

Axial Crushing of Aluminum Tubes

Experimental Results and Finite Element Modeling

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Introduction

- Many Sandia-designed systems may be subjected to severe mechanical environments.
Performance issues require analysis of system response under these conditions.
- System and component level finite element models are widely used to perform a substantial part of the analysis and to guide testing.
- Validation of FE modeling capabilities by comparison to experiment is an essential part of the process.

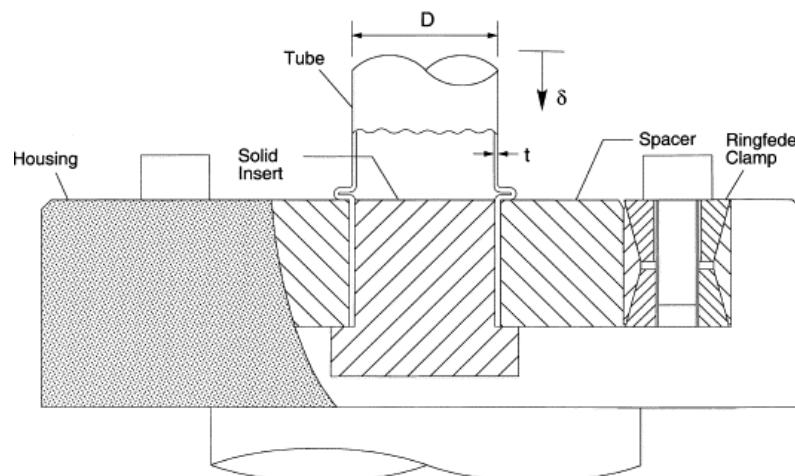
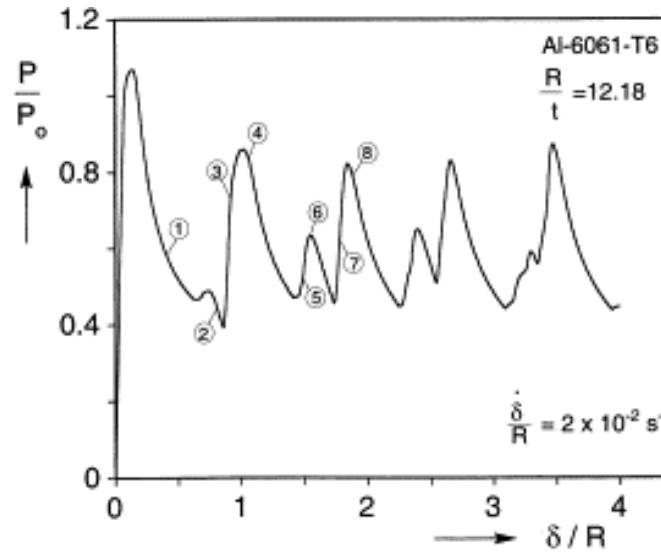
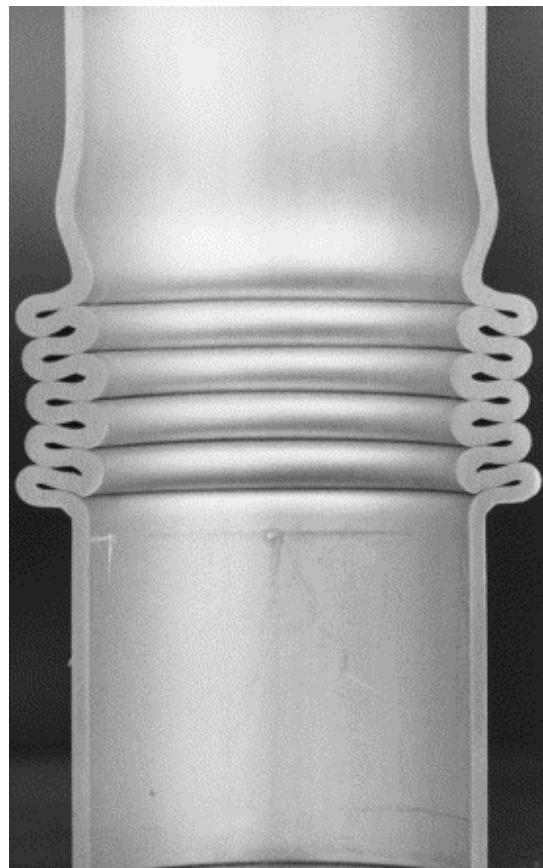


Objectives

- Demonstrate the performance of FE nonlinear structural models to simulate crushing and other large-deflection scenarios.
- Examples:
 - Crushing of tubular structures
 - Hydraulic collapse
 - Puncturing
 - Etc.
- This presentation addresses aluminum tubes crushed by quasi-static axial compression.



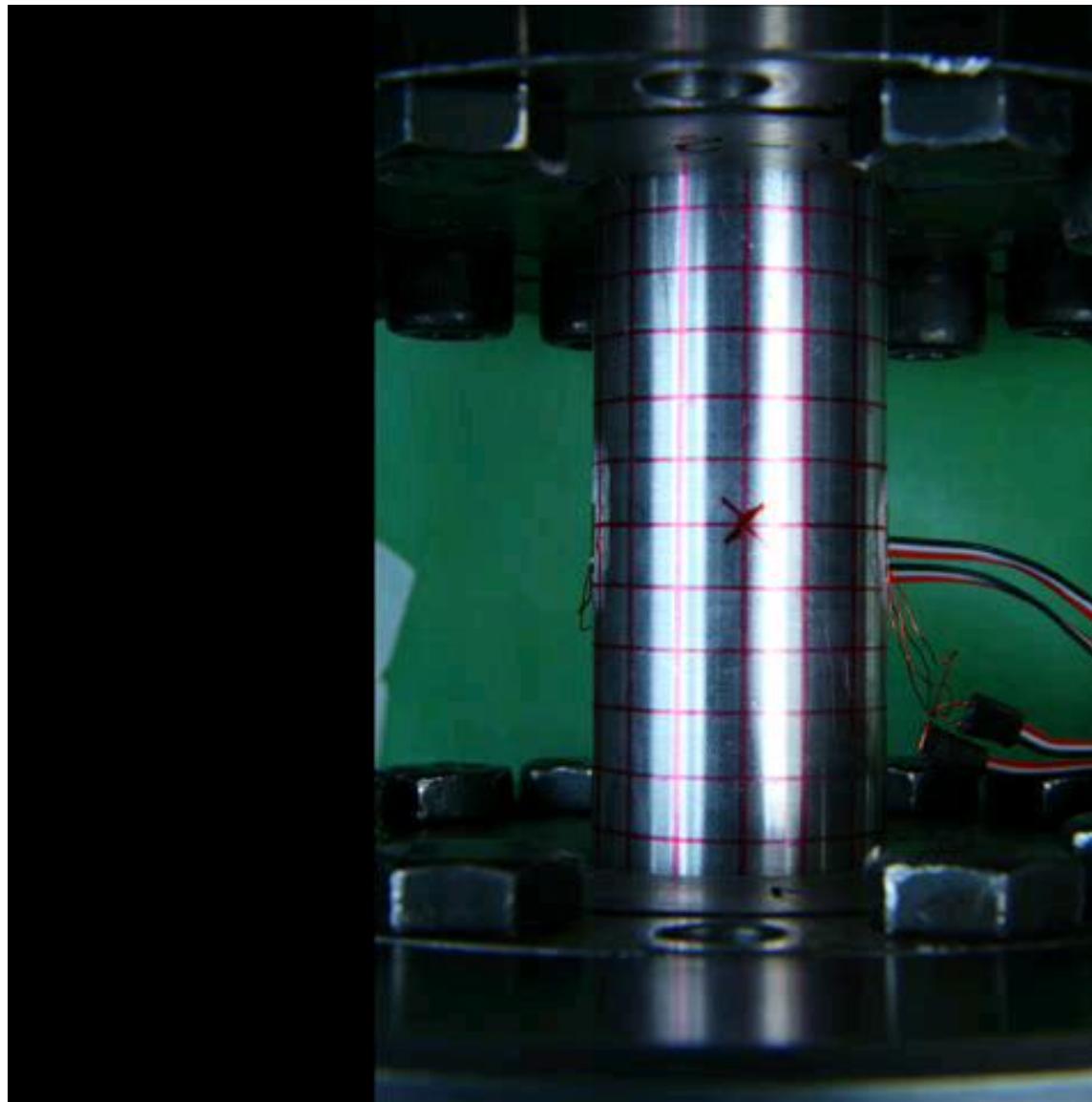
Axisymmetric Collapse (Bardi et al, 2003)



