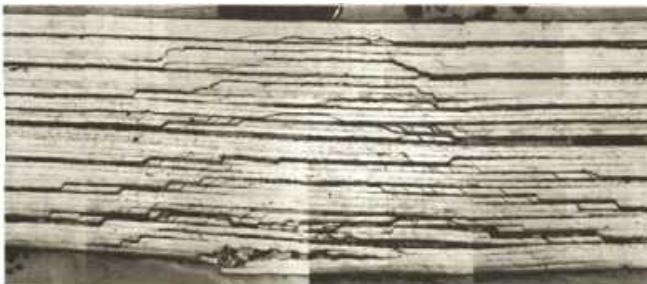


Inspection Options for Detecting Various Types of Impact Damage in Composite Structures

SAND2013-7877C

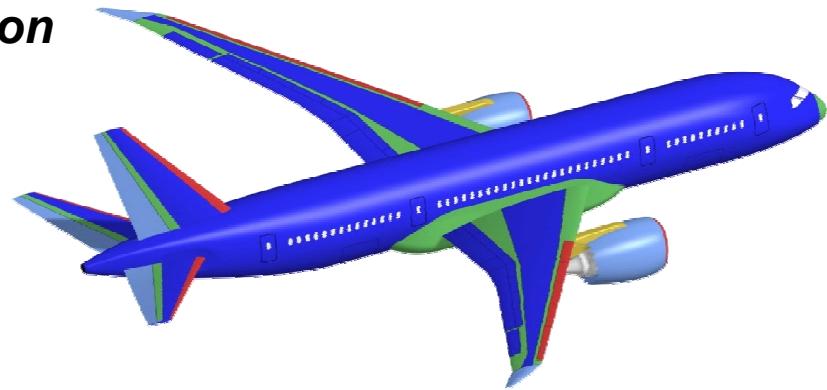


**Dennis Roach, Stephen Neidigk,
Tom Rice, Randy Duvall
Sandia National Labs
FAA Airworthiness Assurance Center**

Program Motivation - Extensive/increasing use of composites on commercial aircraft and increasing use of NDI to inspect them

Composite Structures on Boeing 787 Aircraft

- Carbon laminate
- Carbon sandwich
- Fiberglass
- Aluminum
- Aluminum/steel/titanium pylons



Program Goals: Assess & Improve Flaw Detection Performance in Composite Aircraft Structure



FAA William J. Hughes
Technical Center



Sources of Damage in Composite Structure

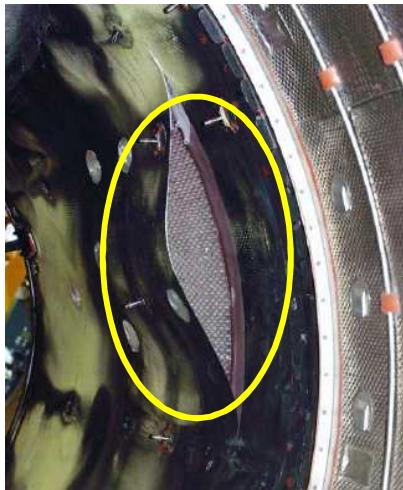
One airline reports 8 composite damage events per aircraft (on avg.) with 87% from impact; cost = \$200K/aircraft



**Lightning
Strike on
Thrust
Reverser**



Bird Strike



Towing Damage



**Disbonding at
skin-to-
honeycomb
interface**



AANC Composite Programs (CACRC Inspection Task Group Guidance)

- Industry wide NDI Reference Standards
- NDI Assessment: Honeycomb Structures
- NDI Assessment: Solid Laminate Structures
- Composite Porosity
- Composite Heat, UV, and Fluid Ingress Damage
- Composite Repairs
- Assessment of Bonds
- Composite Impact Study
 - Identify which impact scenarios are of major concern to aircraft maintenance
 - Identify key parameters governing impact damage formation
 - Relate damage threat & structural integrity to capabilities of NDI to detect hidden impact damage in laminates
 - Develop methodology for impact threat characterization

Blunt – high mass, low velocity
Sharp - low mass, high energy



ITG Team Participants

CACRC Inspection Task Group Members:

Keith Phillips – Airbus

Jim Hofer – Boeing

Jeff Kollgaard – Boeing

Kirk Rackow – Sandia Labs AANC

Dennis Roach – Sandia Labs AANC (Chair)

