

# SNL MHK Modeling Activities

## Partners:

- **Labs:** NREL, PNNL, ORNL
- **Universities:** Penn State ARL, OSU, UC Davis, UW, Bucknell, UMN
- **Industry:** Re Vision, SEA Engineering, Columbia Power Technology, Verdant, Berkeley Wave Tank



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## Key Objectives and Approach

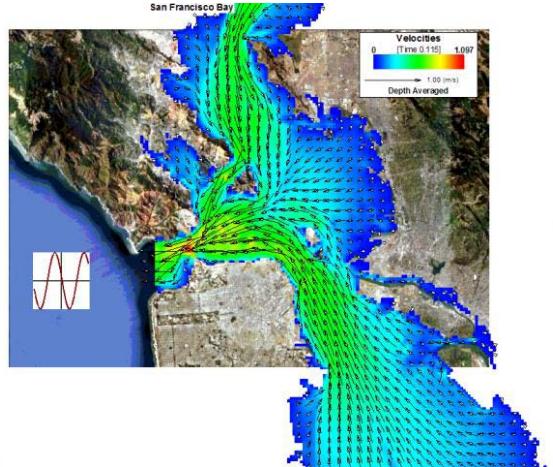
**Use analytical tools, computer models, and testing to investigate:**

- Component and system performance (small scale)
- What happens when energy is extracted from a system (large scale)

## Outcome

1. Reduce costs for MHK build out with predicitive simulations
2. Understanding environmental limits to MHK development
3. Provide MHK specific data sets and assessment tools

**Optimize for maximum energy capture with minimum environmental impact**



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# ***MHK Technology Development***

## ***Task Structure\****

<b>1.3.1 WEC Systems</b>	<b>1.3.2 Current/Tidal Systems</b>
WEC Device Modeling	Single Turbine Performance Modeling
WEC Arrays	Array Performance Modeling
Wave Environment Hydrology	Large Scale Hydrology Modeling for Inflow
	Turbine Design

\*SNL is also the lead for modeling and testing activities in Reference Model (1.2.5), Market Acceleration (2.1.X) and 1.4.1 Testing and Evaluation tasks



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# *Single Turbine Performance Modeling*



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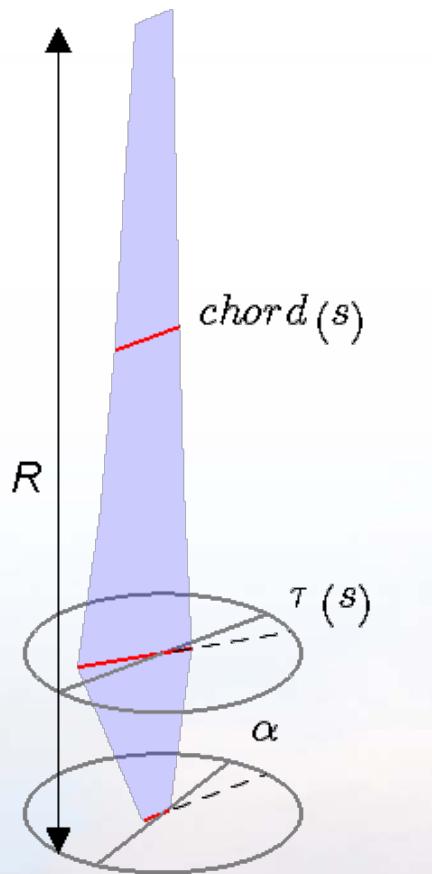
# ***CACTUS (Code for Axial and Cross-flow Turbine Simulation) Overview***

- Marine turbine performance simulation
- Potential flow representation of fluid dynamics
  - Lifting-line element description of blade
  - Free vortex lattice description of wake
  - Panel elements used on boundaries (bottom and free surface)
- VDART3 heritage
  - SNL free vortex wake code for Darrieus wind turbines
- Fortran 95 implementation
  - Modular code structure

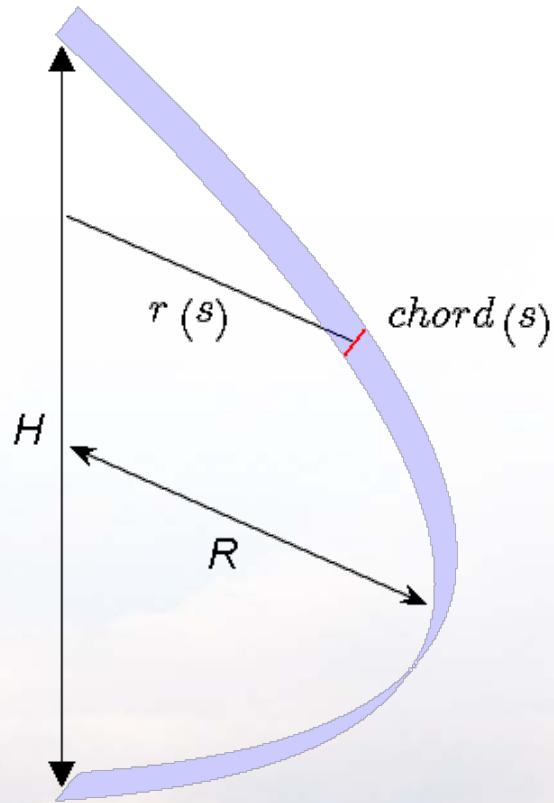


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# Rotor Geometry



a) Axial turbine blade



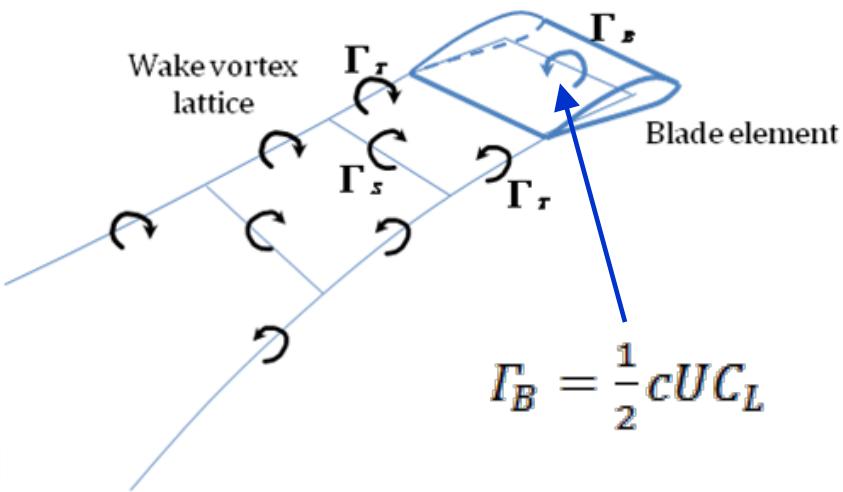
b) Cross-flow turbine blade

- Can model both axial and cross-flow rotors
- General user-specified geometry interface is planned



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# Blade Element Method



## ■ Blade loads from empirical data

- Steady 2D airfoil data including non-linear effects
- Attached flow dynamic effects from pitching flat plate theory
- Additional models for dynamic stall effects

## ■ Blades represented as lifting lines

- Bound vorticity on each element given by Kutta-Joukowski theorem
- Spanwise variation in bound vorticity creates trailing wake vorticity
- Temporal variation in bound vorticity creates spanwise wake vorticity

