

Tunable InP Ring Resonators

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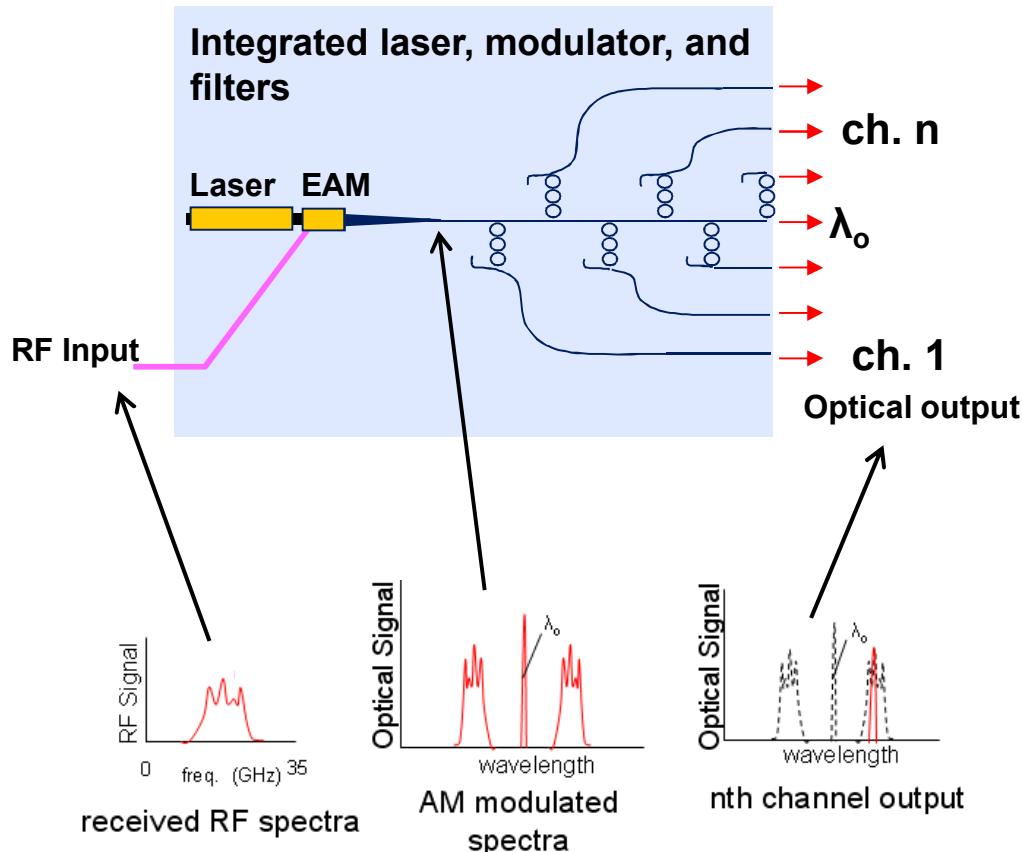
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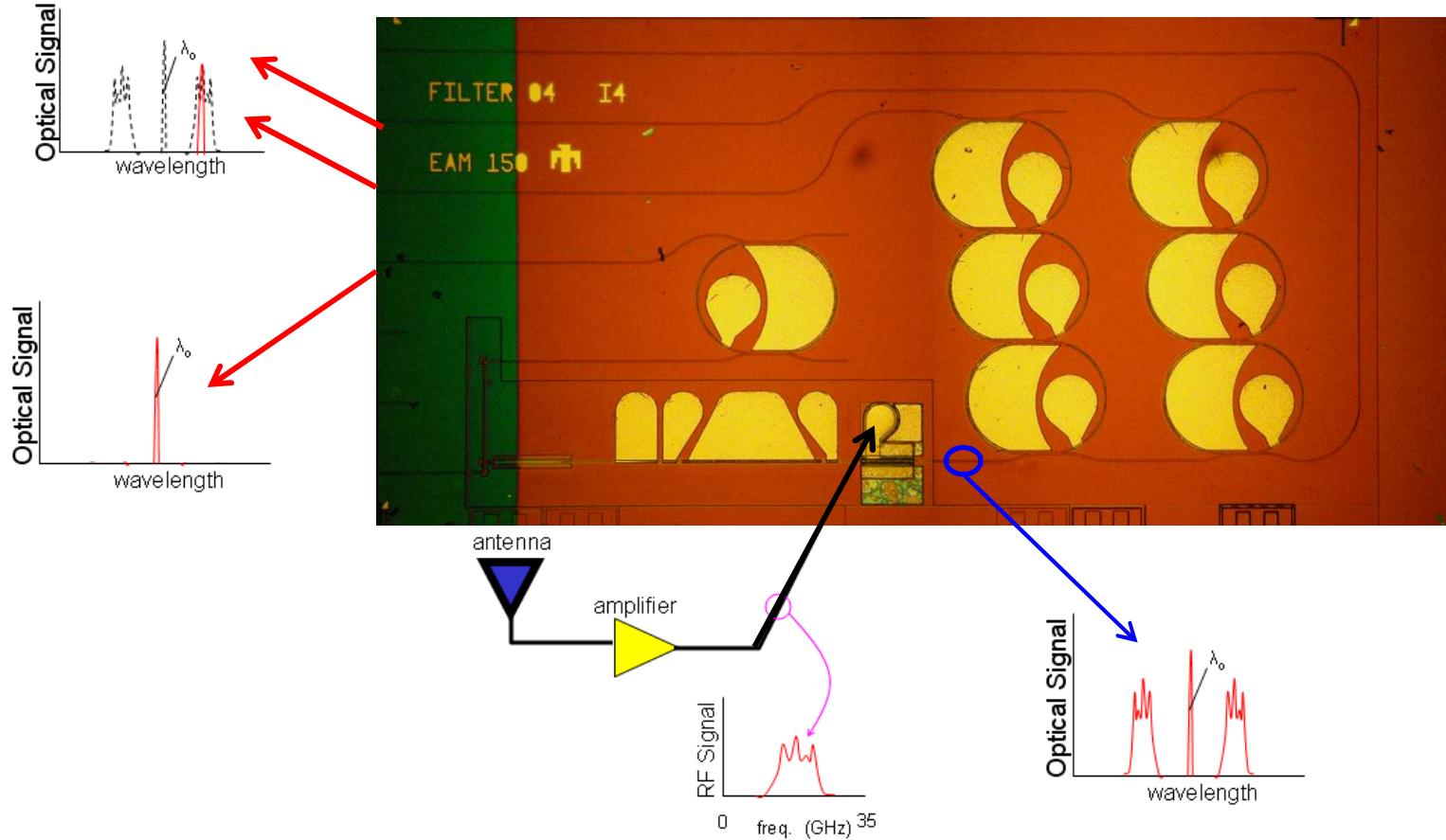
February 7, 2013

Motivation



- Analyze an RF signal for frequency content
 - Filter outputs are spectral power density integrated over the filter bandwidth
- Monolithic integration with active components such as lasers and modulators enables compact, highly functional photonic integrated circuits (PICs)

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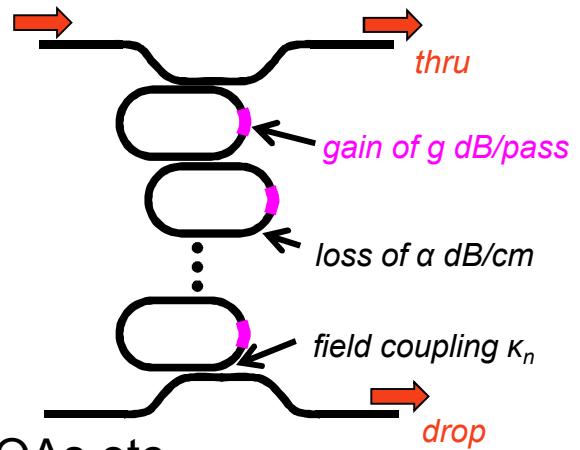


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Motivation

- Active ring resonators offer:
 - Wavelength selectivity
 - Compact size
 - Low, or zero, back reflection
 - Monolithic integration with lasers, modulators, SOAs etc.
 - Gain elements can be used to compensate for waveguide losses
- Design Considerations:
 - Bandwidth determined by:
 - Coupler strength and optical loss
 - Filter profile defined by:
 - Coupler strengths and number of rings and internal net loss
 - Extinction ratio influenced by:
 - Noise from optical amplifiers and optical loss
 - Tunability effected by:
 - Size of tuning section and induced loss

→ **Loss, couplers, and optical gain needs to be tightly controlled**



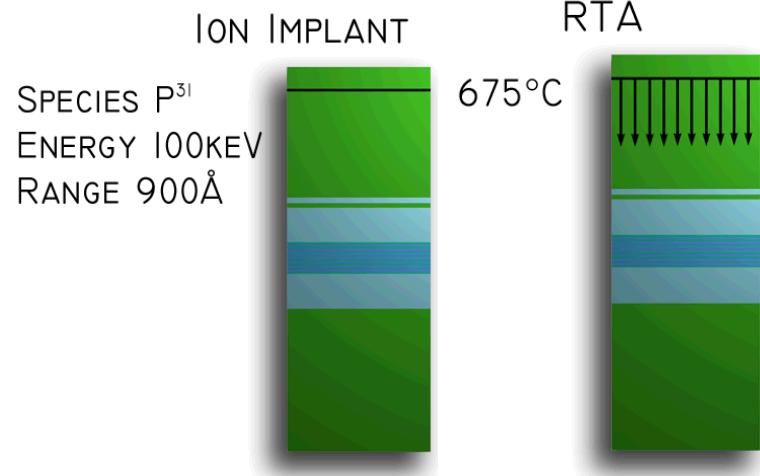
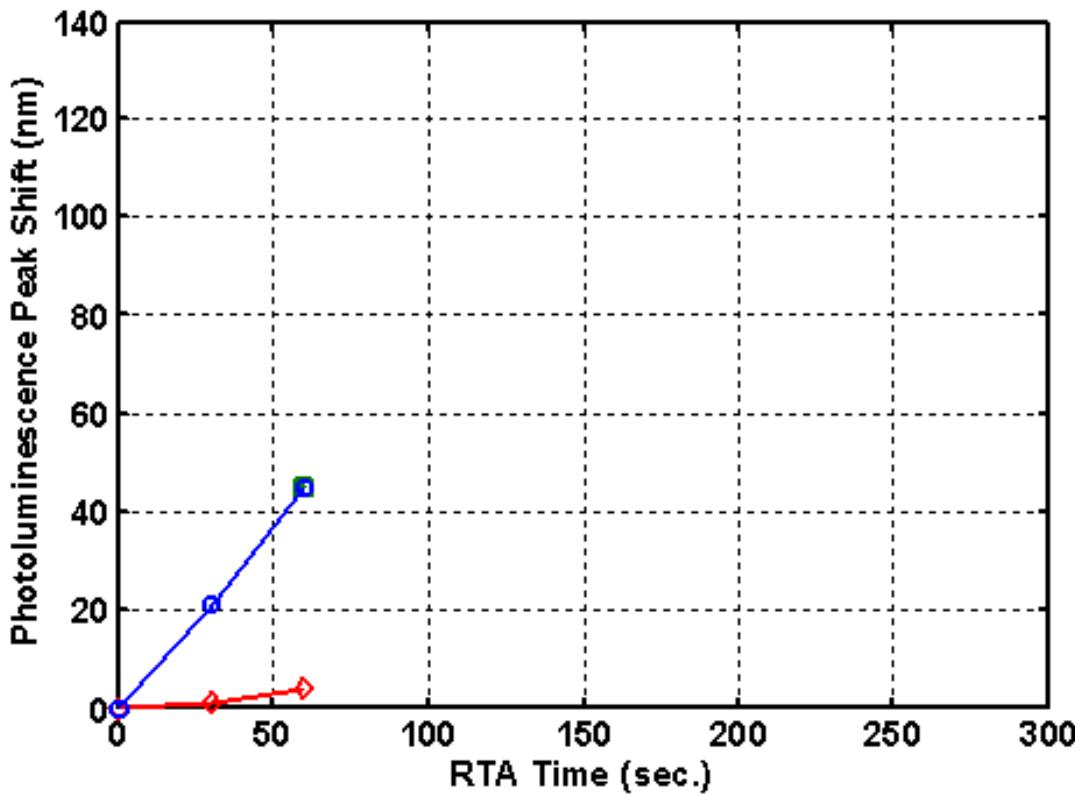
Approach



- Couplers designed for 1-2 GHz linewidth
 - Fractional coupling power of 6% for both couplers
- Integrated 60- μ m-long SOAs in each ring
 - Minimize loss through filter
 - Active/passive integration achieved with quantum well intermixing
 - Length and total gain designed for low noise

