

# The Variable Resolution Spectral Dynamical Core in the Community Atmospheric Model (CAM)

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# Outline

## 1 Background

- HOMME
- Why Do We Refine?
- How Do We Refine?
- Changes Due to Refinement

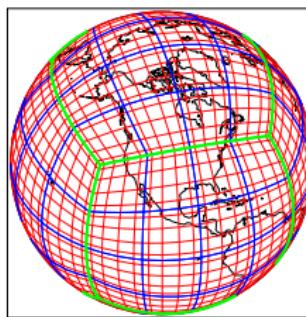
## 2 Results

- Global Advection
- Global Shallow Water

## 3 Conclusions

- Future Work
- Acknowledgements

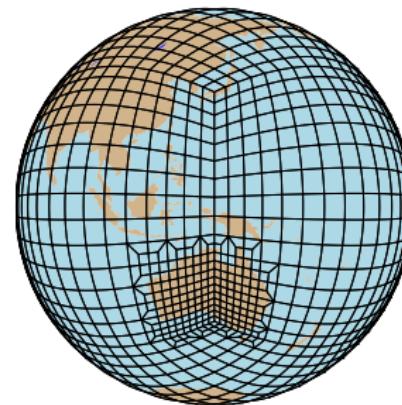
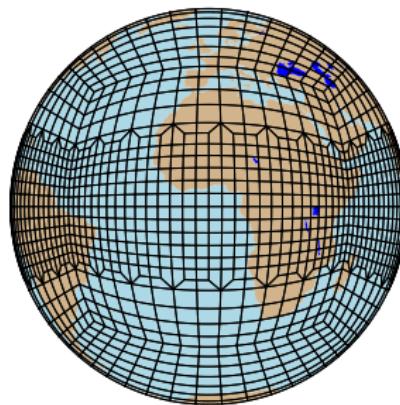
# HOMME (High Order Methods Modeling Environment)



HOMME

- “A scalable and efficient spectral-element-based atmospheric dynamical core” (<http://www.homme.ucar.edu>)
- CAM-HOMME dynamical core available in CCSM
- Elements originally were squares on a cube, projected onto a sphere using gnomonic projection
  - Now able to use any quadrilaterals on cube or sphere (with great-circle edges)

# Why Do We Refine?



## Benefits of Refinement

- High-res studies of specific areas (the tropics, Australia, etc)
  - ➊ Refine over Atmospheric Radiation Measurement [ARM] sites
  - ➋ Calibrate global parameters for high-res runs based on ARM data (significantly cheaper than tuning via 500+ global runs)
- Alternative to nested models for regional climate

# How Do We Refine?

## Refinement Options

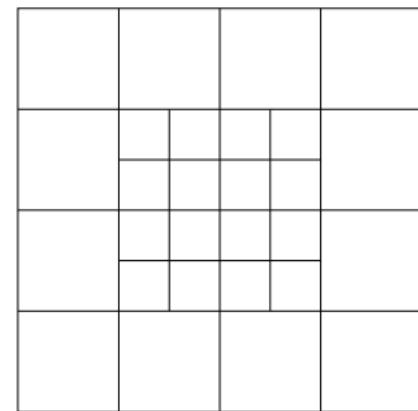
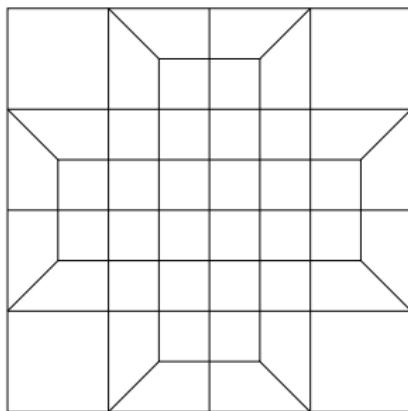
- ➊ Conforming or non-conforming?
- ➋ Structured or unstructured?
- ➌ Static or dynamic?

