

# A Performance Assessment Model for Generic Repository in Salt Formation

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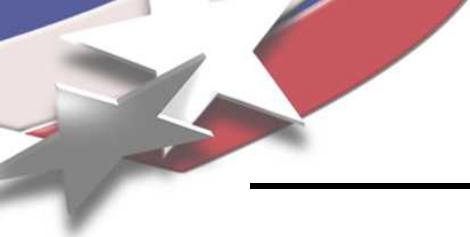
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# Outline

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- **Introduction**
- **Conceptual model**
- **Waste inventories and scenarios**
- **Radionuclide (RN) mobilization and transport**
- **Model results**
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- **Future work**

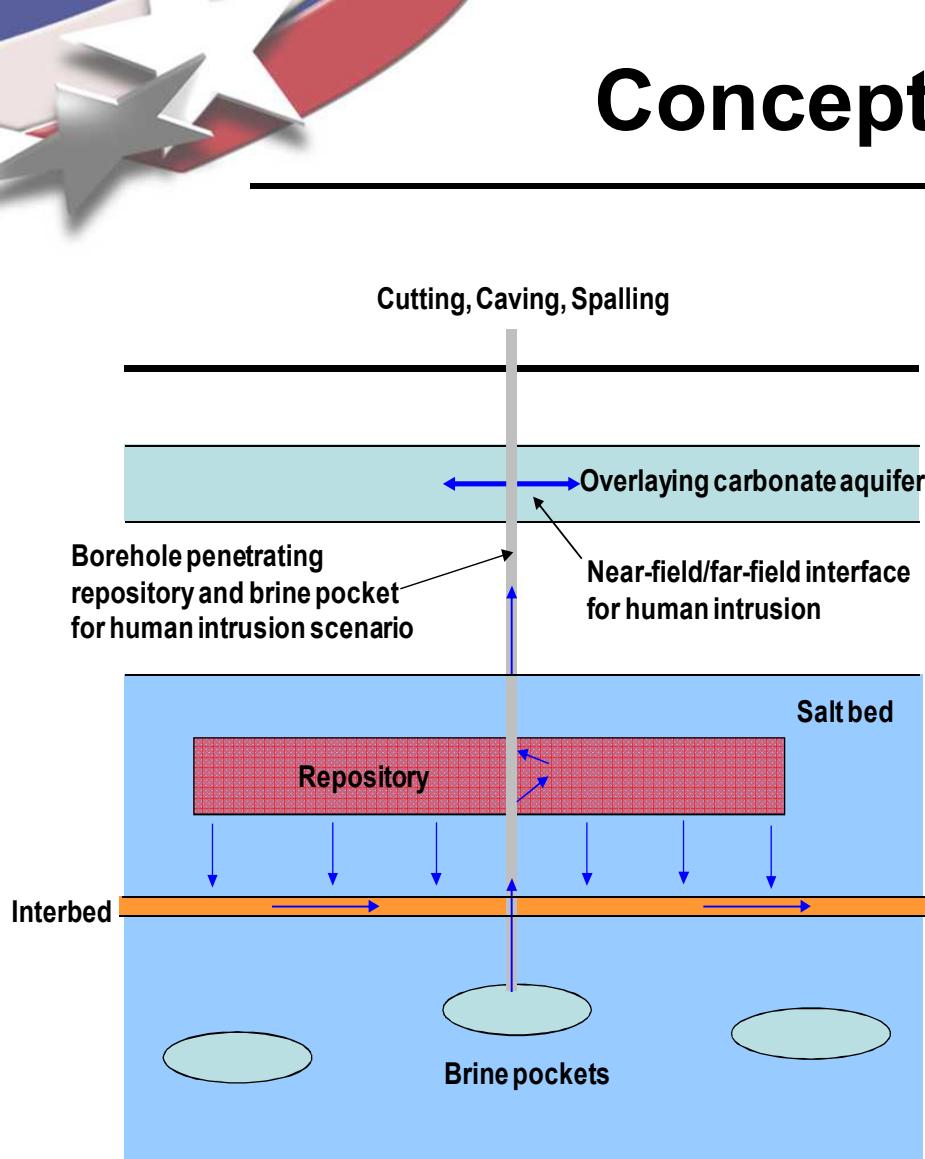


# Introduction

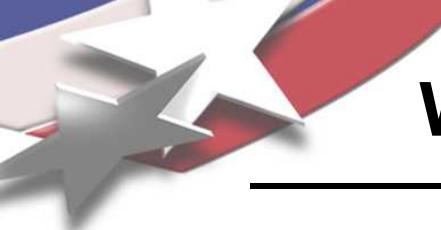
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- Salt repository is one of four generic disposal system environment (GDSE) options currently under study by U.S. DOE
  - Stable geology
  - Chemically reducing condition
  - Self-healing by creep deformation
  - Limited water availability and movement
- The salt GDSE study is to support the development of a long-term strategy for geologic disposal of high-level radioactive waste in a salt formation
- The immediate goal is to develop the necessary modeling tools to evaluate and improve understanding on the repository system response and relevant processes

# Conceptual Model



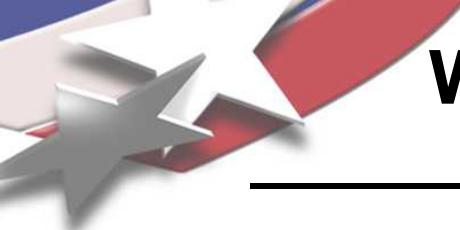
- **Saturated, reducing condition**
  - Assume repository in a bedded salt formation below a carbonate aquifer
- **Isothermal condition at ambient temperature**
- **Undisturbed Scenario**
  - RNs released into and transported in an interbed (1 m thick) below repository
- **Disturbed Scenario**
  - “stylized” human intrusion scenario
  - A single borehole penetration at 1,000 years
  - Sample the number of affected waste packages (WPs) (between 1 and 5)
  - RNs from affected WPs released directly to overlying aquifer by pressurized brines with steady-state flow rates
  - Not consider potential dose impacts of waste brought up by drilling activities



# Waste Inventories and Scenarios

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- **Waste types**
  - Commercial used nuclear fuel (UNF) (140,000 MTU)
