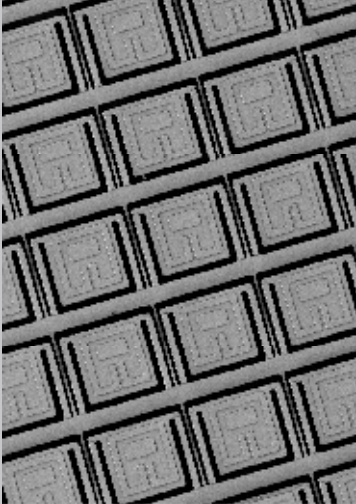




Metamaterial Enhanced Terahertz Sensing

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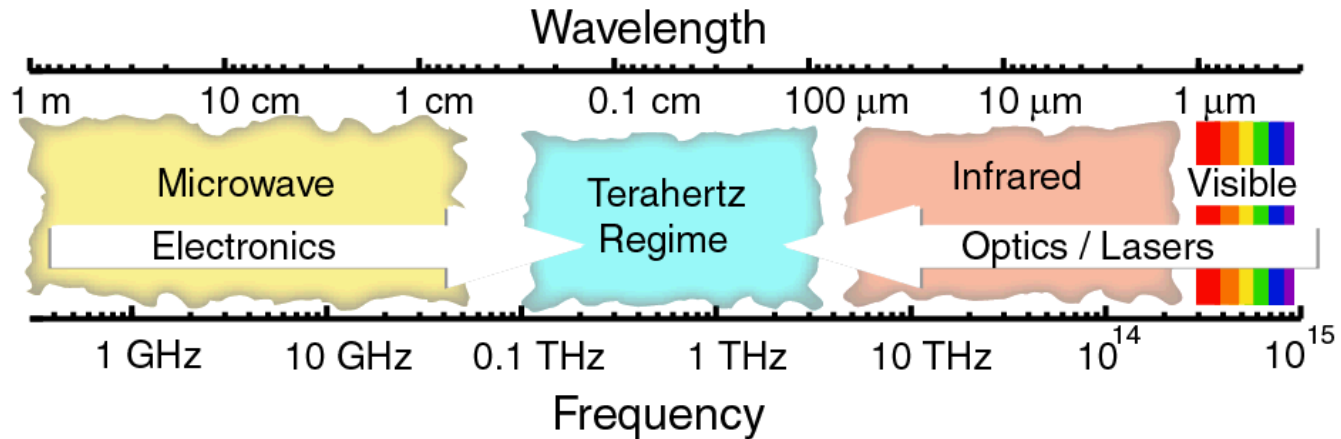
*Exceptional
service
in the
national
interest*



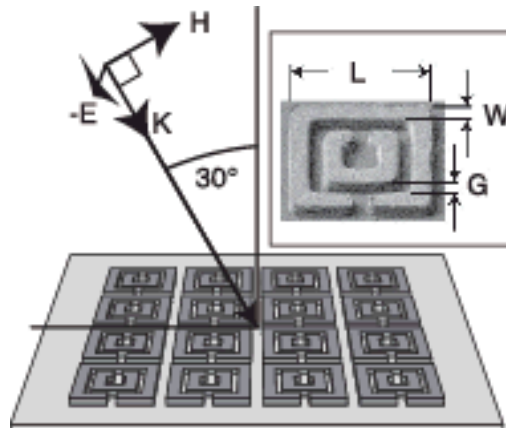
Sandia National Laboratories is a multi-program laboratory managed and operated by Sandia Corporation, a wholly owned subsidiary of Lockheed Martin Corporation, for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000.

THz Regime Good for Metamaterial Sensing

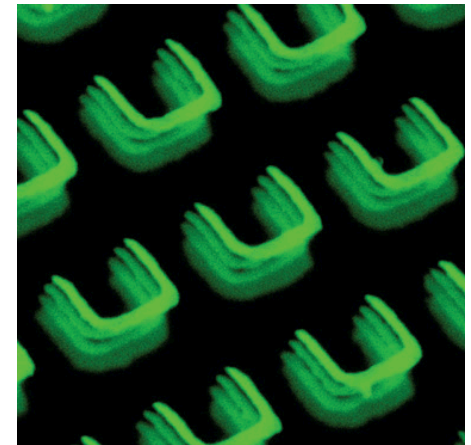
$$1 \text{ THz} \rightarrow 4 \text{ meV} \rightarrow 48 \text{ K} \rightarrow 300 \mu\text{m} \rightarrow 33 \text{ cm}^{-1}$$



D. R. Smith, Phys. Rev. Lett. 14,
234 (2000)

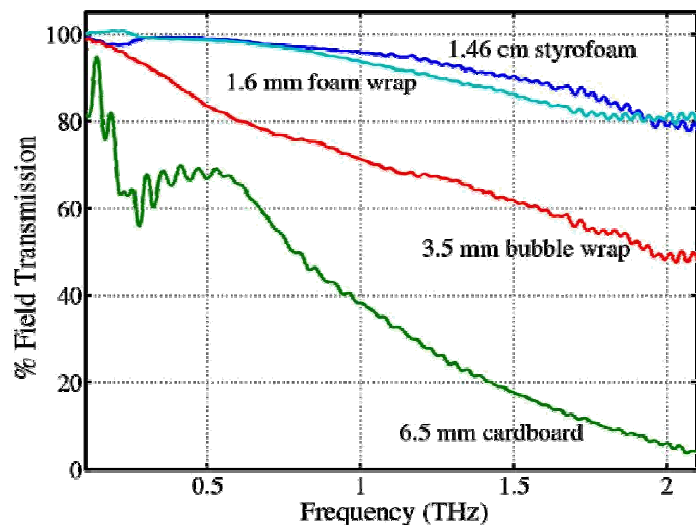


T. J. Yen, Science 393,
1494 (2004)



Na Liu, et al, Nat. Mat. 7,
31 (2008)

THz Imaging – Movement to FPAs



Technology	Sensitivity	Price
Coherent heterodyne	Good	Huge*
Coherent direct (with MMIC preamplification)	Good	Large
Cryogenic Microbolometers	Good	Moderate
Incoherent direct (i.e. diodes, no preamplification)	Moderate	Small
Antenna coupled microbolometers	Poor (active only)	Tiny

Maximum frequency

~200 GHz

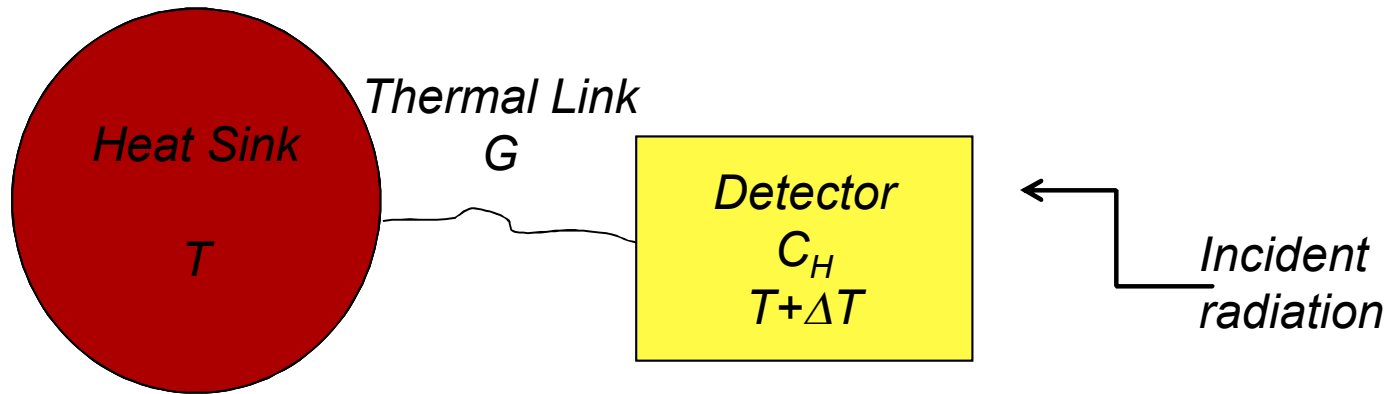
600 GHz

> 1THz

Decreasing complexity
Decreasing sensitivity
Increasing detector requirements

Arttu Luukanen, MilliLab/VTT
Tech. Res. Cent. Finland

Thermal Detector Considerations



Three main considerations

- **Thermal Engineering: Conductance and Heat Capacity**
- Physical property with sensitive thermal response
- Signal readout / amplification etc.

$$\eta_{abs} P_{inc} = G \Delta T + C_H \frac{d(\Delta T)}{dt}$$

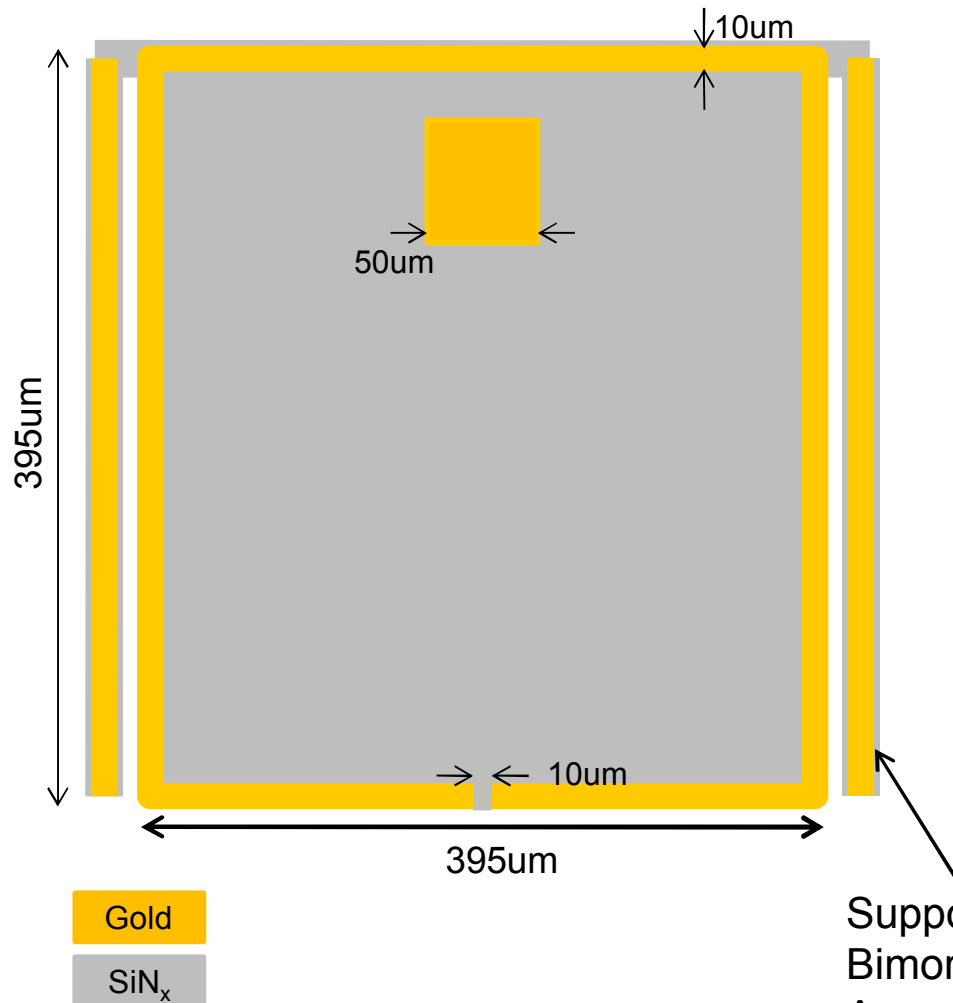
E. H. Putley, "Thermal Detectors"