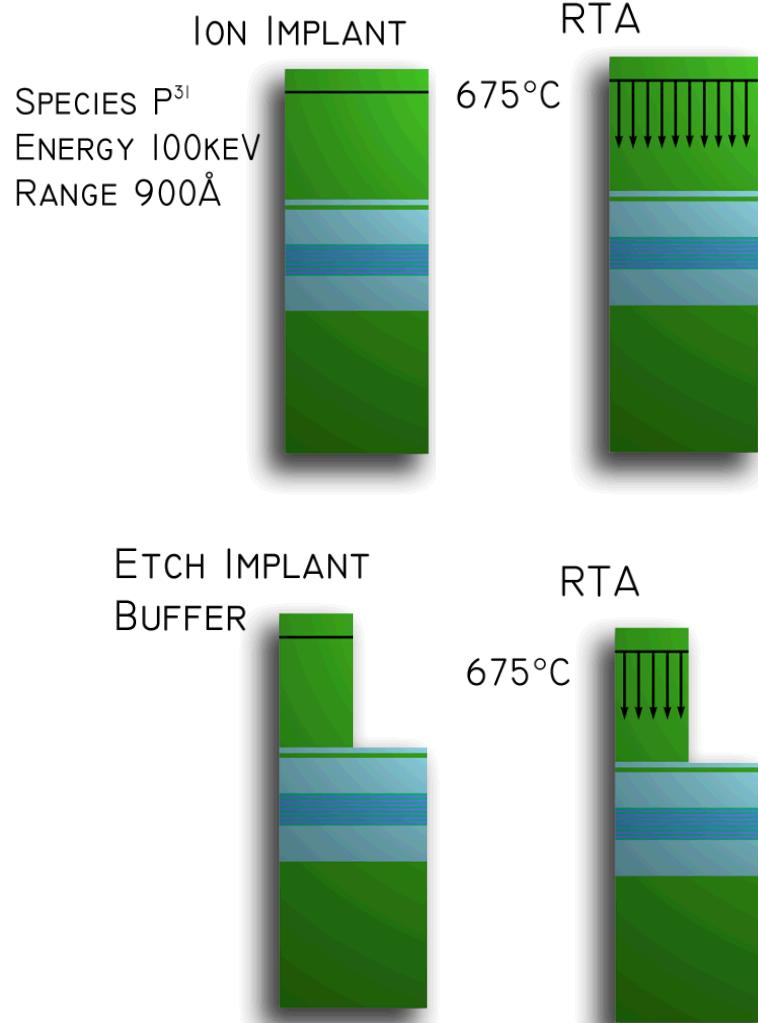
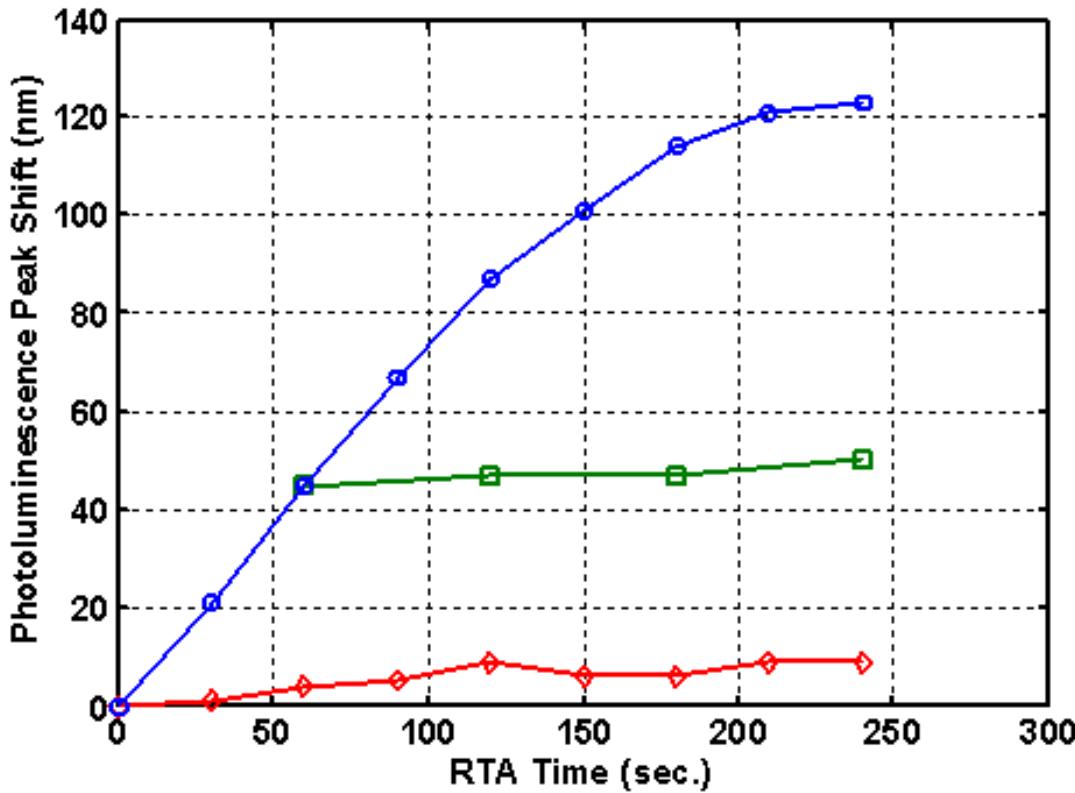
Monolithic Integration Platform

- Quantum well intermixing
 - Metastable interface between well/barrier
 - Add catalyst to enhance interdiffusion
 - Reshaping increases the energy level
 - Reduces the bandgap wavelength
 - Capable >2 bandedges with same epitaxial base



Monolithic Integration Platform

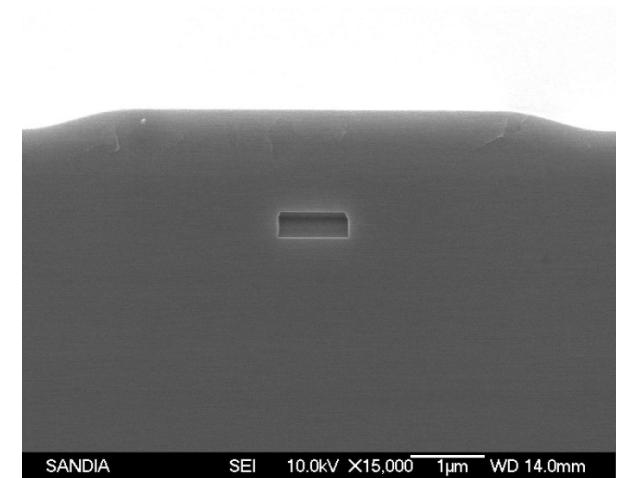
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Buried Heterostucture Waveguides

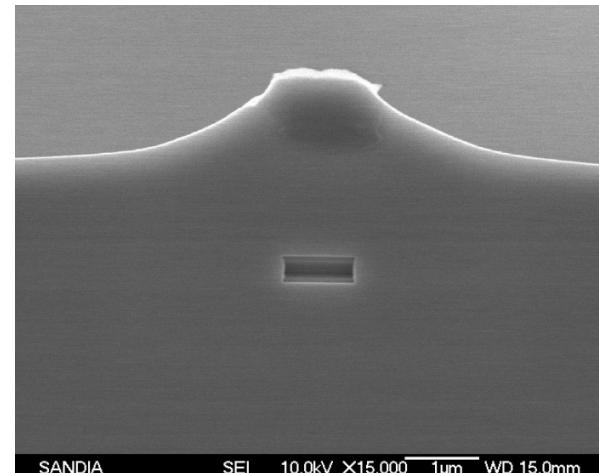
- Waveguide definition process
 - ASML projection stepper
 - 0.6 μm resolution
 - Dry etch
 - MOCVD Regrowth
 - InP cladding
 - InGaAs contact layer
- Buried heterostucture advantages
 - Waveguide thickness defined by epitaxial material
 - Semiconductor etch only defines guiding width and coupler gap
 - Devices are essentially not affected by variations in etch depth

Waveguides in [011]



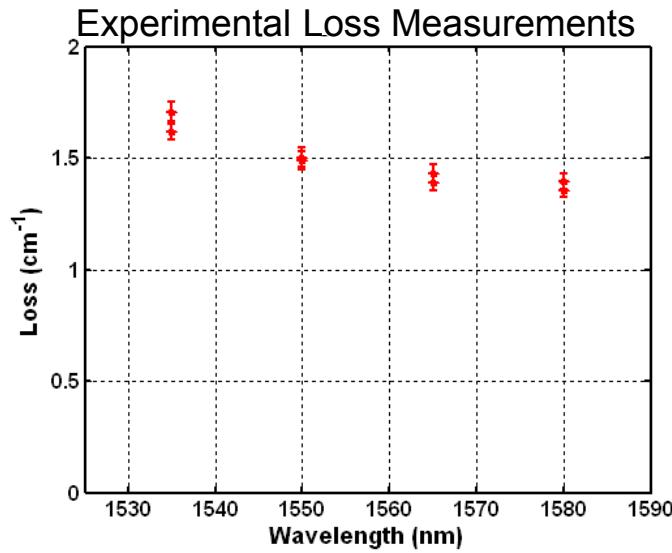
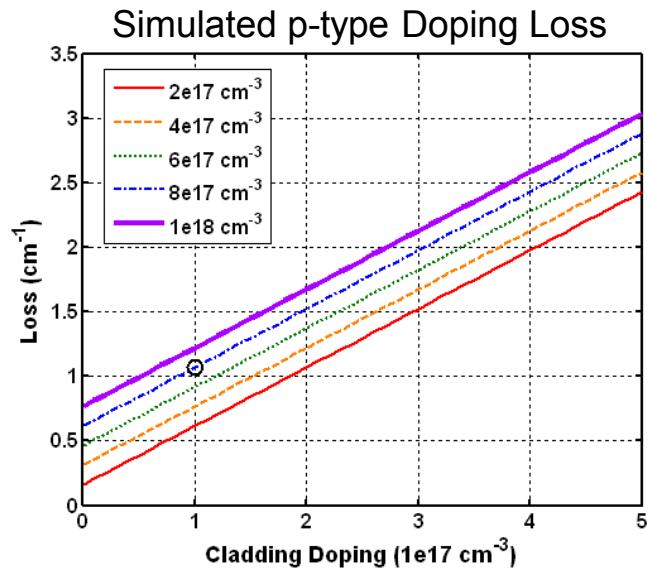
SANDIA SEI 10.0kV X15,000 1μm WD 14.0mm

Waveguides in [011]



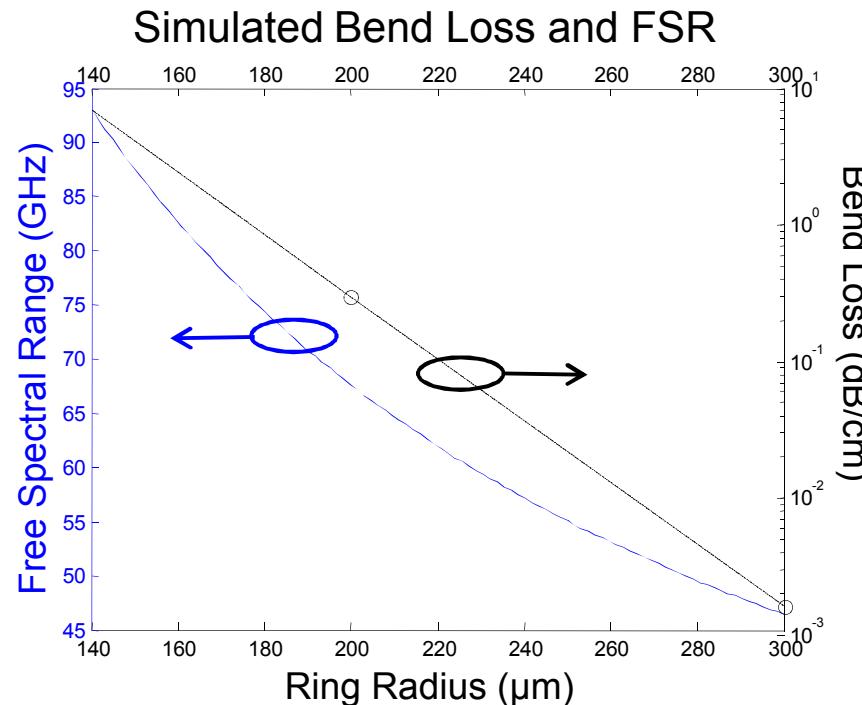
Low Loss Waveguides

- Low loss waveguides
 - Loss and coupling define the bandwidth of the filter
- Scattering and Absorption Loss
 - Modal overlap with InP p-type doping regions is a major source of loss
 - 500 Å doping spike at the regrowth interface
 - Compensates for Si contamination at the regrowth interface
 - Doping of the regrown p-type cladding
 - Waveguide loss was measured using Fabry-Perot cavity measurements
 - 1.5 cm^{-1} at 1550 nm



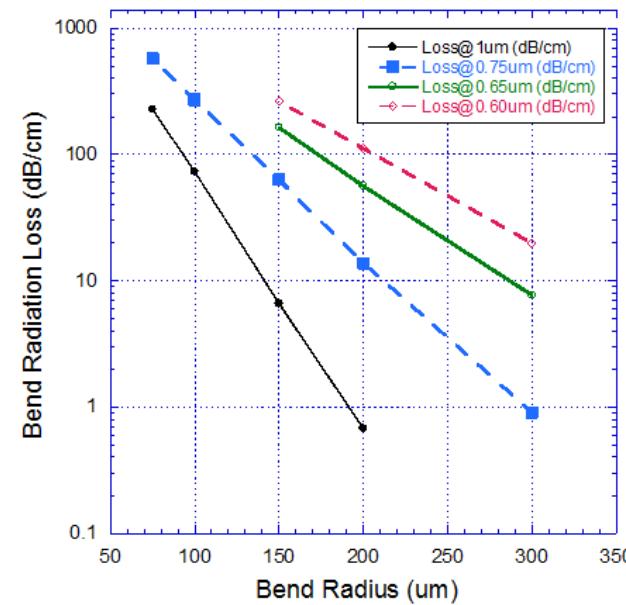
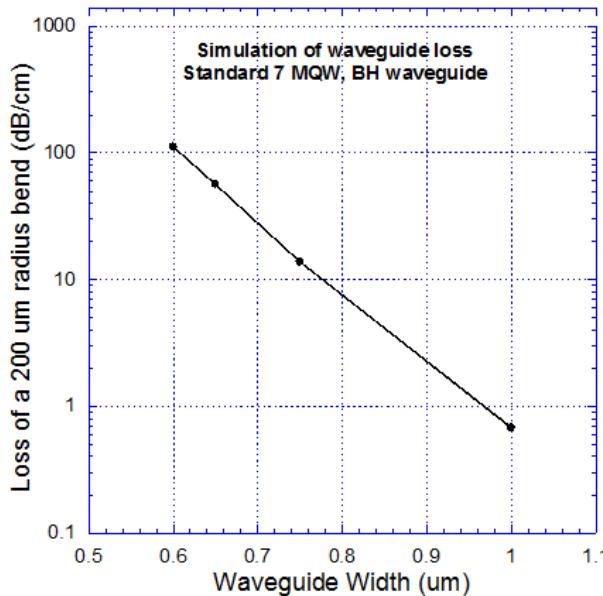
Low Loss Waveguides

- Low loss waveguides
 - Loss and coupling define the bandwidth of the filter
 - Output coupling and waveguide loss
- Bend loss
 - Tradeoff between loss and FSR
 - 200 μm radius for 1 μm waveguide width



