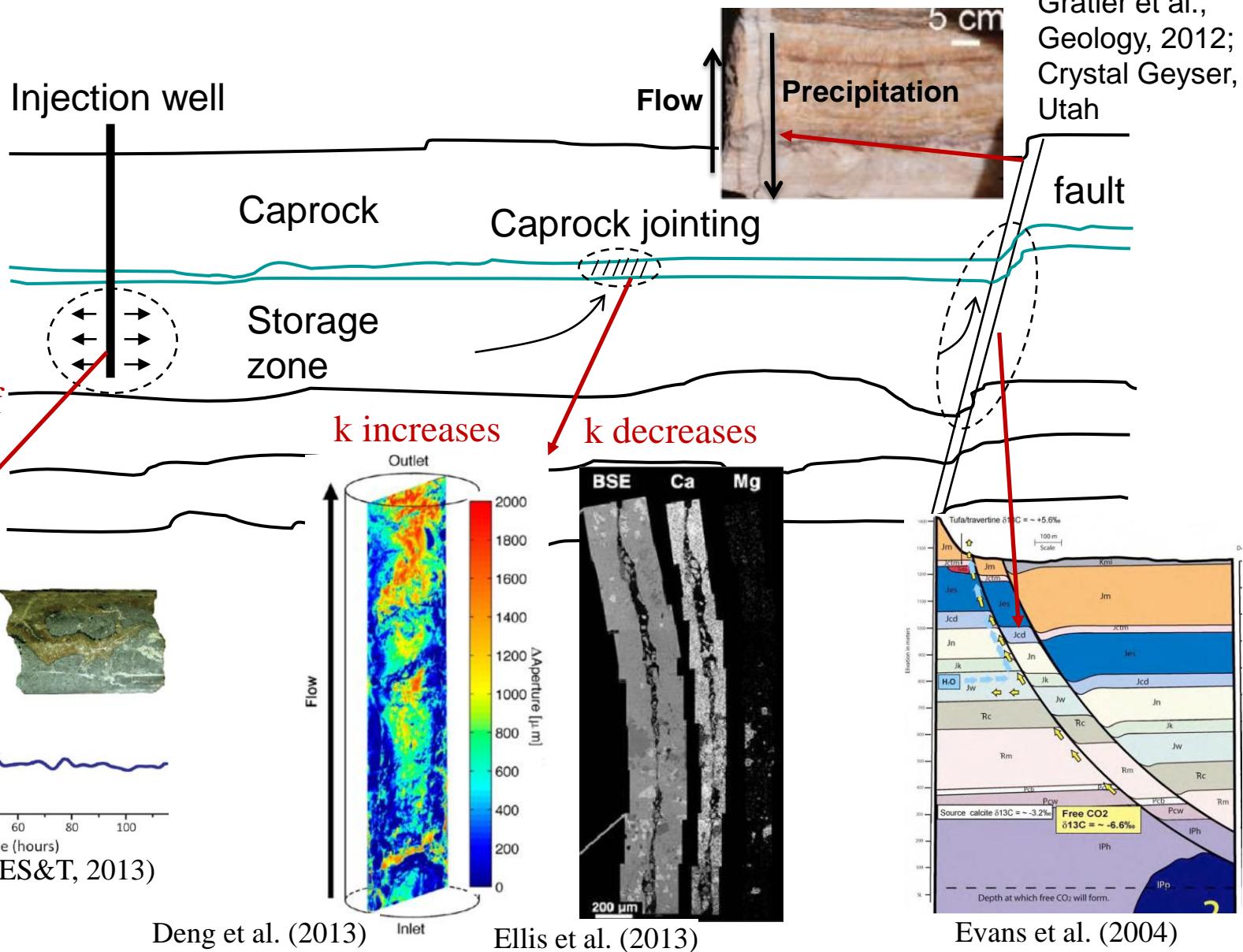
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service  
in the  
national  
interest*

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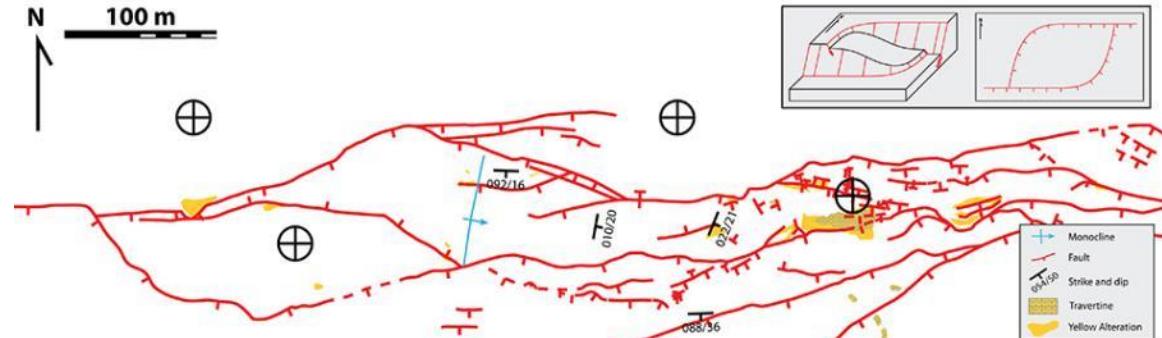
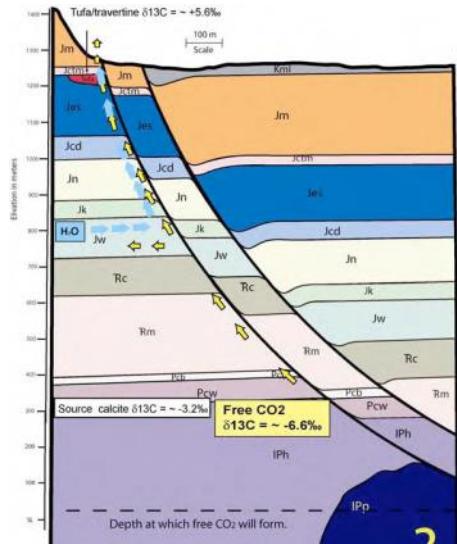
# Reactive Transport Processes during Geological Carbon Storage