$$\Delta T = \frac{\eta_{abs} P_{\omega}}{(G^2 + \omega^2 C_H^2)^{1/2}}$$

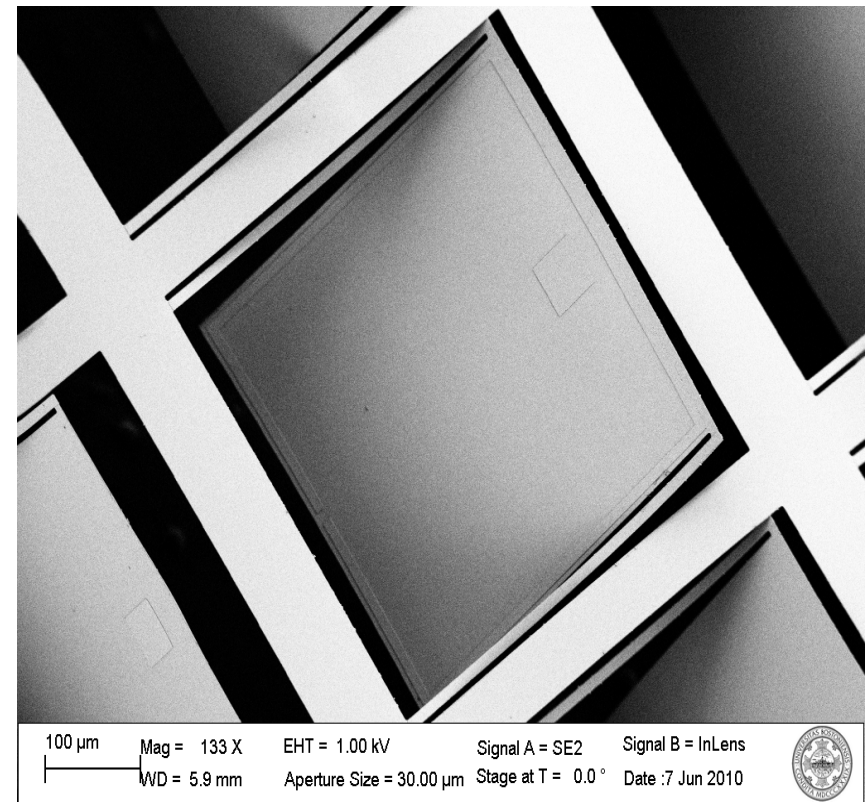
$$\tau = C_H / G$$

95 GHz Detector

Layout of 95 GHz Detector

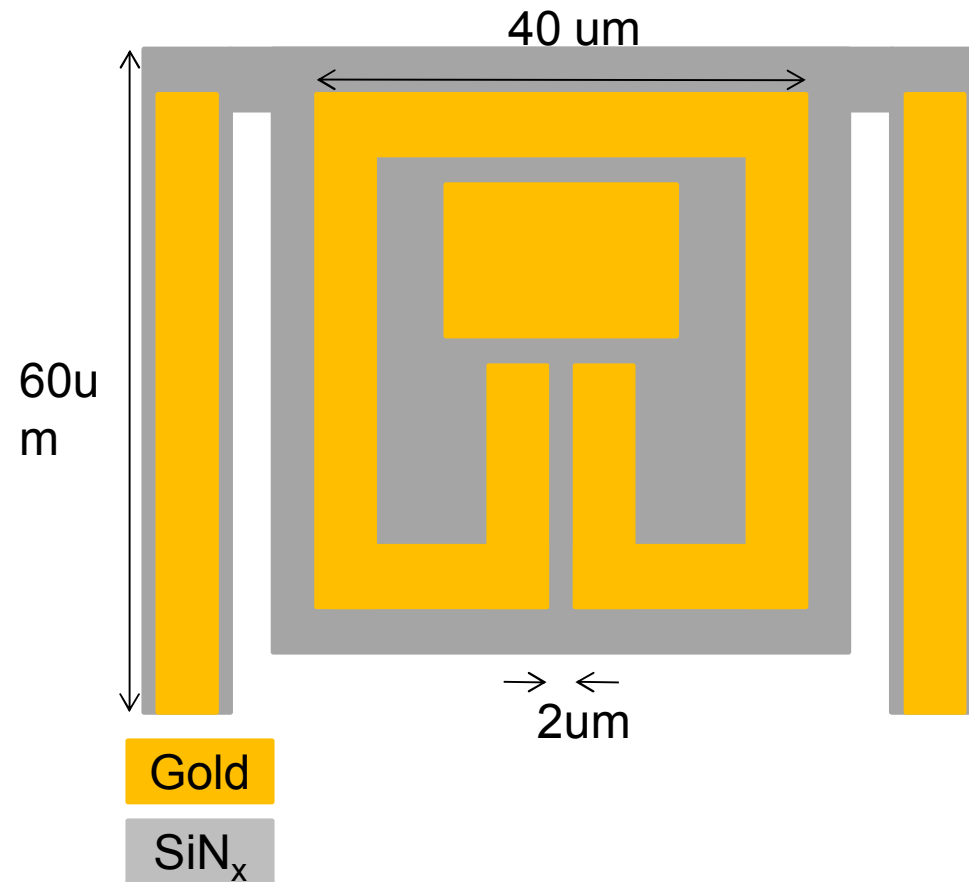


Micrograph of 95 GHz Detector

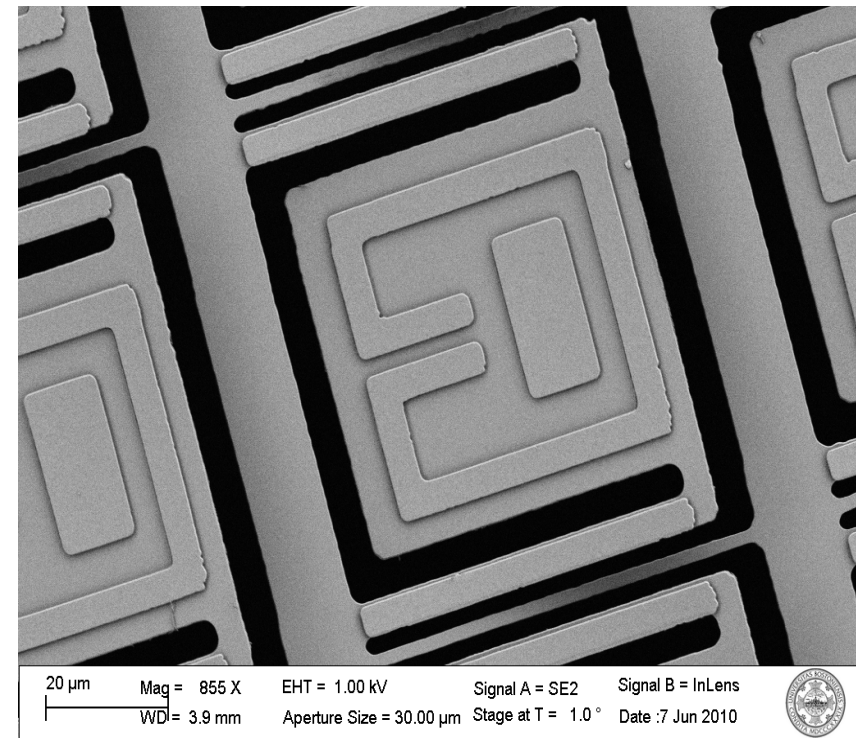


693 GHz Detector

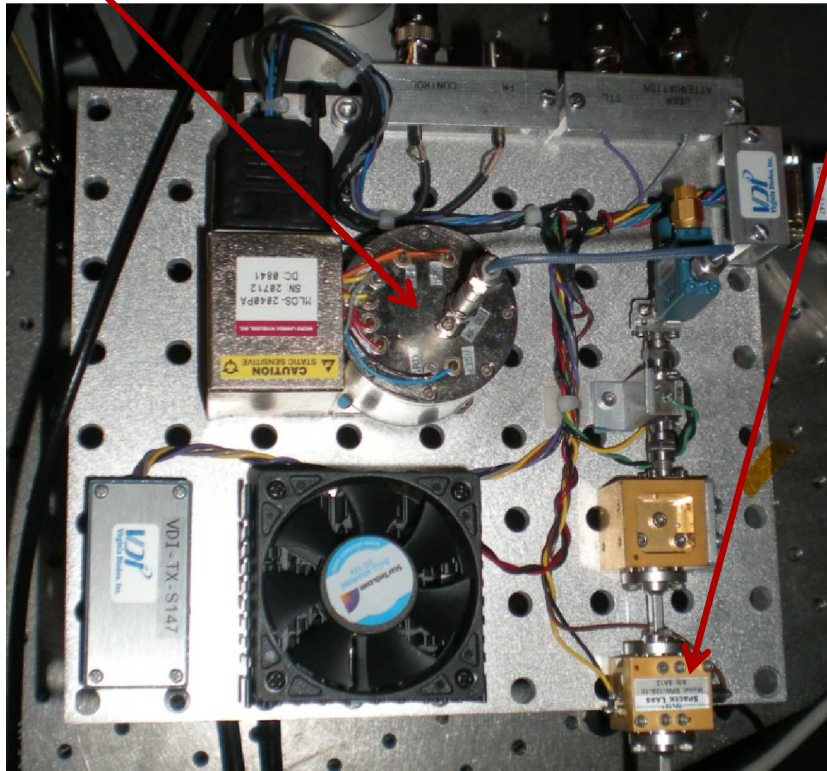