Glae McDonald – US Airways

Darrell Thornton – UPS

Richard Watkins – Delta Air Lines

Eric Bartoletti – American Airlines

Alex Melton – Delta Air Airlines

Ana Tocalino – Embraer

Quincy Howard – Boeing

Chris Dragan – Polish Air Force Institute of Technology

Robert Luiten – KLM Airlines

Dave Galella, Paul Swindell, Al Broz, Rusty Jones, Larry Ilcewicz – FAA

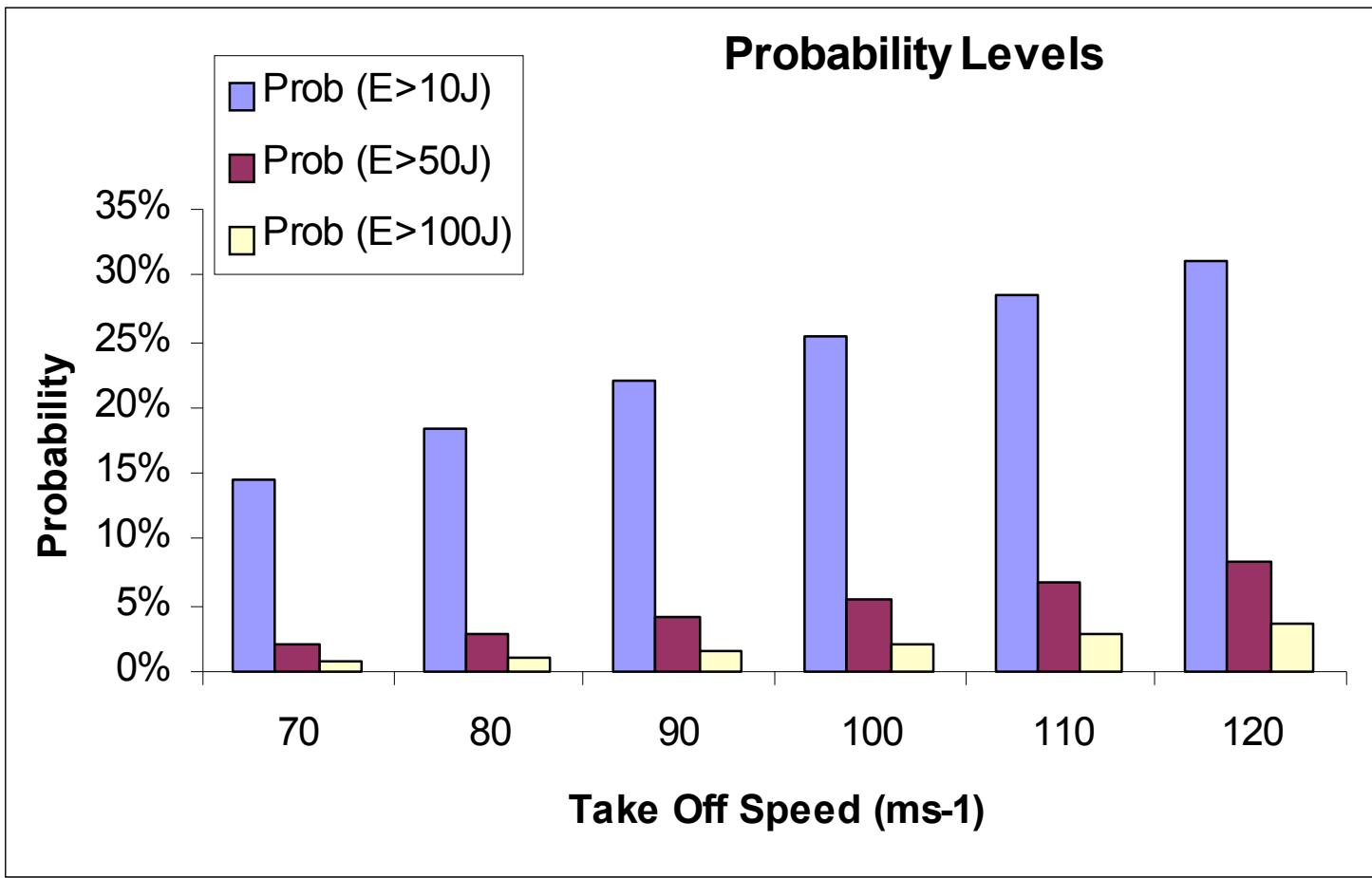


**FAA William J. Hughes
Technical Center**



Probability of Impact Energy as a Function of Take-Off Speed

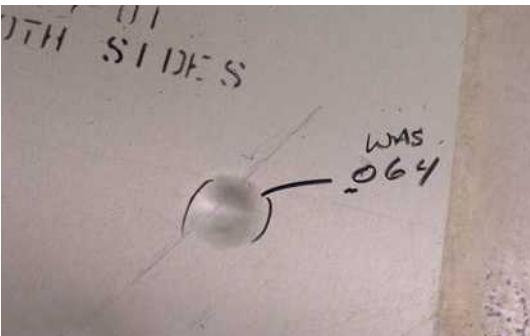
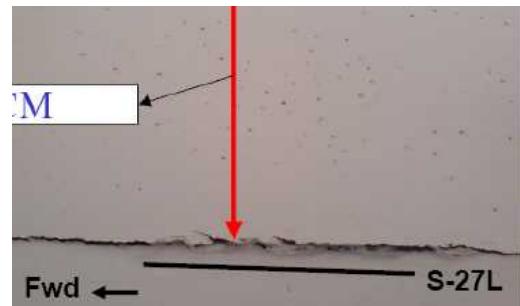
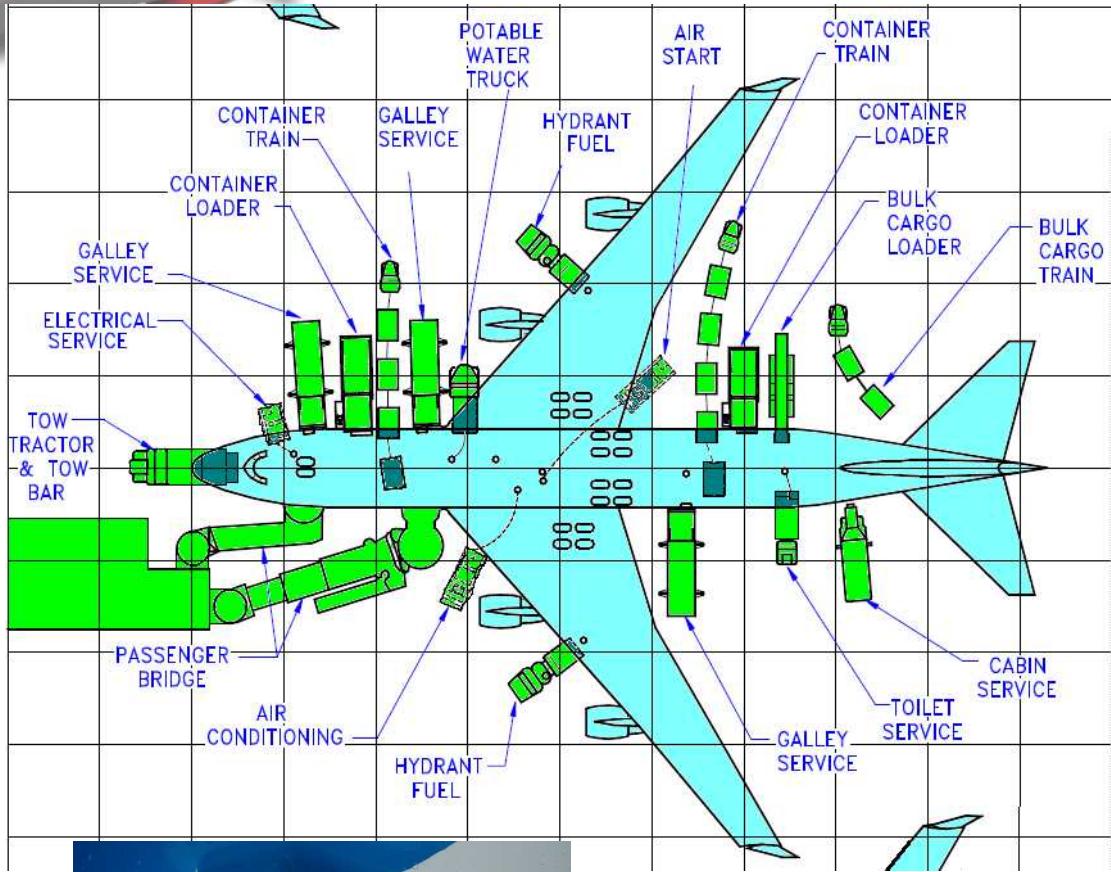
(based on runway debris collected from 4 UK military air bases)



Typical Runway Debris



Blunt Impact Threat from Ground Support Equipment



Damage may be less obvious in composites than in metallic structures

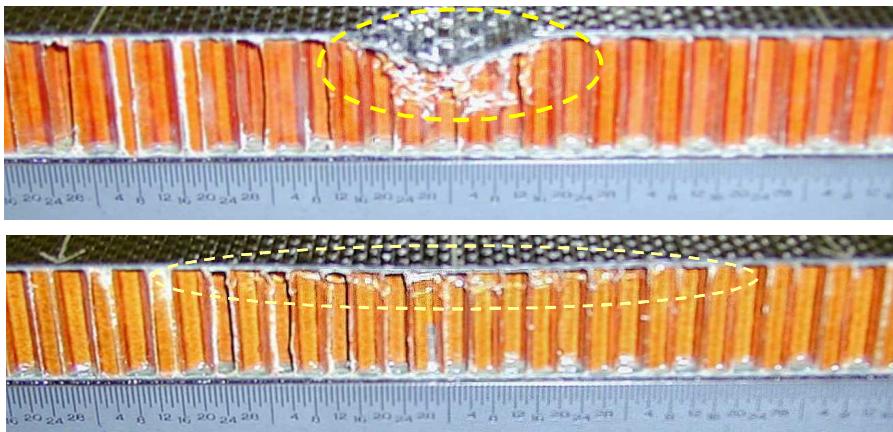


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Technical Center



Inspection Challenge – Hidden Impact Damage

Backside fiber failure from ice impact



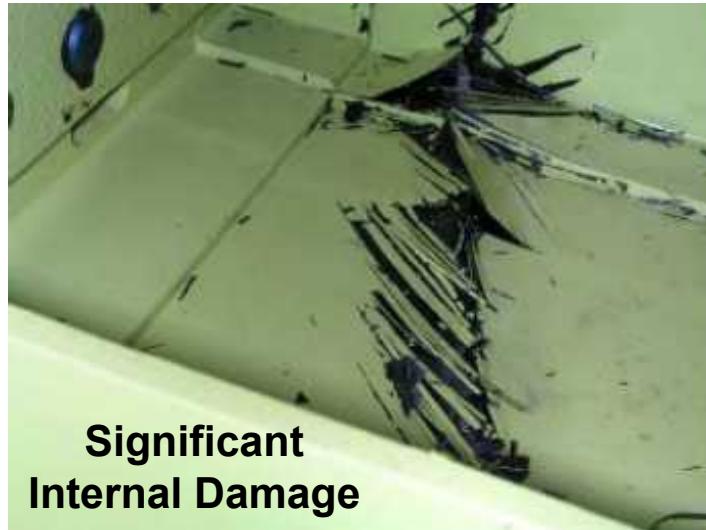
Visible Impact Damage – external skin fracture

Backside Damage – internal skin fracture & core crush

Damage from ground vehicle



Extent of Visible Damage from Outside



Significant Internal Damage

Source: Carlos Bloom (Lufthansa) & S. Waite (EASA)



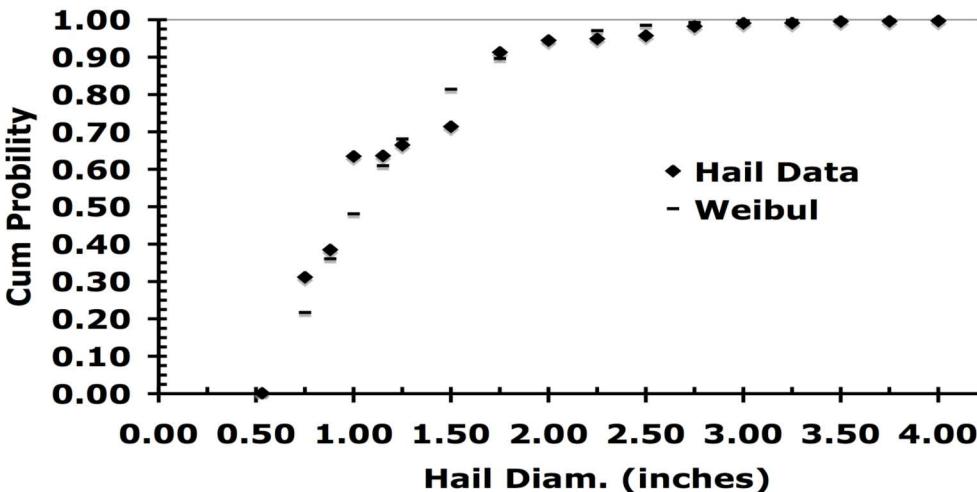
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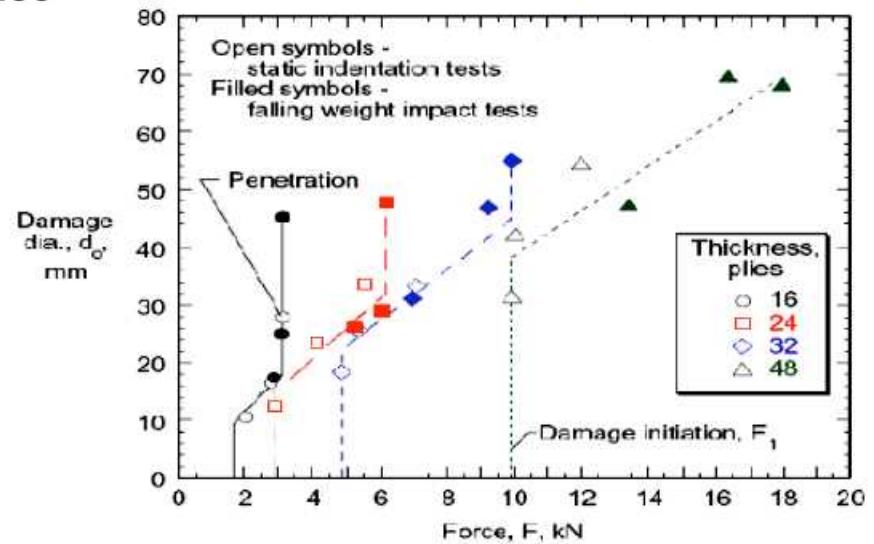
Sandia
National
Laboratories

Impact Damage Formation & Inspection in Composite Aircraft Structures

Joint Effort: UCSD (Hyonny Kim)



- Damage thresholds vs. laminate design; allowable limit
- Threat environment
- Inspection for cause – self evident event vs. self evident damage



Damage size from onset to laminate penetration



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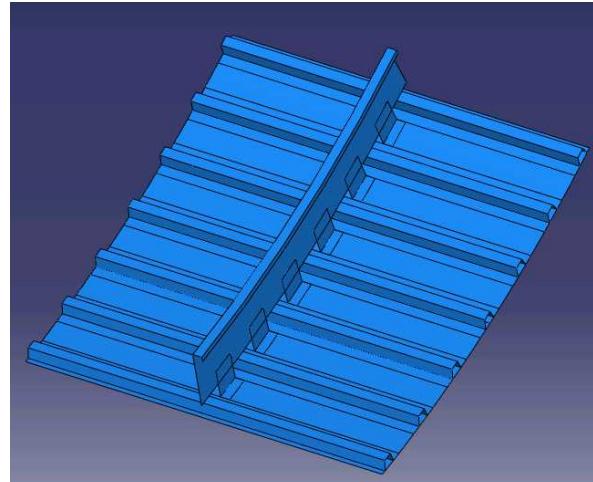


Sandia
National
Laboratories

Composite Impact Study - Background

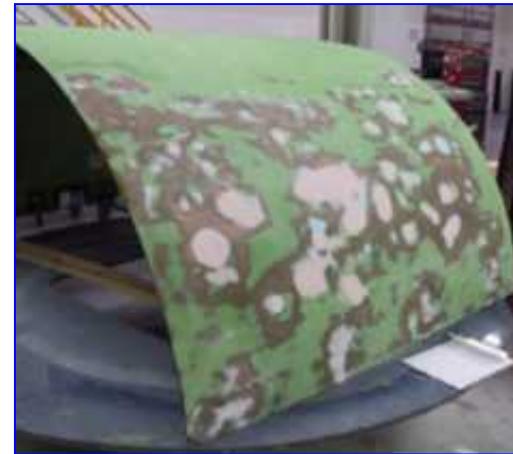
- Identify key phenomena that govern impact damage (model) & relate them to damage initiation
- Correlate global (mass, structure, velocity) and local (contact stiffness, angle) parameters to assess threat level of an impact event → aid maintenance decisions
 - Panel geometry/design, impact energy & orientations, material of impactor (metals, bumpers, ice)
 - Visual detectability related to damage (generation of surface markings)