    - Convert the total inventory to equivalent pressurized water reactor (PWR) inventory for simplification
    - 32,154 UNF WPs (10 assemblies per WP)
    - Isotope inventory based on the PWR UNF
      - 60 GWd/MTHM burn-up
      - 4.73% enrichment
      - 30 yrs after discharge from reactor
  - Vitrified existing DOE high-level radioactive waste (HLW)
    - 5,003 WPs (5 canisters per WP)
  - Vitrified “hypothetical” reprocessing HLW of commercial UNF
    - 99% recovery of U and Pu from commercial UNF
    - Assume all others remain in the waste stream
    - Assume the same RN mass and isotope inventory per canister as DOE HLW
    - 4,055 WPs (5 canisters per WP)



# Waste Inventories and Scenarios

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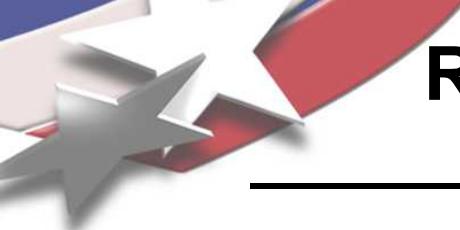
- **Assume a square repository footprint**
  - Spacing between emplacement tunnels: 25 m
  - Spacing between WPs: 6 m
- **Waste inventory cases for Undisturbed Scenario**
  - Case 1: UNF plus DOE HLW
    - A square repository footprint with a side of 3,270 m
  - Case 2: DOE HLW plus reprocessing HLW
    - A square repository footprint with a side of 1,615 m
- **Waste inventory cases for Disturbed Scenario**
  - Case 1: assume only UNF WPs affected
  - Case 2: assume only DOE HLW WPs affected



# Radionuclide Mobilization and Transport

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- Not consider WP containment barrier performance
  - Waste form degradation and RN release at the beginning of simulation
  - Treat the WP interior as porous medium of corrosion products of WP, internal components and waste form
- Fractional degradation rate model for waste form degradation
  - Commercial UNF: log-triangular: min =  $10^{-8}/\text{yr}$ , mode =  $10^{-7}/\text{yr}$ , max =  $10^{-6}/\text{yr}$
  - Glass waste form: log-uniform: min =  $3.4 \times 10^{-6}/\text{yr}$ , max =  $3.4 \times 10^{-3}/\text{yr}$
- Model the near-field as a large mixing cell
  - Not consider RN sorption on corrosion products and geologic materials
- Radio-element solubility for two redox conditions
  - Near-field brines (reducing condition)
  - Far-field brines (less reducing or slightly oxidizing condition)



