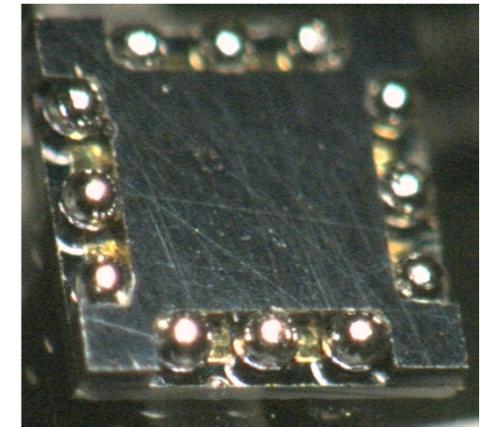
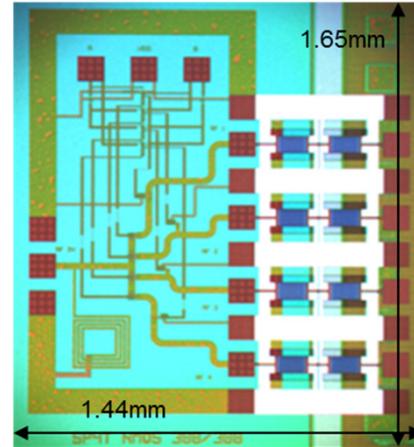
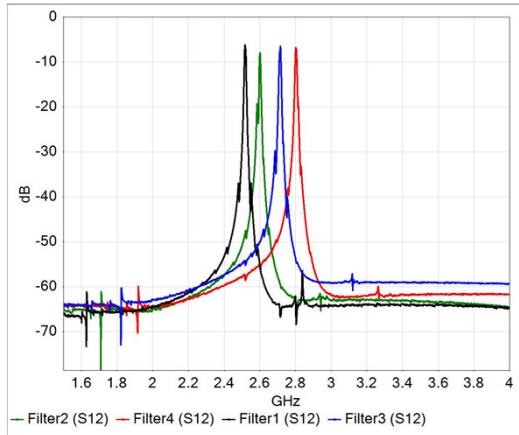


*Exceptional service in the national interest*



## TUNING THE BANDWIDTH AND CENTER FREQUENCY OF MICROMECHANICAL ACOUSTIC FILTERS

Roy H. Olsson III, Bongsang Kim, Janet Nguyen, Peggy Clews, Tammy Pluym and Kenneth E. Wojciechowski



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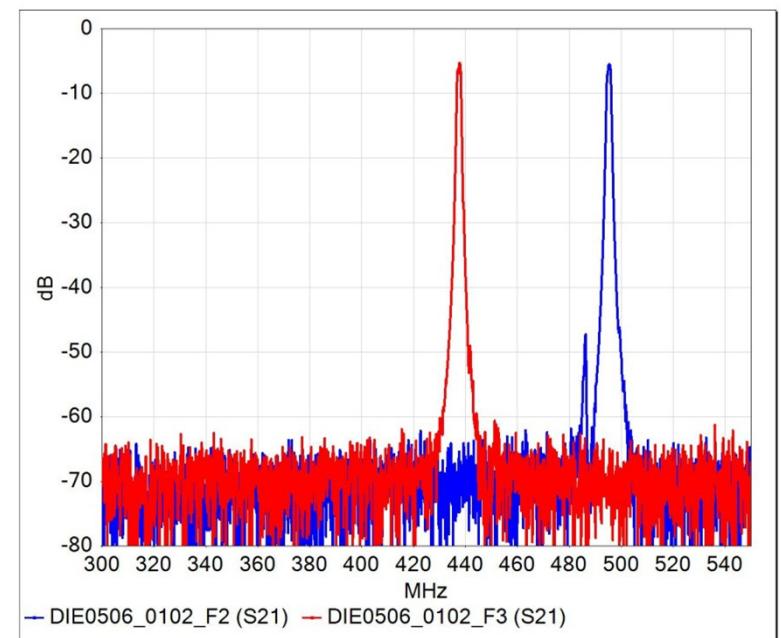
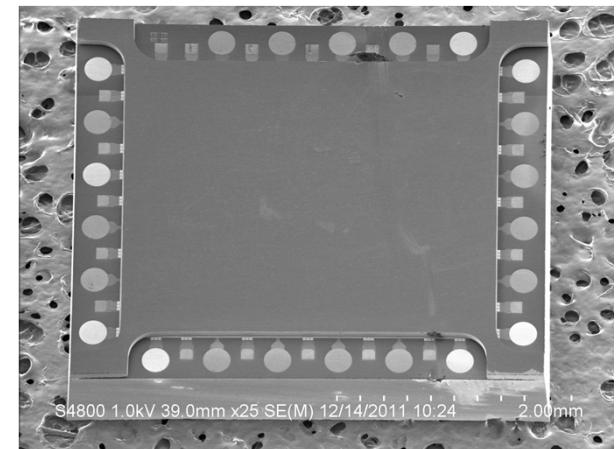
# Acoustic Micro-Scale Resonators



## Outline

- *Motivation*
- *Fundamentals*
  - $k_t^2$ -Q FOM
  - Material Based Tuning Limitations
- *Tuning of Acoustic Resonators*
  - Tuning Range
  - Tunable Filters
  - Active Tuning
- *New Materials and Impact on Performance*
  - Comparing Acoustic Resonators
  - High  $k_t^2$  Microresonators
  - Impact on Tuning

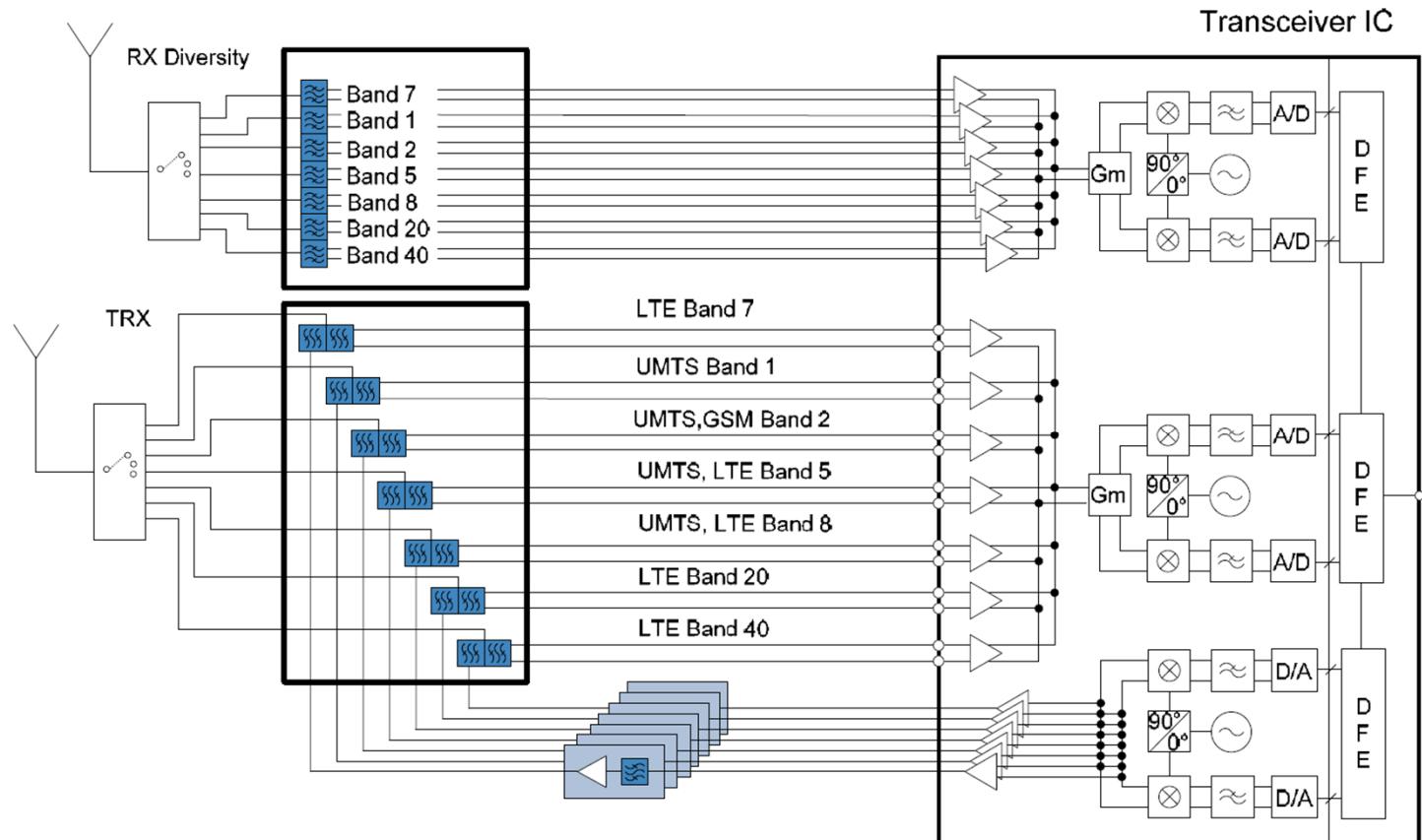
IF Filter Die  
Containing  
3 Filters



# Filter Arrays for Handsets

- Diagram Contains 28 Filters Operating in ~ 7 Bands
- Microresonator Technology Can Potentially Address Many of These Filters on a Single Chip, Reducing Size and Assembly Costs

