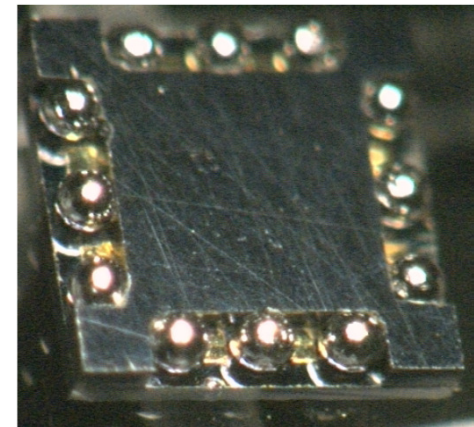
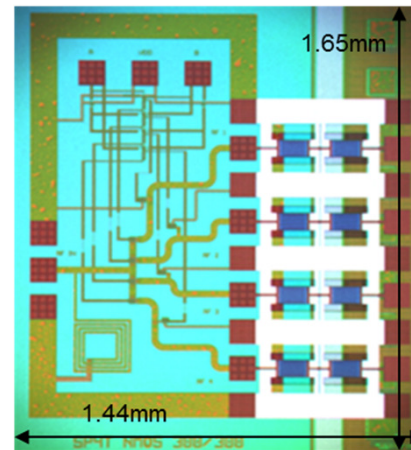
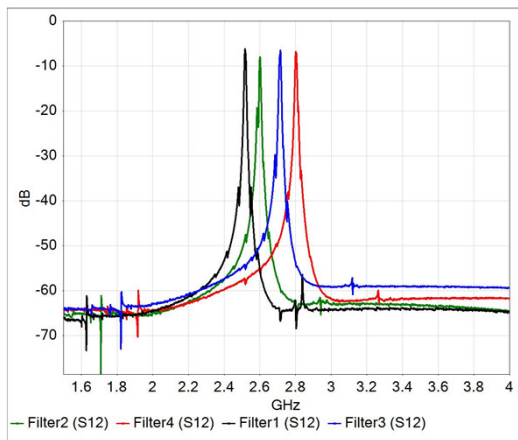


Exceptional service in the national interest



TUNING THE BANDWIDTH AND CENTER FREQUENCY OF MICROMECHANICAL ACOUSTIC FILTERS

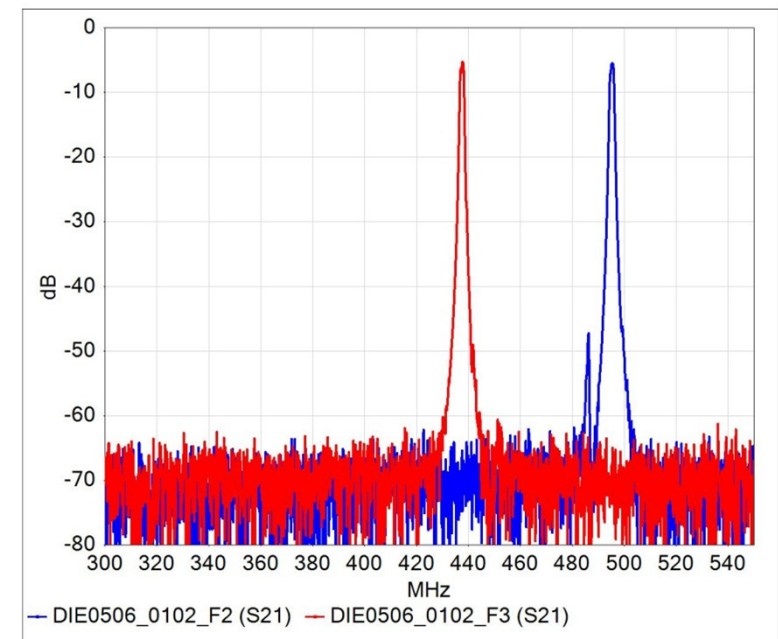
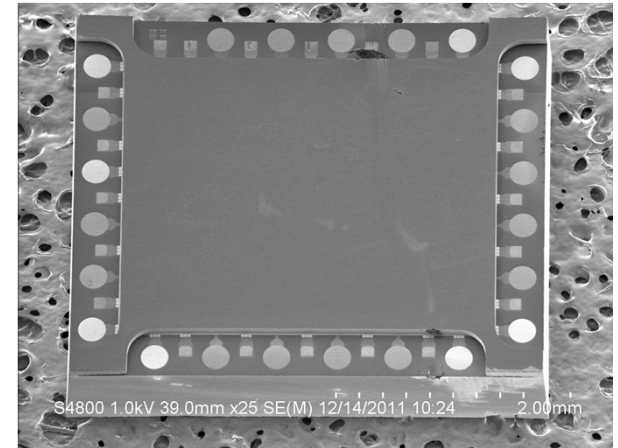
Roy H. Olsson III, Bongsang Kim, Janet Nguyen, Peggy Clews, Tammy Pluym and Kenneth E. Wojciechowski

Acoustic Micro-Scale Resonators

Outline

- *Motivation*
- *Fundamentals*
 - k_t^2 -Q FOM
 - Material Based Tuning Limitations
- *Tuning of Acoustic Resonators*
 - Tuning Range
 - Tunable Filters
 - Active Tuning
- *New Materials and Impact on Performance*
 - Comparing Acoustic Resonators
 - High k_t^2 Microresonators
 - Impact on Tuning

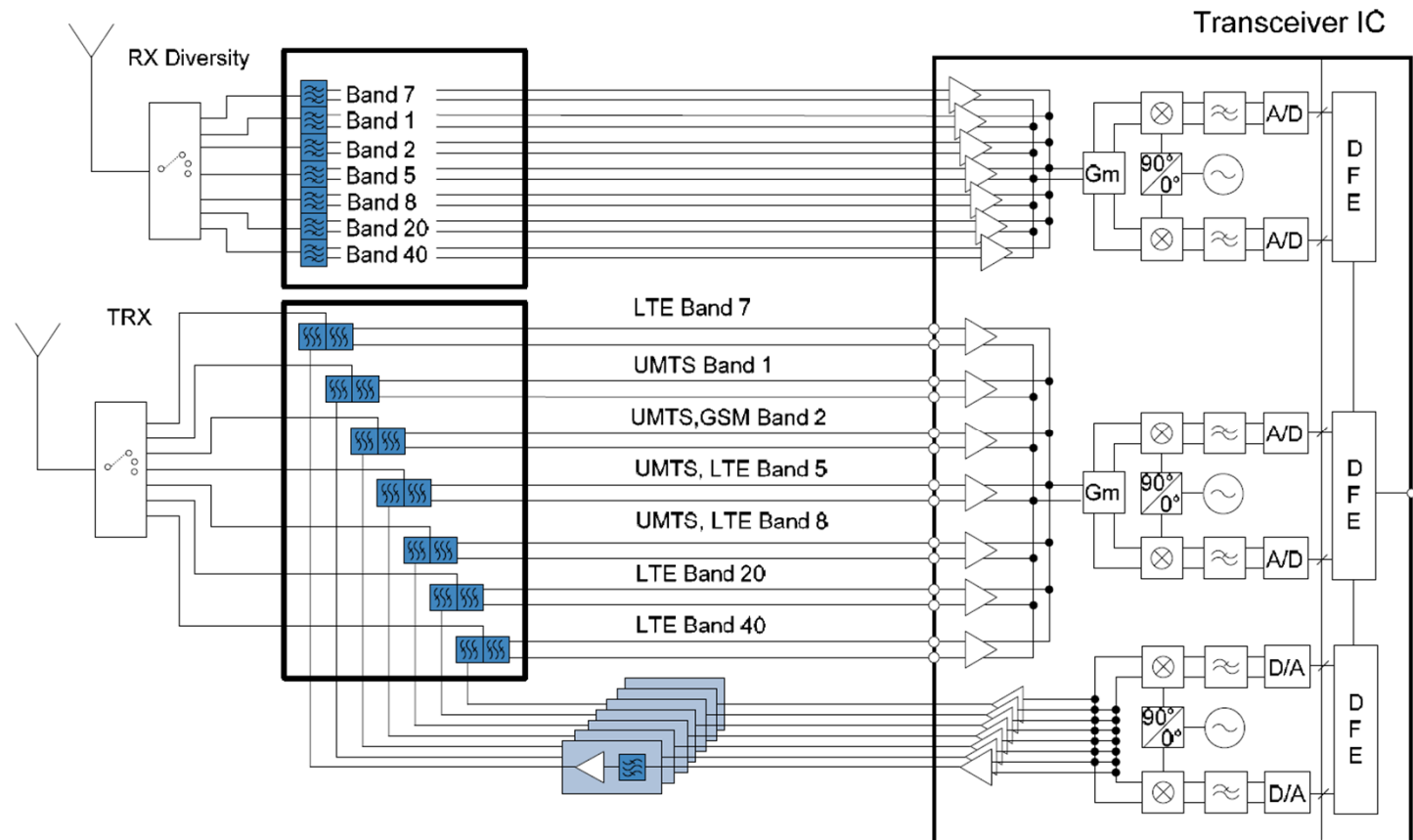
IF Filter Die
Containing
3 Filters



Filter Arrays for Handsets

- Diagram Contains 28 Filters Operating in ~ 7 Bands
- Microresonator Technology Can Potentially Address Many of These Filters on a Single Chip, Reducing Size and Assembly Costs