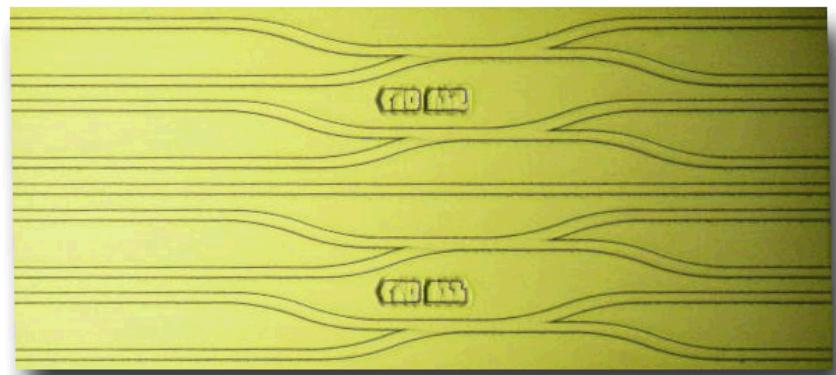
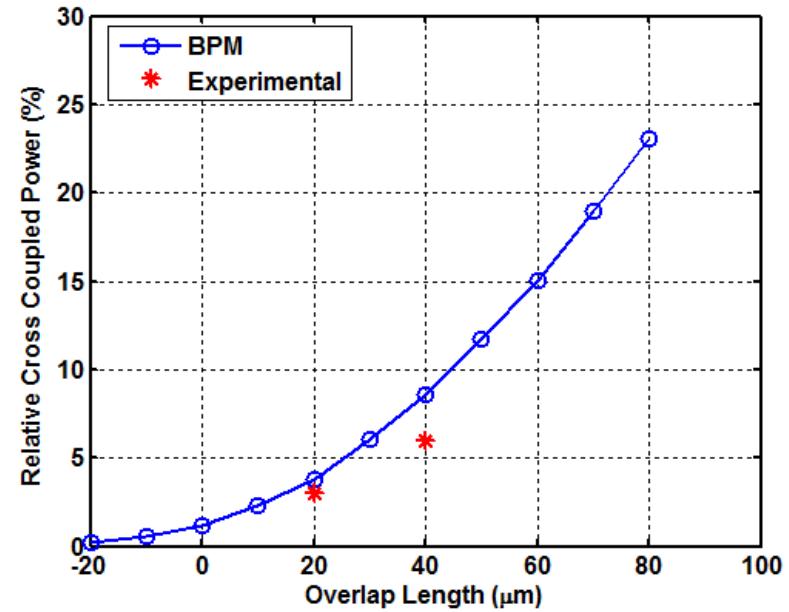
Low Loss Waveguides

- Waveguide width is very important to bend loss
- Lithographic bias can significantly effect bend losses
 - Projection lithography/stepper used
 - Dimensions verified by CD SEM measurements
 - Monitors bias drift over time
 - Done before waveguide etch allowing for rework.



Couplers

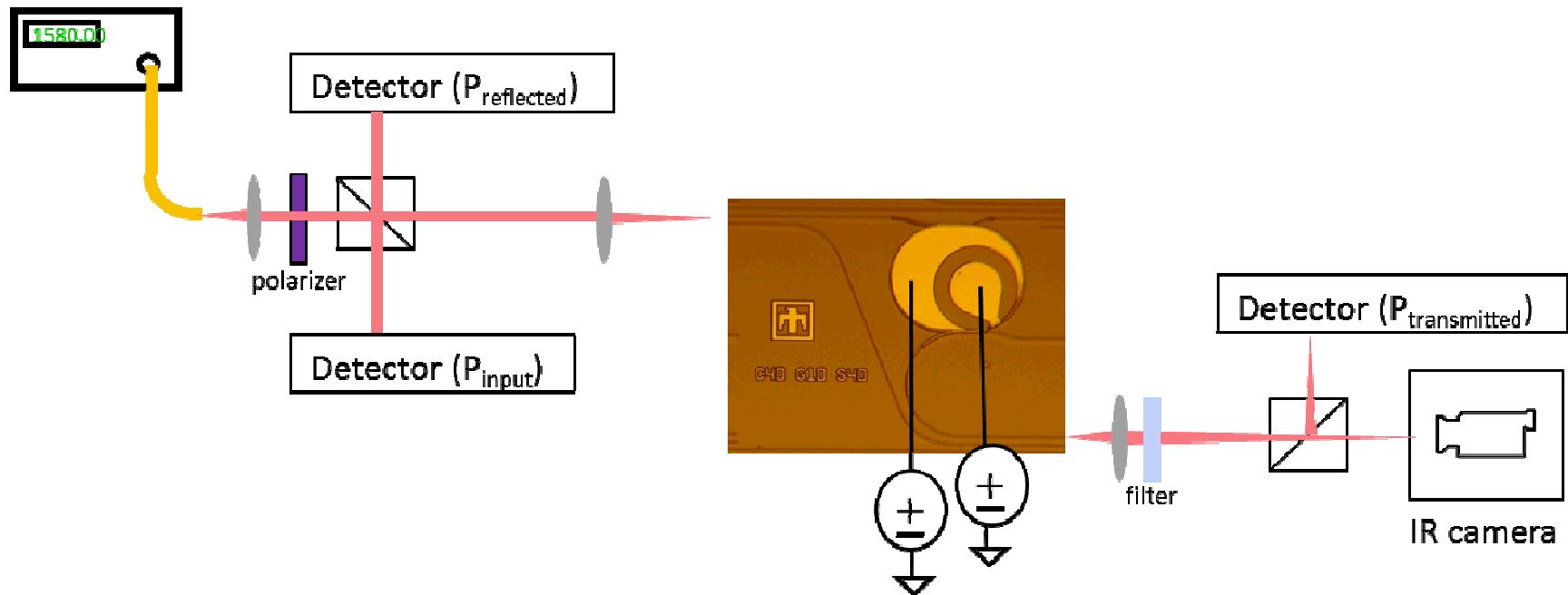
- Coupler design
 - Couplers utilize 1 μm waveguides with 1 μm gap
 - Coupling defined by length overlap region
 - Lithography biases are constant
→ **Consistency in coupler values within and between process runs**
- Simulations used to predict coupling
 - BPM simulation
 - Includes waveguide bends
 - Experiment shows lower coupling than predicted by BPM
 - Waveguide widths and gap has a bias due to fabrication



Experimental results

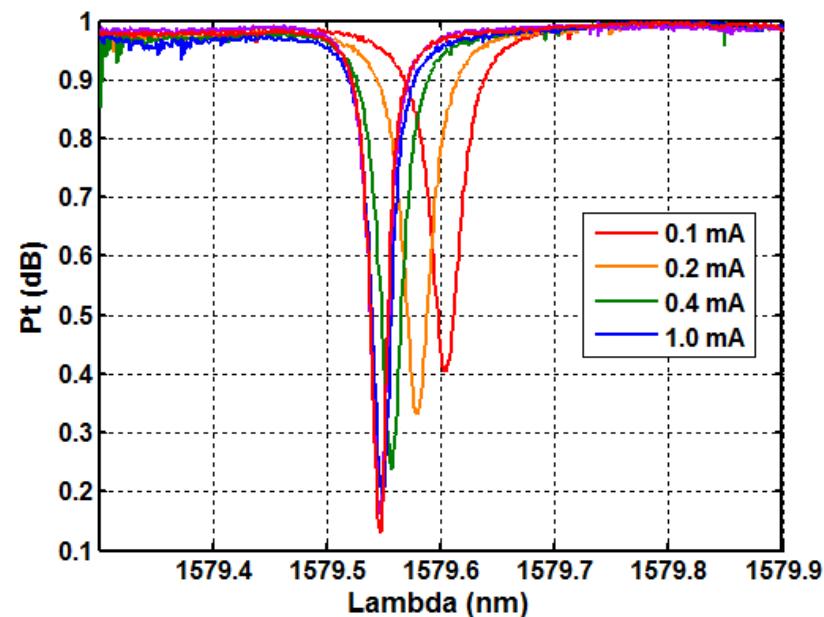
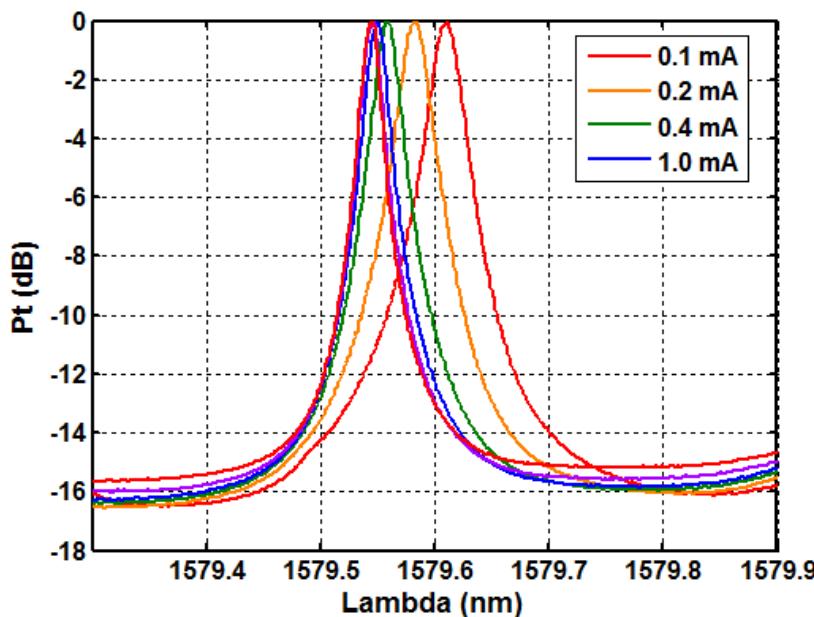
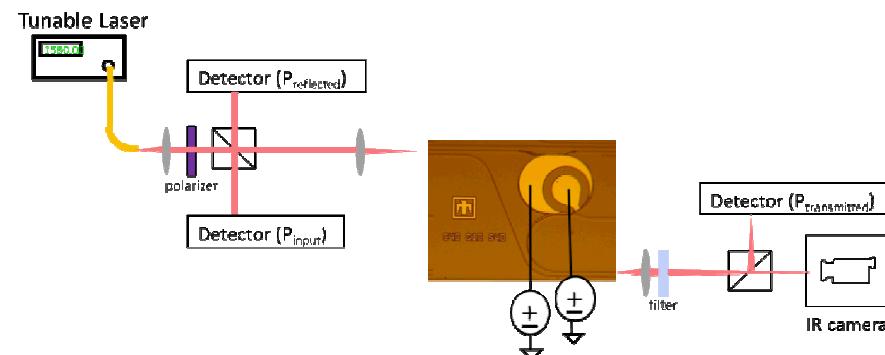
- Scanning source measurement
 - Wavelength swept on a tunable laser source
 - 12 nm filter added to the ring output
 - This filters out much of the ASE from the SOA

Tunable Laser



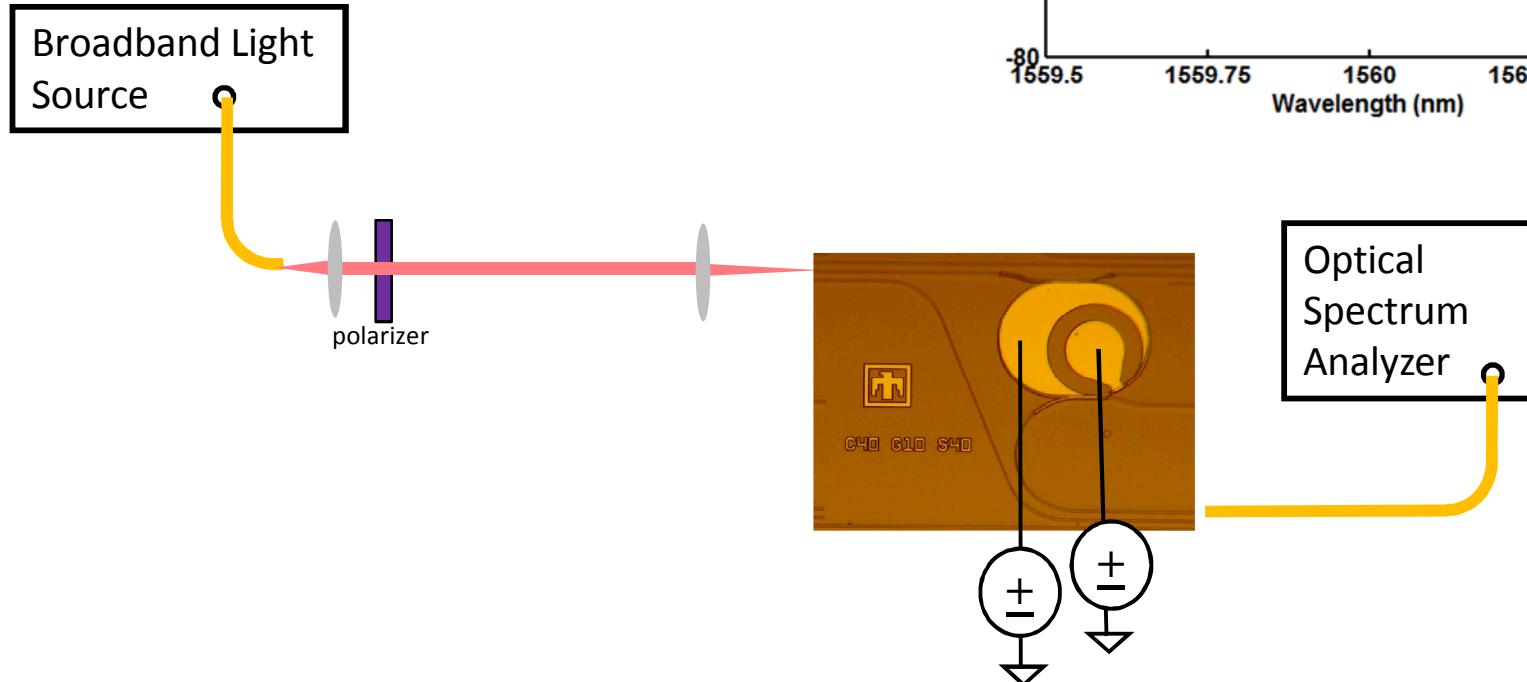
Experimental results

- Scanning source measurement
 - Variation in SOA current from 0.1-1.0 mA
 - >15 dB extinction
 - 3.47 GHz to 2.16 GHz FWHM optical linewidth