# Radionuclide Mobilization and Transport

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- RN sorption in the near-field and far-field transport
  - Linear equilibrium sorption ( $K_d$ ) models for interbed and overlying carbonate aquifer
- Pore flow velocity in interbed
  - Log-uniform ( $10^{-8}$  m/yr,  $2 \times 10^{-2}$  m/yr)
- Pore flow velocity in overlying aquifer
  - Log-uniform ( $3.1 \times 10^{-3}$  m/yr, 31 m/yr)
- Performance measure matrix
  - RN mass flux from major system components (e.g., near-field and far-field boundaries)
  - Mean dose at “hypothetical” accessible environment (AE)
    - 5 km down-gradient from the edge of repository
    - IAEA BIOMASS Example Reference Biosphere 1B (ERB1B) dose model
    - Dilution rate of  $1 \times 10^4$  m<sup>3</sup>/yr in aquifer
    - Individual water consumption rate of 1.2 m<sup>3</sup>/yr

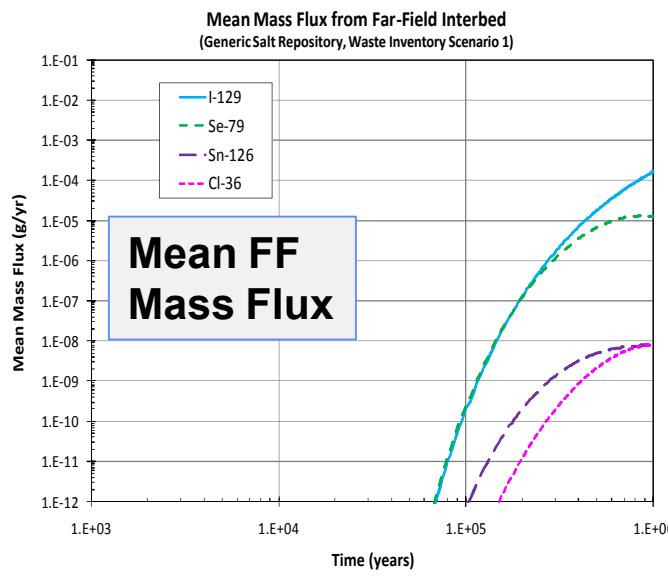
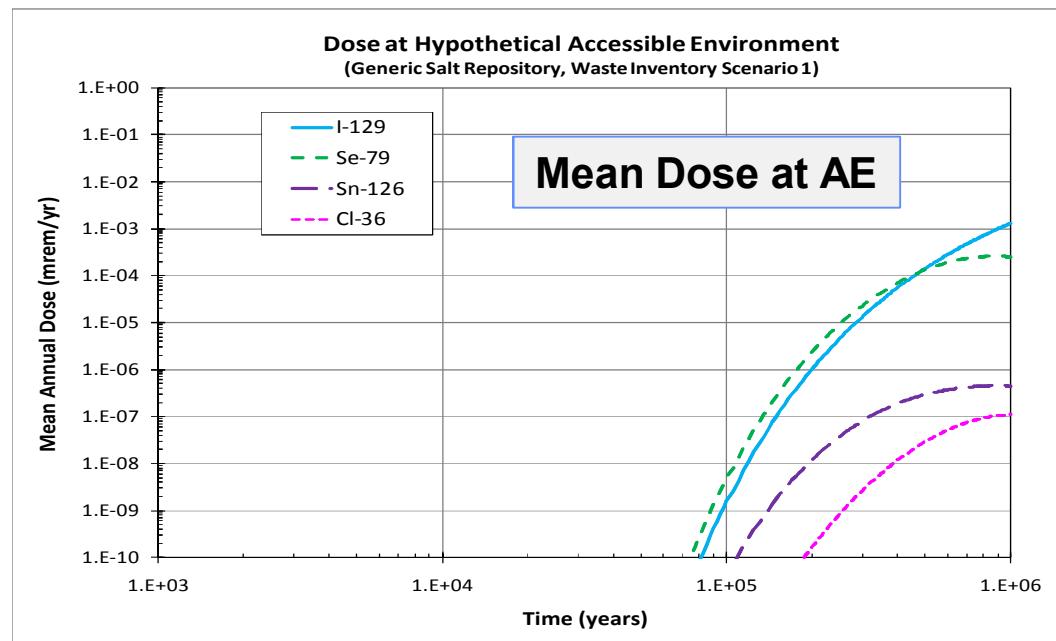
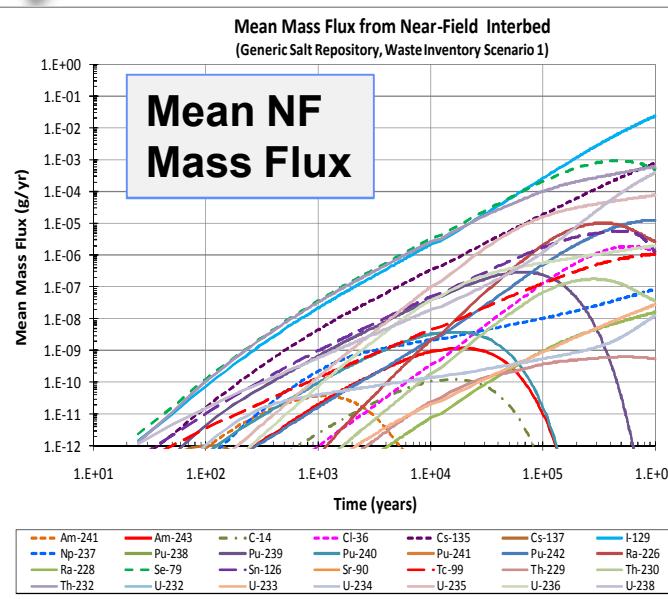