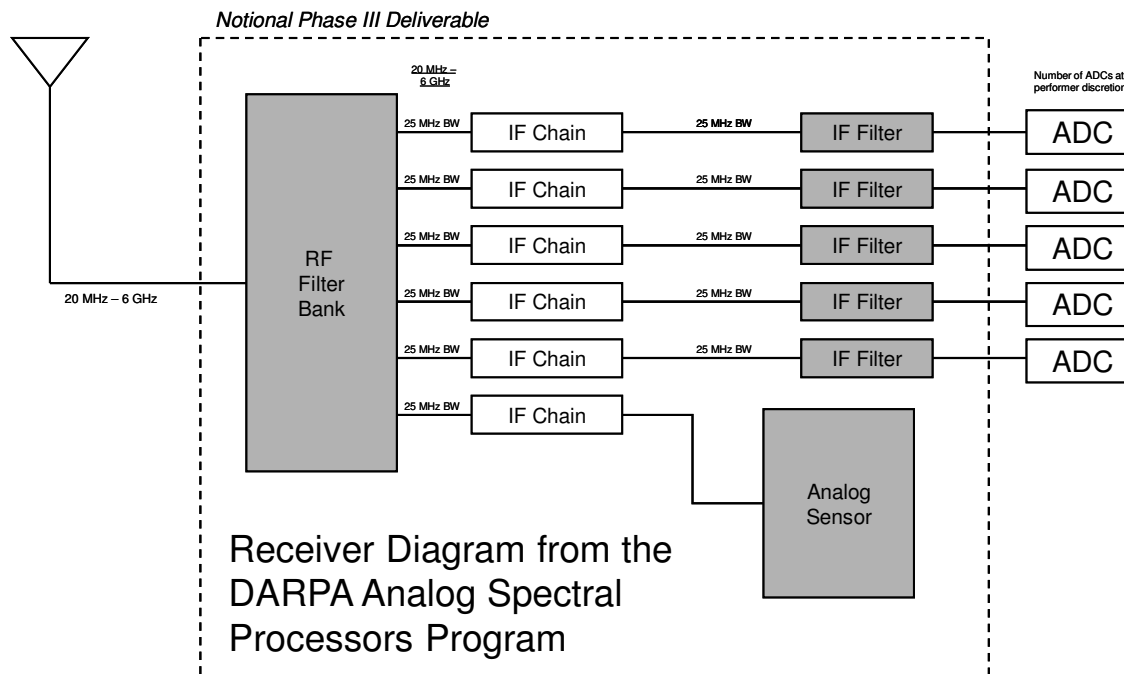
R. Vazny et al.
“Front-End
Implications to
Multi-Standard
Cellular Radios:
State-of-the-Art
and Future
Trends”, *Proc. Of
the 2010 IEEE
Ultrasonics
Symposium*, pp.
95 – 98, Oct.
2010



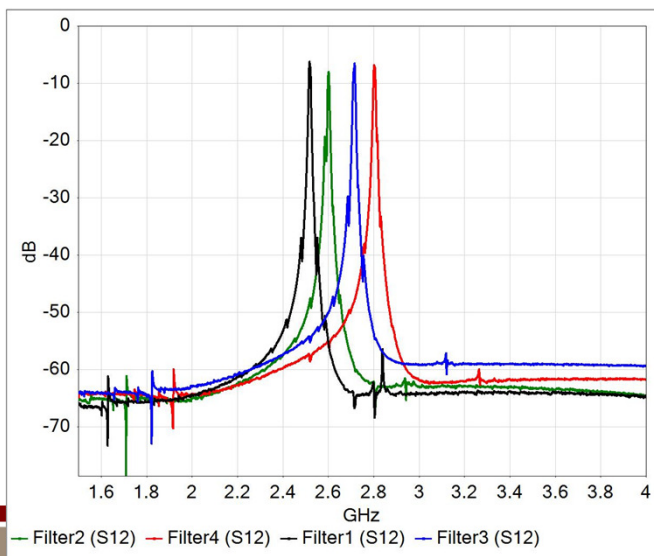
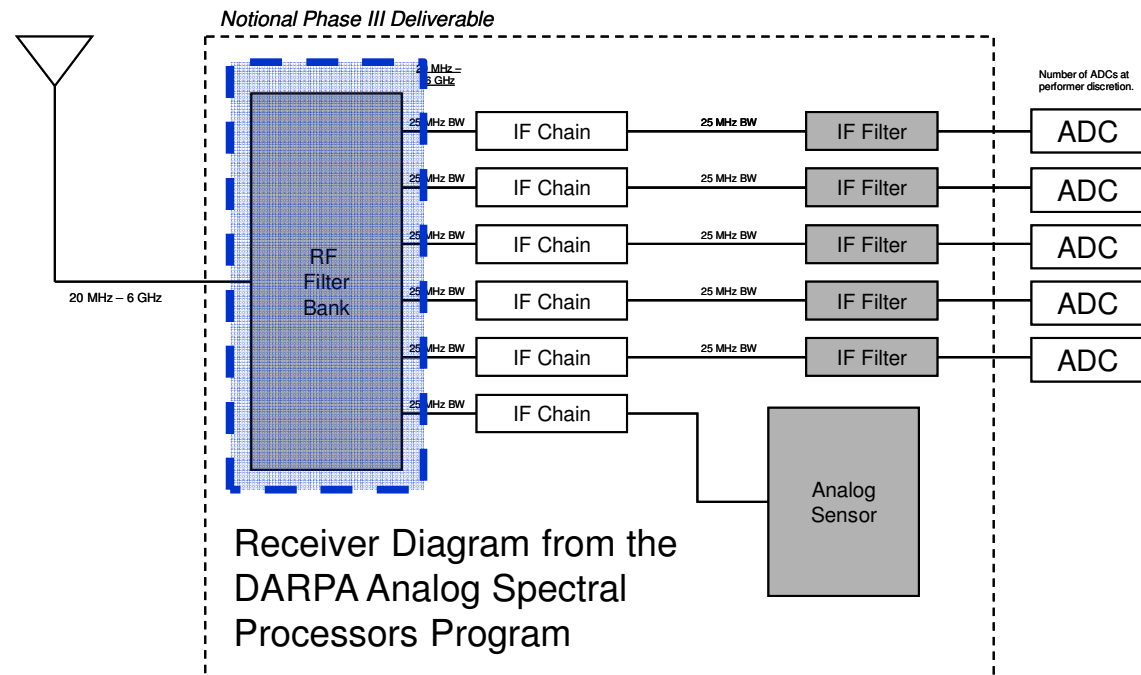
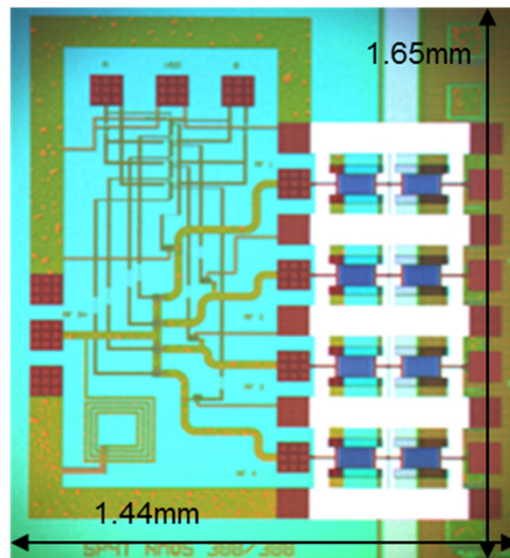
RF Front-End of a Modern Cellular Radio

Filters in Military Radios

- Current Military Radios Are Mandated to be Backwards Compatible
 - *Legacy and Updated Frequencies and Waveforms*
 - *Many RF Frequencies and Bandwidths Required*
- Future Military Radios Will Require Spectral Knowledge and Real Time Adaptability to Mitigate Both Co-Site and Adversary Jamming