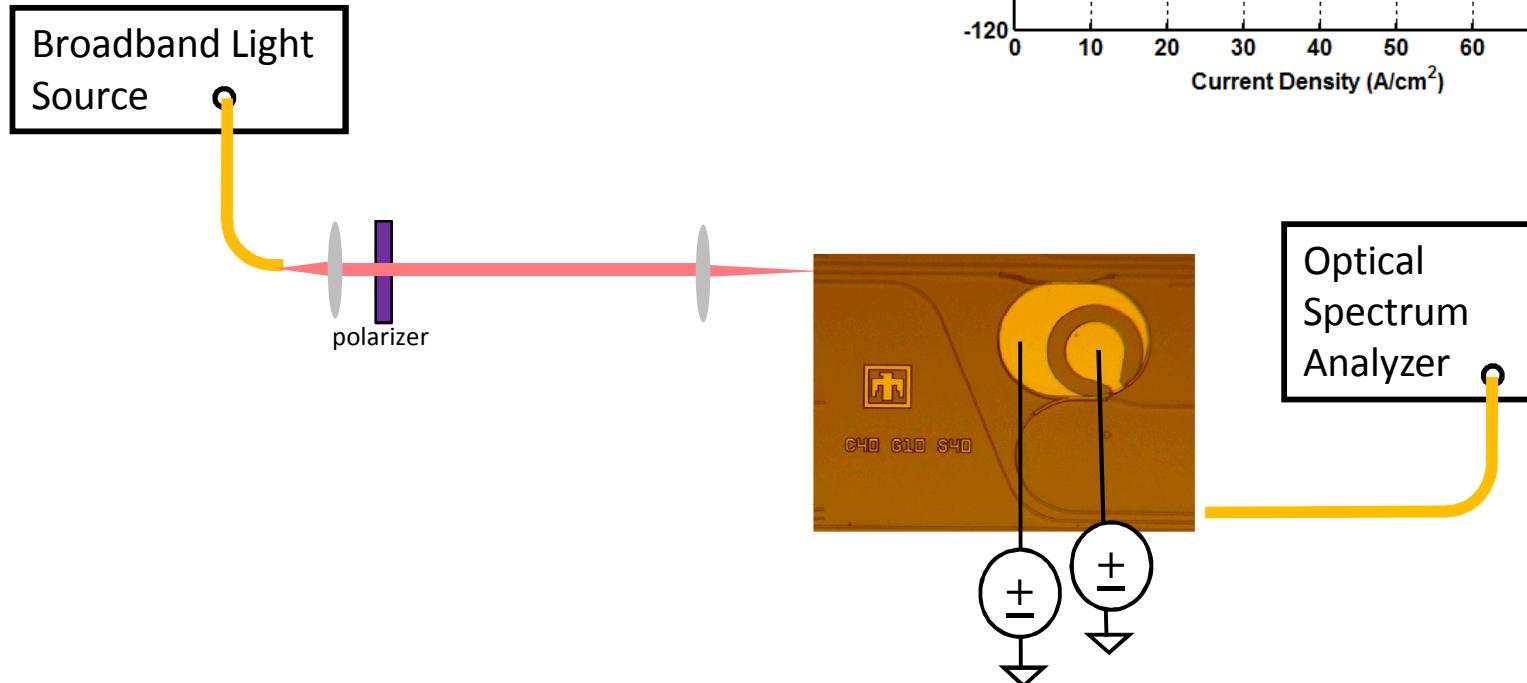
Experimental results

- Optical spectrum analyzer measurement
 - Broadband light source
 - Ring output fiber coupled to OSA
 - Better for larger wavelength scans
 - $I_{SOA1} = 2 \text{ mA}$
 - Extinction ratio of $>15 \text{ dB}$



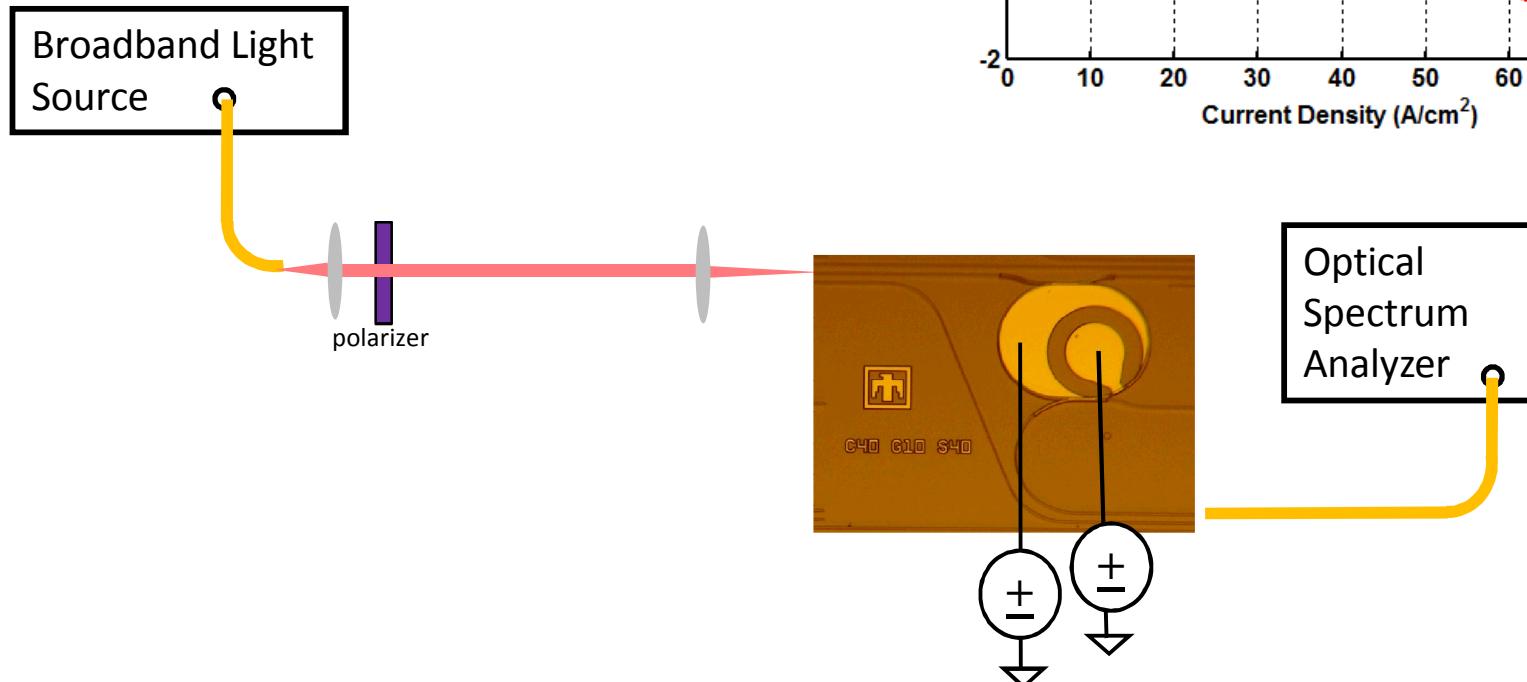
Experimental results

- Optical spectrum analyzer measurement
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 - Ring output fiber coupled to OSA
 - $I_{SOA1} = 2 \text{ mA}$
 - Extinction ratio of $>15 \text{ dB}$
 - 110 GHz with $I_{\text{Tune}} = 1 \text{ mA}$
 - Nearly twice the free spectral range

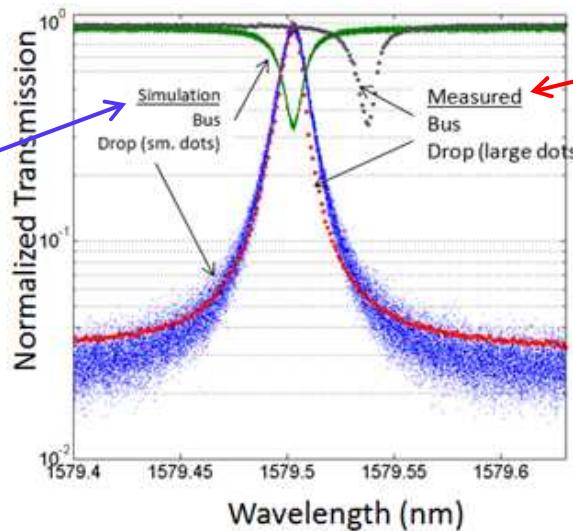
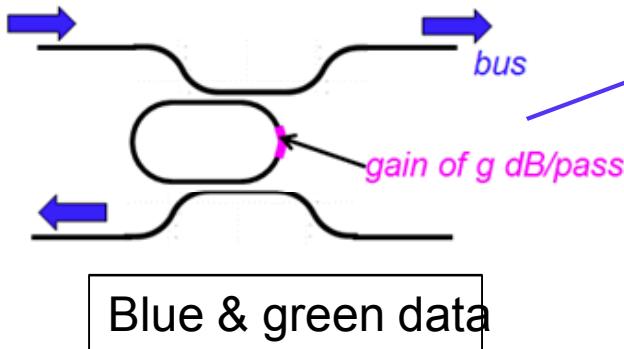


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Simulation benchmarking

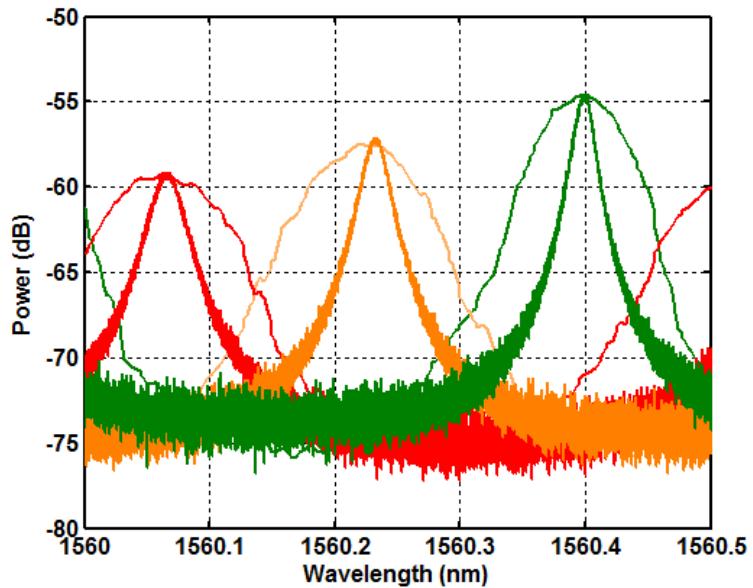


Red & black data

- Complete simulation of dynamic range and noise of active InGaAsP multi-ring filters
 - Include gain distortions and spontaneous emission noise
- Time dependent rate equation method
 - Gain and spontaneous emission modeled as function of injection current at all wavelengths simultaneously
- Fit experimental bandwidth of drop and extinction of bus to extract net round trip loss and coupling fraction
 - 6% coupler with 1.4 cm^{-1}

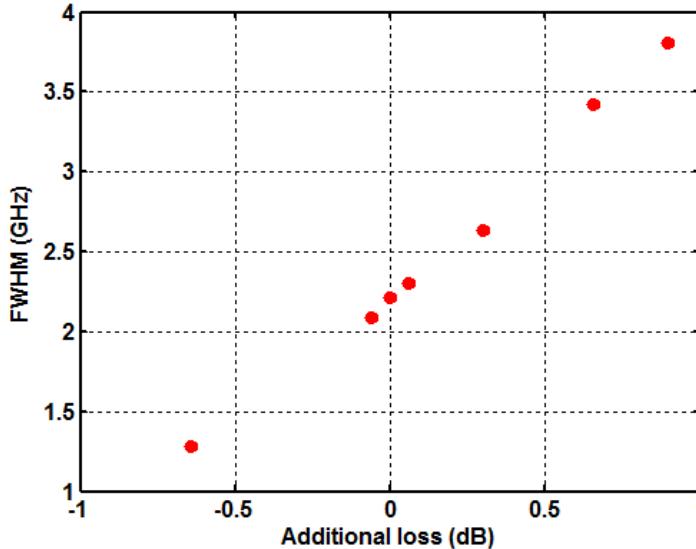
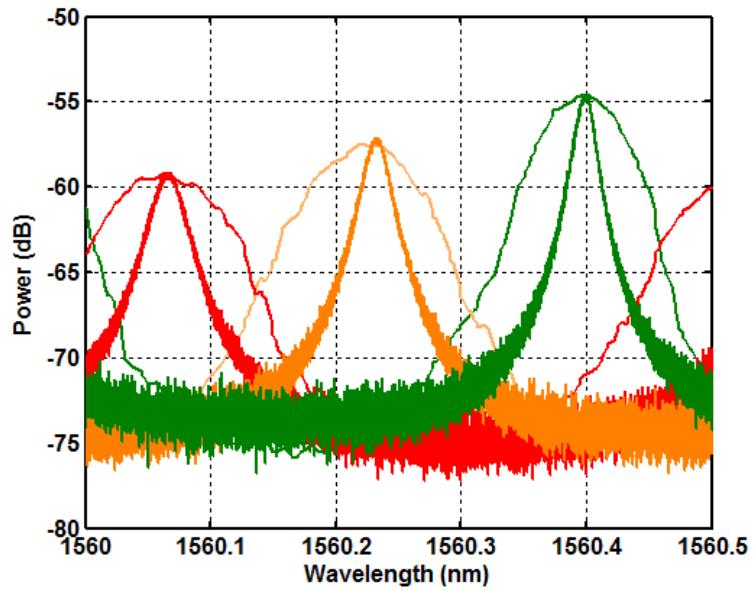
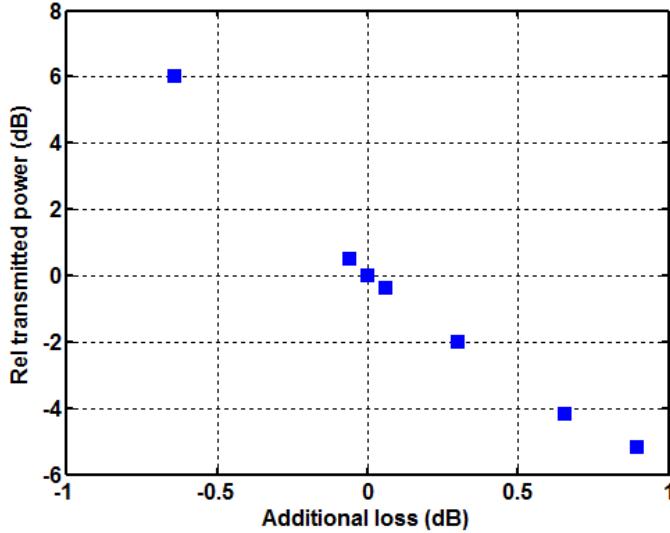
Simulation

