

# Tunable InP Ring Resonators

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C. Alford<sup>1</sup>, D. Torres<sup>2</sup>, and F. Cajas<sup>1</sup>

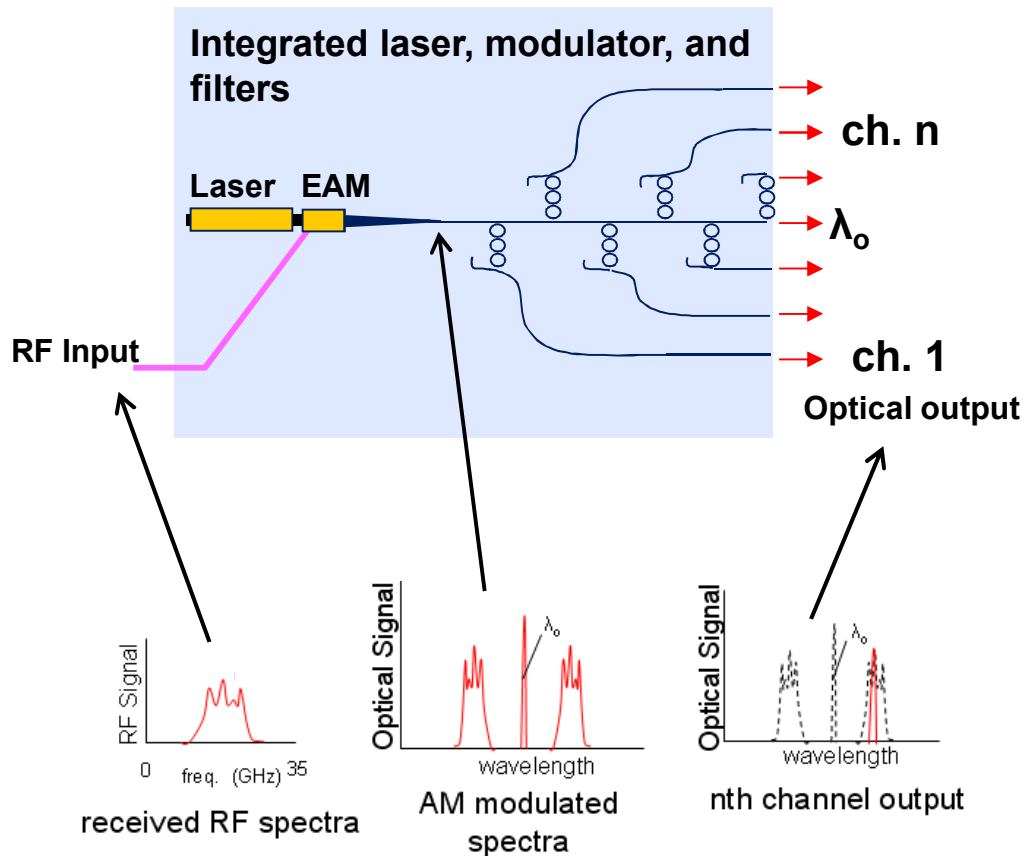
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Photonics West, San Francisco, CA

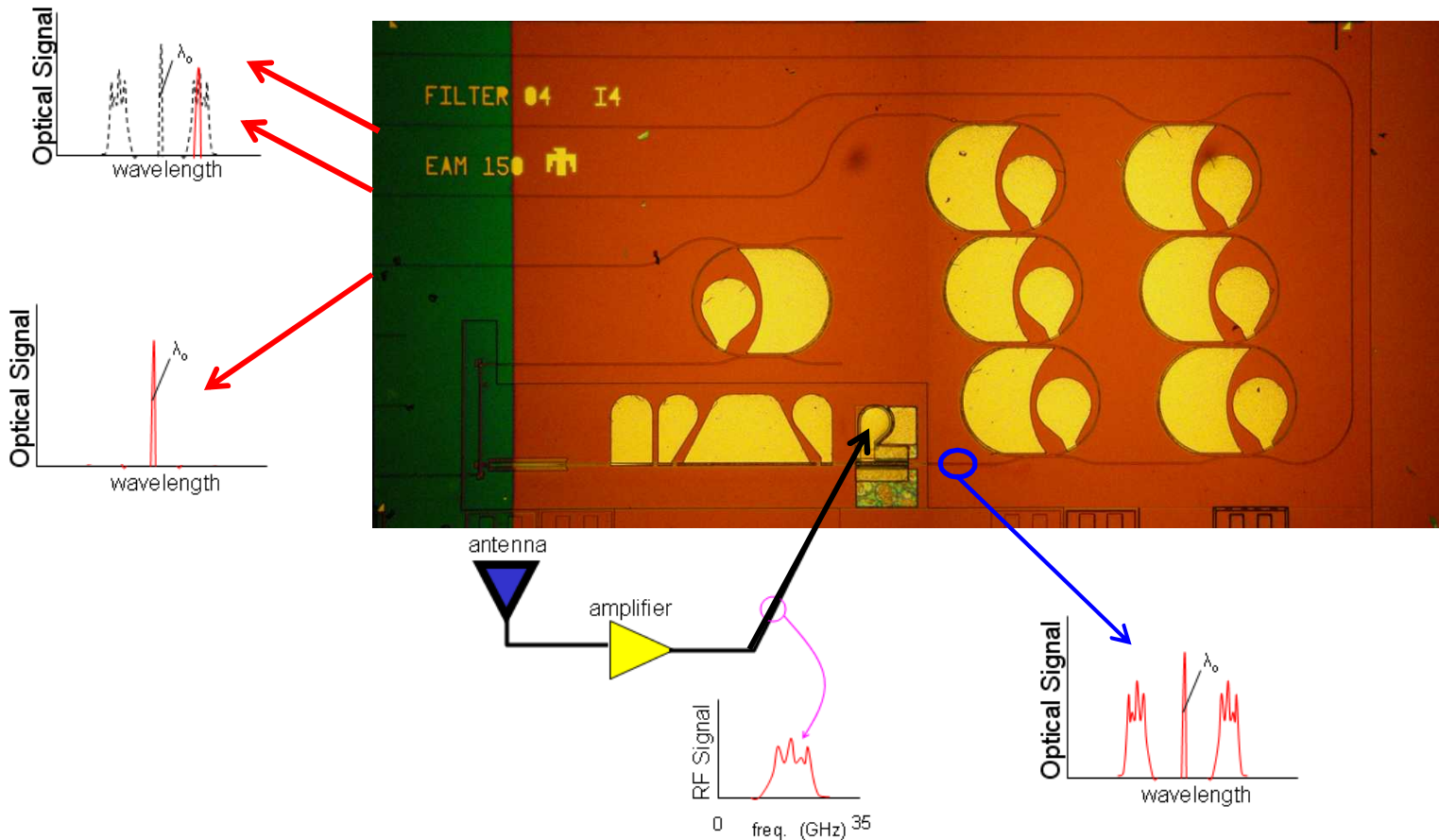
February 7, 2013

# Motivation



- Analyze an RF signal for frequency content
  - Filter outputs are spectral power density integrated over the filter bandwidth
- Monolithic integration with active components such as lasers and modulators enables compact, highly functional photonic integrated circuits (PICs)

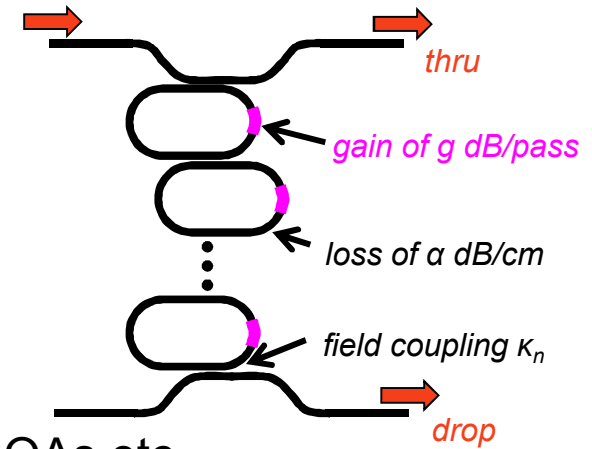
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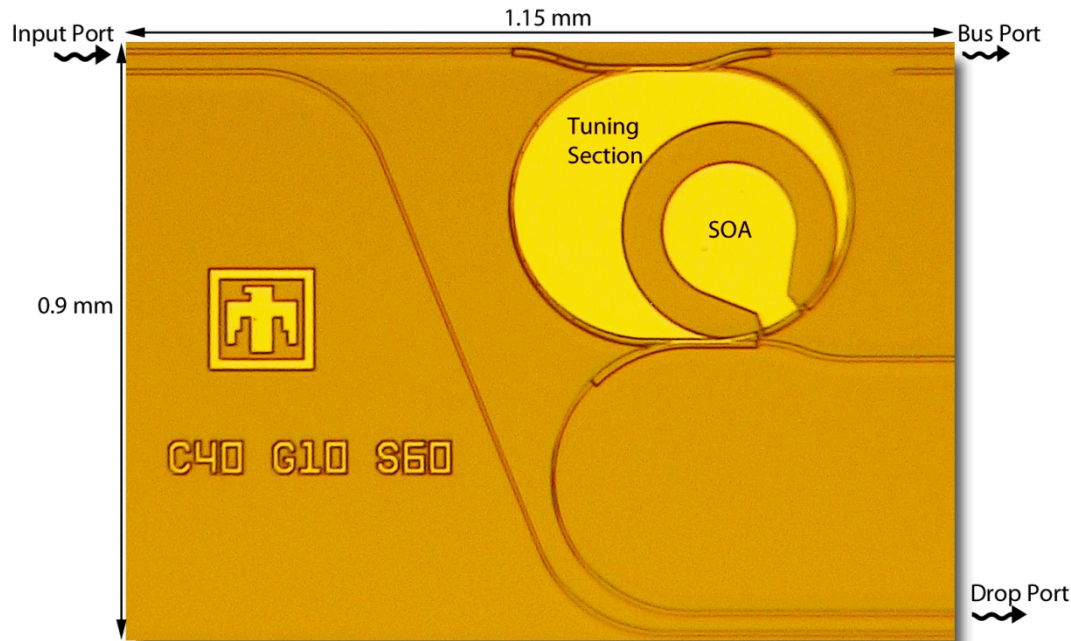
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# Motivation

- Active ring resonators offer:
    - Wavelength selectivity
    - Compact size
    - Low, or zero, back reflection
    - Monolithic integration with lasers, modulators, SOAs etc.
    - Gain elements can be used to compensate for waveguide losses
  - Design Considerations:
    - Bandwidth determined by:
      - Coupler strength and optical loss
    - Filter profile defined by:
      - Coupler strengths and number of rings and internal net loss
    - Extinction ratio influenced by:
      - Noise from optical amplifiers and optical loss
    - Tunability effected by:
      - Size of tuning section and induced loss
- Loss, couplers, and optical gain needs to be tightly controlled



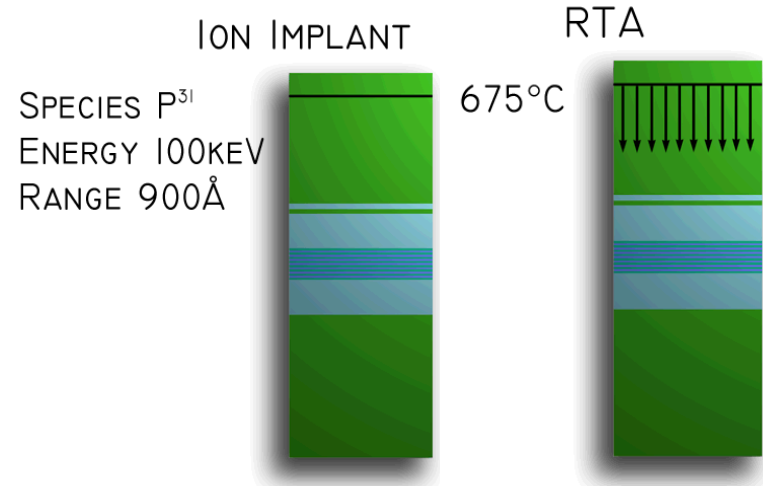
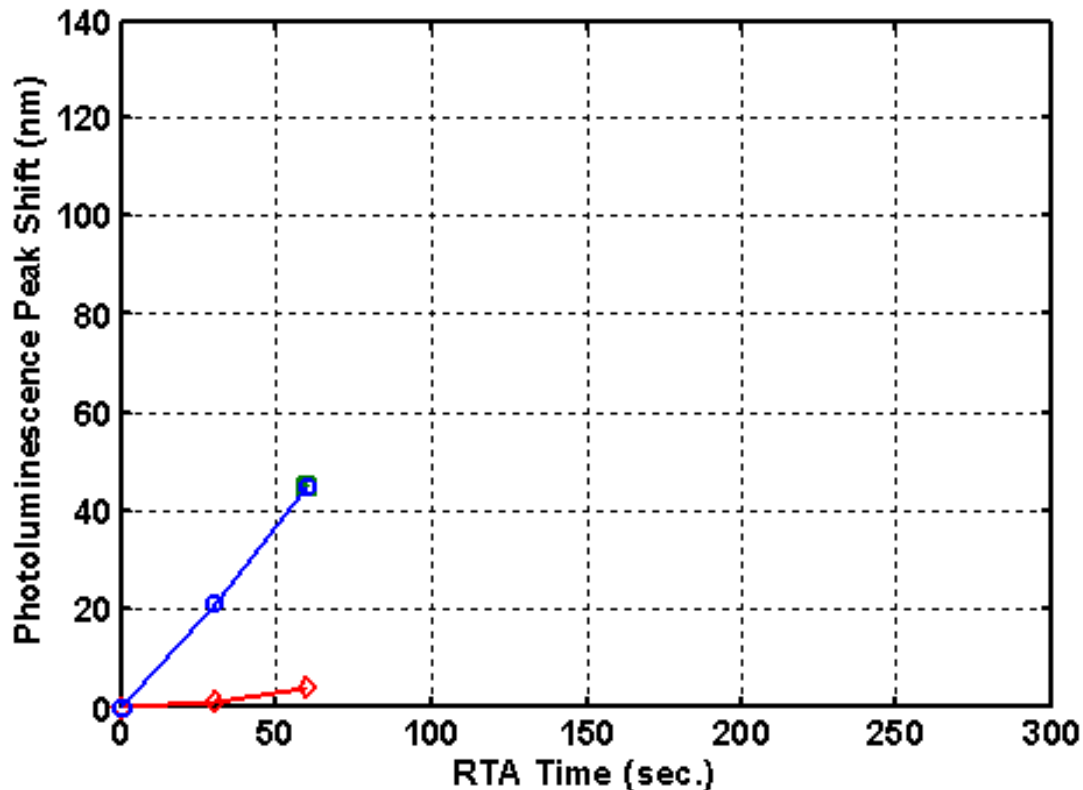
# Approach



- Couplers designed for 1-2 GHz linewidth
  - Fractional coupling power of 6% for both couplers
- Integrated 60- $\mu\text{m}$ -long SOAs in each ring
  - Minimize loss through filter
  - Active/passive integration achieved with quantum well intermixing
  - Length and total gain designed for low noise