# Major Conservative Bounding Assumptions

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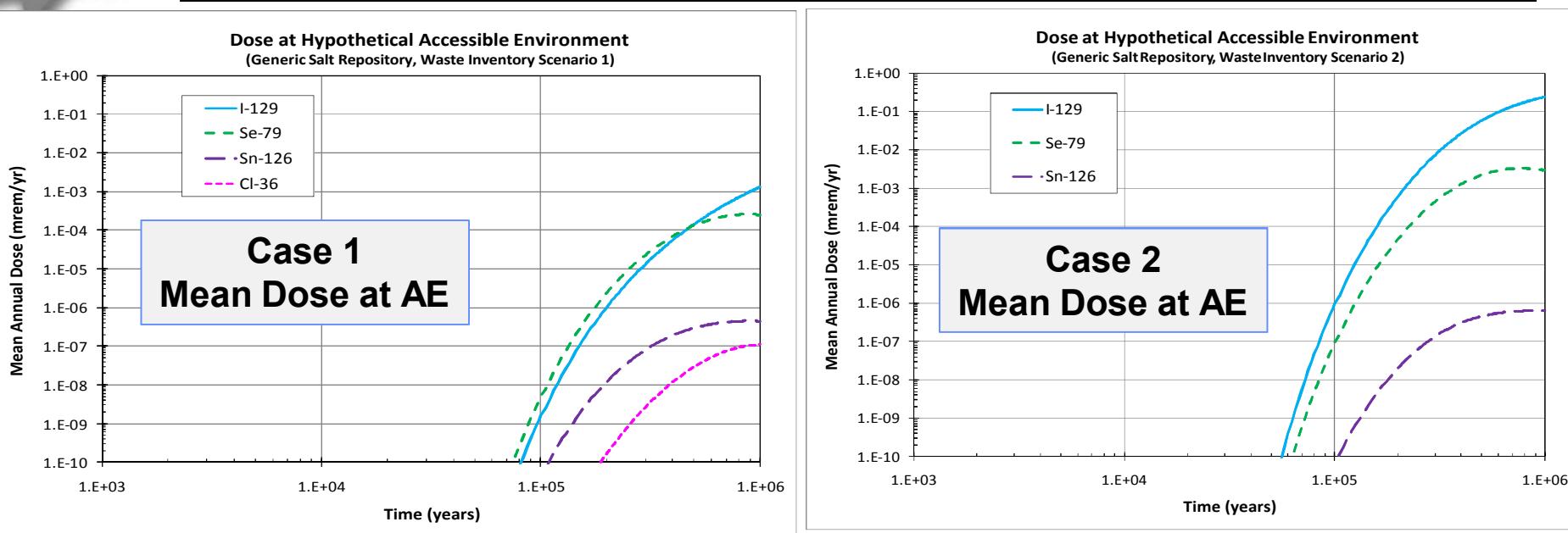
- Not consider RN release delays during initial dry-out period around the waste disposal area due to waste decay heat
  - Dry-out period depending on repository thermal loading, WP heat output characteristics, repository thermal-hydrologic response
- No containment barrier performance of waste package
- No RN sorption on corrosion products in the near-field mixing cell
- Continuous brine flow from waste disposal area to underlying interbed for the entire simulation period for Undisturbed Scenario
- Continuous steady-state upward brine flows through the borehole for the entire simulation period for Disturbed Scenario