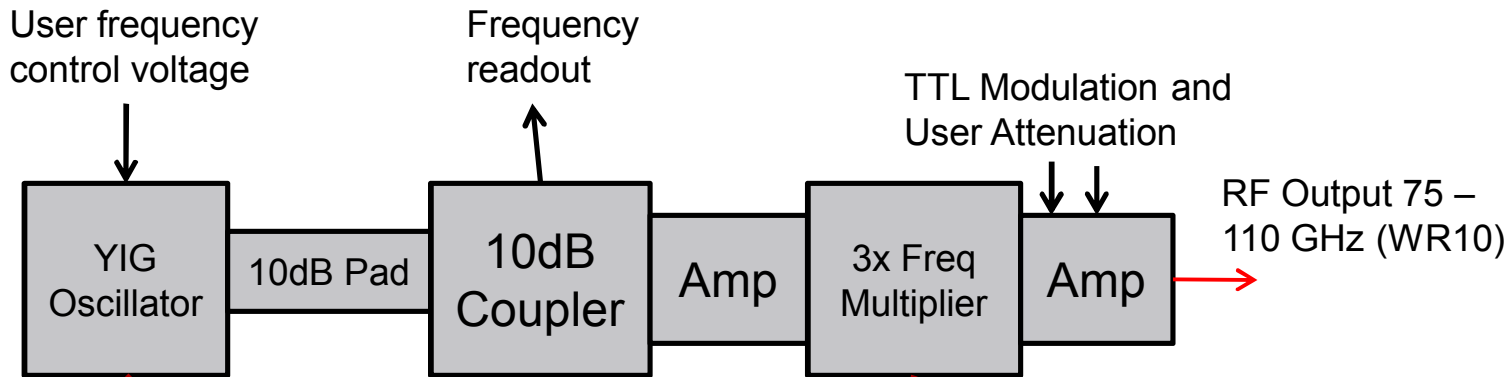
Layout of 693 GHz Detector



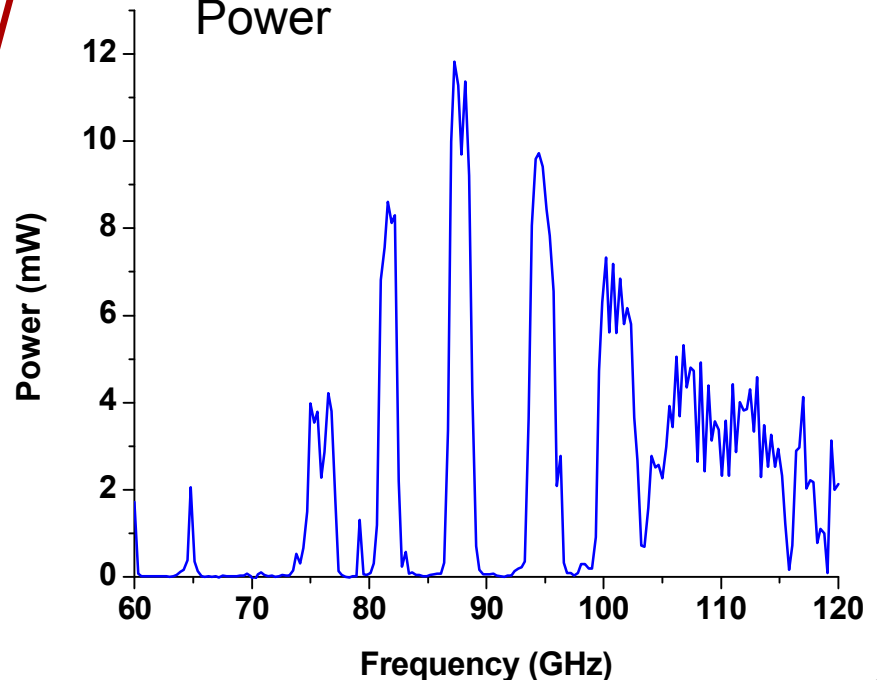
Micrograph 693 GHz Detector



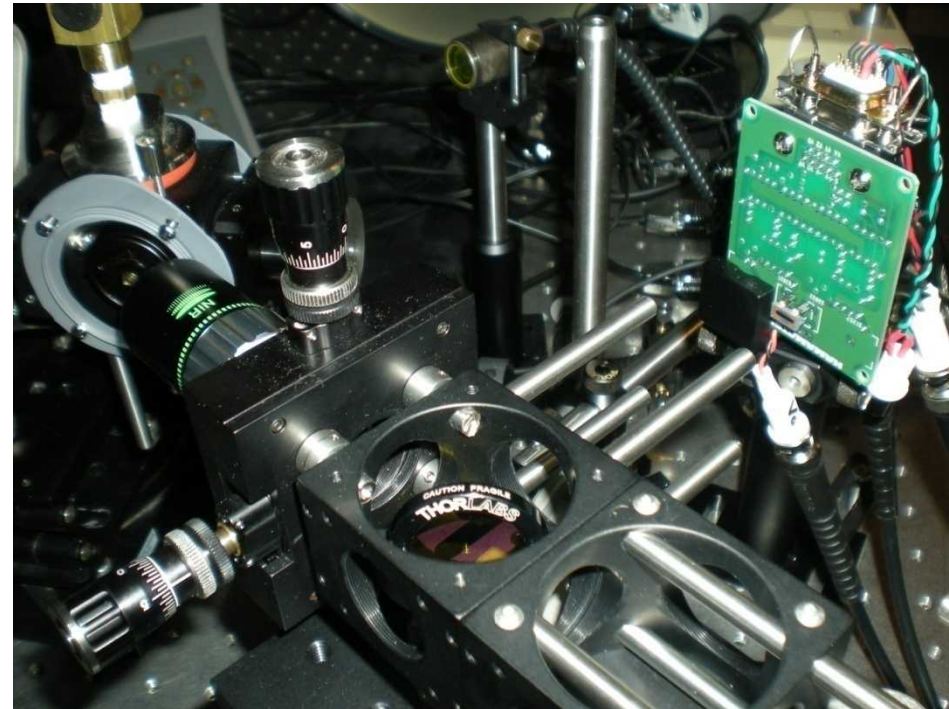
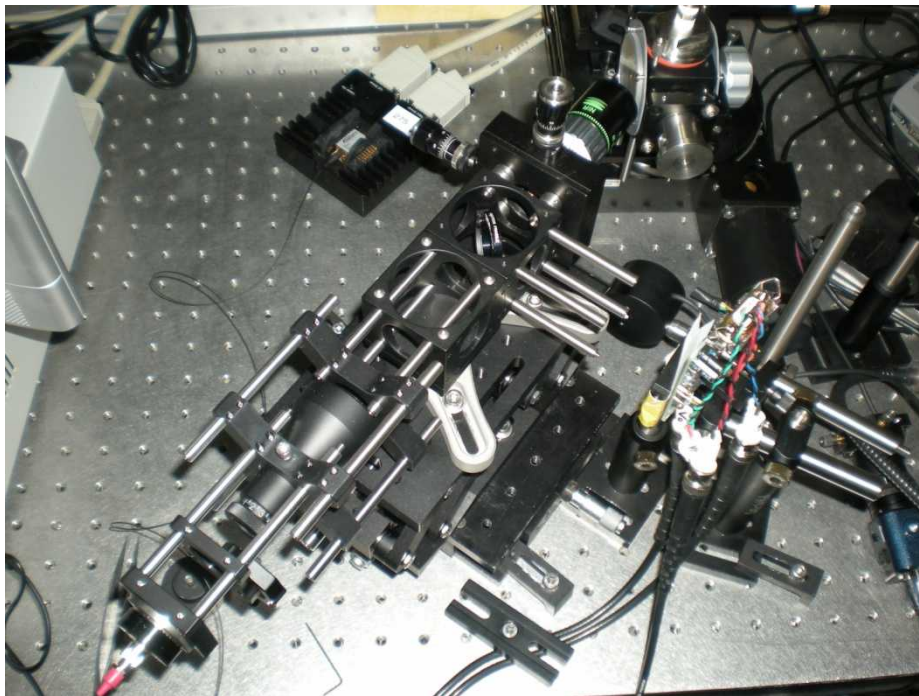
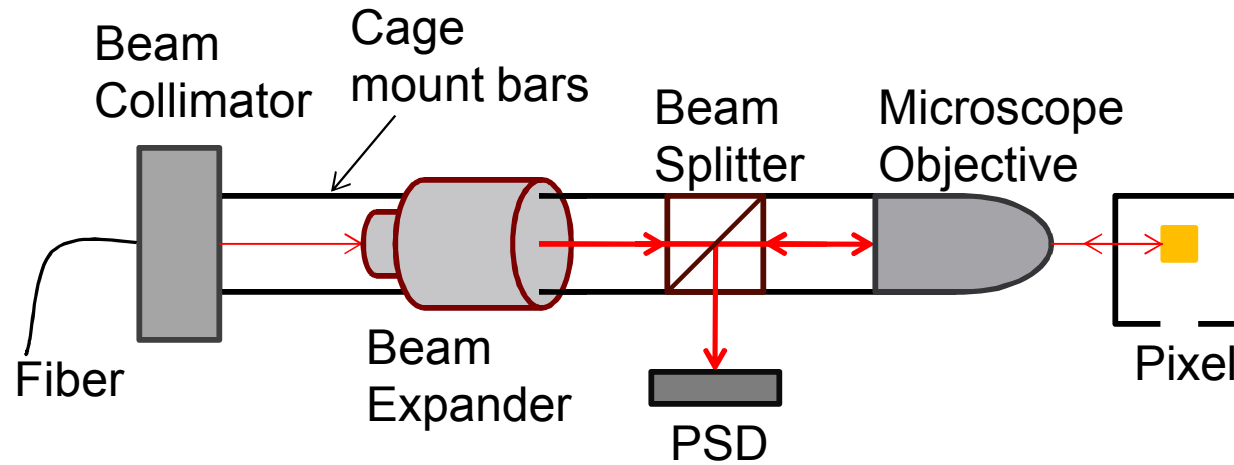
95 GHz Characterization - Virginia Diodes Tunable THz Source