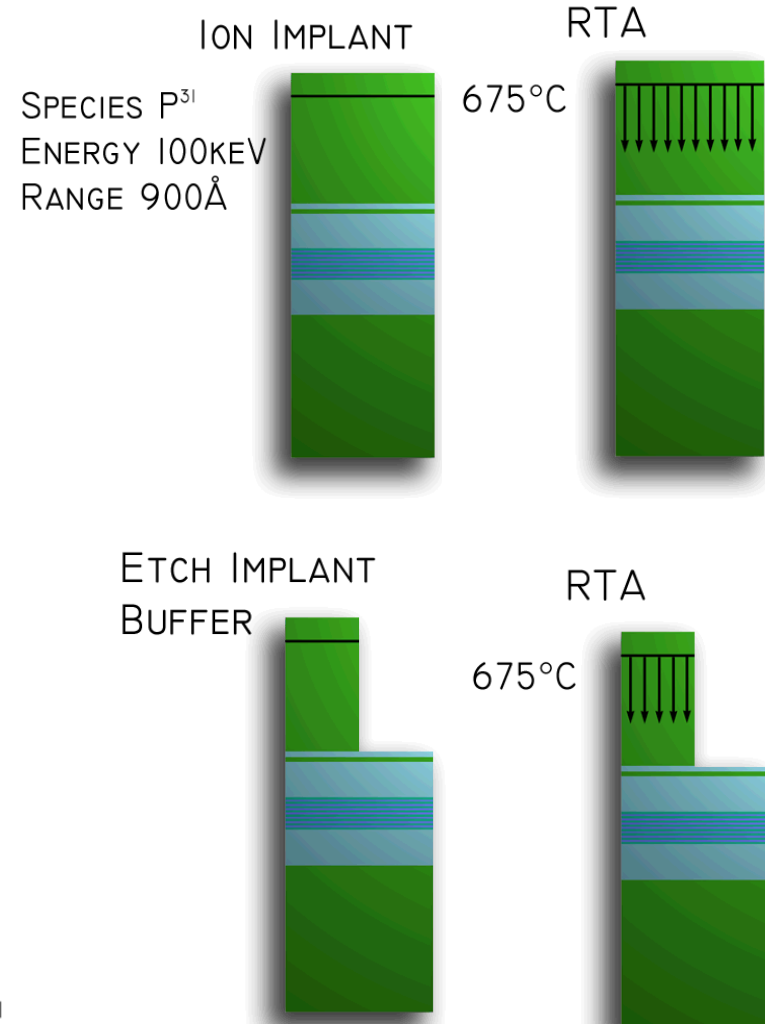
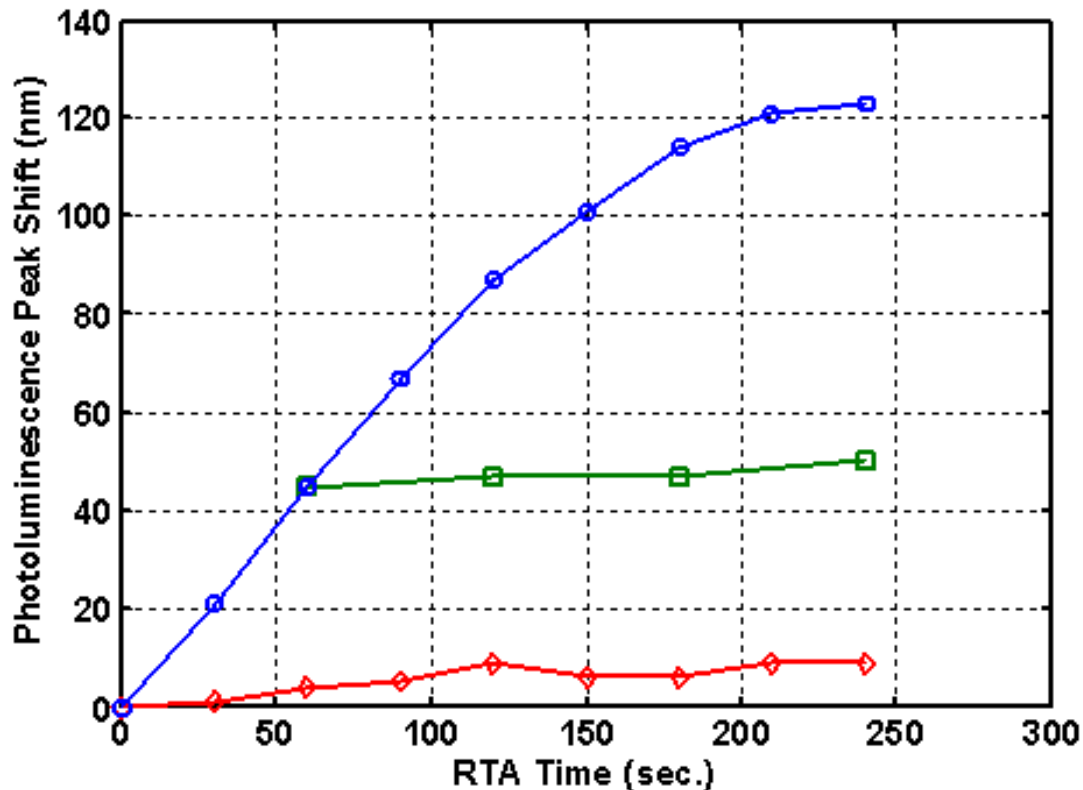
# Monolithic Integration Platform

- Quantum well intermixing
  - Metastable interface between well/barrier
  - Add catalyst to enhance interdiffusion
  - Reshaping increases the energy level
    - Reduces the bandgap wavelength
  - Capable >2 bandedges with same epitaxial base



# Monolithic Integration Platform

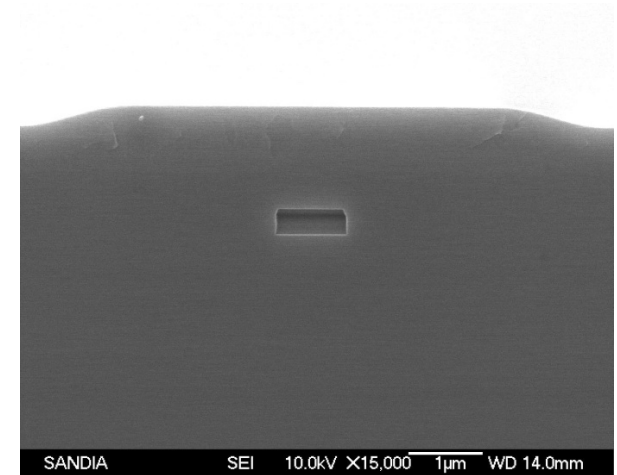
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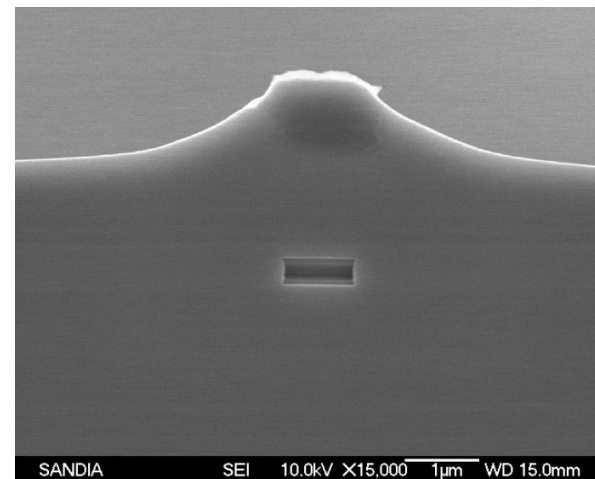
# Buried Heterostucture Waveguides

- Waveguide definition process
  - ASML projection stepper
    - 0.6  $\mu\text{m}$  resolution
  - Dry etch
  - MOCVD Regrowth
    - InP cladding
    - InGaAs contact layer
- Buried heterostucture advantages
  - Waveguide thickness defined by epitaxial material
  - Semiconductor etch only defines guiding width and coupler gap
  - Devices are essentially not affected by variations in etch depth

Waveguides in [011]



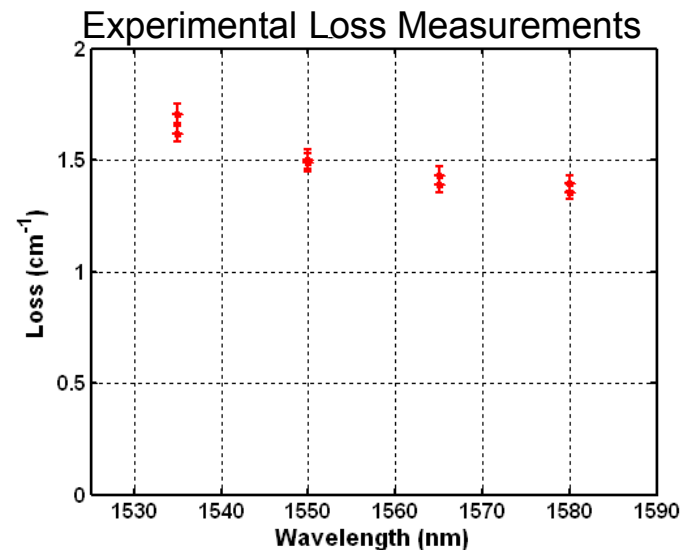
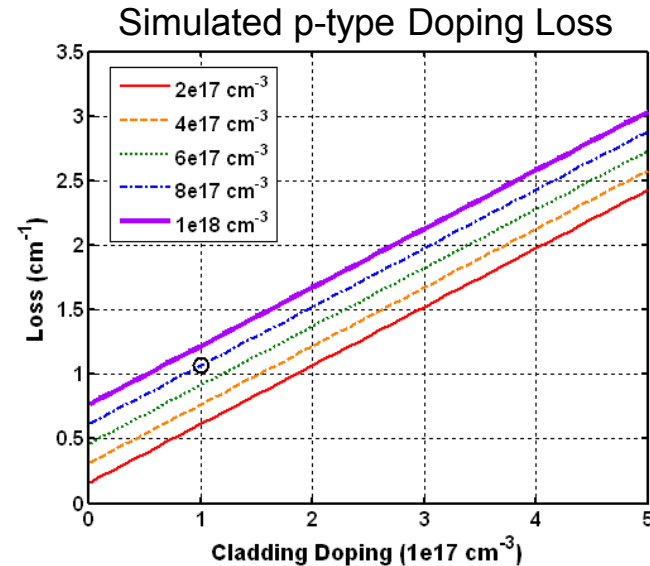
Waveguides in  $[0\bar{1}\bar{1}]$





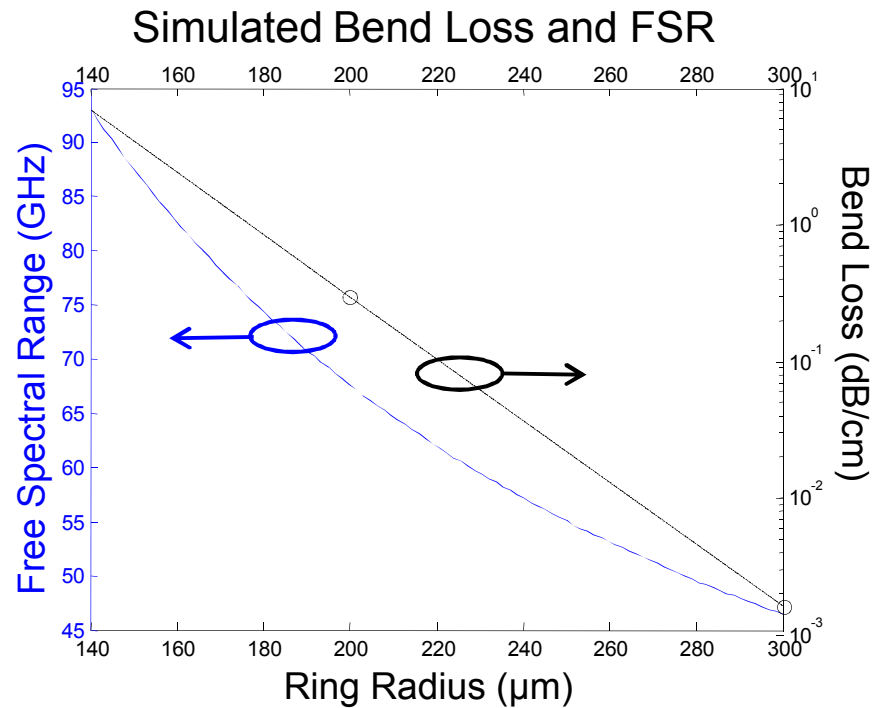
# Low Loss Waveguides

- Low loss waveguides
  - Loss and coupling define the bandwidth of the filter
- Scattering and Absorption Loss
  - Modal overlap with InP p-type doping regions is a major source of loss
    - 500 Å doping spike at the regrowth interface
      - Compensates for Si contamination at the regrowth interface
    - Doping of the regrown p-type cladding
  - Waveguide loss was measured using Fabry-Perot cavity measurements
    - $1.5 \text{ cm}^{-1}$  at 1550 nm



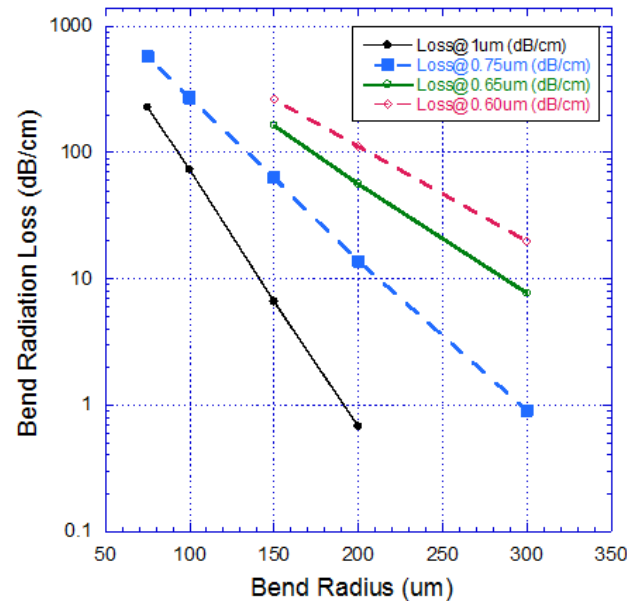
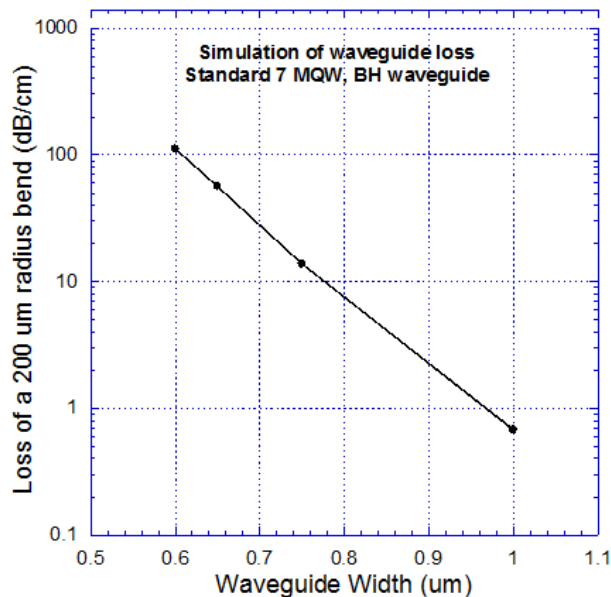
# Low Loss Waveguides