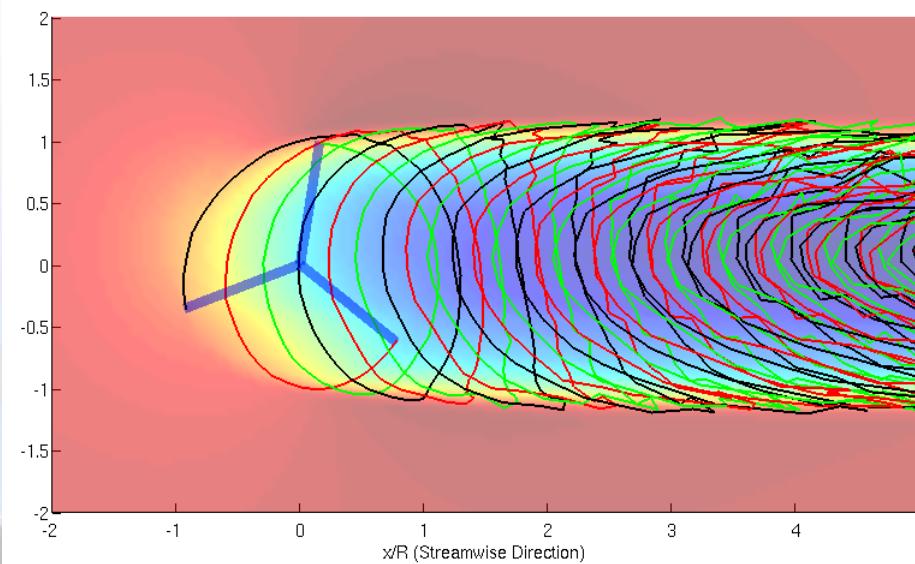
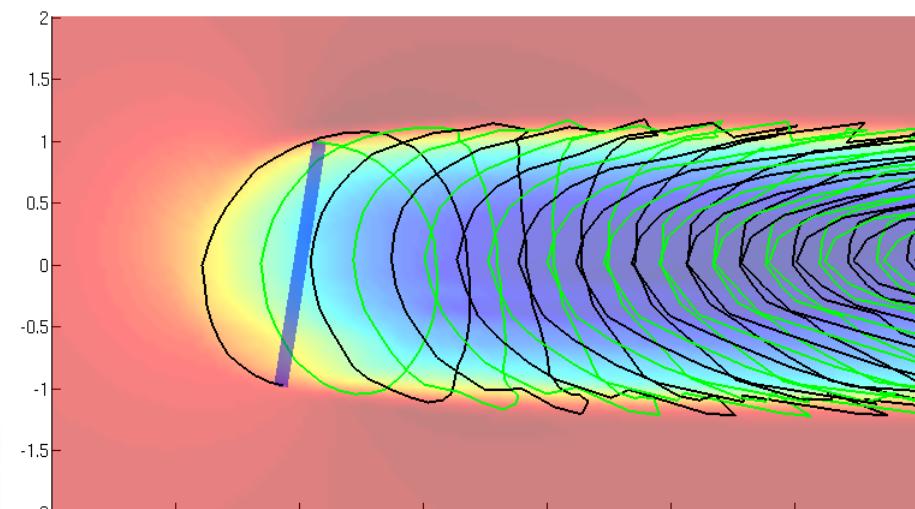
## ■ Bound and wake vorticity model effects of rotor on fluid flow



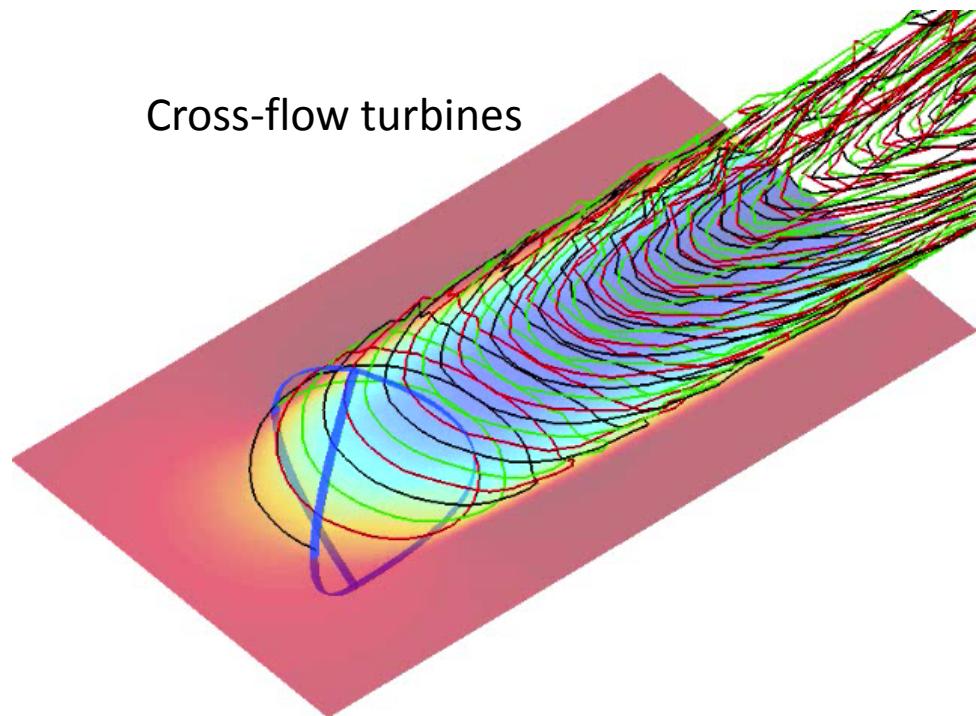
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# MATLAB Post Processing

Axial-flow turbines



Cross-flow turbines



- Visualizations of velocity field and vortex filament traces.



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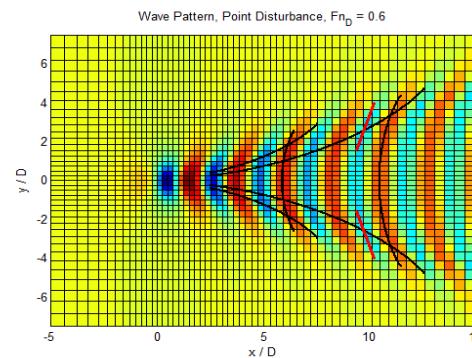
# Progress and Future Enhancements

## ■ Progress

- Free Surface Verification
- Validation with Sandia 34 Meter VAWT

## ■ Future Activities

- Cavitation onset prediction
  - Significant damage is possible for blades operating in cavitating flow
  - Onset when fluid pressure reaches vapor pressure
- Panel element blades
  - Full description of blade geometry and near field flow
  - May be necessary for high solidity rotors
- Acceleration of wake influence calculations
  - Wake velocity influence calculation is very expensive
  - Parallel implementation on GPU
  - Calculation easily ported using CUDA programming language



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# *Array Performance Modeling*



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*Updated EFDC Model*

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**SNL-EFDC**

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*Remains Public Domain*



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# *Turbine Energy Extraction*

- Turbine energy extraction is manifest as:

- Decreased momentum
  - Altered (usually increased) turbulent kinetic energy
  - Increased turbulence dissipation rate (turbulent length scale)

- These quantities (momentum and  $K-\varepsilon$ ) are advected and dispersed downstream



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# *Momentum Sink: Turbine*

$$P_{\text{MHK}} = -\frac{1}{2} C_T A_{\text{MHK}} \rho U^3$$

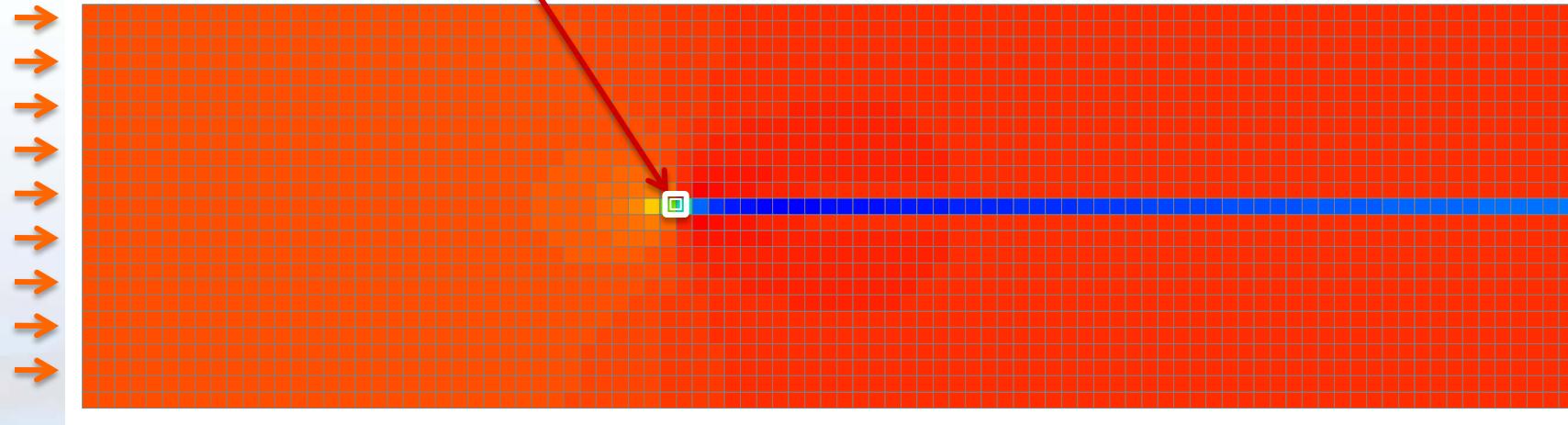
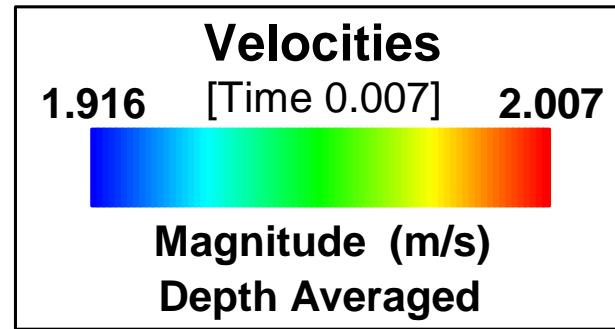
$$S_Q = -\frac{1}{2} C_T A_{\text{MHK}} U^2$$