Composite skin with substructure



Composite Impact Study – Hail Impact Task Description

- 112 carbon composite panels were fabricated using BMS8-276N uniaxial material; consisted of 8, 16, and 24 ply configurations (12" x 12")
- All panels are being impacted with ice balls of different diameters and velocities to simulate hail and create various levels of impact damage
- The goal was to create damage associated with Failure Threshold ~ BVID range & complete NDI to evaluate the sensitivity of each method in detecting and sizing the damaged area (reliable, sensitive, gate deployment, cost effective)
- NDI methods used for this evaluation include: Through Transmission Ultrasonics (TTU), Phased Array UT, Pulse-Echo UT, Resonance, Flash Thermography, Damage Checker (PE-UT), Mechanical Impedance Analysis, Low Frequency Bond Test



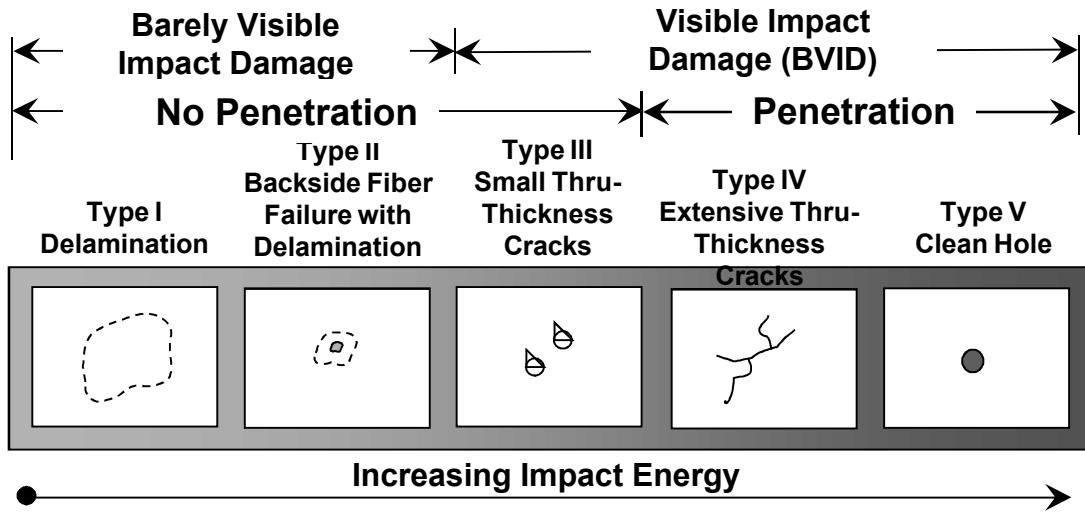
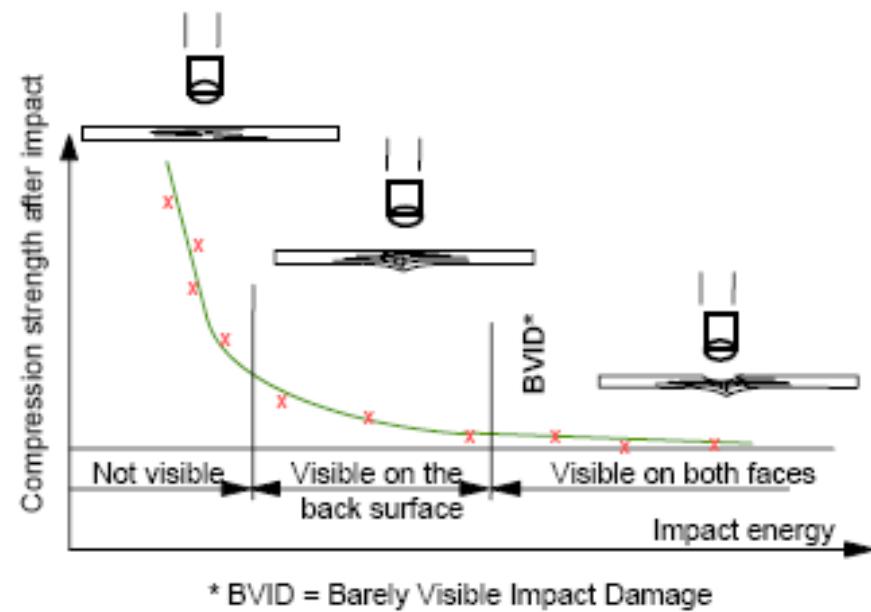
Hail Ice Impact

- upward & forward facing surfaces
- low mass, high velocity



Effects of Impact on Composite Structures

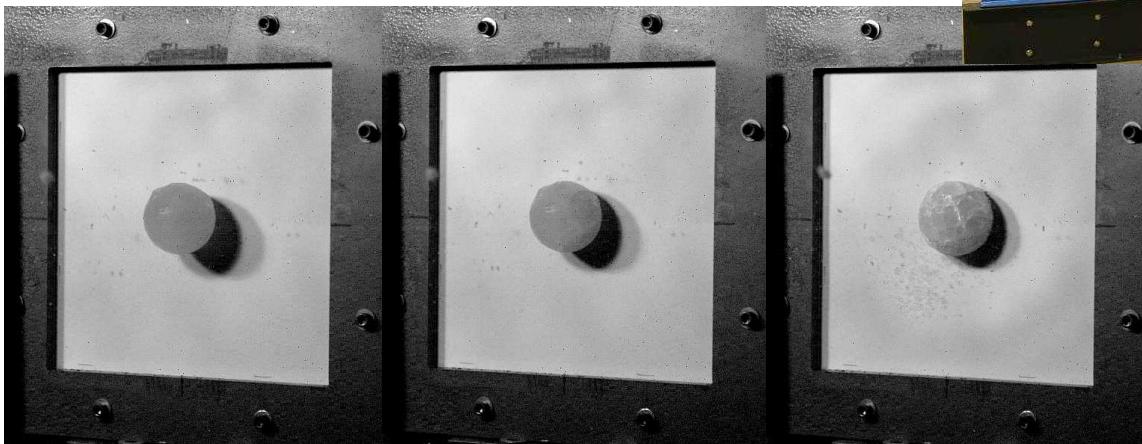
Challenge: hidden damage in composite structures can be difficult to detect visually and/or require special trained technicians and special equipment to be detected



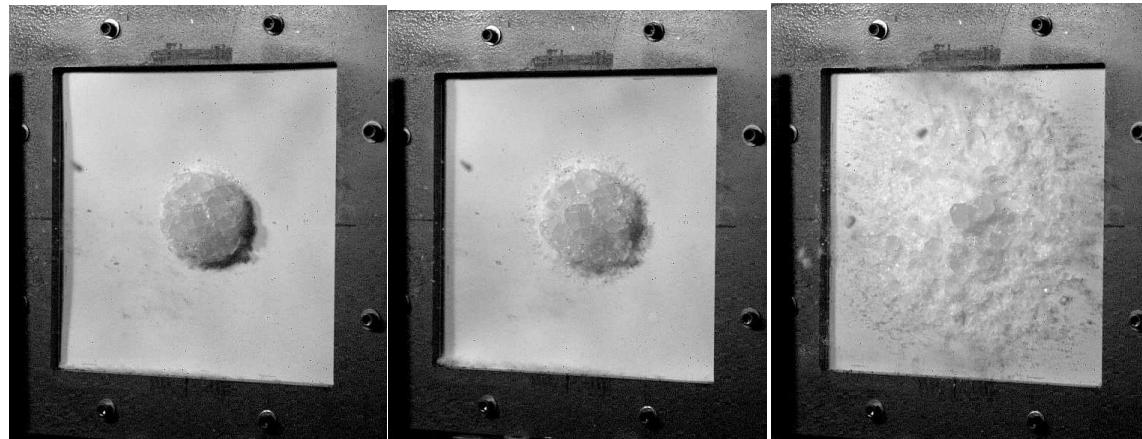
Backside fiber failure from ice impact



Ice Impact at UCSD



UCSD High Velocity
Gas Gun



Still Images from 61 mm
Ice Impact on 8 Ply
Carbon Panel at 72 m/s

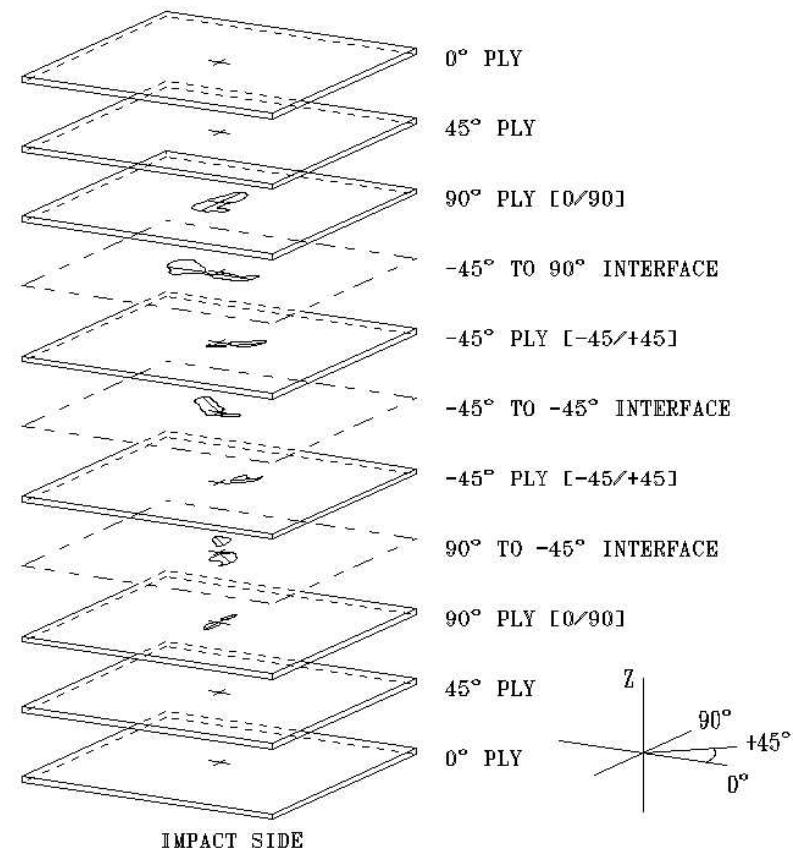
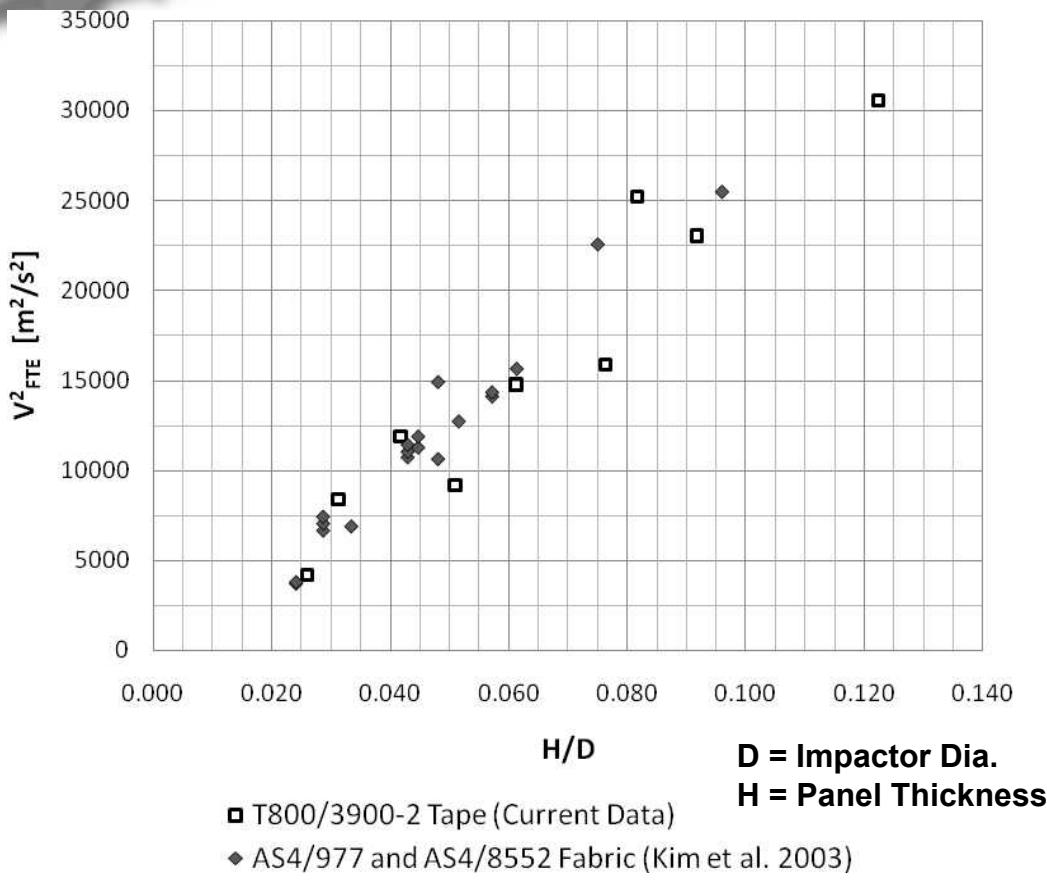