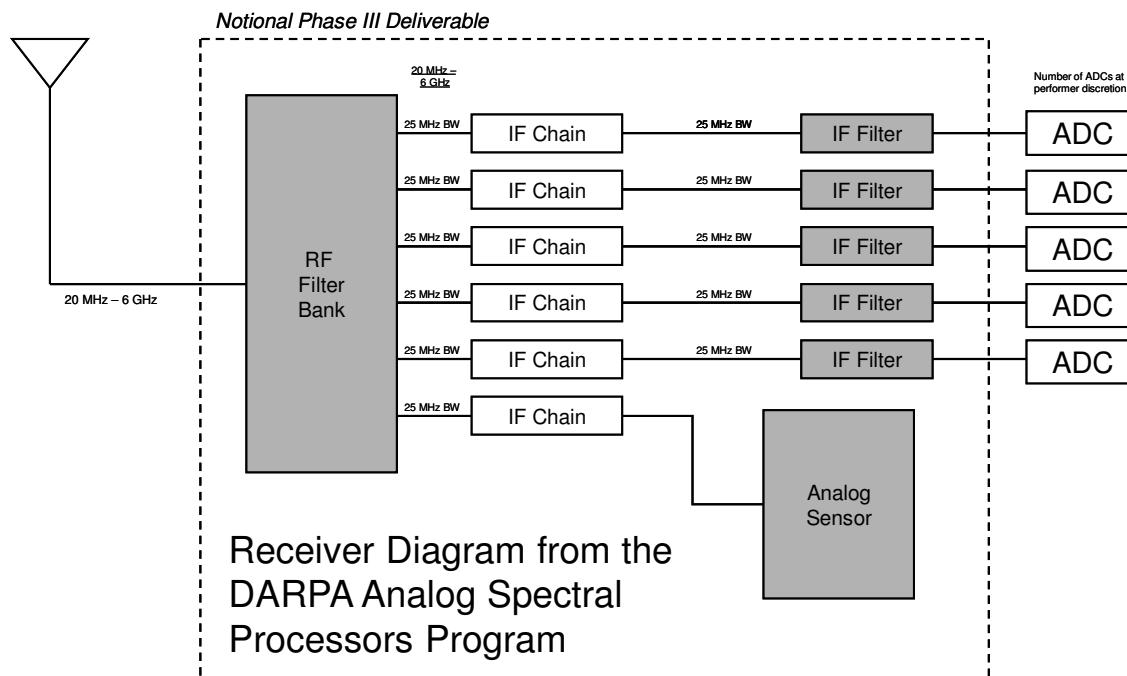
R. Vazny et al.  
“Front-End Implications to Multi-Standard Cellular Radios: State-of-the-Art and Future Trends”, *Proc. Of the 2010 IEEE Ultrasonics Symposium, pp. 95 – 98, Oct. 2010*



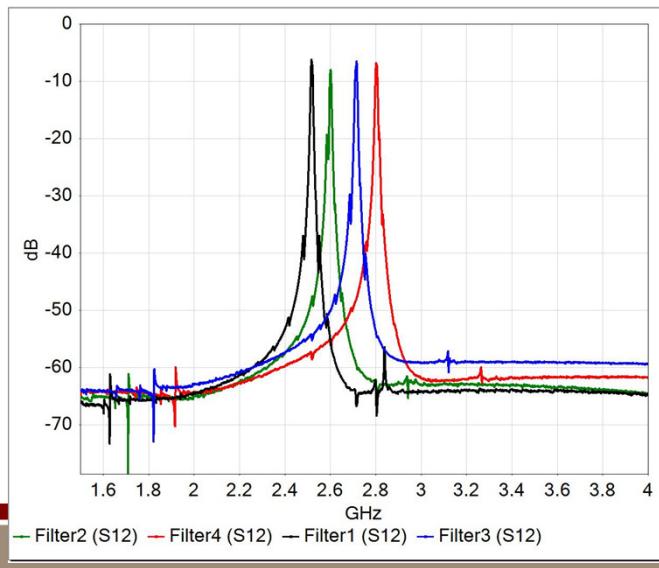
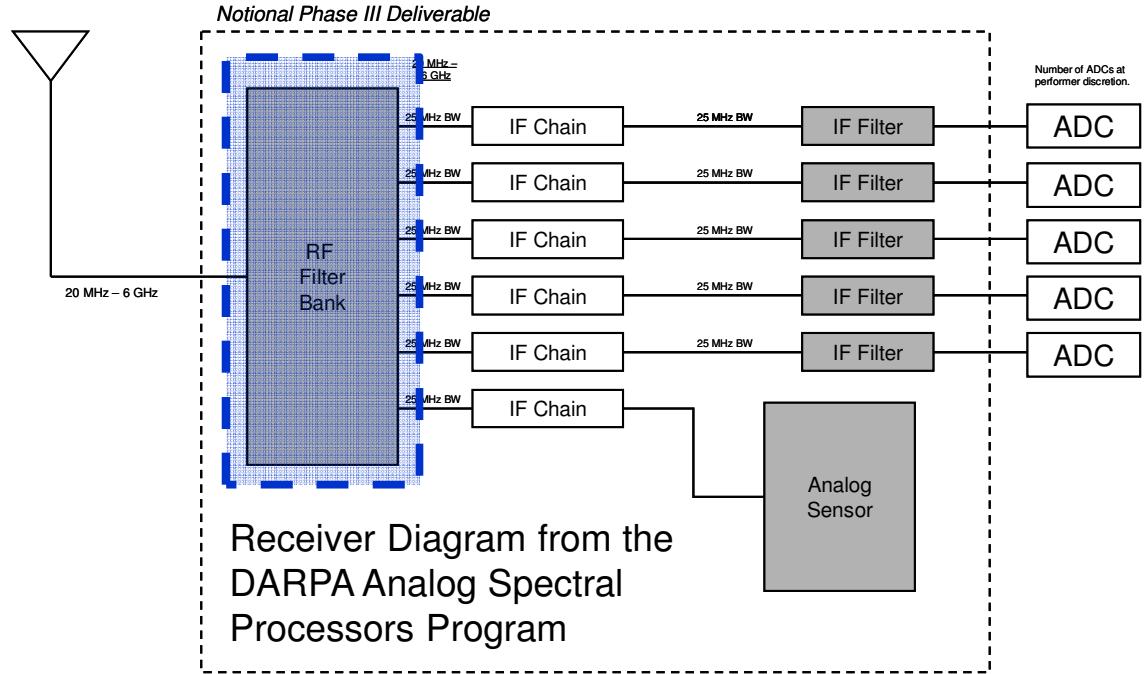
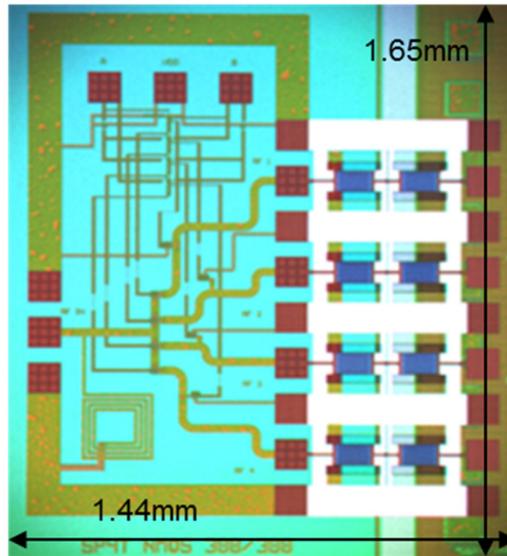
RF Front-End of a Modern Cellular Radio

# Filters in Military Radios

- Current Military Radios Are Mandated to be Backwards Compatible
  - *Legacy and Updated Frequencies and Waveforms*
    - *Many RF Frequencies and Bandwidths Required*
- Future Military Radios Will Require Spectral Knowledge and Real Time Adaptability to Mitigate Both Co-Site and Adversary Jamming