- Low loss waveguides
  - Loss and coupling define the bandwidth of the filter
    - Output coupling and waveguide loss
- Bend loss
  - Tradeoff between loss and FSR
  - 200  $\mu\text{m}$  radius for 1  $\mu\text{m}$  waveguide width



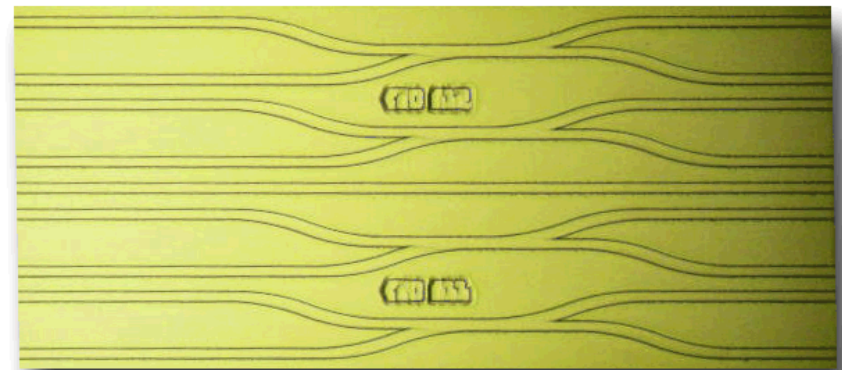
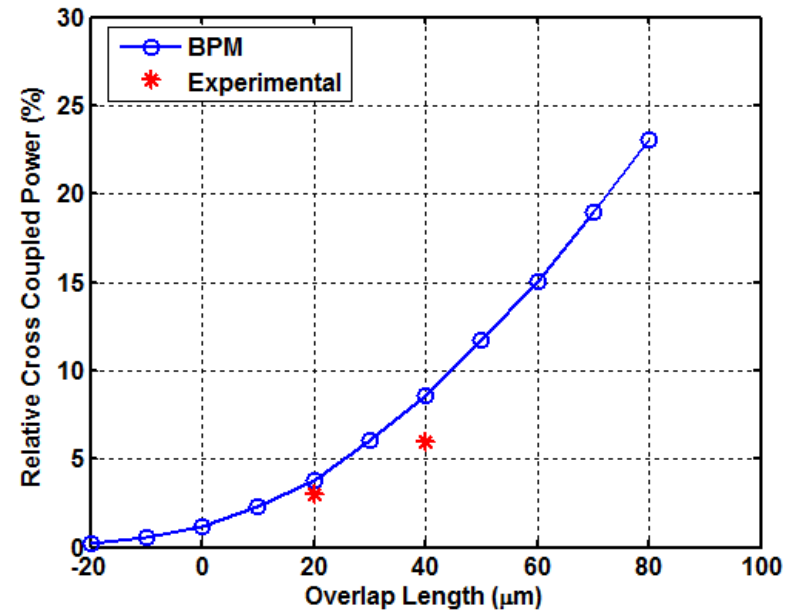
# Low Loss Waveguides

- Waveguide width is very important to bend loss
- Lithographic bias can significantly effect bend losses
  - Projection lithography/stepper used
  - Dimensions verified by CD SEM measurements
    - Monitors bias drift over time
    - Done before waveguide etch allowing for rework.



# Couplers

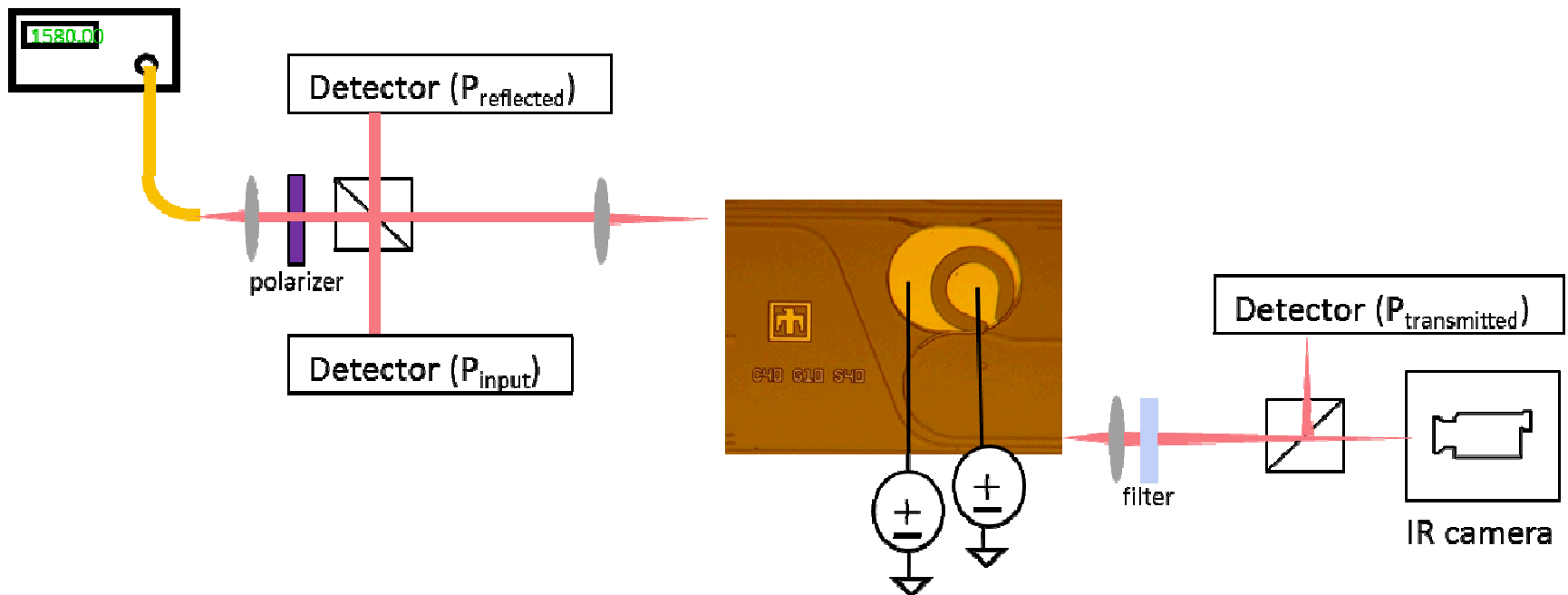
- Coupler design
  - Couplers utilize 1  $\mu\text{m}$  waveguides with 1  $\mu\text{m}$  gap
  - Coupling defined by length overlap region
  - Lithography biases are constant
  - Consistency in coupler values within and between process runs
- Simulations used to predict coupling
  - BPM simulation
    - Includes waveguide bends
  - Experiment shows lower coupling than predicted by BPM
    - Waveguide widths and gap has a bias due to fabrication



# Experimental results

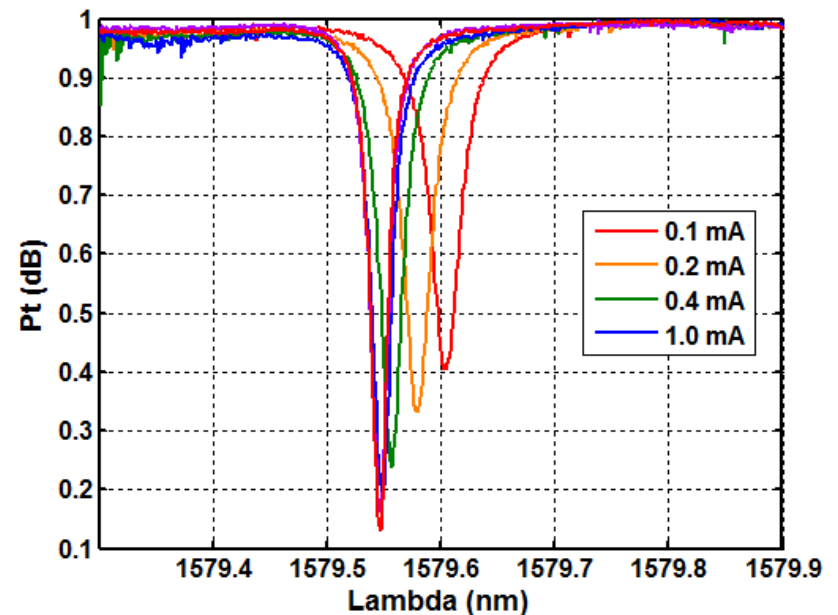
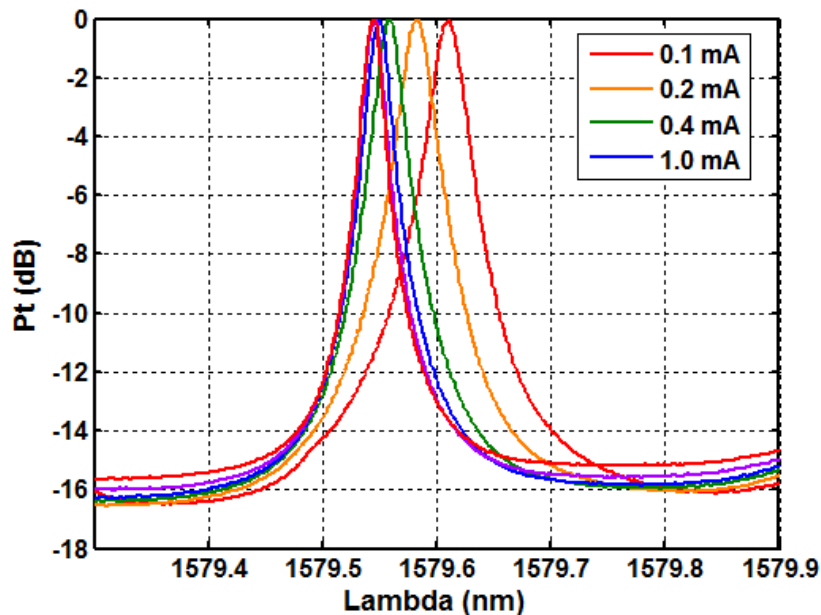
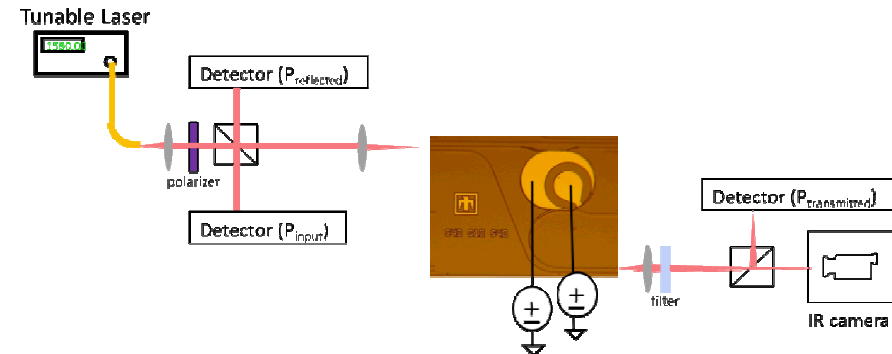
- Scanning source measurement
  - Wavelength swept on a tunable laser source
  - 12 nm filter added to the ring output
    - This filters out much of the ASE from the SOA

Tunable Laser



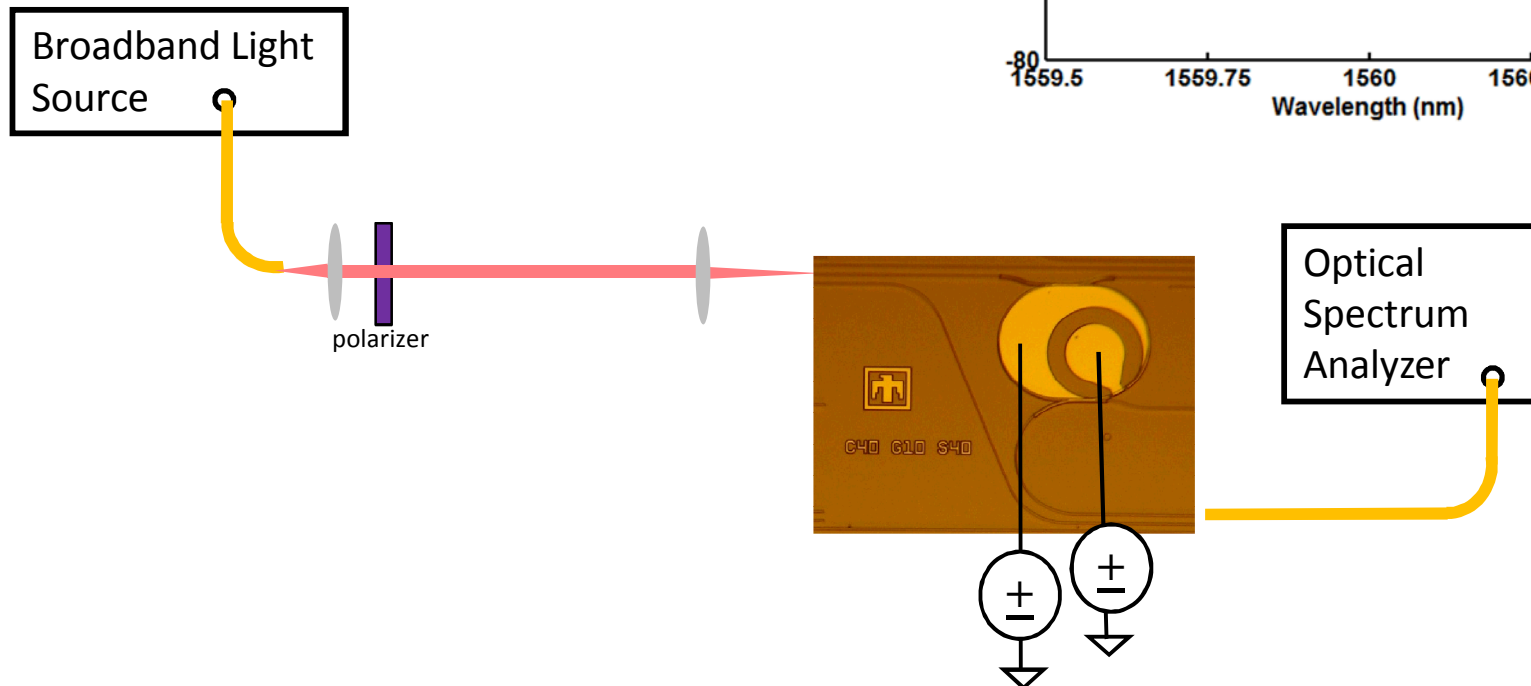
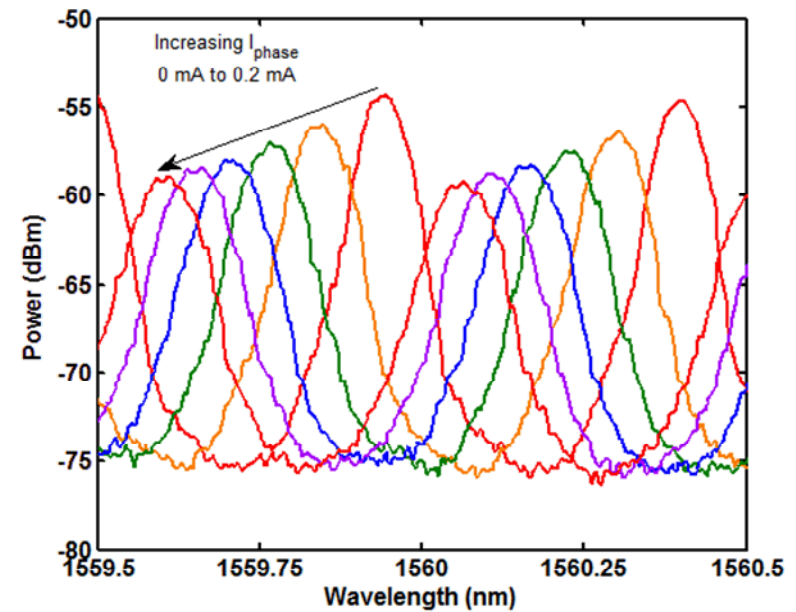
# Experimental results