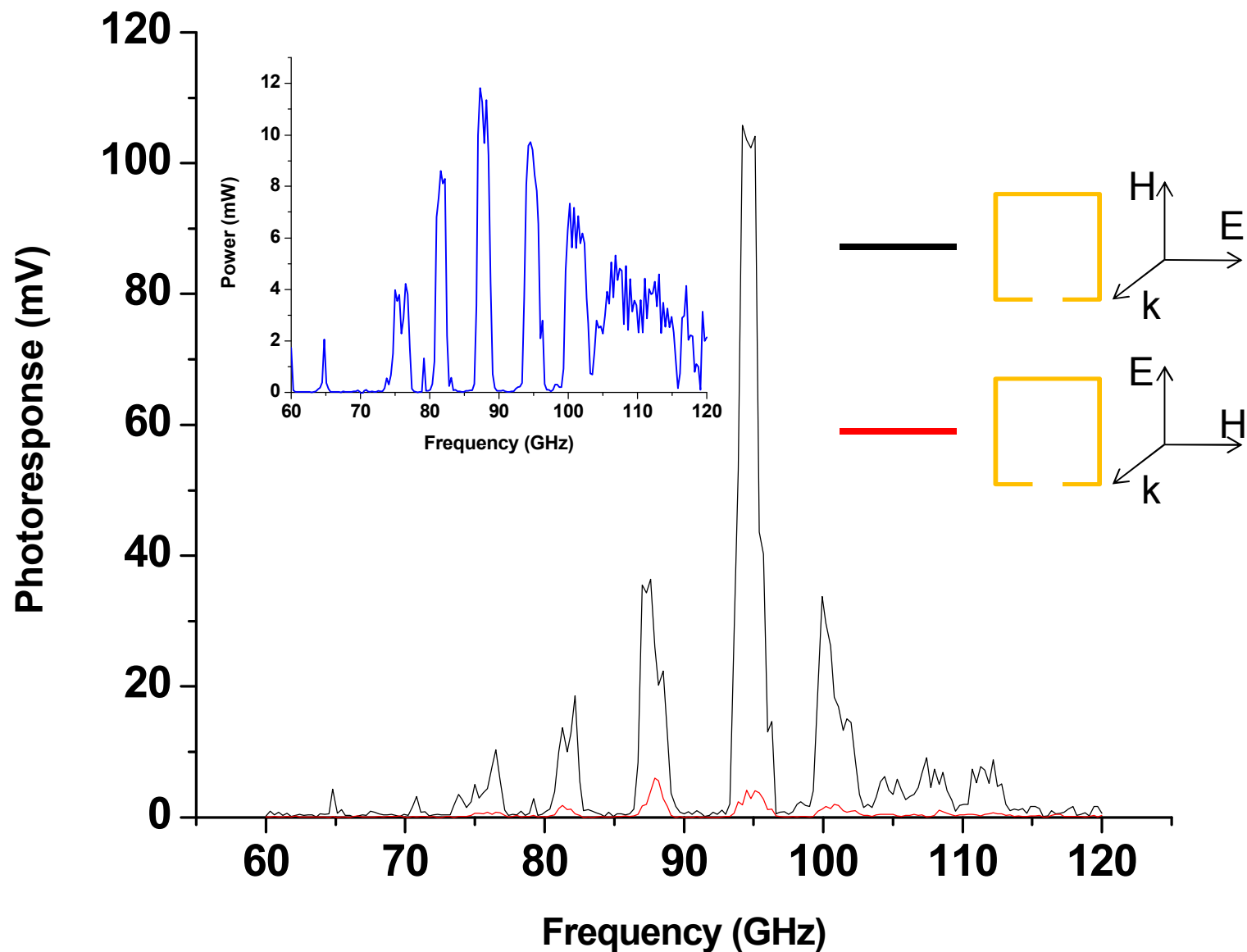
VDI THz Source – Output Power



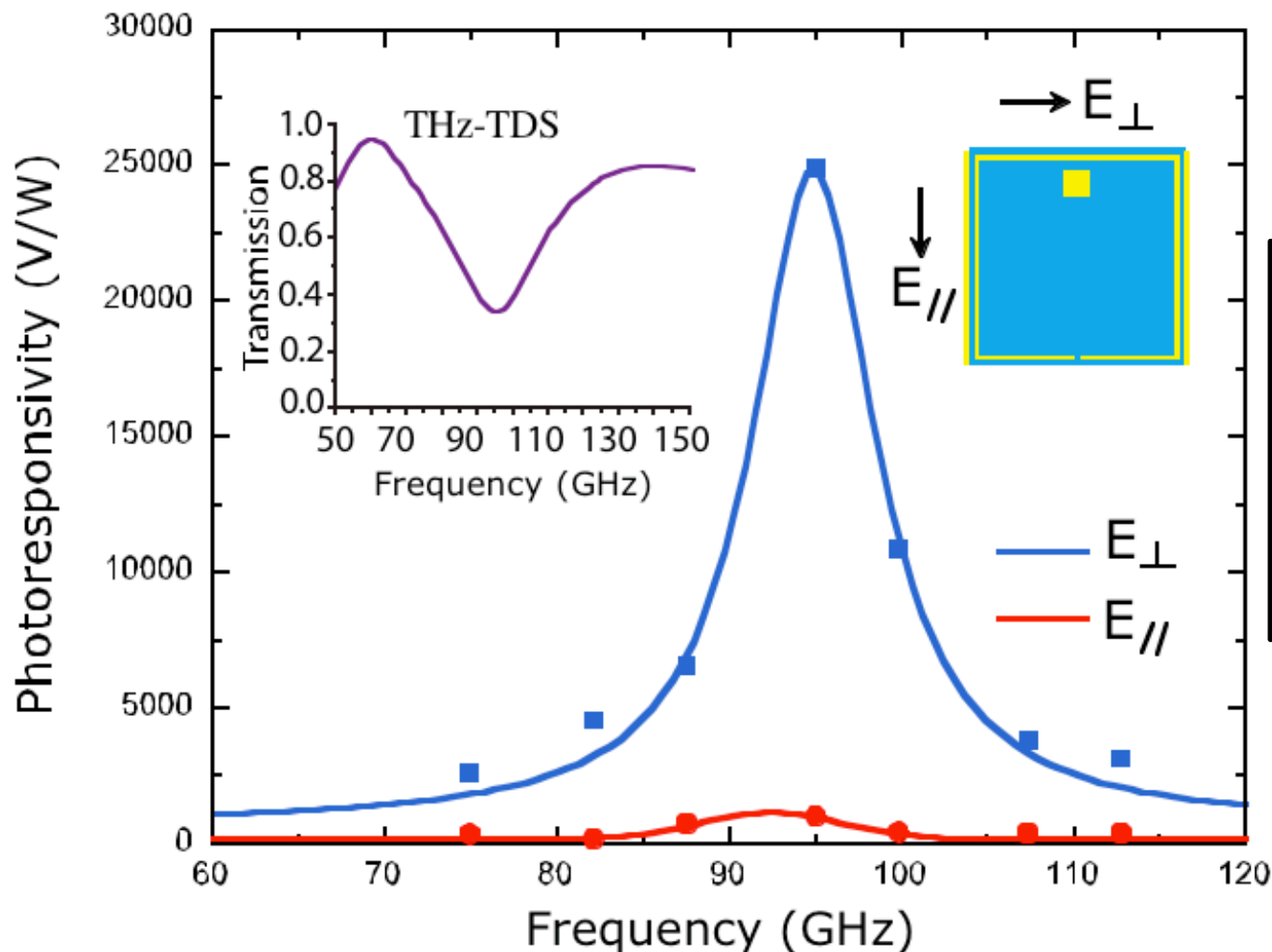
Optical Measurement Apparatus



Spectral Response of 95 GHz Detector

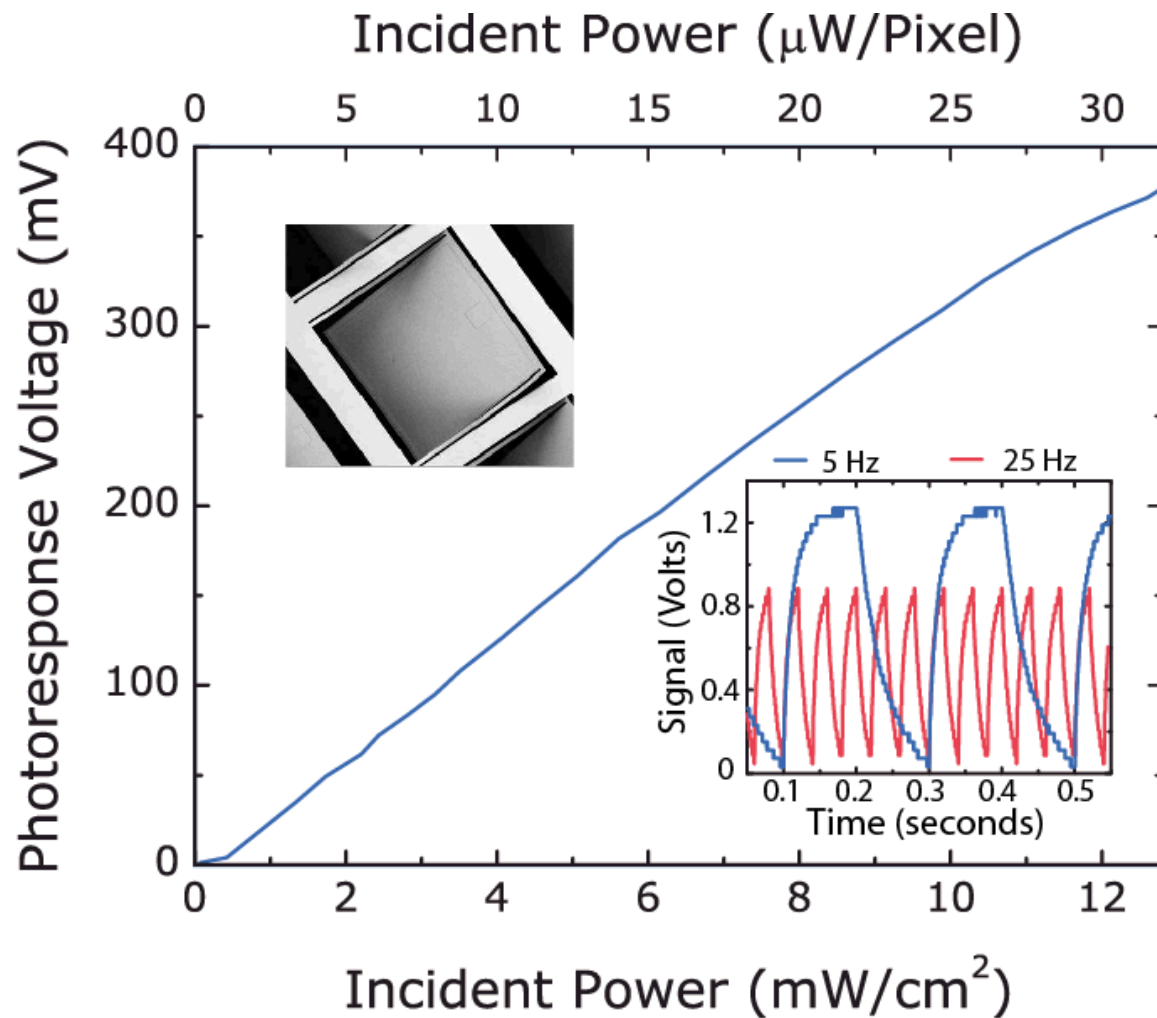


Lorentz Fit of Peak Power Points



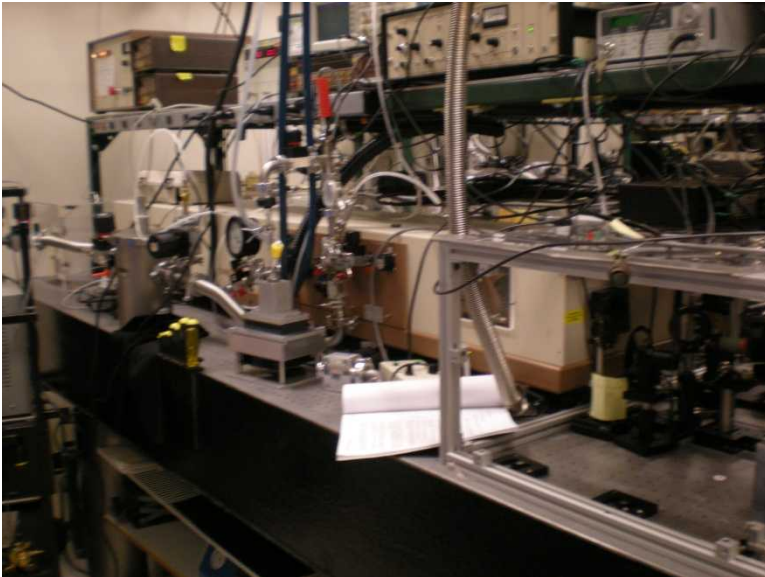
- Room T
- Ambient Pressure
- 15 Hz Chop Rate
- Lorentz fit matches TDS measurement (insert)

95 GHz Response to Power Attenuation