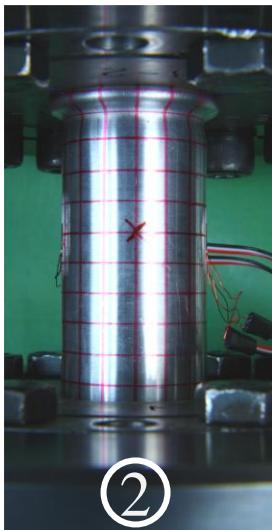
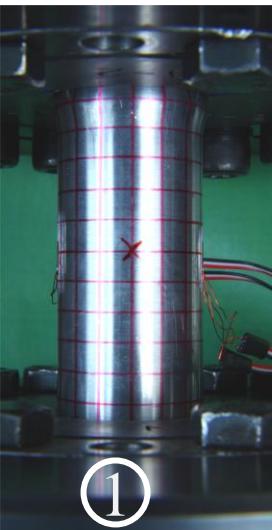
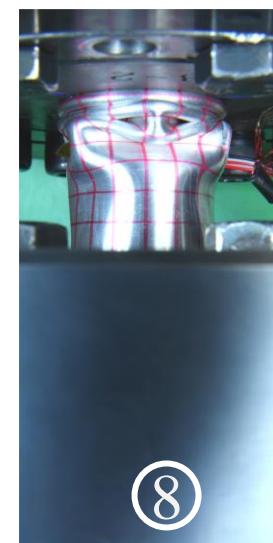
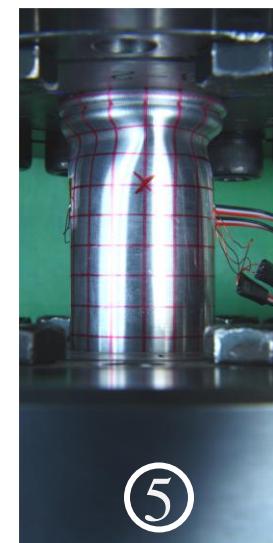
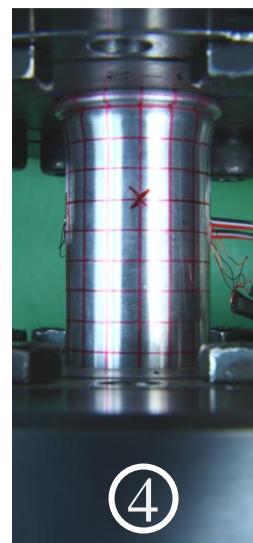
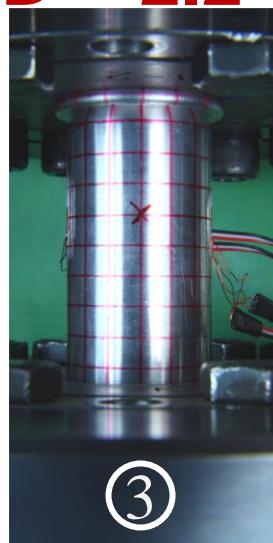
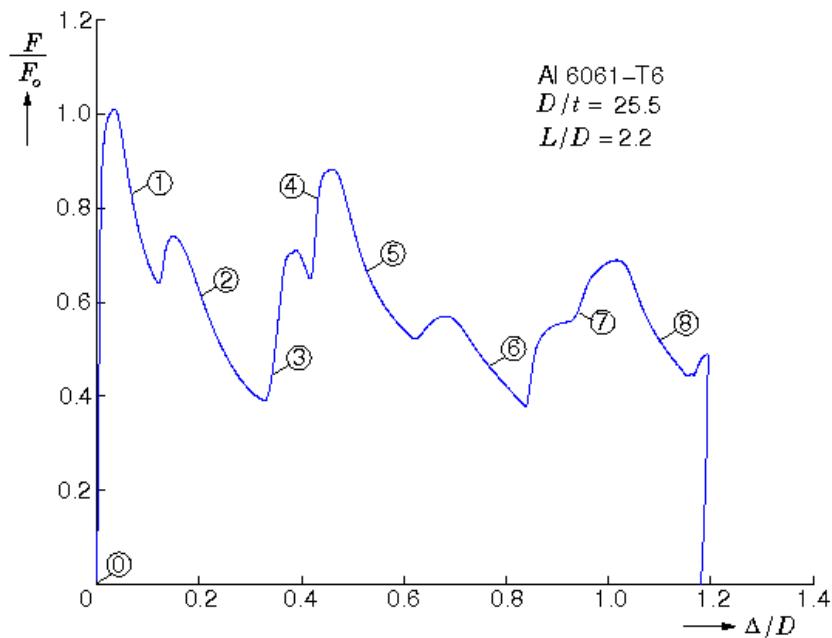