- Scanning source measurement
  - Variation in SOA current from 0.1-1.0 mA
  - >15 dB extinction
  - 3.47 GHz to 2.16 GHz FWHM optical linewidth



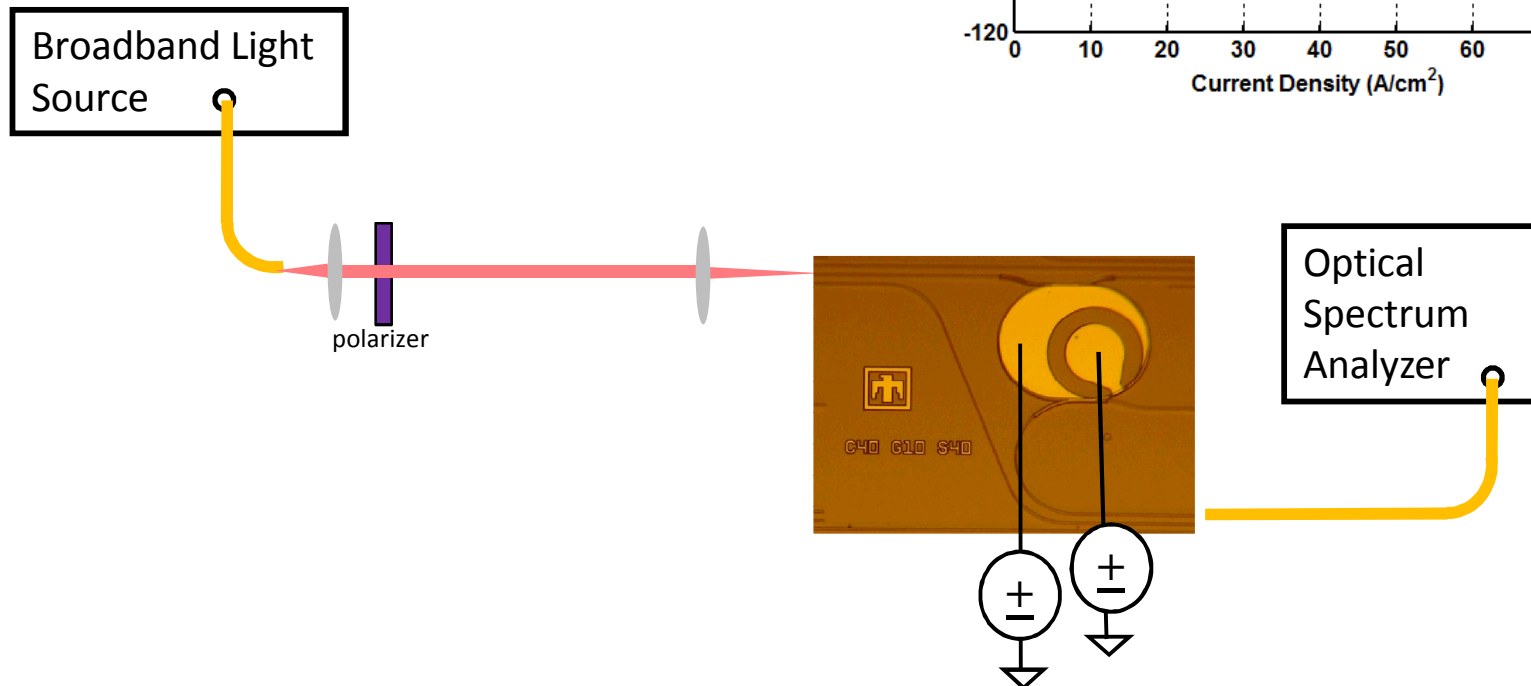
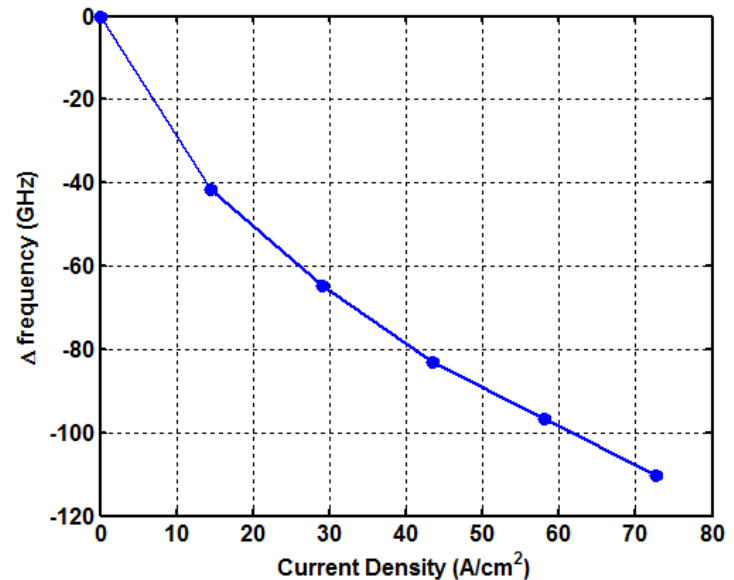
# Experimental results

- Optical spectrum analyzer measurement
  - Broadband light source
  - Ring output fiber coupled to OSA
  - Better for larger wavelength scans
  - $I_{\text{SOA1}} = 2 \text{ mA}$
  - Extinction ratio of  $>15 \text{ dB}$



# Experimental results

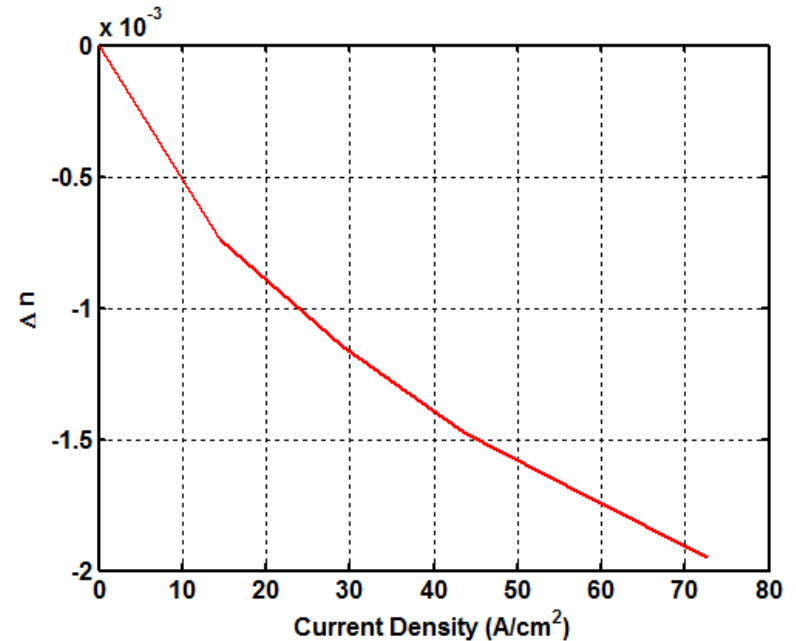
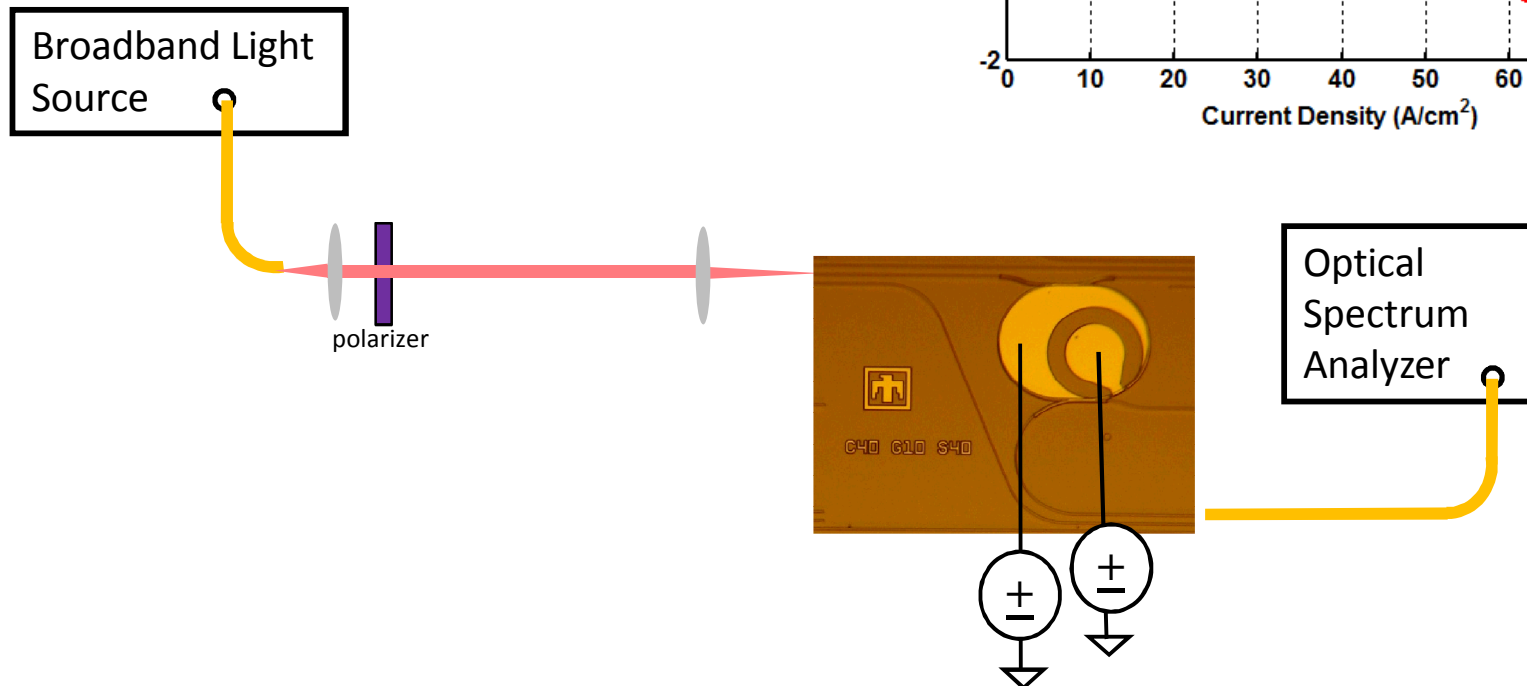
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  - $I_{\text{SOA1}} = 2 \text{ mA}$
  - Extinction ratio of  $>15 \text{ dB}$
  - $110 \text{ GHz}$  with  $I_{\text{Tune}} = 1 \text{ mA}$ 
    - Nearly twice the free spectral range



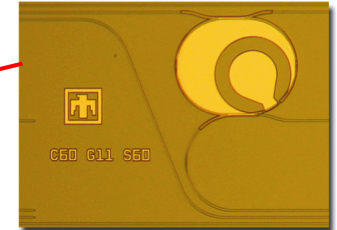
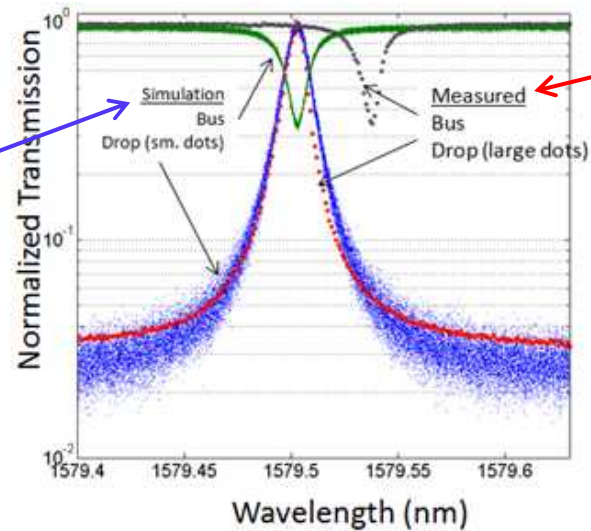
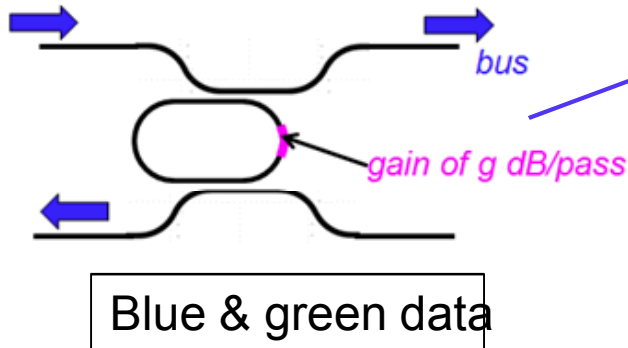