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Damage in Composite Laminates from Ice Impact



Impact-Induced Damage Morphology for 8 Ply Panel; 42.7 mm Ice at 120.4 m/s (267 J)

Selected panels were sectioned and observed by microscopy to map out the damage. The laminates develop the series of classic peanut shaped delaminations/fractures that stack together to give the overall appearance shown in the scans



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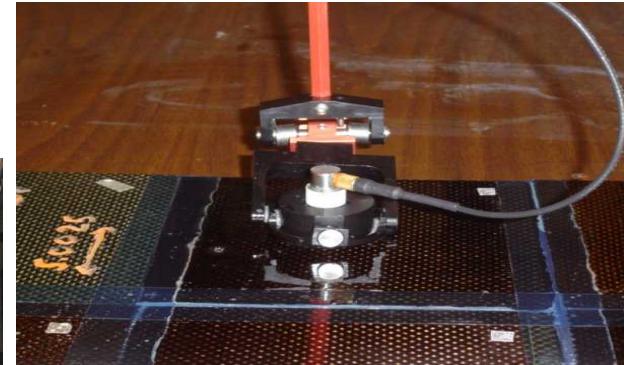
Composite Impact Damage – Inspection Methods Deployed



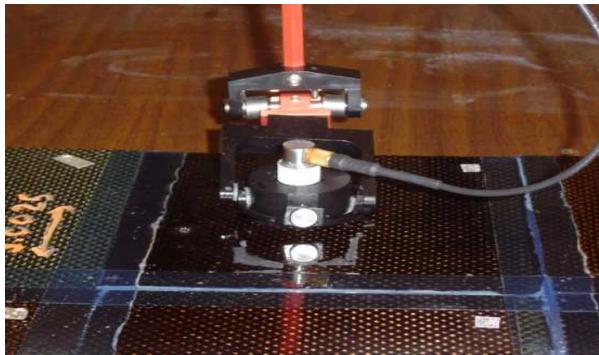
TTU



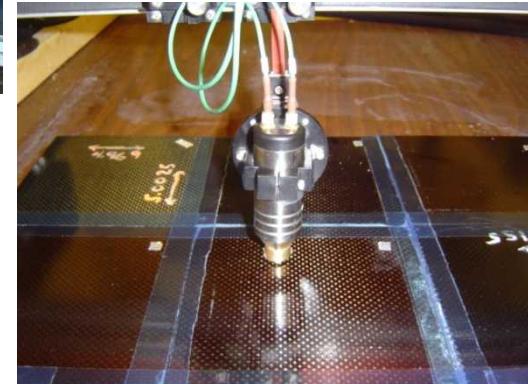
Thermography



MAUS PE



MAUS
Resonance



MAUS MIA



FAA William J. Hughes
Technical Center



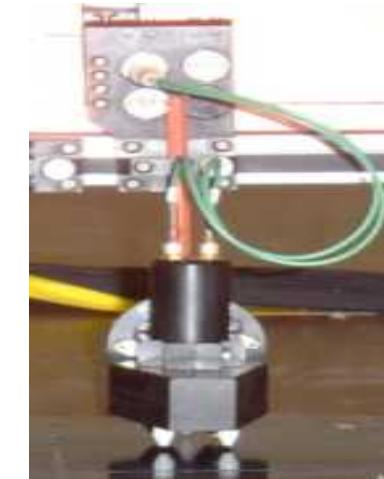
Composite Impact Damage – Inspection Methods Deployed



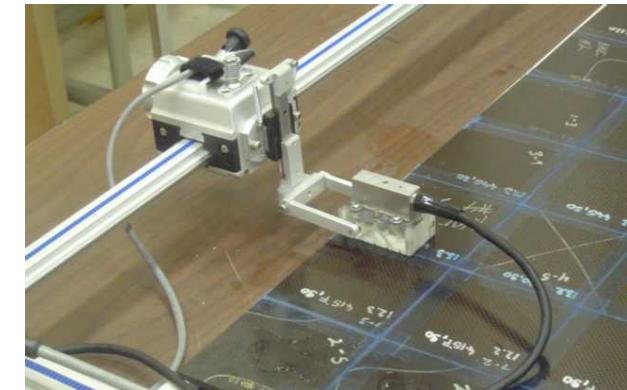
**Damage Check Device
(Pulse-Echo UT)**



**V-95
(Mechanical Impedance
Analysis)**



MAUS LFBT



Omniscan Phased Array UT



**FAA William J. Hughes
Technical Center**



**Sandia
National
Laboratories**

TC-8-06

Impact Energy (J) - 328

Impact Velocity (m/s) - 78

Flaw Size SNL/UCSD (mm²) - 1,122/n/a

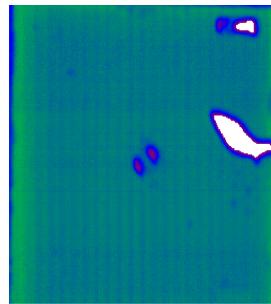
Projectile Size (mm) - 61.0

Flaw Size (major/minor dia. in mm) - 41.4/34.5

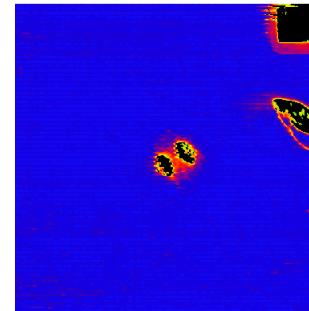
Picture



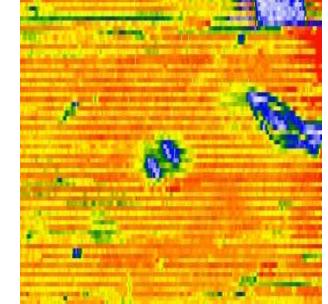
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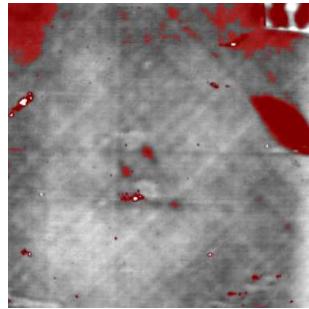
MAUS PE



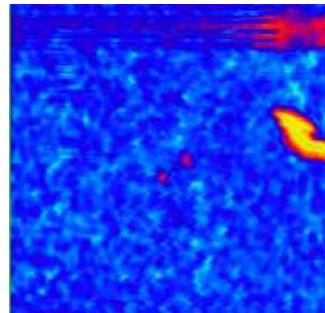
Omni PE



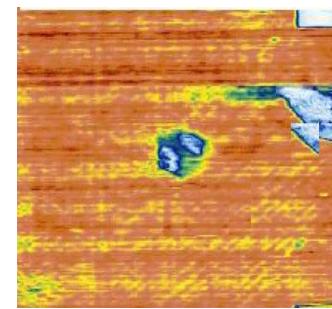
IR



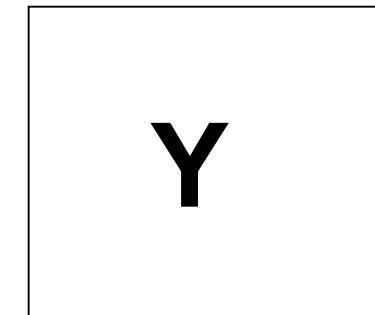
MAUS Resonance



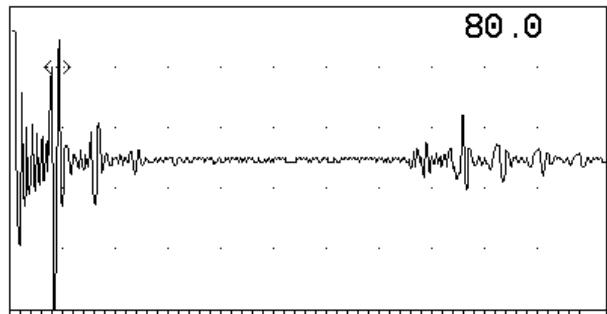
Omni PA



Damage Check
(flaw indicated)