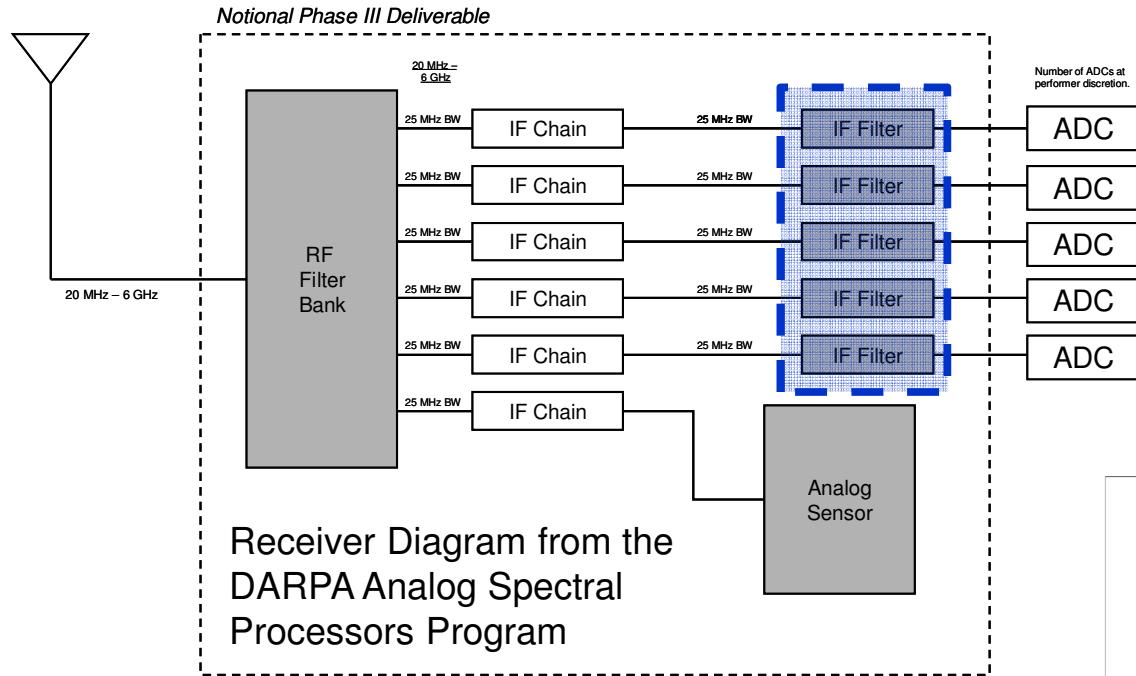


# Frequency Adaptability on the RF Front-End

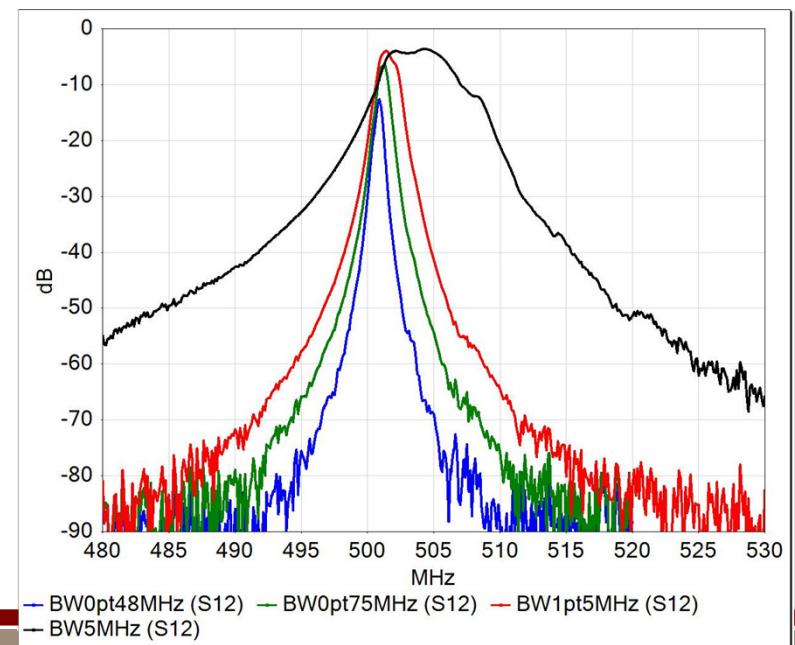
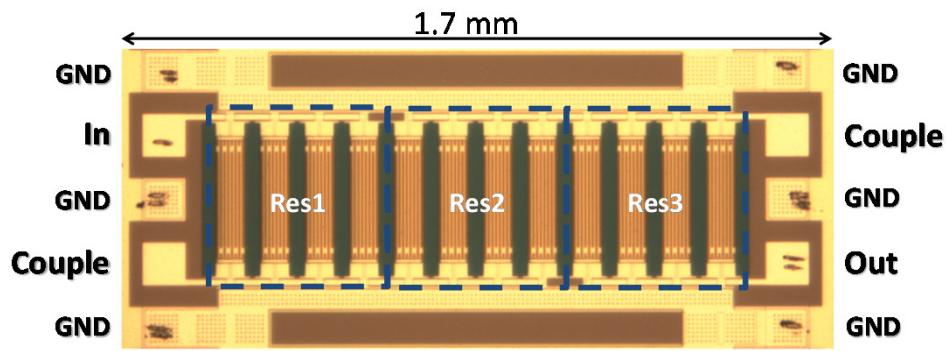


S-Band Switched Filter Array on CMOS for RF Center Frequency Adaptability

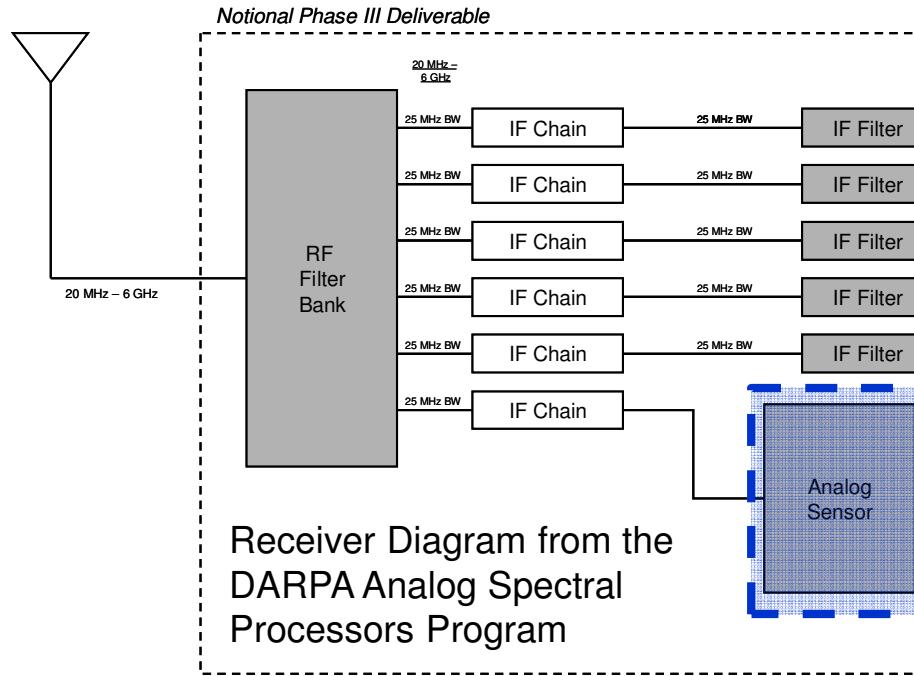
# Waveform and Bandwidth Adaptability IF Filtering



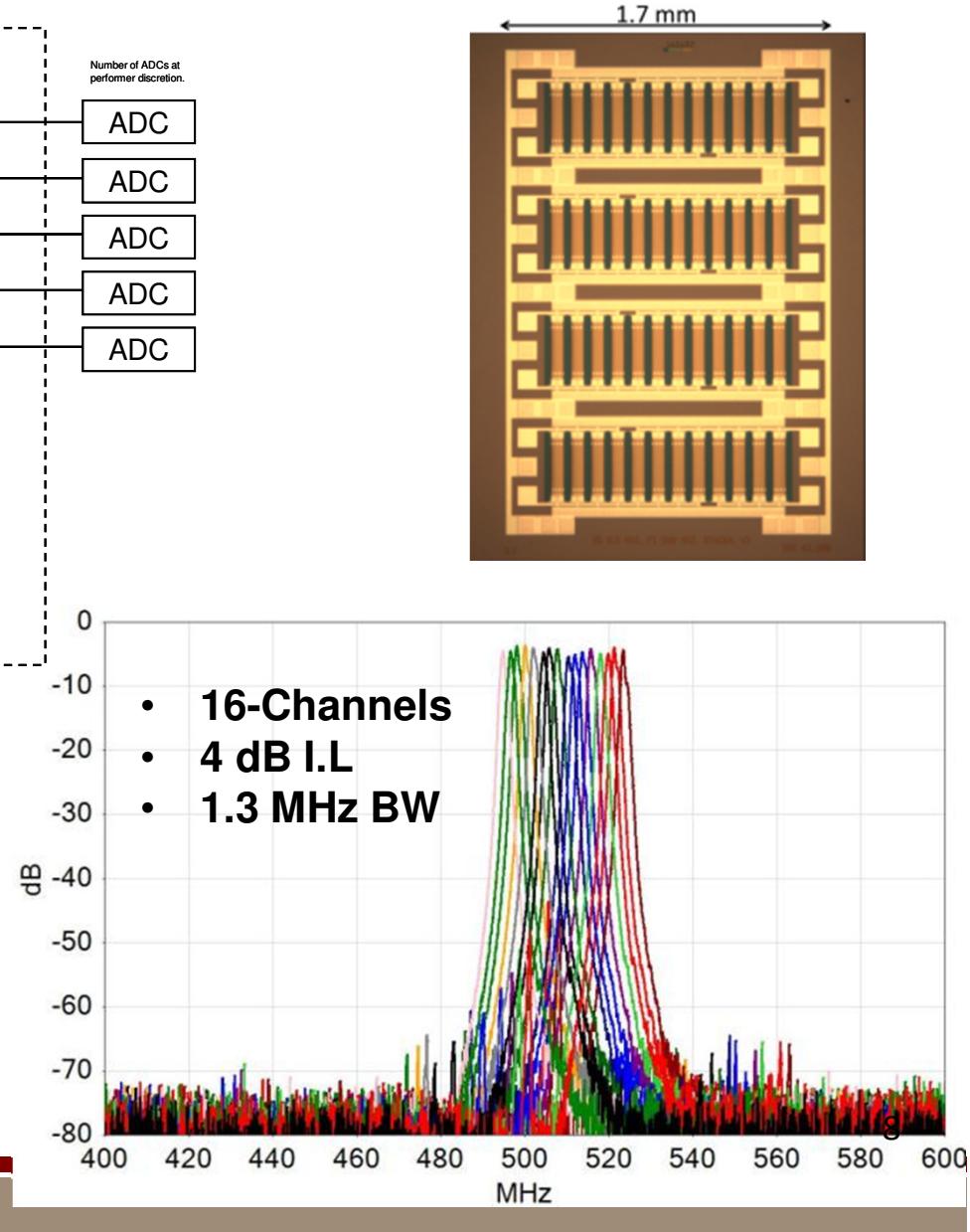
IF Filter with  
Programmable  
Bandwidth from 5.1  
MHz to 0.48 MHz



# RF Spectral Awareness

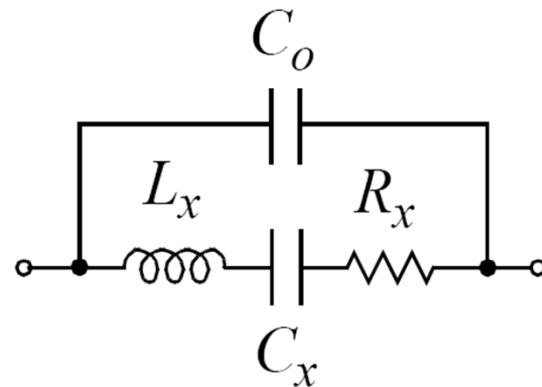
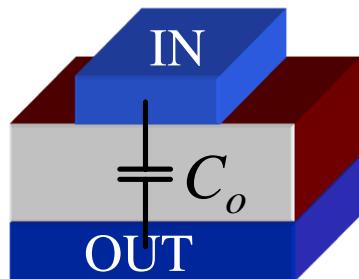