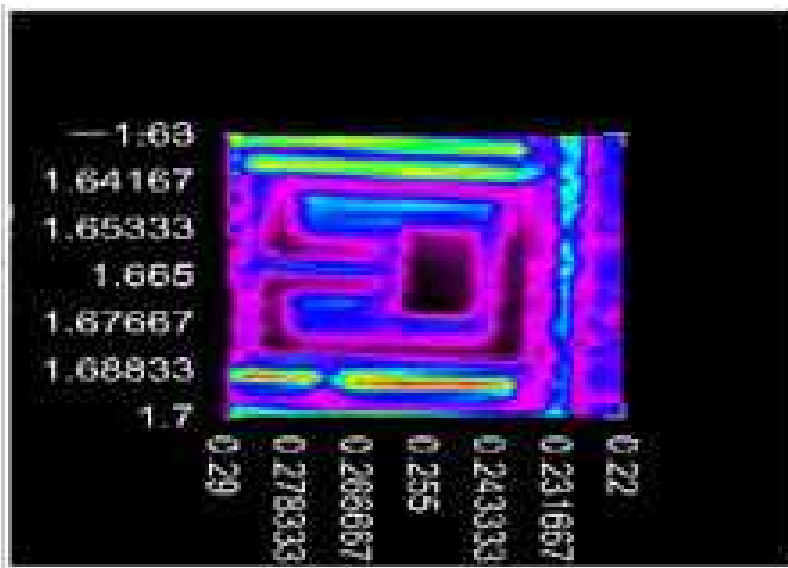


- Linear response with power
- $\tau \approx 10$ ms, sufficient for video rate applications

Characterization of 693 GHz Detector



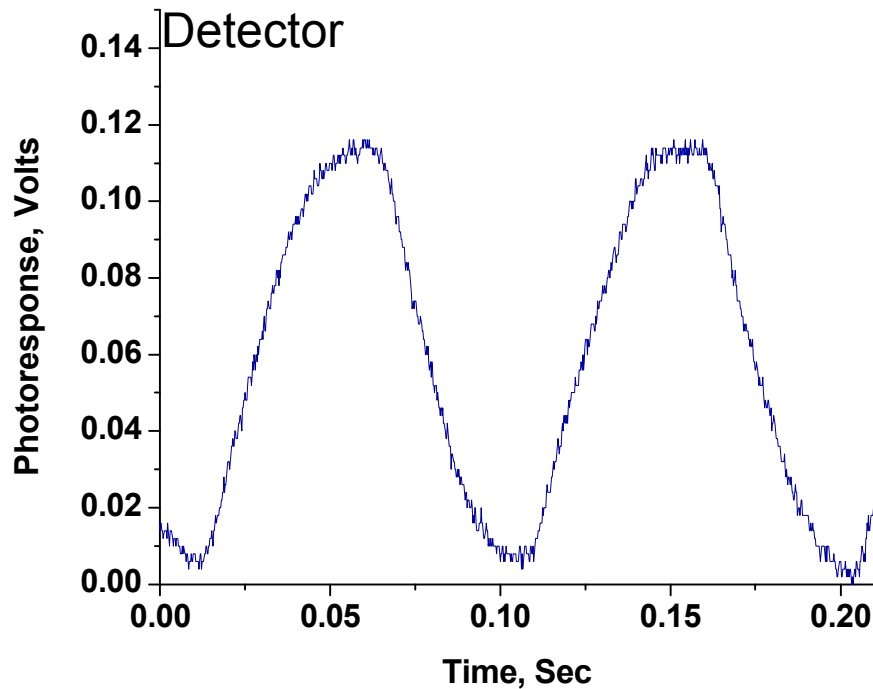
- Characterization done using a far infrared laser
- Formic acid line pumped with CO₂
- High power but not tunable



- Beam alignment done using labview
- Raster scan of detector measuring transmission of measurement beam