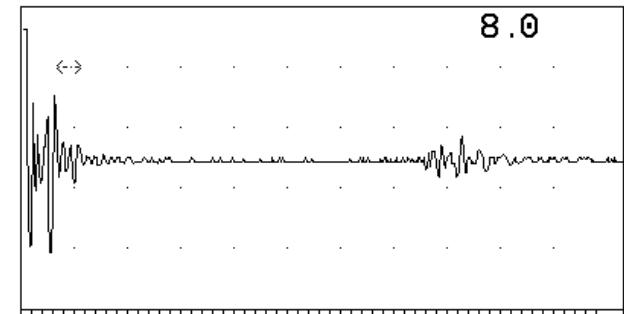


A-scan Ref



FAA William
Technical

A-scan Flaw



TC-16-04

Impact Energy (J) - 203, 271, 302

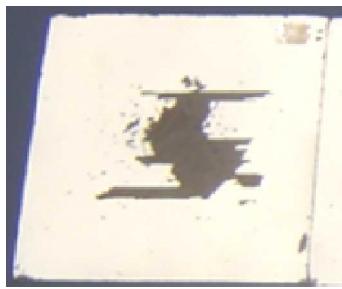
Impact Velocity (m/s) - 129, 146, 157

Flaw Size SNL/UCSD (mm²) - 1,420/0

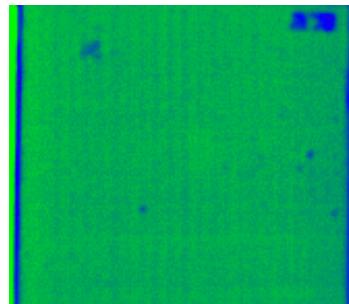
Projectile Size (mm) - 38.1

Flaw Size (major/minor dia. in mm) - 46.5/38.9

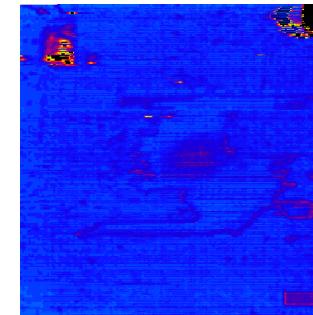
Picture



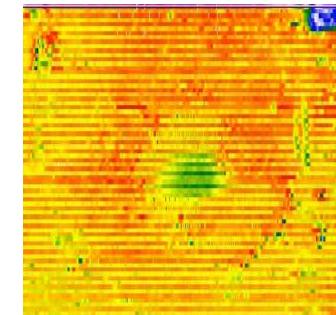
TTU



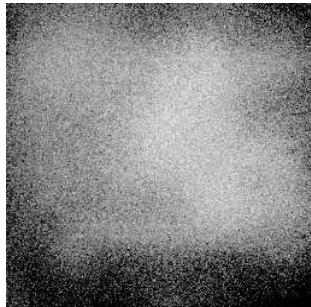
MAUS PE



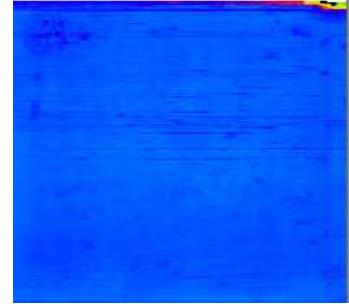
Omni PE



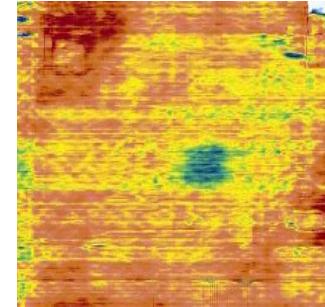
IR



MAUS Resonance



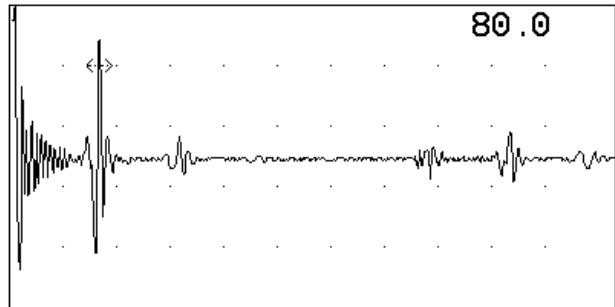
Omni PA



**Damage Check
(no flaw indicated)**

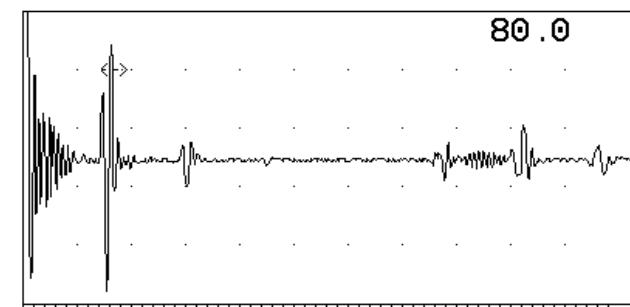
N

A-scan Ref



**FAA William
Technical**

A-scan Flaw



TC-16-06

Impact Energy (J) - 332

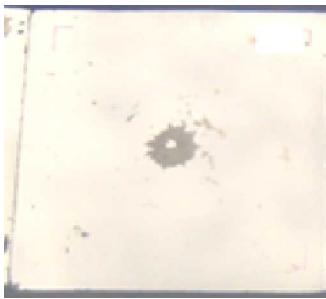
Impact Velocity (m/s) - 162

Flaw Size SNL/UCSD (mm²) - 5,460/2768

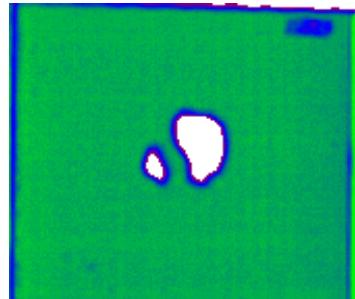
Projectile Size (mm) - 38.1

Flaw Size (major/minor dia. in mm) - 85.3/81.5

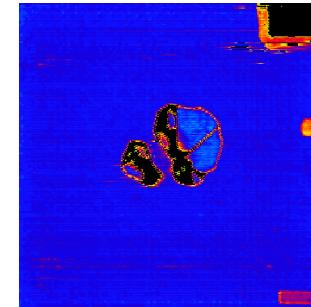
Picture



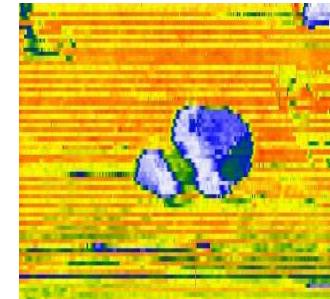
TTU



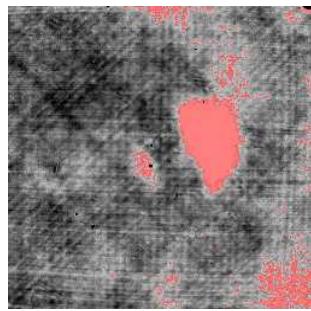
MAUS PE



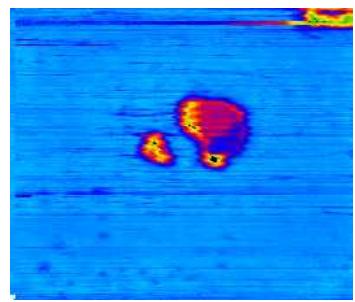
Omni PE



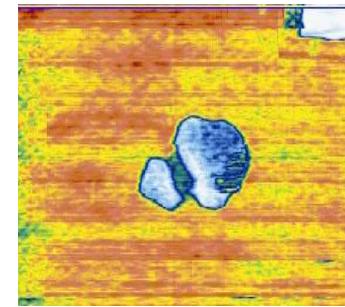
IR



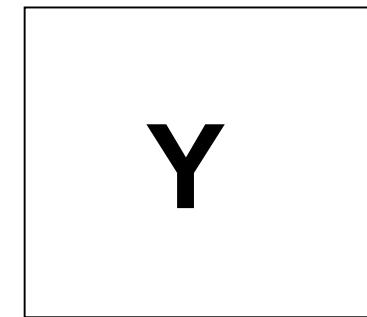
MAUS Resonance



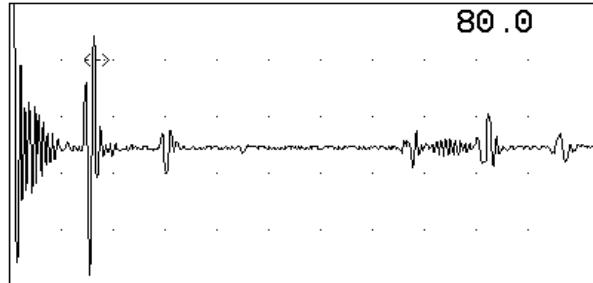
Omni PA



Damage Check
(flaw indicated)



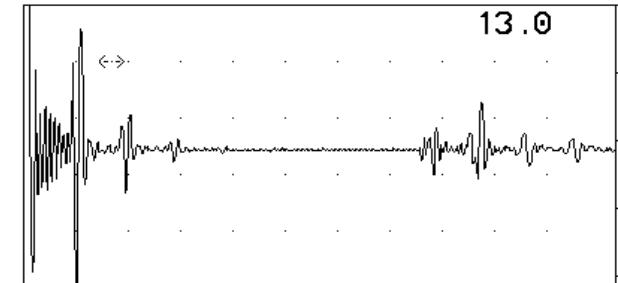
A-scan Ref



FAA William
Technical Center

80.0

A-scan Flaw



13.0



Impact Damage Program Inspection Results from 24 Ply Panel

TC-24-11

Impact Energy (J)- 704 & 819

Flaw Size MAUS PE (mm³) - 8708

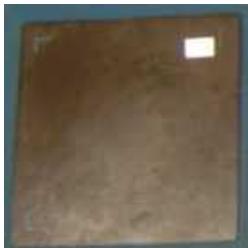
Impact Velocity (m/s) - 151 & 163

Flaw Size Omniscan PE (mm²) - 9030

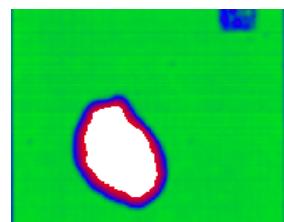
Projectile Size (mm)- 50.8

Flaw Size TTU UCSD (mm³) - n/a

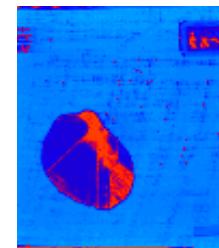
Picture



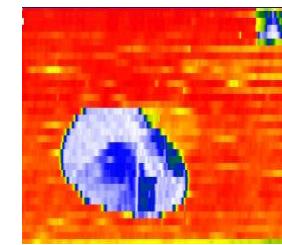
TTU



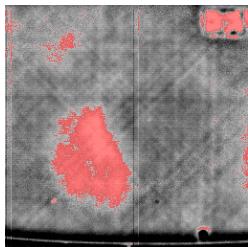
MAUS PE



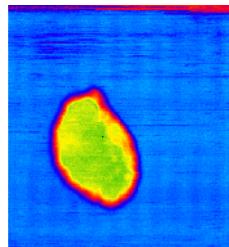
Omni PE



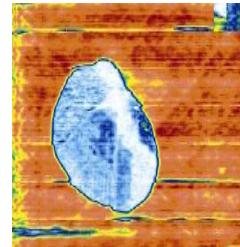
IR



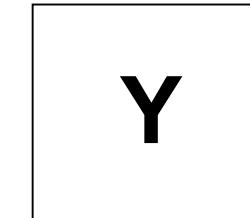
MAUS Resonance



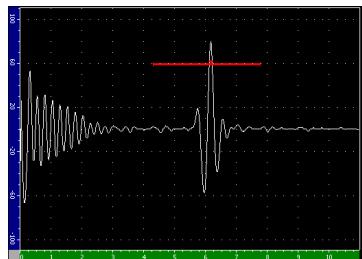
Omni PA



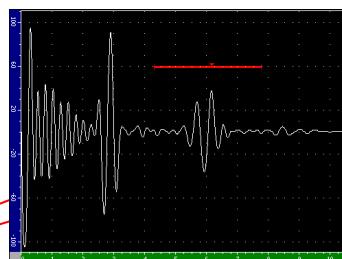
Damage Check
(flaw indicated)