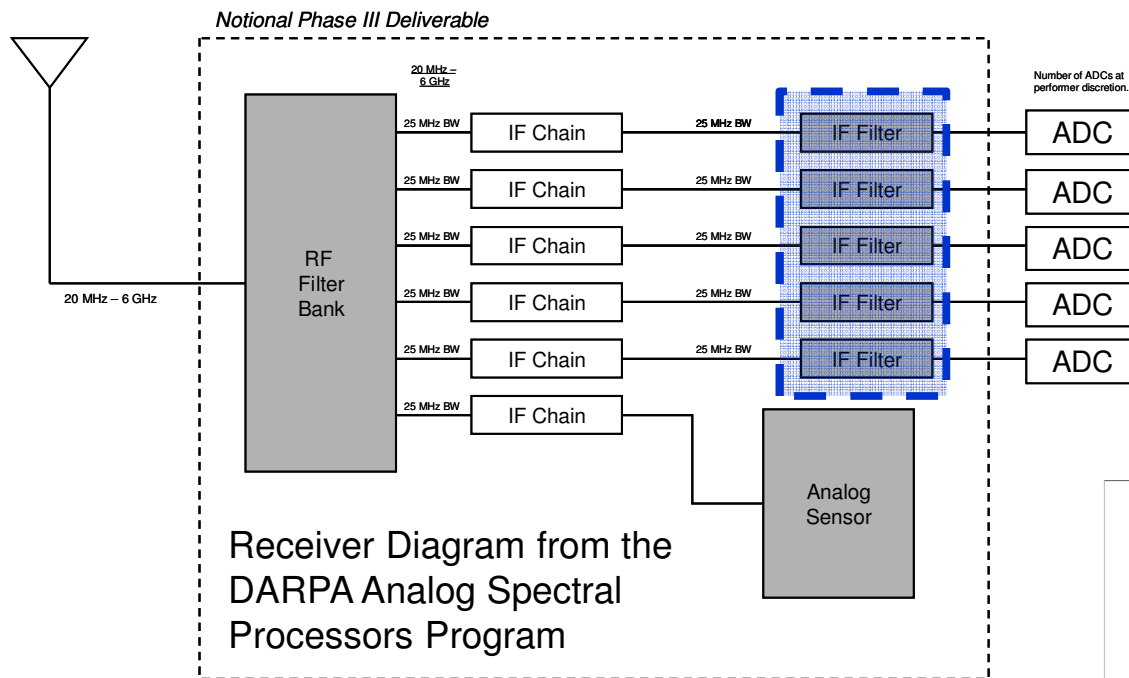


Frequency Adaptability on the RF Front-End

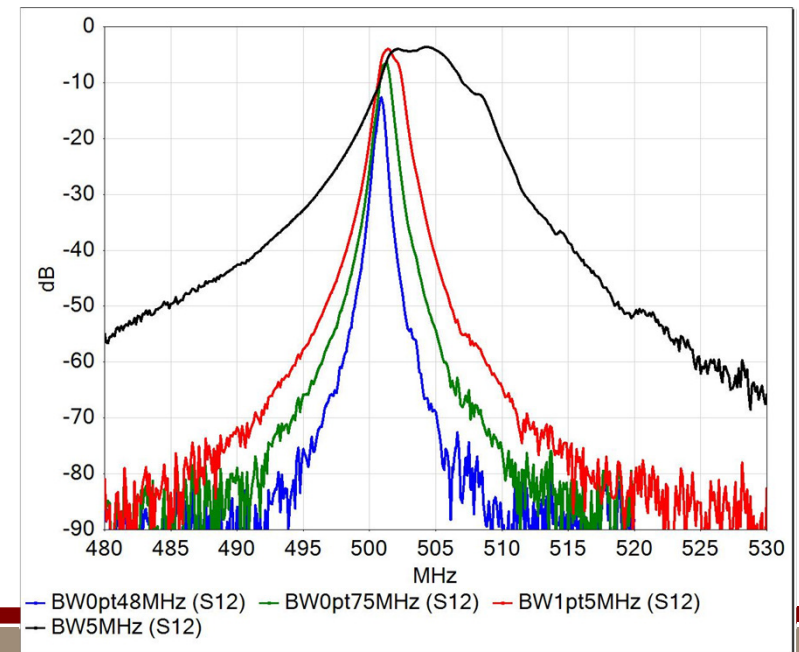
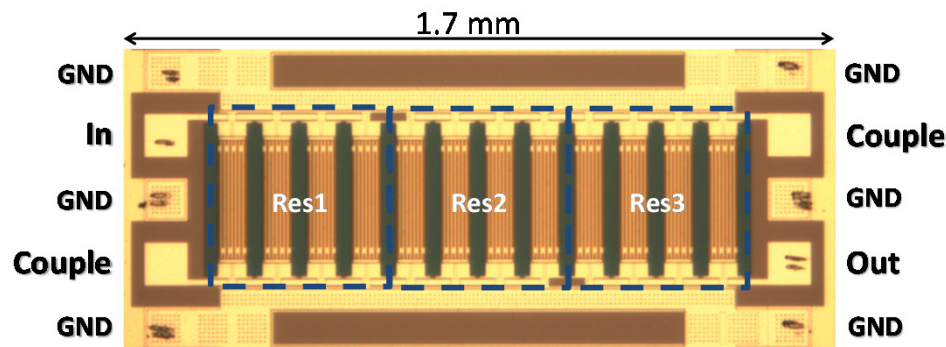


S-Band Switched Filter Array on CMOS for RF Center Frequency Adaptability

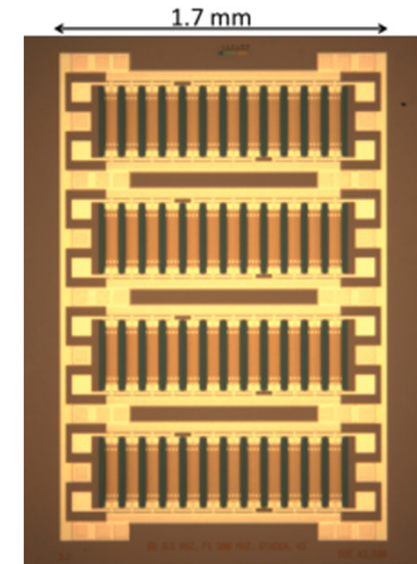
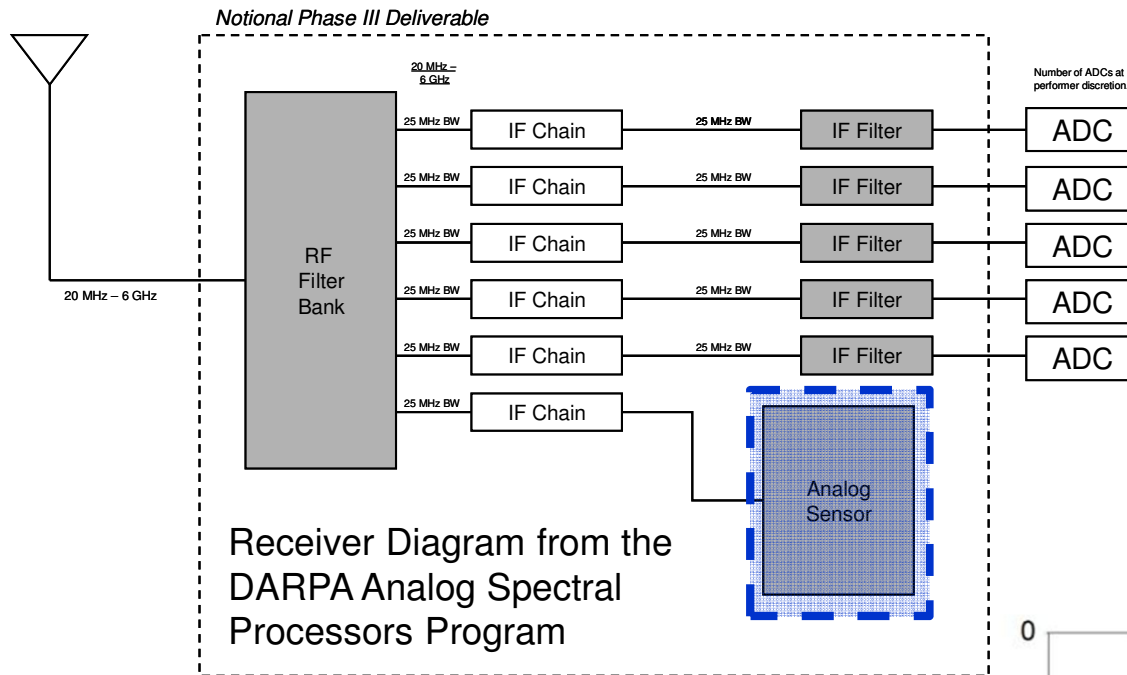
Waveform and Bandwidth Adaptability IF Filtering



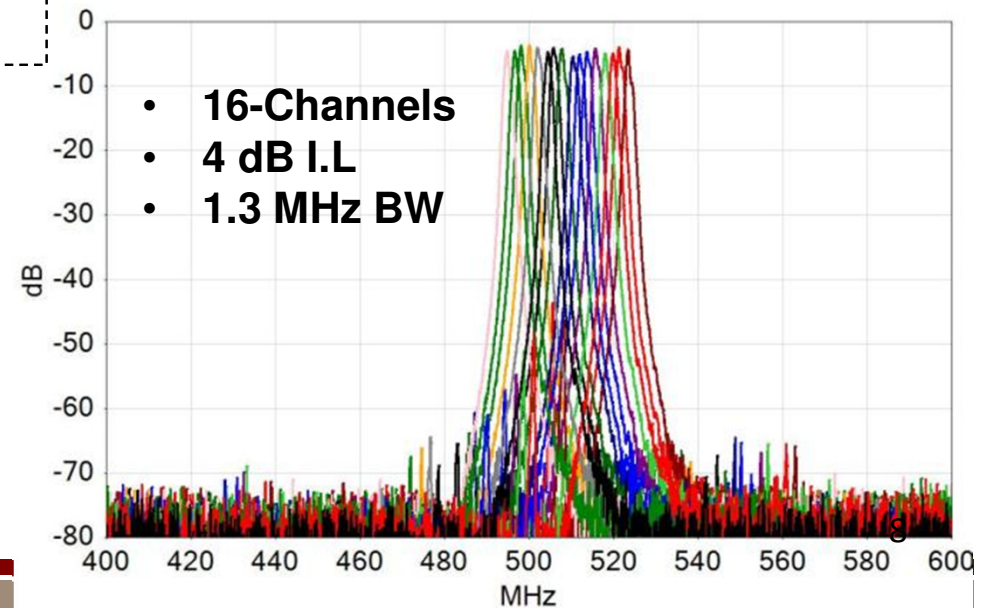
IF Filter with Programmable Bandwidth from 5.1 MHz to 0.48 MHz



RF Spectral Awareness

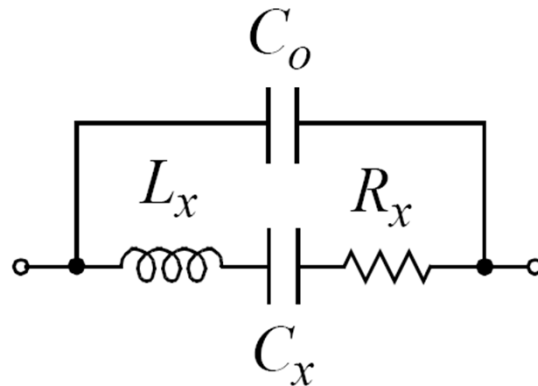
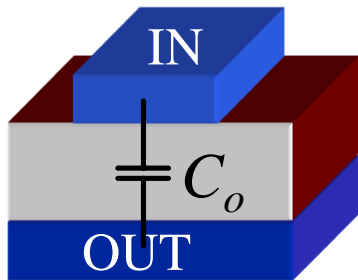