# Little Grand Wash Fault

## Crystal Geyser, Utah

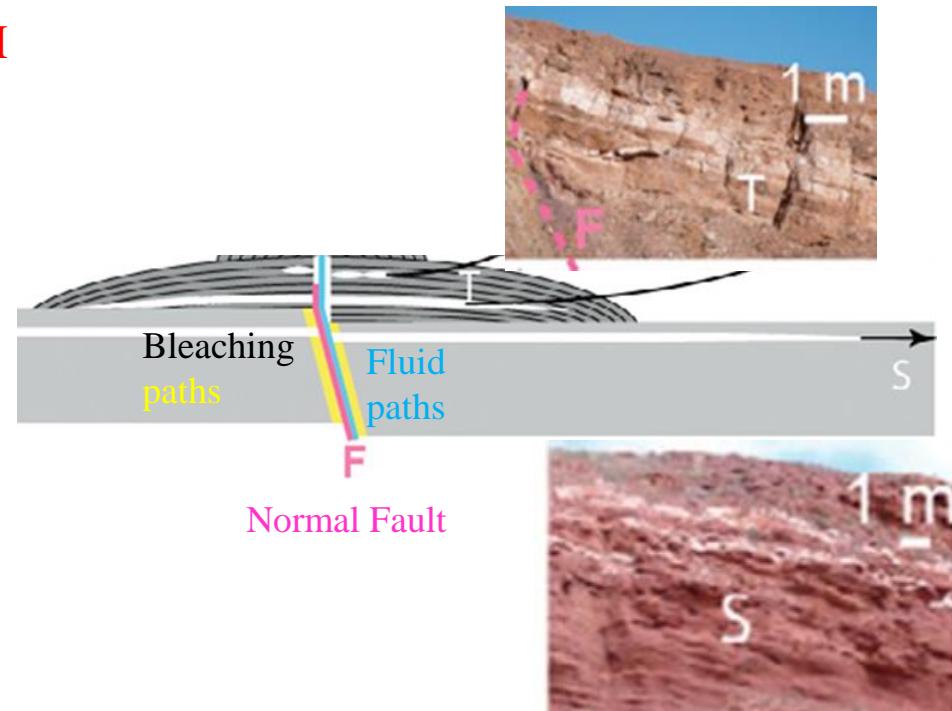
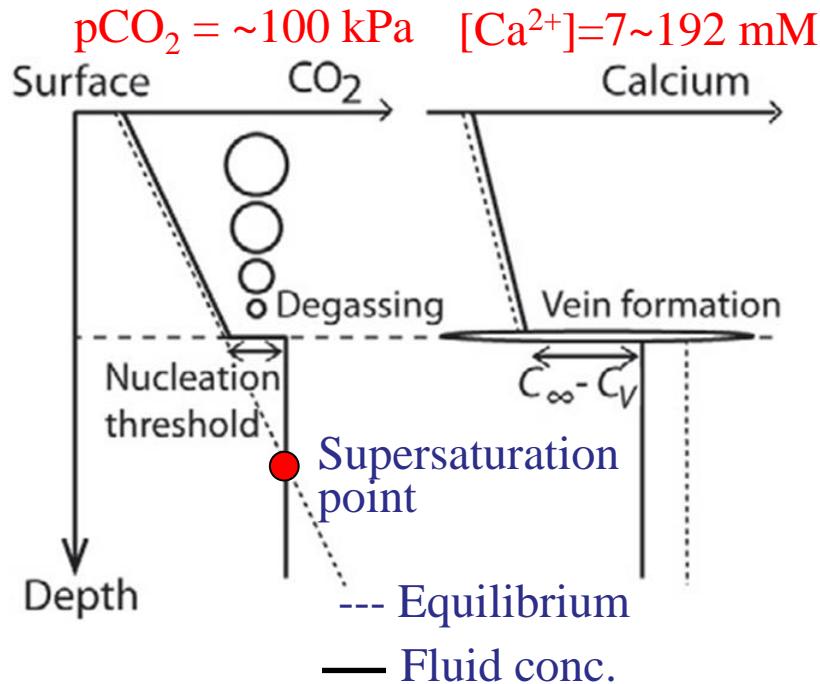
- Observations along the surface exposure of the Grand Wash fault indicate alteration zones of 10-50 m width with spacing on the order of 100 m
- Different flow conduits active at different times
- Locations of conduits controlled by fault-segment intersections and/or topography
- Sandstone permeability reduced by 3 to 4 orders of magnitude in alteration zones by carbonate cementation



From Peter Eichhubl

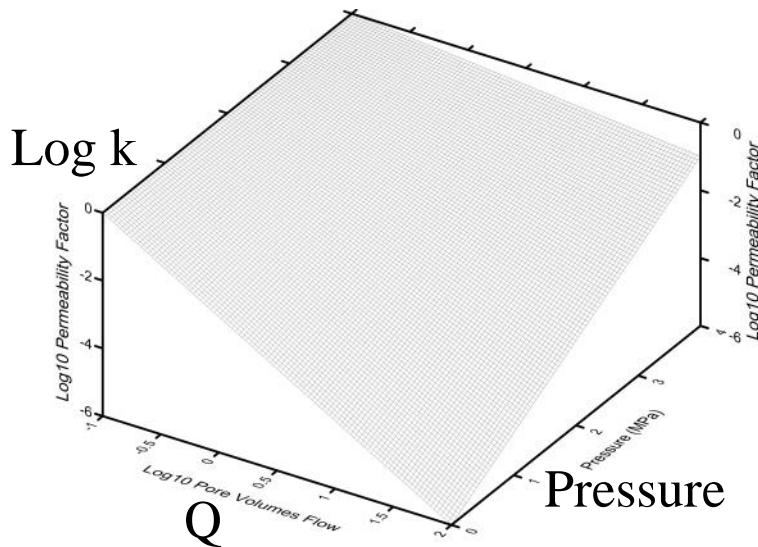
# Succinct chemistry & mineralogy

- Spring water: Low temperature and Mg concentrations
- Aragonite (metastable  $\text{CaCO}_3$  phase) precipitation indicates large, sudden increase of supersaturation with respect to  $\text{CaCO}_3$  in solution  $\rightarrow$  high  $\text{CO}_2$  degassing rate
- Springs: high concentrations of dissolved  $\text{CO}_2$  ( $\text{pCO}_2 = \sim 100 \text{ kPa}$ )
- Both calcite and aragonite are present
- For some horizontal travertine veins, veins grow top to bottom (U-Th dating)