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# Simulation benchmarking

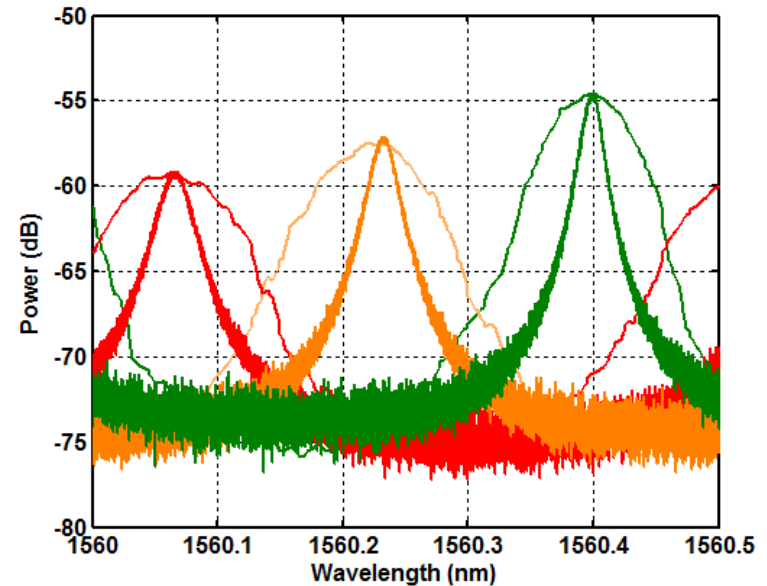


Red & black data

- Complete simulation of dynamic range and noise of active InGaAsP multi-ring filters
  - Include gain distortions and spontaneous emission noise
- Time dependent rate equation method
  - Gain and spontaneous emission modeled as function of injection current at all wavelengths simultaneously
- Fit experimental bandwidth of drop and extinction of bus to extract net round trip loss and coupling fraction
  - 6% coupler with  $1.4 \text{ cm}^{-1}$

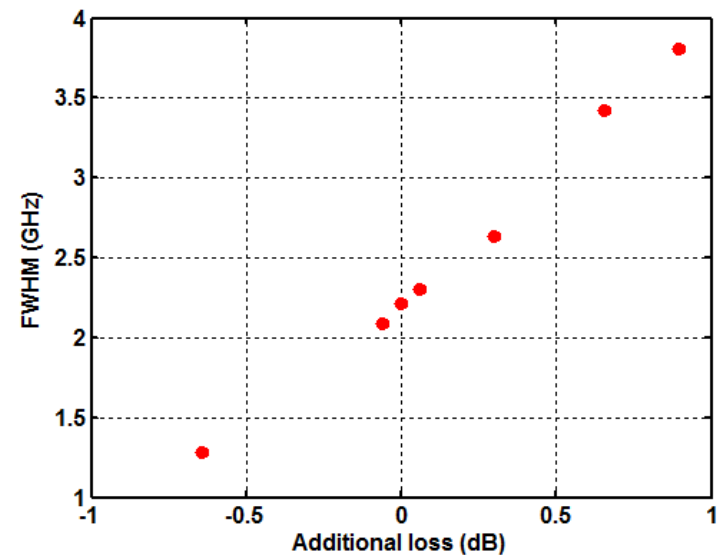
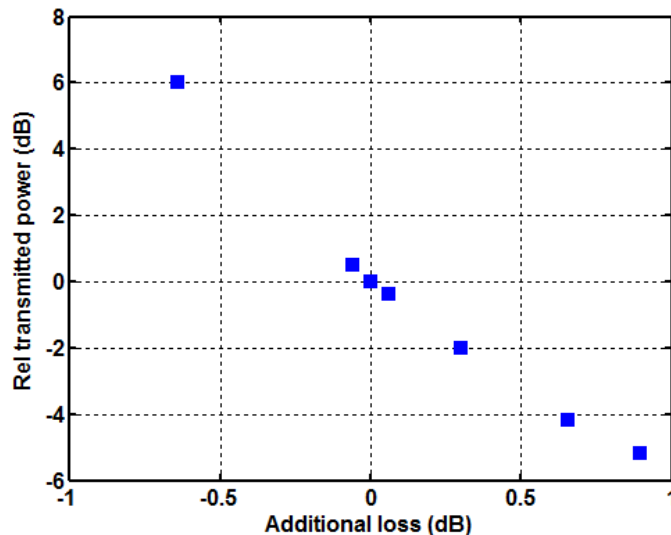
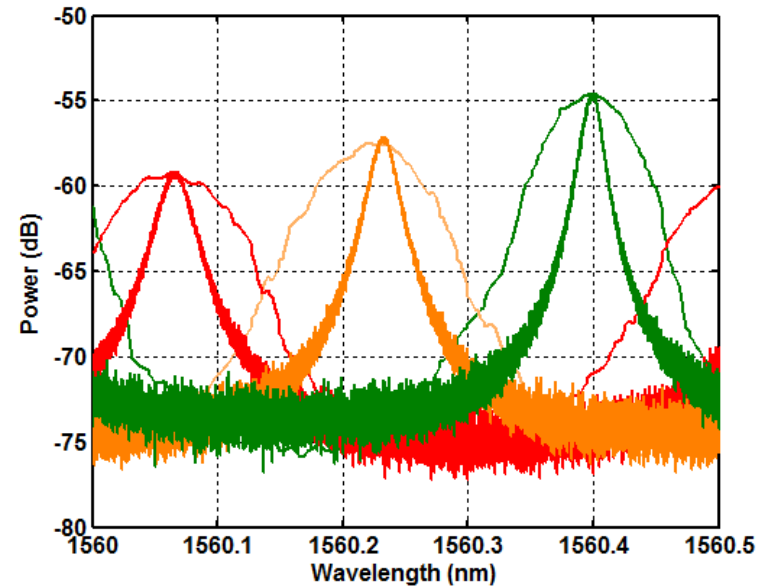
# Simulation

- Tuning and loss from benchmarked from filter tuning data
- Effects of tuning induced loss on FWHM linewidth
- 0.9 dB of additional loss caused by tuning current
  - reduces peak power 5 dB
  - Increase FWHM by 1.6 GHz
- Loss can be compensated for by increase in SOA gain



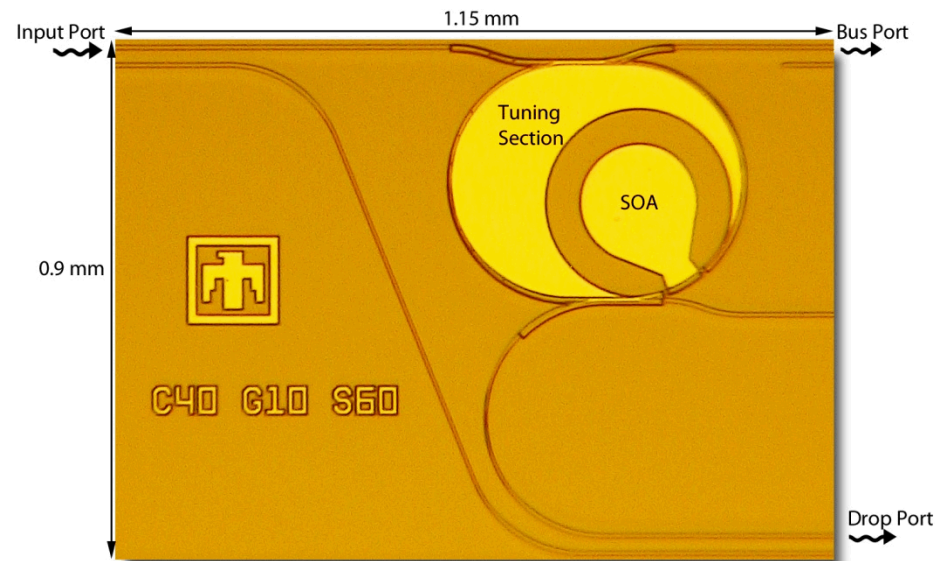
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# Conclusions and Future Work

- Fabricated and demonstrated tunable ring filter
  - Process compatible with monolithic integration of lasers and modulators
  - >15 dB extinction
  - 56 GHz free spectral range
  - 2.17 GHz passband
- Future work will focus on:
  - Integration with lasers and modulators
  - Measure insertion loss and bus channel characteristics
  - Exploring offsetting loss with SOA gain to maintain constant peak power
    - Look at SNR and dynamic range