16-Channel Filter Array for RF Spectral Sensing



# Piezoelectric Resonator Transduction

## Top-Bottom Transduction



$$C_x = 0.8k_t^2 C_0$$

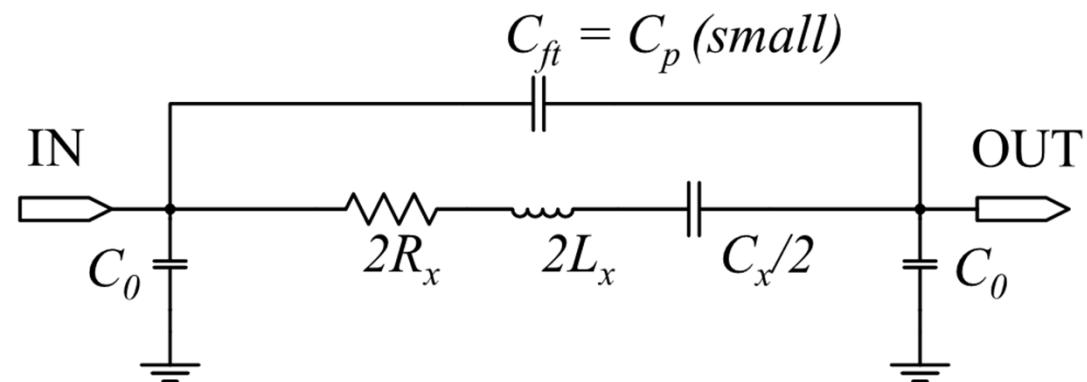
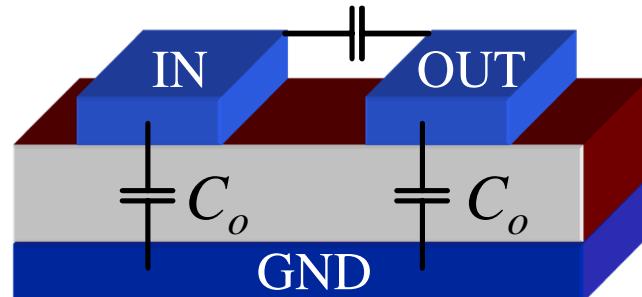
$$L_x = \frac{1}{0.8\omega^2 k_t^2 C_0}$$

$$R_x = \frac{1}{0.8\omega C_0 k_t^2 Q}$$

$$k_t^2 = \frac{d_{31}^2 E}{\epsilon}$$

$$FOM = k_t^2 Q$$

## Top-Top Transduction



■ Top electrode

■ Bottom electrode

■ Piezoelectric Film (AlN)

# Piezoelectric Resonator Transduction



## ➤ Loss

- Proportional to FOM
- $R_x$  Set by FOM, Frequency,  $C_0$  (Area)

$$C_x = 0.8k_t^2 C_0$$

## ➤ Tuning

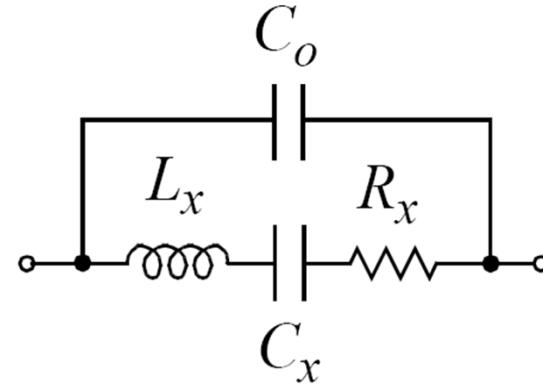
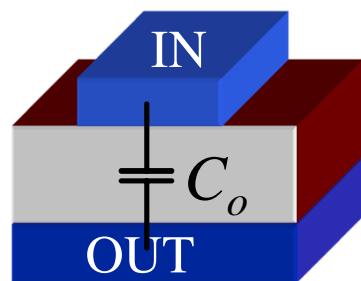
- Maximum Tuning Range is Determined by  $k_t^2$

$$L_x = \frac{1}{0.8\omega^2 k_t^2 C_0}$$

## ➤ Bandwidth

- Minimum Practical Filter Bandwidth is Determined by  $Q$
- Maximum Practical Filter Bandwidth is Determined by  $k_t^2$

$$R_x = \frac{1}{0.8\omega C_0 k_t^2 Q}$$



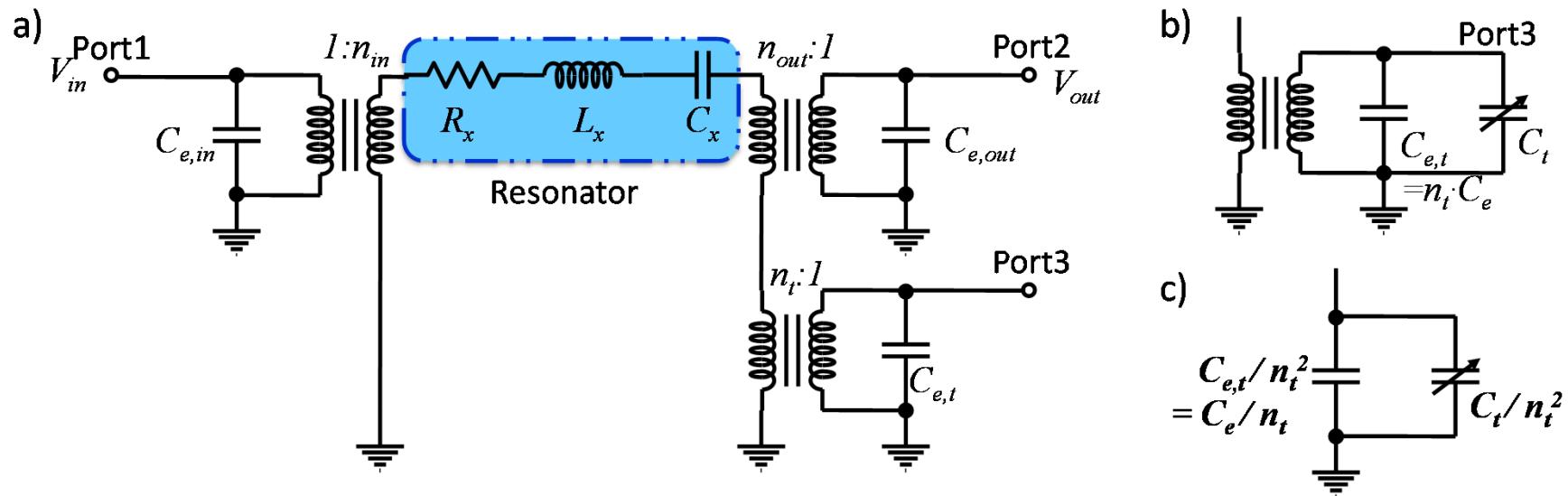
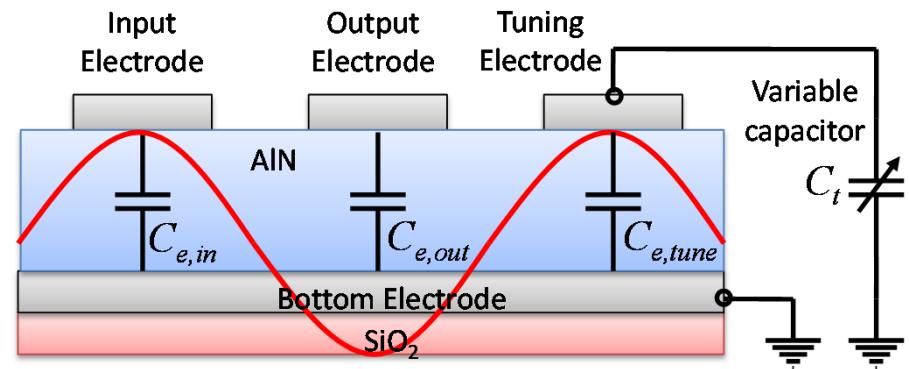
$$k_t^2 = \frac{d_{31}^2 E}{\epsilon}$$

$$FOM = k_t^2 Q$$

# $k_t^2$ Limits the Tuning Range



3-Port Tunable Micromechanical Resonator Cross-Section



3-Port Tunable Micromechanical Resonator Equivalent Circuit Model

# $k_t^2$ Limits the Tuning Range

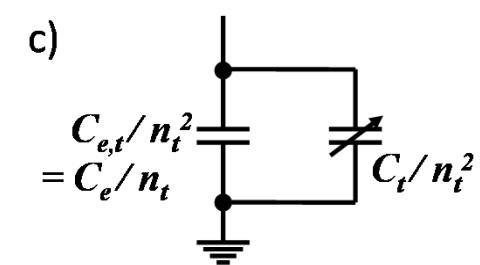
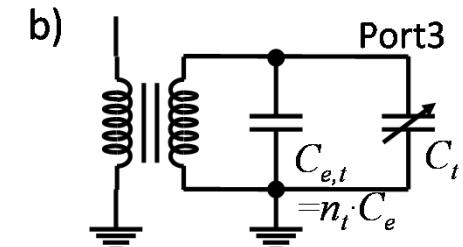
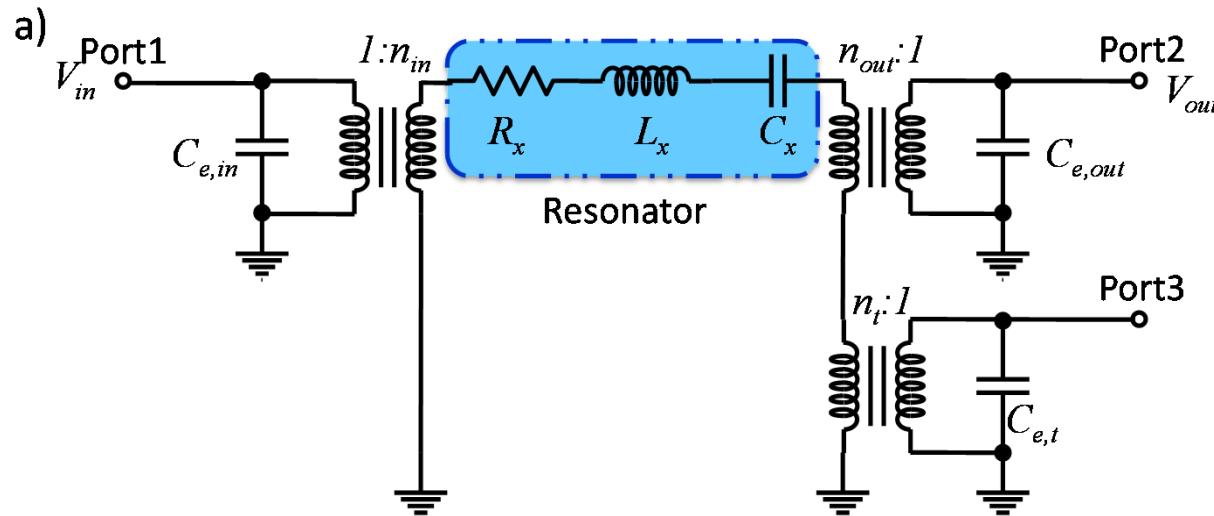
$$\frac{1}{C_x} = \frac{1}{C_x} + \frac{n_t^2}{n_t C_e + C_t}$$