# Undisturbed Scenario: Waste Inventory Case 1



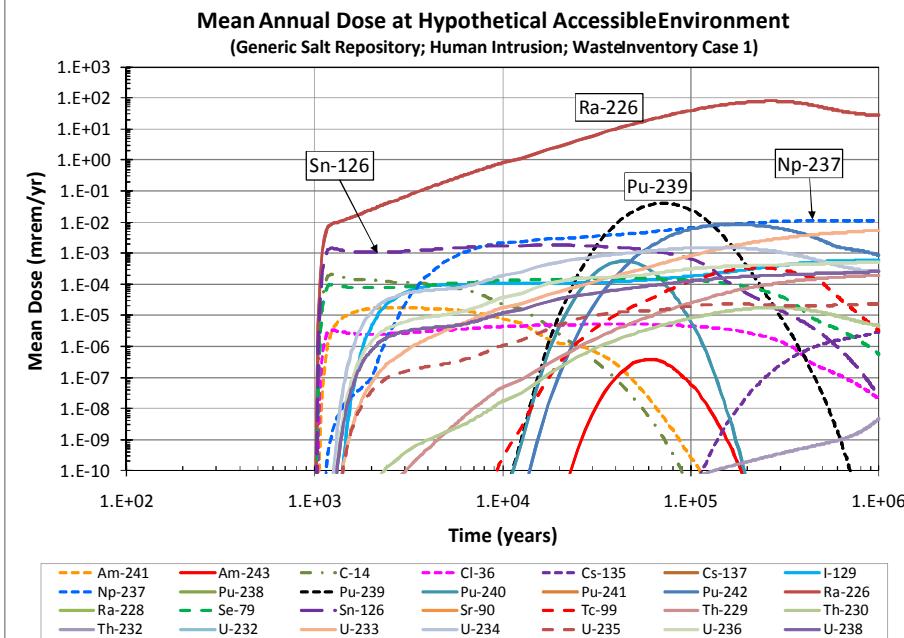
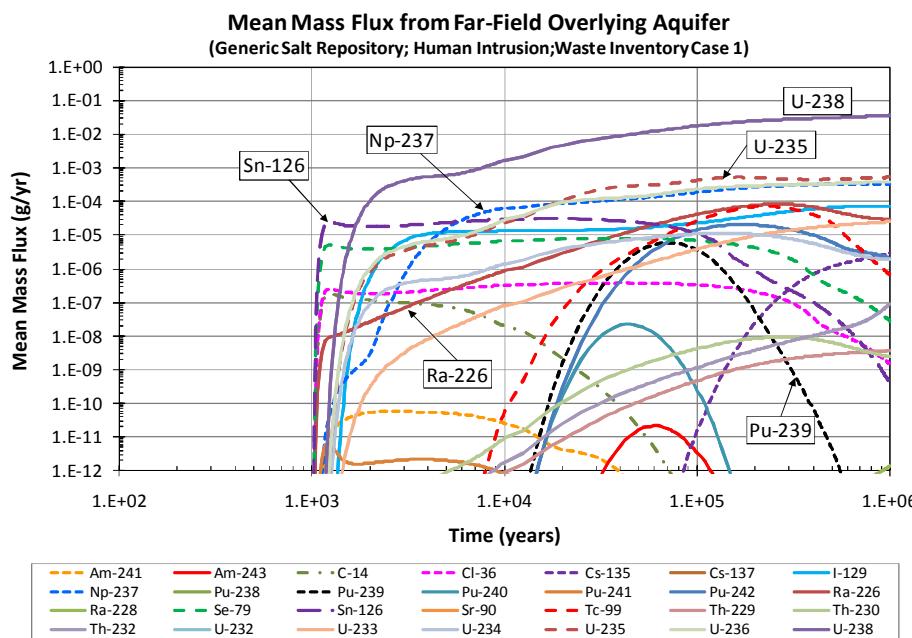
- RN transport greatly retarded in the far-field interbed by sorption
- Non-sorbing or weakly sorbing RNs (I-129, Se-79, Cl-36) with a significant inventory are released from the far-field interbed at noticeable rates
- I-129 is the dominant long-term dose contributor
  - unconstrained solubility
  - Extremely long half-life (~16 M yrs)
  - Significant inventory in the waste