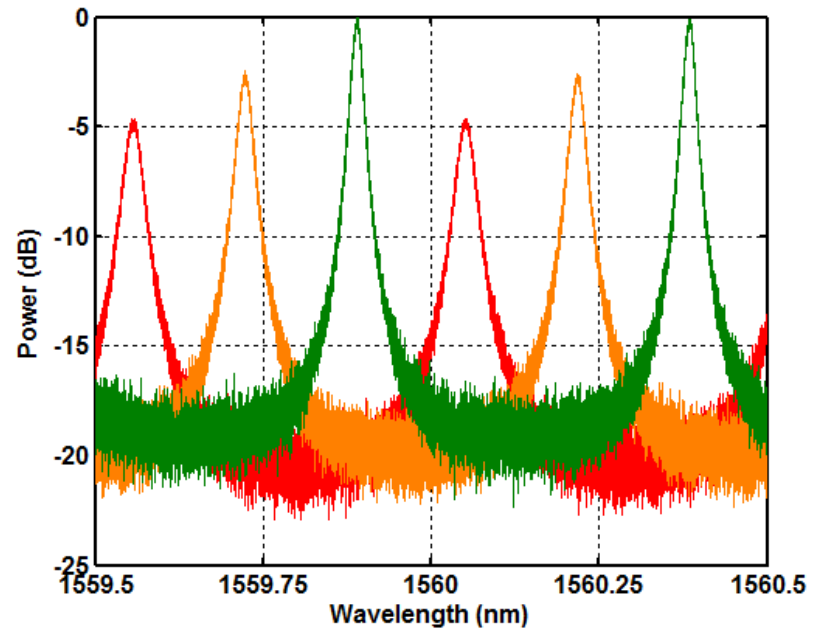






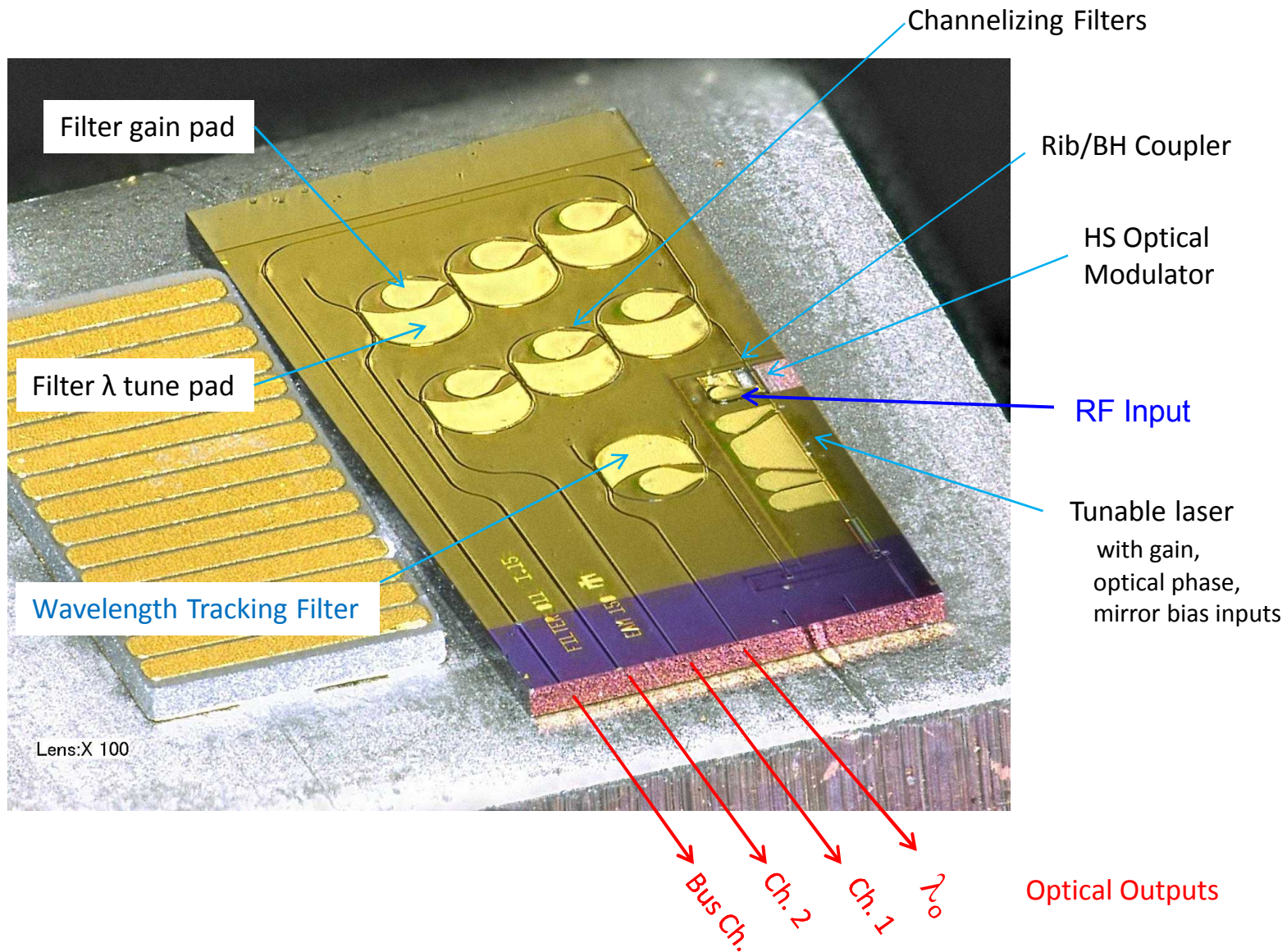
# Backup Slides

# Simulation benchmarking





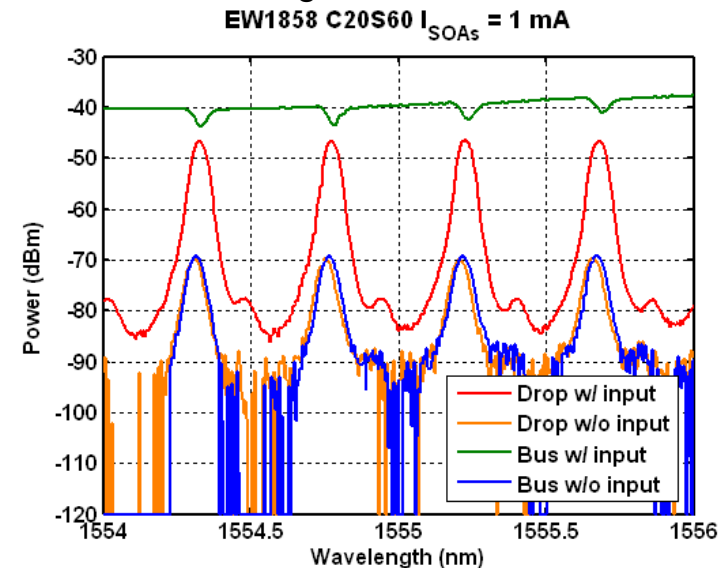
# Full PIC design



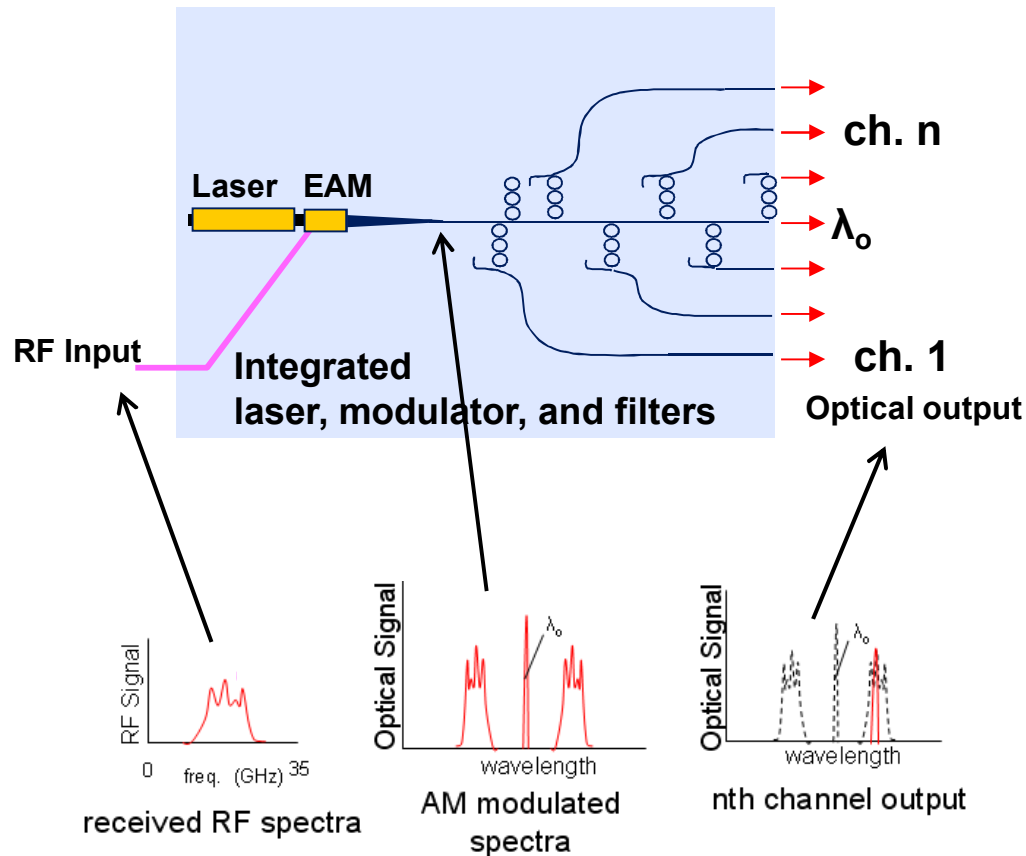
# InP Active 2-ring Filter

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on fig

- ASE source and OSA
  - Higher extinction
    - SOA-ASE goes is correct wavelength 'bin'
- Tunable laser and photodiode
  - Lower extinction
    - off resonance measurement includes SOA-ASE from all wavelengths
  - A filter ( $\sim 5$  nm) will give results similar to OSA
    - This can be external for testing
    - On a monolithic chip we need to add additional filtering

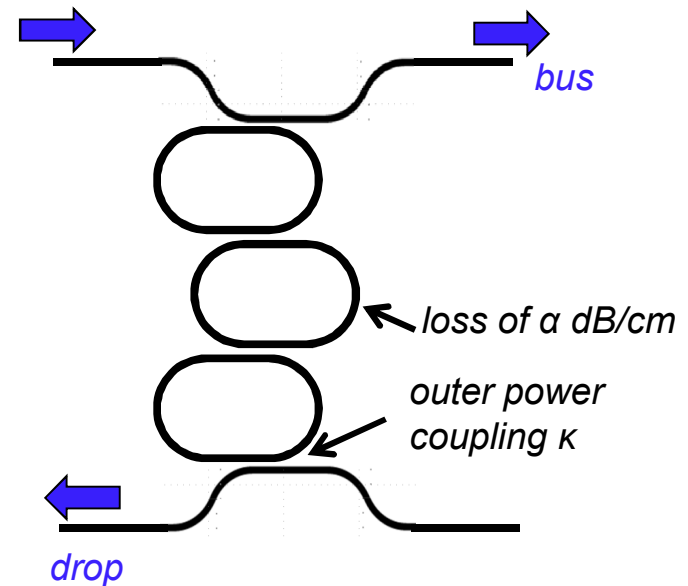
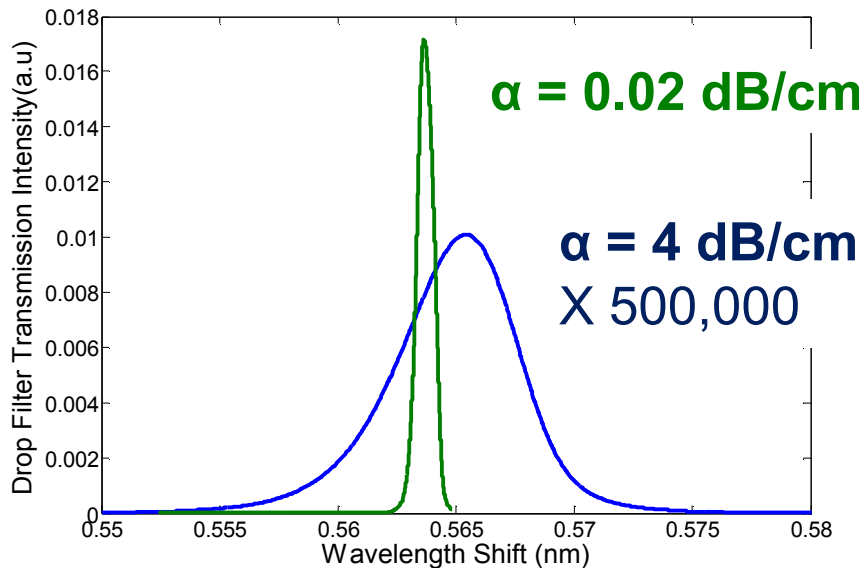


# Channel-Dropping Filters

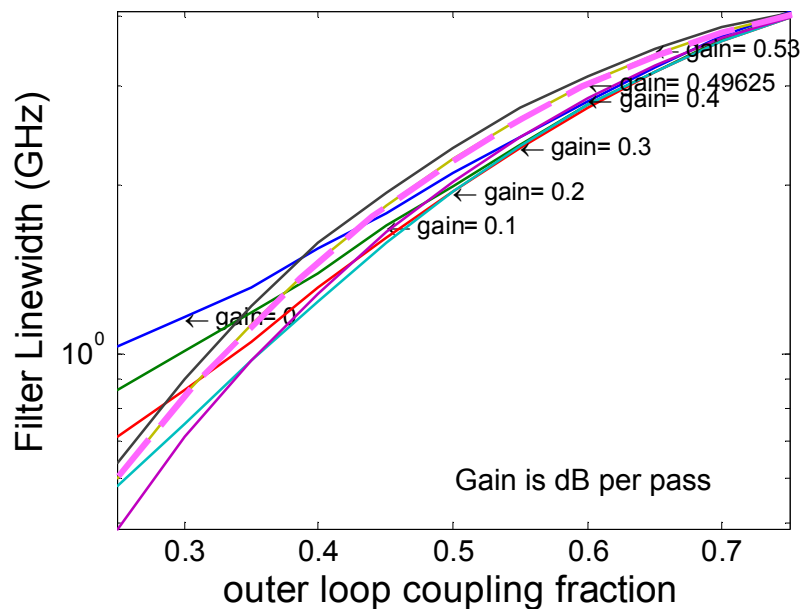
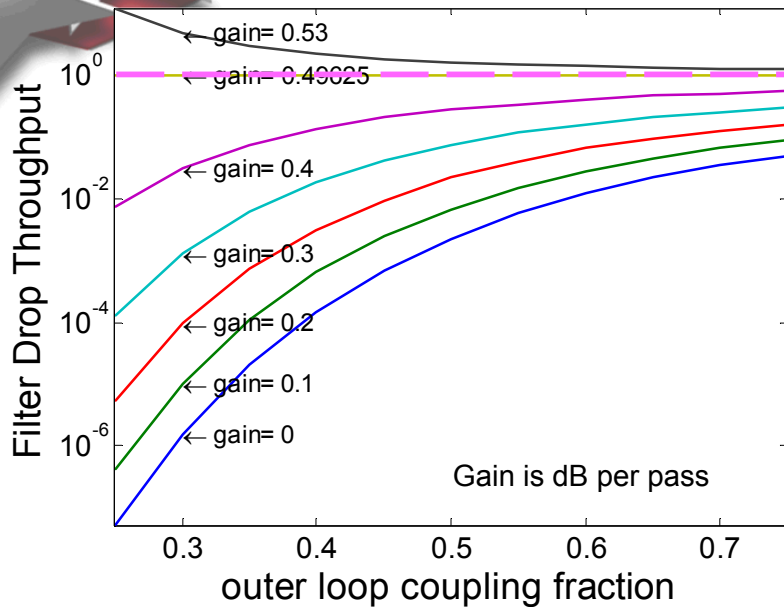


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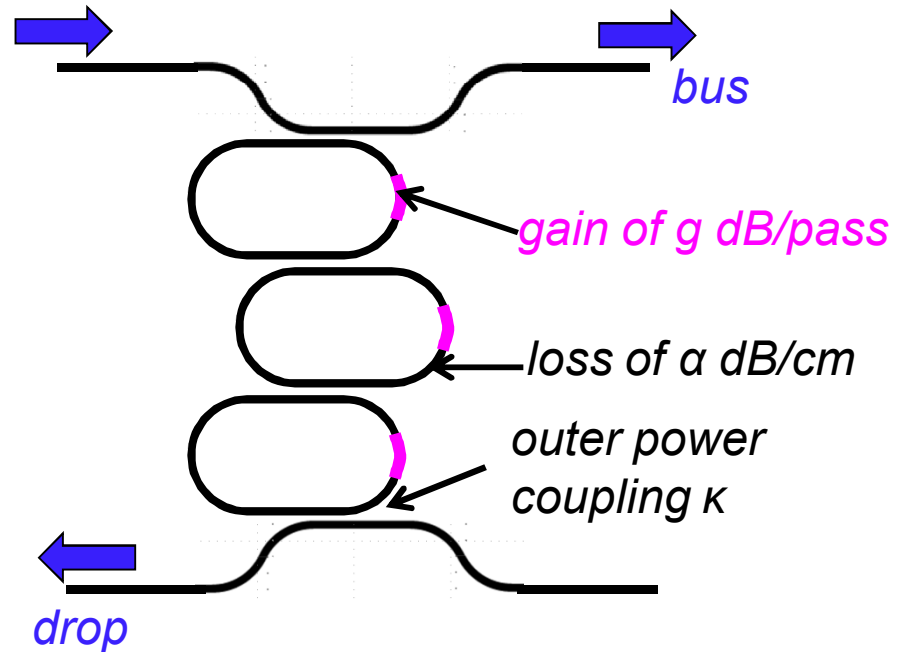
# Monolithic Integration and Loss-Limited Filter Response



- Optical waveguide losses dominate the filter performance
- Useful passive ring resonant filters are typically made of glasses or undoped semiconductors with very low optical loss.
- Ring Filters with losses commonly seen in doped InGaAsP waveguides for active PICs have too little optical transmission to be useful as GHz-class filters



## A Small Amount of Gain Offsets Losses



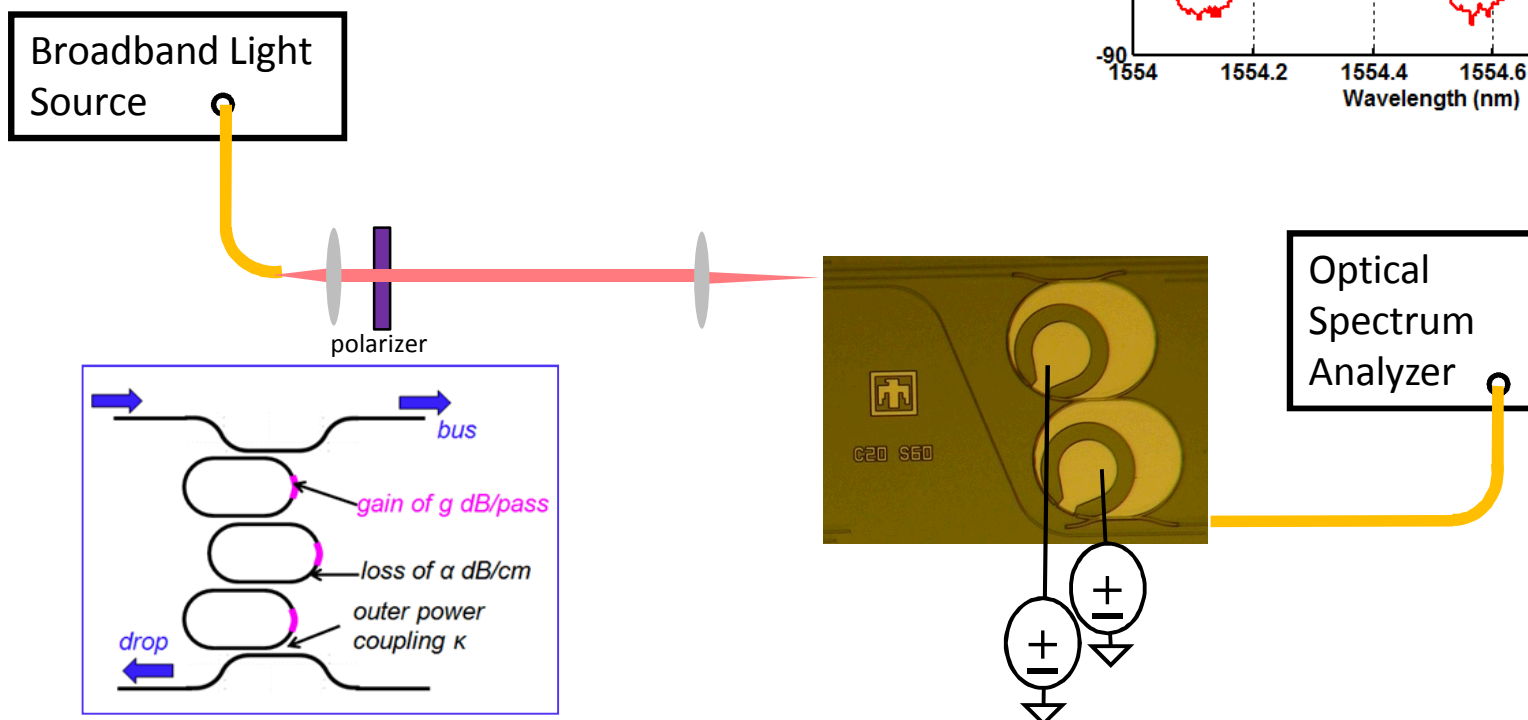
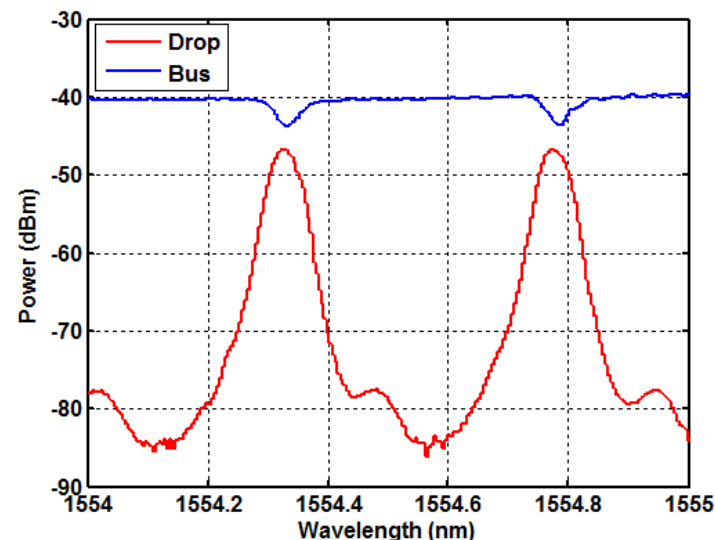
- SOAs enable monolithic integration
- Introduce an ideal loop gain to each filter
  - No noise in model, yet
- Ring waveguide loss
  - 4 dB/cm
- Loss-less filter achieved
  - 0.5 dB/pass gain element



