

# Used Fuel Disposition Campaign

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## Interim Storage Container Corrosion Testing at SNL

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Sandia National Laboratories**

**EPRI/ESCP International Subcommittee Meeting  
November 30<sup>th</sup>, 2012**

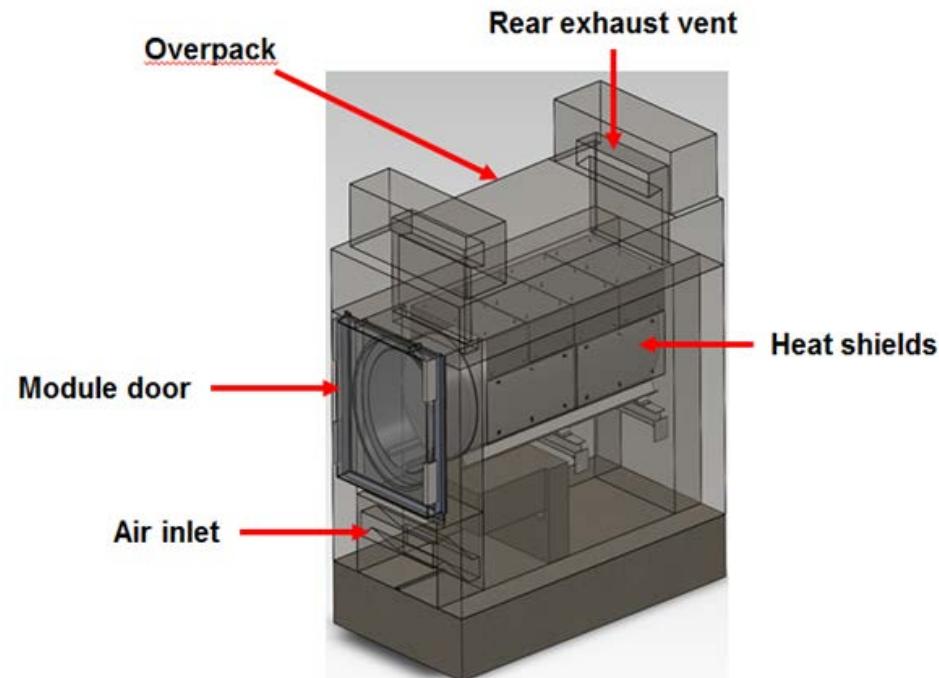
## Goal of test program

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- Understand nature of the deposit chemistries which may exist on the container surface, as well as pertinent environmental conditions
  - Composition
  - Quantity
  - Temperature
  - Dewpoint
- Understand the relevant corrosion degradation mechanisms which may result in the a potential breach of the container
  - Localized attack
  - Stress corrosion cracking

# Characterization of the Conditions on the Surface of a Storage Container

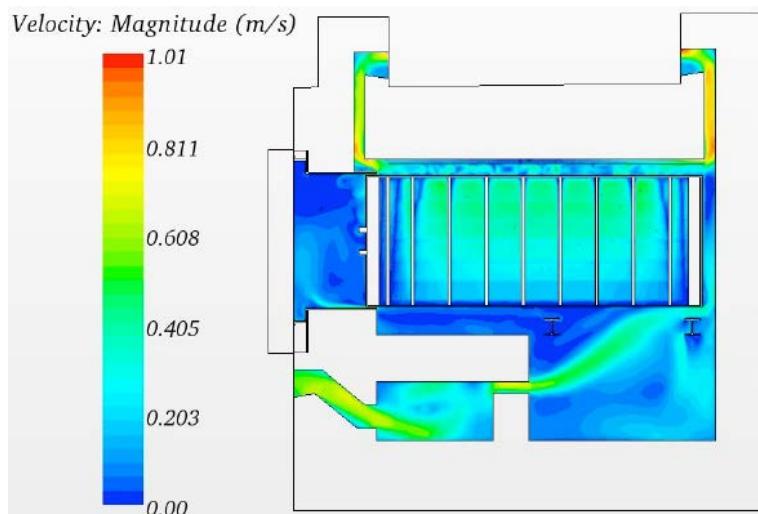
- NRC inspection of the Calvert Cliffs ISFSI performed in June, 2012
- Imaging of two containers, coupled with temperature measurement and surface deposit sampling



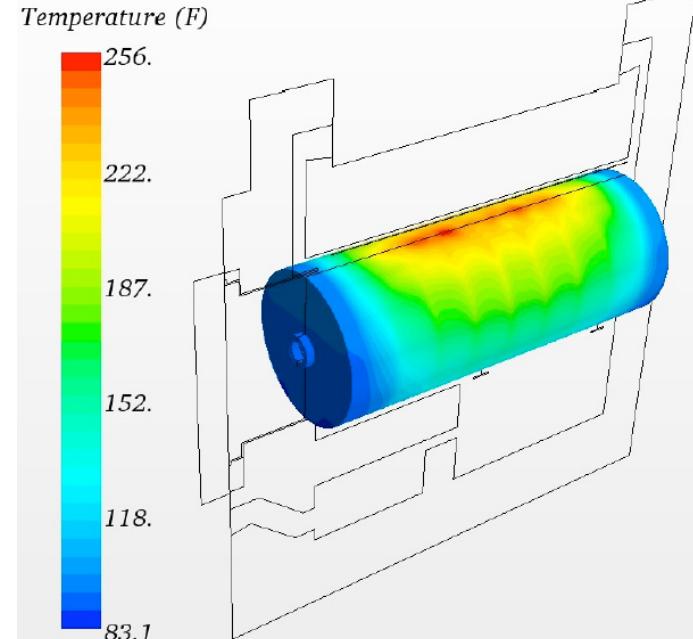
# Parameters Controlling Deliquescence: Temperature

## ■ PNNL modeling

- Calvert Cliffs NUHOMS HSM-15 canister and storage module
- Temperature map of full canister surface, internals (huge temperature range on the surface, corresponding to a huge range in relative humidity)
- Provides ventilation velocities (useful for determining potential salt load)
- Seasonal temperature fluctuations evaluated (correspond to similar-magnitude temperature fluctuations on the container surface)



FCRD-UFD-2012-000344  
Figure 7.1



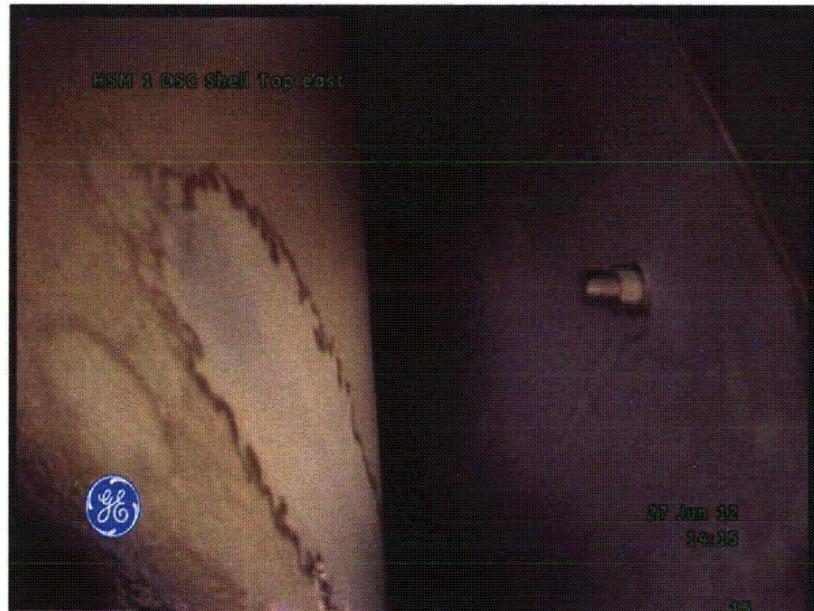
FCRD-UFD-2012-000344  
Figure 7.3

- *However:*
  - Provides snapshots, but does not model full temperature evolution through time.
  - Currently, for only one waste profile (thermal load)