# Crystal Geyser Site: Grand Wash Fault Modeling

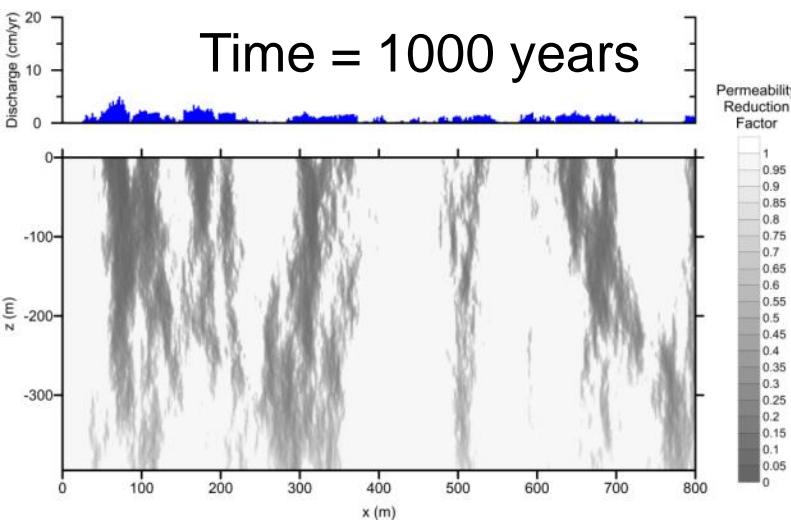
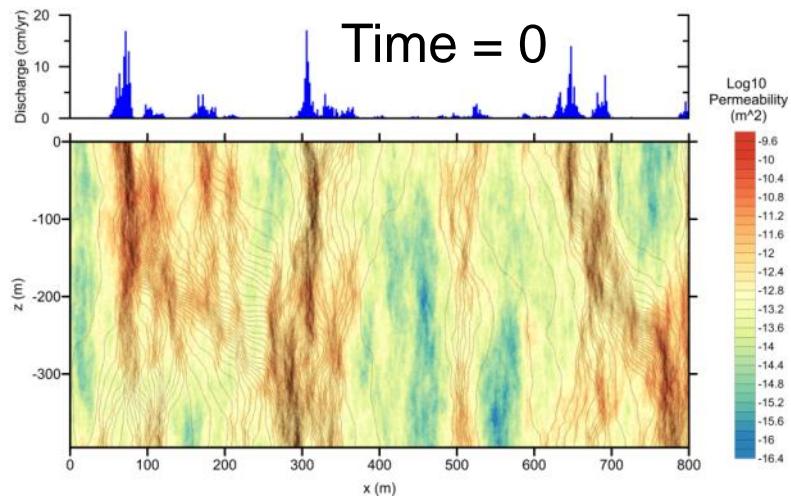
- Simplified, two-dimensional response surface
- Permeability reduction due to calcite precipitation is a function of cumulative pore volume ( $Q$ ) of groundwater and fluid pressure ( $P$ )
- Fluid pressure is taken as a gross proxy for chemical conditions in which higher calcite solubility is associated with higher fluid pressure (greater depth)



Adapted from Mehmani et al. (2012)

# Crystal Geyser Site: Grand Wash Fault Modeling

- Unconditional geostatistical simulation
- Initial simulated steady-state flow pattern is qualitatively similar to the spacing of seeps along the Grand Wash fault (~100's of m between locations of groundwater discharge)
- Transient flow simulation includes explicit updating of  $k$  field at each time step using the response surface (FEHM)
- $k$  is reduced by several orders of magnitude by calcite precipitation, primarily in the shallower high-flow channels
- Evolution of the flow field results in more dispersed groundwater discharge at the surface



# Response Function based on Pore Scale Simulations

- Vigorously tested pore-scale model can be used to develop a response function (or dimension reduction model) for continuum-scale permeability and porosity ( $k$ - $\varepsilon$ ) relationships
- $k$ - $\varepsilon$  and surface area- $\varepsilon$  relationships will be developed over a range of solution chemistry, chemical reaction, and pore structure configurations in addition to Pe and Da numbers

**Changes in porosity due to precipitation ~tortuosity and permeability by phenomenological power law relations**

$$\tau(\varphi) = \tau_0 \left( \frac{\varphi}{\varphi_0} \right)^n \quad k(\varphi) = k_0 \left( \frac{\varphi}{\varphi_0} \right)^n \quad a_{cc} = a_{cc}^0 \left( \frac{\varphi}{\varphi_0} \right)^{2/3}$$

# Response Function based on Pore Scale Simulations

- Pe & Da numbers

Pe( $\mu\text{L}/\text{D}$ ) = 0.08, 0.8, 8

Da( $\text{kL}/(\text{K}_{\text{sp}}^{0.5} \times \text{D})$ ) = 0.002, 0.02, 0.1

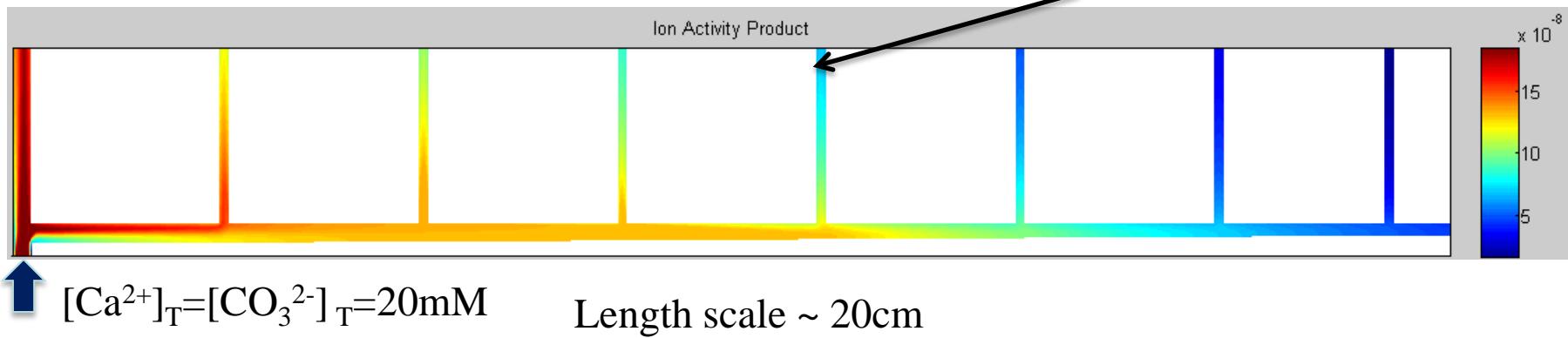
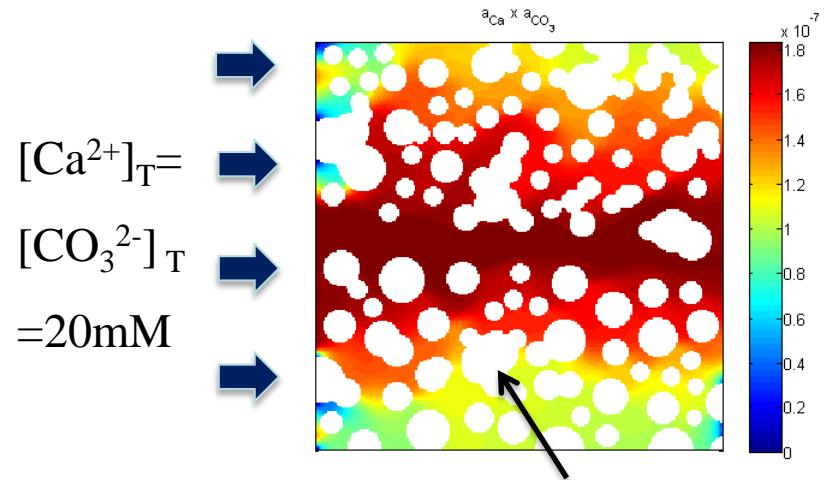
( $\text{K}_{\text{sp}}$ , calcite =  $3.3 \times 10^{-9} \text{ M}^2$ )