# Undisturbed Scenario: Waste Inventory Case 1 vs. Case 2

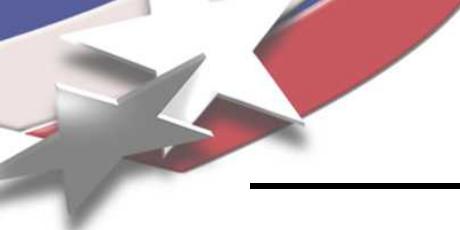


- Higher mean peak dose for Waste Inventory Case 2
  - Higher fission products inventory on a per-WP basis for Waste Inventory Case 2
    - Assumptions on the reprocessing HLW inventory
  - Degradation rate of the glass waste form (DOE HLW and reprocessing HLW) 2 to 3 orders of magnitude higher than the UNF degradation rate
  - Higher concentrations of soluble RNs (I-129, Se-79) in the near-field water for Waste Inventory Case 2
    - A smaller near-field water volume

# Disturbed Scenario: Waste Inventory Case 1



- **Different mass release rate and dose histories from Undisturbed Scenario**
  - RNs transported advectively at much higher rates in the overlying aquifer than the interbed
- **Ra-226 is the dominant dose contributor**
  - Assume unconstrained solubility and non-sorbing behavior for Ra
  - Ra known to readily sorb on geologic materials and not mobile in groundwater
- **Higher doses for the actinides due to direct release into the overlying aquifer with higher water flow rates**



# Summary and Conclusions

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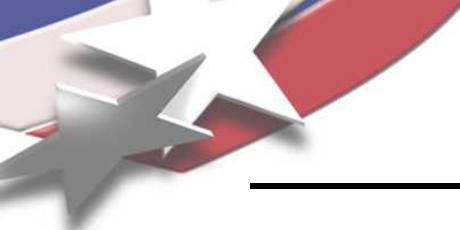
- Soluble, non-sorbing fission products (I-129, Se-79) are the major dose contributors
  - Uncertain solubility and sorption behavior of Se in chemically reducing geologic environments
- RN release pathways and scenarios are important to the response of a generic salt repository
  - Improved conceptual models that are more representative of a salt repository
- Need to evaluate impact of the conceptual model simplification and bounding conservative assumptions
  - Brine movement under thermal perturbation
  - WP performance
  - Geologic behaviors of key RNs (I, Se and Ra)



# Future Work

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- Develop thermal analysis tools for thermal loading and thermo-hydrologic response in generic salt repository, incorporating associated processes
  - Salt creep deformation and consolidation
  - Brine movement
- Improve near-field chemistry for generic salt repository environment
  - High ionic strength, elevated temperature, reducing condition
  - Solubility and sorption of RNs in near-field environments
- Flow and RN transport in generic interbed
- Degradation of WP, candidate waste forms and other EBS components in generic salt repository environment
  - Characterization and quantification of gases generated from corrosion in concentrated brine under reducing condition



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# Backup Slides



# Near-Field and Far-Field Radionuclide Elemental Solubility

## Near-field Radionuclide Elemental Solubility

Element	Distribution Type	Solubility (molal)
U	Triangular	4.89E-08 (min); 1.12E-07 (mode); 2.57E-07 (max)
Pu	Triangular	1.40E-06 (min); 4.62E-06 (mode); 1.53E-05 (max)
Am	Triangular	1.85E-07 (min); 5.85E-07 (mode); 1.85E-06 (max)
Np	Triangular	4.79E-10 (min); 1.51E-09 (mode); 4.79E-09 (max)
Th	Triangular	2.00E-03 (min); 4.00E-03 (mode); 7.97E-03 (max)
Tc	Log-Triangular	4.56E-10 (min); 1.33E-08 (mode); 3.91E-07 (max)
Sn	Triangular	9.87E-09 (min); 2.66E-08 (mode); 7.15E-08 (max)
C, Cl, Cs, I, Se, Sr	n/a	Unlimited solubility

Note: Source: Ref. 3.