# Quantifying the Composition and Quantity of Surface deposits

## ■ Calvert Cliffs inspection

- SaltSmart device used to acquire surface chloride levels
- Single measurement made at the 0900 location
- 543 mg/m<sup>2</sup> (54.3 µg/cm<sup>2</sup>) for container which was in service for 19 years
- Significant particulate visible on the surface of the container



## Parameters Controlling Deliquescence: Temperature, RH

### ■ Observed temperature range

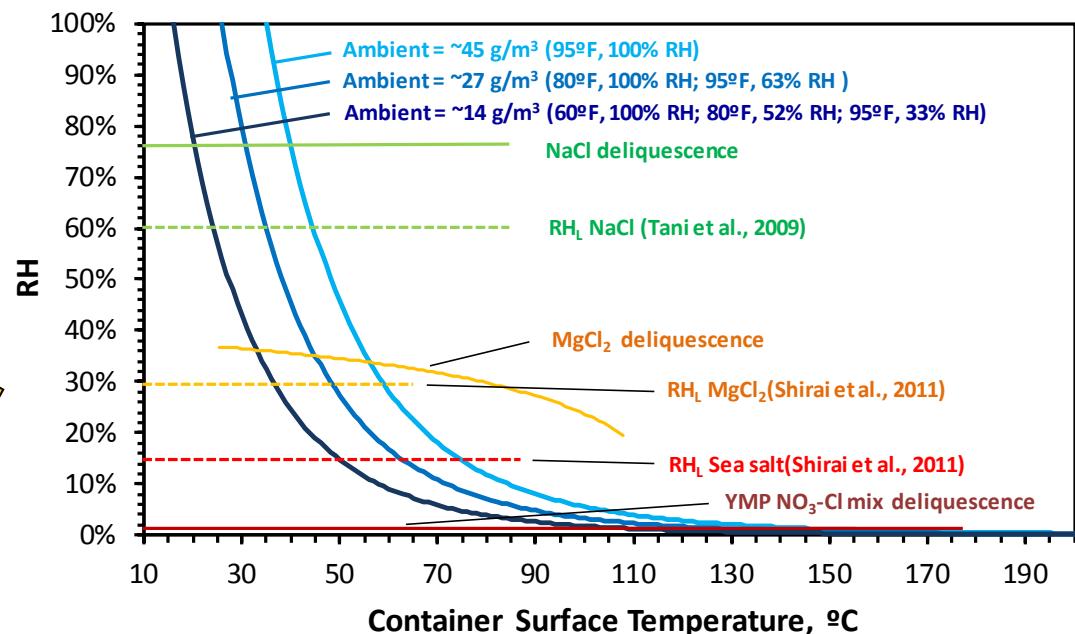
- Temperature range on even a single waste package surface is large.
- Minimum temperatures: ambient or near ambient (for example, 80.6°F on PNNL HMS-15 model)
- Maximum temperatures: >200°C for largest containers (for example, 243°C for HI-STORM 32 PWR container)

*But we don't need to consider the entire temperature range, as depending on the salt compositions and RH, aqueous conditions will only exist over a limited range of temperatures*



### ■ RH at the container surface

- Can be calculated from the ambient RH and air temperature (monitored) and the container surface temperature at a specific location. Will vary with daily/seasonal variations air RH/T and waste package T.



## Is Localized Corrosion Possible Under Atmospheric Conditions?

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- For corrosion resistant materials such as Ni-Cr-Mo-W alloys or many stainless steels, theoretical limitations imply crevice corrosion is unlikely under these conditions
- Available active surface area outside of a potential crevice limits the ability for crevice corrosion to initiate and/or propagate.
  - Relocation of cathode inside crevice does not allow maintenance of the critical crevice solution
    - *Turnbull (NPL), Kelly et al. (UVA)*
  - Limitation of cathodic capacity outside of the crevice
    - *Payer, et al. (CWRU), Kelly et al. (UVA)*

# Work Described in this Presentation

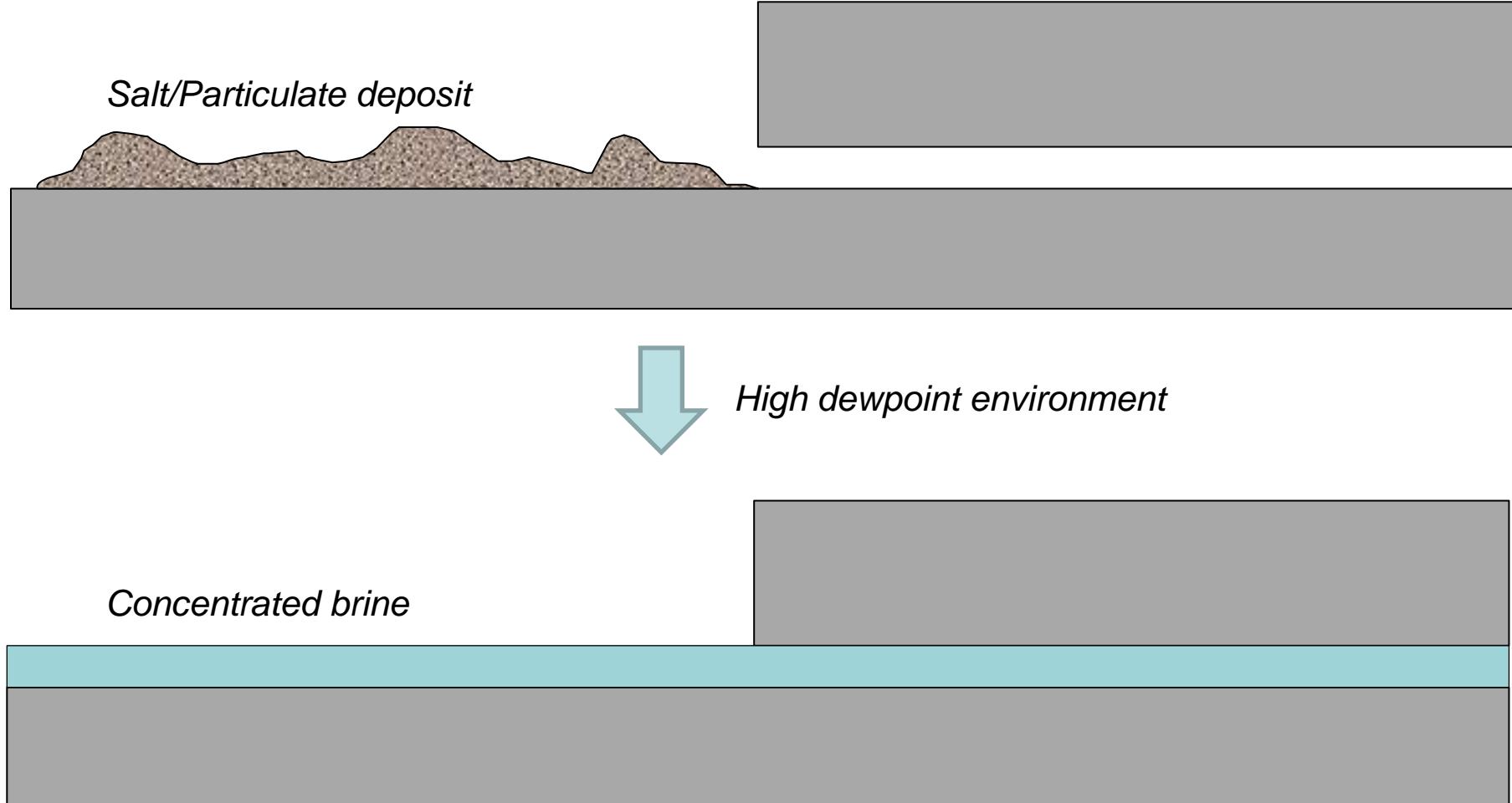
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- Experiments began during previous repository work in order to assess if multi-salt assemblages on the waste package surface could initiate and sustain localized corrosion.
- Secondary goal is to strengthen the corrosion stifling argument
  - Significant support in the form of modeling results which indicate that cathodic limitations will likely dominate
  - Critical need for a dataset which could provide direct support to the stifling argument