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# *Single Turbine Model – Momentum Sink Only*

MHK Device



- Overly persistent velocity defect



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# $K-\varepsilon$ Modifications: Turbine

## Empirical constants

$$S_K = \frac{1}{2} C_T A_{\text{MHK}} \left( \beta_p U^3 - \beta_d U K \right)$$
$$S_\varepsilon = C_{\varepsilon 4} \frac{\varepsilon}{K} S_K$$

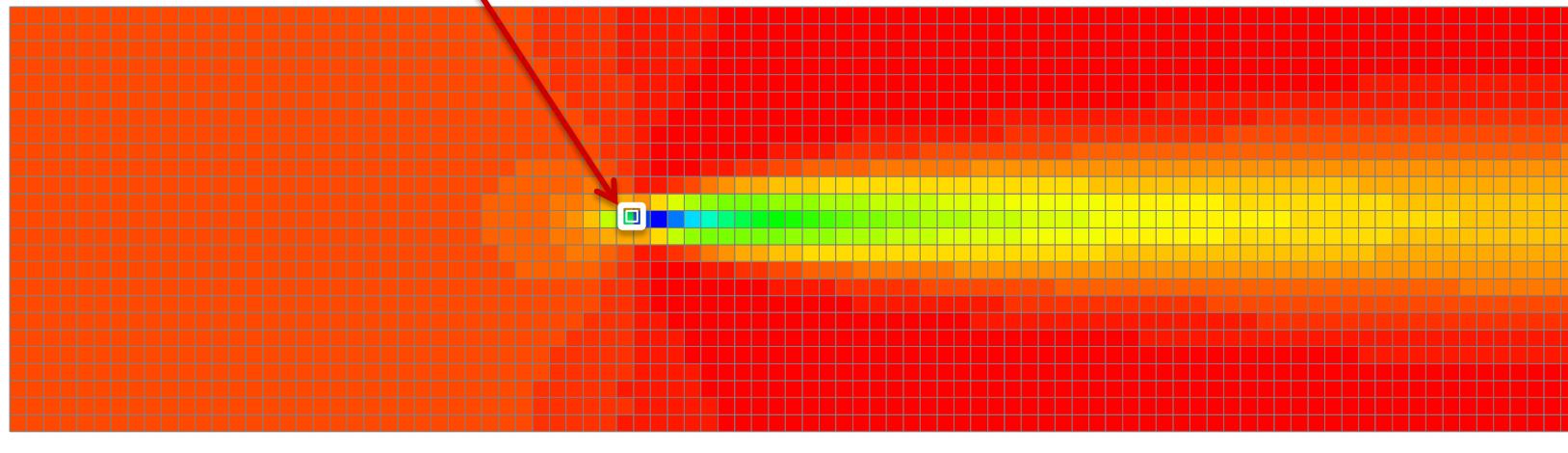
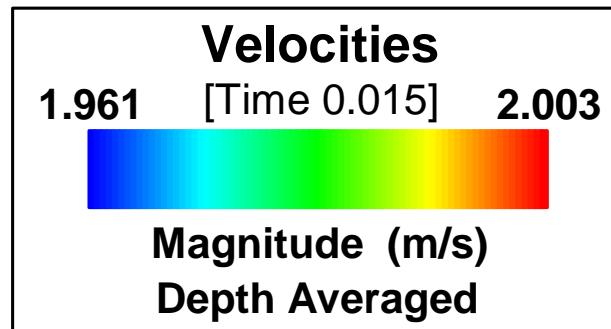
Katul, G. G., L. Mahrt, D. Poggi, and C. Sanz (2004), One- and two-equation models for canopy turbulence, *Boundary-Layer Meteorology*, 113, 81-109.



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# *Single Turbine Model – K-e Sinks Included*

MHK Device

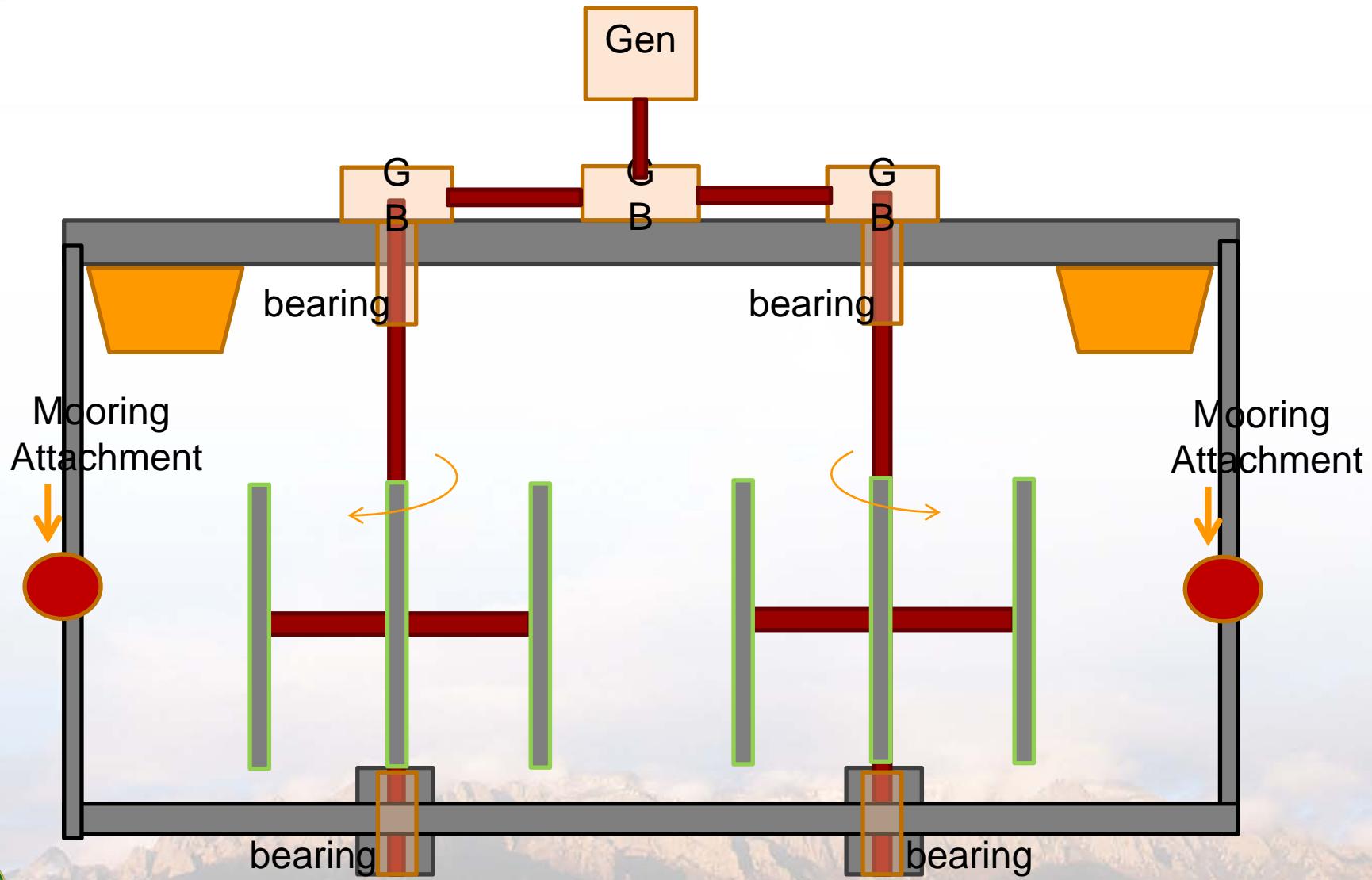


- Realistic fluid energy loss/wake behavior
- Verified with Meyer and Bahaj, 2010