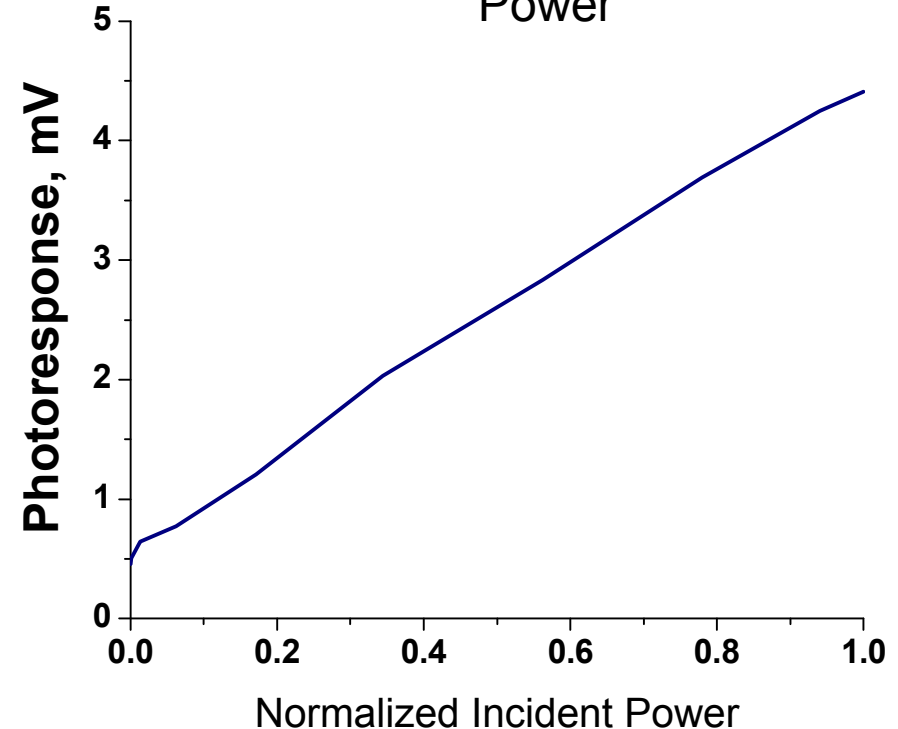
693 GHz Detector - Characterization

Temporal Response of 693 GHz
Detector



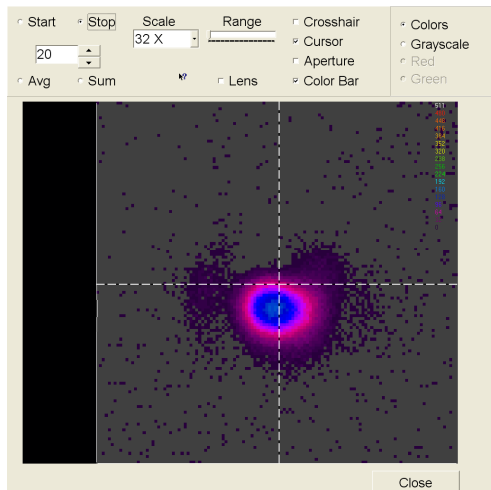
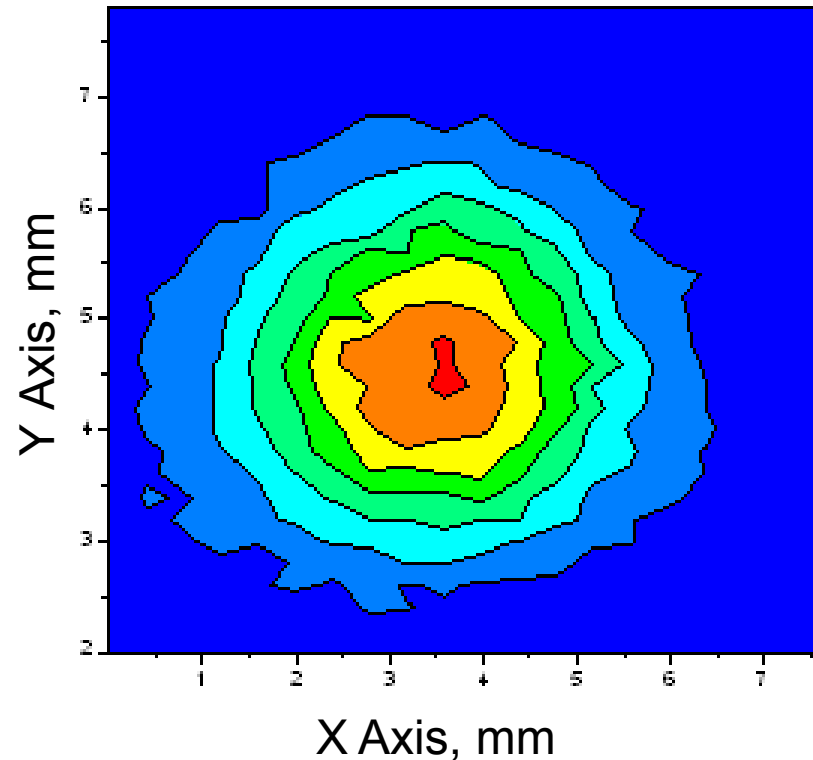
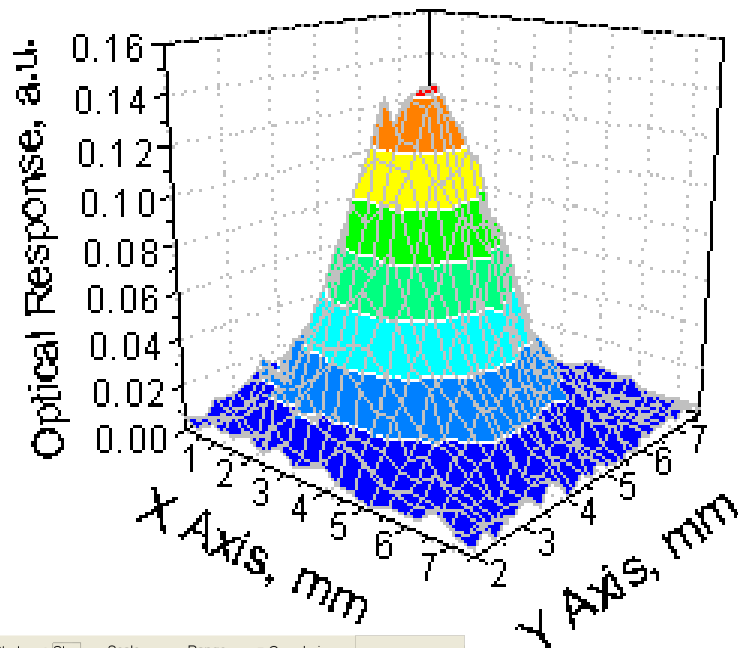
$NEP = 2.96 \times 10^{-8} \text{ W}/\sqrt{\text{Hz}}$
 $\tau = 20 \text{ ms}$
Sufficient for video rate
applications

Response of 693 GHz Detector Variabl
Power



Detector response linear with
respect to incident power

693 GHz Detector - Beam Image of FIRL

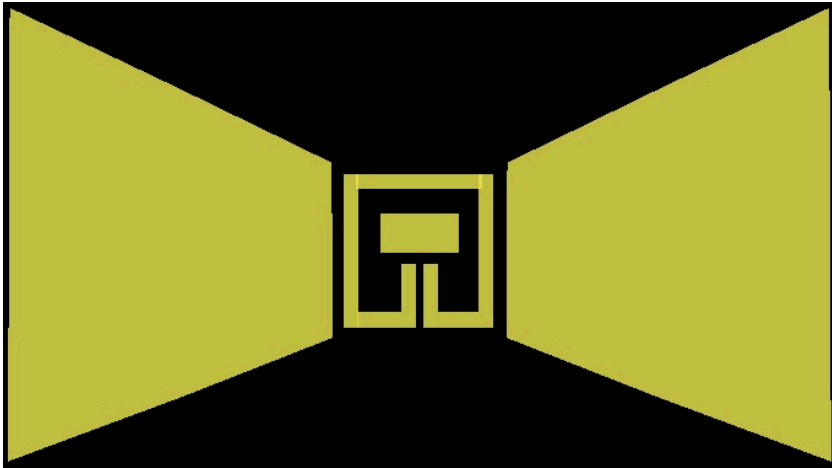


Beam profile
matches
Pyrocam
image

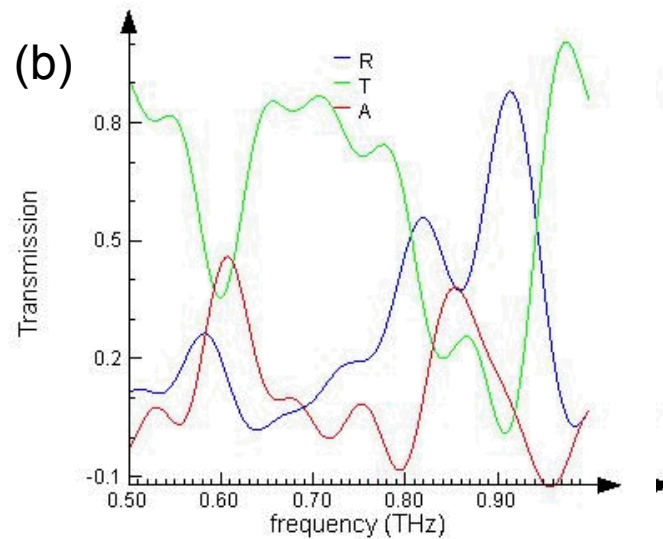
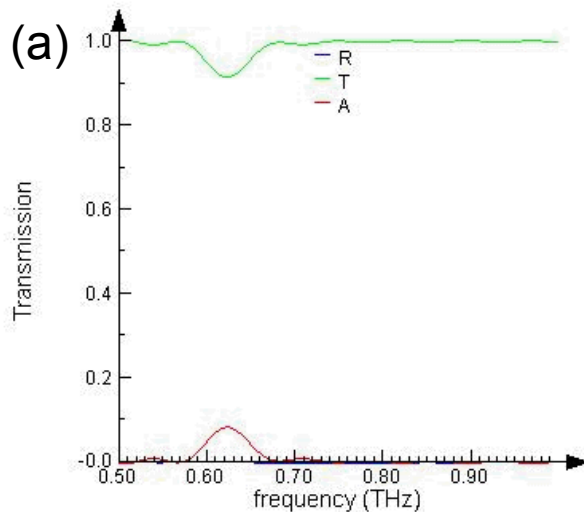
Beam profile taken by performing a
raster scan of the FIRL beam

- The 95 GHz and 693 GHz detectors can be used in beam diagnostics

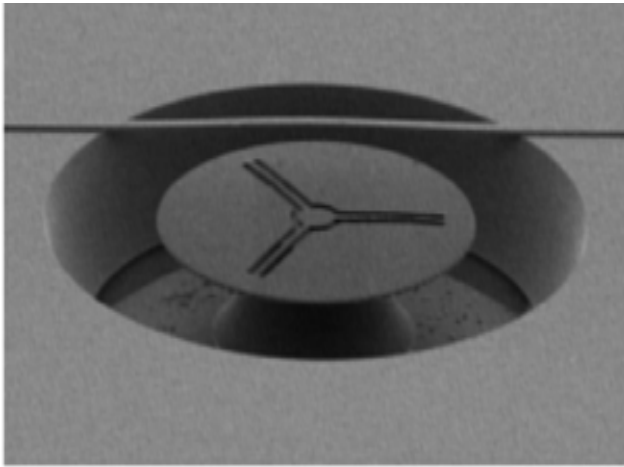
Future Work – Dipole coupled SRR



- SRR size $\sim \lambda/10$
- Far below diffraction limit
- Dipole Antenna $\sim \lambda/2$
maintain fast thermal time constant



- (a) Absorption and transmission plot of single SRR with no dipole antenna
- (b) Plot of Absorption in SRR with dipole antenna

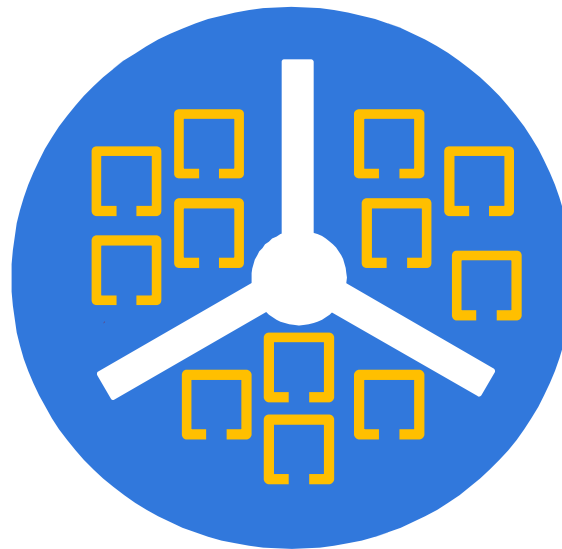


Thermal Micro Photonic Focal Plane Array (TMFPA)