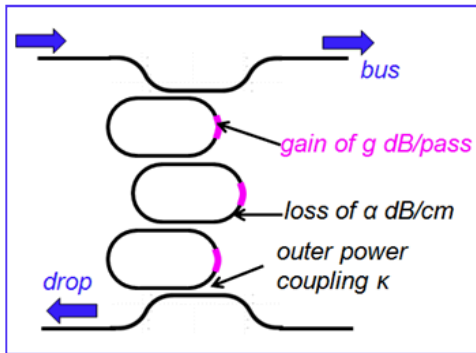
# Active Rings : Experimental

See paper OThW2  
Thur. @ 4 pm

- Dual-ring filters
  - > 30 dB extinction ratio
  - 2.5 GHz linewidth
  - $I_{\text{SOA1}} = I_{\text{SOA2}} = 1 \text{ mA}$
  - Extinction ratio of >30 dB
  - Filter loss of 1.7 dB
    - Loss defined as total power on resonance compared to total power off resonance
- OSA measurement
  - Broadband light source



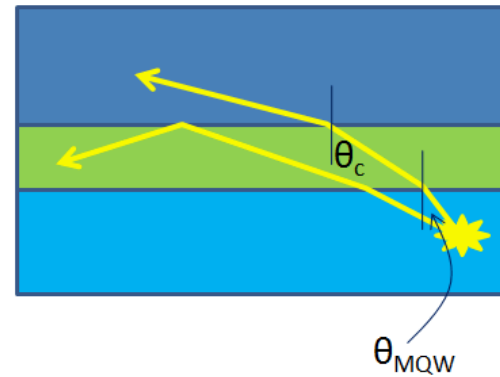
# Active filter modeling



- Time domain travelling wave model of single and multi-ring filters
- Semiconductor Optical Amplifier (SOA) embedded in each ring
- Local gain and spontaneous emission modeled as functions of injection current and optical power
  - Time-dependent rate-equation approach
- Complete power spectra computed at each time step

# Fraction of SOA spontaneous emission coupled into waveguide mode

- Amplified spontaneous emission (ASE) noise from SOAs creates a noise floor on filter spectra
- ASE noise computation in two steps
  - Spontaneous emission recombination event
  - Coupling of spontaneous emission into guided mode of ring
- The spontaneous emission factor influences the noise floor due to ASE



- Indexes
  - InP,  $n = 3.168$
  - Q13,  $n = 3.3877$
  - MQW,  $n = 3.427$
- Included angle of captured light
  - 44.8 deg
- Area of spherical cap
  - $A_{cap} = 2\pi r h$
  - $H = r(1 - \cos\theta)$
- Area of sphere
  - $A_{total} = 4\pi r^2$
- Fractional area
  - $A_{cap}/A_{total} = (1 - \cos\theta)/2$
  - $\theta = 22.4$  deg
  - Fractional area = 0.0378
- Fraction of light capture by guided mode
  - Multiply fractional area by overlap integral with guided mode
  - $\Gamma(\text{fractional area}) = 0.06989 \times 0.0378 = 0.00264$
- $SponBetaNA = 0.00264$



# Model of Active Ring

0.1 mW  
1.54  $\pm$   $\Delta$   $\mu$ m

Bus

Drop

Radius: 200  $\mu$ m

Couplers: 17% power cross-coupling

Passive guides: 3  $\text{cm}^{-1}$

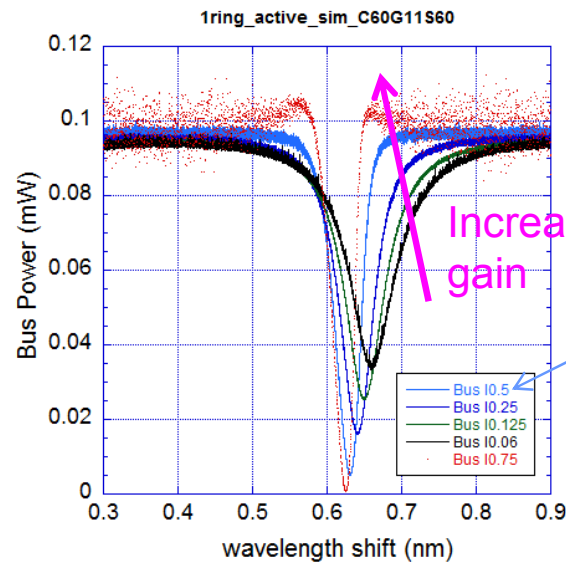
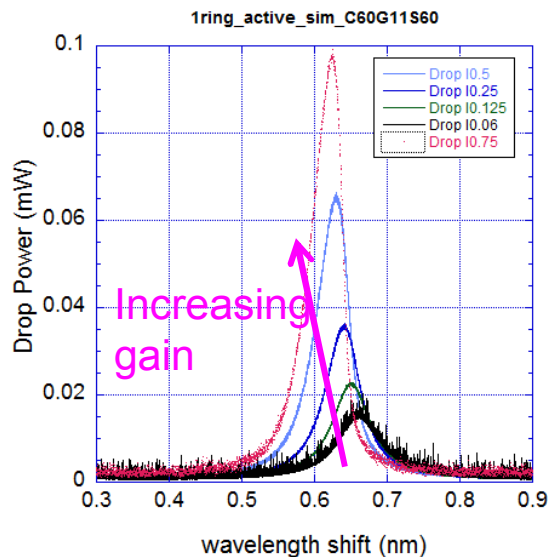
SOA: 60  $\mu$ m long

7 QW centered, 25C

1  $\mu$ m wide BH

current flow *only* in the MQW

Spontaneous Coupling: 0.0037



$J = 830 \text{ A/cm}^2$   
 $I = 0.5 \text{ mA}$

- Variation of SOA injection current
  - Insertion loss drops and bandwidth narrows as SOA current is increased

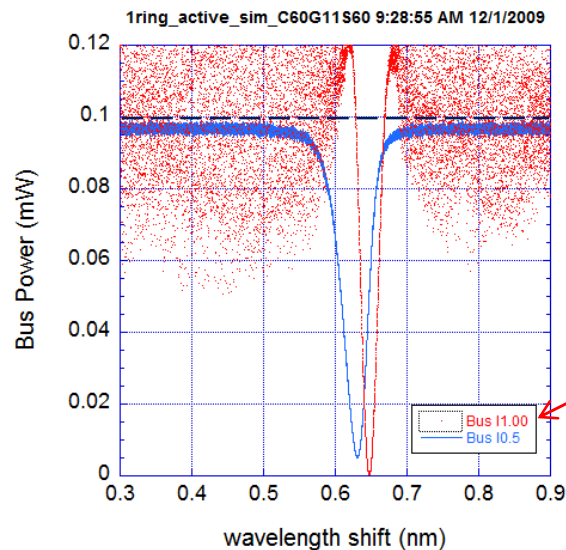
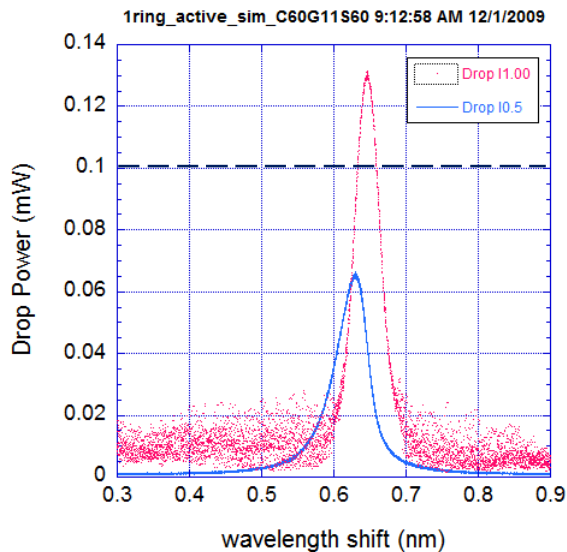
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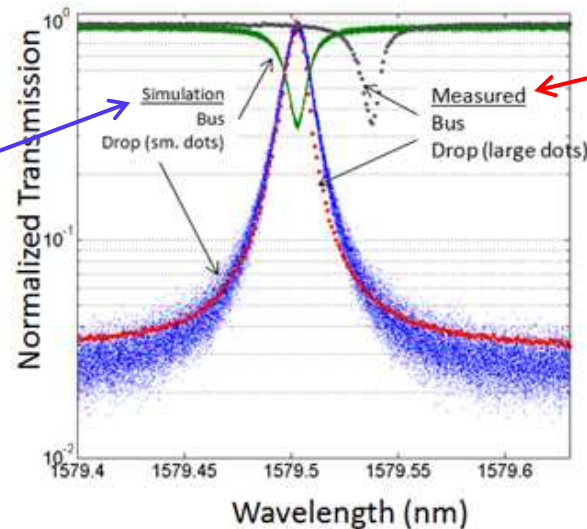
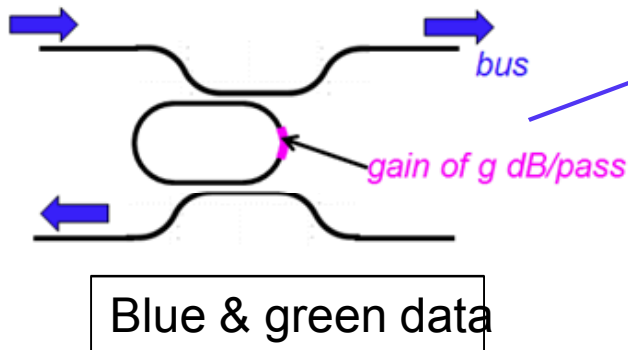
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SOA: 60  $\mu\text{m}$  long  
7 QW centered, 25C  
1  $\mu\text{m}$  wide BH  
current flow *only* in the MQW  
Spontaneous Coupling: 0.0037



$J = 1.67 \text{ KA/cm}^2$   
 $I = 1.0 \text{ mA}$

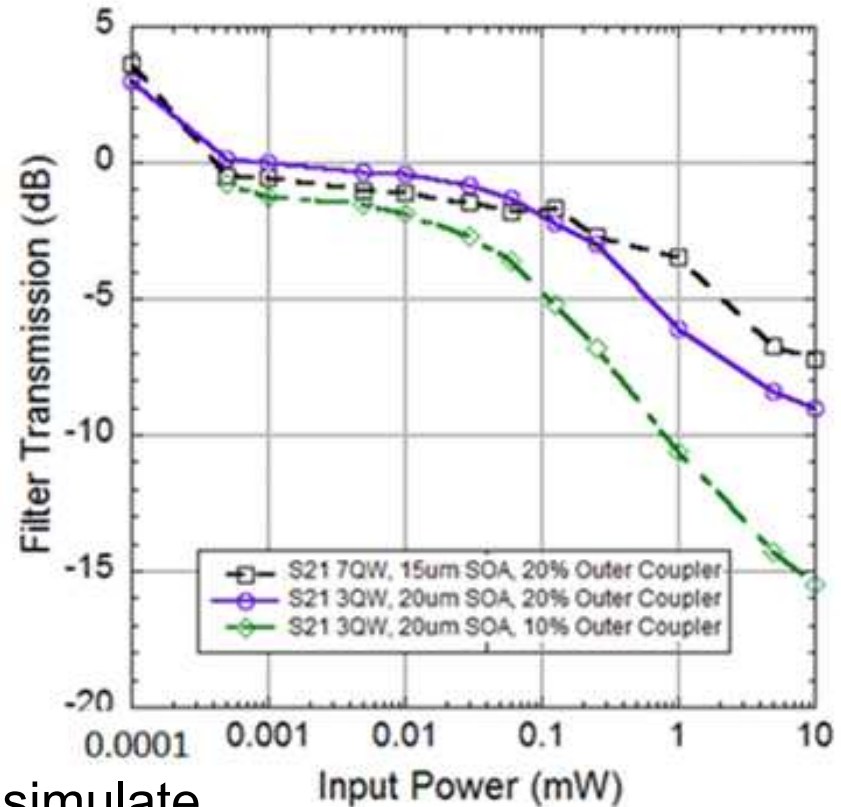
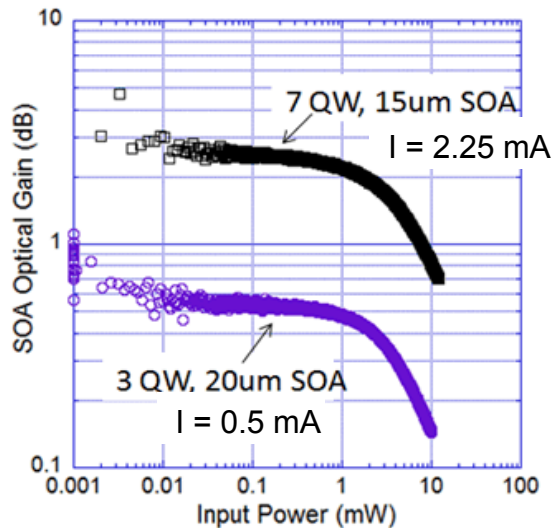
- Operation at very high gain (SOA injected current)
  - Negative insertion loss achievable, but very noisy