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# *Floating Platform with Dual Rotors*

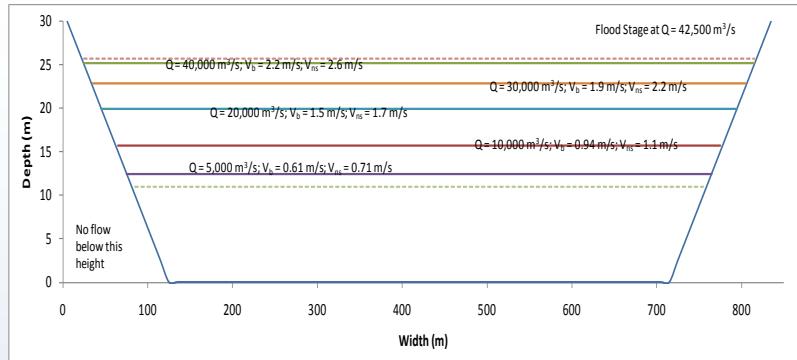


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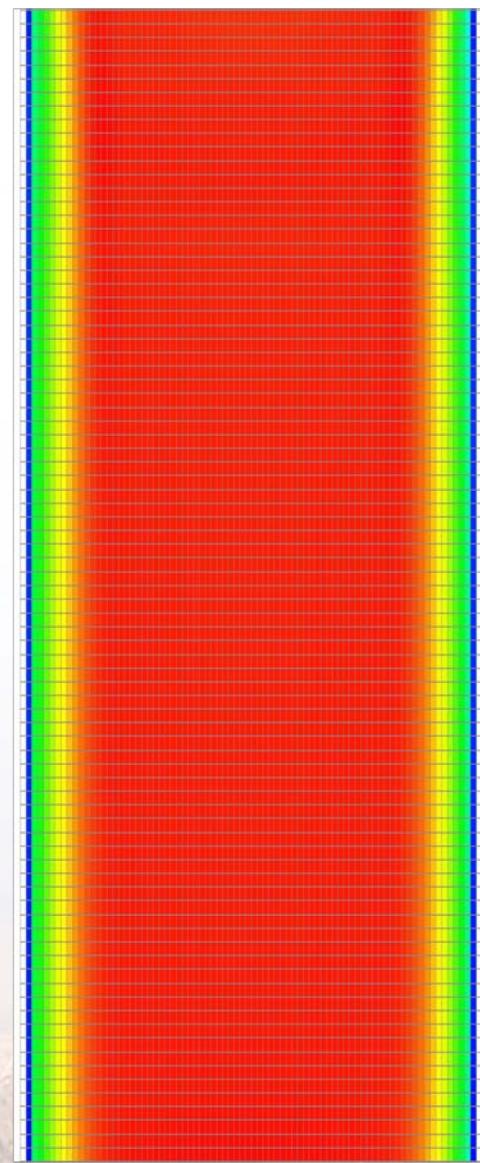
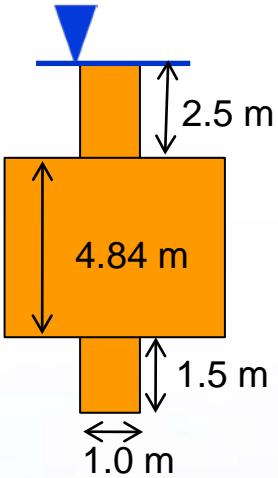
# Model Domain: Turbine Array Optimization

## General Model Conditions

- Grid is 840 m by 4,200 m
- Cells are 10 m x 30 m
- 10 vertical layers
- Channel full top width is 840 m
- Bottom width is 600 m
- Max depth is 30 m



## Turbine Geometry



## Specific Model Conditions

- Flow is constant  $20,000 \text{ m}^3/\text{s}$
- $U_\infty \approx 1.6 \text{ m/s}$
- Top width is  $\approx 750 \text{ m}$
- Max depth is  $\approx 20 \text{ m}$



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# Horizontal Turbine Array Optimization

0.5 Platform Spacing

1.0 Platform Spacing

1.5 Platform Spacing

2.0 Platform Spacing

2.5 Platform Spacing

3.0 Platform Spacing



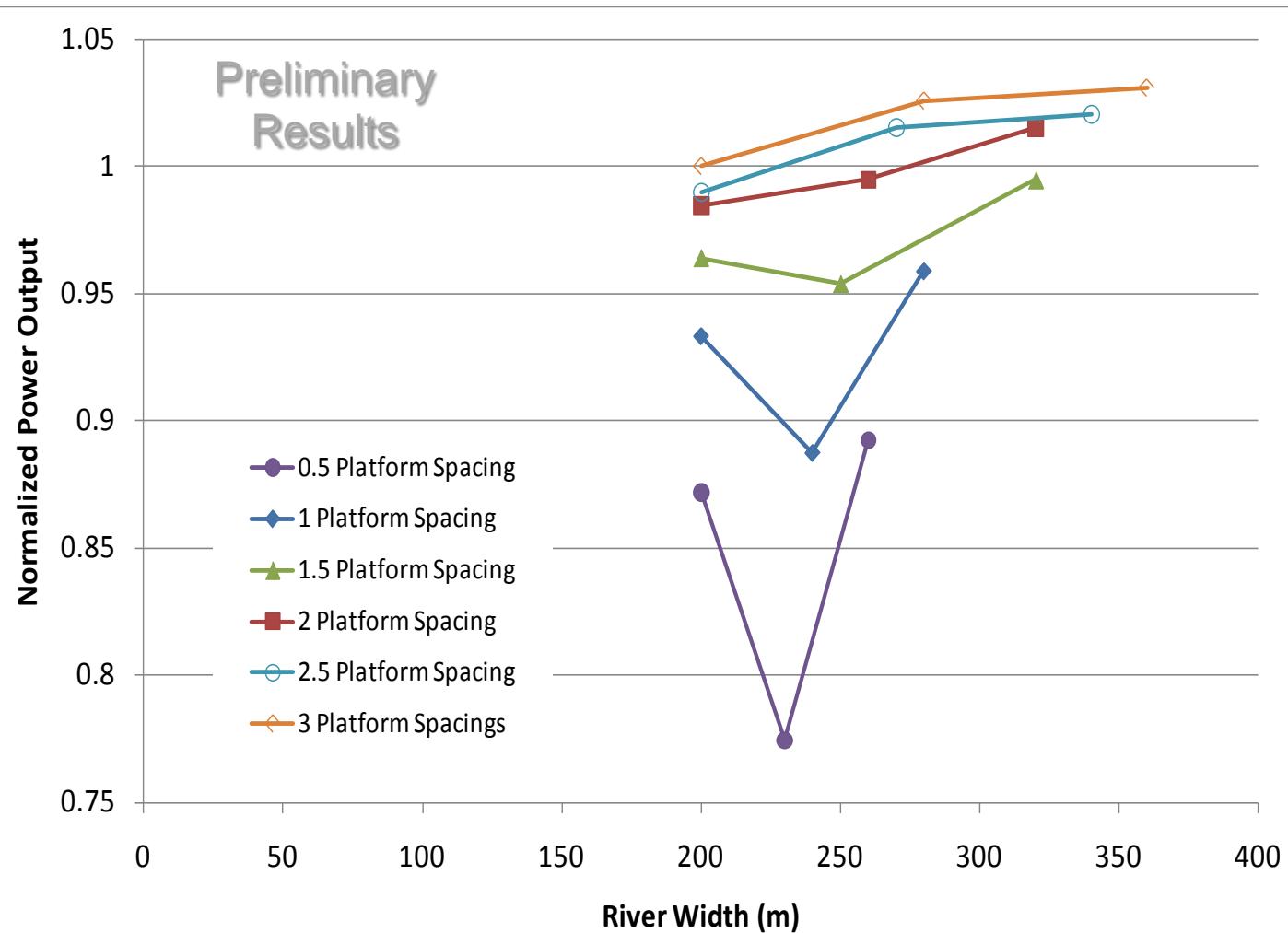
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# Effects of Horizontal Turbine Spacing

Normalized by power output from 1 Platform near center of channel!