## Constraint

The spectral element method, as implemented in HOMME, requires **quadrilateral meshes** tiling a sphere.

Spoiler: conforming unstructured static refinement

# Conforming vs Non-Conforming [Quadrilateral] Refinement



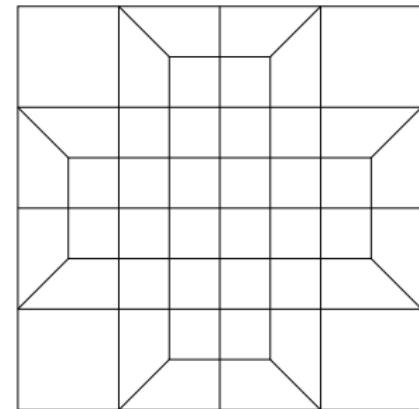
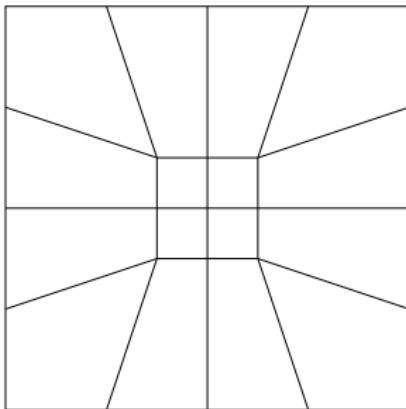
## Conforming Refinement (left)

- **Focus of this talk**
- Every edge is shared by exactly two elements

## Non-Conforming Refinement (right)

- Refine grid by splitting an edge
- Allows for “hanging nodes”

# Structured vs Unstructured [2D] Meshes



## Structured Mesh (left)

- Domain is tiled by elements in such a way that elements can be numbered with  $(i, j)$  coordinates

## Unstructured Mesh (right)

- **Focus of this talk**
- Domain is tiled arbitrarily

# Static vs Dynamic Mesh Refinement

## Static Refinement

- **Focus of this talk**
- Refine grid initially (based on topography, regional interests, etc), then run

## Dynamic Refinement

- Refine grid continually throughout the run (based on gradients, mass, or some other user-defined criterion)
- Computationally more expensive, also far more complicated to implement

**This project: conforming unstructured static refinement**

# More on Refinement Choice

## Why Conforming Unstructured Static Refinement?

- ① CAM-HOMME currently uses conservative SEM
  - Non-conforming refinement breaks conservation in SEM, would be better suited for DG (currently not part of CAM-HOMME)
  - Unstructured meshes allow more flexibility in refinement
- ② Will be running CAM-HOMME with variable resolution by end of fiscal year
  - Dynamic refinement would take significantly longer to implement (and would restrict refinement options)

# Changes Due to Refinement

## Two Major Changes to HOMME

- ① Implement hyperviscosity with variable viscosity coefficient, rather than static
- ② Ability to read in mesh (Exodus file) rather than simply generate “uniform” meshes

## And Some Minor Changes

- Map directly from element on sphere to reference element, bypassing cube (hope to move from “cubed sphere” to “global quads” in description of method)
- Change to resolution statistics (e.g. calculate average element length rather than average equatorial element length)

# Changes Due to Refinement

## Variable Viscosity

- Spectral Element core includes constant hyperviscosity

$$\frac{\partial \mathbf{u}}{\partial t} = -\nu \nabla^4 \mathbf{u},$$

implemented with auxiliary variable  $\mathbf{f}$ :

$$\begin{aligned}\frac{\partial \mathbf{u}}{\partial t} &= -\nu \left( \nabla(\nabla \cdot \mathbf{f}) - \nabla \times \hat{\mathbf{k}}(\nabla \times \mathbf{f}) \right) \\ \mathbf{f} &= \nabla(\nabla \cdot \mathbf{u}) - \nabla \times (\nabla \times \mathbf{u})\hat{\mathbf{k}}\end{aligned}$$