- Tuning and loss from benchmarked from filter tuning data
- Effects of tuning induced loss on FWHM linewidth
- 0.9 dB of additional loss caused by tuning current
 - reduces peak power 5 dB
 - Increase FWHM by 1.6 GHz
- Loss can be compensated for by increase in SOA gain



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Conclusions and Future Work

- Fabricated and demonstrated tunable ring filter
 - Process compatible with monolithic integration of lasers and modulators
 - >15 dB extinction
 - 56 GHz free spectral range
 - 2.17 GHz passband
- Future work will focus on:
 - Integration with lasers and modulators
 - Measure insertion loss and bus channel characteristics
 - Exploring offsetting loss with SOA gain to maintain constant peak power
 - Look at SNR and dynamic range

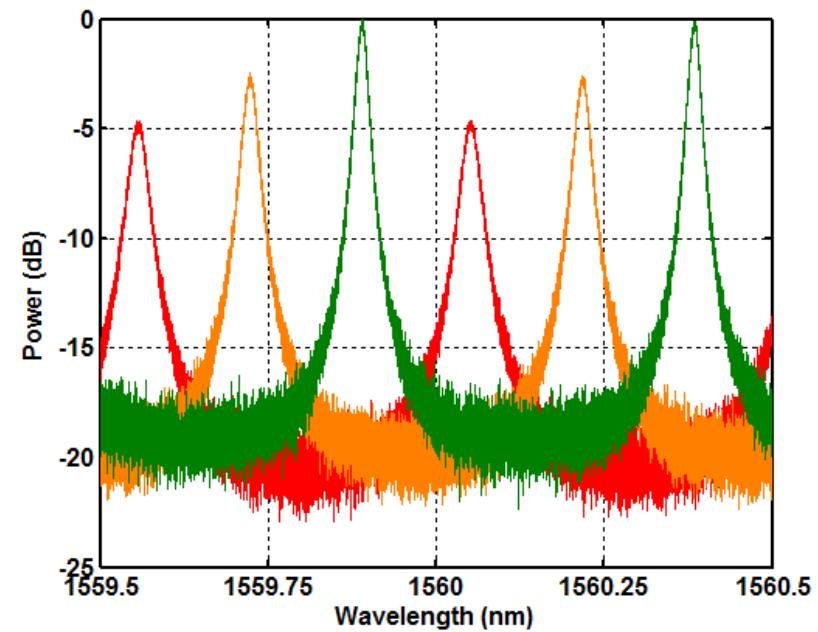




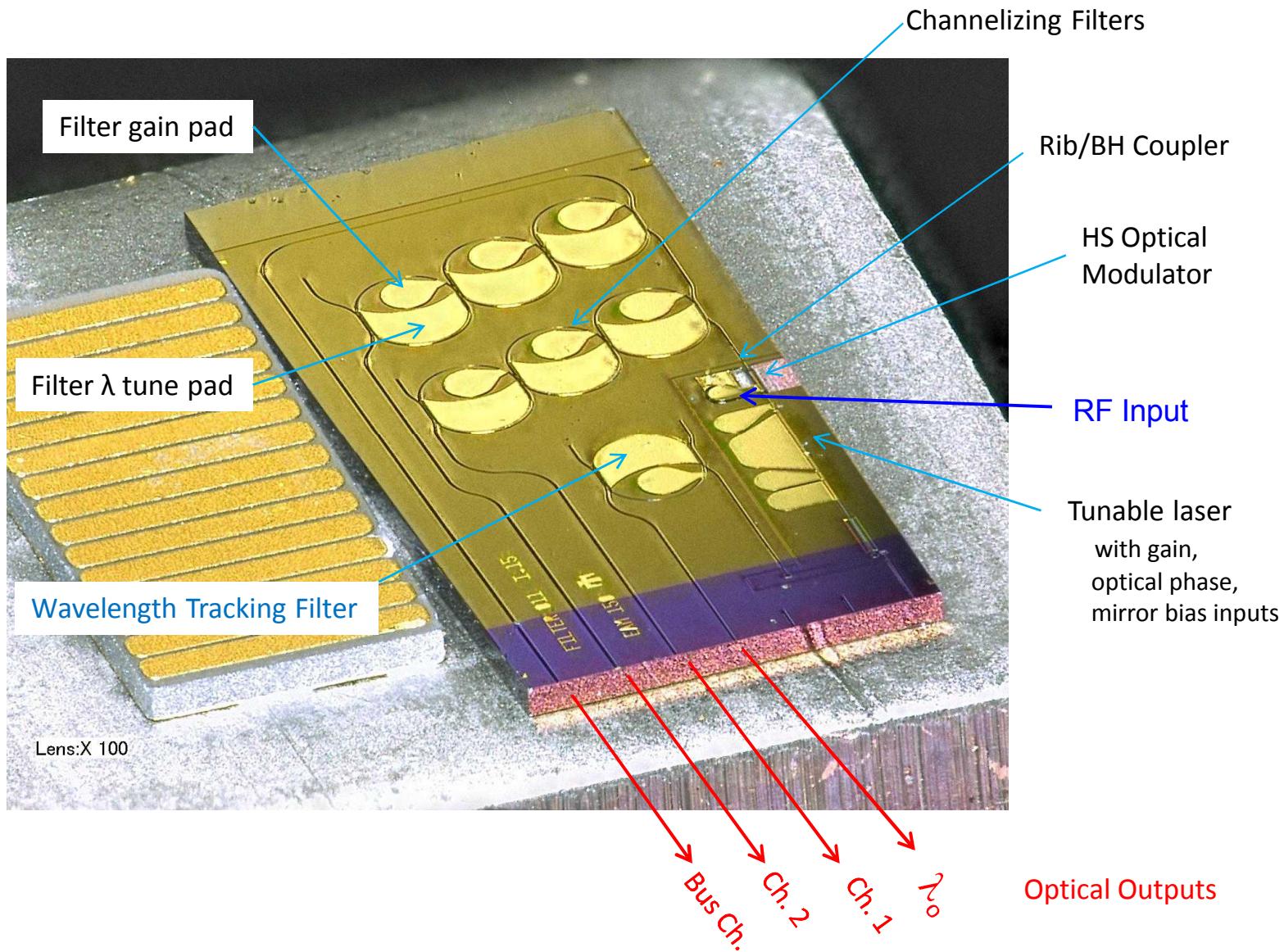


Backup Slides

Simulation benchmarking



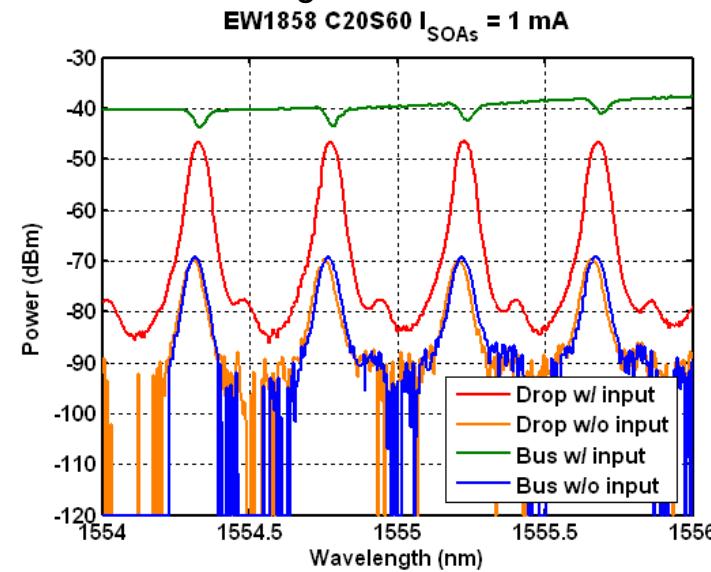
Full PIC design



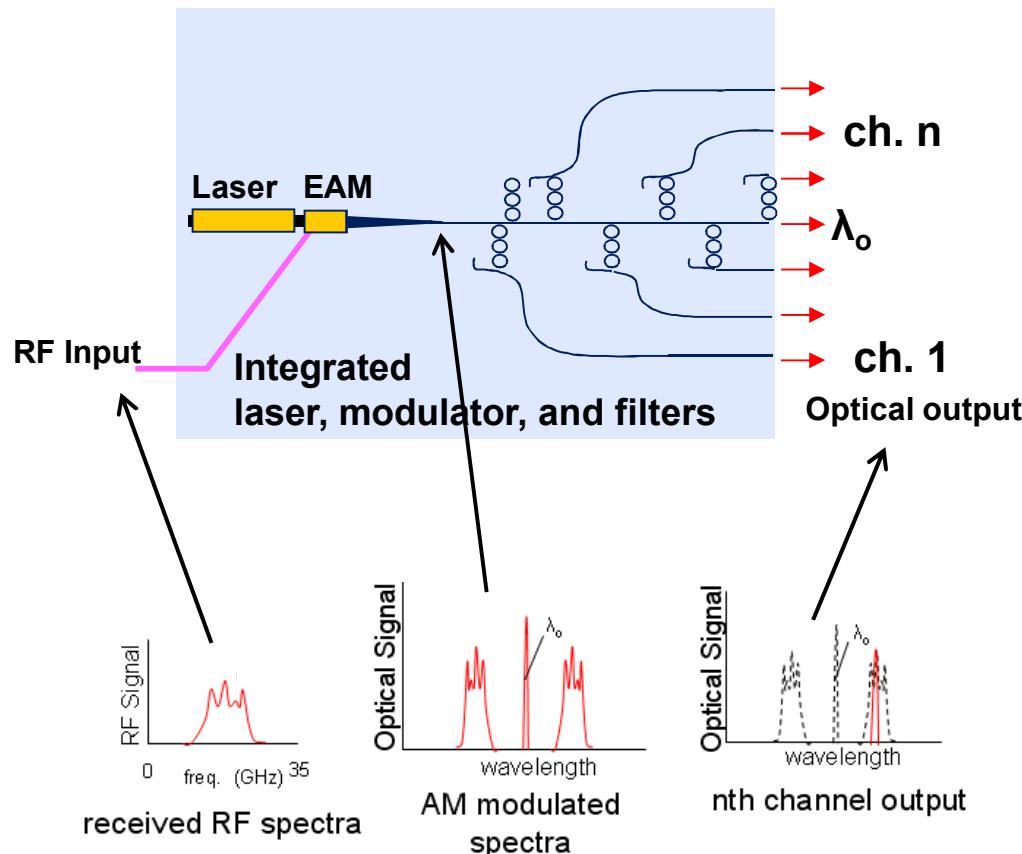
InP Active 2-ring Filter

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on fig

- ASE source and OSA
 - Higher extinction
 - SOA-ASE goes is correct wavelength ‘bin’
- Tunable laser and photodiode
 - Lower extinction
 - off resonance measurement includes SOA-ASE from all wavelengths
 - A filter (~5 nm) will give results similar to OSA
 - This can be external for testing
 - On a monolithic chip we need to add additional filtering

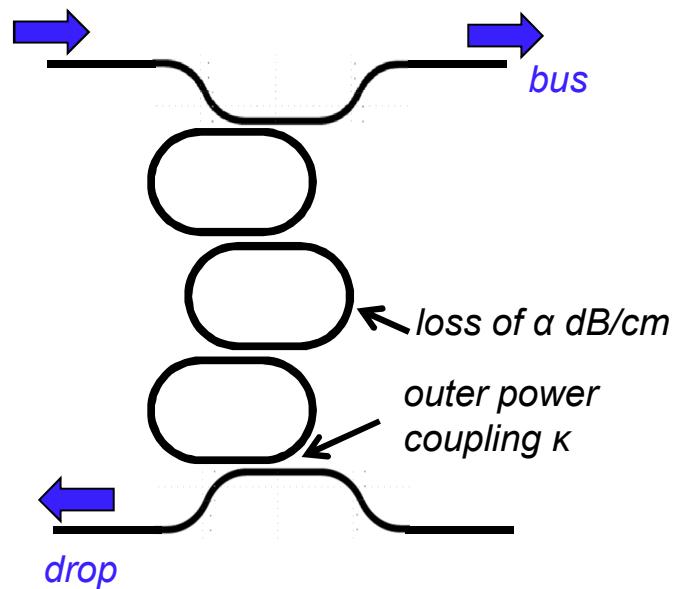
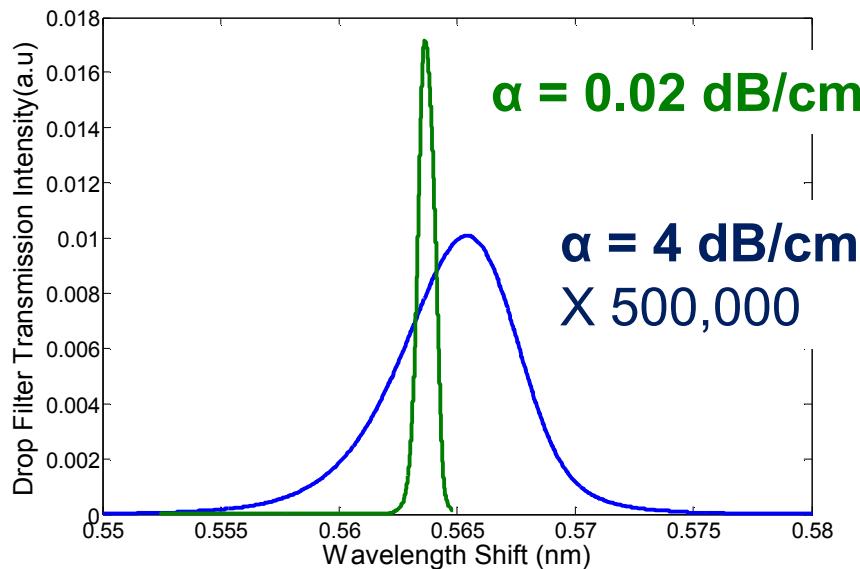