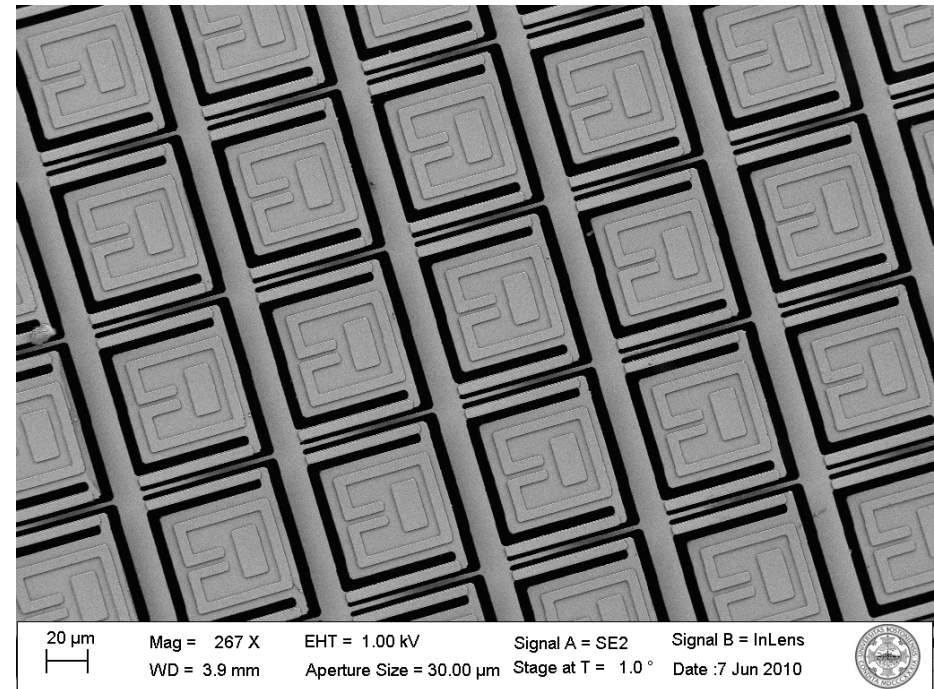
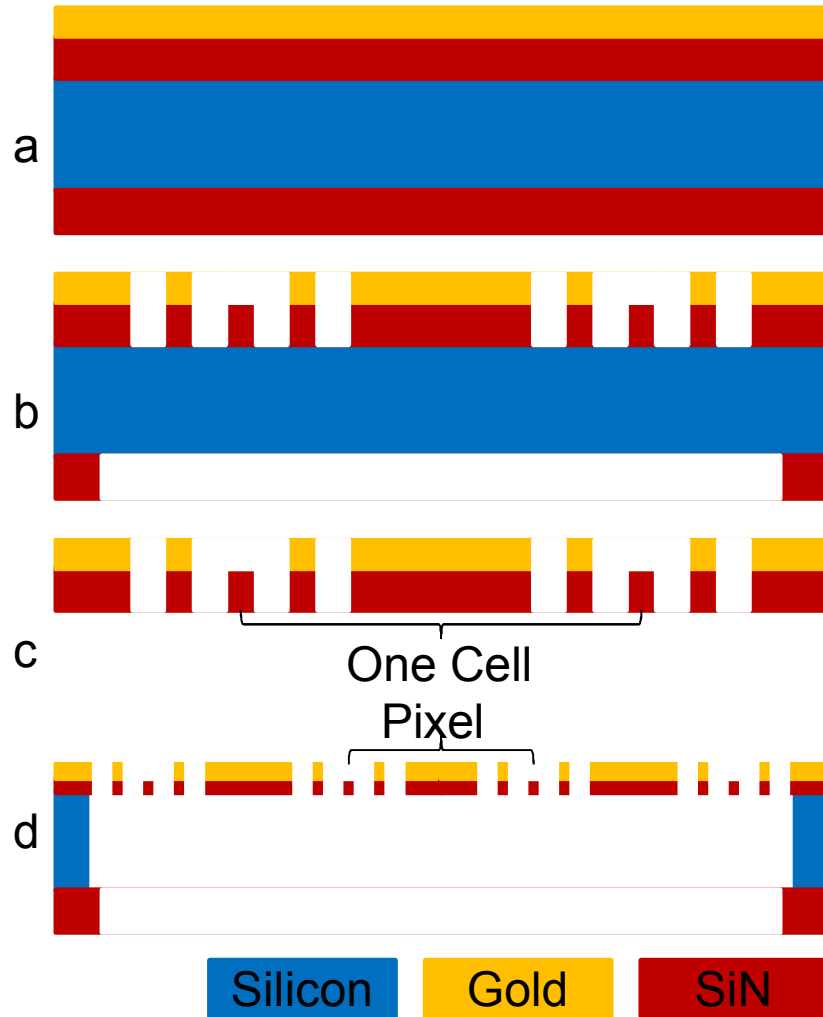
- $NEP = 7.15 \times 10^{-12} \text{ W/Hz}^{1/2}$
- $\tau = 2 \text{ ms}$
- $D = 2.47 \times 10^8 \text{ cmHz}^{1/2}/\text{W}$

Design layout combining silicon photonics and metamaterials

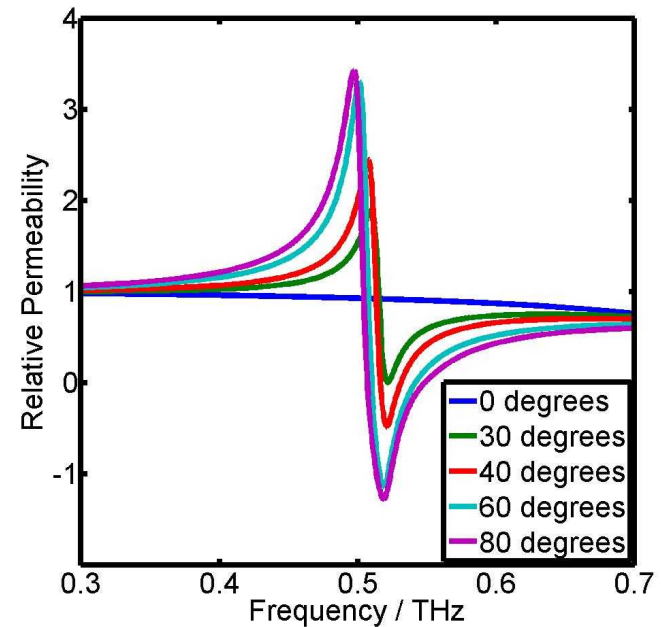
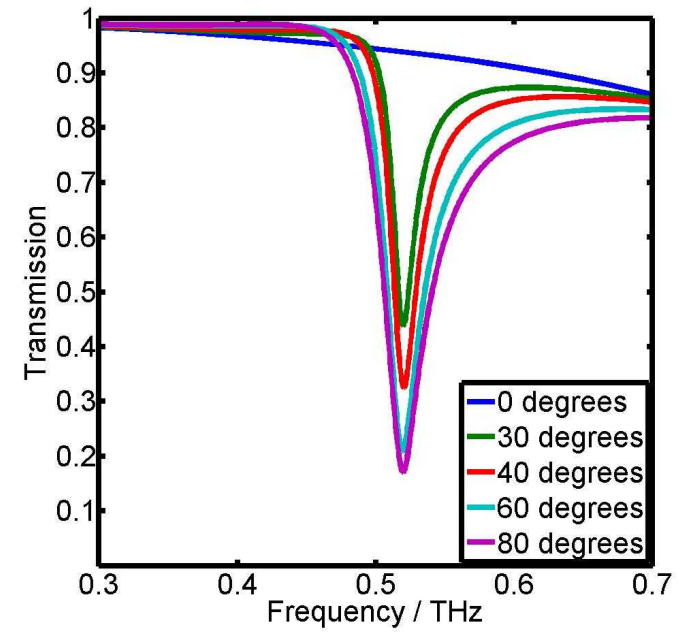
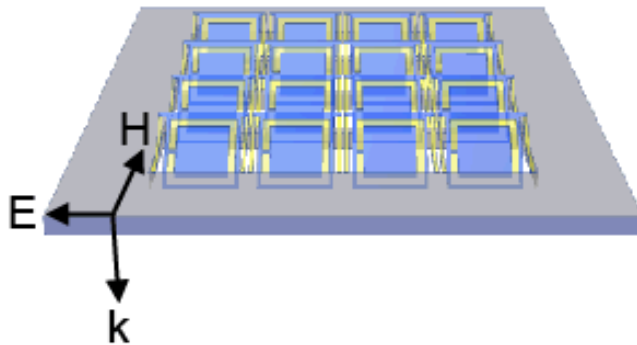
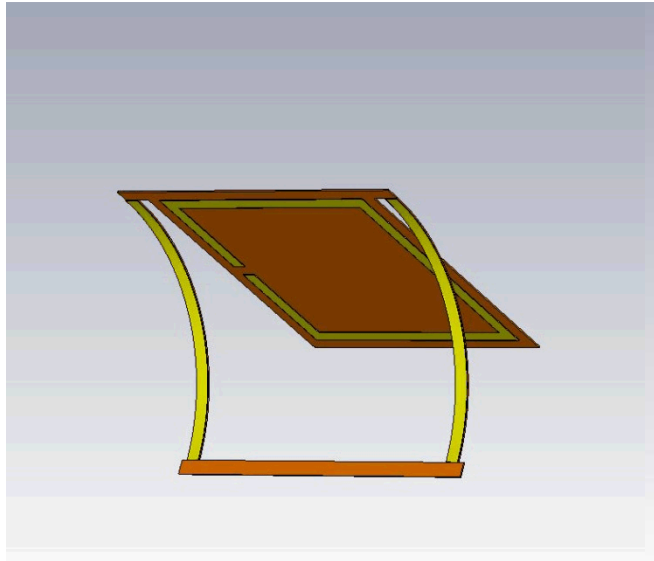
- Place SRRs onto microdisk resonator
- Enhance absorption in LWIR
- Extend detection into other regions (THz)