- Chemically reducing conditions.
- Elements Ac, Cm, Nb, Pa, Pd, Ra, Sb, Zr are known to be solubility-limited, but are implemented as unlimited solubility in the near- and far-field model because their solubility calculations have not been completed.

## Far-field Radionuclide Elemental Solubility

Element	Distribution Type	Solubility (molal)
U	Triangular	9.16E-05 (min); 2.64E-04 (mode); 7.62E-04 (max)
Pu	Triangular	7.80E-07 (min); 2.58E-06 (mode); 8.55E-06 (max)
Am	Triangular	3.34E-07 (min); 1.06E-06 (mode); 3.34E-06 (max)
Np	Log-triangular	1.11E-06 (min); 1.11E-05 (mode); 1.11E-04 (max)
Th	Triangular	8.84E-06 (min); 1.76E-05 (mode); 3.52E-05 (max)
Sn	Triangular	1.78E-08 (min); 4.80E-08 (mode); 1.29E-07 (max)
C, Cl, Cs, I, Se, Sr, Tc	n/a	Unlimited solubility

Note: Source: Ref. 3.

- Chemically less reducing conditions than the near-field concentrated brines.
- Elements Ac, Cm, Nb, Pa, Pd, Ra, Sb, Zr are known to be solubility-limited, but are implemented as unlimited solubility in the near- and far-field model because their solubility calculations have not been completed.

# Radionuclide Transport Parameters

## Interbed Transport Parameters

Parameter	Distribution Type	Parameter Value
Aquifer thickness	Constant	4 m
Matrix porosity	Uniform	0.07 (min); 0.3 (max)
Bulk density	Constant	2800 kg/m <sup>3</sup>
Matrix Tortuosity	Uniform	0.03 (min); 0.5 (max)
Brine flow rate upward through borehole (m <sup>3</sup> /yr)	Uniform	0.1 (min); 5.0 (max)
Aquifer water flow rate (m/yr)	Log-uniform	3.15E-03 (min); 3.15E+01 (max)
Longitudinal Dispersivity	Constant	10% of flow conduit length
Kd for Radioelements (ml/g):		
Uranium	Uniform	0.03 (min); 20 (max)
Plutonium	Log-uniform	20 (min); 1.0E+04 (max)
Neptunium	Log-uniform	1 (min); 200 (max)
Americium	Uniform	20 (min); 400 (max)
Thorium	Log-uniform	7.0E+02 (min); 1.0E+04 (max)
Technetium	Triangular	0 (min); 50 (mode); 100 (max)
Cesium	Triangular	40 (min); 500 (mode); 3000 (max)
Strontium	Triangular	5 (min); 13 (mode); 4.0E+04 (max)
Iodine	Uniform	0.01 (min); 100 (max)
Carbon, chlorine, Selenium & Tin	Constant	0 (no sorption)

## Carbonate Aquifer Transport Parameters

Parameter	Distribution Type	Parameter Value
Thickness	Constant	1 m
Porosity	Constant	0.01
Density	Constant	2500 kg/m <sup>3</sup>
Brine flow rate below repository (m/yr)	Log-uniform	1.0E-08 (min); 3.0E-02 (max)
Brine flow rate away from repository (m/yr)	Log-uniform	1.0E-08 (min); 2.0E-02 (max)
Longitudinal Dispersivity	Constant	10% of flow conduit length
Kd for Radioelements (ml/g):		
Uranium	Uniform	0.2 (min); 1 (max)
Plutonium	Uniform	70 (min); 100 (max)
Neptunium	Uniform	1 (min); 10 (max)
Americium	Uniform	25 (min); 100 (max)
Thorium	Uniform	100 (min); 1000 (max)
Technetium	Uniform	0 (min); 2 (max)
Cesium	Uniform	1 (min); 20 (max)
Strontium	Uniform	1 (min); 80 (max)
Carbon, chlorine, Selenium & Tin	Constant	0 (no sorption)

# Undisturbed Scenario: Waste Inventory Case 2