Channel-Dropping Filters



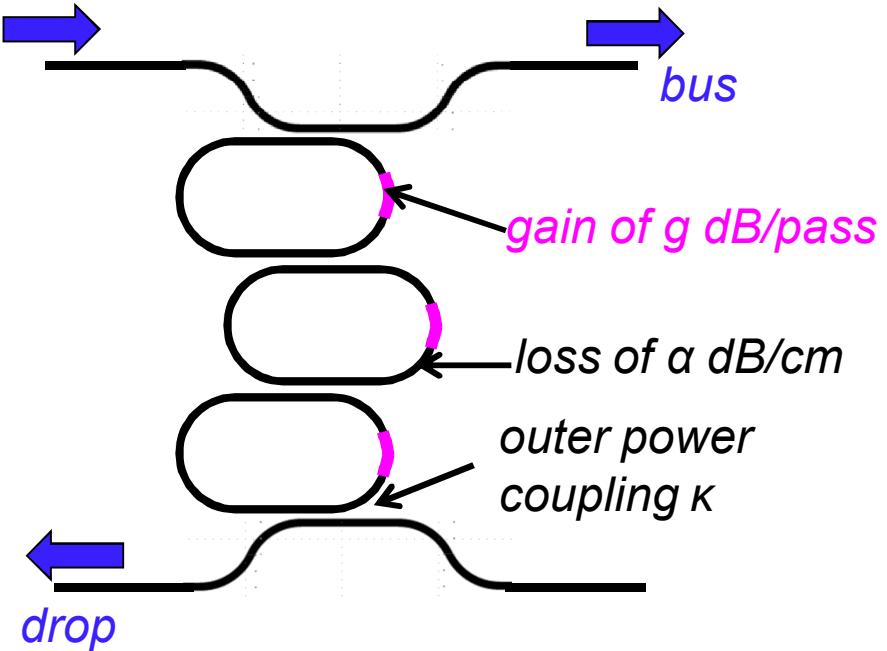
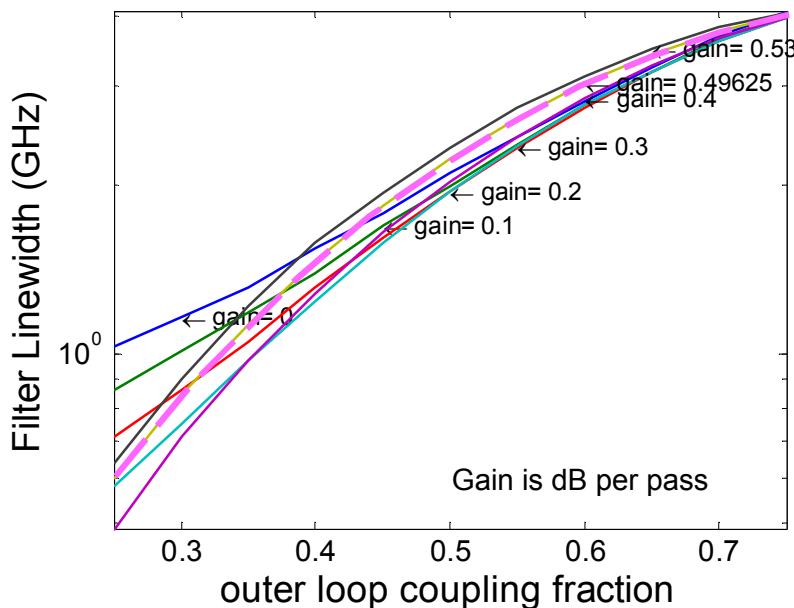
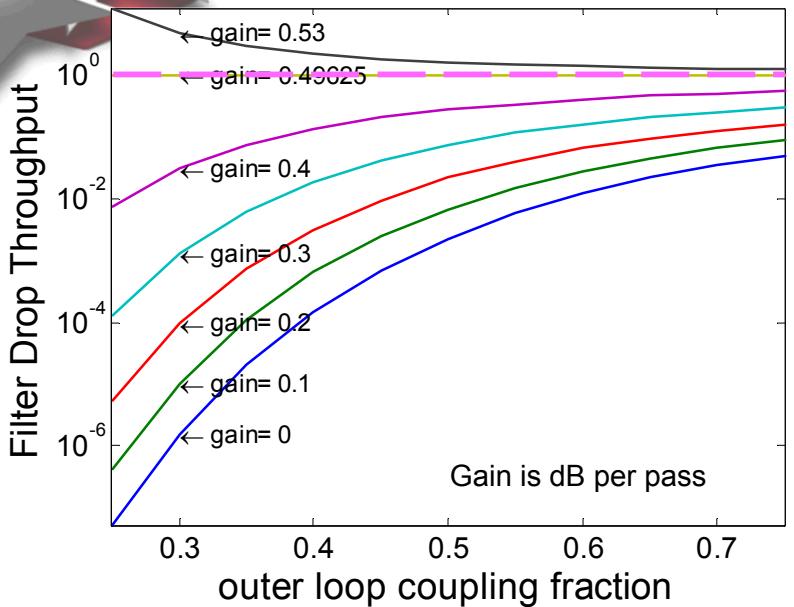
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Monolithic Integration and Loss-Limited Filter Response



- Optical waveguide losses dominate the filter performance
- Useful passive ring resonant filters are typically made of glasses or undoped semiconductors with very low optical loss.
- Ring Filters with losses commonly seen in doped InGaAsP waveguides for active PICs have too little optical transmission to be useful as GHz-class filters

A Small Amount of Gain Offsets Losses



- SOAs enable monolithic integration
- Introduce an ideal loop gain to each filter
 - No noise in model, yet
- Ring waveguide loss
 - 4 dB/cm
- Loss-less filter achieved
 - 0.5 dB/pass gain element

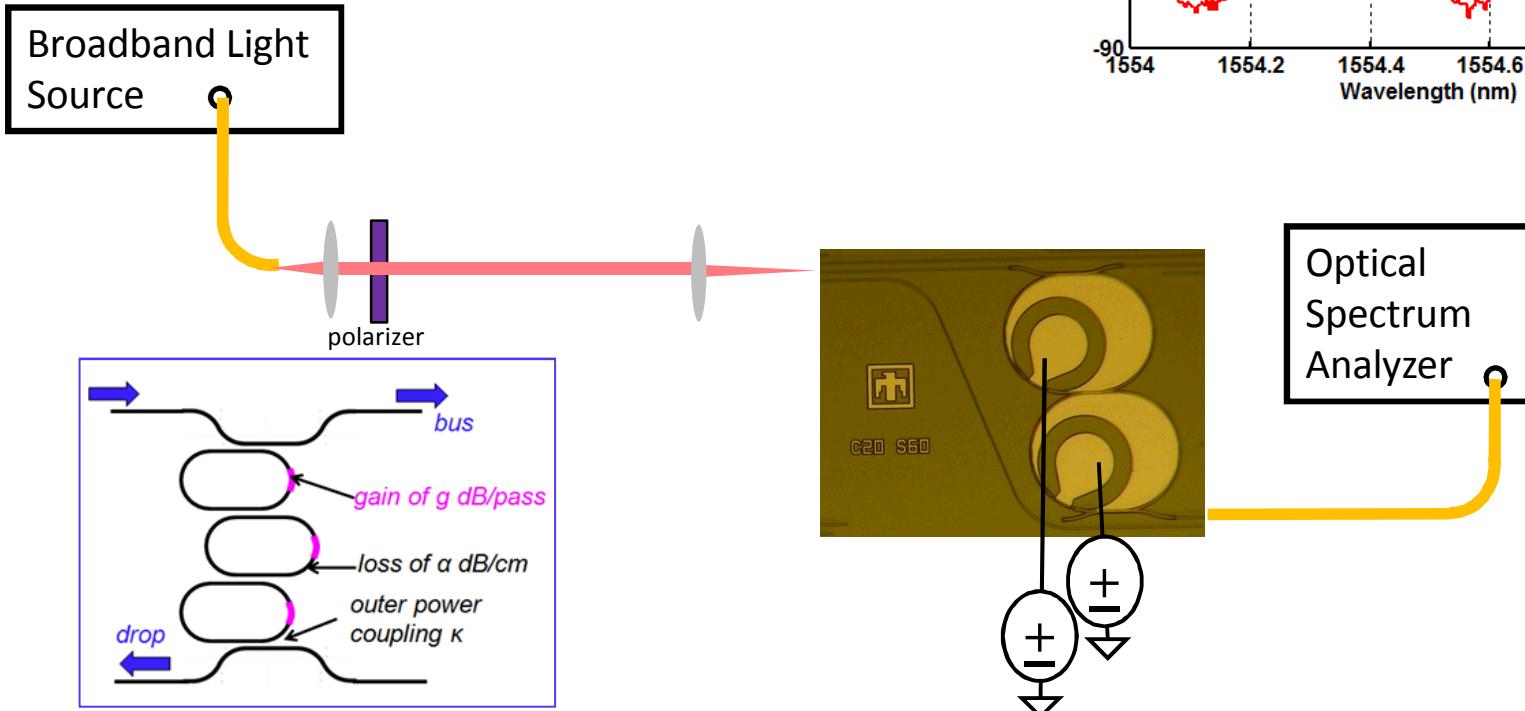
Active Rings : Experimental

- Dual-ring filters

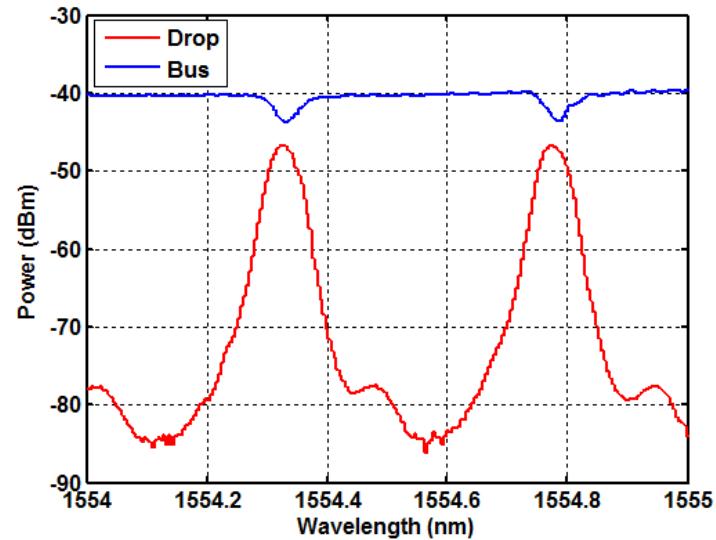
- > 30 dB extinction ratio
- 2.5 GHz linewidth
- $I_{SOA1} = I_{SOA2} = 1 \text{ mA}$
- Extinction ratio of >30 dB
- Filter loss of 1.7 dB
 - Loss defined as total power on resonance compared to total power off resonance

- OSA measurement

- Broadband light source

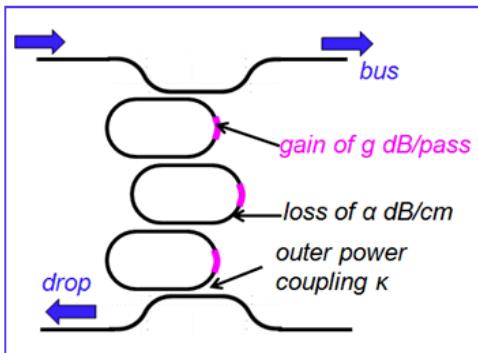


See paper OThW2
Thur. @ 4 pm



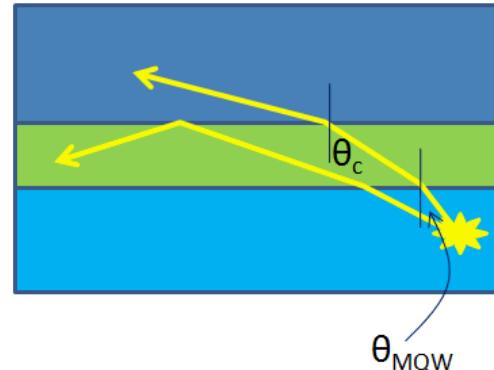
Active filter modeling

- Time domain travelling wave model of single and multi-ring filters
- Semiconductor Optical Amplifier (SOA) embedded in each ring
- Local gain and spontaneous emission modeled as functions of injection current and optical power
 - Time-dependent rate-equation approach
- Complete power spectra computed at each time step



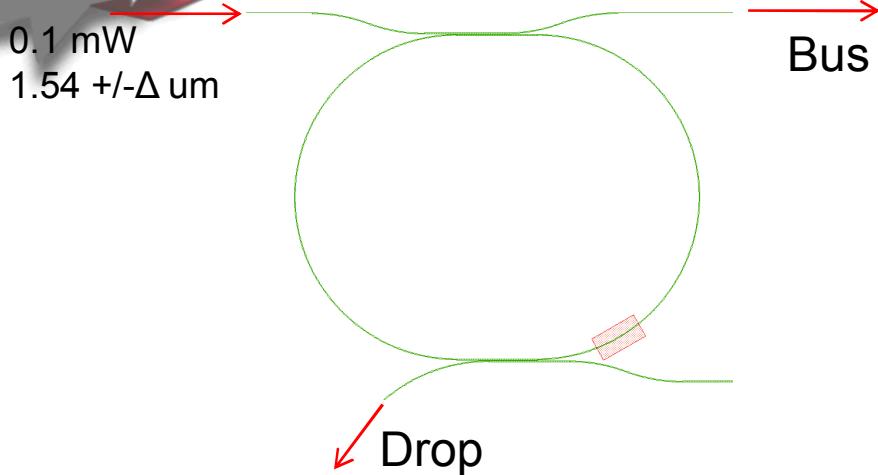
Fraction of SOA spontaneous emission coupled into waveguide mode

- Amplified spontaneous emission (ASE) noise from SOAs creates a noise floor on filter spectra
- ASE noise computation in two steps
 - Spontaneous emission recombination event
 - Coupling of spontaneous emission into guided mode of ring
- The spontaneous emission factor influences the noise floor due to ASE