$$f' = \frac{1}{2\pi} \sqrt{\frac{1}{L_x C_x}} = \frac{1}{2\pi} \sqrt{\frac{1}{L_x} \left( \frac{1}{C_x} + \frac{n_t^2}{n_t C_e + C_t} \right)}$$

$$\frac{\Delta f}{f} = \frac{1}{2} \frac{n_t^2 \cdot C_x}{n_t C_e + C_t}$$

$$0 < \frac{\Delta f}{f} < \frac{n_t}{2} \frac{C_x}{C_e}$$

$$\frac{C_x}{C_e} = \frac{8}{\pi^2} k_t^2$$

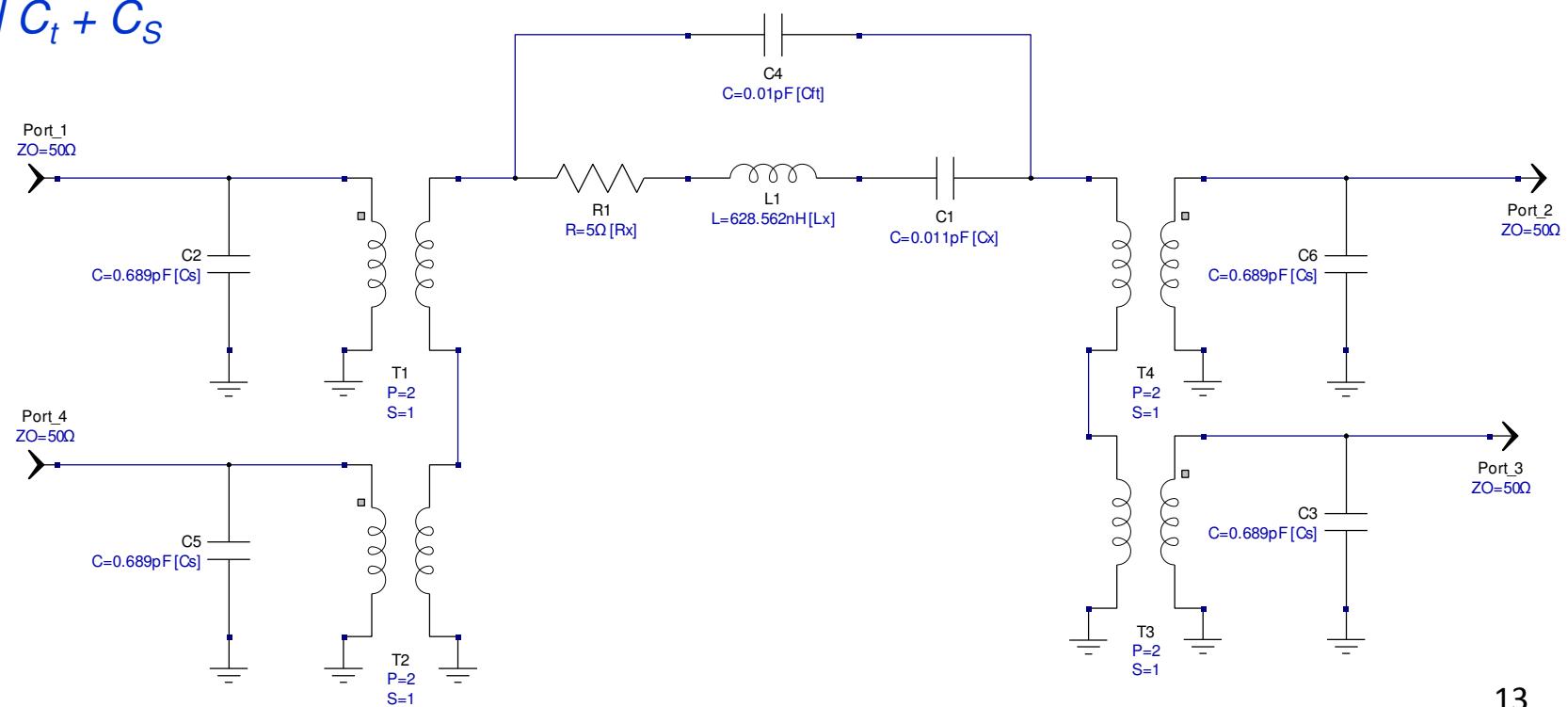
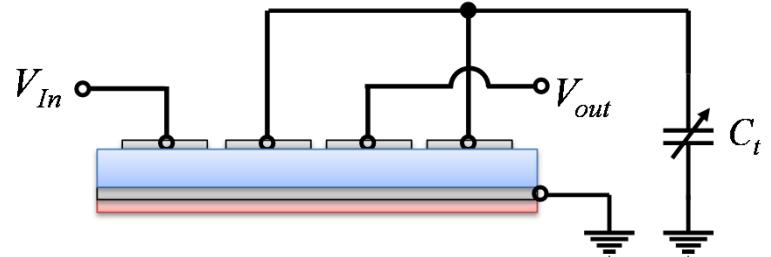


# Multi-Port Resonators for Tuning



- *½ of Electrodes Used for Filtering*
- *½ of Electrodes Used for Tuning*
- *Tuning Range Limited by  $C_X/C_S$  or  $k_t^2$*
- *Feedback Signal on  $C_t$  is 90 deg. Out of Phase with the Input and is Maximized for Small  $C_t + C_S$*

a) **Configuration A**



# AlN Microresonator Tuning



## ➤ AlN Microresonator

- $k_t^2 = 2\%$
- $Q = 1500$
- $R_X = 5 \Omega$
- Tuning Range = 0.4%

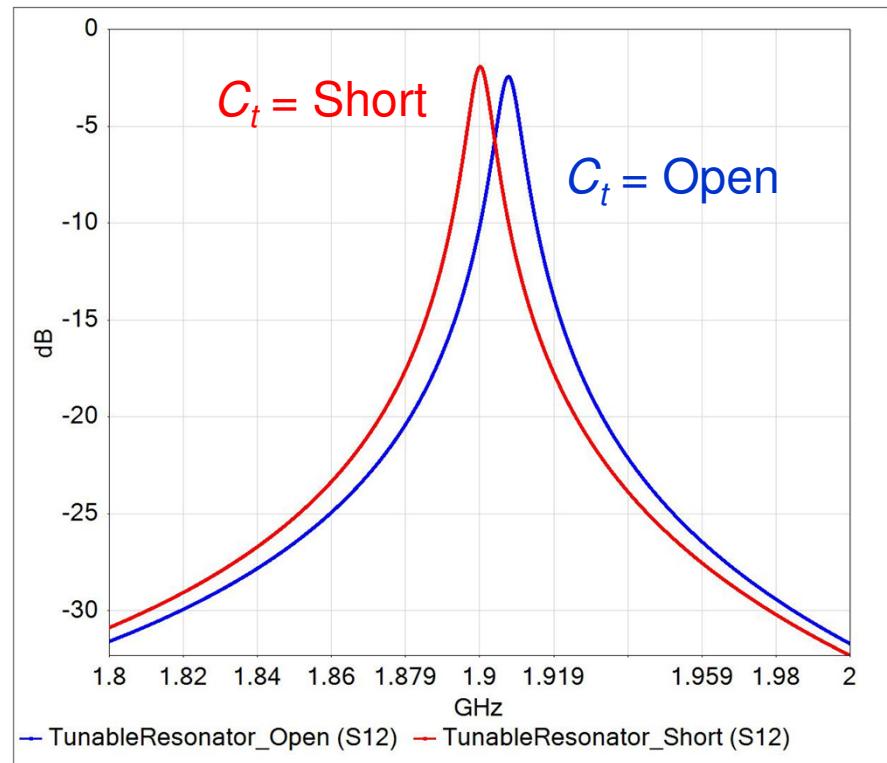
## ➤ Using $\frac{1}{2}$ of the $k_t^2$ for Bandwidth and $\frac{1}{2}$ for Tuning

## ➤ $C_t$ Varied From Open to Short

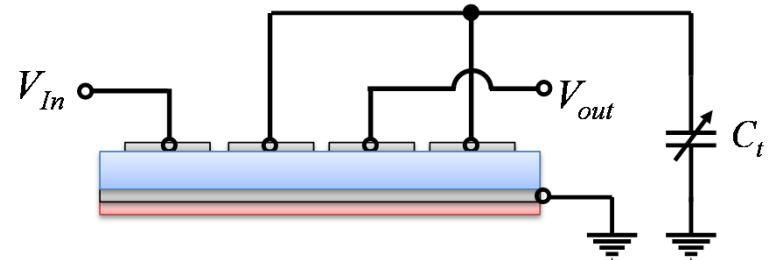
## ➤ Additional 0.5 dB Loss is From the Finite Q of the Electrode Capacitors

## ➤ As We Tune Away From the Acoustic Resonance

- More Energy Stored in the Capacitors
- Higher Capacitor Q Required
- Trade Off Between Acoustic and Capacitor Q With Metal Thickness