A-scan Ref



A-scan Flaw



Notice loss of backwall signal
and new intermediate signal



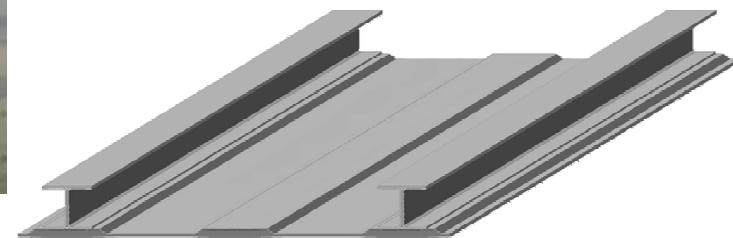
FAA William J. Hughes
Technical Center



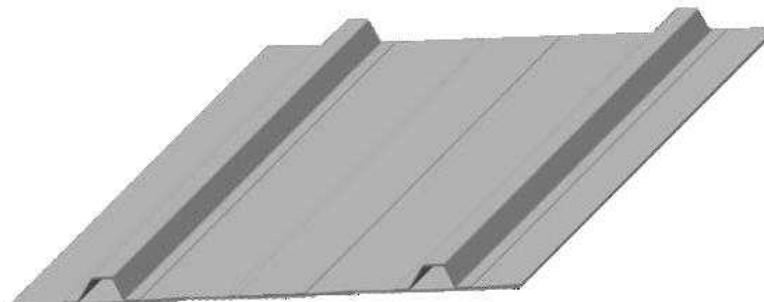


Image Based NDE for Modern Rotorcraft Sustainment – Composite Inspection of Solid Laminate Structures

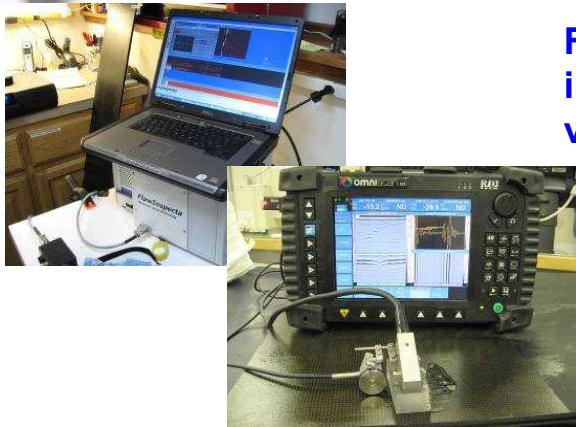
- Support for Bell Helicopter BAA
- Detect and characterize impact damage in full-scale panels
- Impact energies range from 25 to 500 in-lb
- Fast, low-cost, large-area inspection methods – visual based displays
- Screening NDI (“go” – “no go”) for ramp personnel (minimal training)



Full-Scale Panel Designs



Bell Helicopter – Composite Inspection of Solid Laminate Structures

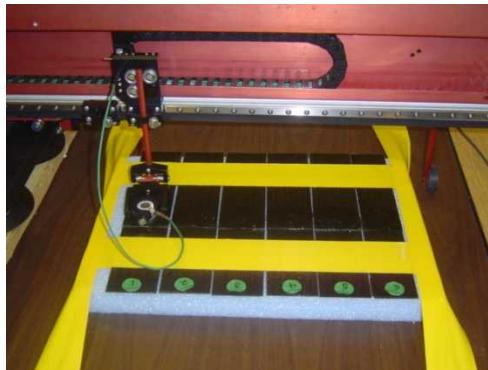


Phased Array Ultrasonic Imaging (PAUT)

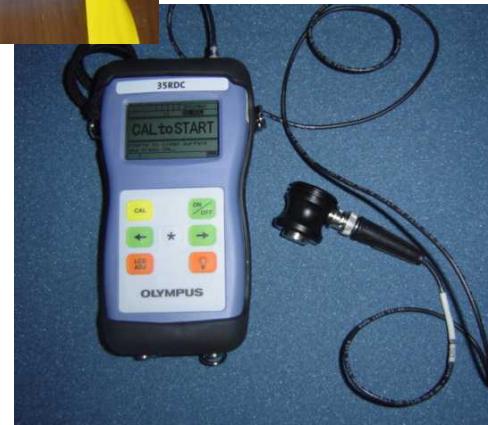
Field deployable infrared imaging (FDIR) to enhance visual inspections



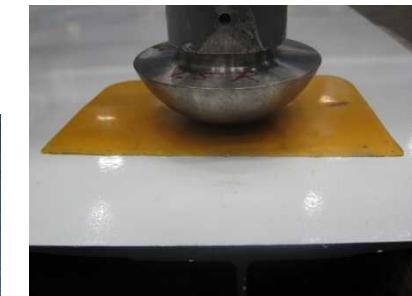
MAUS PE UT, Resonance; Hand-Held PE UT



Digital Acoustic Video (DAV)



Olympus Damage Checker



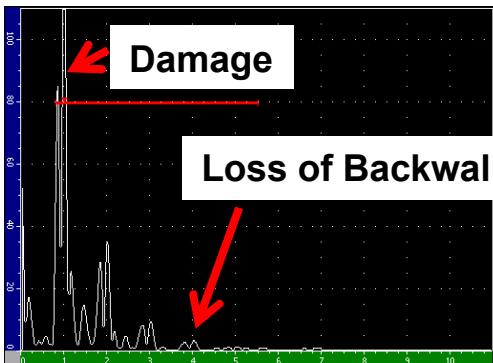
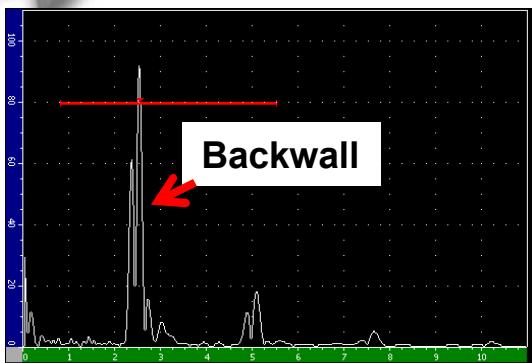
Impact Device



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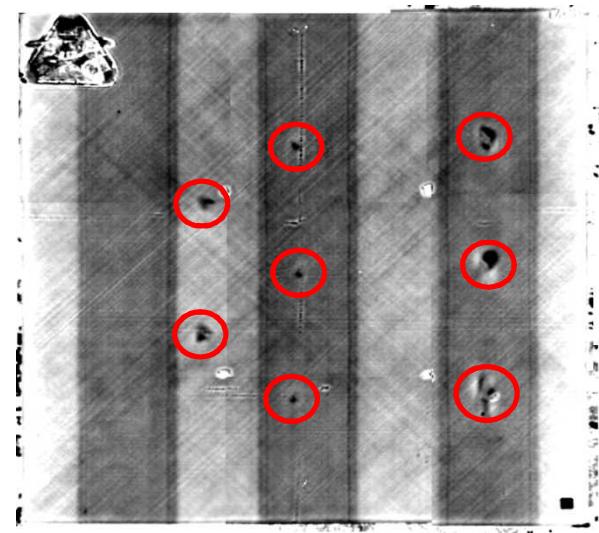
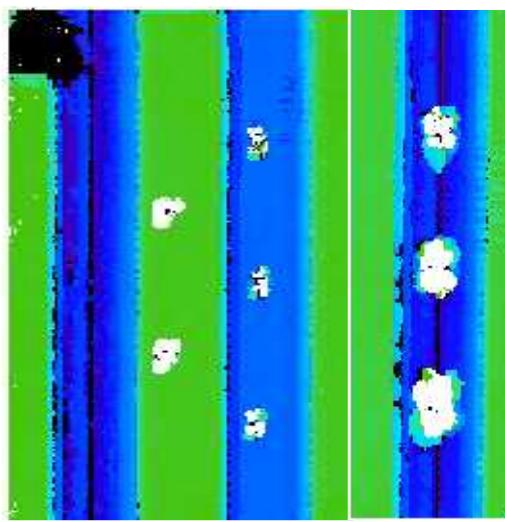
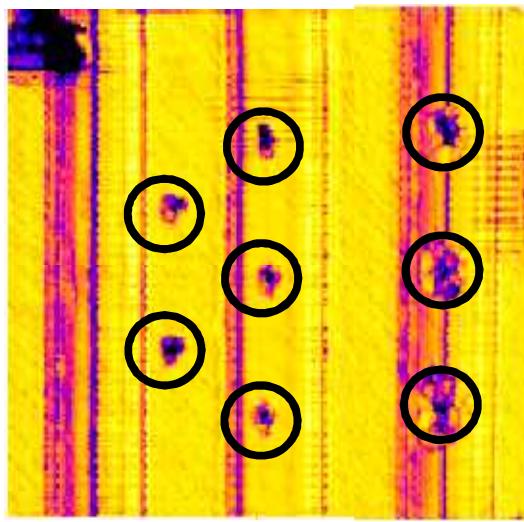
Bell Helicopter – Composite Inspection of Solid Laminate Structures