- Allowing  $\nu$  to vary, hyperviscosity is

$$\begin{aligned}\frac{\partial \mathbf{u}}{\partial t} &= - \left( \nabla \sqrt{\nu}(\nabla \cdot \mathbf{f}) - \nabla \times \hat{\mathbf{k}}\sqrt{\nu}(\nabla \times \mathbf{f}) \right) \\ \mathbf{f} &= \nabla \sqrt{\nu}(\nabla \cdot \mathbf{u}) - \nabla \times \sqrt{\nu}(\nabla \times \mathbf{u})\hat{\mathbf{k}}\end{aligned}$$

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## 2 Questions about Variable Viscosity

### 1. Why vary $\nu$ ?

Short Answer: Relationship between  $\nu$  and effective resolution

- If  $\nu$  is too large for fine mesh, results look similar to coarse mesh with same  $\nu$
- Alternately, if  $\nu$  is too small for coarse mesh, results are noisy

Complicated Answer: Locally, want to dissipate near the grid scale

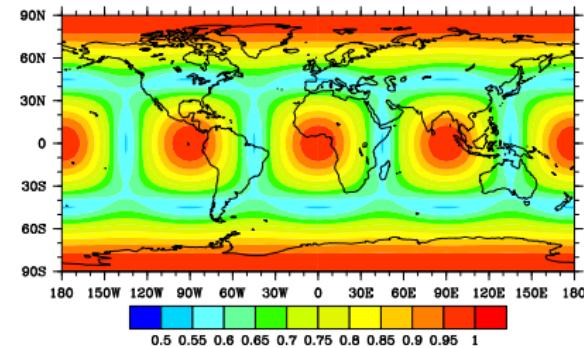
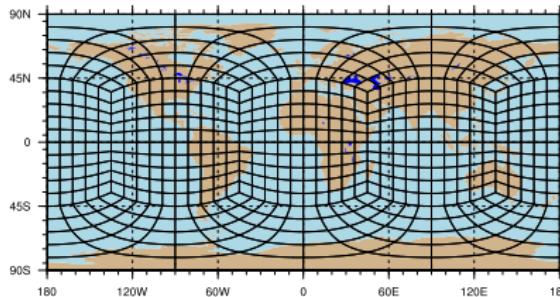
- This implies we want  $\nu = \nu(\Delta x)$

### 2. What's the best way to vary $\nu$ ?

Dissipation rate of mode  $k = 2\Delta x$  is  $\nu/\Delta x^4$

- Keeping dissipation rate constant  $\Rightarrow \nu = C\Delta x^4$

## 2 Questions about Variable Viscosity

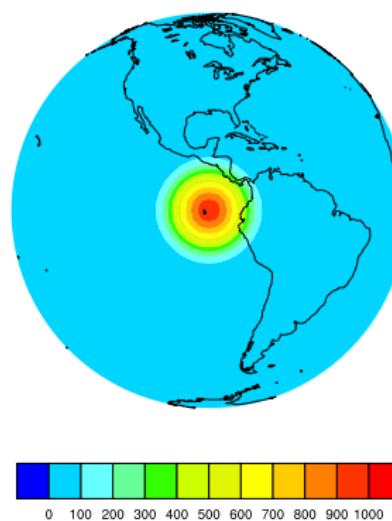


### More on Varying $\nu$

Since this is 2D code, vary  $\nu$  by square of element area:

- Define area of element  $\Omega_e := A_e$  and  $\Omega_i :=$  largest element.
- For any element  $\Omega_j$ ,  $\nu = \nu_0 \left( \frac{A_j}{A_i} \right)^2 \Rightarrow 0 < \nu \leq \nu_0$
- Continuity is enforced by averaging over element corners then using bilinear interpolation for element edges / interior nodes