16-Channel Filter Array for RF Spectral Sensing



Piezoelectric Resonator Transduction

Top-Bottom Transduction



$$C_x = 0.8k_t^2 C_0$$

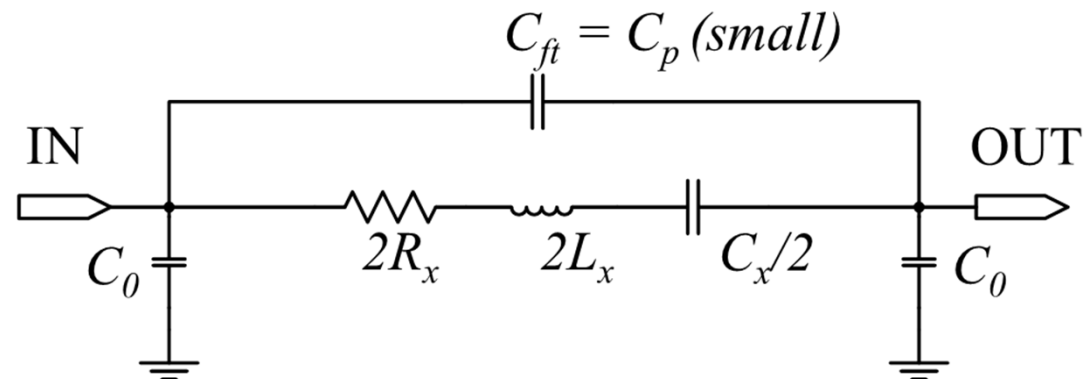
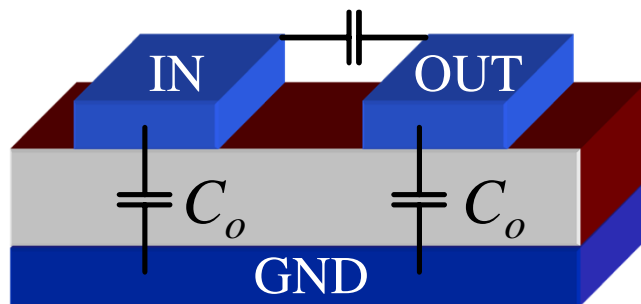
$$L_x = \frac{1}{0.8\omega^2 k_t^2 C_0}$$

$$R_x = \frac{1}{0.8\omega C_0 k_t^2 Q}$$

$$k_t^2 = \frac{d_{31}^2 E}{\epsilon}$$

$$FOM = k_t^2 Q$$

Top-Top Transduction



 Top electrode  Bottom electrode  Piezoelectric Film (AlN)

Piezoelectric Resonator Transduction

➤ Loss

- Proportional to FOM
- R_x Set by FOM, Frequency, C_0 (Area)

$$C_x = 0.8k_t^2 C_0$$

➤ Tuning

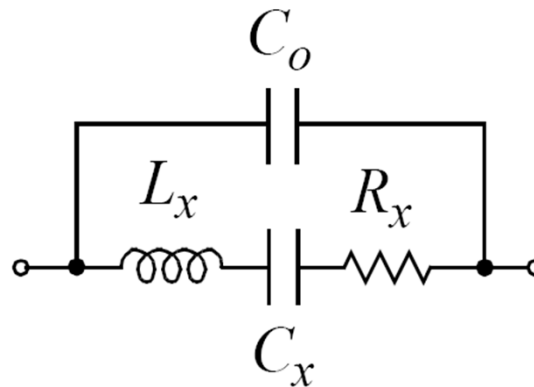
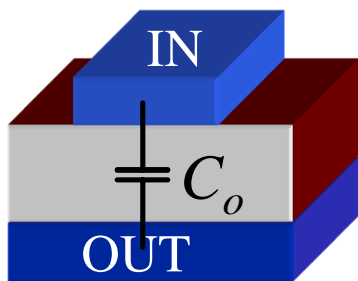
- Maximum Tuning Range is Determined by k_t^2

$$L_x = \frac{1}{0.8\omega^2 k_t^2 C_0}$$

➤ Bandwidth

- Minimum Practical Filter Bandwidth is Determined by Q
- Maximum Practical Filter Bandwidth is Determined by k_t^2

$$R_x = \frac{1}{0.8\omega C_0 k_t^2 Q}$$

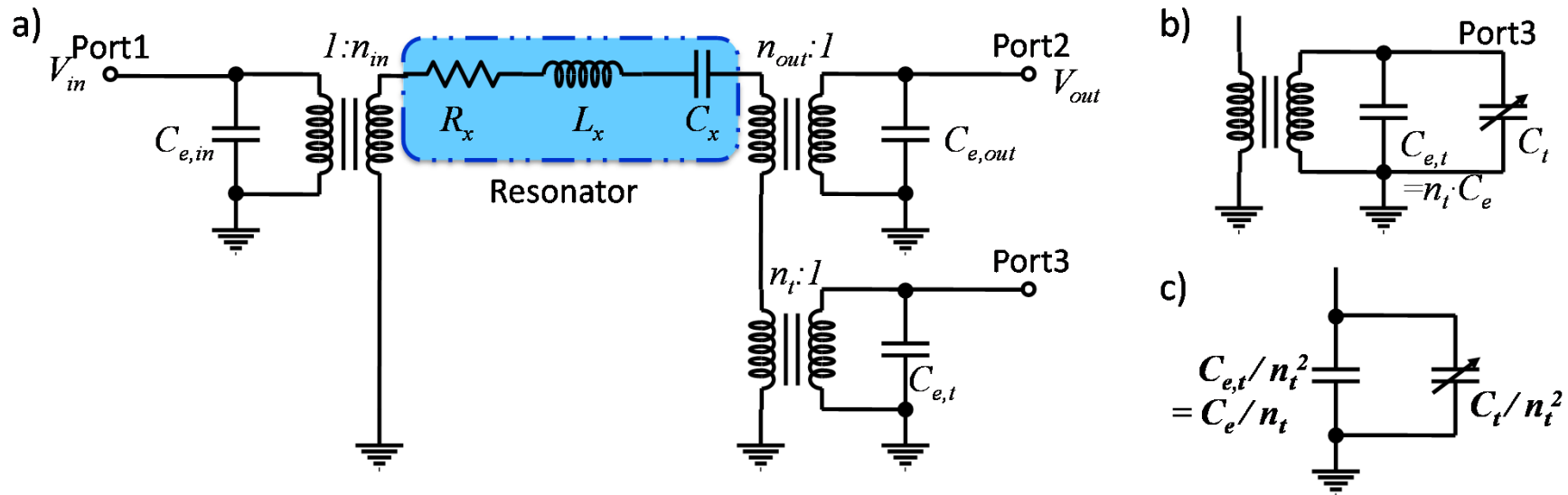
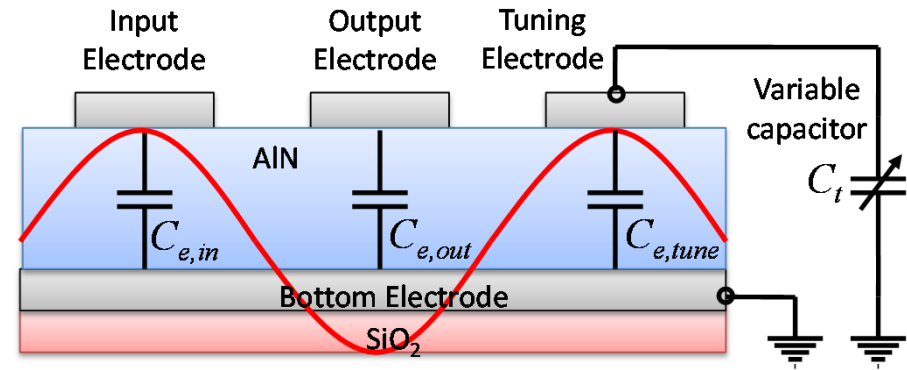


$$k_t^2 = \frac{d_{31}^2 E}{\epsilon}$$

$$FOM = k_t^2 Q$$

k_t^2 Limits the Tuning Range

3-Port Tunable Micromechanical Resonator
Cross-Section



3-Port Tunable Micromechanical Resonator Equivalent Circuit Model

k_t^2 Limits the Tuning Range

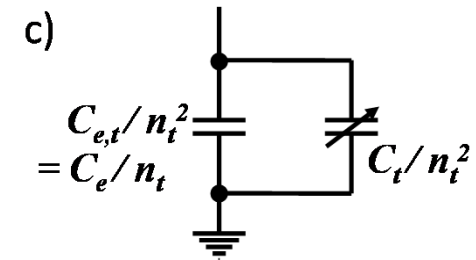
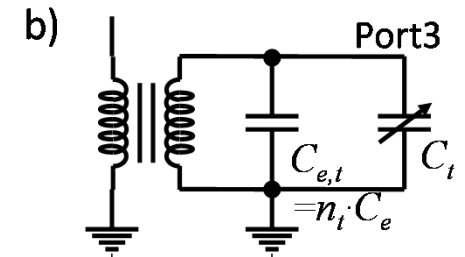
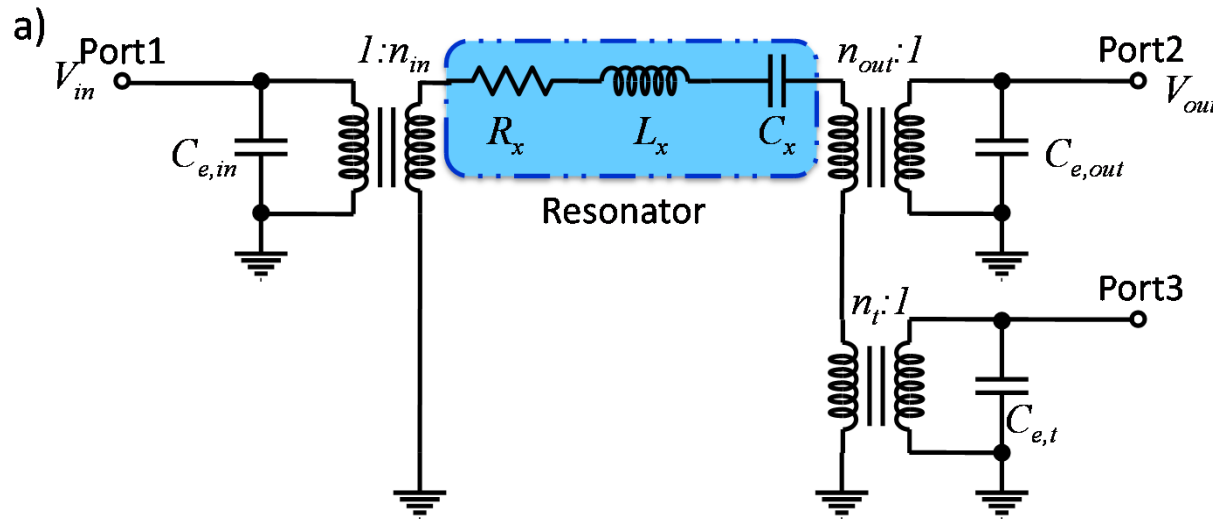
$$\frac{1}{C_x'} = \frac{1}{C_x} + \frac{n_t^2}{n_t C_e + C_t}$$