L/D = 2.2

Al 6061-T6
D/t = 25.5
L/D = 2.2



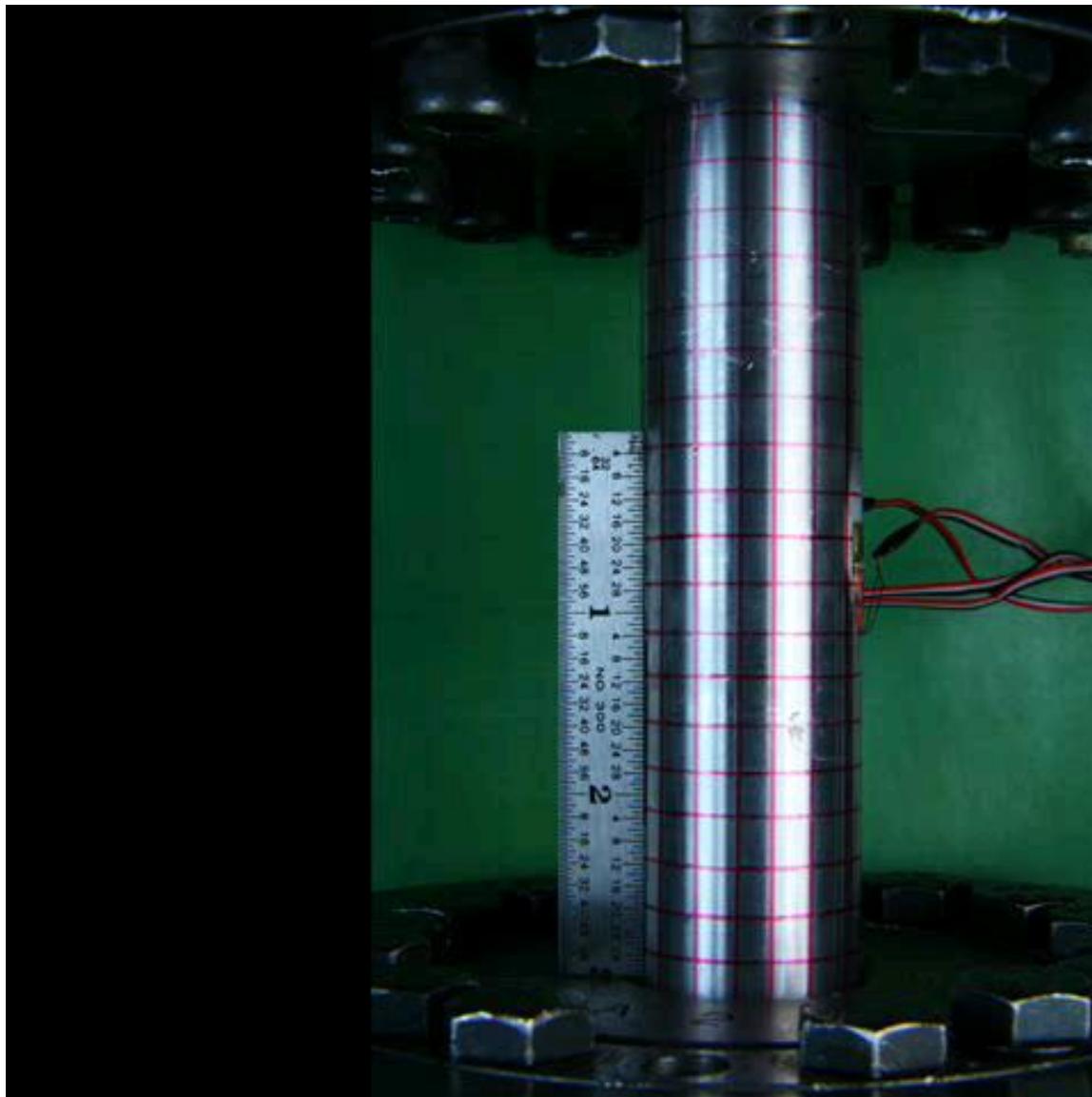
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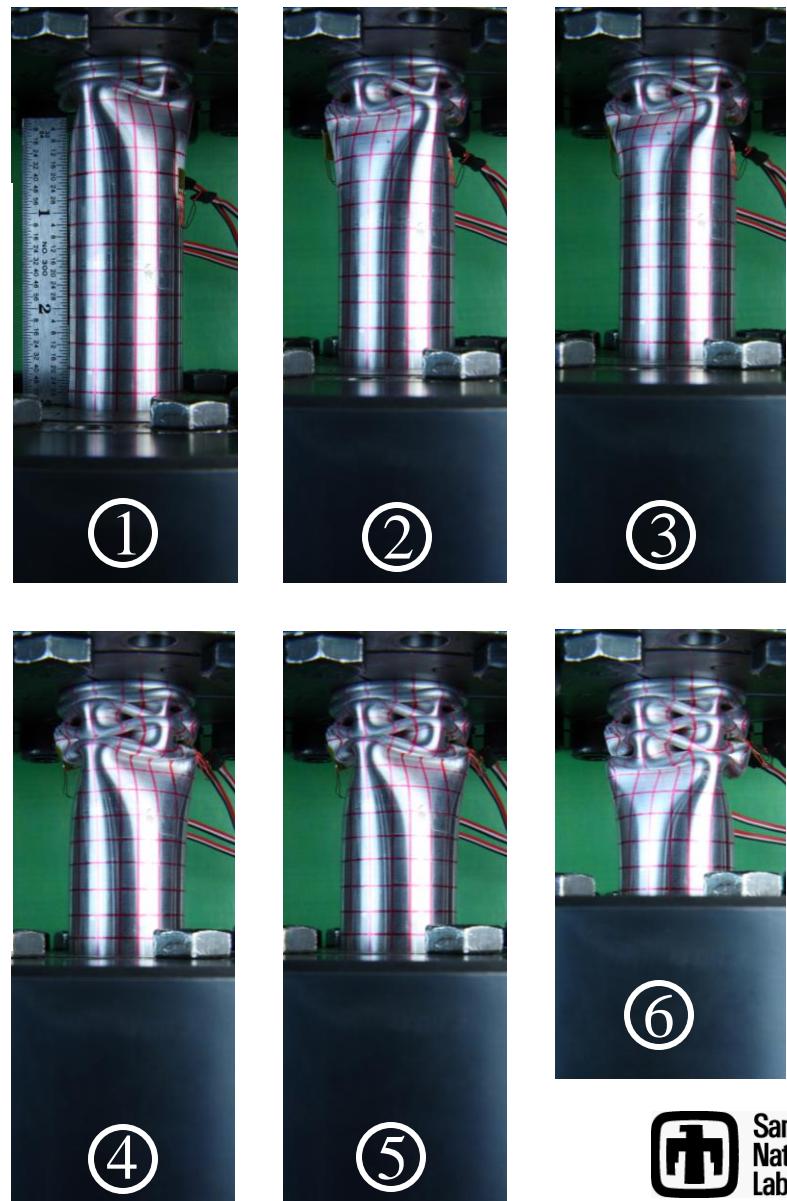
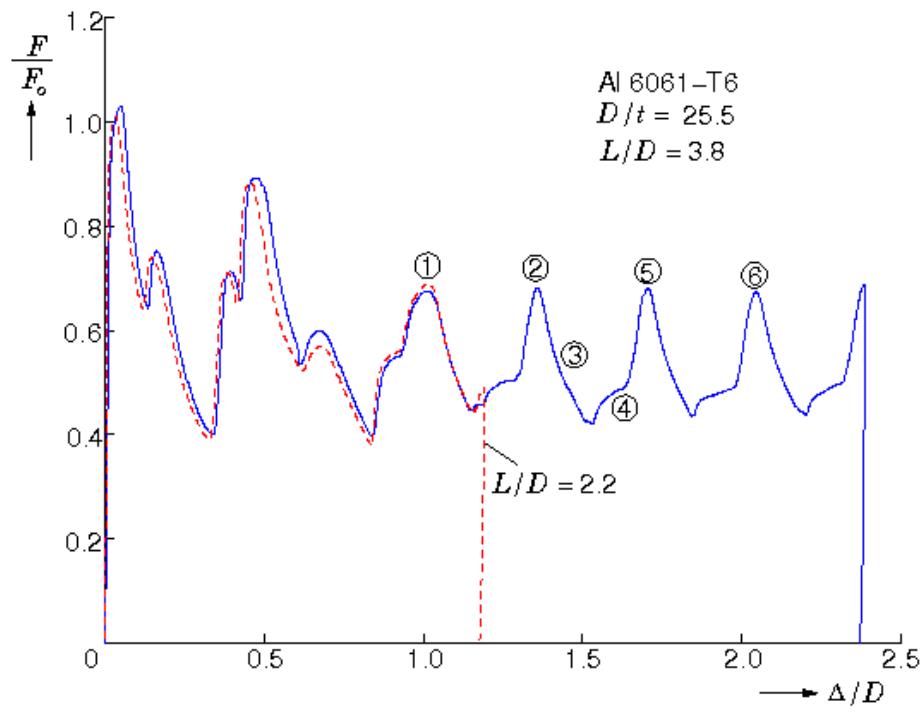