**Goal:** Establish if localized corrosion (crevice corrosion) can initiate under deliquescent conditions

- A series of relevant materials has been evaluated
  - Stainless steels used in interim storage applications
  - Alloy 22
  - Inconel 625
  - Hastelloy C276
  - 80:20 Ni:Cr
- Thin film of salt (with known mass loading) deposited on surface, followed by the use of a traditional PTFE coated ceramic crevice former

## Schematic of a Crevice

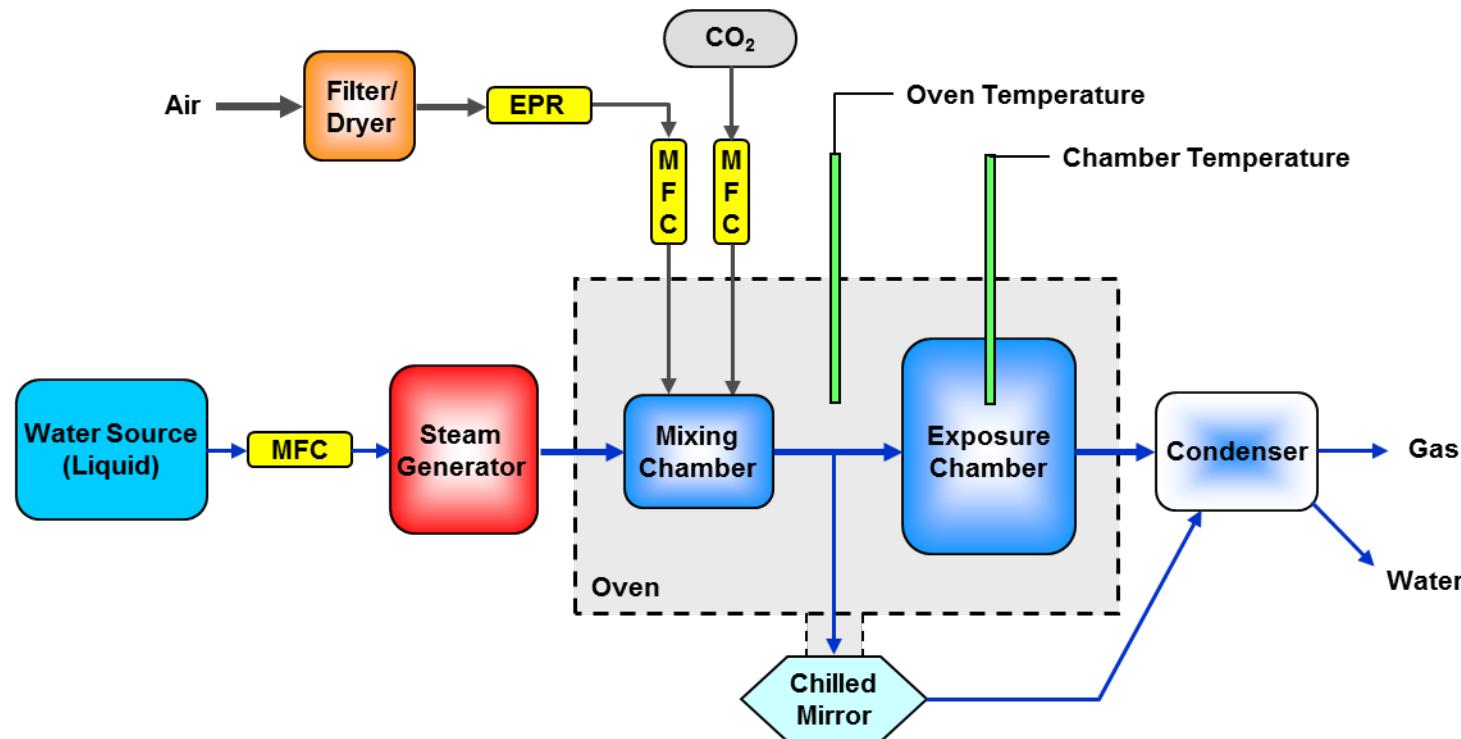


## Environmental conditions under consideration and why

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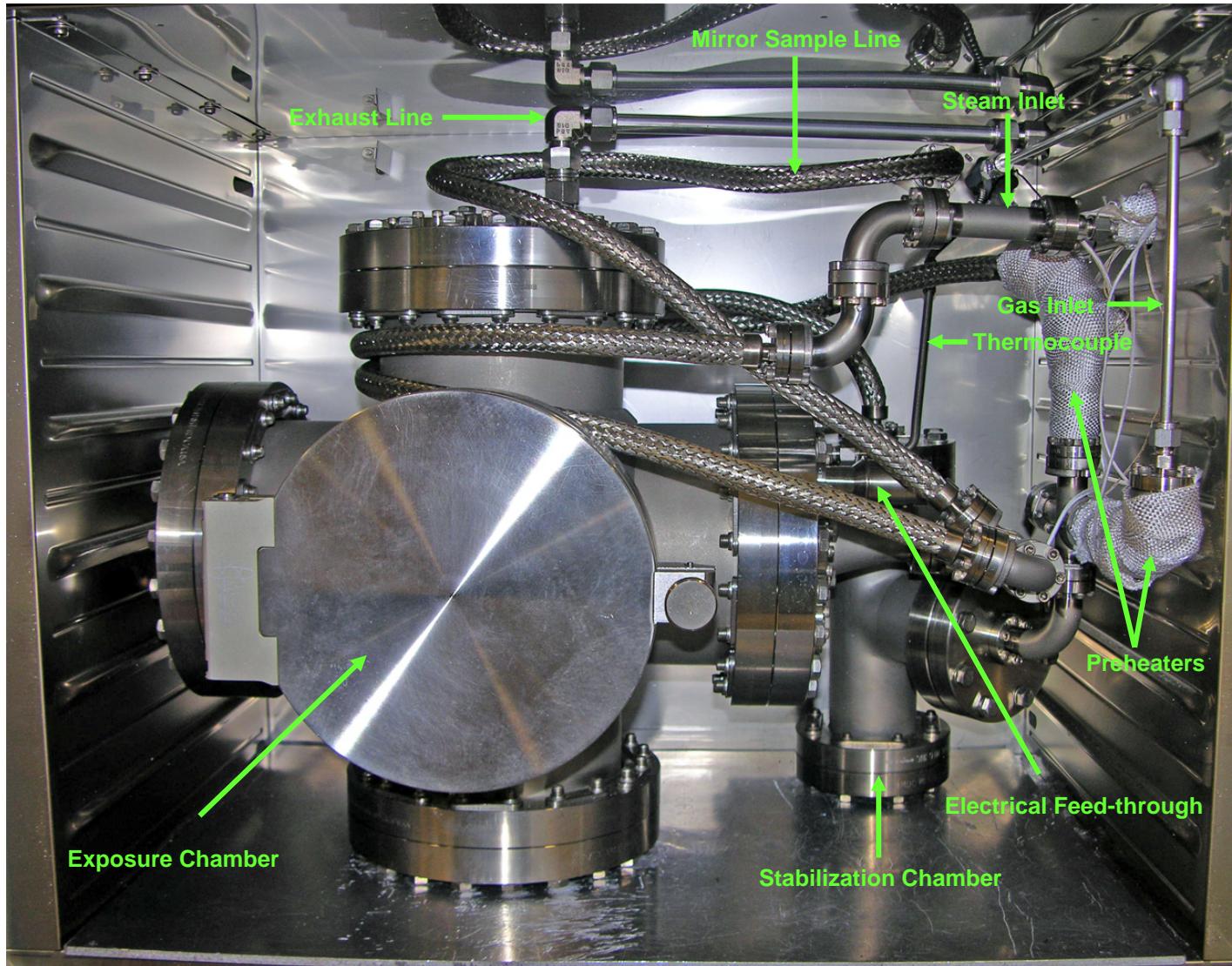
- **Temperature profiles identified via modeling and measurement**
  - Temperatures will begin well above the boiling point of water, then gradually decay over time
- **Heavy surface deposits observed on containers, containing potentially high concentrations of chloride bearing salts**
- **Considerable ongoing work evaluating the composition/nature of deposits anticipated at various storage sites**
- **Clear evidence of moisture intrusion in Calvert Cliffs ISFSI (conditions were dry on inspection, though) – observations at other sites (e.g., North Anna) have revealed considerable water present within the overpack**
- **Variety of conditions possible, ranging from warm and dry to hot with a very high water content in the air**