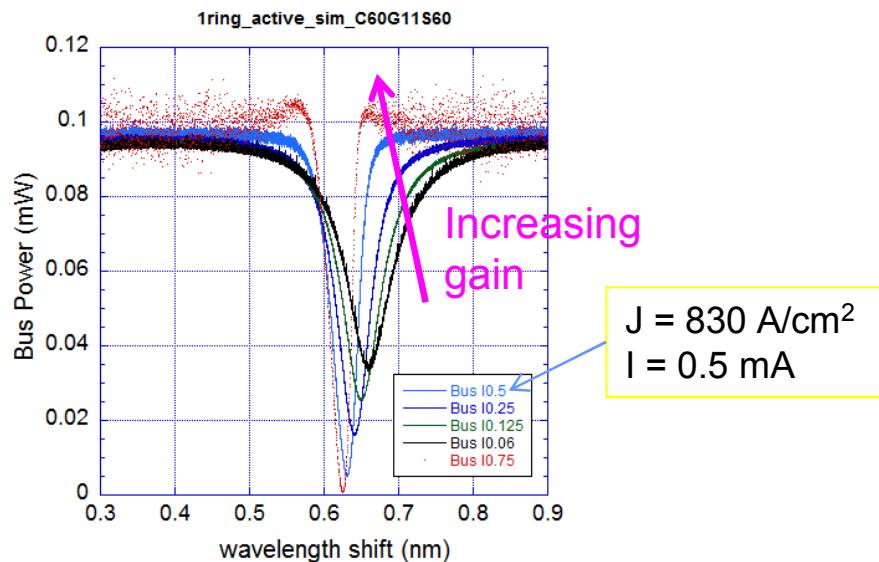
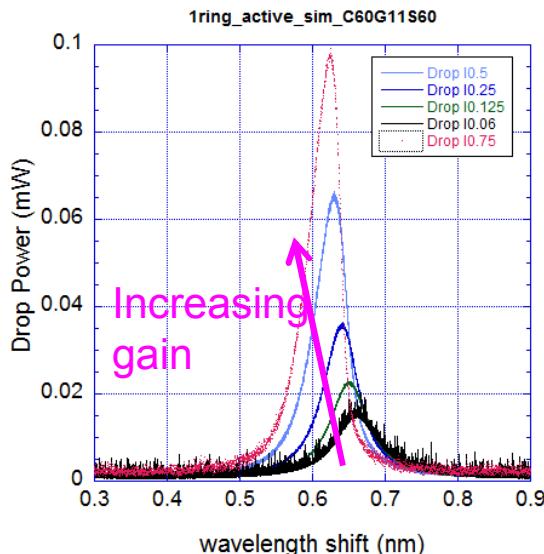


- Indexes
 - InP, $n = 3.168$
 - Q13, $n = 3.3877$
 - MQW, $n = 3.427$
- Included angle of captured light
 - 44.8 deg
- Area of spherical cap
 - $A_{cap} = 2\pi r h$
 - $H = r(1 - \cos\theta)$
- Area of sphere
 - $A_{total} = 4\pi r^2$
- Fractional area
 - $A_{cap}/A_{total} = (1 - \cos\theta)/2$
 - $\theta = 22.4$ deg
 - Fractional area = 0.0378
- Fraction of light capture by guided mode
 - Multiply fractional area by overlap integral with guided mode
 - Γ (fractional area) = $0.06989 \times 0.0378 = 0.00264$
- SponBetaNA = 0.00264

Model of Active Ring

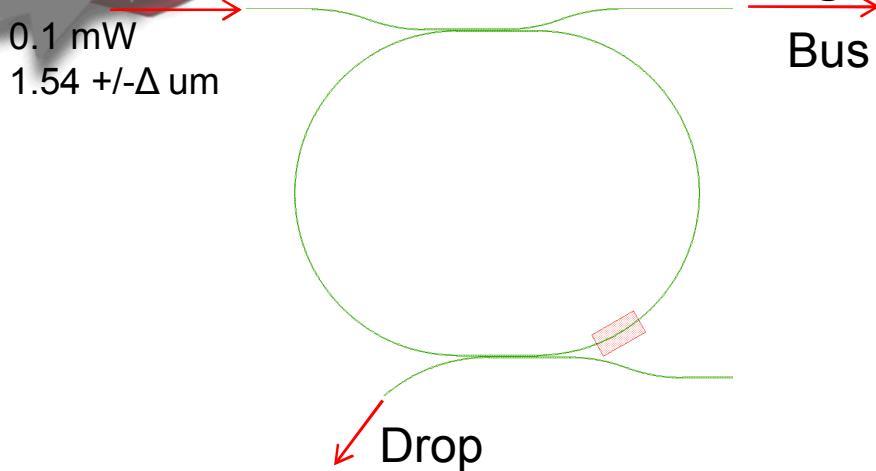


Radius: 200 μm
 Couplers: 17% power cross-coupling
 Passive guides: 3 cm^{-1}
 SOA: 60 μm long
 7 QW centered, 25C
 1 μm wide BH
 current flow *only* in the MQW
 Spontaneous Coupling: 0.0037

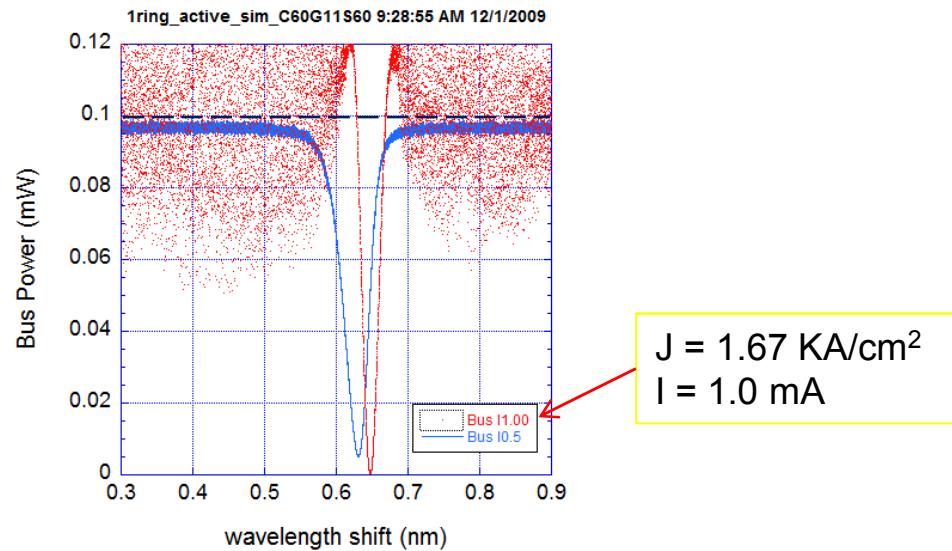
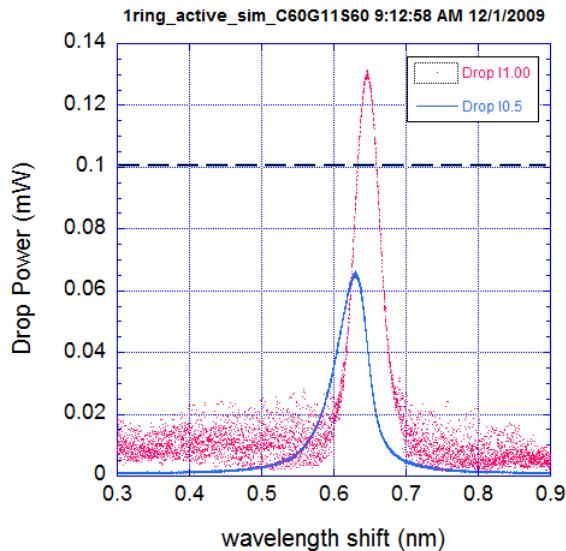


- Variation of SOA injection current
 - Insertion loss drops and bandwidth narrows as SOA current is increased

Model of Active Ring

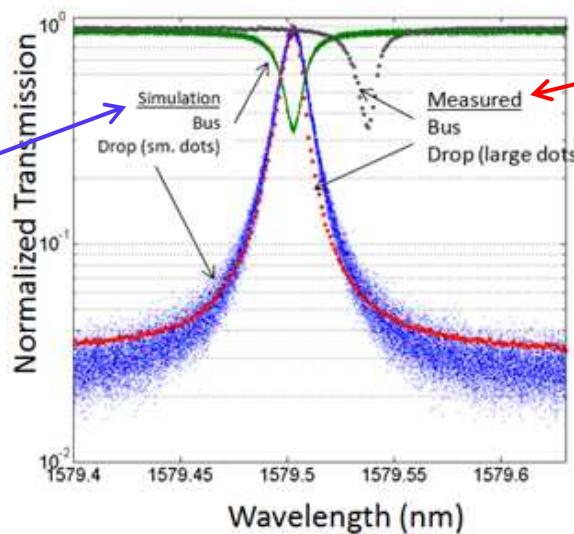
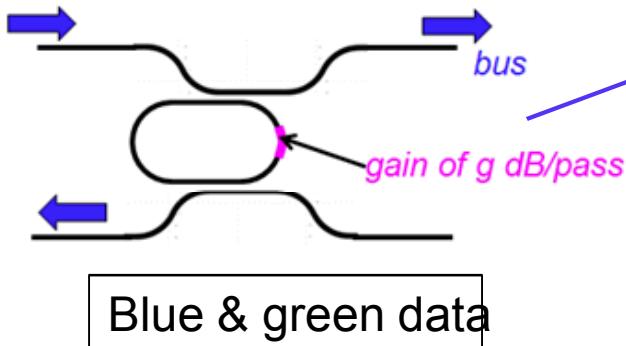


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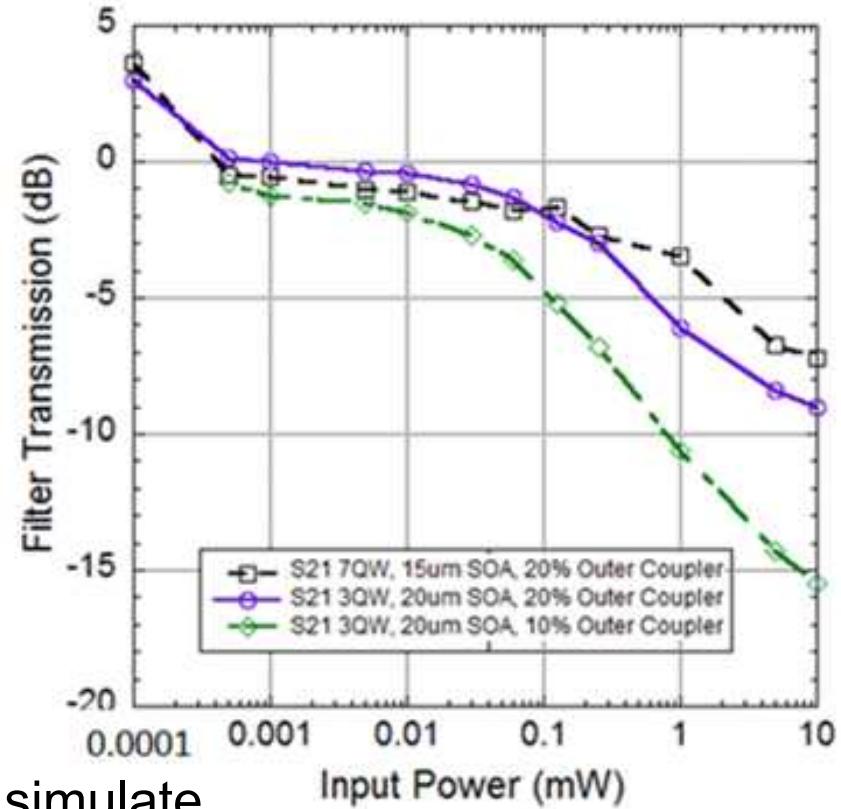
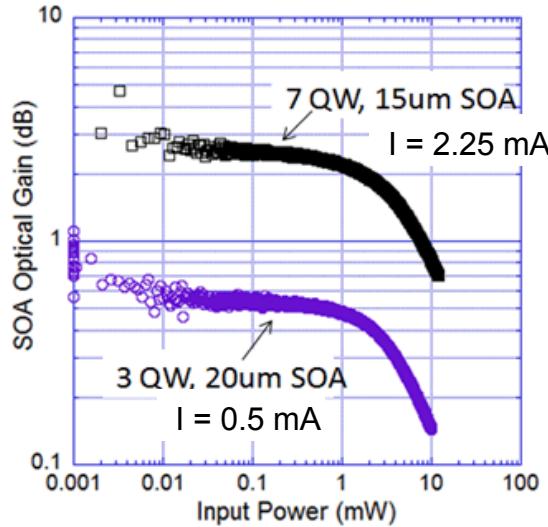
- Operation at very high gain (SOA injected current)
 - Negative insertion loss achievable, but very noisy