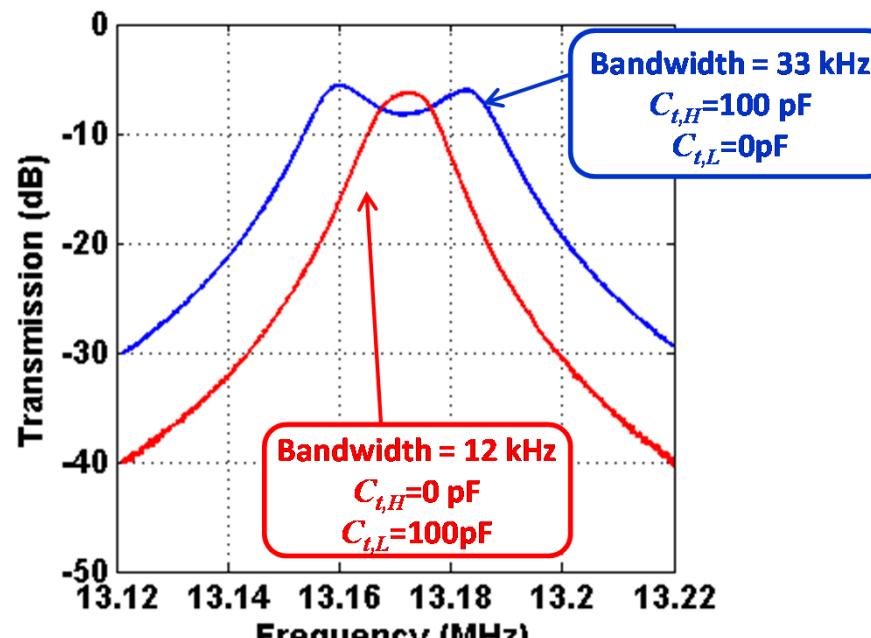
a) **Configuration A**



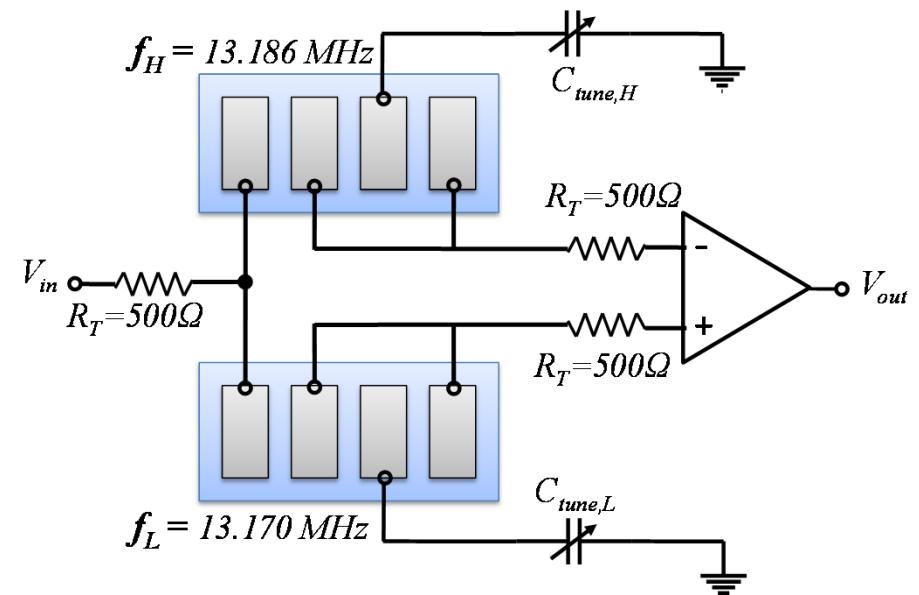
# Tunable Bandwidth Lattice Filter



- Achieved  $\sim 3x$ , 3 dB Bandwidth Tuning Range
- Parallel Lattice Filter Architecture
- Resonator Tuning Range Limited to  $< k_t^2/2$

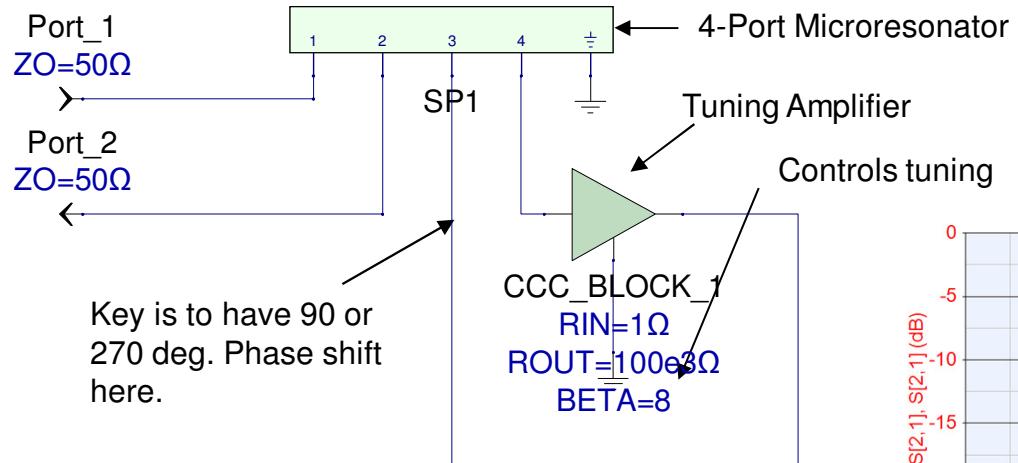


Tunable Bandwidth Filter Response



Tunable Bandwidth Filter Schematic

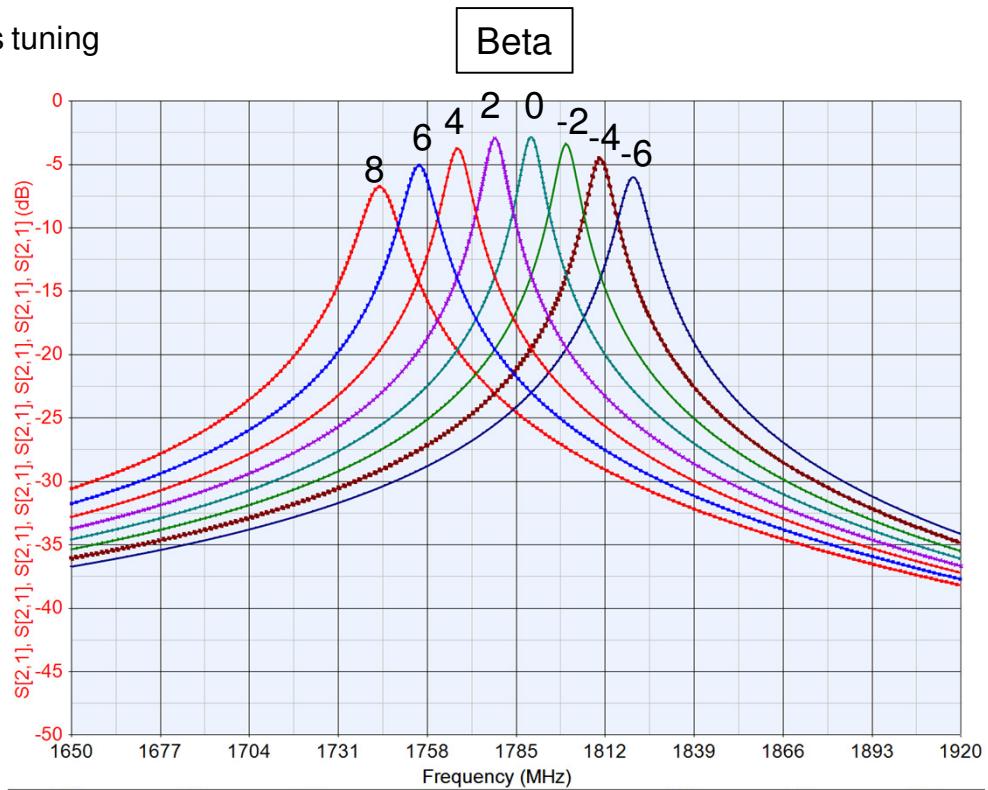
# Active Resonator Tuning



Initial Tuning Schematic

## ➤ Active Tuning

- AlN Microresonator with a  $k_t^2$  of 1.5%
- RF filters can be tuned >7.0%
- Passive Tuning was 0.3%
- Can be implemented in several ways using existing transistors
- Requires realistic current gains of 8



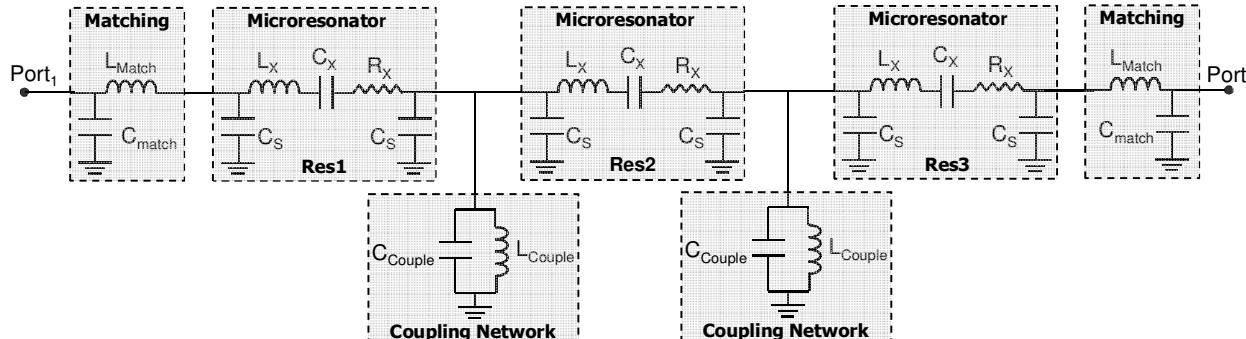
Utilizing Active Gain to Extend the Tuning Range of Microresonators

# Programmable Bandwidth Filter

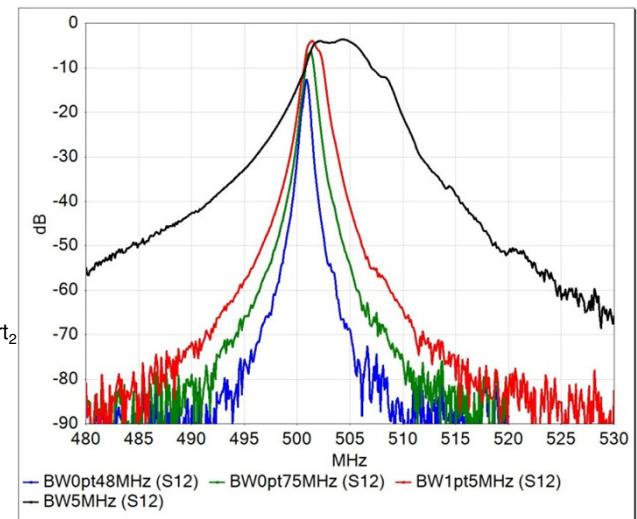
➤ Alters Resonator Coupling by Tunable Coupling Networks