# Schematic of High Temperature System

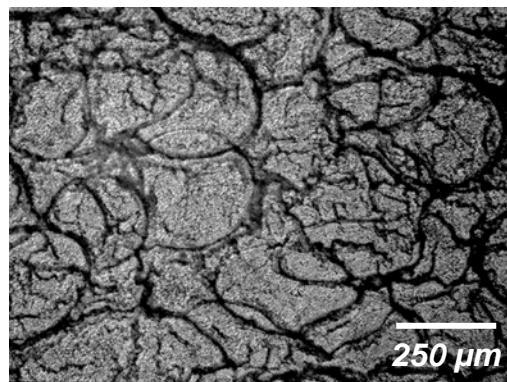


EPR = Electronic Pressure Regulator and MFC = Mass flow controller

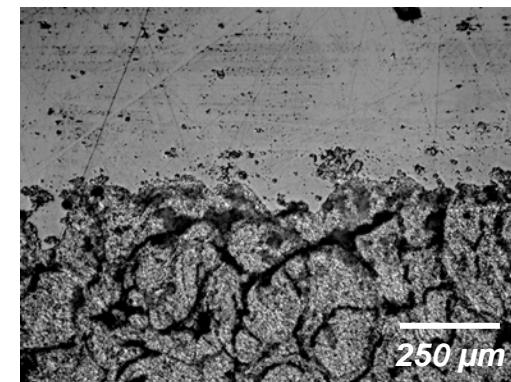
# High Temperature, Controlled Dewpoint System



- Alloy 22, Inconel 625, Hastelloy C276, 80:20 Ni:Cr, 304SS, and 303SS evaluated
- PTFE coated ceramic crevice former torqued to 70 in-lbs, Mirror finish on coupon surface
- Range of salt loadings from 50 to 250  $\mu\text{g}/\text{cm}^2$  of a NaCl-KCl mixture (approx. 1  $\mu\text{m}$  thick)
- $T=105^\circ\text{C}$ ,  $T_d=\sim 94.5^\circ\text{C}$  (pure steam) for test intervals of 100 days



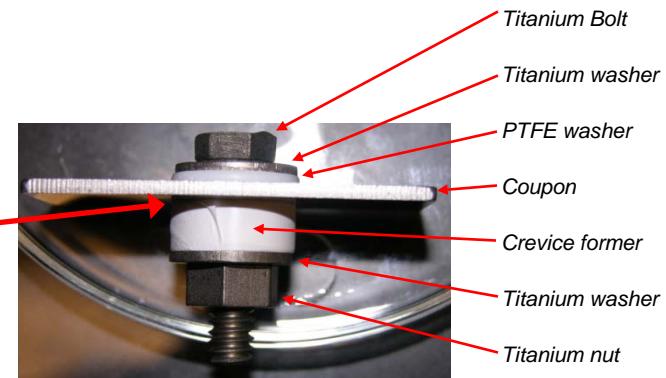
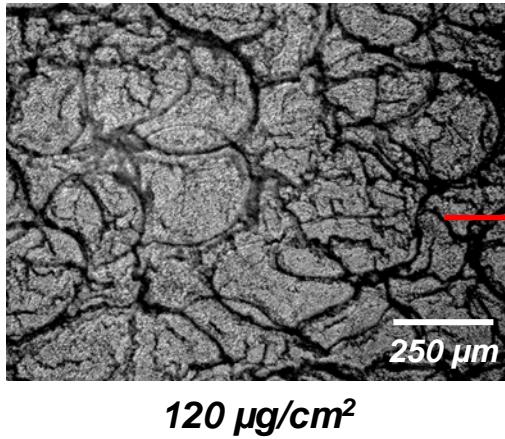
120  $\mu\text{g}/\text{cm}^2$



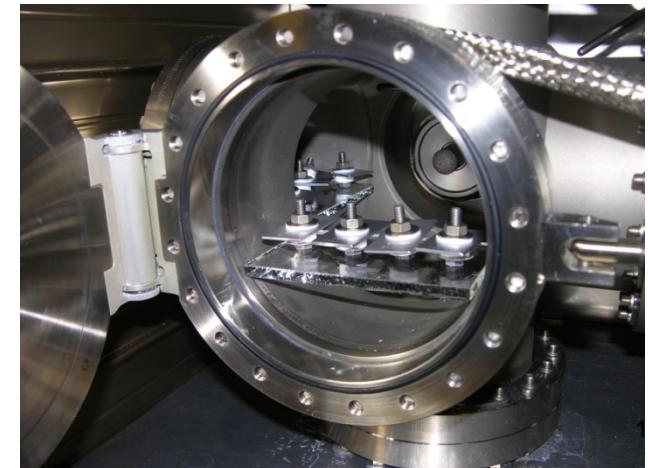
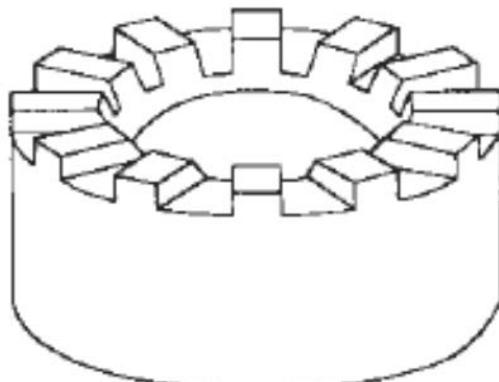
Wiped region

# Dust Deliquescence Testing: Initiation Studies

- Crevice former and salt on one side of coupon which was polished to a mirror finish



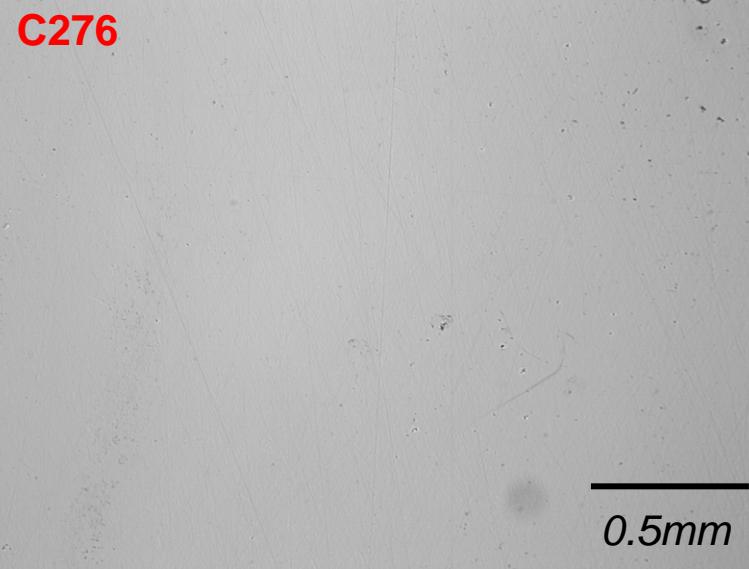
(All titanium hardware electrically isolated from the sample)