- Chemical speciation

Speciation:  $\text{Ca}^{2+}$ ,  $\text{H}^+$ ,  $\text{CO}_3^{2-}$ ,  $\text{HCO}_3^-$ ,  $\text{H}_2\text{CO}_3$

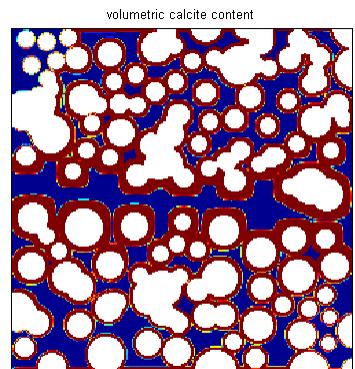
No speciation:  $\text{Ca}^{2+}$ ,  $\text{CO}_3^{2-}$

- Pore structures

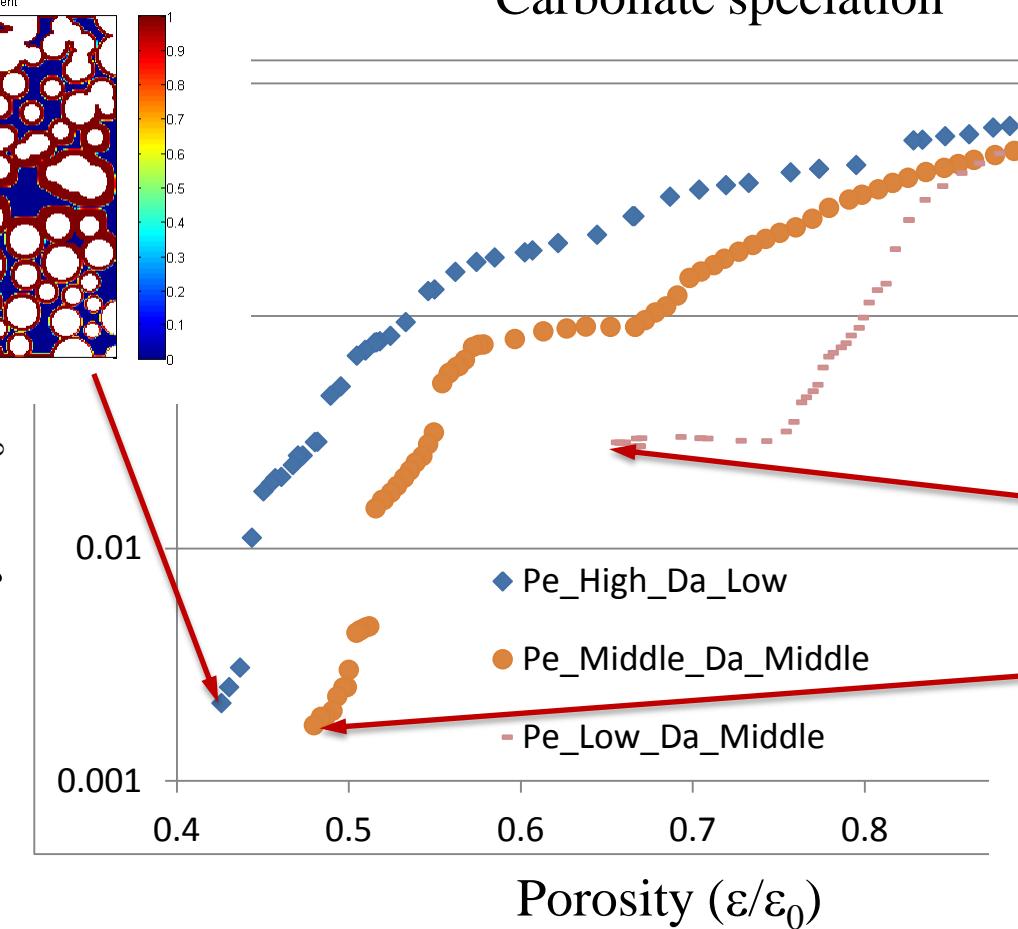


# Permeability-Porosity Relationships

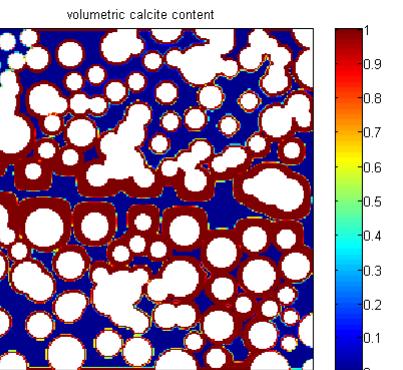
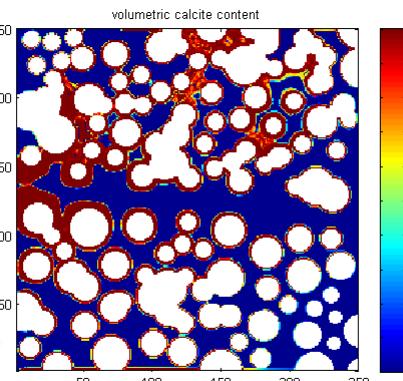
High Pe; Low Da



Permeability ( $k/k_0$ )



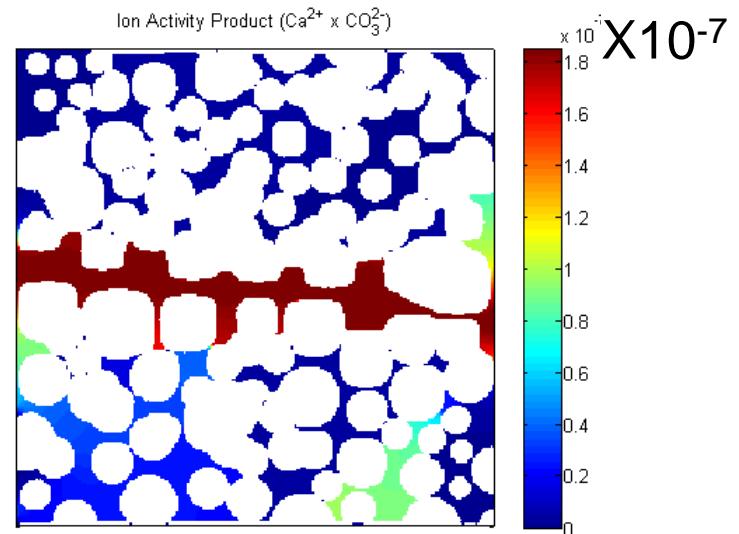
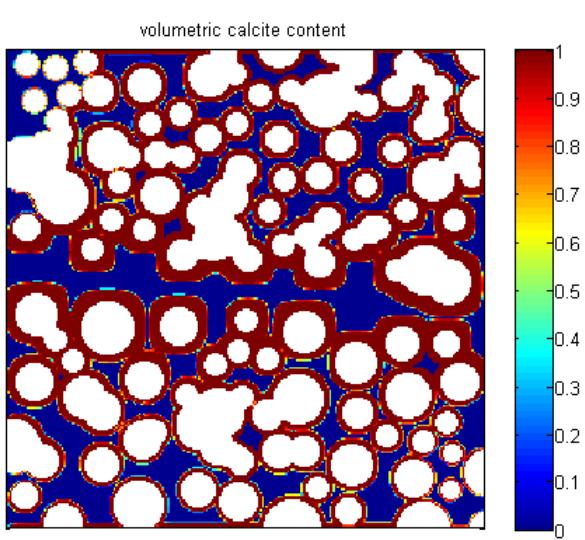
Low Pe;  
Medium Da