# SWTC 1



## Williamson et al. – Test 1

- Advect a cosine bell around the globe
- A great test for refinement: refine the path of the bell

# Two Refinements

## Refinement Scheme #1

Start with  $6 \times 6$  uniform grid on all faces, refine to  $24 \times 24$  on the four equatorial faces ( $1 \rightarrow 16$  splitting)

## Refinement Scheme #2

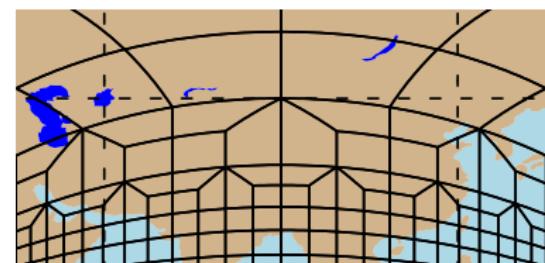
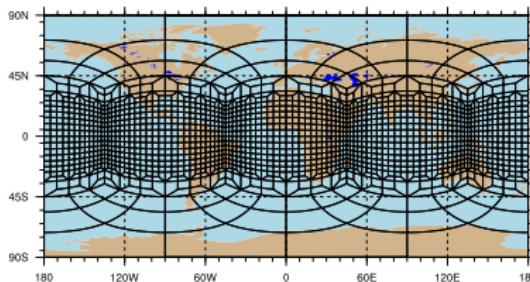
Start with  $12 \times 12$  uniform grid on all faces, refine to  $24 \times 24$  on the four equatorial faces ( $1 \rightarrow 4$  splitting)

### Notes:

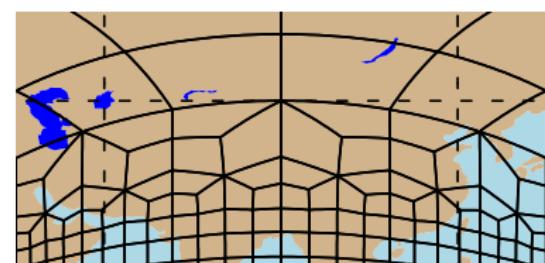
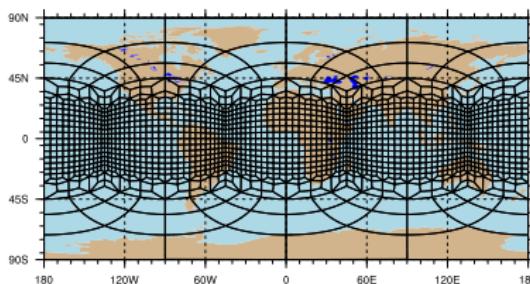
- The transition from coarse to fine occurs on equatorial faces
- Compare numerically to  $24 \times 24$  uniform grid
- “Improve” grid by [smoothing](#)

# SWTC 1 – Refinement #1

Not Smoothed

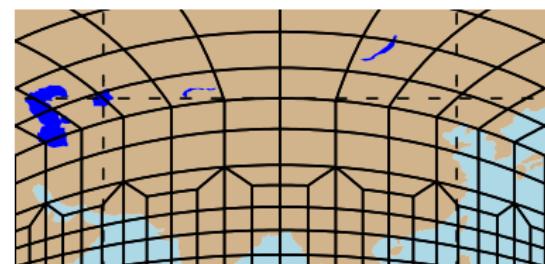
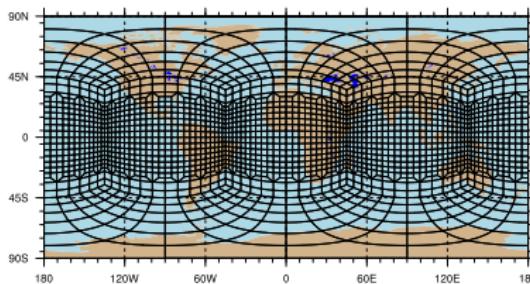