L/D = 3.8

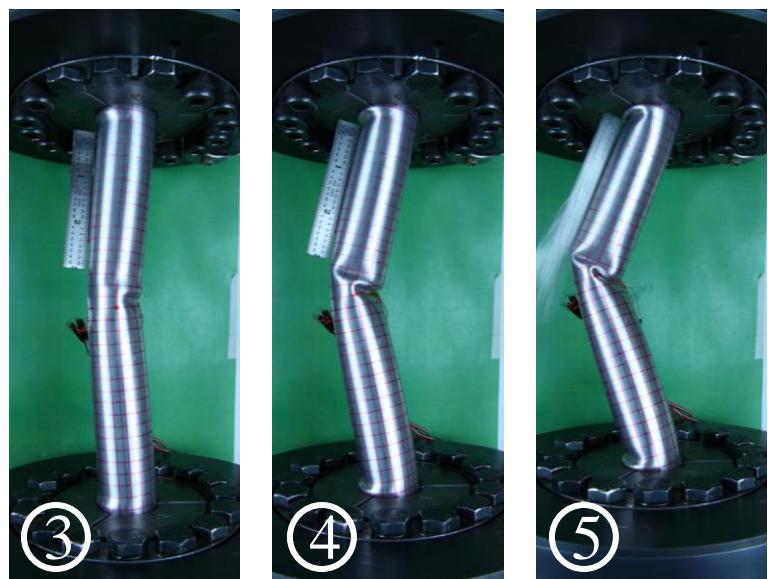
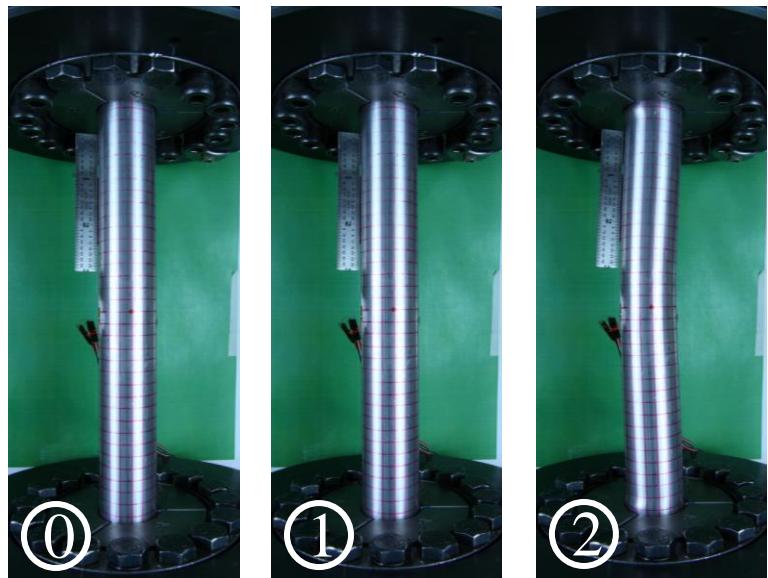
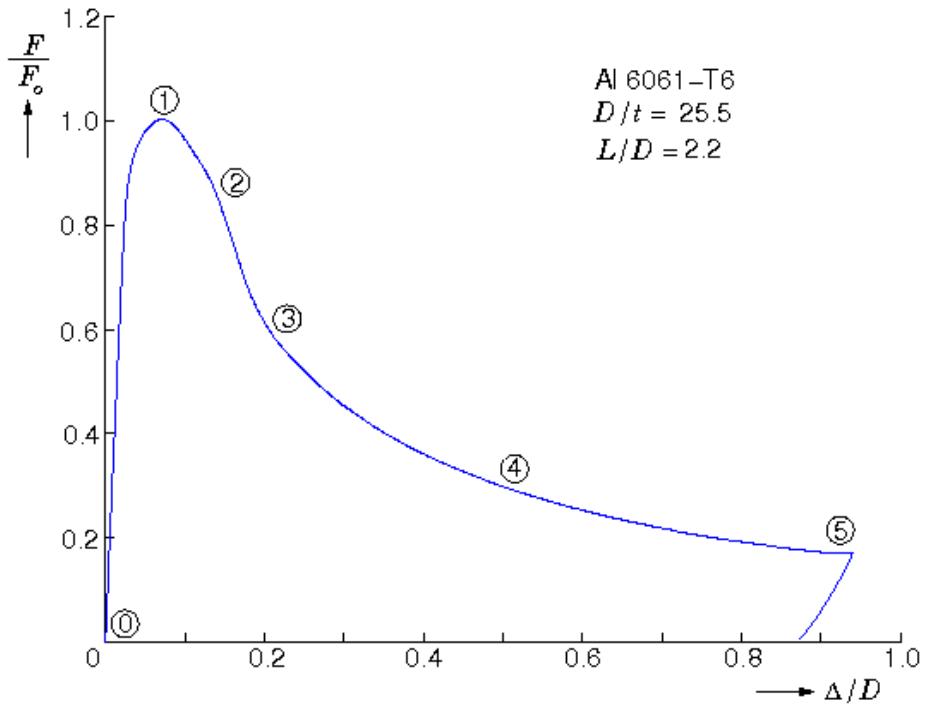
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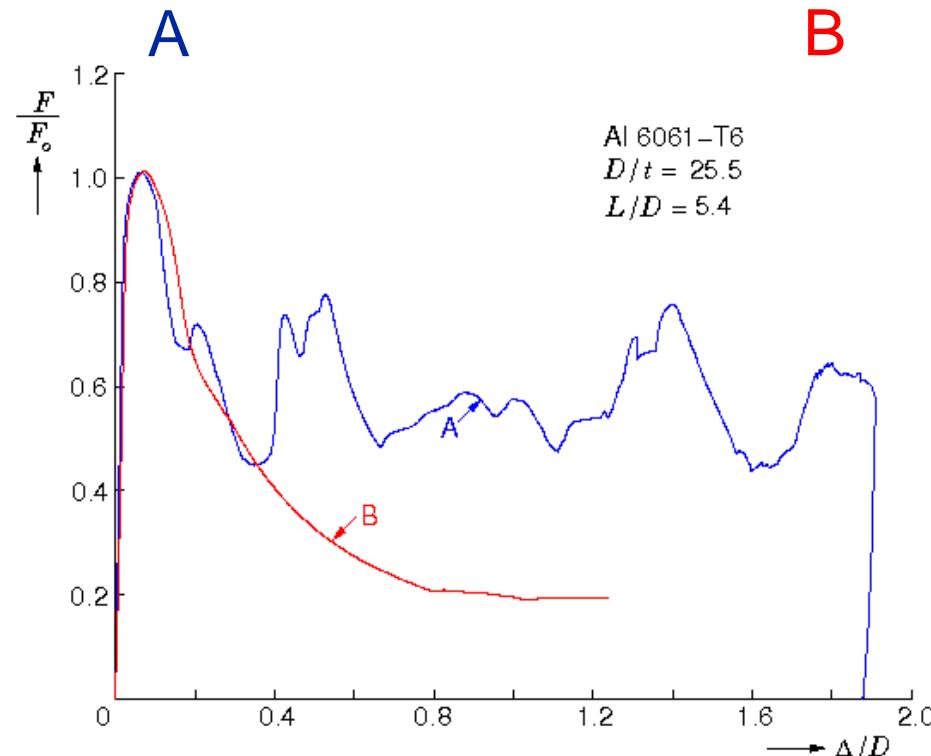
L/D = 3.8