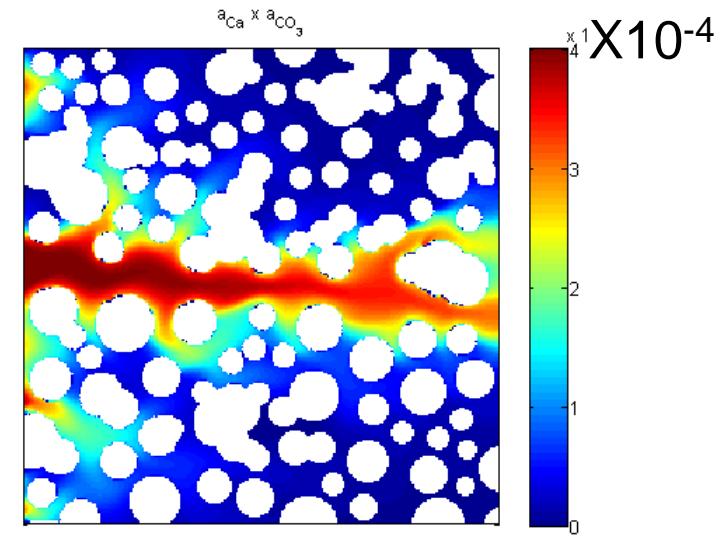
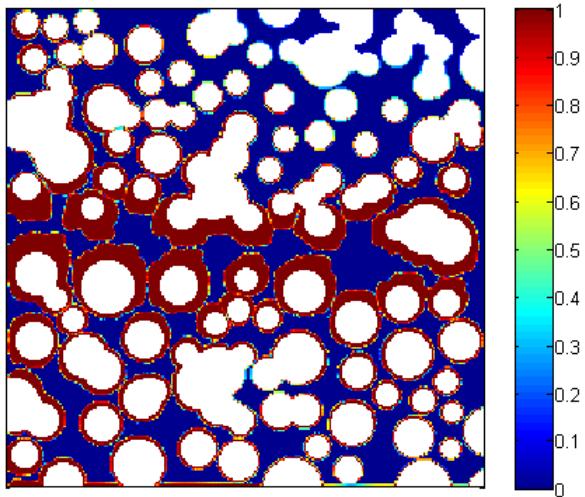
Medium Pe; Medium Da

# High Pe & Low Da

Speciation

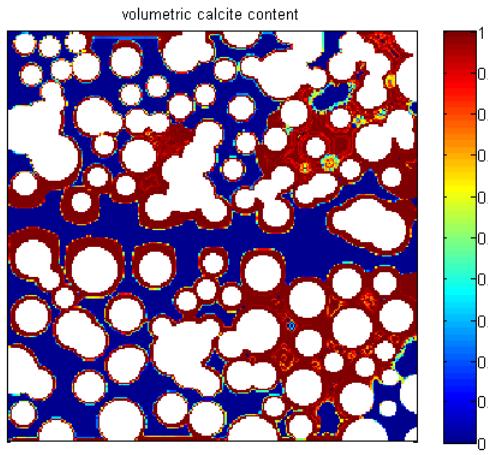


No speciation

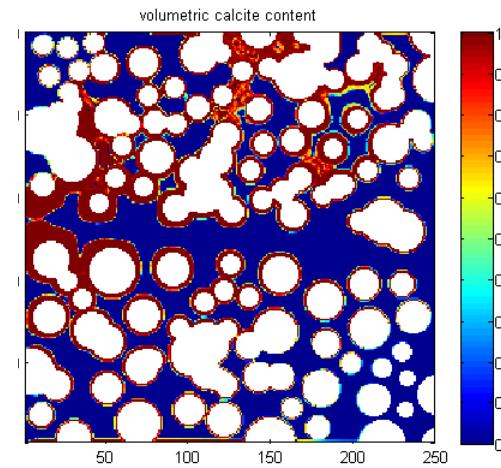


# Pore clogging at the front

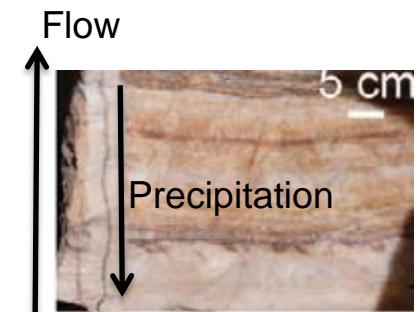
Medium Pe; High Da



Low Pe; Medium Da

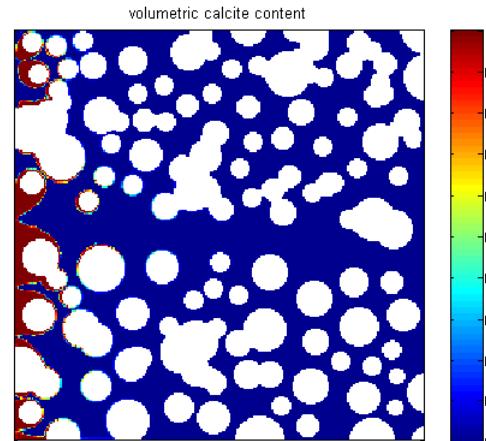
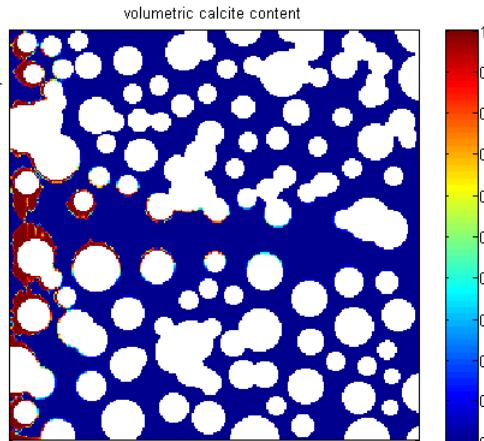