I-Beam Stiffened Panel FAA-I-1



Assessment of A-Scan Signals in Real Damage



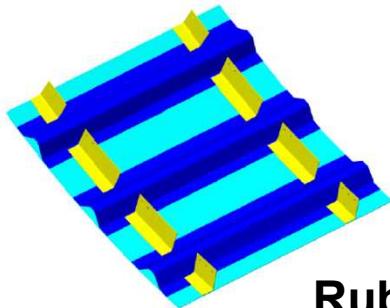
Flash Thermography Image

MAUS PE UT Amp & Tof F C-Scan Images

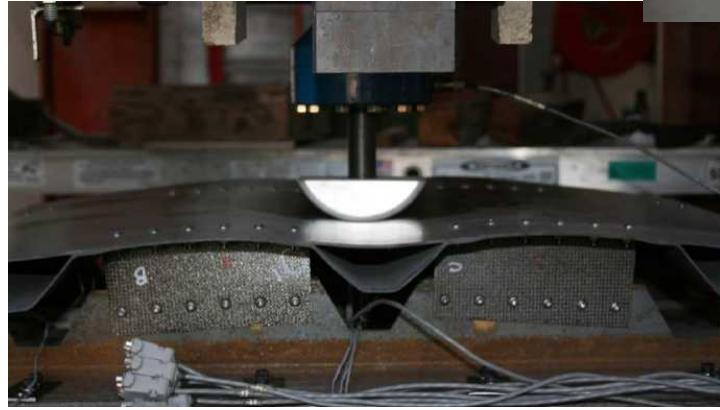
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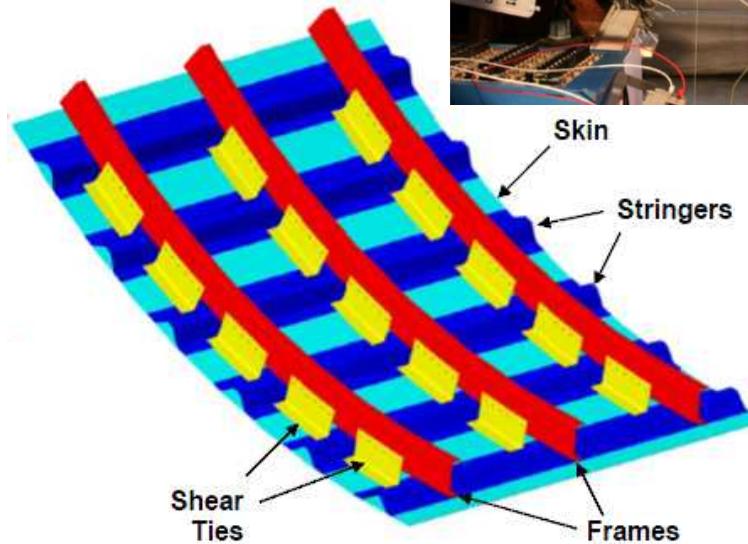
Impact Damage Program - Inspection of Full Scale Panels with Low Velocity-High Mass Impacts



Rubber Bumper
from Baggage
Loading Cart



2' X 3' and 4' X 6' Panels With
Substructure Elements



Wide area blunt impact – internal, distributed damage;
high interlaminar shear & failure of co-cured joints

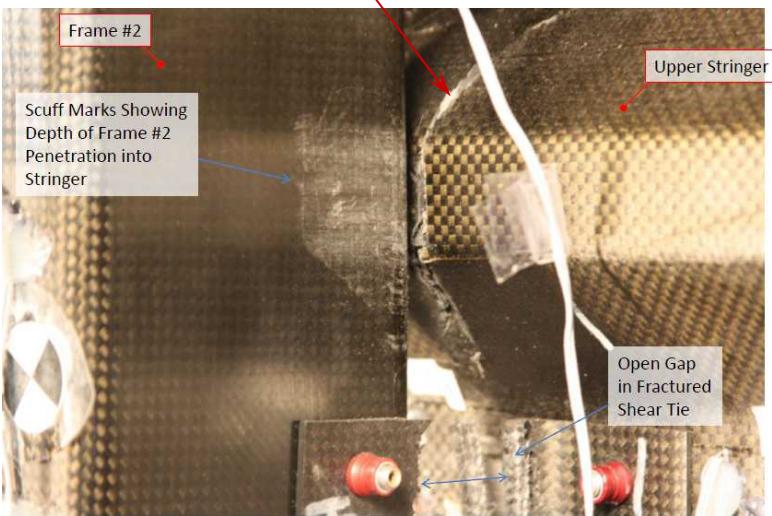


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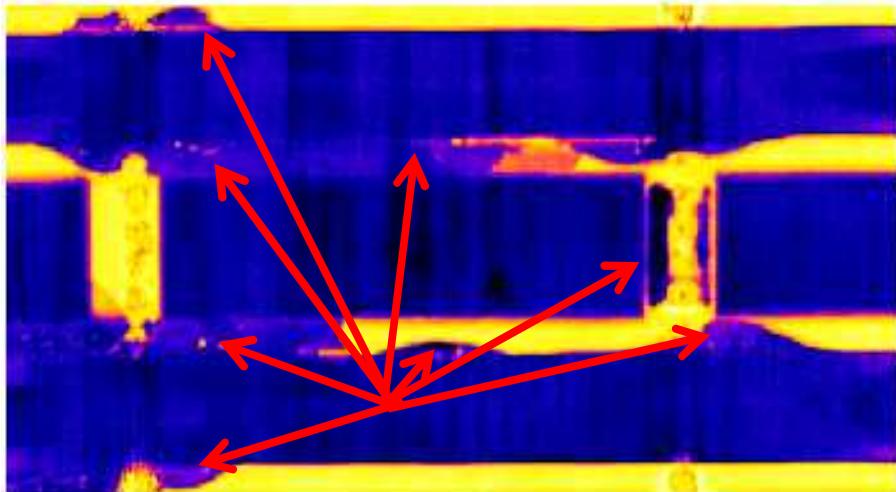


Inspection of Full Scale Panels with Low Velocity-High Mass Impacts

Stringer Fracture



Note: subsurface damage & comparison to visual inspection



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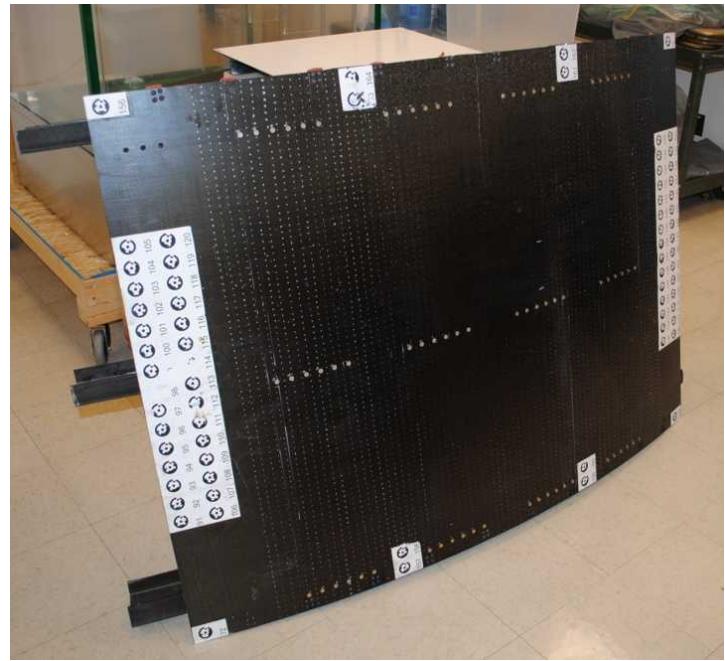
Fracture of Co-Cured Joint at Stringer-Skin Interface



Stringer & shear tie areas that are not yellow correspond to disbonds.



Full-Scale Carbon Aircraft Panels for Impact Assessment

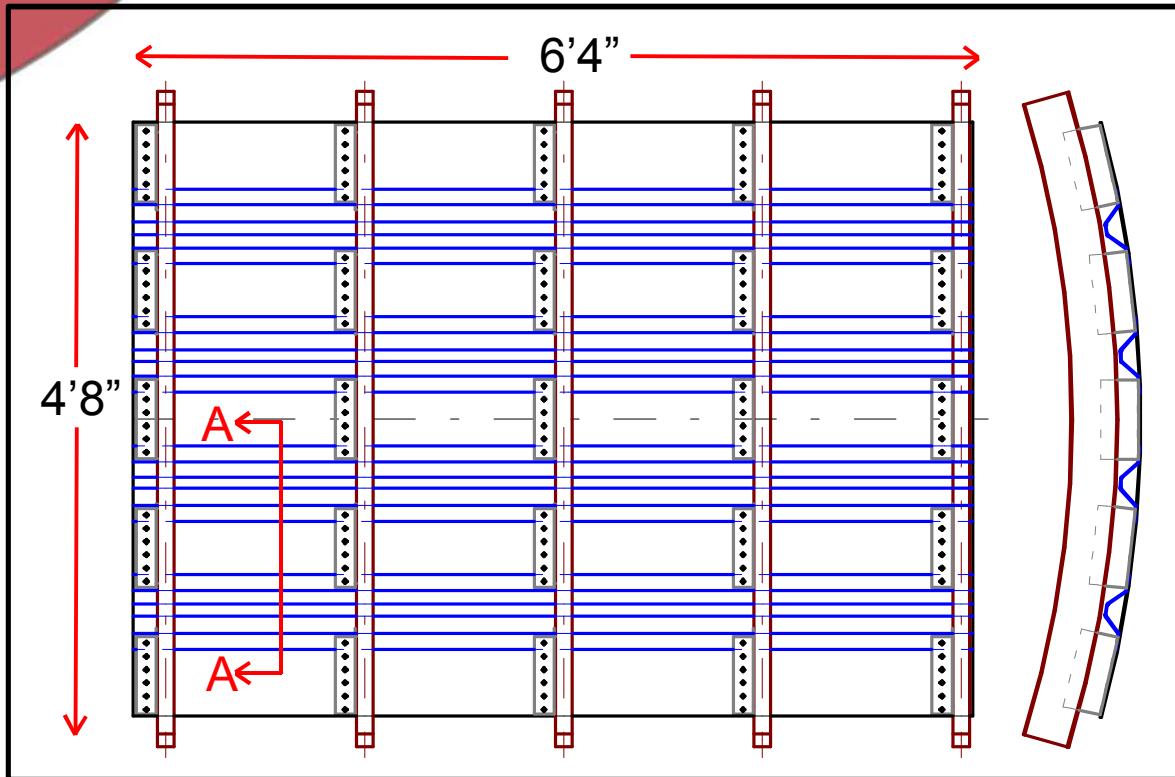


Full-scale carbon fiber aircraft fuselage section with co-cured stringers and attached frames



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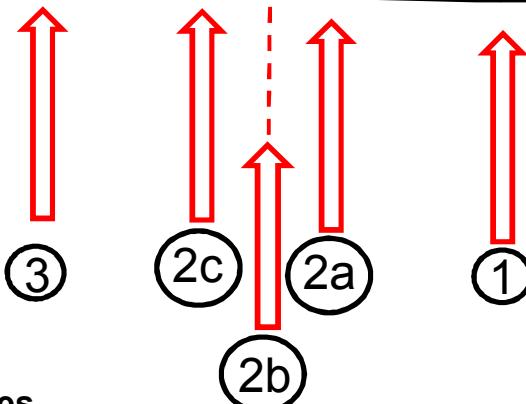