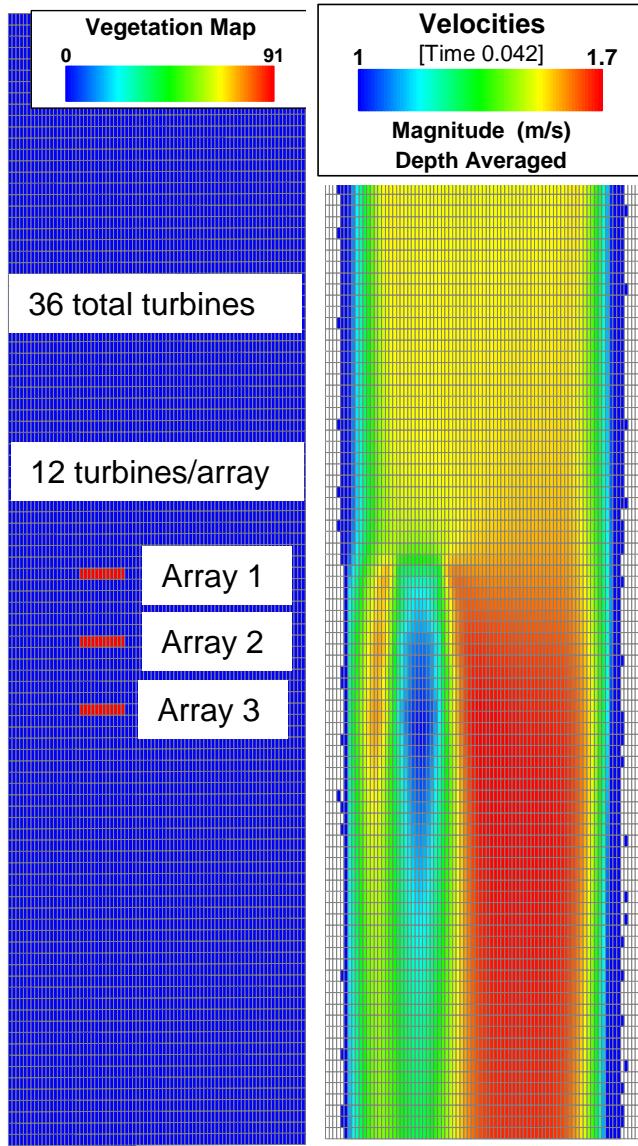


- The 'left' turbines are affected by horizontal velocity profile (slower flow nearer to bank).
- An increase in power (above a single platform by itself) can be seen as the turbines are placed further apart (helping each other).

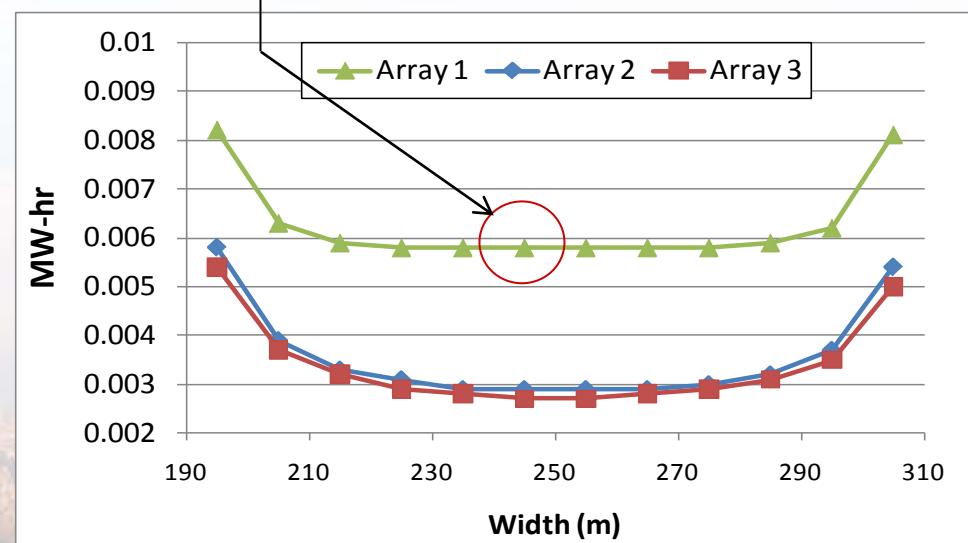
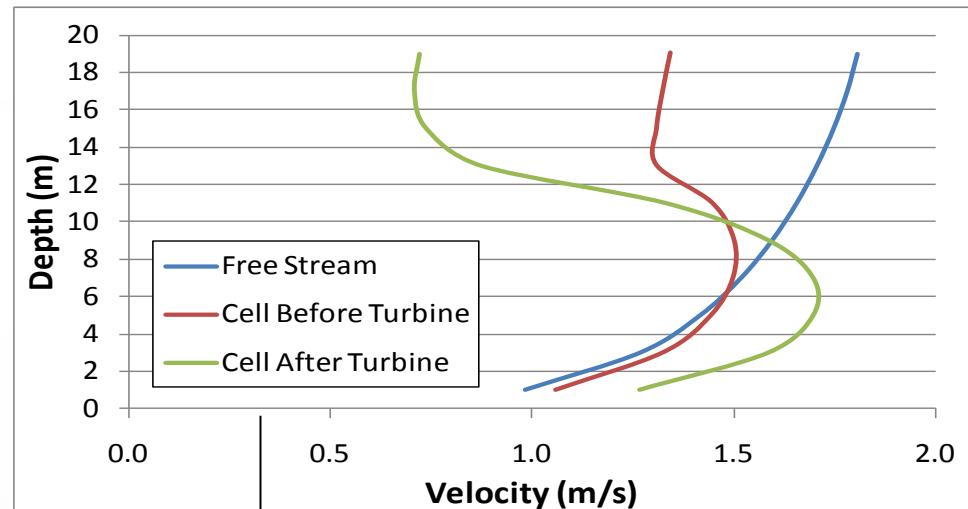