Speciation



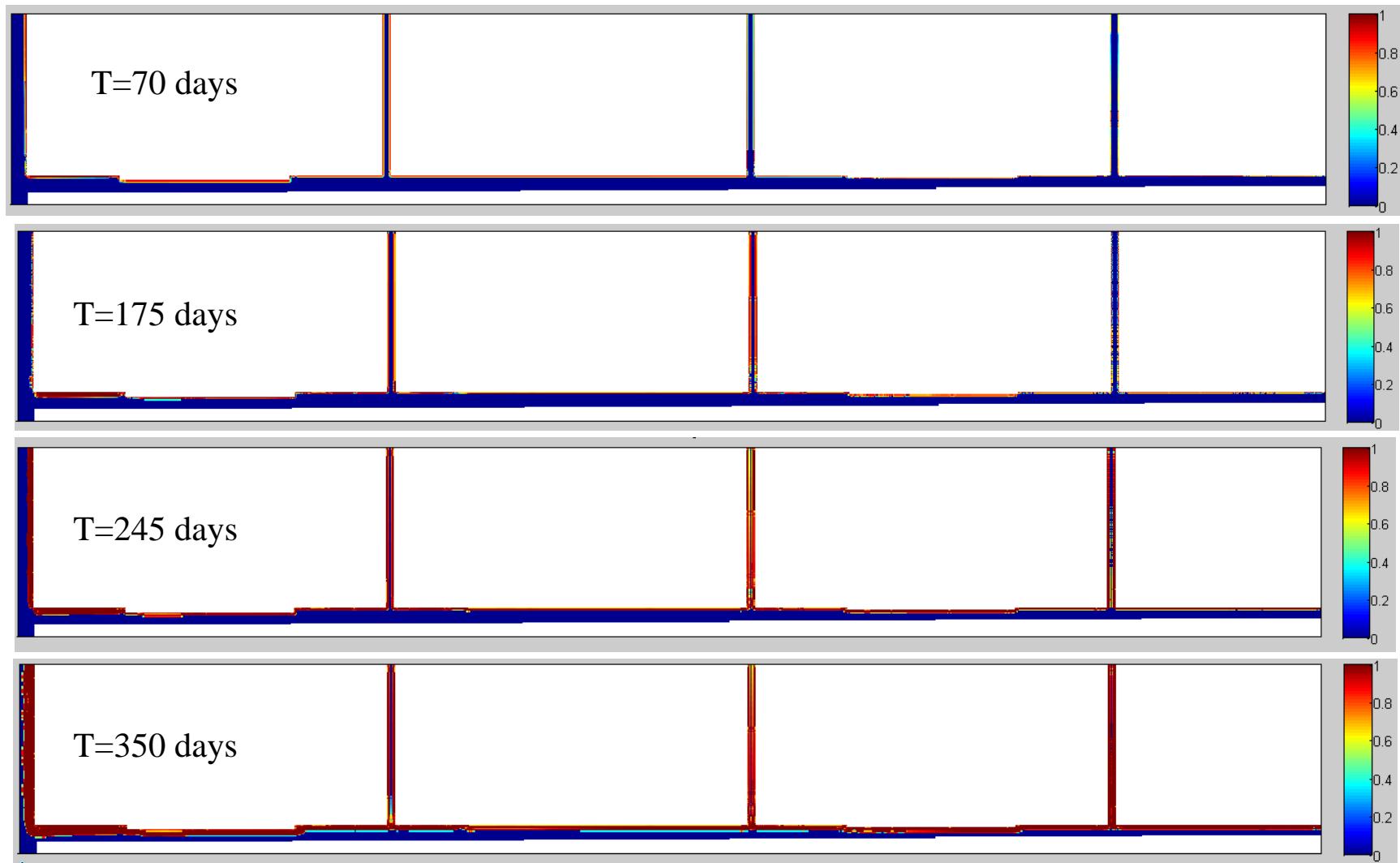
Gratier et al. (2012);  
Crystal Geyser, Utah