$$f' = \frac{1}{2\pi} \sqrt{\frac{1}{L_x C_x'}} = \frac{1}{2\pi} \sqrt{\frac{1}{L_x} \left(\frac{1}{C_x} + \frac{n_t^2}{n_t C_e + C_t} \right)}$$

$$\frac{\Delta f}{f} = \frac{1}{2} \frac{n_t^2 \cdot C_x}{n_t C_e + C_t}$$

$$0 < \frac{\Delta f}{f} < \frac{n_t}{2} \frac{C_x}{C_e}$$

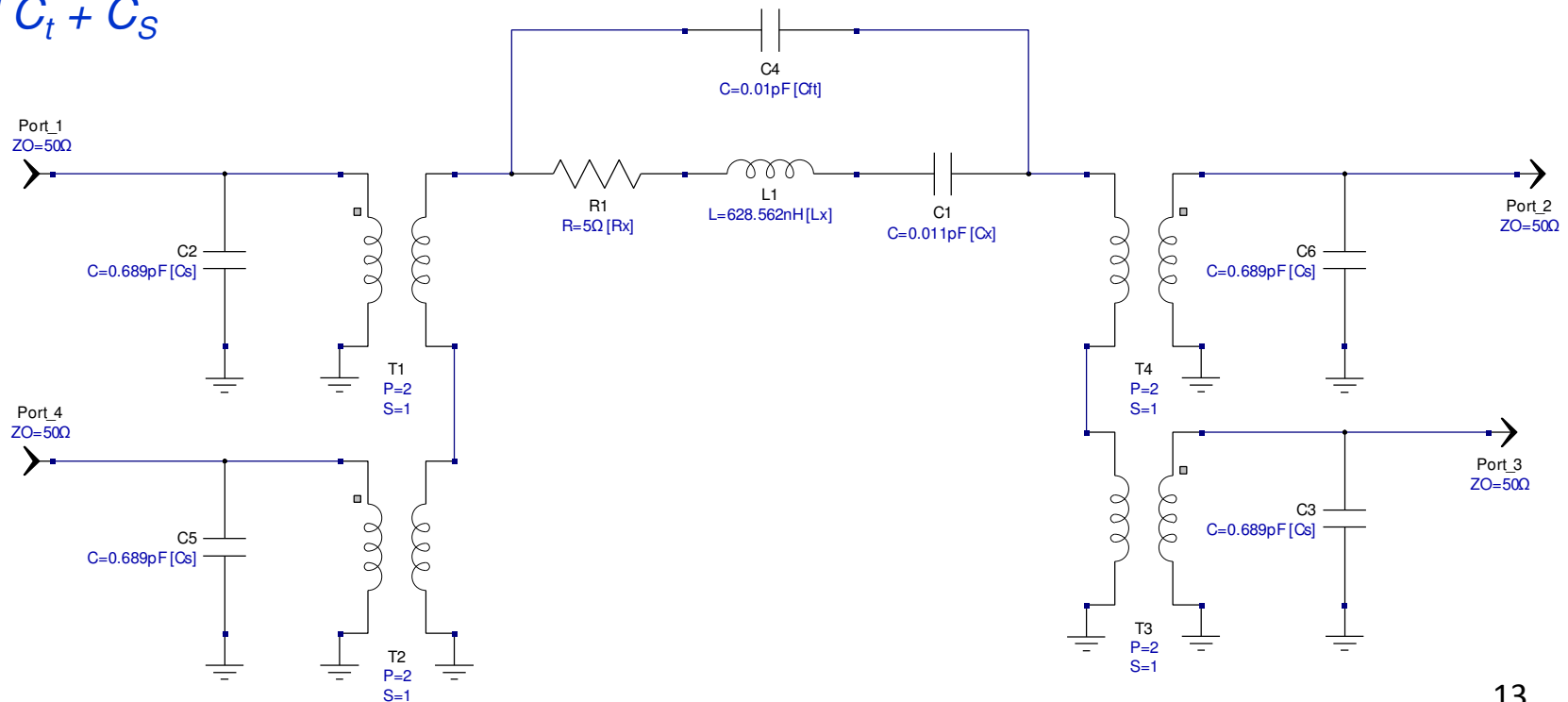
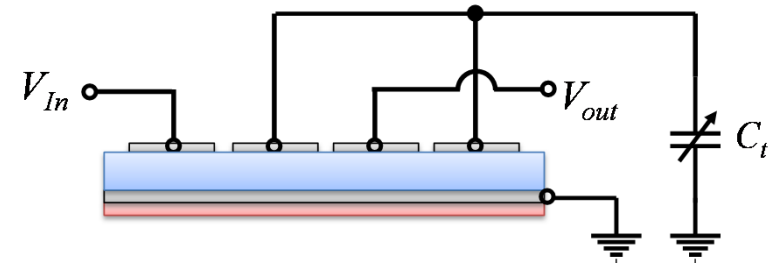
$$\frac{C_x}{C_e} = \frac{8}{\pi^2} k_t^2$$



Multi-Port Resonators for Tuning

- $\frac{1}{2}$ of Electrodes Used for Filtering
- $\frac{1}{2}$ of Electrodes Used for Tuning
- Tuning Range Limited by C_X/C_S or k_t^2
- Feedback Signal on C_t is 90 deg. Out of Phase with the Input and is Maximized for Small $C_t + C_S$

a) **Configuration A**



AlN Microresonator Tuning

➤ AlN Microresonator

- $k_t^2 = 2\%$
- $Q = 1500$
- $R_x = 5 \Omega$
- Tuning Range = 0.4%

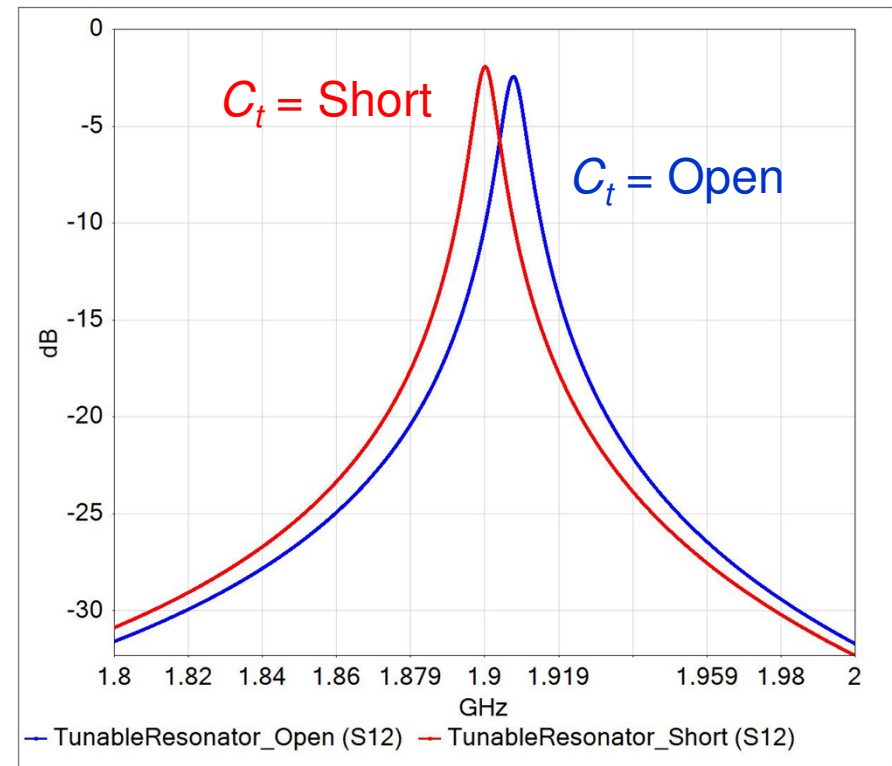
➤ Using $\frac{1}{2}$ of the k_t^2 for Bandwidth and $\frac{1}{2}$ for Tuning

➤ C_t Varied From Open to Short

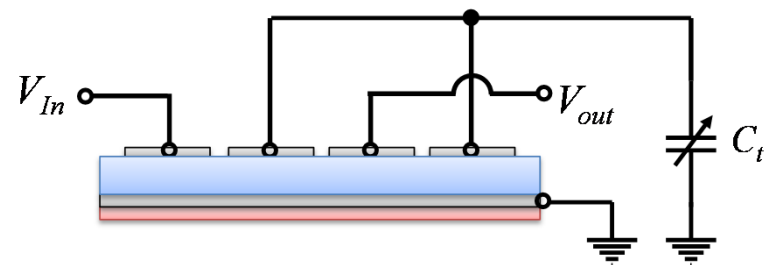
➤ Additional 0.5 dB Loss is From the Finite Q of the Electrode Capacitors

➤ As We Tune Away From the Acoustic Resonance

- More Energy Stored in the Capacitors
- Higher Capacitor Q Required
- Trade Off Between Acoustic and Capacitor Q With Metal Thickness