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## Preliminary Results



# Turbine Array Effects



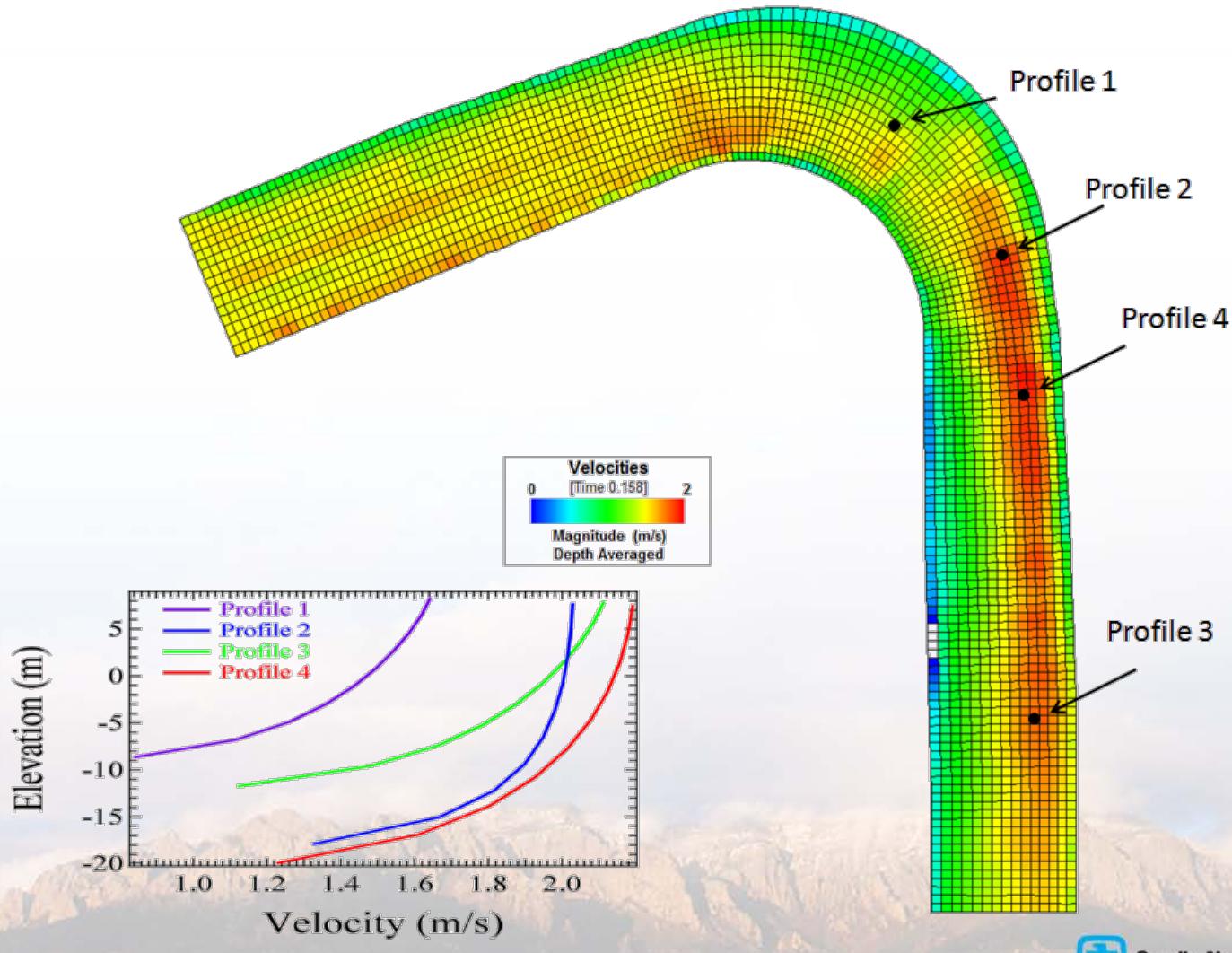
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# *Large Scale Hydrology Modeling for Inflow*



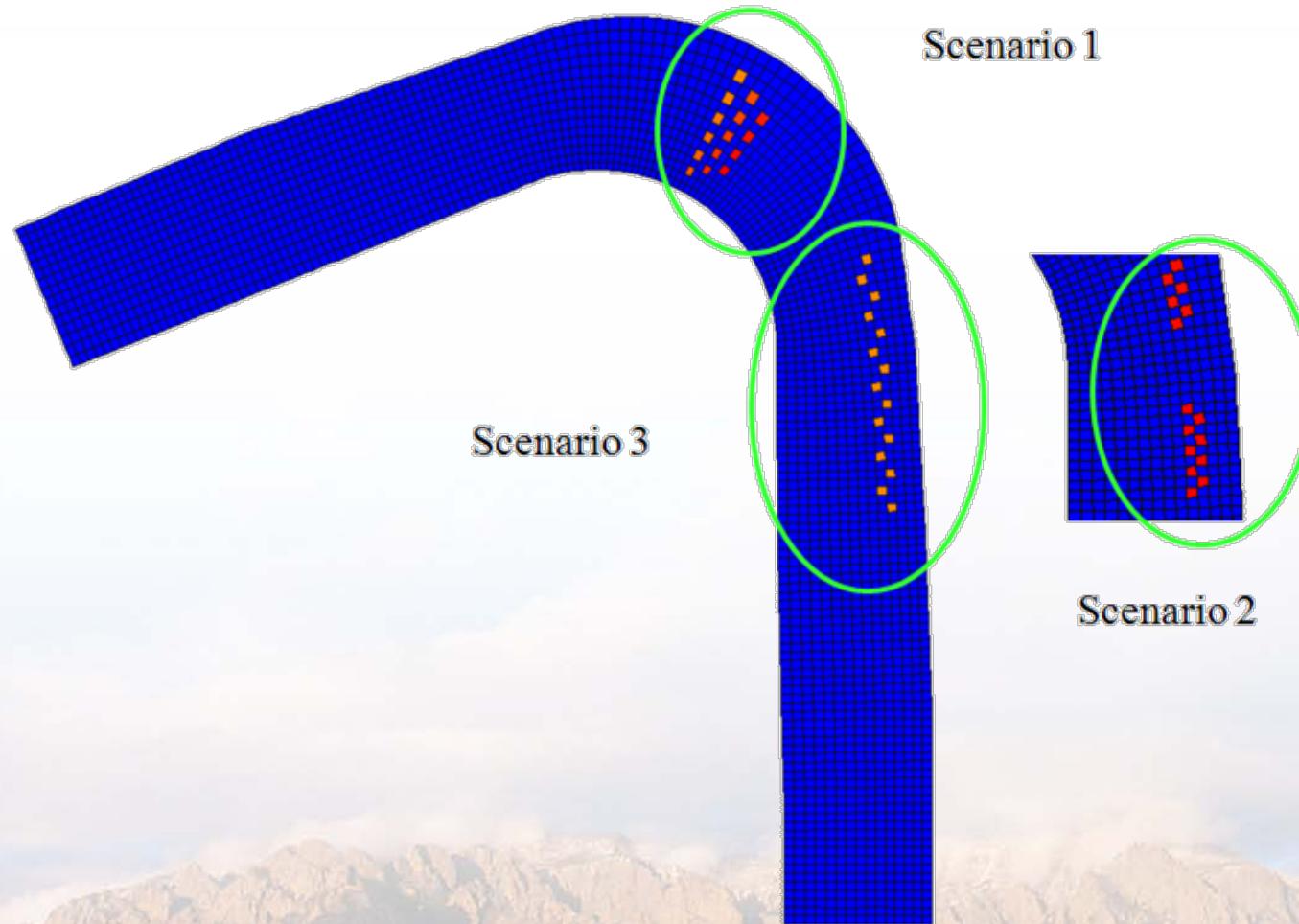
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# Mississippi River, Scotlandville Bend



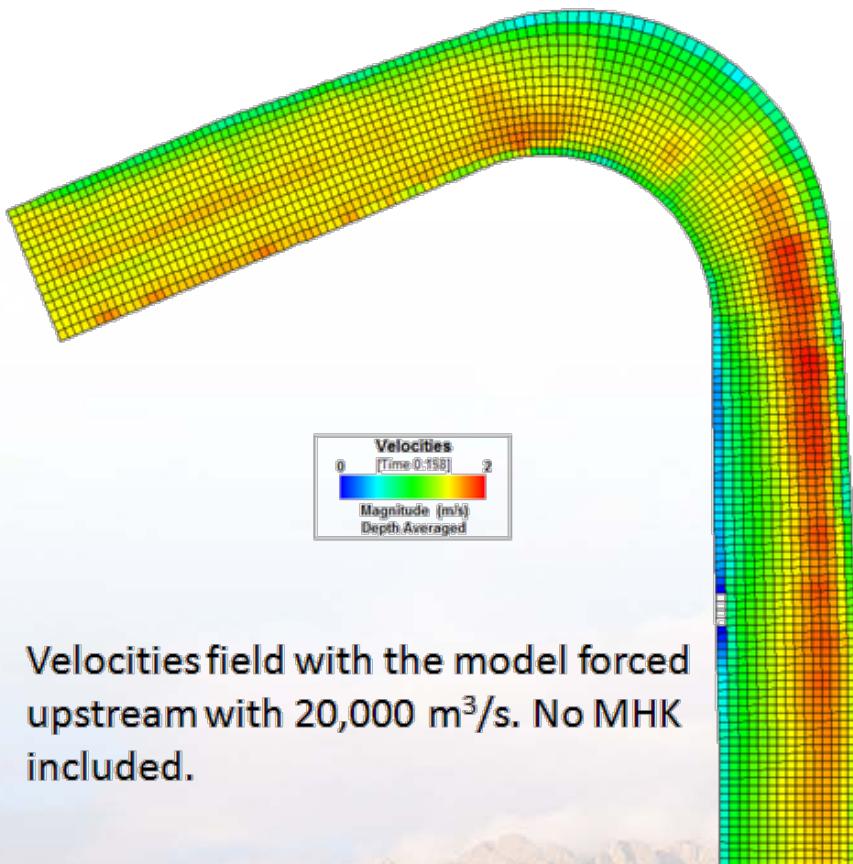
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# *Mississippi River, Scotlandville Bend*