# Single Ring Active Filter: Simulation Benchmark to Experiment



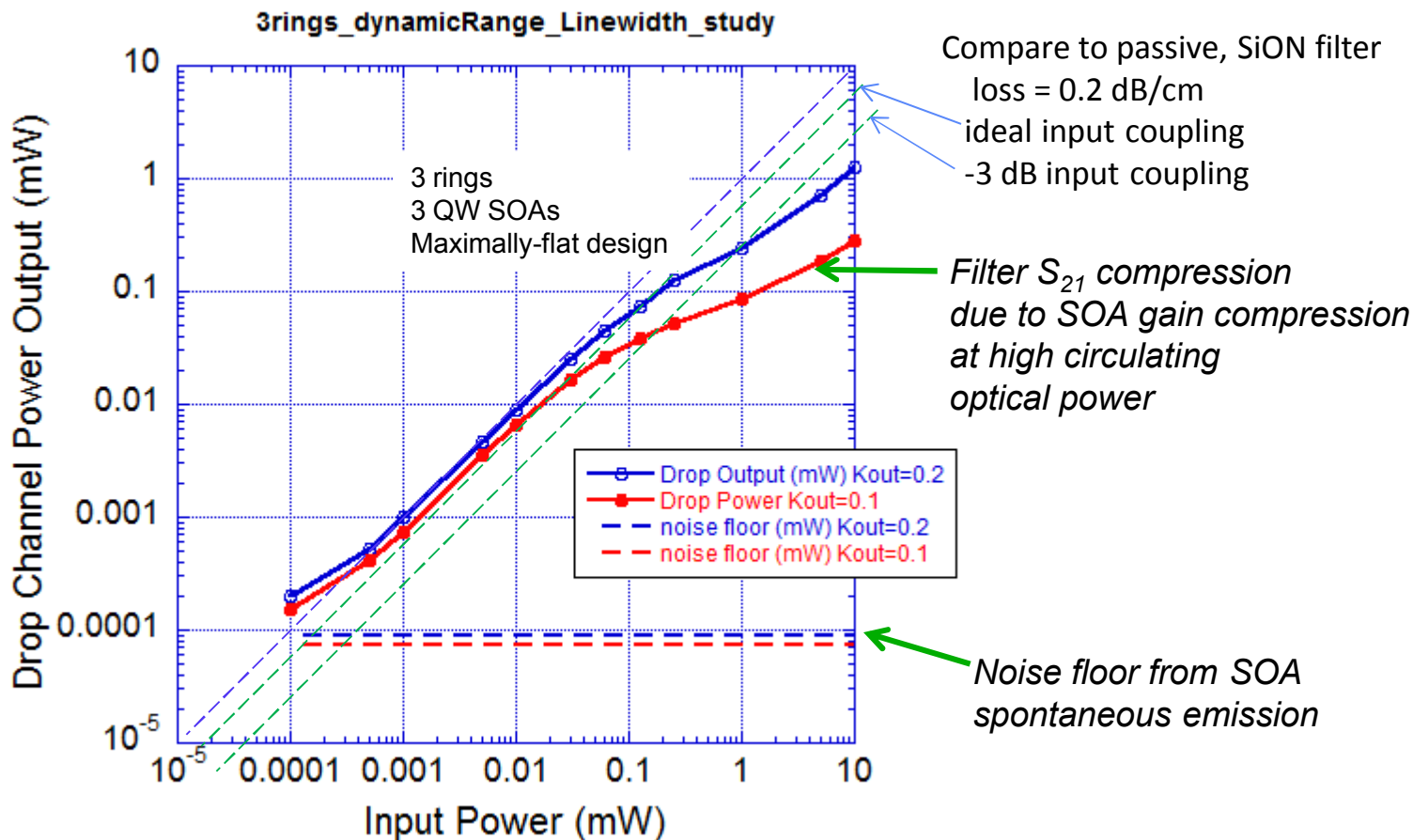
- Complete simulation of dynamic range and noise of active InGaAsP multi-ring filters
  - Include gain distortions and spontaneous emission noise
- Time dependent rate equation method
  - Gain and spontaneous emission modeled as function of injection current at all wavelengths simultaneously

# 3-ring active filter simulations



- For 3-ring maximally flat filters simulate
  - Linewidth, Insertion loss
  - Dynamic range and Noise floor
- SOA gain and power saturation depend on key factors
  - Number and configuration of QWs and Injected current
  - Simulate case of both 3 and 7 QW SOA

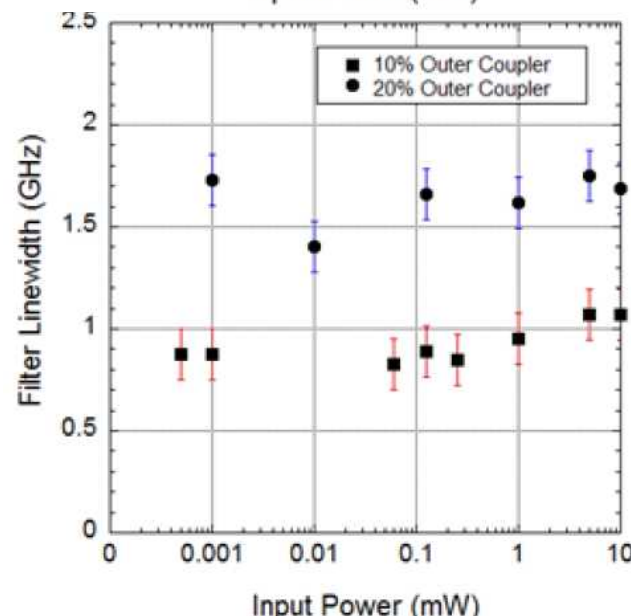
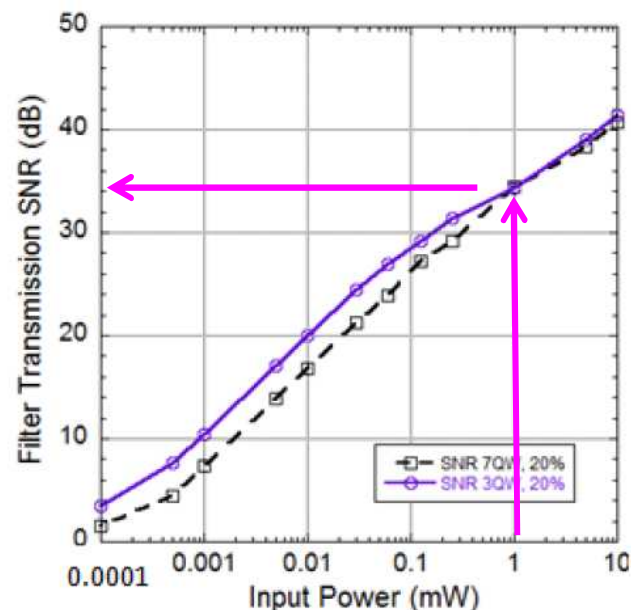
# InP Filter Dynamic Range



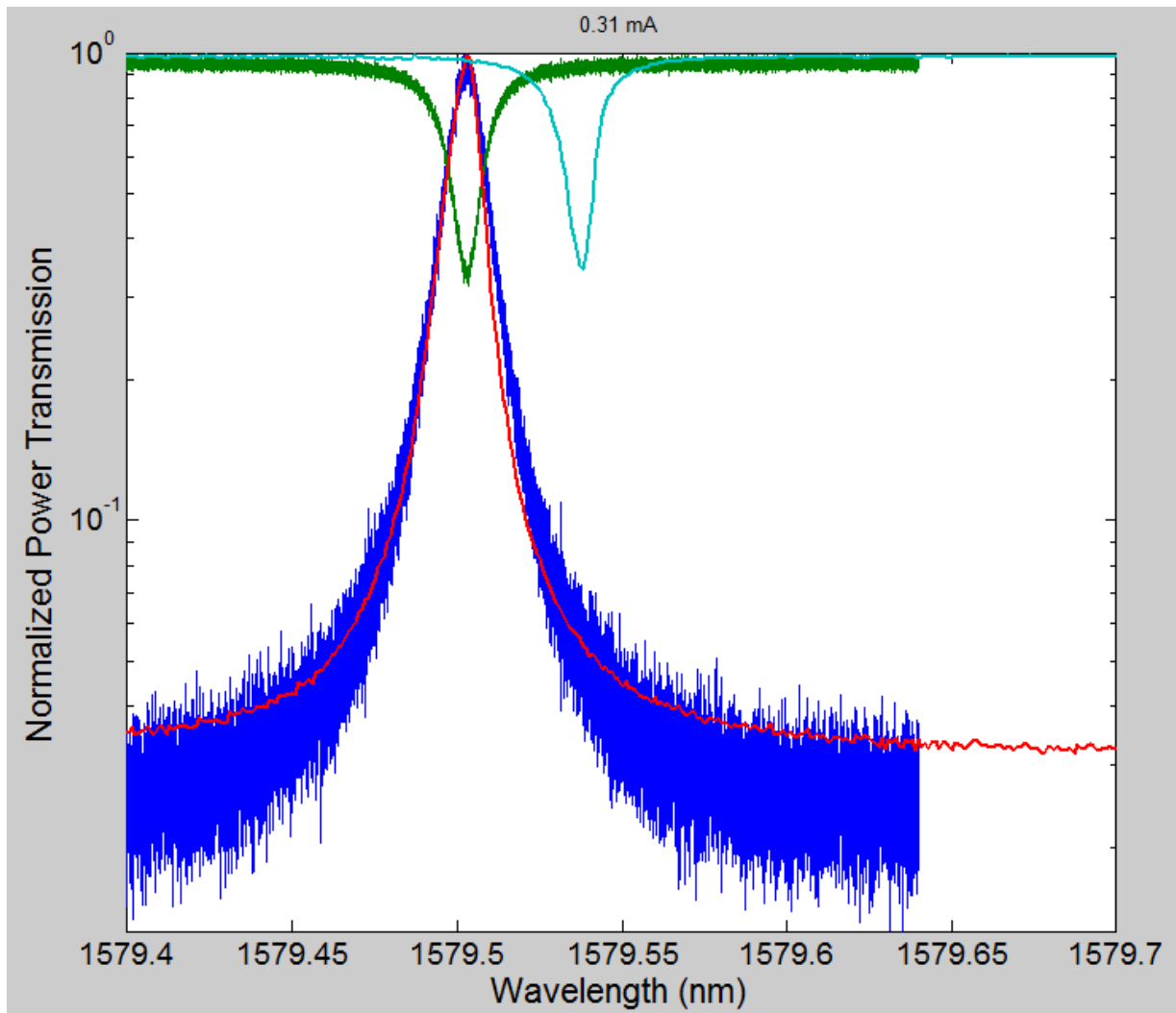
- Active InGaAsP filter shows improved filter transmission compared to passive SiON design over >30 dB dynamic range
- Spontaneous emission noise in SOAs limits SNR at lowest input optical powers
- SOA saturation causes compression of filter  $S_{21}$  at resonance at high end of input power

# Summary

- Time domain model of active ring with SOAs developed
  - SOA model includes gain saturation and ASE
- 3-ring filter with 3 and 7 quantum well gain sections simulated
  - Optical linewidth
  - Noise floor
  - Linearity and dynamic range of  $S_{21}$  versus input power
- InP active filters show promise for frequency-domain signal processing in monolithic integrated photonic integrated circuits
  - 50 dB input dynamic range
    - Output compressed at high power
  - 0 dB loss in mid range accessible for 1 GHz filters
  - Filters with power gain are possible but quickly become limited by noise
  - Possible methods to improve dynamic range
    - Reduce optical confinement factor
      - Balance against lower gain or more complex offset active lasers in remainder of PIC
    - Wider SOAs
    - More pump current



# Best Fit to C20G10S100, EW1858

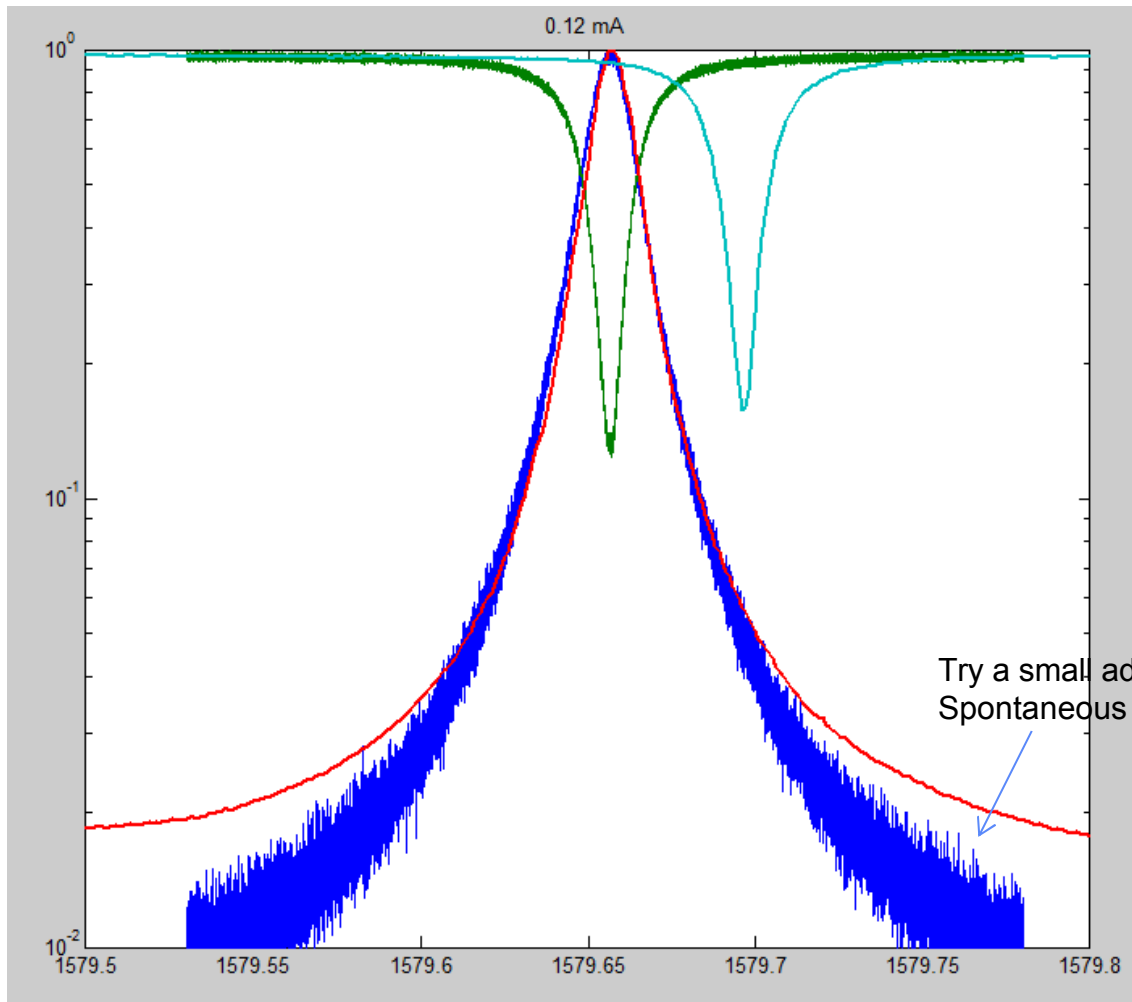


- 8 QW offset
- 100  $\mu\text{m}$  SOA
- $K^2 = 0.03$
- Loss = 1.4  $\text{cm}^{-1}$
- $P_{\text{in}} = 0.005$  mW
- $I_{\text{SOA}}$  model
  - 0.31 mA
- $I_{\text{SOA}}$  exp
  - 1 mA

Simulation data is in SOA100\_K03\_alpha14\_8mqw\_offset.xls and .mat



# Detail Fit to C40G10S20, EW1858



- 8 QW offset
- 20  $\mu\text{m}$  SOA
- $K^2 = 0.06$
- Loss = 1.4  $\text{cm}^{-1}$
- $P_{\text{in}} = 0.005$  mW
- $I_{\text{SOA}}$  model
  - 0.12 mA
- $I_{\text{SOA}}$  exp
  - 0.2 mA
- $P_{\text{in}}$  exp
  - 0.2 mW

Simulation data is in SOA20\_K06\_alpha14\_8mqw\_offset.xls and .mat