Section A-A

Stringer

Skin



Impact Regions:

- (1) skin between the stringers
- (2) stringer/skin interface
- (3) center of the stringer
- (4) shear-tie/skin interface



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Schematic of Impact Damage



Drop Weight
(hardened) Impact

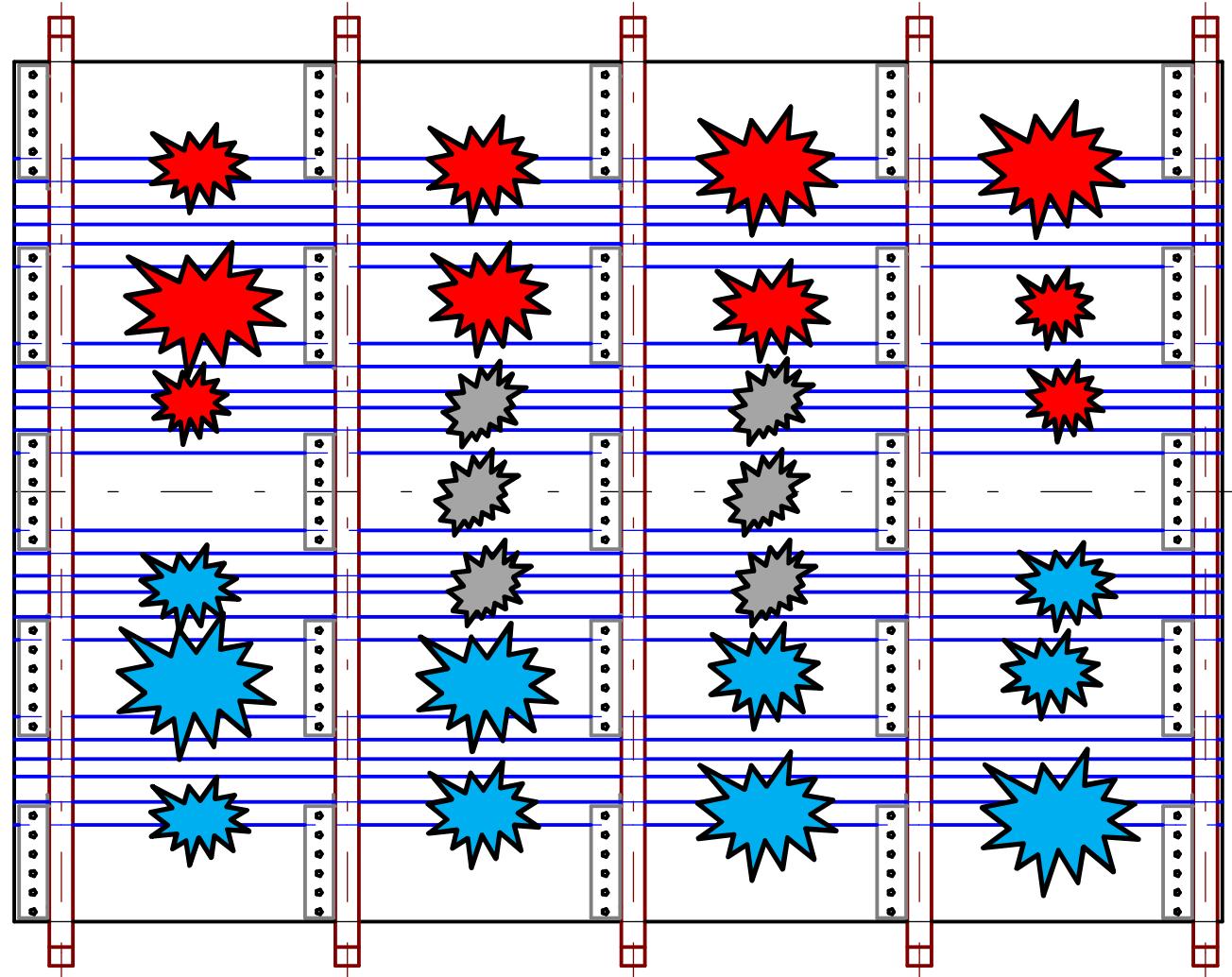


Quasi-Static
Impact



Ice Impact

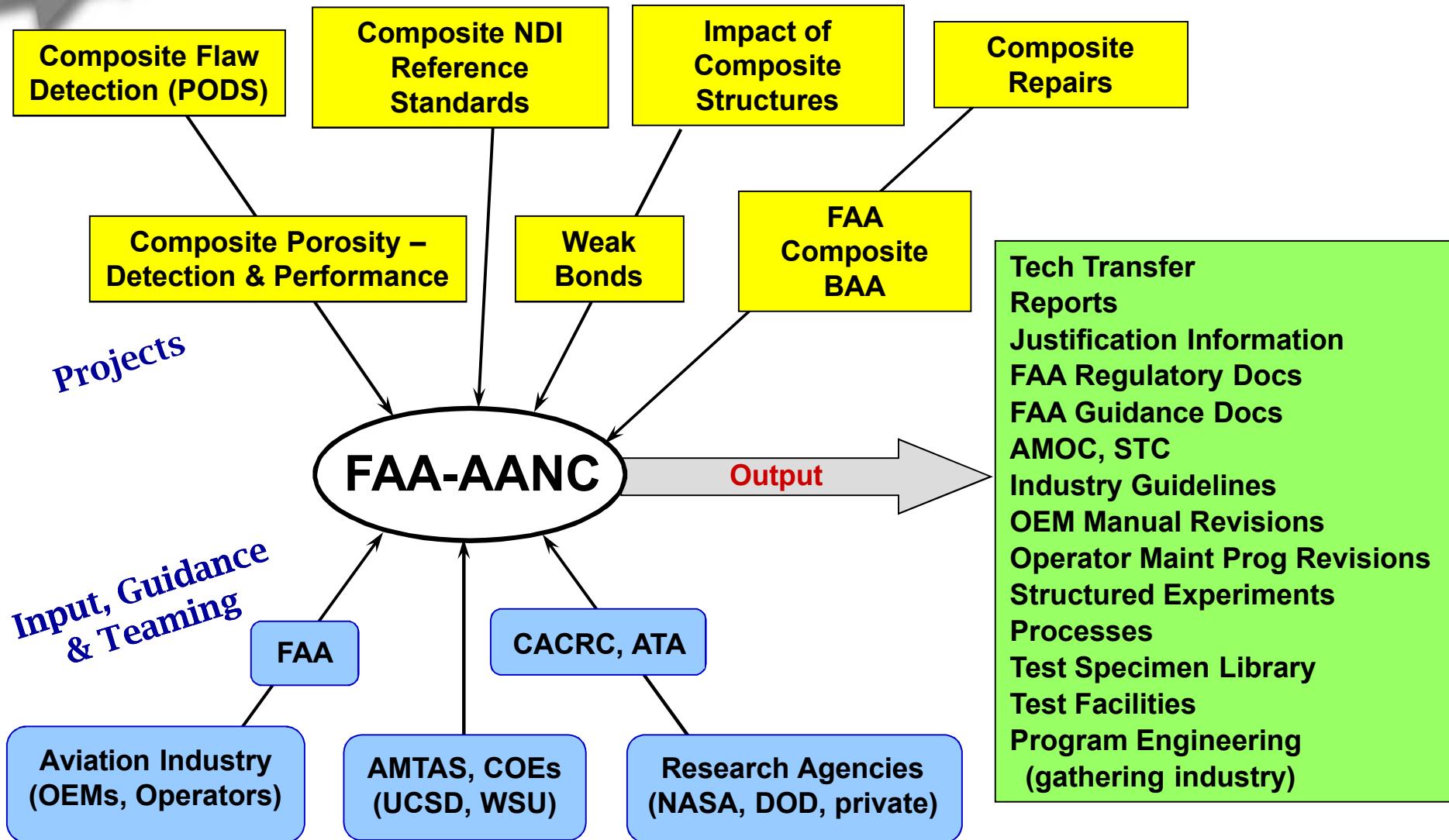
Damage location is divided into "bays" separated by stringers and frames (shear-ties) to avoid effect on neighboring impacts.



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FAA-AANC Composite Programs



Conclusions – Inspection of Composite Structures

- Engineering and economic benefits of composites will continue to expand its use
- Impact damage is a primary concern (hidden subsurface damage)
- **Composite Impact Study is:**
 - Identifying impact scenarios of concern
 - Identifying key parameters governing impact damage
 - Characterizing FTE & overall impact threat
 - Relating damage threat to capabilities of NDI
- **NDI ability** to detect impact damage was assessed in FTE ~ BVID range → sensitivity, sizing, procedures, deployment
- Multiple **impact parameters** must be studied – hardness of impactor, low mass-high velocity impact, high mass-low velocity impact, angle of impact, surface demarcations & visual clues, panel stiffness





Inspection Options for Detecting Various Types of Impact Damage in Composite Structures

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Abstract

Aircraft structures made from polymer-matrix composites are vulnerable to damage created by impact from ground vehicles/equipment, as well as from events such as hail and bird strikes. These impacts can create internal damage that is not visually detectable and thus of great concern from a damage tolerance and safety standpoint. The focus of this study is on the detection of damage stemming from a variety of impact types and the relationship between inspection capabilities and the damage resistance of carbon/epoxy tape laminates. Panels of varying thicknesses were impacted with a variety of impactors (hardened, hail, bumpers) where the input energy was derived from both high velocity-low mass and low velocity-high mass scenarios. Impact location was also varied in order to study the effect on substructure elements. Different nondestructive inspection (NDI) methods were applied to damage stemming from impacts in the vicinity of the failure threshold energies (FTE) of these composites. FTE is defined as the minimum amount of energy required to create initial delamination damage in the structure. Relationships between failure threshold velocity and the ratio of panel thickness to impactor diameter were determined and the sensitivities of multiple nondestructive inspection (NDI) methods were intercompared. NDI testing included both hand-held A-scan or meter response methods, as well as wide area C-scan mapping techniques. Rapid, "Go/No-Go" NDI devices were assessed to establish the viability of using gate-check inspections on in-service aircraft to identify damage of concern. The inspection portion of this impact study seeks to determine the ability of conventional and advanced NDI to detect hidden impact damage that is at or below the level referred to as Barely Visible Impact Damage (BVID). This study will allow flaw detection to be adequately judged based on the effects of impact on the structural integrity of composites. It will aid maintenance engineers in assessing whether an incident could have caused damage to a structure, and if so, what type of inspection technique should be applied to resolve the extent of damage.