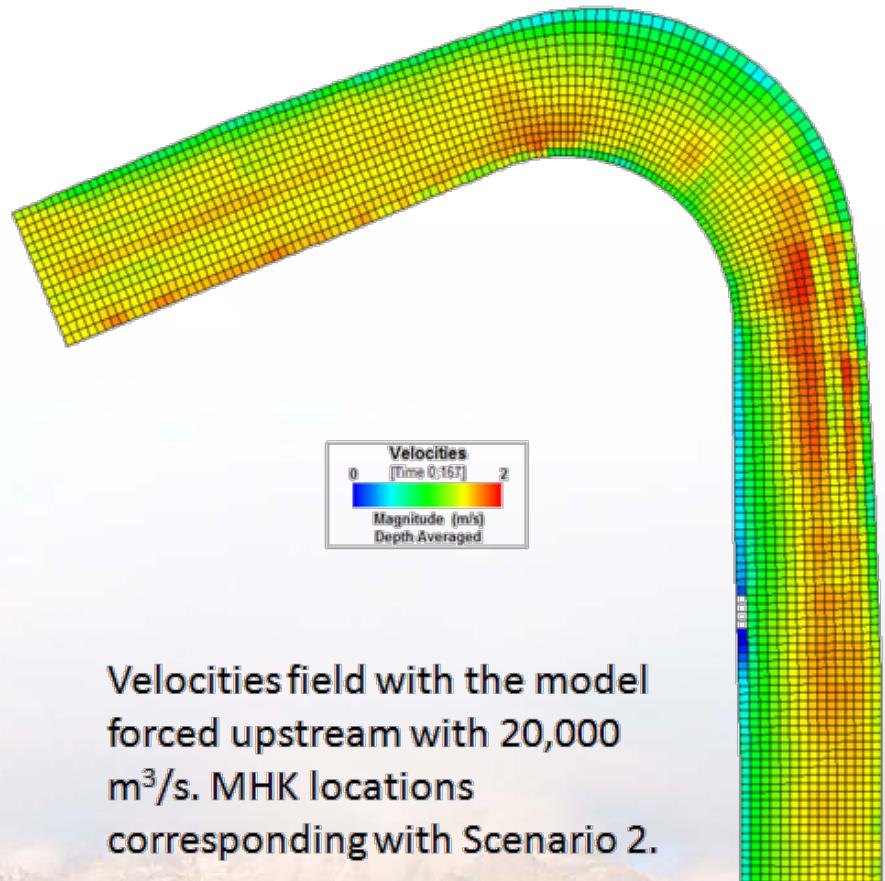


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# Mississippi River, Scotlandville Bend



Velocities field with the model forced upstream with 20,000 m<sup>3</sup>/s. No MHK included.



Velocities field with the model forced upstream with 20,000 m<sup>3</sup>/s. MHK locations corresponding with Scenario 2.



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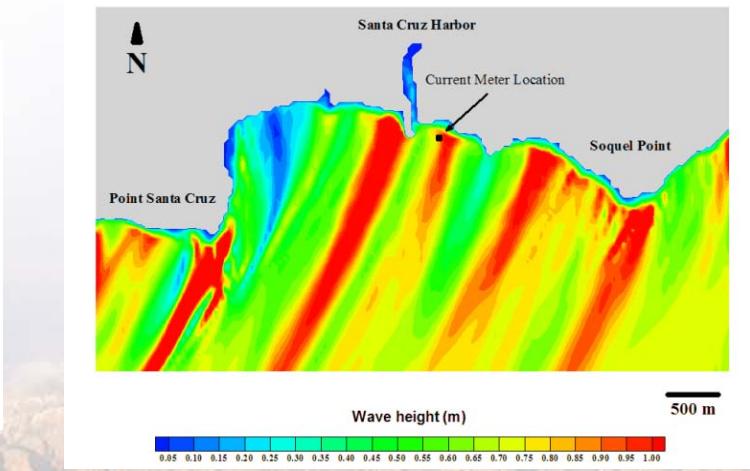
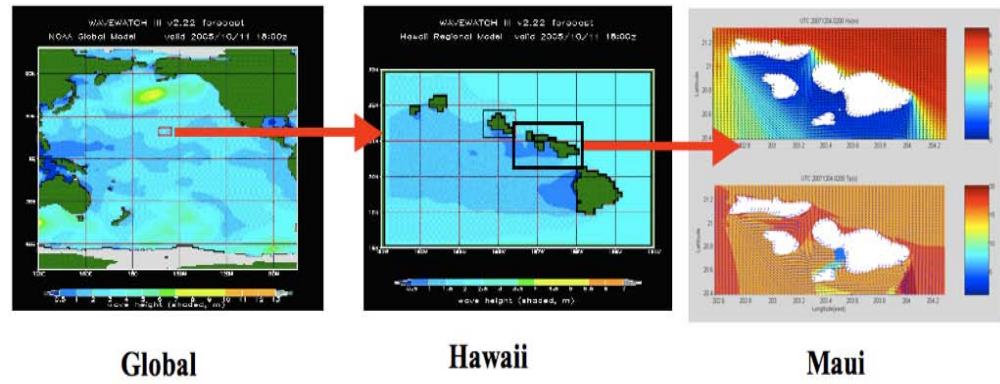
# *Wave Environment Hydrology*



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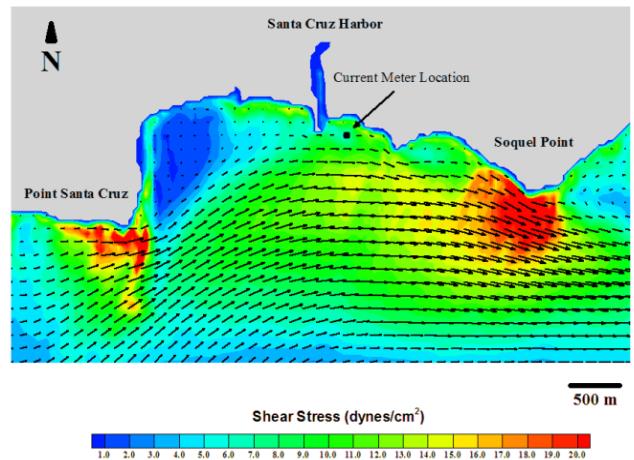
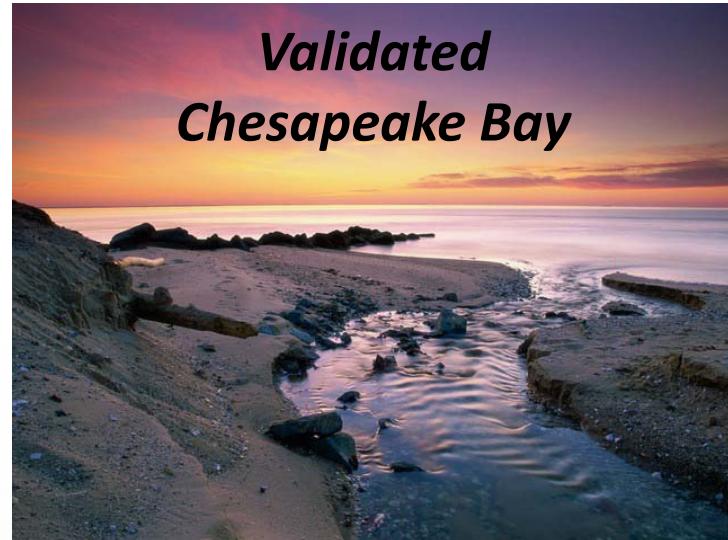
# *SWAN and WaveWatchIII – Wave Modeling*