No speciation



# High Pe & High Da

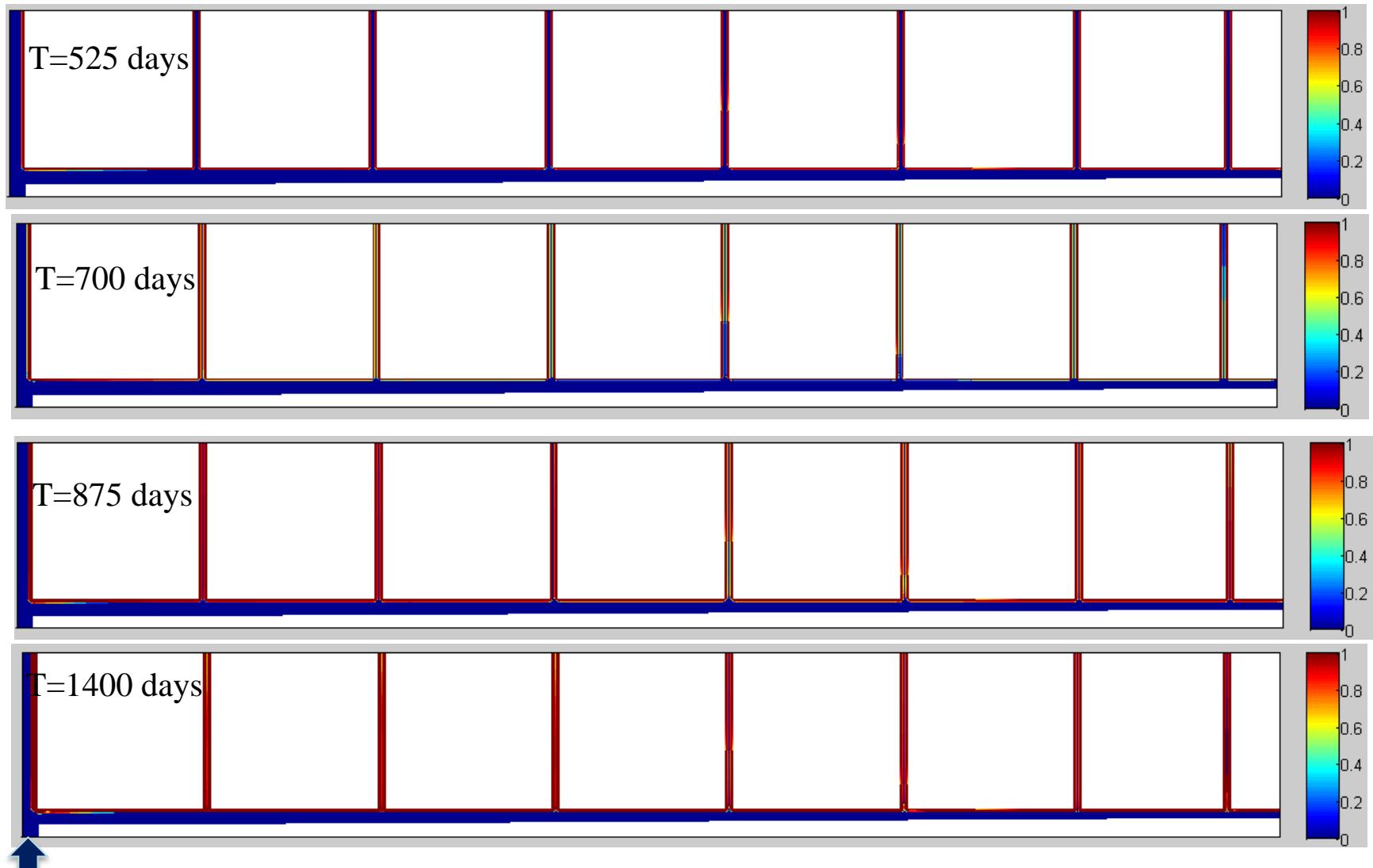
$\text{CaCO}_3$  volumetric content



$[\text{Ca}^{2+}]_T = [\text{CO}_3^{2-}]_T = 20\text{mM}$

# High Pe & Medium Da

CaCO<sub>3</sub> volumetric content



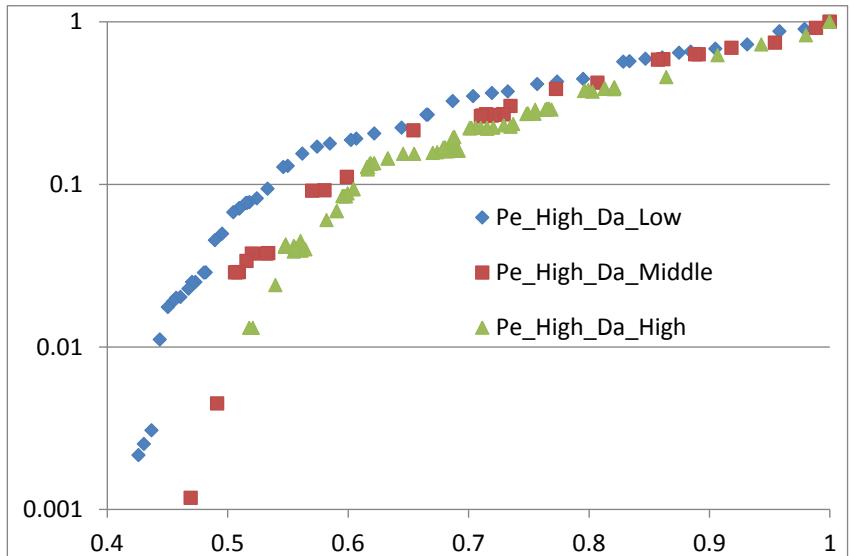
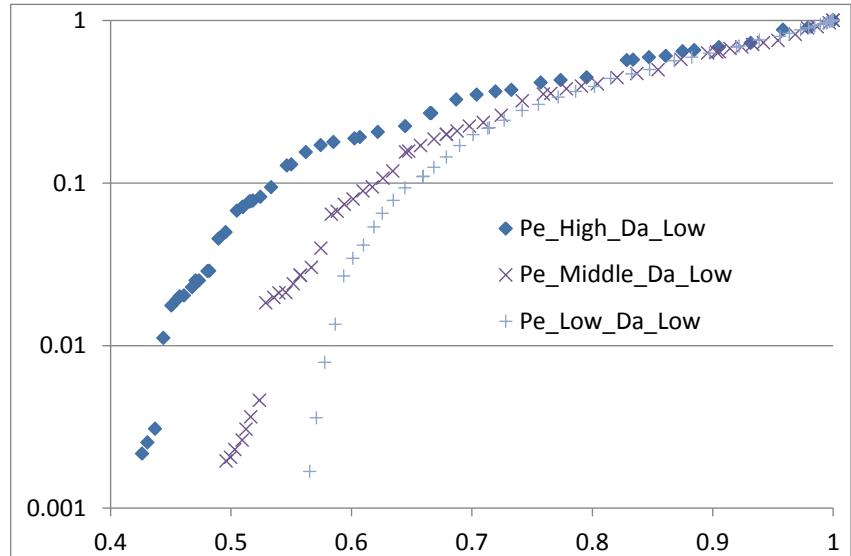
# Summary

- Vigorously tested pore-scale model was used to develop a response function (or dimension reduction model) for continuum-scale permeability and porosity ( $k-\varepsilon$ ) relationships
- Pore scale model was able to qualitatively capture pore clogging patterns observed at the Little Grand Wash Fault
- An adaptive strategy to couple pore- and continuum scale using a response function approach will be tested against travertine patterns observed in the Little Grand Wash Fault
- Algorithms developed in this work will be implemented into a continuum scale reactive transport model (p-FLOTRAN)

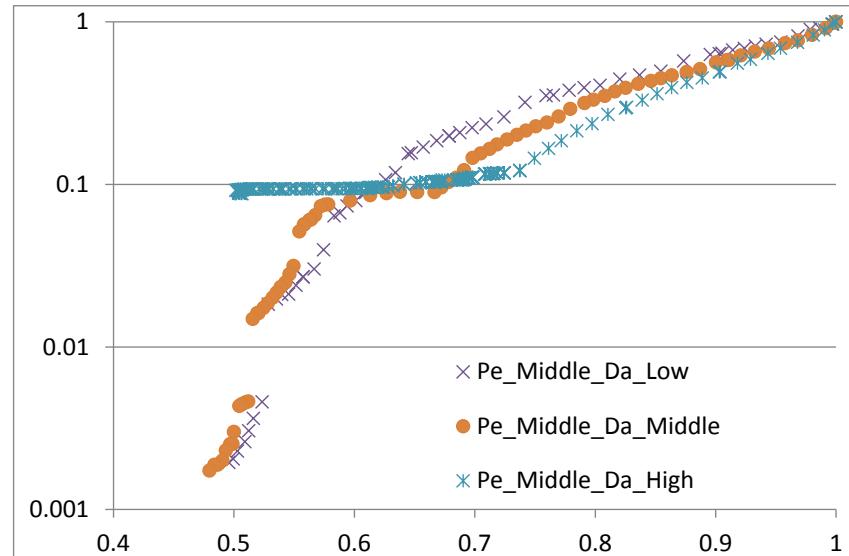
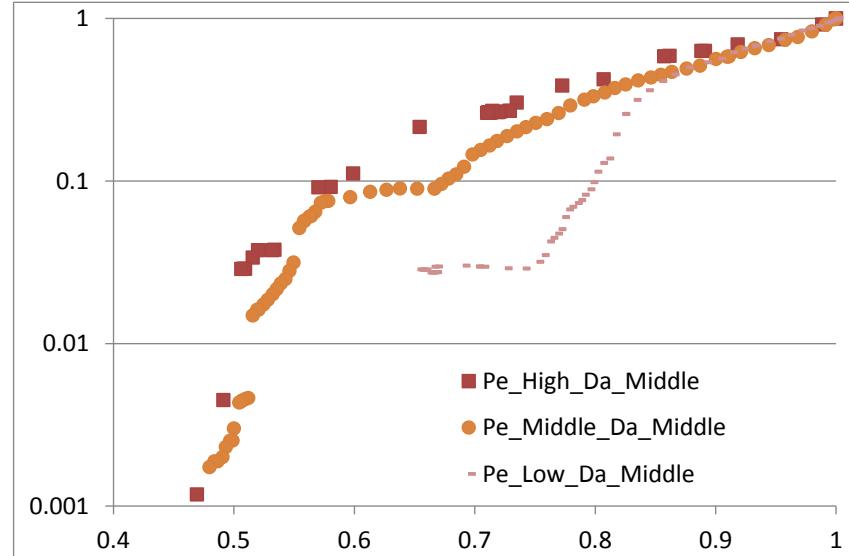
# Questions?

