

# SILICON CARBIDE LATERAL OVERTONE BULK ACOUSTIC RESONATOR

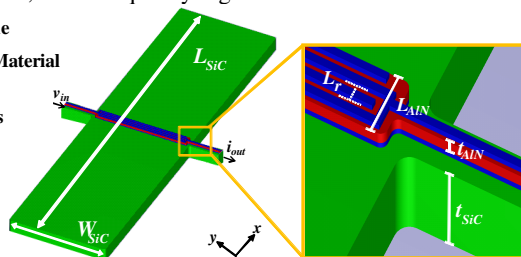
## with ULTRAHIGH QUALITY FACTOR

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### LATERAL OVERTONE BULK ACOUSTIC RESONATOR (LOBAR)

- The LOBAR design decouples the piezoelectric transduction and energy storage mechanisms, resulting in high  $f \cdot Q$  and  $k_t^2 \cdot Q$  at microwave frequencies.
- Lithographically defined frequencies and bandwidths
- multi-bandwidth, multi-frequency cognitive radios

**Silicon Carbide**  
**Piezoelectric Material**  
**Bottom and Top Electrodes**



**Silicon Carbide (SiC) :**

**Low Loss Material → High Q**

SiC has the lowest phonon-phonon damping  
SiC has high acoustic speed, high mechanical and chemical strength

**Aluminum Nitride (AlN) :**

**High Transduction Efficiency → High  $k_t^2$**

AlN is a piezoelectric material that efficiently couples the acoustic and electrical domains resulting in low motional impedance

### THEORY and SIMULATION

**High number of overtones stored in resonator → Higher Quality Factor**

$$Q = 2\pi \frac{E_{\text{Stored}}}{E_{\text{Lost}} \text{ Cycle}}$$

$$Q_{\text{LOBAR}} \approx \left[ \frac{1}{\frac{Q_{\text{SiC}}}{L_{\text{SiC}}} + \frac{I_{\text{AlN}}}{L_{\text{SiC}} Q_{\text{AlN}}}} + \frac{I_{\text{AlN}}}{L_{\text{SiC}}} \right]^{-1}$$

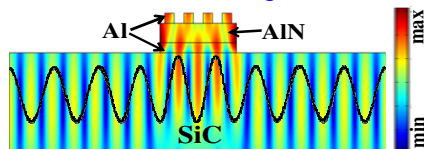
The resonance frequency of LOBAR is defined lithographically by the interdigitated electrodes on AIN ( $L_r = 2 \times \text{Al finger width}$ );

$E_{\text{eff}}$  and  $\rho_{\text{eff}}$  are the effective Young's modulus and mass density of the composite SiC-Piezoelectric stack

At 3 GHz,  $L_r = 7.52 \mu\text{m}$  for AlN transducer with 4 fingers

$$f_{\text{LOBAR}} = \frac{1}{2L_r} \sqrt{\frac{E_{\text{eff}}}{\rho_{\text{eff}}}}$$

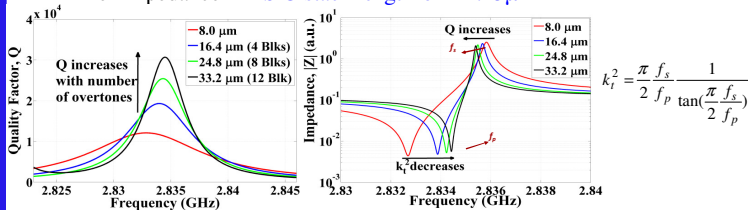
**LOBAR Simulations in COMSOL® showing Displacement Mode Shape in the x-direction**



For optimum  $f \cdot Q$  and insertion loss need to maximize energy coupling from the piezoelectric AlN stack to the low loss SiC

→ For  $1 \mu\text{m}$  SiC,  $t_{\text{AIN}} = 200\text{nm}$ , and  $t_{\text{Al}} = 100\text{nm}$

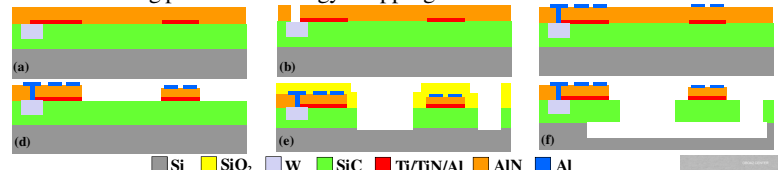
Frequency of the composite stack should matches that of the SiC ends to minimize impedance → SiC stack length of  $12.25 \mu\text{m}$



**As wavelengths of SiC are added → Quality factor increases and  $k_t^2$  decreases**

### FABRICATION PROCESS

The Silicon Carbide LOBARs were fabricated in a CMOS-compatible surface micromachining process → Energy Trapping in All 3-axis



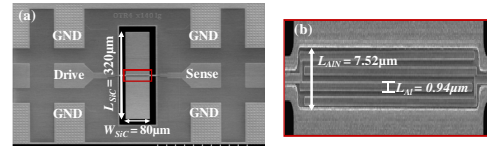
Si SiO<sub>2</sub> W SiC Ti/TiN/Al AlN Al

- Highly textured Cubic 3C-SiC (111) film was deposited using LPCVD
- SiC film has as-deposited tensile stress of <150MPa
- SiC film was polished to a surface roughness of <1nm, which is critical for high Q resonators

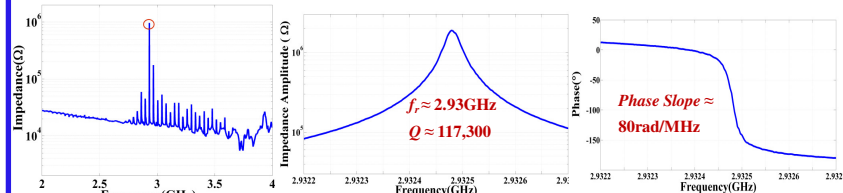
SEM and AFM of SiC polished using Tungsten CMP: rms < 1nm

### RESULTS

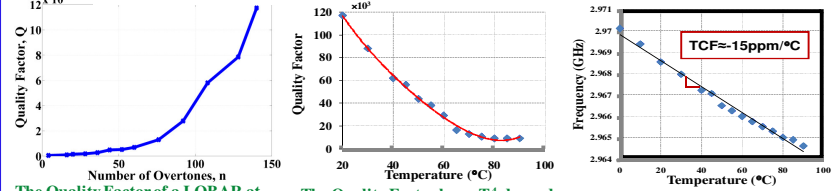
Scanning Electron Microscope (SEM) images of a silicon carbide lateral overtone bulk acoustic resonator with 140 added overtones



The wide span two port impedance response of the LOBAR from its transmission response in air shows the peaks corresponding to the higher order harmonics of the SiC length extensional resonance transduced by the piezoelectric AlN layer



### Measurements for LOBAR with 140 Added Overtones



The Quality Factor of a LOBAR at 3GHz increases from <500 for one overtone to >100,000 for 140 overtones

The Quality Factor has a  $T^4$  dependence → LOBAR operates in Landau-Rumer regime → Good on-chip temperature sensor

Temperature stability of uncompensated LOBAR

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