- NWW3 – NOAA operational wave model
  - Generate deepwater offshore wave conditions
- SWAN – Simulating WAves Nearshore (Delft)
  - Propagation of deepwater waves into nearshore
    - Refraction, diffraction, shoaling, energy dissipation, breaking



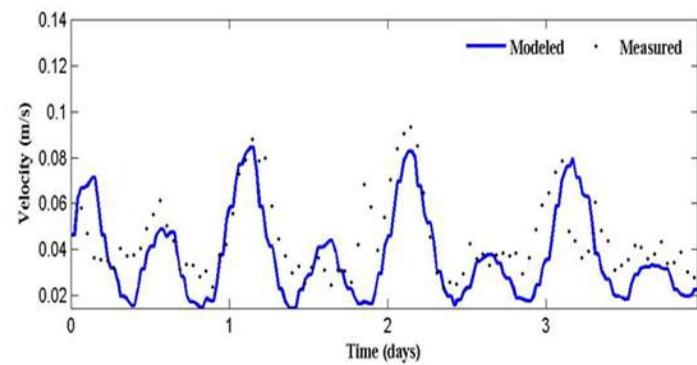
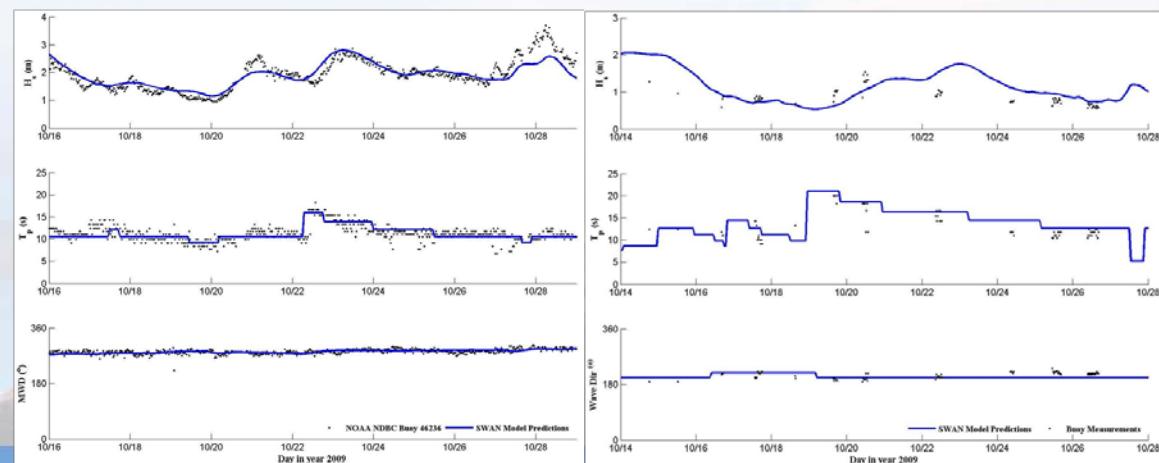
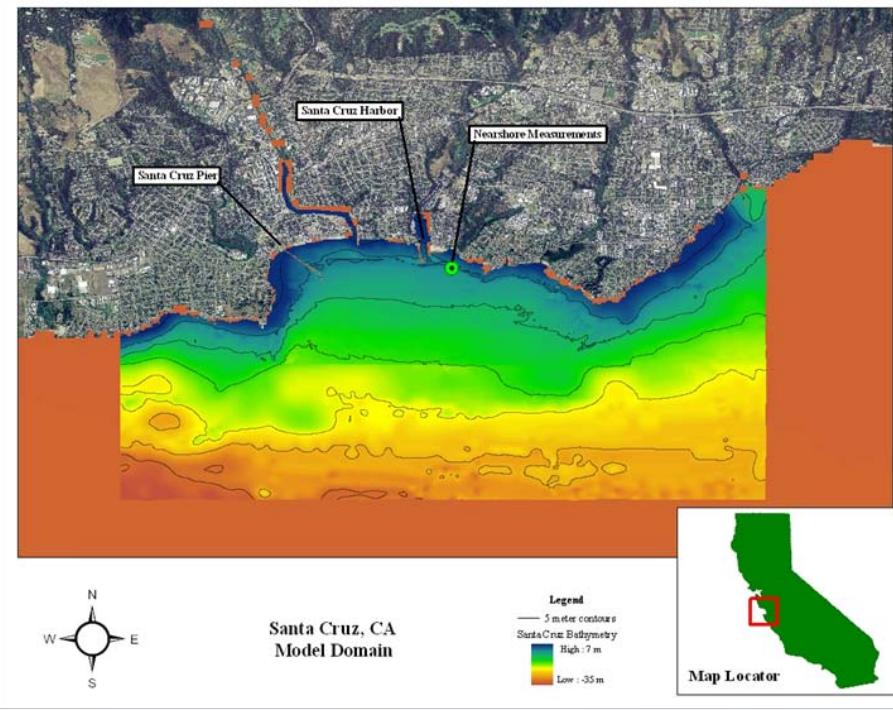
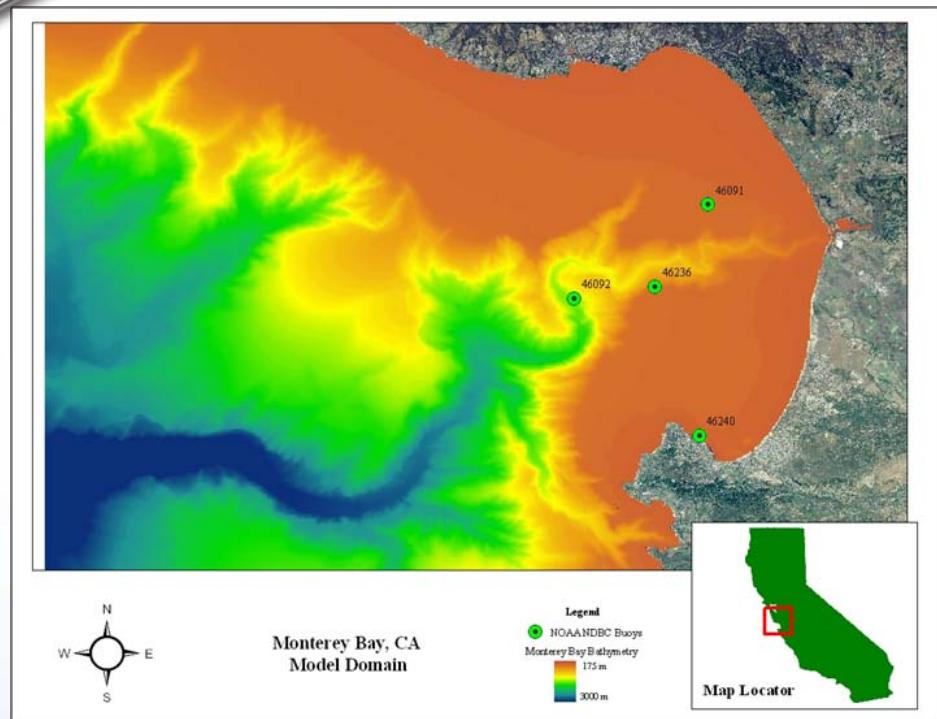
# EFDC – Flow and Transport

- EPA open-source code
- Curvilinear orthogonal grid
- Coupled-equation solution
  - Mass conservation
  - Momentum conservation
  - $K-\varepsilon$  conservation
  - Temperature transport
  - Salinity transport
  - Dye transport
- Links with SWAN time-series



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# Wave and Circulation Model – Santa Cruz



# ***MHK Technology Development***

## ***Task Structure\****

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	Turbine Design

\*SNL also modeling and testing activities in Reference Model and Market Acceleration tasks



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# *Extra Slides*



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# ***SEDZLJ – Sediment Dynamics***

Flumes necessitated the development of improved model

- Simultaneous treatment of cohesive and non-cohesive sediments
- Erosion – **Based on site-specific flume data**
- Transport – **Bedload and suspended load**
- Bed armoring and consolidation
- Bed-slope effects
- Multiple sediment size classes
- Slope dependence
- Cohesive bed consolidation
- Morphological feedback to flow
- 3-D sediment bed

***Sediment Model – Cedar Lake***

Total Suspended Sediment Concentraion (mg/L)



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