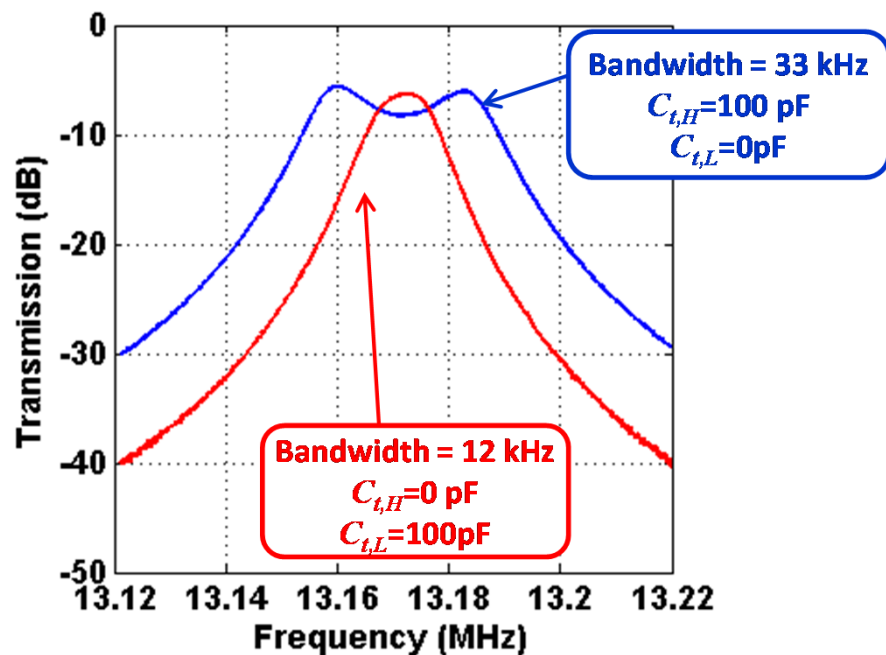


a) Configuration A

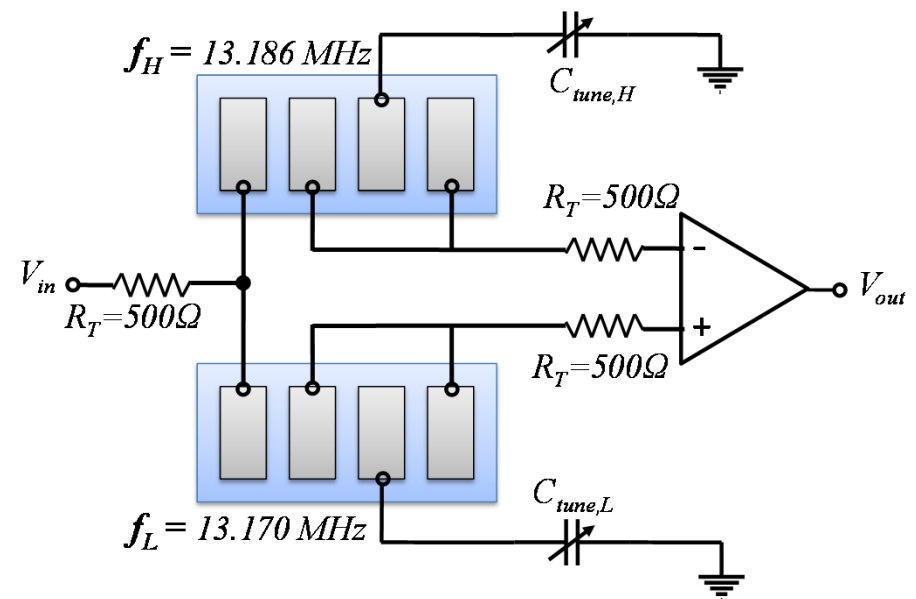


Tunable Bandwidth Lattice Filter

- Achieved $\sim 3\times$, 3 dB Bandwidth Tuning Range
- Parallel Lattice Filter Architecture
- Resonator Tuning Range Limited to $< k_t^2/2$

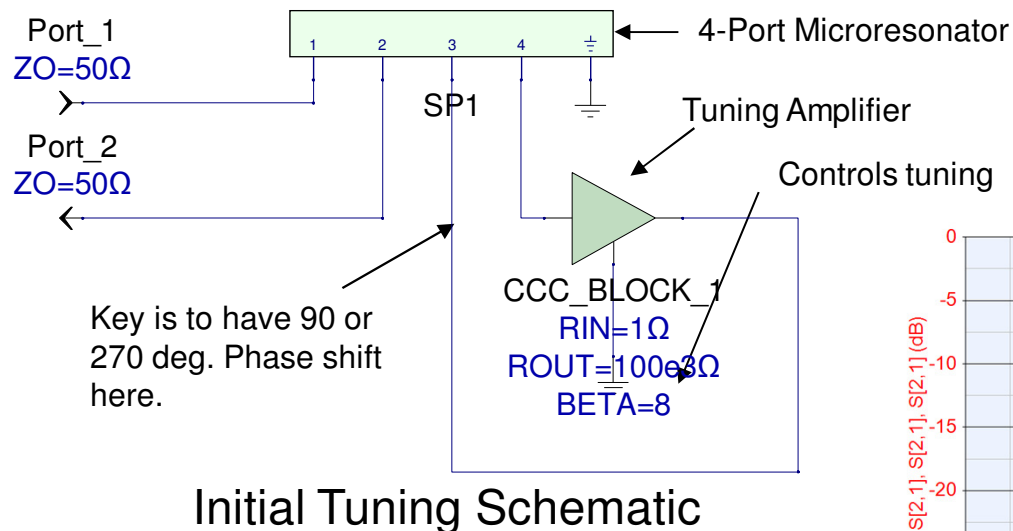


Tunable Bandwidth Filter Response



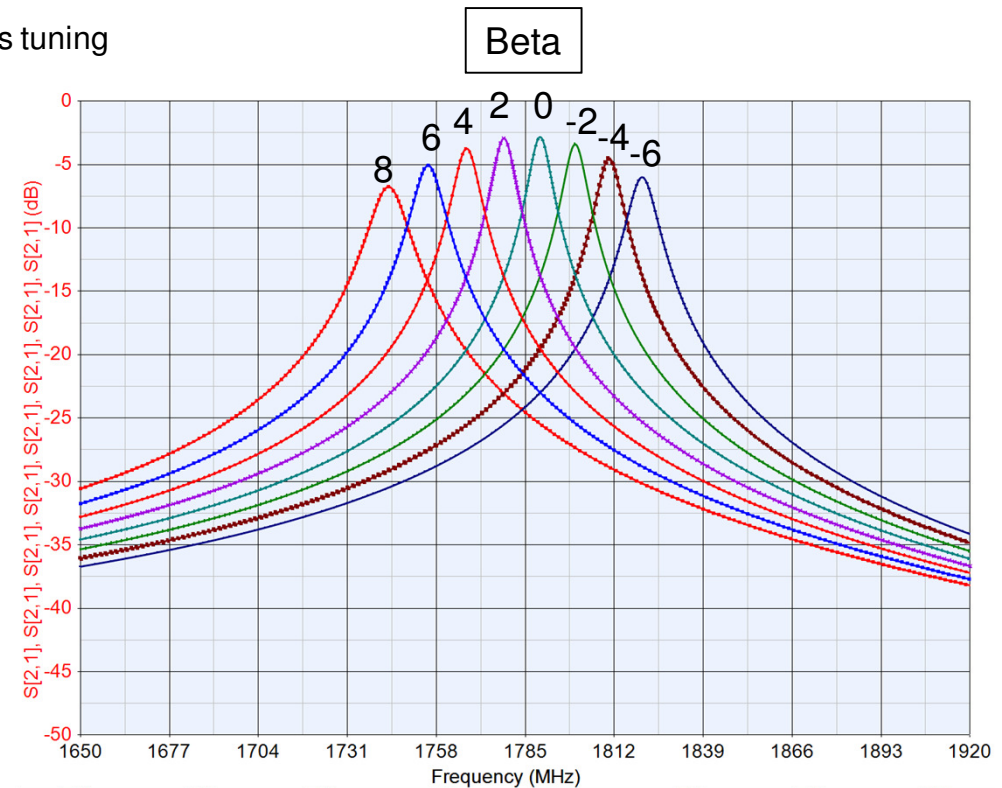
Tunable Bandwidth Filter Schematic

Active Resonator Tuning



➤ Active Tuning

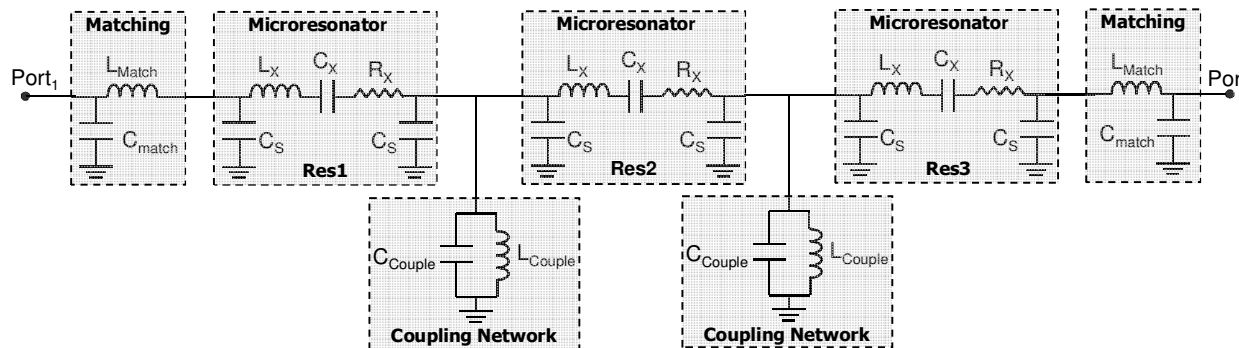
- AlN Microresonator with a k_t^2 of 1.5%
- RF filters can be tuned >7.0%
- Passive Tuning was 0.3%
- Can be implemented in several ways using existing transistors
- Requires realistic current gains of 8



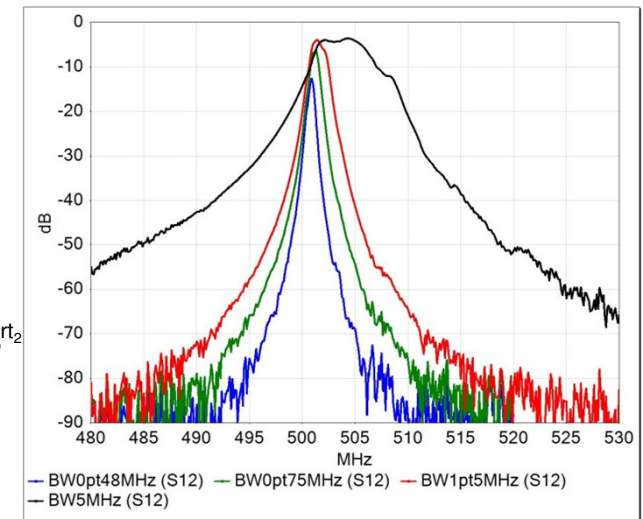
Utilizing Active Gain to Extend the Tuning Range of Microresonators