L/D = 7.0



L/D = 5.4





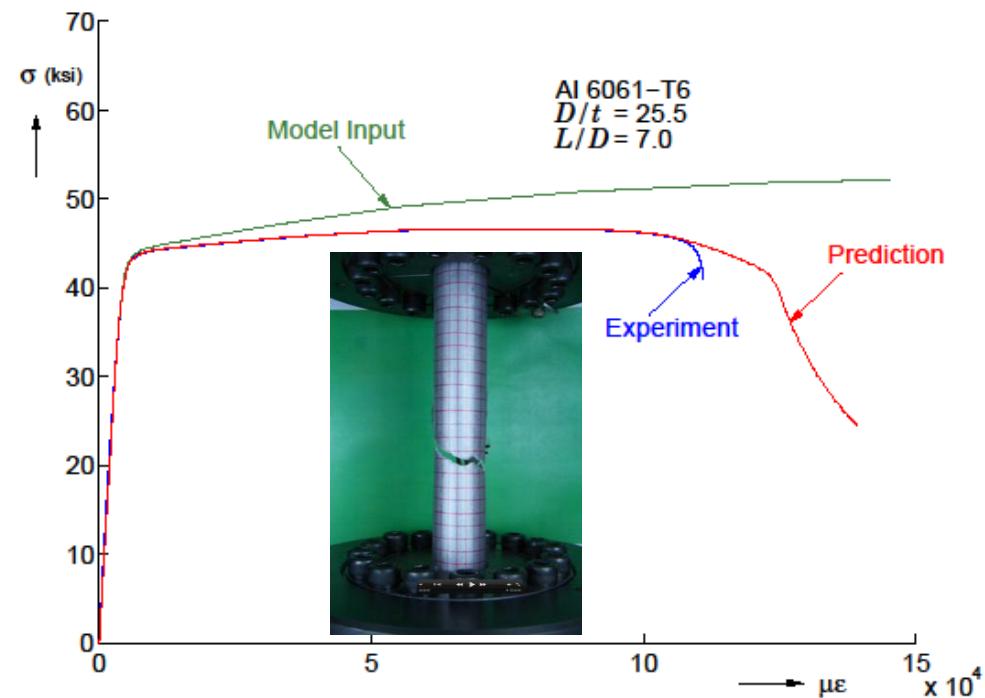
Modeling Overview

- Abaqus/Explicit
- Shell Elements on Tube
 - Reduced Integration (S4R)
 - Relax Stiffness Hourglass Control
- Rigid Fixtures
- Two Step Procedure
 - Clamping Pressure on Fixtures
 - Displacement on End
- Shell Contact Thickness
 - Set by Contact Algorithm
 - $\leq 42\%$ of Element Edge Length



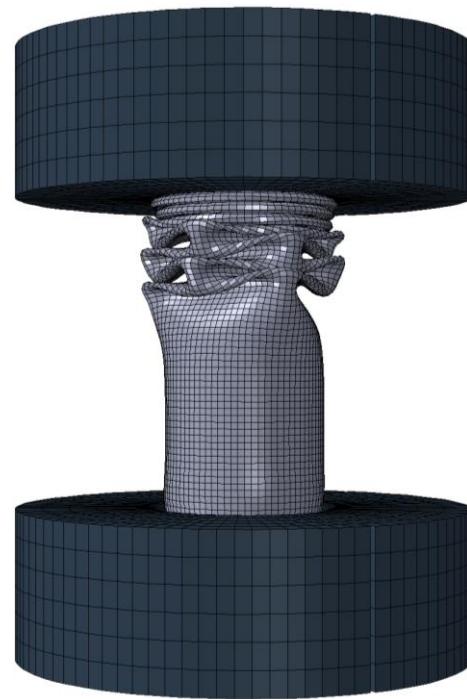
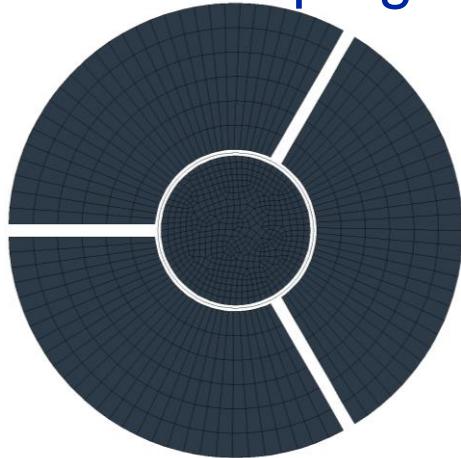
Material Properties

- **Tensile Test of Tube**
 - Pulled a Section from Same Tube
- **Material Model Input**
 - Up to UTS from Test
 - Iteratively Determined from UTS till Near Failure

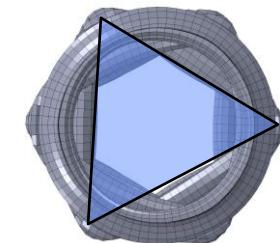


Crushing Pattern

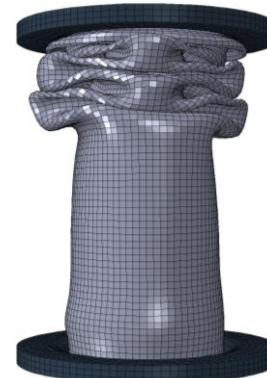
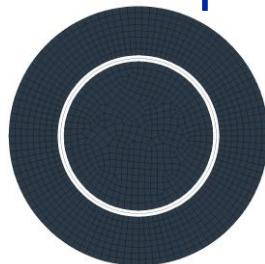
3 Piece Fixture
w/ Clamping



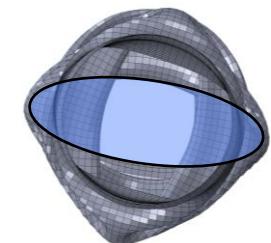
N=3



Continuous Fixture
No Clamping



N=2



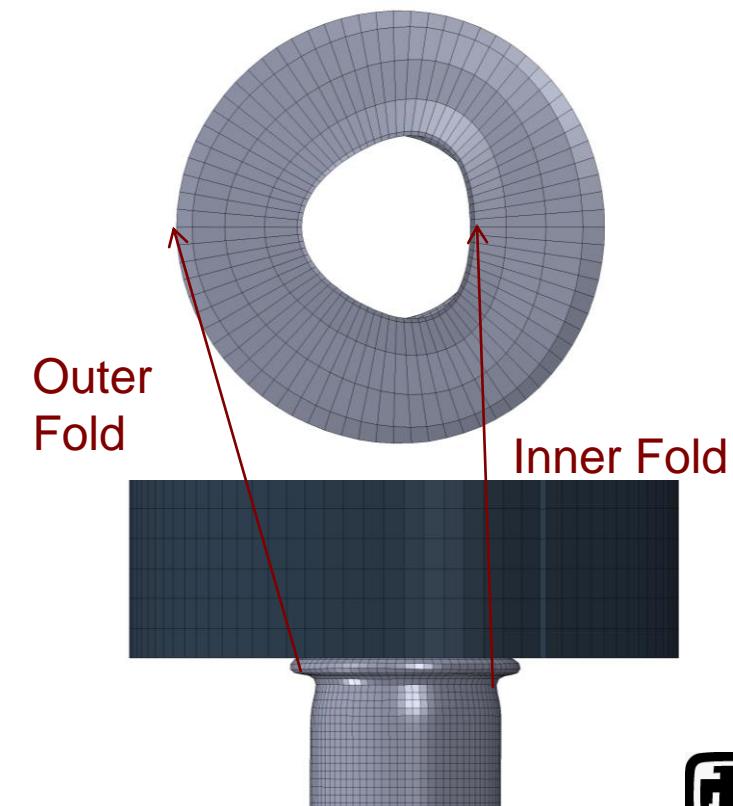


N = 3 Pattern

Tube End After
Clamping
(5x Displacement)

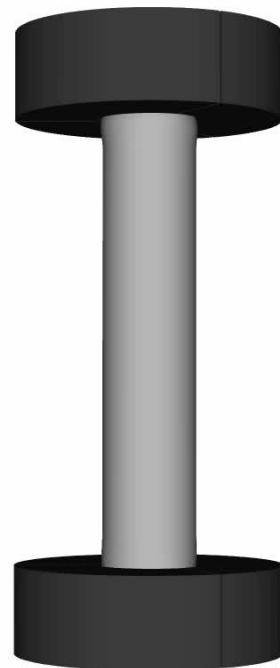


X-Section at First
Neck
(5x Displacement)