Smoothed (Mean Ratio technique)

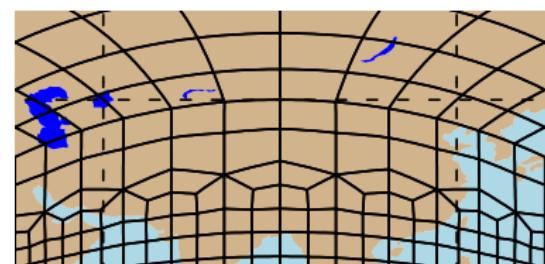
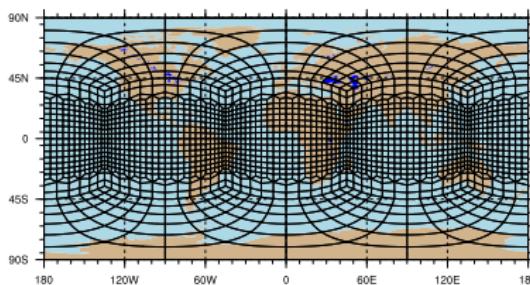


## SWTC 1 – Refinement #2

Not Smoothed



Smoothed (Mean Ratio technique)



## SWTC 1 – Computational Efficiency (Tabular)

Grid	# Elem	tstep (s)	Work Units	$L^2$ error
$12 \times 12$	864	720	1	$5.784 \cdot 10^{-2}$
$18 \times 18$	1944	480	3.38	$2.333 \cdot 10^{-2}$
$24 \times 24$	3456	360	8	$1.225 \cdot 10^{-2}$
Refine 1	1656	360	3.83	$1.343 \cdot 10^{-2}$
Refine 2	1920	360	4.44	$1.261 \cdot 10^{-2}$
Smooth 1	1656	360	3.83	$1.228 \cdot 10^{-2}$
Smooth 2	1920	360	4.44	$1.227 \cdot 10^{-2}$

## Table Details

- 1 work unit = computation (time) to run coarsest uniform grid  
*As resolution increases, time step decreases*
- Refined grids are slightly more work than 1944 element uniform grid, error is comparable to 3456 element uniform grid  
*Even better results w/ smoothing*

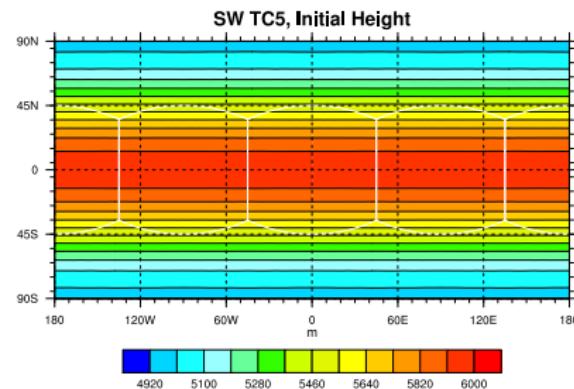
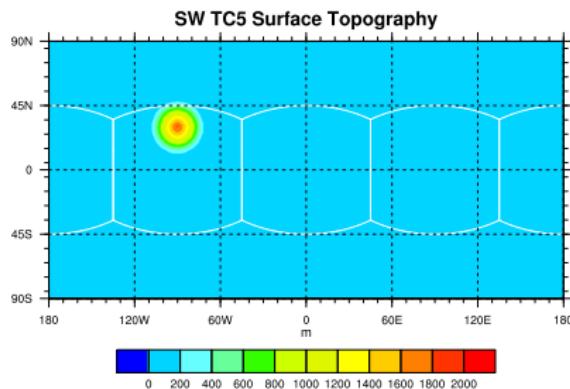
## SWTC 1 – Computational Efficiency (Graphical)



## Graph Details

- Same data as presented in table on previous slide
- Red line = uniform meshes, blue points = refined / smoothed
- Not shown: advecting through low-res region of refined mesh (over poles) results in same error as global low-res mesh