Programmable Bandwidth Filter

- Alters Resonator Coupling by Tunable Coupling Networks
- Over 10x Bandwidth Programmability Using COTs Passives with $Q = 50$
- Working to Integrate Switched Coupling and Matching Capacitors Under Resonator to Enable Tunable Bandwidth



Programmable Bandwidth Filter Schematic



Programmable Bandwidth Filter
Measured Response

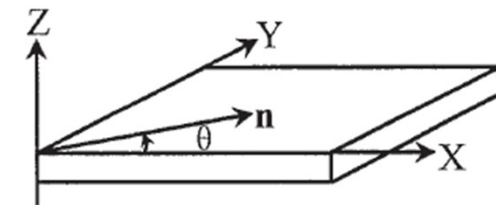
3 dB Bandwidth (MHz)	Insertion Loss (dB)	Stop Band Rejection (dB)	L_{couple} (nH)	C_{couple} (pF)	L_{match} (nH)	C_{match} (pF)
0.475	12.6	75	0	14	11	6
0.75	6.3	80	0	5	0	0
1.5	4.0	80	0	0	0	0
5.1	3.6	76	22	0	37	0

Increasing the Tuning Range

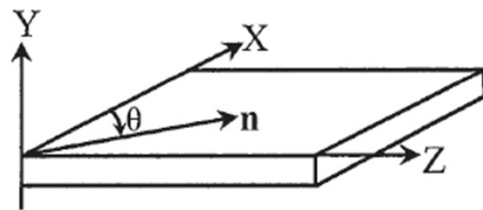
Types of Acoustic Resonators

Technology/ Metric	k_t^2 theory	k_t^2 experiment	Q @ ~ 1 GHz	FOM	Multiple Frequencies on a Substrate
AlN BAW/FBAR	6.5%	7%	3000	~200	High Cost
Standard LiNbO ₃ SAW	5.5%	5.5%	2000	~100	Yes
AlN Microresonator	2%	2%	2000	~40	Yes
Capacitive Microresonator	~Gap, Bias	< 0.1%	10,000	<1	Yes
Advanced SAW	> 20%	20%	2000	~400	Limited
PZT/BST BAW	7-12%	7-12%	60-250	~7-18	High Cost
Doped AlN BAW	15%	12%	< Undoped	TBD	High Cost
LiNbO ₃ Microresonator	> 30%	20%	1200	TBD	Yes

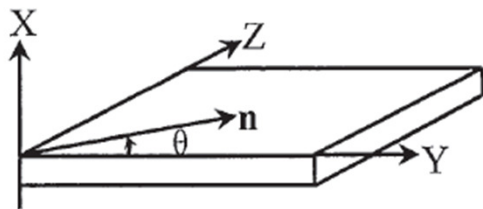
LiNbO₃ S0 Mode Microresonators



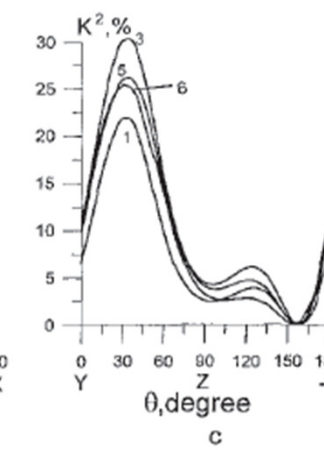
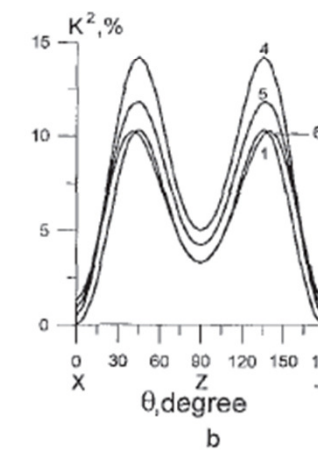
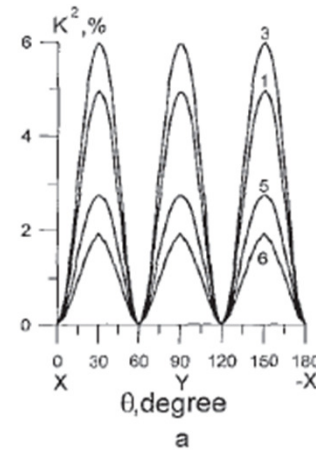
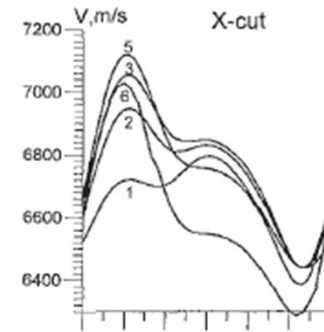
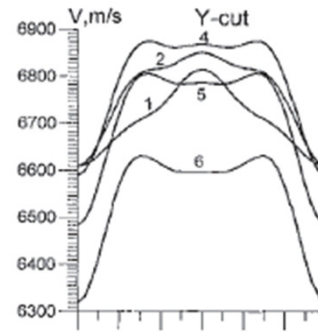
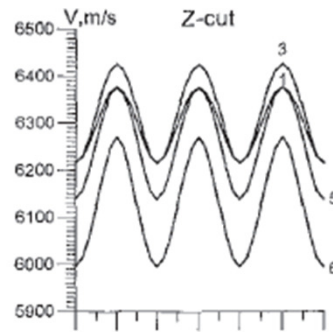
a



b



c



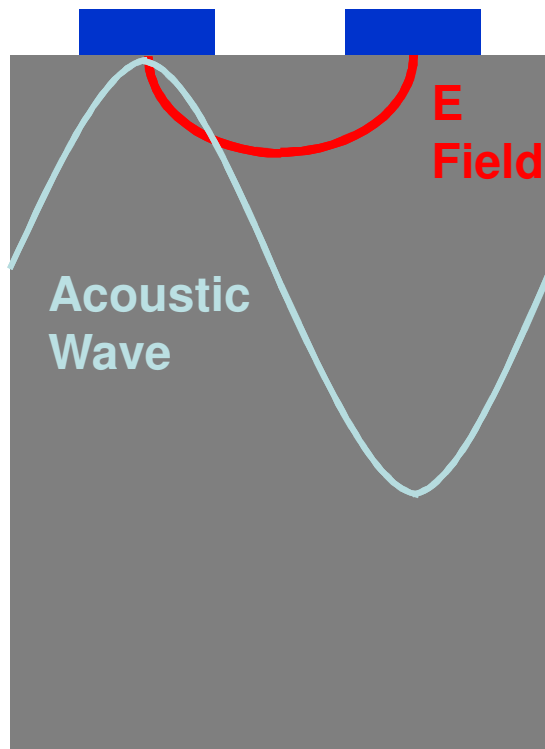
S0 Mode in LiNbO₃

1,2,3,4,5,7 (h/λ) = 0.01, 0.025, 0.05, 0.1, 0.25 and 0.35

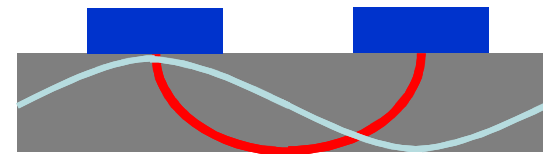
Kuznetsova et al., "Investigation of Acoustic Waves in Thin Plates of Lithium Niobate and Lithium Tantalate," *IEEE Trans. On Ultrasonics, Ferroelectrics and Freq. Cntrl.*, Vol 48, No. 1, January 2001.

Why the Increase in Coupling?

- *Increased Interaction of the Acoustic Wave With the RF Electric Field Compared to SAW as a Result of the Thin Plate*



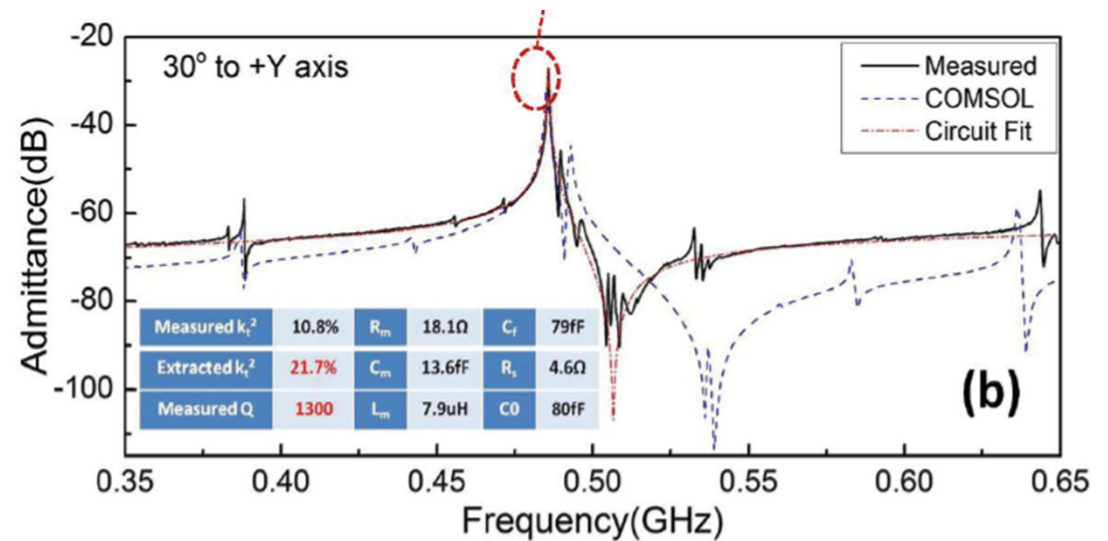
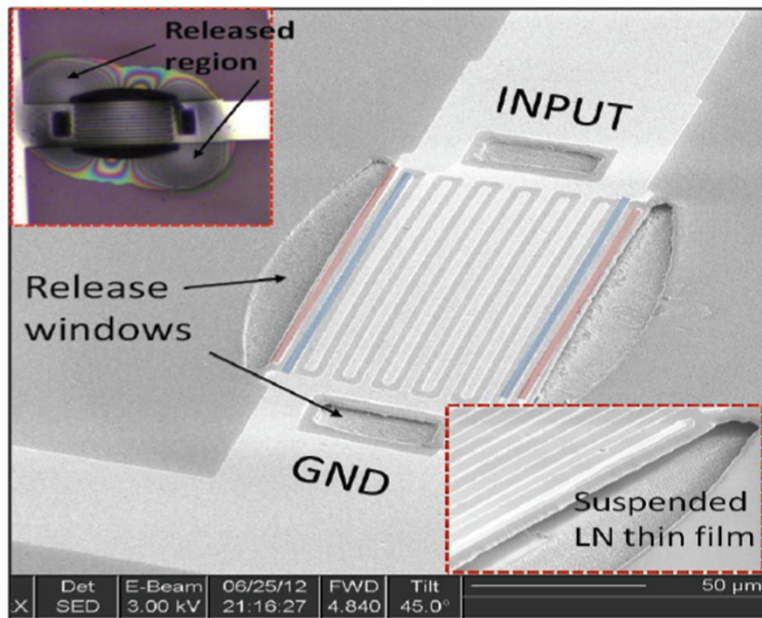
SAW