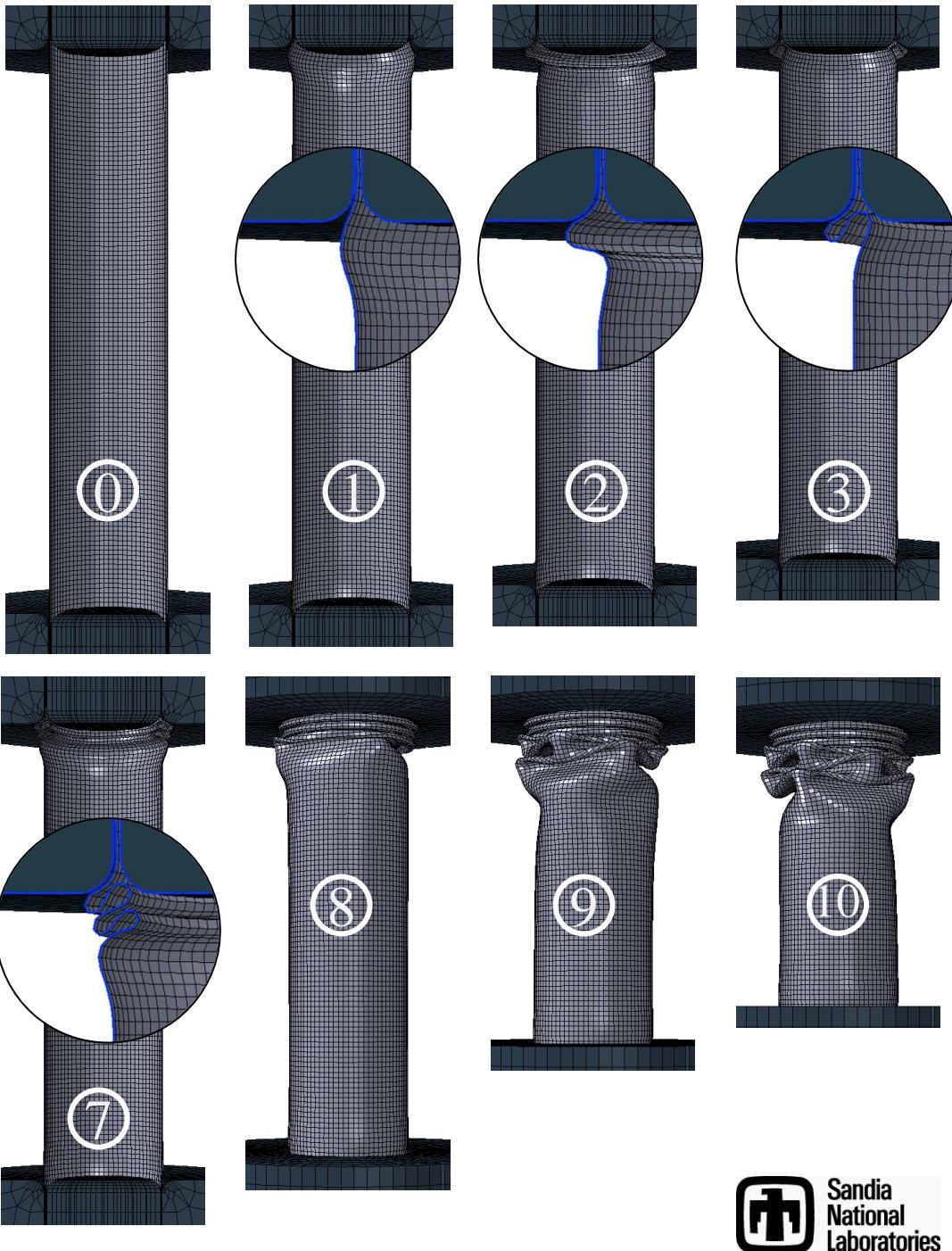
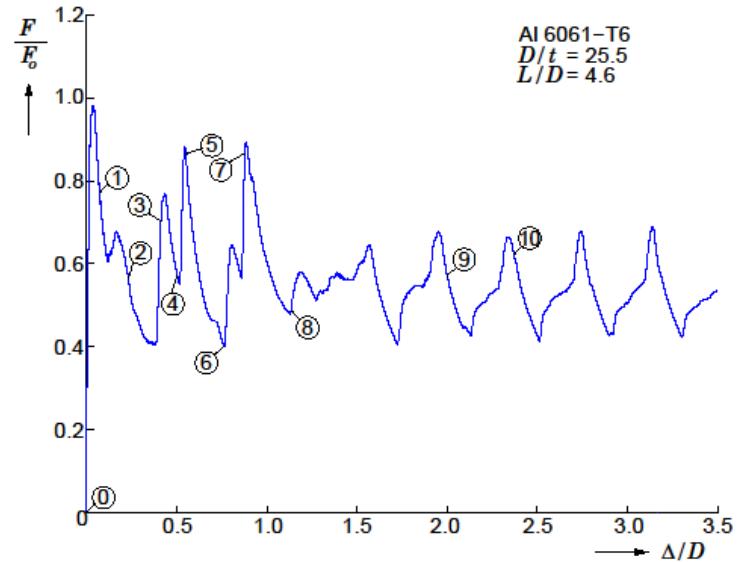