Used  
Fuel  
Disposition

# Nickel Alloys in Chloride Brines

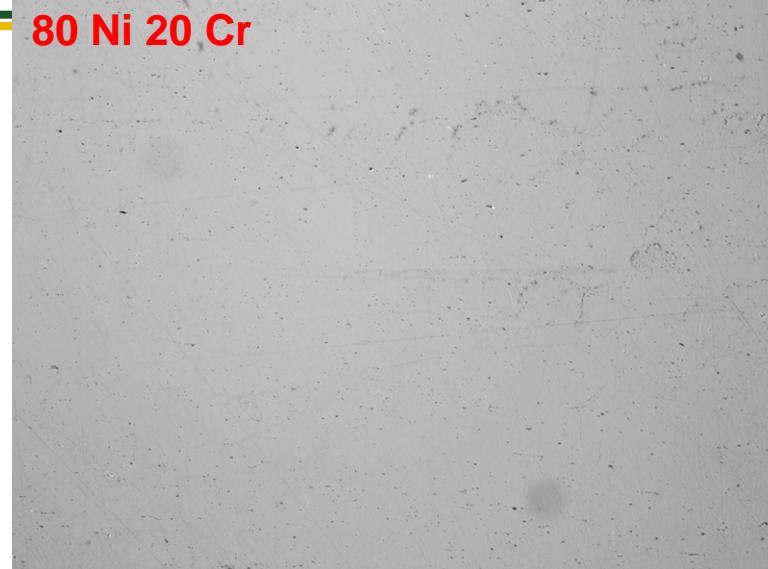
C276



0.5mm

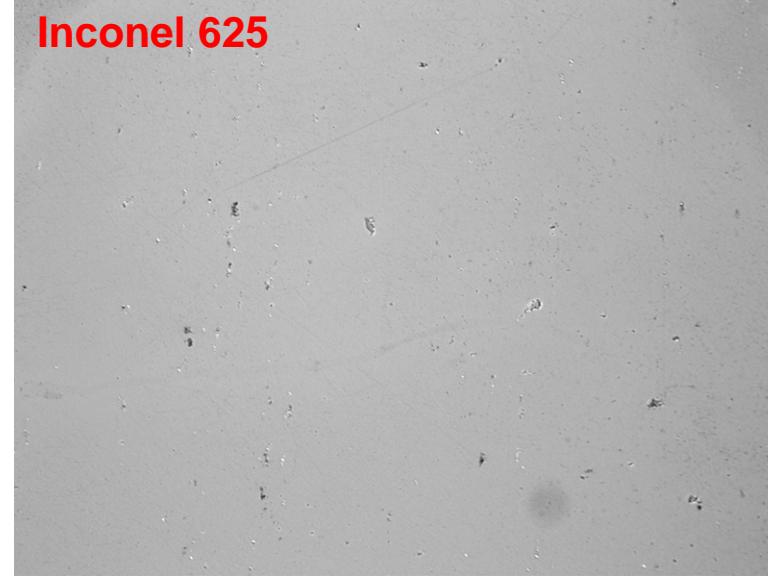
C22

80 Ni 20 Cr



0.5mm

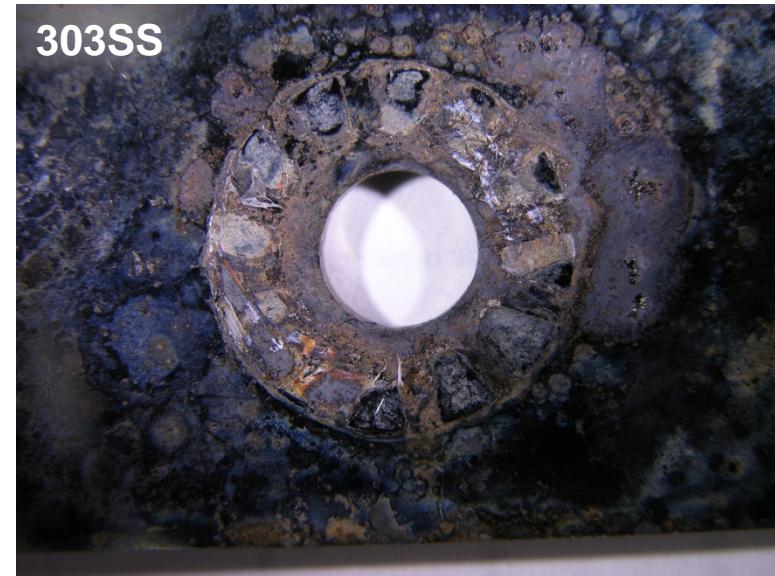
Inconel 625



*No crevice  
corrosion  
initiation*

- Critical need to validate the capability of the technique to support the initiation and propagation of crevice corrosion in susceptible materials. (NWTRB, 2010)
- At the time work was focused on the behavior of Ni-Cr-Mo alloys – it was suggested that the incorporation of a very susceptible material be explored to see if attack was possible for a known problem material
- Experiments initiated on 303SS
  - Free machining stainless steel with elevated sulfur content
  - Material is extremely susceptible to localized attack (pitting and crevice corrosion)

*To alleviate concern that technique was not capable of supporting crevice corrosion even on highly susceptible materials, 303SS was introduced into the test matrix*

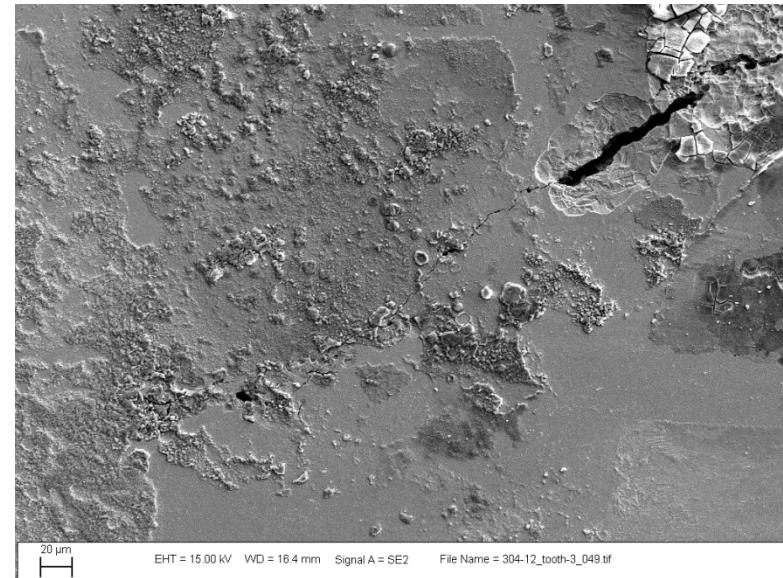
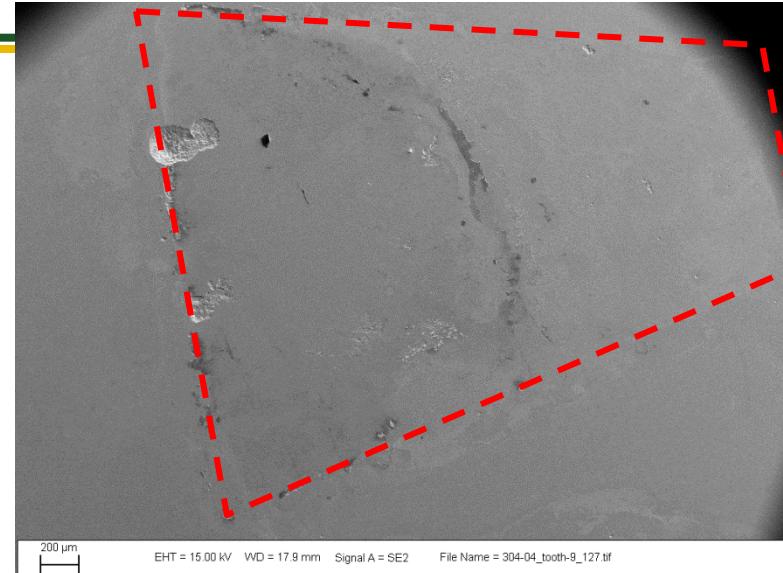
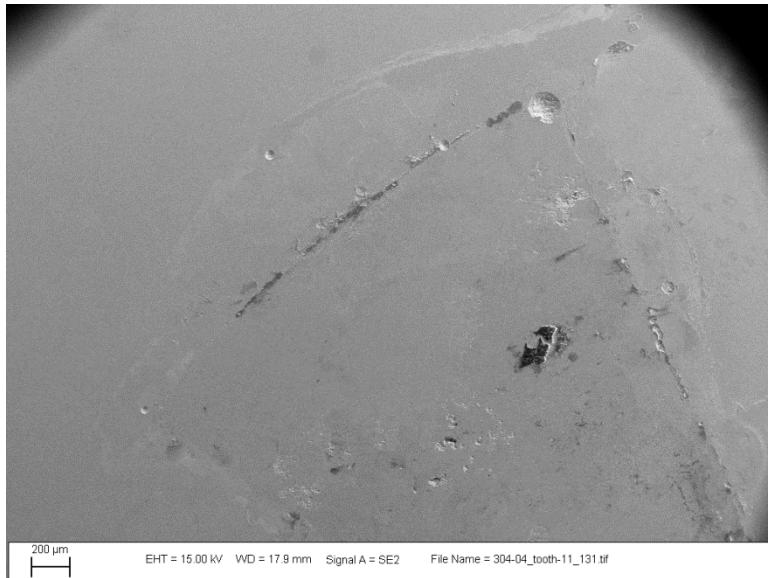