# Permeability-Porosity Relationships

Permeability ( $k/k_0$ )



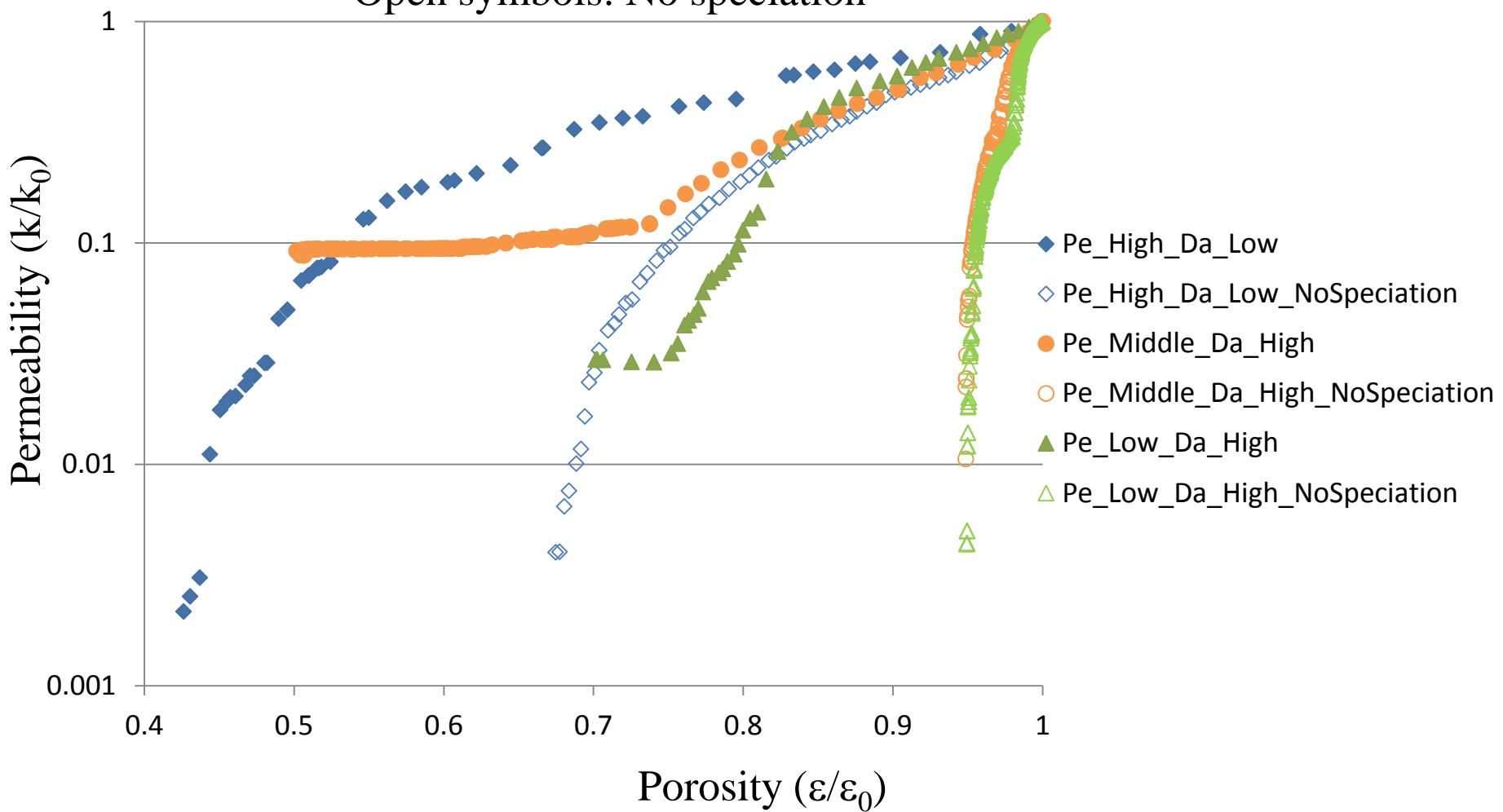
Porosity ( $\varepsilon/\varepsilon_0$ )



# Chemical Speciation

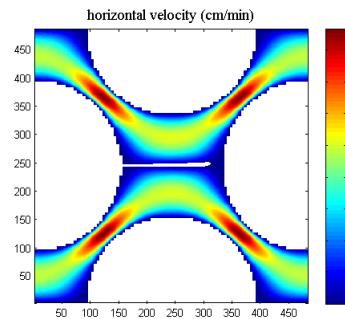
Solid symbols: Speciation

Open symbols: No speciation



# Pore Scale Model Framework

Lattice Boltzmann Method:  
Velocity field ( $u$ ) at pore scale



Velocity at 1 micron resolution

Finite Volume Method: Reactive transport at pore scale

$\Delta t$

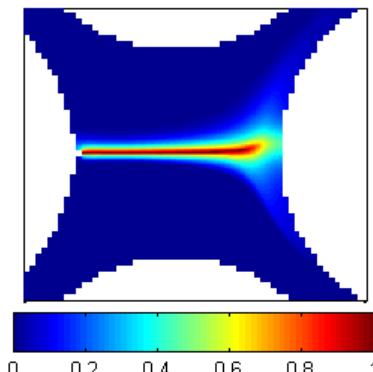
$\Psi_j = C_j + \sum_{i=1}^{N_{eq}} \nu_{ji} C_i$  Chemical equilibrium in bulk fluid (e.g.,  $\text{H}^+$ ,  $\text{HCO}_3^-$ , ...)  
Extended Debye-Hückel Equation for activity coefficients

$$D \frac{\partial \Psi_j}{\partial \mathbf{n}} = -I_m \quad \text{on reactive surface}$$

$$I_m = k_{cc} \left( [\Omega]^n - 1 \right)^n \quad \Omega = \frac{Q_{cc}}{K_{sp}} \text{ or } \ln \left( \frac{Q_{cc}}{K_{sp}} \right)$$

Update of  $\text{CaCO}_3$  volumetric content ( $V_m$ )

$$\frac{\partial V_m}{\partial t} = \overline{V_m} s_m k_{cc} \left( \left[ \frac{a_{\text{Ca}^{2+}} a_{\text{CO}_3^{2-}}}{K_{sp}} \right]^n - 1 \right)^m$$



Mineral phase  
volumetric content

# Fracture network