➤ Over 10x Bandwidth Programmability Using COTs Passives with  $Q = 50$

➤ Working to Integrate Switched Coupling and Matching Capacitors Under Resonator to Enable Tunable Bandwidth



Programmable Bandwidth Filter Schematic



Programmable Bandwidth Filter  
Measured Response

3 dB Bandwidth (MHz)	Insertion Loss (dB)	Stop Band Rejection (dB)	$L_{couple}$ (nH)	$C_{couple}$ (pF)	$L_{match}$ (nH)	$C_{match}$ (pF)
0.475	12.6	75	0	14	11	6
0.75	6.3	80	0	5	0	0
1.5	4.0	80	0	0	0	0
5.1	3.6	76	22	0	37	0

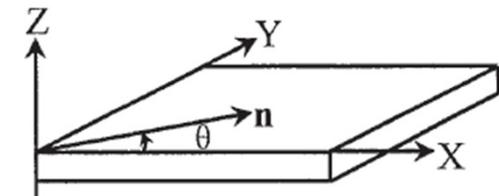
# Increasing the Tuning Range

# Types of Acoustic Resonators

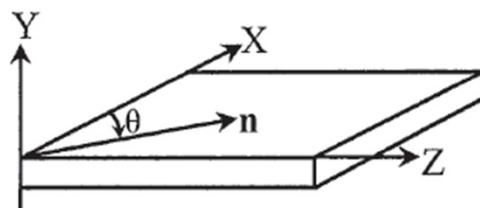


Technology/ Metric	$k_t^2$ theory	$k_t^2$ experiment	Q @ ~ 1 GHz	FOM	Multiple Frequencies on a Substrate
AlN BAW/FBAR	6.5%	7%	3000	~200	High Cost
Standard LiNbO <sub>3</sub> SAW	5.5%	5.5%	2000	~100	Yes
AlN Microresonator	2%	2%	2000	~40	Yes
Capacitive Microresonator	~Gap, Bias	< 0.1%	10,000	<1	Yes
Advanced SAW	> 20%	20%	2000	~400	Limited
PZT/BST BAW	7-12%	7-12%	60-250	~7-18	High Cost
Doped AlN BAW	15%	12%	< Undoped	TBD	High Cost
LiNbO <sub>3</sub> Microresonator	> 30%	20%	1200	TBD	Yes

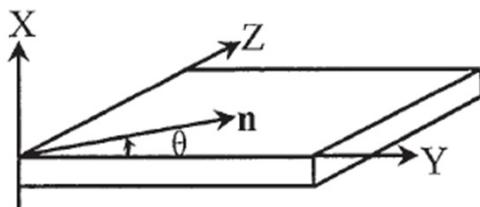
# $\text{LiNbO}_3$ S0 Mode Microresonators



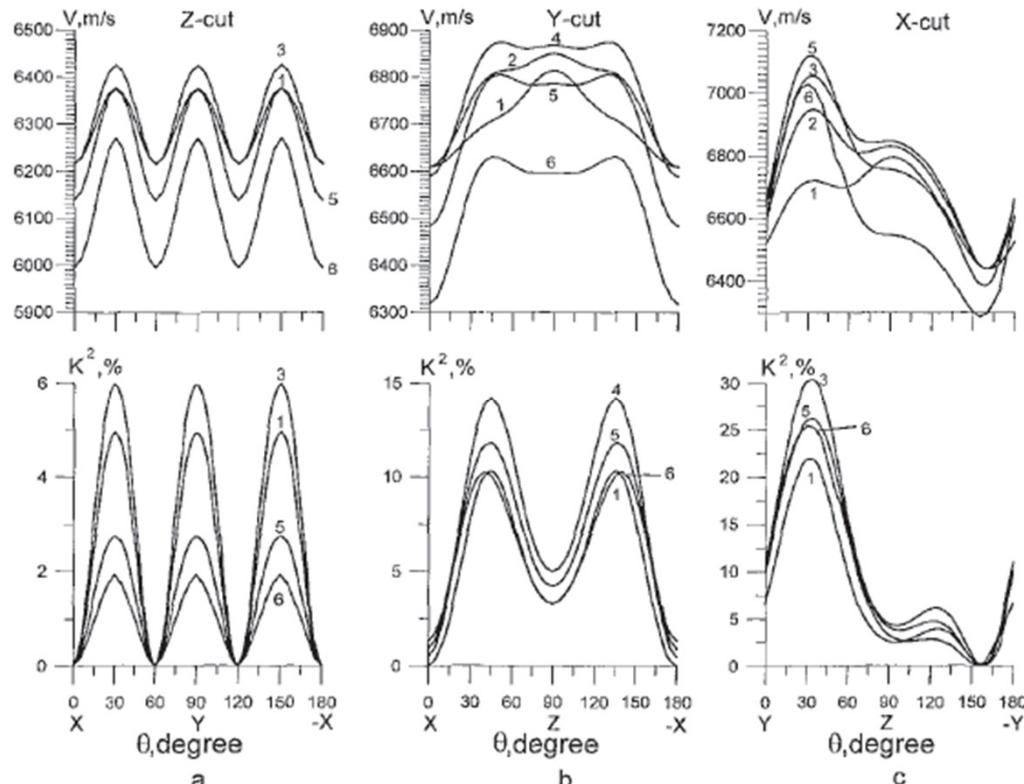
a



b



c



S0 Mode in  $\text{LiNbO}_3$

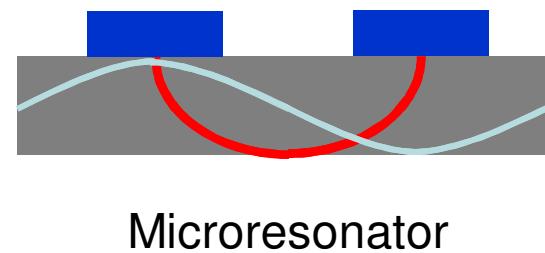
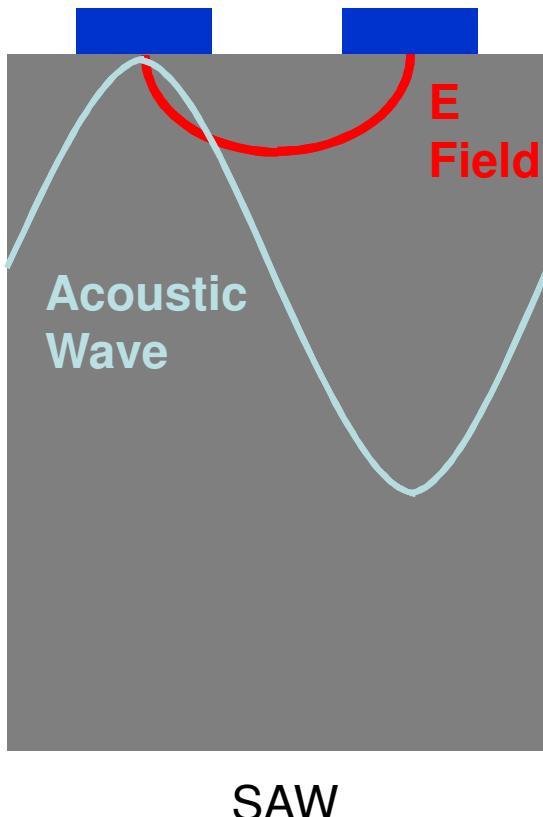
$1, 2, 3, 4, 5, 7$  ( $h/\lambda$ ) = 0.01, 0.025, 0.05, 0.1, 0.25 and 0.35

Kuznetsova et al., "Investigation of Acoustic Waves in Thin Plates of Lithium Niobate and Lithium Tantalate," *IEEE Trans. On Ultrasonics, Ferroelectrics and Freq. Cntrl.*, Vol 48, No. 1, January 2001.

# Why the Increase in Coupling?



- *Increased Interaction of the Acoustic Wave With the RF Electric Field Compared to SAW as a Result of the Thin Plate*

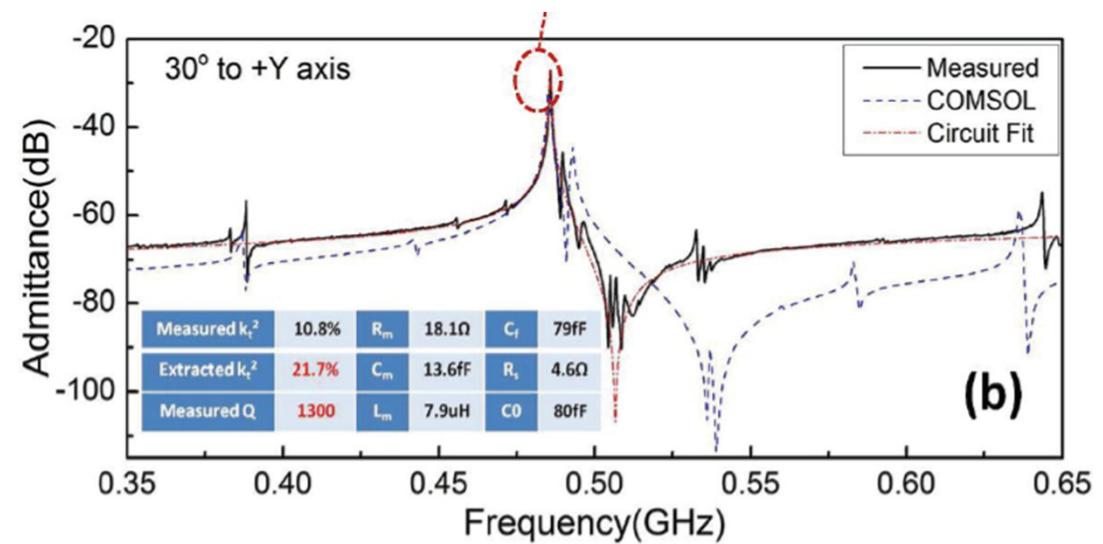
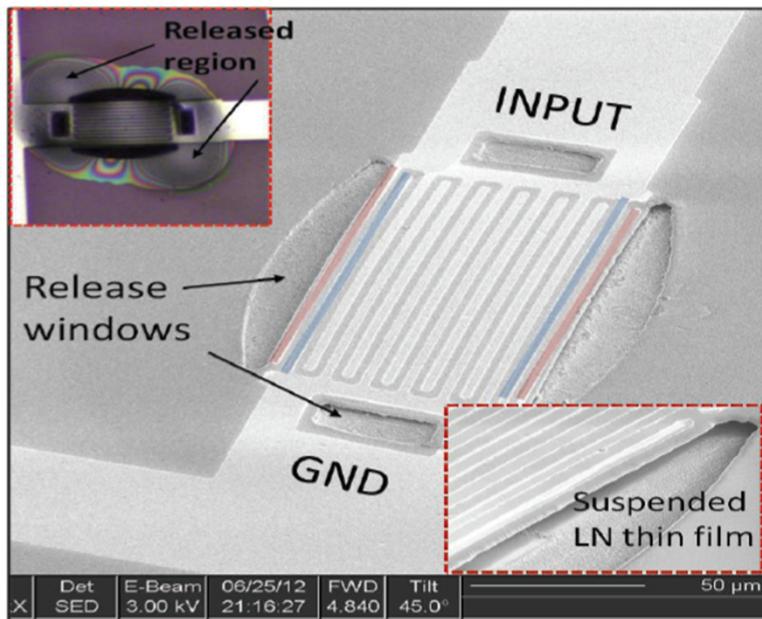