Crushing Prediction L/D=4.6



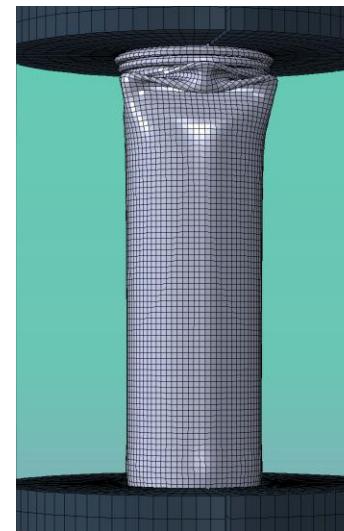
L/D = 4.6



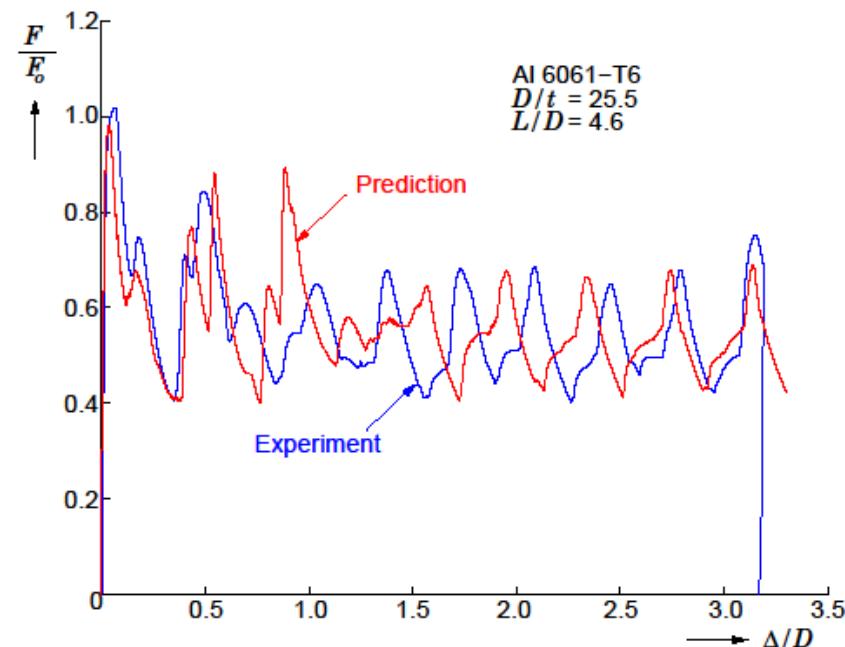
L/D = 4.6



Experiment



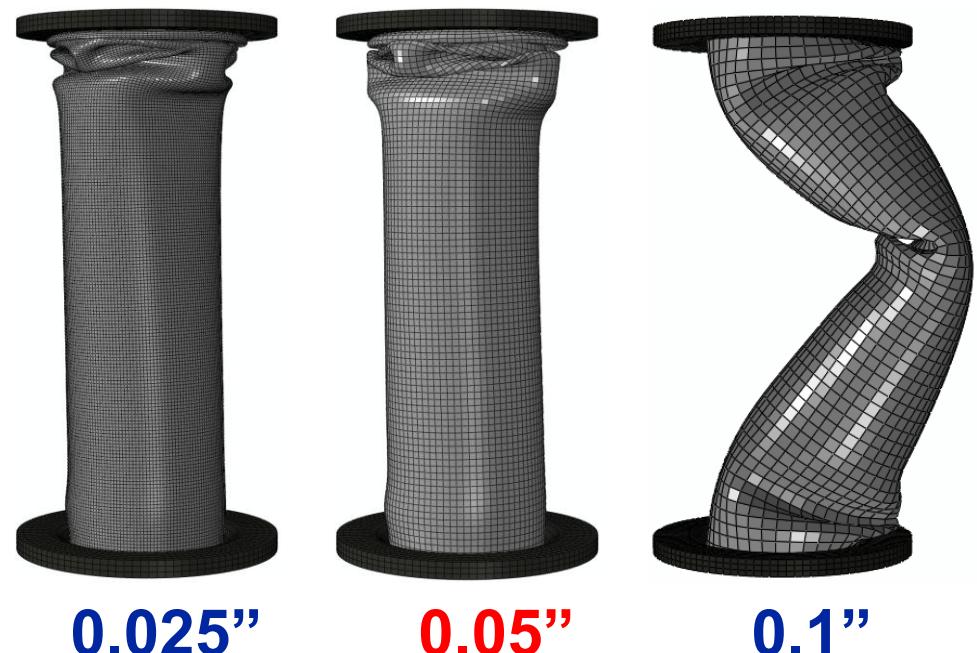
Prediction





Sensitivity Investigations

- Mesh Sensitivity
 - 0.025, 0.05, 0.1 inch squares studied
- Other Studies
 - Clamping Pressure
 - Fixture Dimensions
- Future Studies
 - Hex-Based Meshes



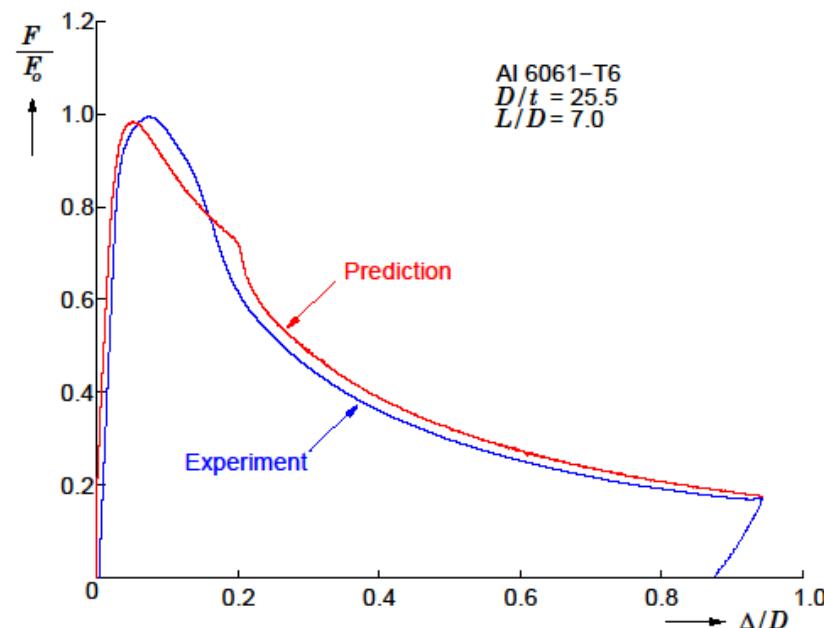
L/D = 7



Experiment



Prediction





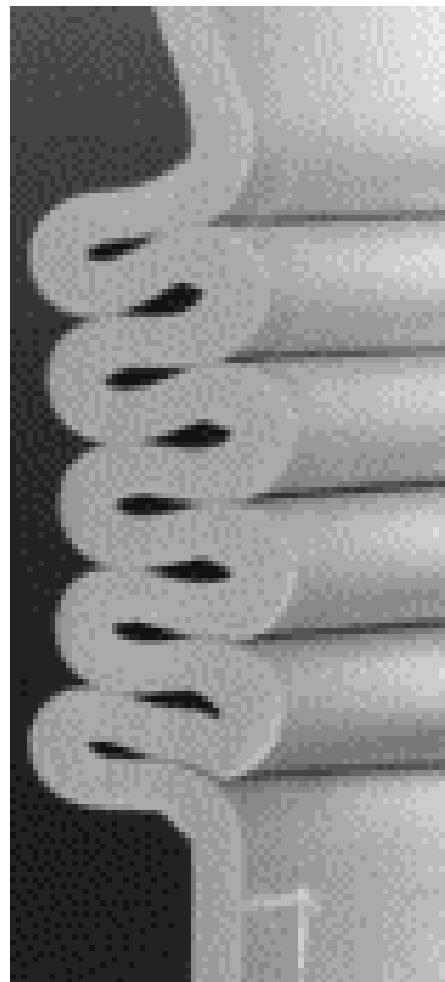
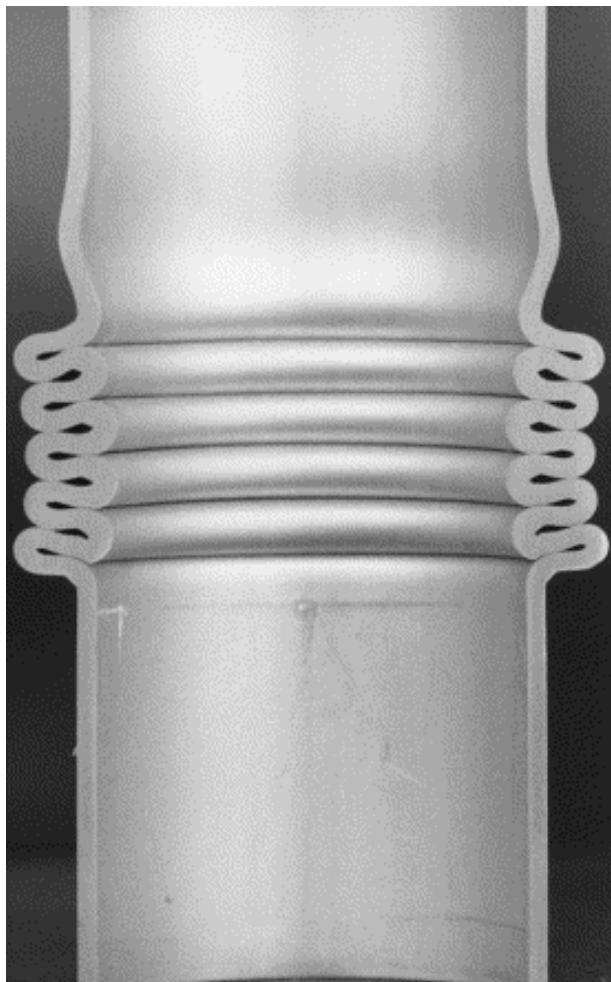
Summary of Results

L/D	Mode Experiment	Mode Prediction	$\lambda (\Delta/D)$ Experiment	$\lambda (\Delta/D)$ Prediction
2.2	N=3 / N=3	N=3	-	-
3.8	N=3 / N=2-3 (t)	N=3	0.352	0.388
4.6	N=3 / N=2-3 (t)	N=3	0.354	0.394
5.4	N=3 (t)/ Lateral	N=3	-	0.395
7.0	Lateral / Lateral	Lateral	-	-



Axisymmetry?