Cantilever Fabrication Process



Simulation of the Magnetic Response



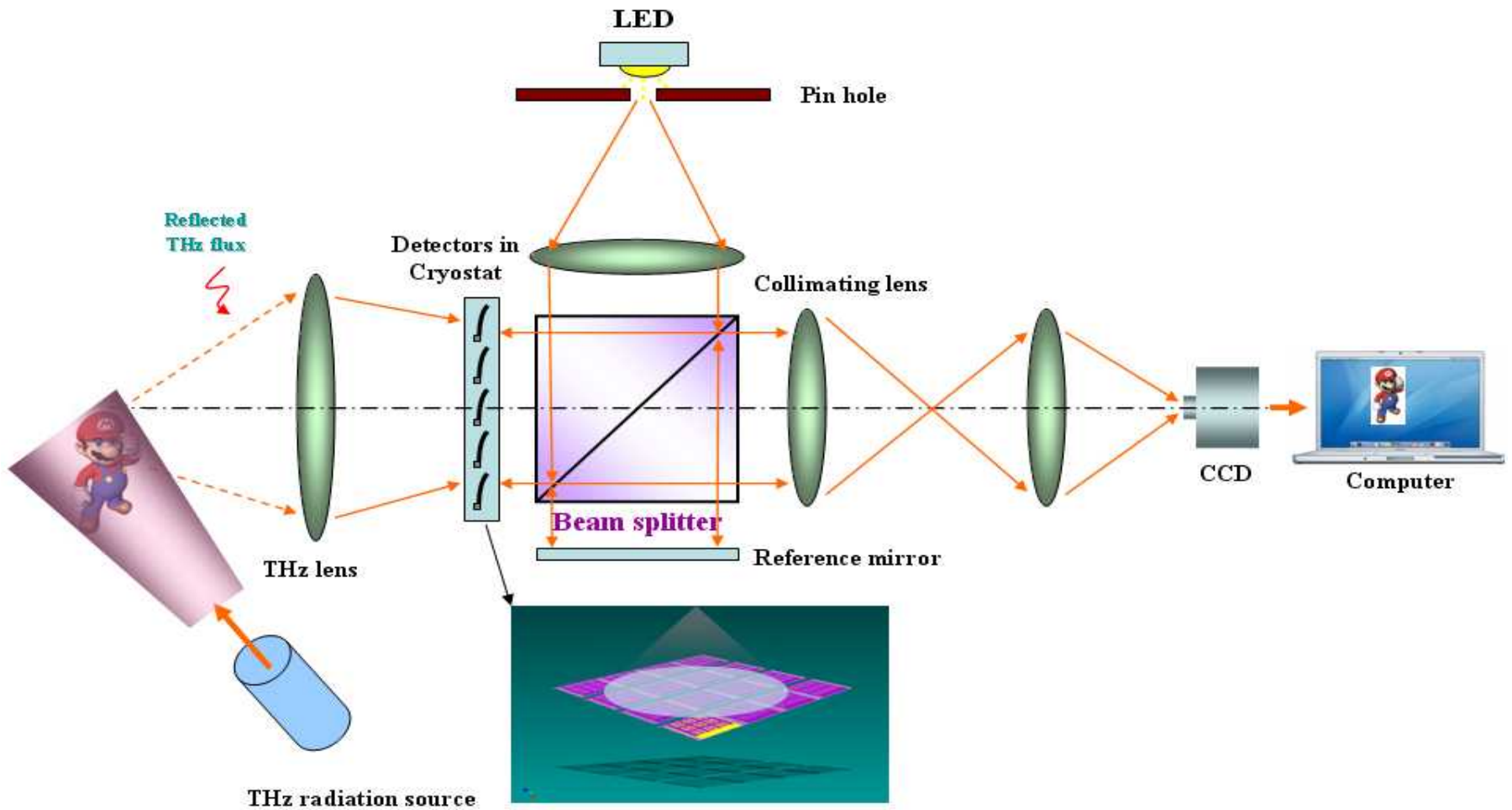
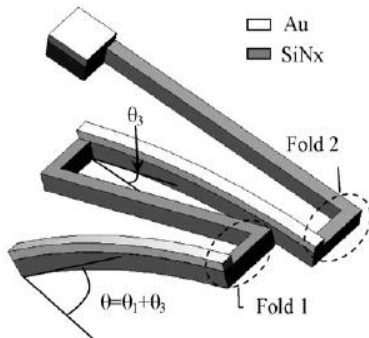


Table 1: Thermophysical properties of materials

	Young's modulus (GPa)	Poisson ratio	Expansion coefficient ($\times 10^{-6} \text{ K}^{-1}$)	Thermal conductivity (W/(m·K))	Heat Capacity (J/Kg·K)	Emissivity	Density (g/cm ³)
Au	73	0.42	14.2	296	132	0.01	19.30
SiN _x	180	0.26	3.2	5.5	333	0.8	2.44

Table 2: Dimension of microcantilever unit

Unit Size (μm)	Reflector (μm)	Leg length (μm)	Leg width (μm)	Au thickness (μm)	SiN _x thickness (μm)	Frame width (μm)	Fold number
200×200	180×25	180	2	0.4	0.55	10	2

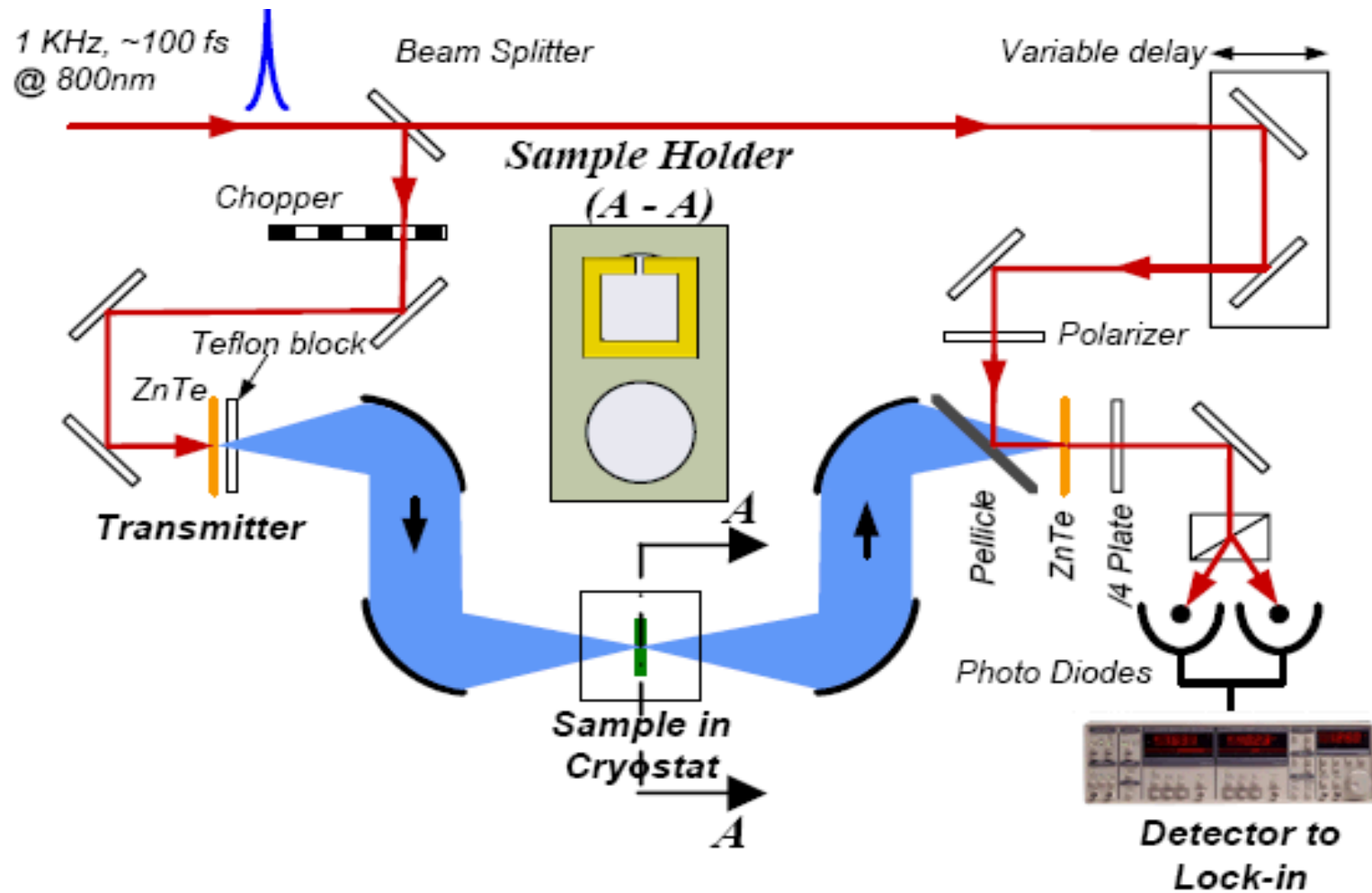


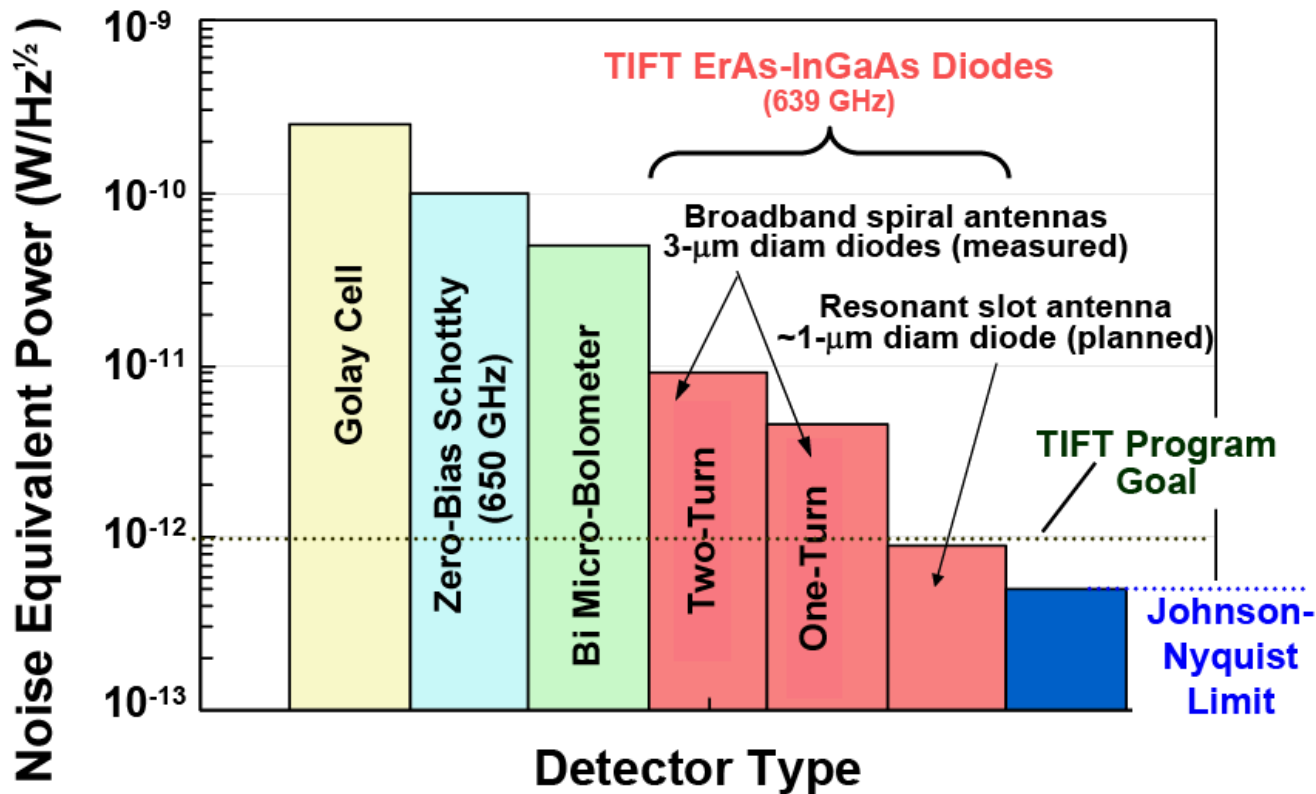
Thermal Analysis Yields

NETD: 10 mK

Limited by temperature stability

Experimental Setup: THz-TDS





We have an NEP of $\sim 10^{-10} \text{ W/Hz}^{1/2}$

Similar Responsivity at 640 GHz

We think we can easily obtain a factor of ten improvement by increasing the absorptivity and decreasing the thermal conductance