Single Ring Active Filter: Simulation Benchmark to Experiment



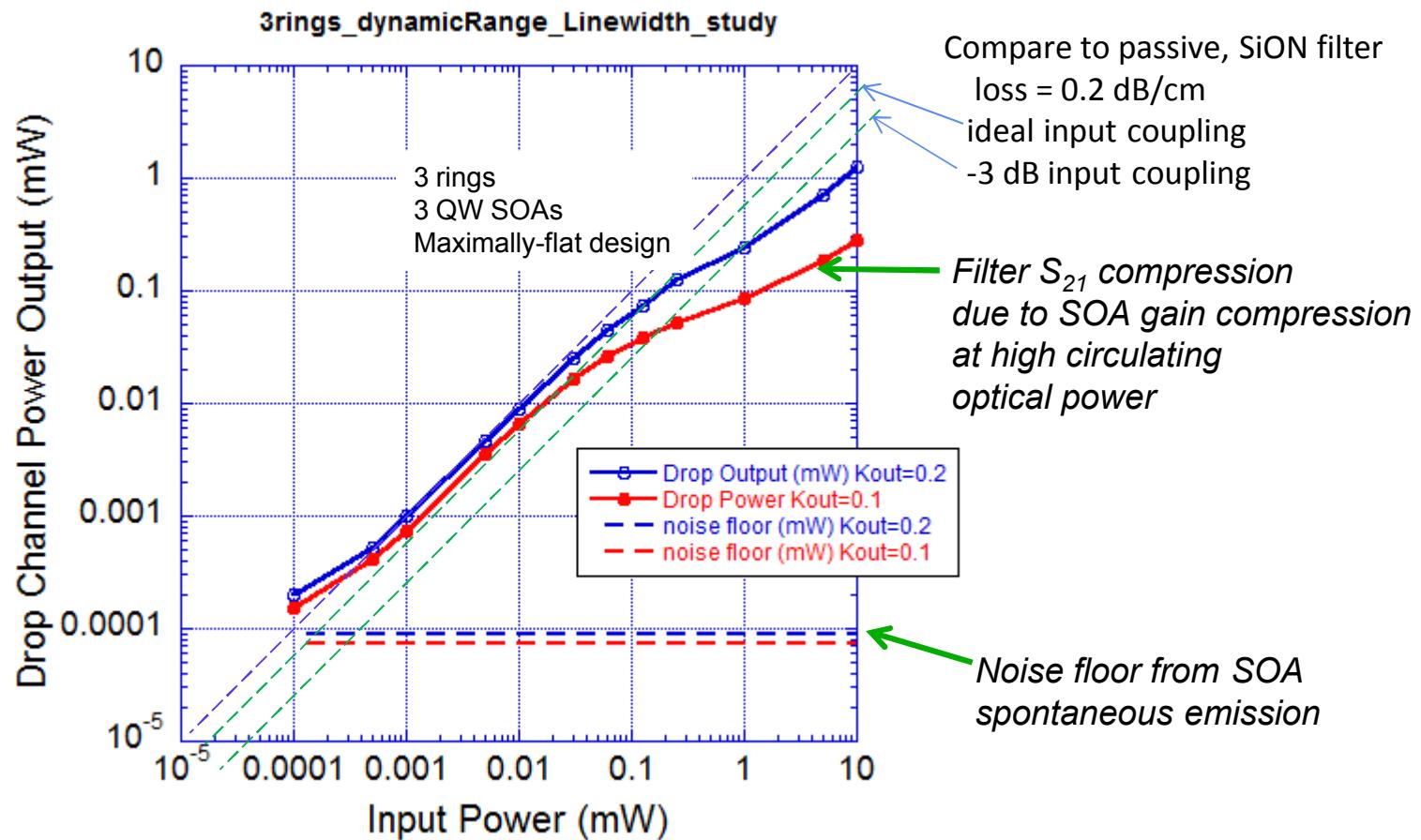
- Complete simulation of dynamic range and noise of active InGaAsP multi-ring filters
 - Include gain distortions and spontaneous emission noise
- Time dependent rate equation method
 - Gain and spontaneous emission modeled as function of injection current at all wavelengths simultaneously

3-ring active filter simulations



- For 3-ring maximally flat filters simulate
 - Linewidth, Insertion loss
 - Dynamic range and Noise floor
- SOA gain and power saturation depend on key factors
 - Number and configuration of QWs and Injected current
 - Simulate case of both 3 and 7 QW SOA

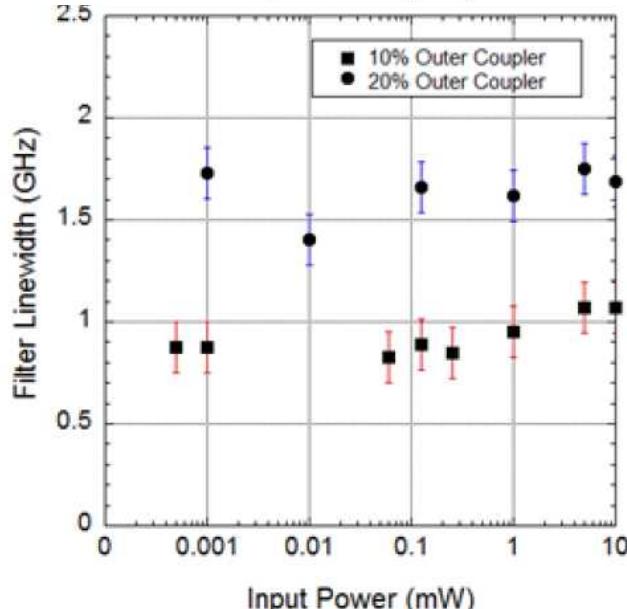
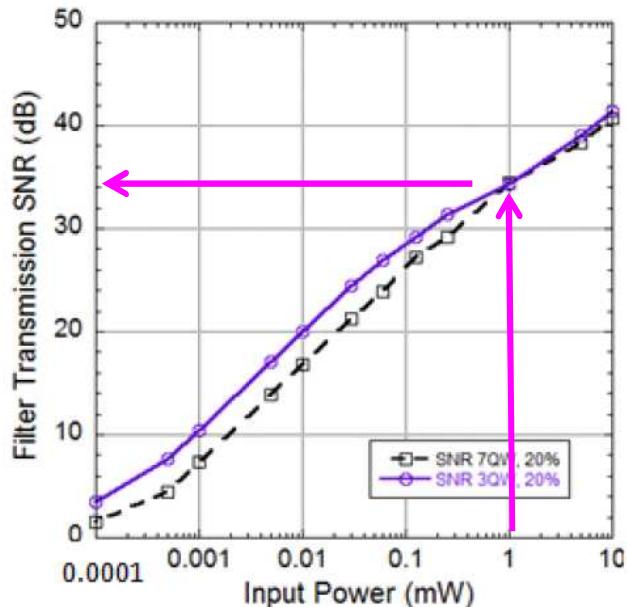
InP Filter Dynamic Range



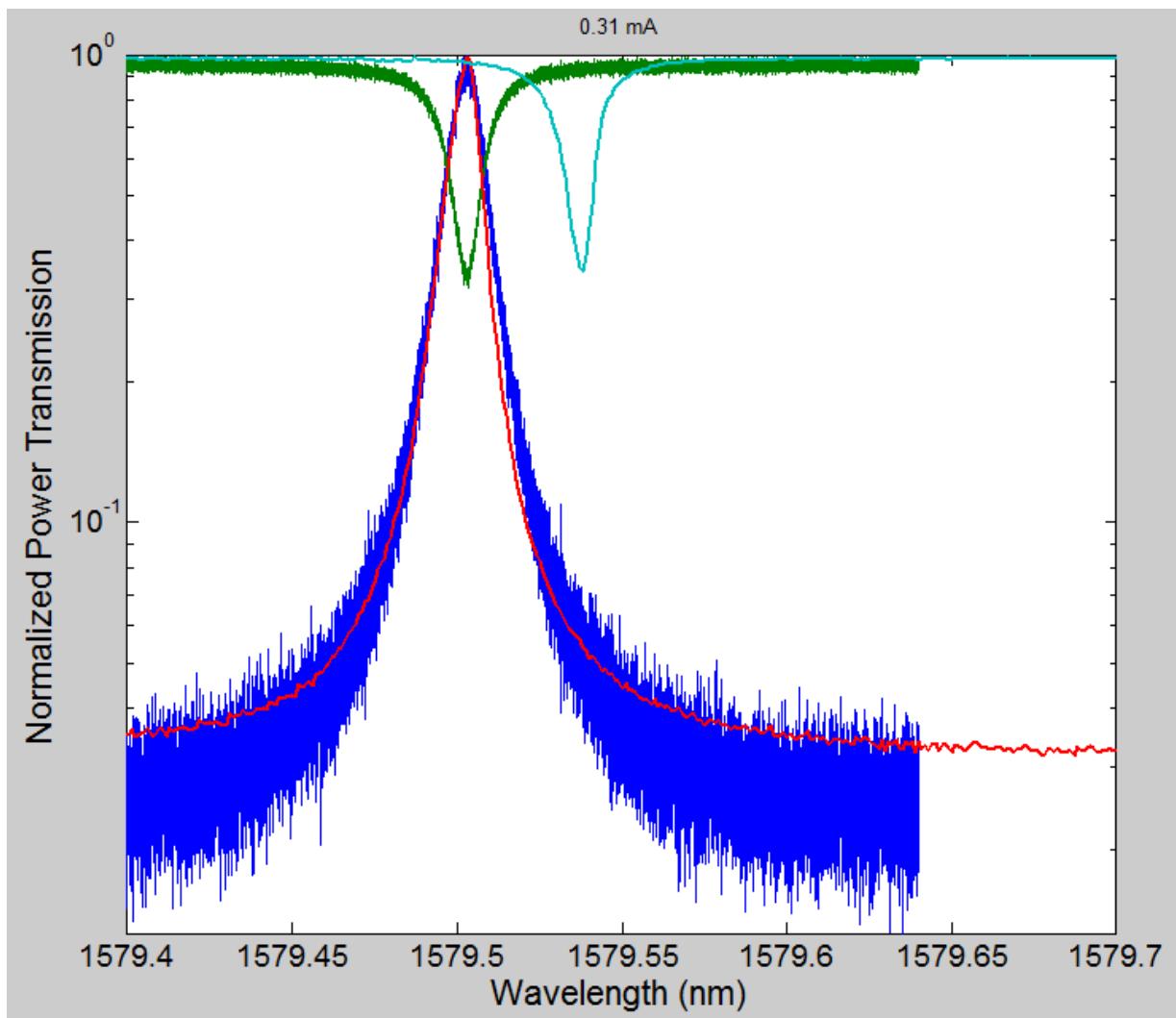
- Active InGaAsP filter shows improved filter transmission compared to passive SiON design over >30 dB dynamic range
- Spontaneous emission noise in SOAs limits SNR at lowest input optical powers
- SOA saturation causes compression of filter S_{21} at resonance at high end of input power

Summary

- Time domain model of active ring with SOAs developed
 - SOA model includes gain saturation and ASE
- 3-ring filter with 3 and 7 quantum well gain sections simulated
 - Optical linewidth
 - Noise floor
 - Linearity and dynamic range of S_{21} versus input power
- InP active filters show promise for frequency-domain signal processing in monolithic integrated photonic integrated circuits
 - 50 dB input dynamic range
 - Output compressed at high power
 - 0 dB loss in mid range accessible for 1 GHz filters
 - Filters with power gain are possible but quickly become limited by noise
 - Possible methods to improve dynamic range
 - Reduce optical confinement factor
 - Balance against lower gain or more complex offset active lasers in remainder of PIC
 - Wider SOAs
 - More pump current



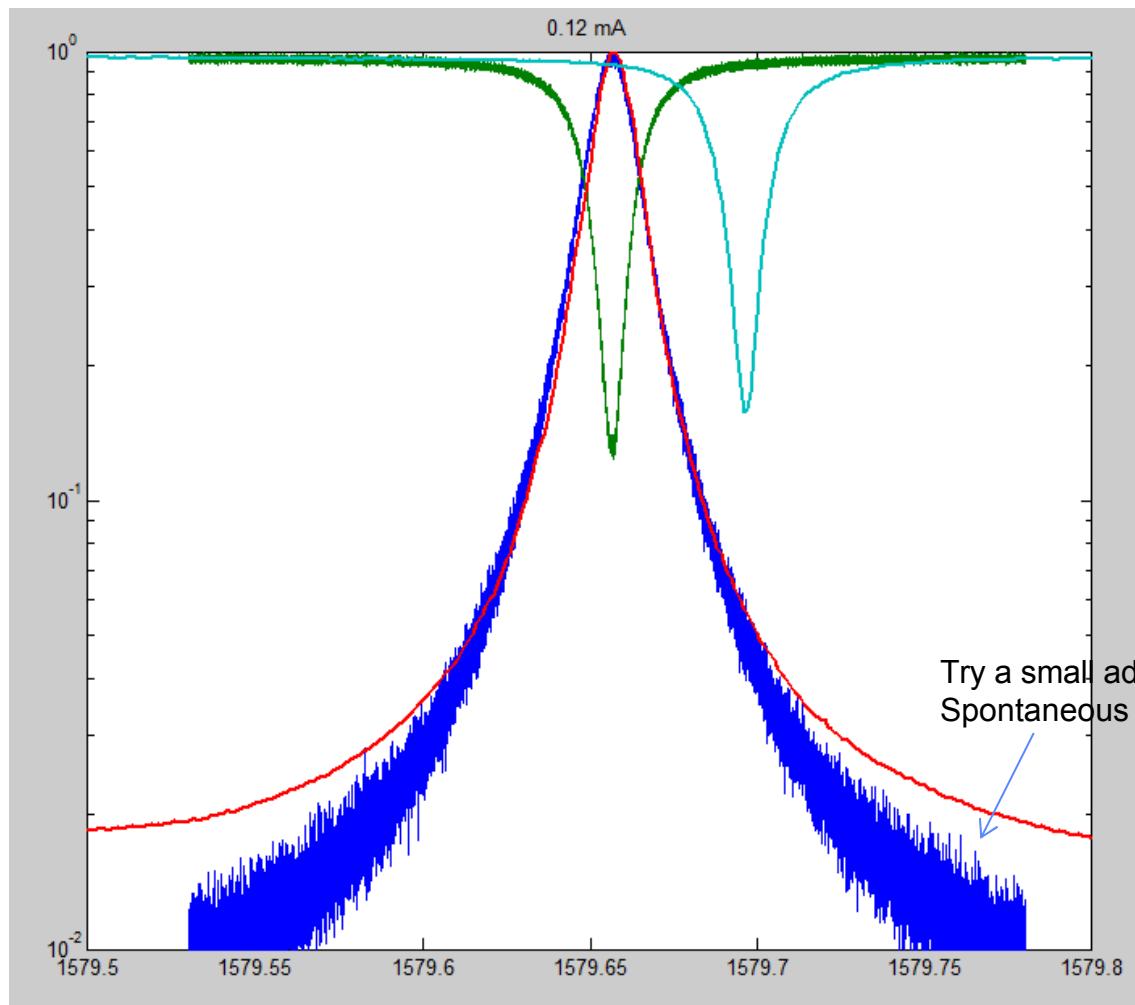
Best Fit to C20G10S100, EW1858



- 8 QW offset
- 100 μ m SOA
- $K^2 = 0.03$
- Loss = 1.4 cm^{-1}
- $P_{in} = 0.005$ mW
- I_{SOA} model – 0.31 mA
- I_{SOA} exp – 1 mA

Simulation data is in SOA100_K03_alpha14_8mqw_offset.xls and .mat

Detail Fit to C40G10S20, EW1858



- 8 QW offset
- 20 μm SOA
- $K^2 = 0.06$
- Loss = 1.4 cm^{-1}
- $P_{\text{in}} = 0.005 \text{ mW}$
- $I_{\text{SOA model}}$
 - 0.12 mA
- $I_{\text{SOA exp}}$
 - 0.2 mA
- $P_{\text{in exp}}$
 - 0.2 mW

Simulation data is in SOA20_K06_alpha14_8mqw_offset.xls and .mat