# SWTC 5



## Williamson et al. – Test 5

- Flow around an isolated mountain
- Another good test for refinement: refine around the mountain

# Experiment

Mountain has radius of  $20^\circ$ , refine area w/ radius  $30^\circ$   
Compare meshes based on coarsest elements

## Notation

Grid: N20\_x4\_s9

- N20 Begin with uniform grid based on  $20 \times 20$  elements on each face of cubed sphere
- x4 Refine such that edge length in coarse region is 4 times the length of that in fine
- s9 Apply smoothing operator to grid 9 times

## Source

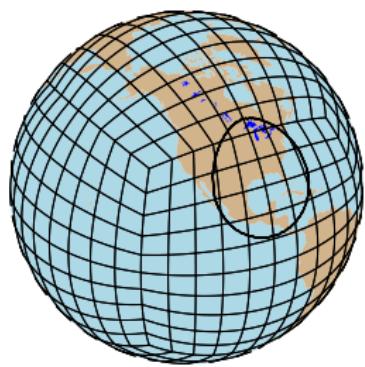
*Exploring a Multi-Resolution Modeling Approach within the Shallow-Water Equations*

T. D. Ringler, D. Jacobsen, M. Gunzburger, L. Ju, M. Duda, W. Skamarock

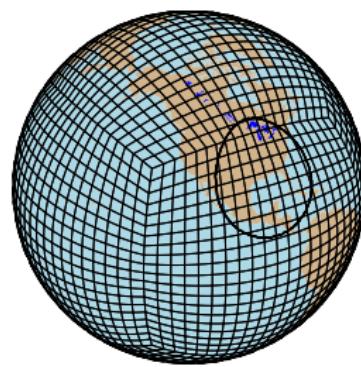
Submitted to Monthly Weather Review

# Comparing three grids

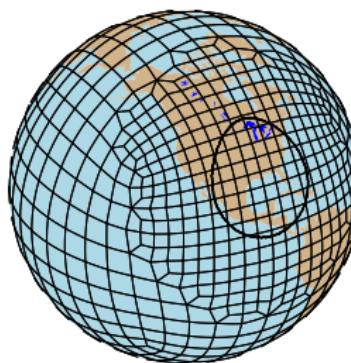
N10\_x1.g