*Evaluation of the impact of salt loading was pursued for 304SS (difficult to interpret 303SS results as material was too active) to explore stifling argument*

- 303SS too susceptible – significant attack wherever salt mixture was present
- Three different mass loadings evaluated (50, 100, and 200  $\mu\text{g}/\text{cm}^2$ )
- Initial experiments performed for a period of 100 days
  - Initiation observed at all mass loadings
  - Extent of attack correlated with mass loading
- Samples exhibited SCC in a number of cases, but did not correlate with mass loading

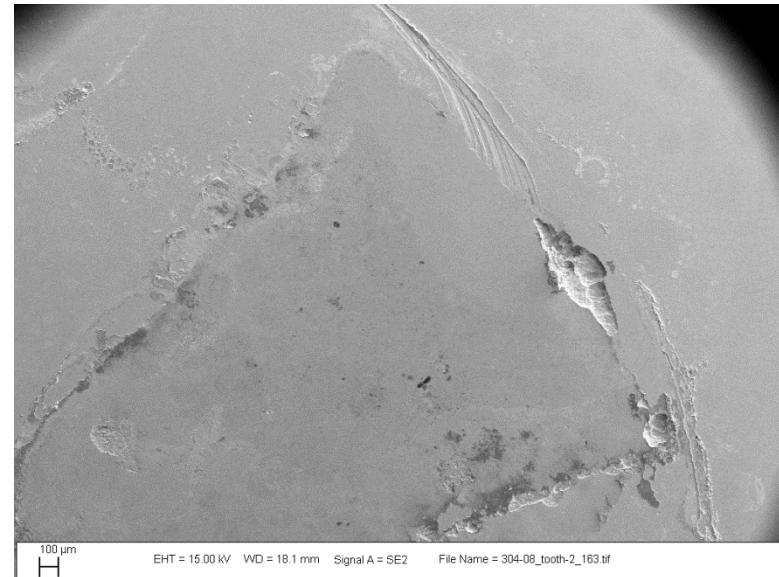
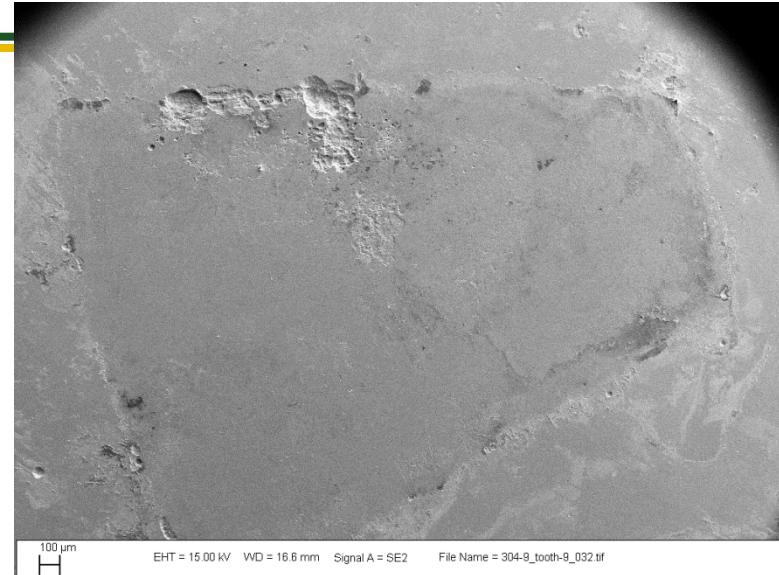
# Impact of Salt Loading on 304SS 50 $\mu\text{g}/\text{cm}^2$

- At least small sites on most teeth
- Cracking observed on some teeth
- Propagation limited in extent



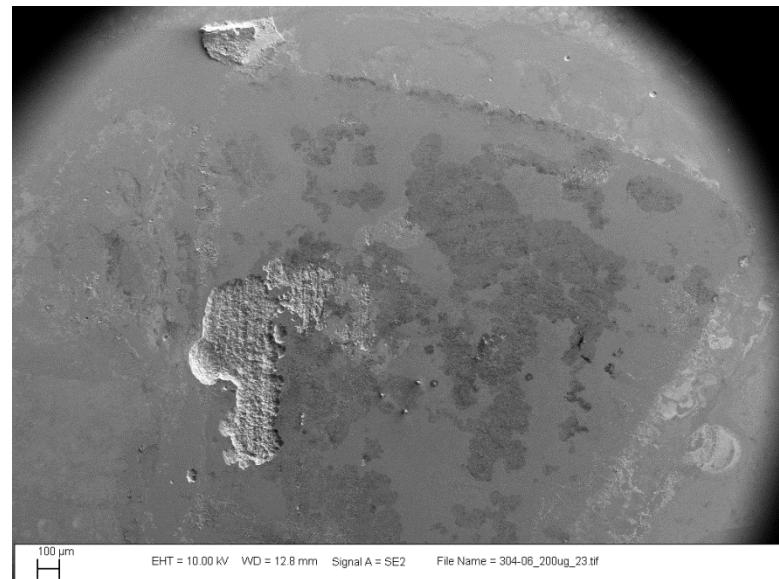
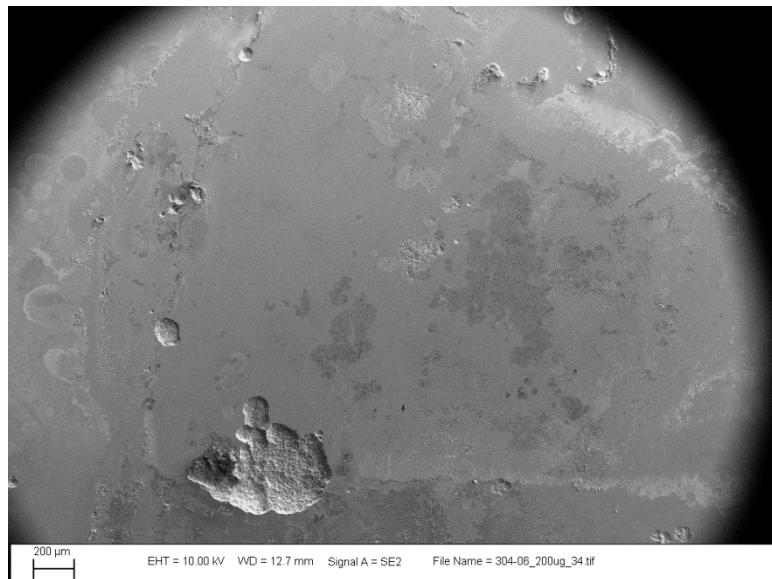
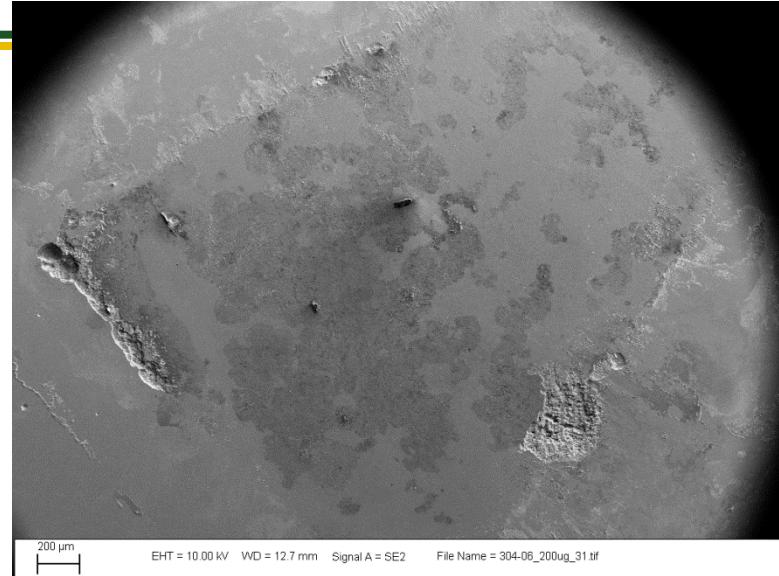
# Impact of Salt Loading on 304SS 100 $\mu\text{g}/\text{cm}^2$