SAW

21

# $\text{LiNbO}_3$ Microresonators

- $k_t^2$  Extracted ~ 22%
- $Q = 1300$
- X-Cut
- Thin 3x3 cm<sup>2</sup> Pieces of  $\text{LiNbO}_3$  on BCB on  $\text{LiNbO}_3$  Provided by Srico



S. Gong and G. Piazza., "Weighted Electrode Configuration for Electromechanical Coupling Enhancement in a New Class of Micromachined Lithium Niobate Laterally Vibrating Resonators," *IEEE Int. Elect. Dev. Meeting.*, 15.6.1-15.6.4, Dec. 2012.

# Tuning of High $k_t^2$ Microresonators



## ➤ *LiNbO<sub>3</sub> Microresonator 2-Pole Filter*

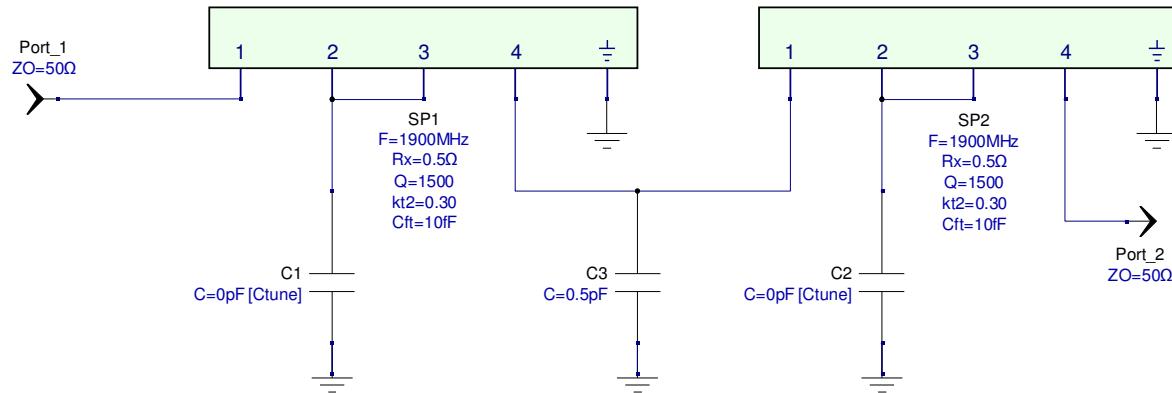
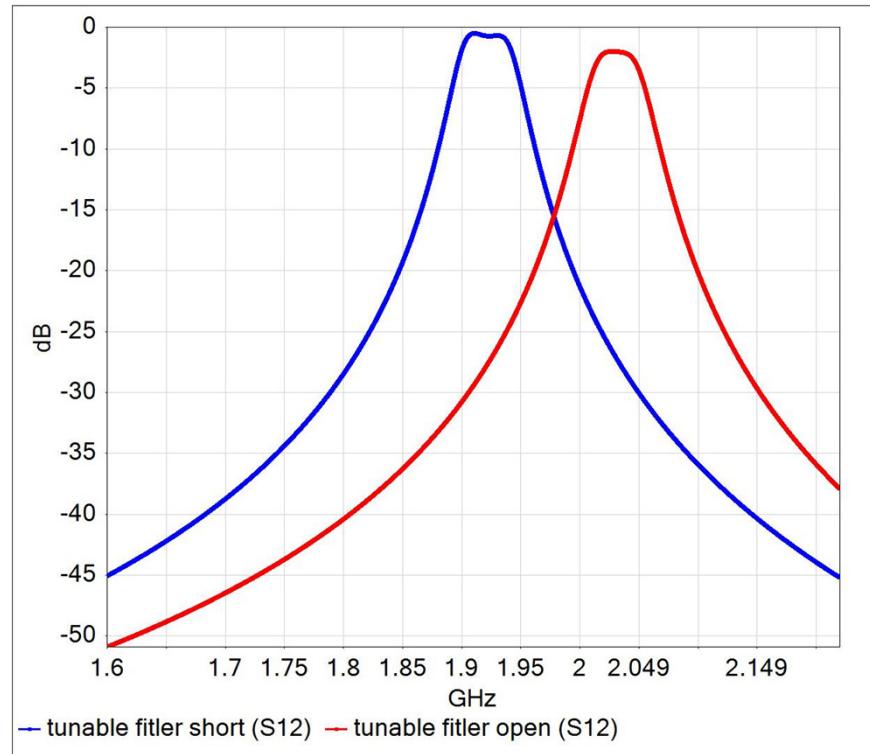
- $k_t^2 = 30\%$
- $Q = 1500$
- $R_X = 0.5 \Omega$

## ➤ *Q of all Capacitors = 40*

## ➤ *BW = 2.7%*

## ➤ *Tuning Range = 6.1%*

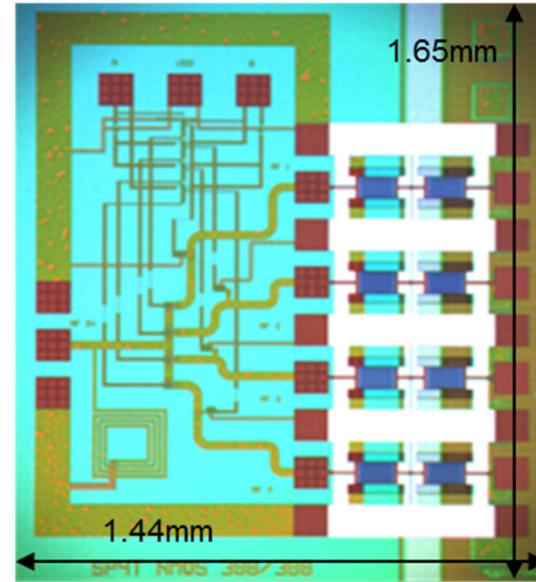
## ➤ *Significantly Reduces Number of Switched Acoustic Resonators*



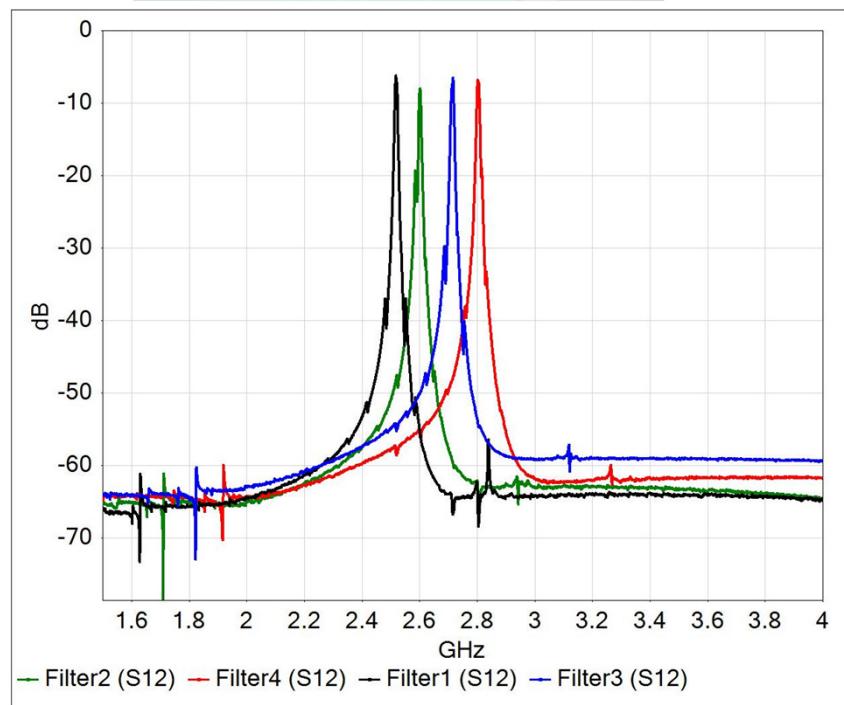
Tunable Filter Model and Simulated Response

# Conclusions

- Future Adaptive and Cognitive Radios Require Tunable Center Frequency and Bandwidth Filters
- Acoustic Filters Are Desirable Because of Their Small Size and High-Q in Common RF Bands
- The Fundamental Resonator Figures of Merit ( $k_t^2$ , Q) Limit Performance Metrics Such as Bandwidth, Tuning, and Insertion Loss
- Current Acoustic Resonator Technologies Can Achieve Tunable Bandwidth and Switchable Center Frequency
- New Materials With Higher Coupling Coefficient Will Enable Tunable Center Frequency Acoustic Filters



S-Band  
Switched  
Filter Array



# Acknowledgments



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