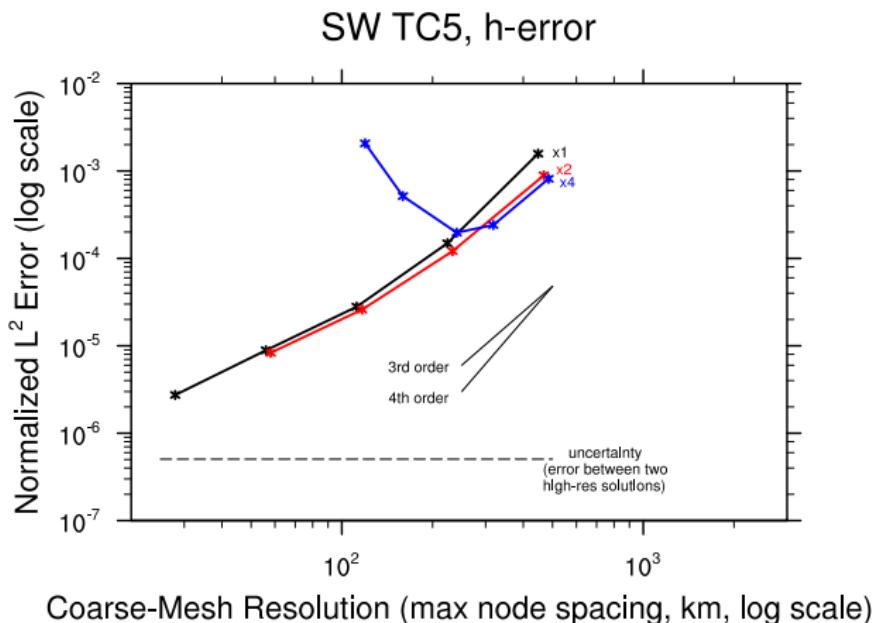
N20\_x1.g



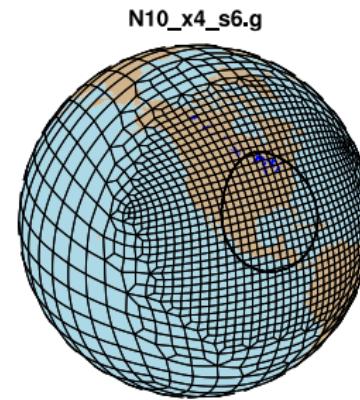
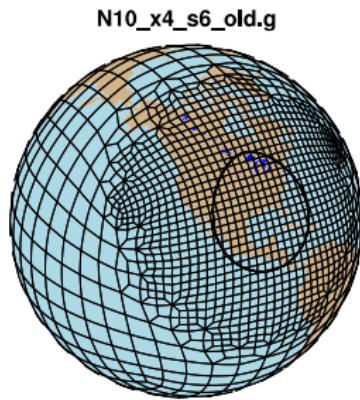
N10\_x2\_s6.g



## First wave of results



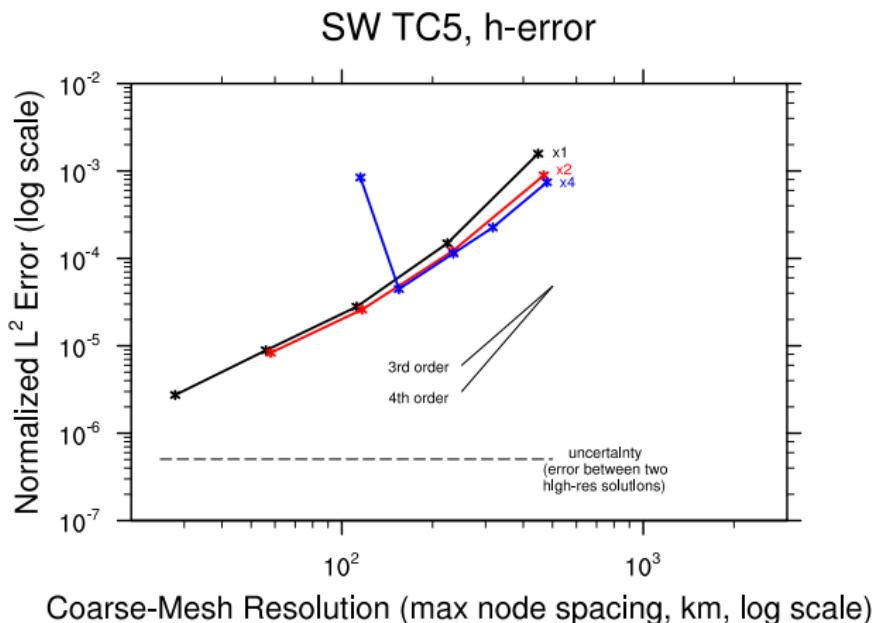
# Problem in the x4 Grids



## Transition Region

We kept the size of the fine mesh the same, but enlarged the transition region. This fixed the low-res x4 grids, but still had a problem around N40.

## Second Wave of Results



# Future Work

## Still to Come

- ① Improve grid construction (“sizing function” determines how elements are located, Anderson et al.)
  - Though transition region improved look of x4 results, didn’t help much with x8 grids
- ② Initial 3D runs: start w/ aquaplanet
- ③ Full 3D: look into vertical dissipation (Tribbia and Temam report)
- ④ Get mesh refinement working with DG core of HOMME

# Acknowledgements



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