Microresonator

LiNbO₃ Microresonators

- k_t^2 Extracted ~ 22%
- $Q = 1300$
- X-Cut
- Thin 3x3 cm² Pieces of LiNbO₃ on BCB on LiNbO₃ Provided by Srico



S. Gong and G. Piazza., "Weighted Electrode Configuration for Electromechanical Coupling Enhancement in a New Class of Micromachined Lithium Niobate Laterally Vibrating Resonators," *IEEE Int. Elect. Dev. Meeting.*, 15.6.1-15.6.4, Dec. 2012.

Tuning of High k_t^2 Microresonators

➤ *LiNbO₃ Microresonator 2-Pole Filter*

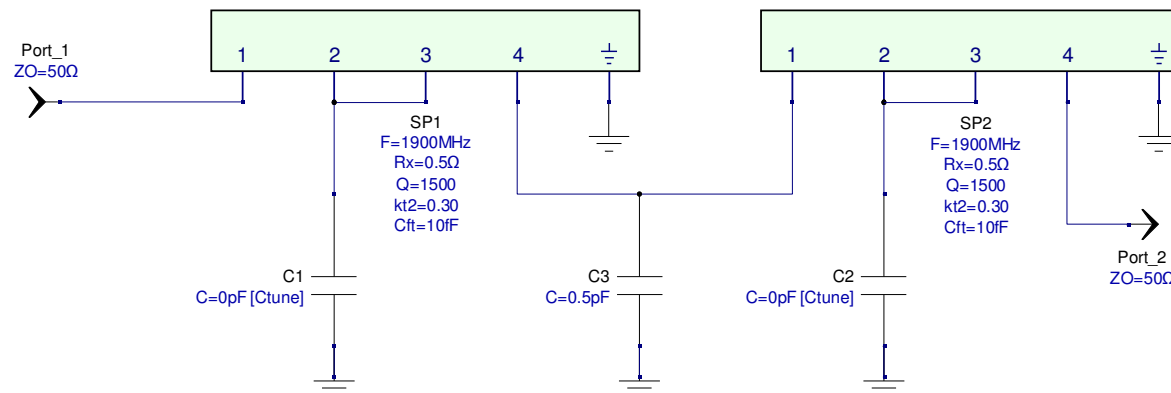
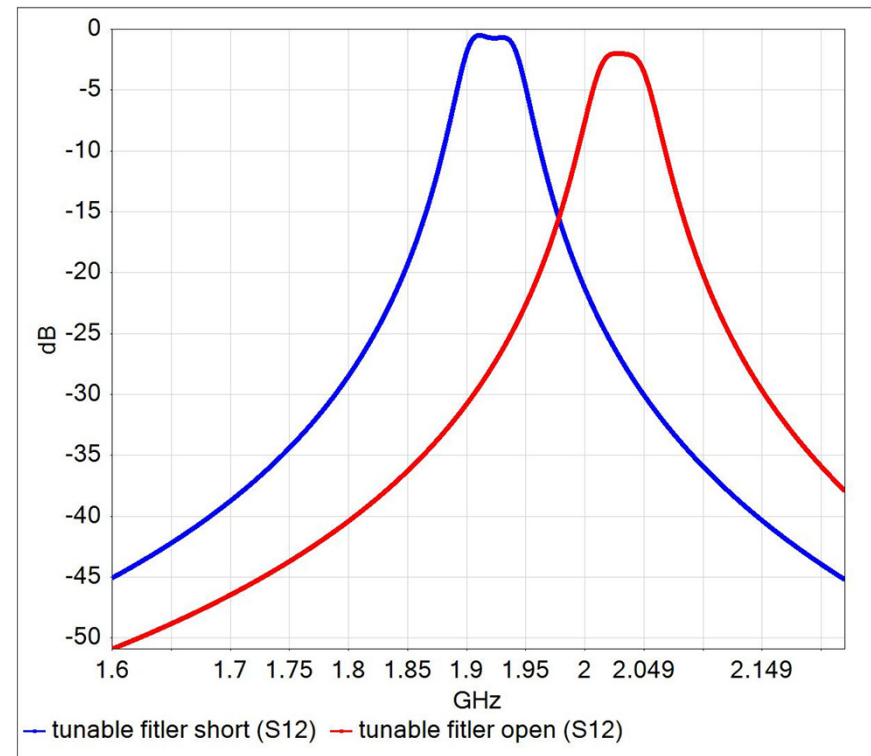
- $k_t^2 = 30\%$
- $Q = 1500$
- $R_x = 0.5 \Omega$

➤ *Q of all Capacitors = 40*

➤ *BW = 2.7%*

➤ *Tuning Range = 6.1%*

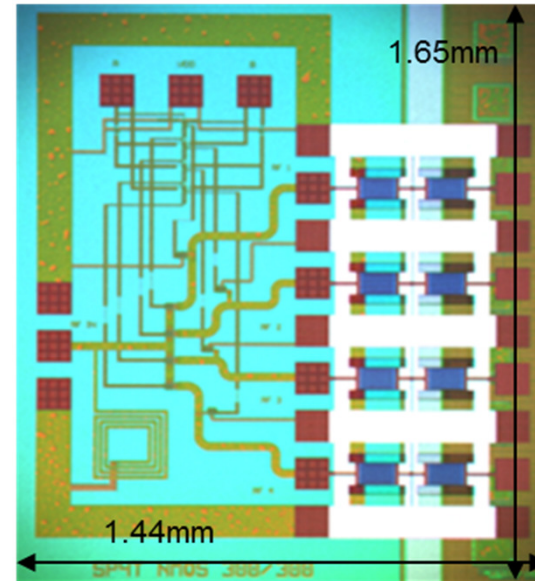
➤ *Significantly Reduces Number of Switched Acoustic Resonators*



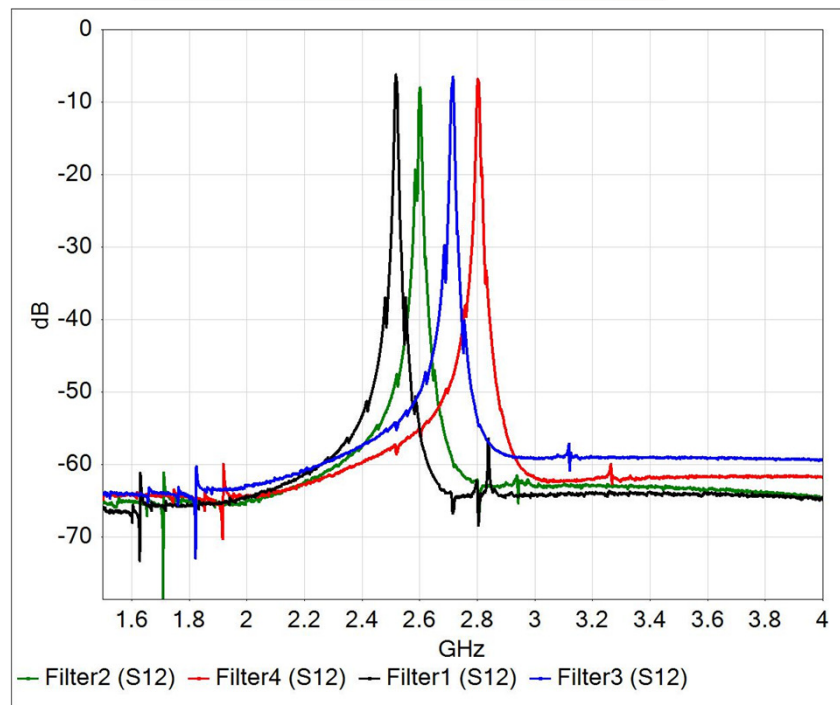
Tunable Filter Model and
Simulated Response

Conclusions

- *Future Adaptive and Cognitive Radios Require Tunable Center Frequency and Bandwidth Filters*
- *Acoustic Filters Are Desirable Because of Their Small Size and High-Q in Common RF Bands*
- *The Fundamental Resonator Figures of Merit (k_t^2 , Q) Limit Performance Metrics Such as Bandwidth, Tuning, and Insertion Loss*
- *Current Acoustic Resonator Technologies Can Achieve Tunable Bandwidth and Switchable Center Frequency*
- *New Materials With Higher Coupling Coefficient Will Enable Tunable Center Frequency Acoustic Filters*



S-Band
Switched
Filter Array



Acknowledgments

Sandia wins R&D
Magazine's 2011
R&D100 Award:
"Microresonator
Filters and
Frequency
References"



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Program, DARPA ASP, CSSA and
RFFPGA Programs, Many Others

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Laboratories