- *More teeth where crevice corrosion initiated*
- *Typically multiple sites on teeth where crevice corrosion initiated*
- *Propagation more extensive (further/deeper)*



# Impact of Salt Loading on 304SS 200 $\mu\text{g}/\text{cm}^2$

- *Crevice corrosion initiated on most teeth*
- *Typically multiple sites on teeth where crevice corrosion initiated*
- *Propagation more extensive (sites tended to be larger/deeper)*



## Is There a Time Dependence for Crevice Corrosion Under Deliquescent Conditions?

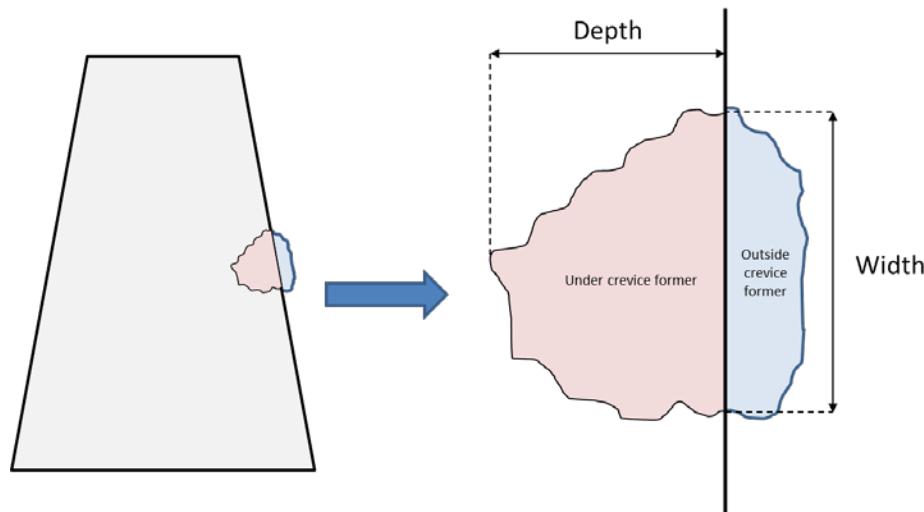
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- While the experiments at 100 days do illustrate that localized attack is possible for a variety of relevant chloride surface concentrations, they do not answer our initial question/concern
  - Does initiation time correlate with mass loading?
  - Is the likelihood of initiating localized corrosion at a given site a function of the quantity of brine present on the surface?
  - Is it that the extent of damage is a result of the mass loading (i.e., attack advances and stifles) or is it that the rate of attack is a function of the mass loading?

- **Same mass loadings and material as in longer time period experiments**
  - 304SS, polished to a mirror surface to simplify surface inspection
  - PTFE coated ceramic crevice former, torqued to 70 in-lbs
  - 50, 100, and 200  $\mu\text{g}/\text{cm}^2$  of a NaCl/KCl mixture
  - Material deposited using airbrush technique using a methanol carrier
- **Environmental conditions**
  - Temperature of 100-102°C
  - Pure steam environment (dewpoint equal to boiling point of water)
- **Multiple time intervals to build on 100 day experiments**
  - 7, 14, 25, and 50 days
- **Data analysis is proving to be problematic**
  - Large number of areas to quantify
  - Difficult to assess size/shape/depth of sites

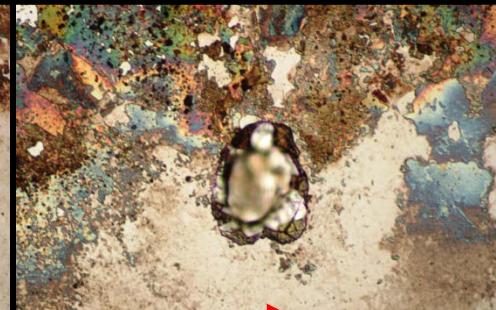
## Optical Characterization of Sites

- Quantify the number, size, and shape of all crevice sites initiated on 4 representative teeth from each sample



*Quantitative measurement of the width and depth beneath crevice former for each site*

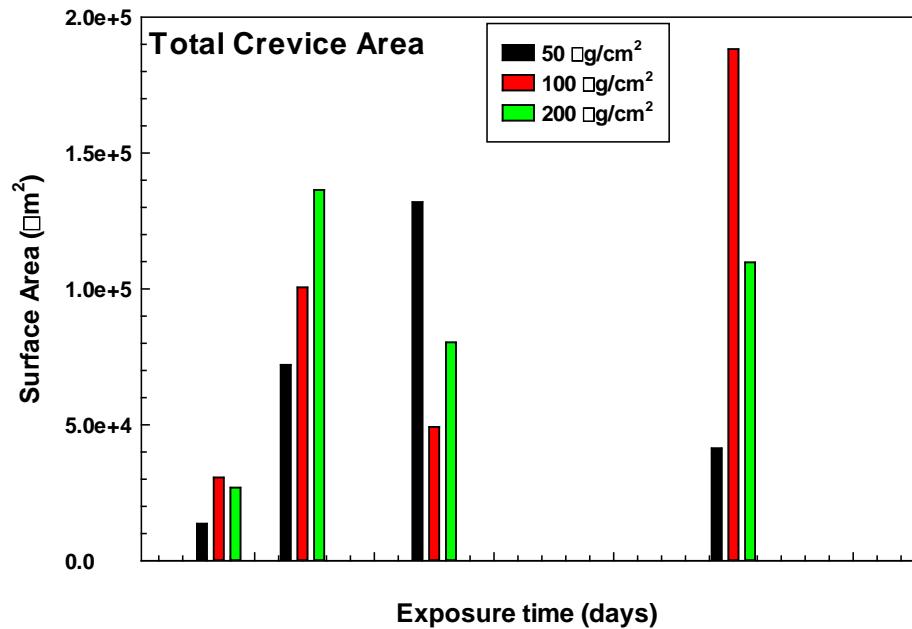
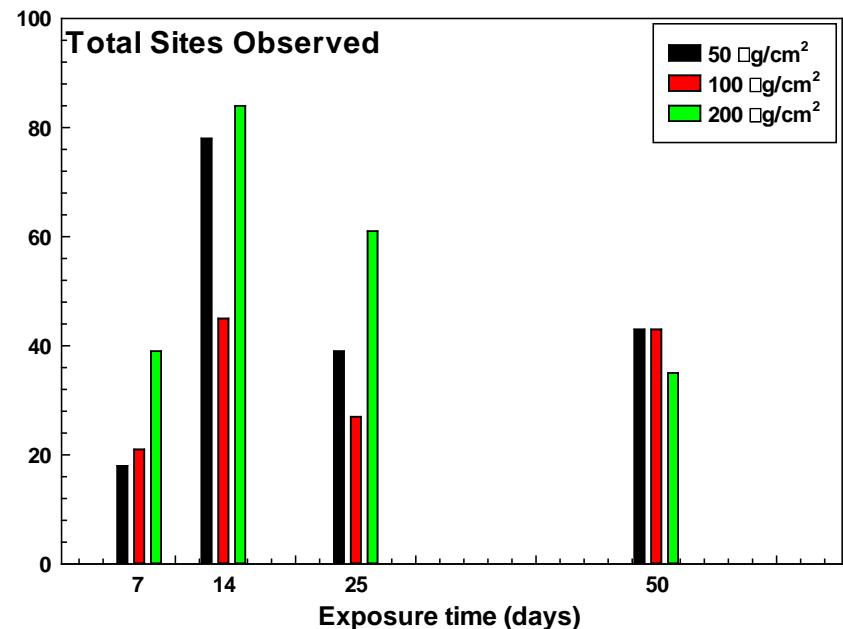
*Qualitative assessment of the degree of penetration into the sample surface for each site*



Shallow

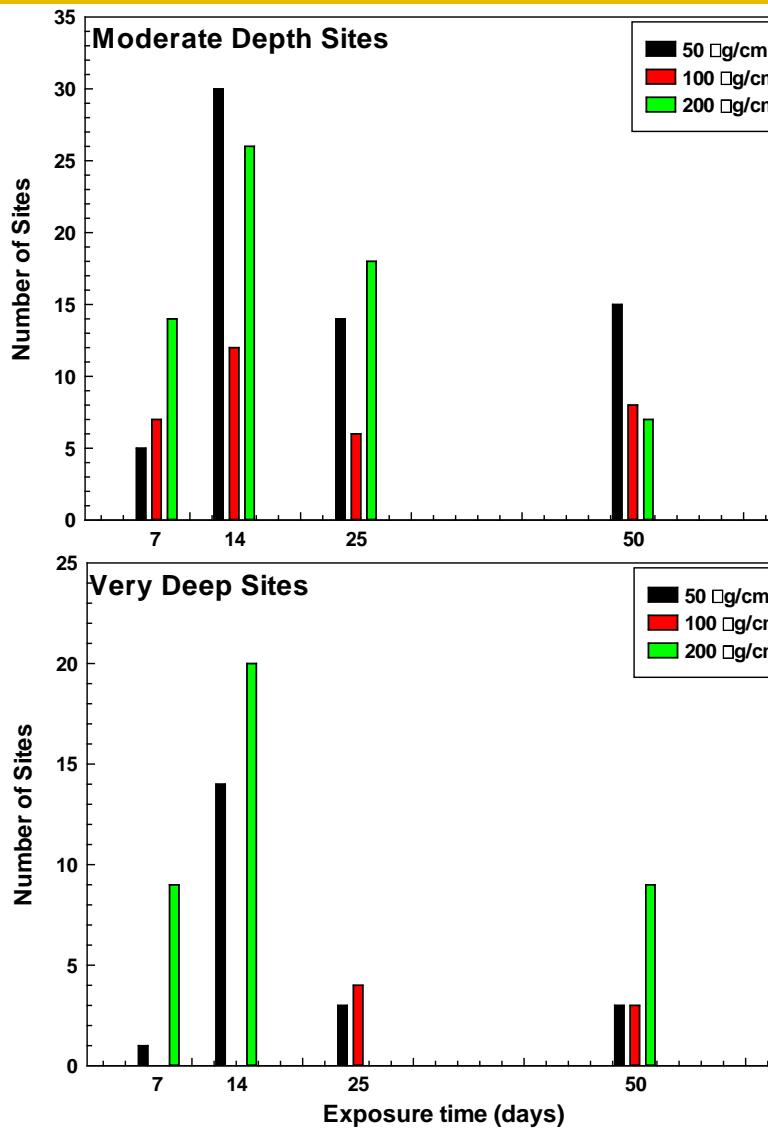
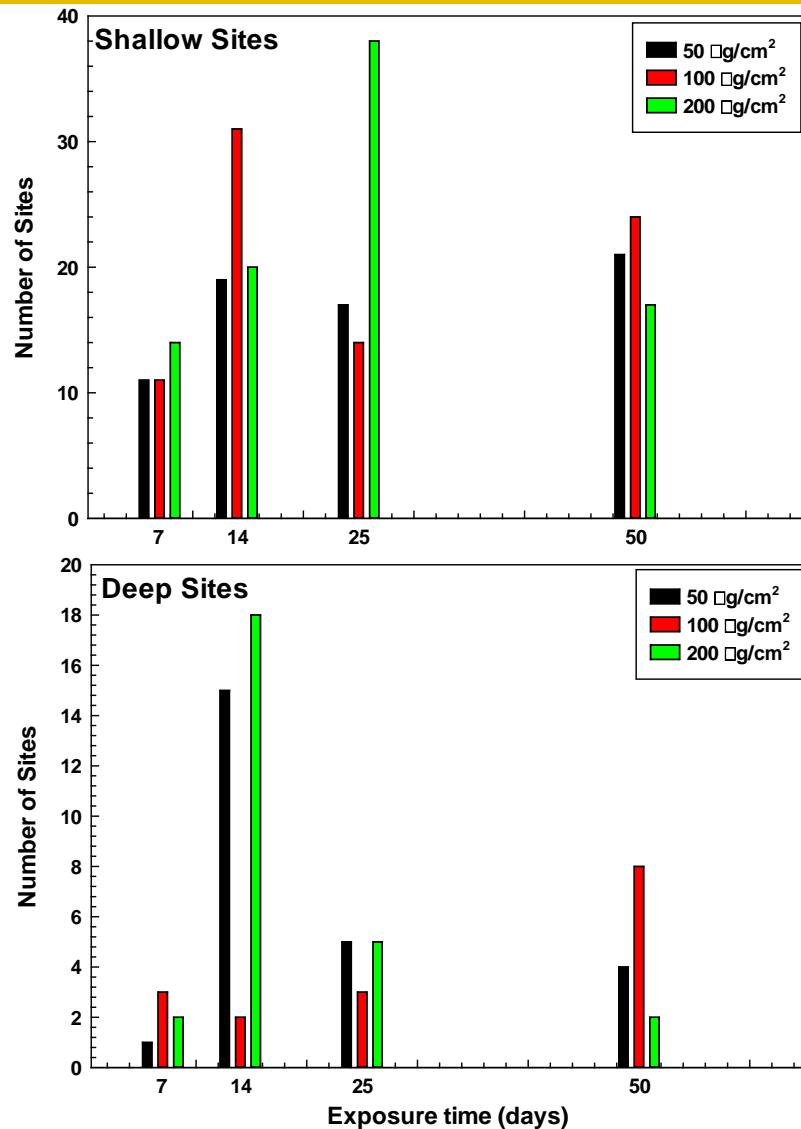
Very Deep

# Total Number and Surface Area of Sites (Summed Over 4 Crevice Teeth)



- Number density and overall surface area of sites appears to increase and stabilize after 14-25 days (but data is too sparse to be conclusive)

# Number of Sites of Each “Depth” as a Function of Time



## Summary

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- Containers for both interim storage and long term disposal will be under environmental conditions where salt particulates will be deposited that are capable of forming a brine at elevated temperature and humidity.
- Information from the literature suggests that localized corrosion under conditions where limited reactant is present should be difficult due to limitations in the cathodic capacity
- Tests at moderate temperature with a chloride rich brine did not result in crevice corrosion initiation for a variety of Ni-Cr-X alloys
- Crevice corrosion initiation was observed on both 303 and 304SS under moderate temperature, chloride rich brines
- The extent of attack was characterized for 304SS and was found to correlate with the quantity of salt deposited on the metal surface prior to the experiment.

## Conclusions

- Ni-Cr-X alloys are resistant to crevice corrosion initiation where limited reactant and a thin electrolyte layer is present, consistent with assertions in the literature
- 304 and 303 SS were susceptible to crevice corrosion initiation
- The extent of damage on 304SS roughly correlated with the quantity of reactant present
  - Number of sites seemed to be stable after a short time period
  - Surface area roughly correlated with mass loading
  - Need more data...
- Results suggest that crevice corrosion will stifle under conditions where limited reactant is present, presumably due to cathodic limitations or consumption of the reactant

## Acknowledgements

### At Sandia National Labs

- Sam Lucero – Salt deposition and experimental setup
- Alice Kilgo – Surface preparation
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### NWTRB

- David Duquette, Ron Latanison – Fruitful technical discussions