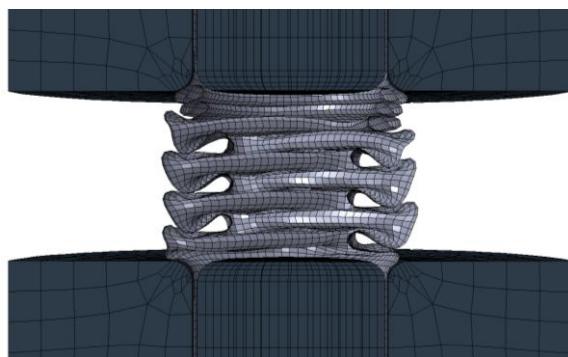
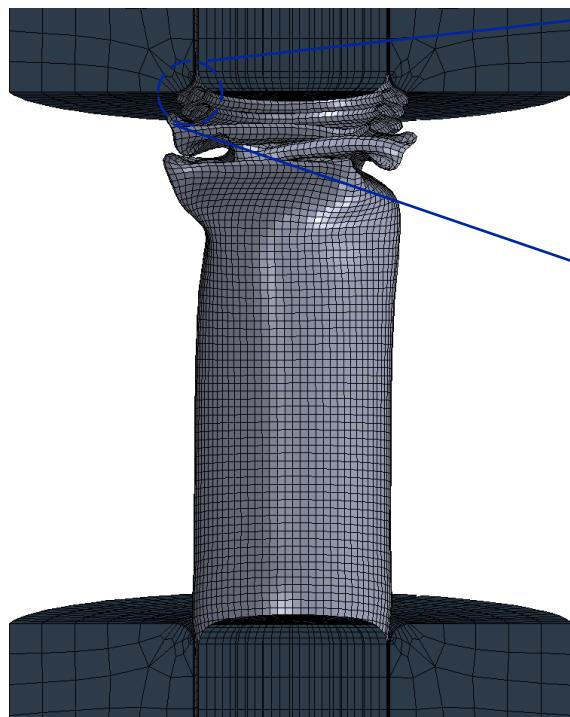
Bardi et al



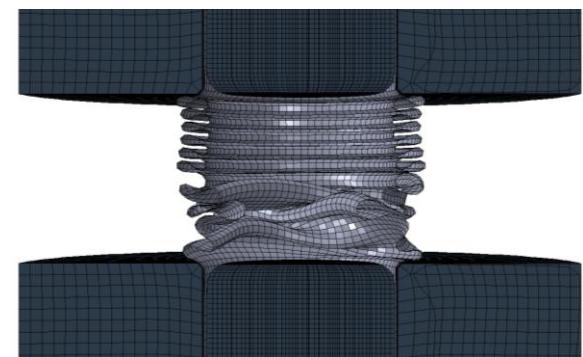
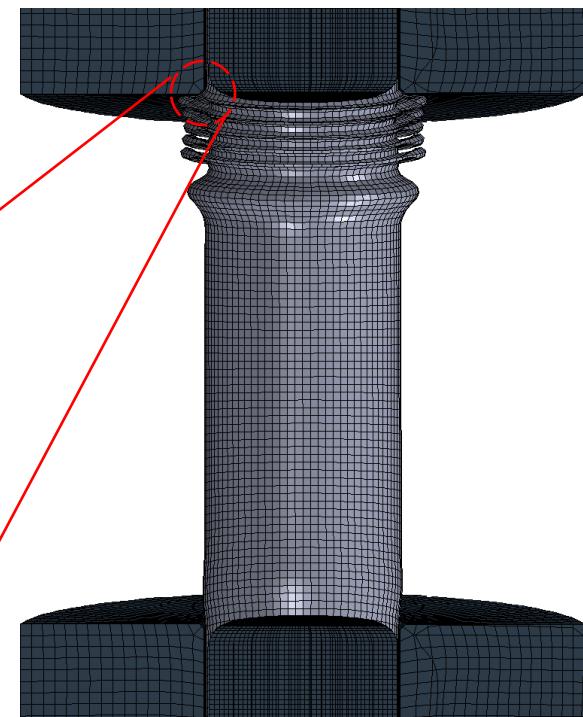


Boundary Effects

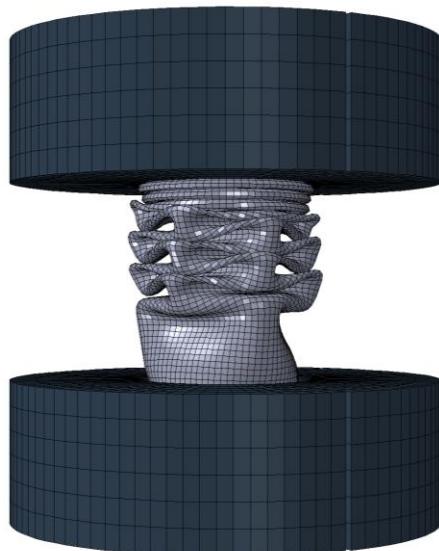
Fillet



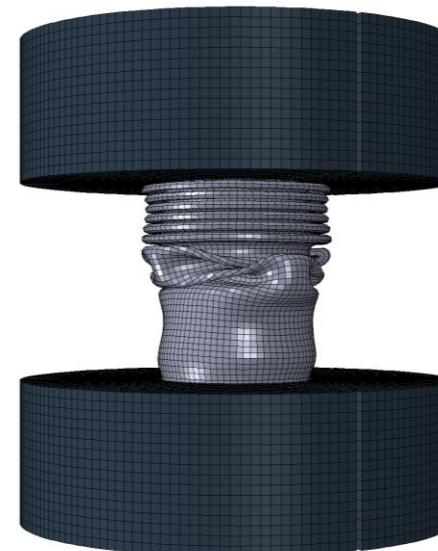
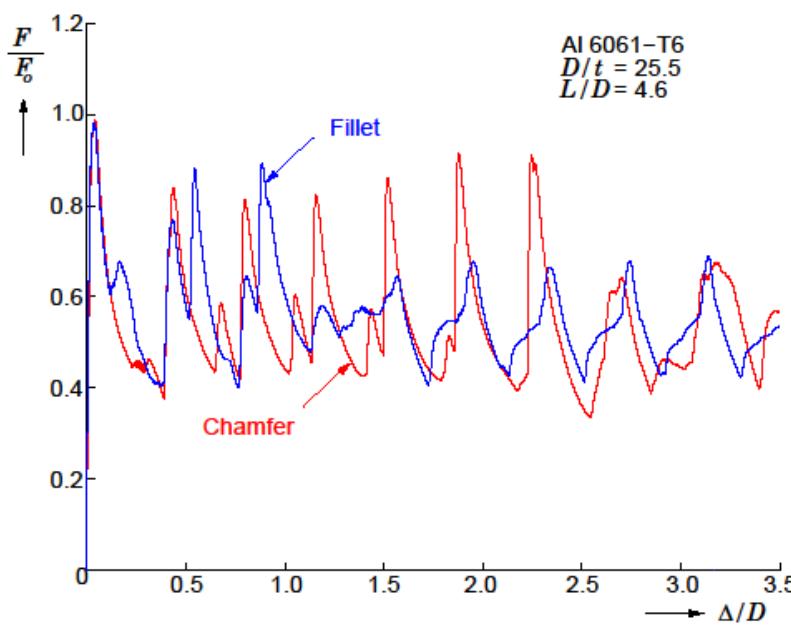
Chamfer



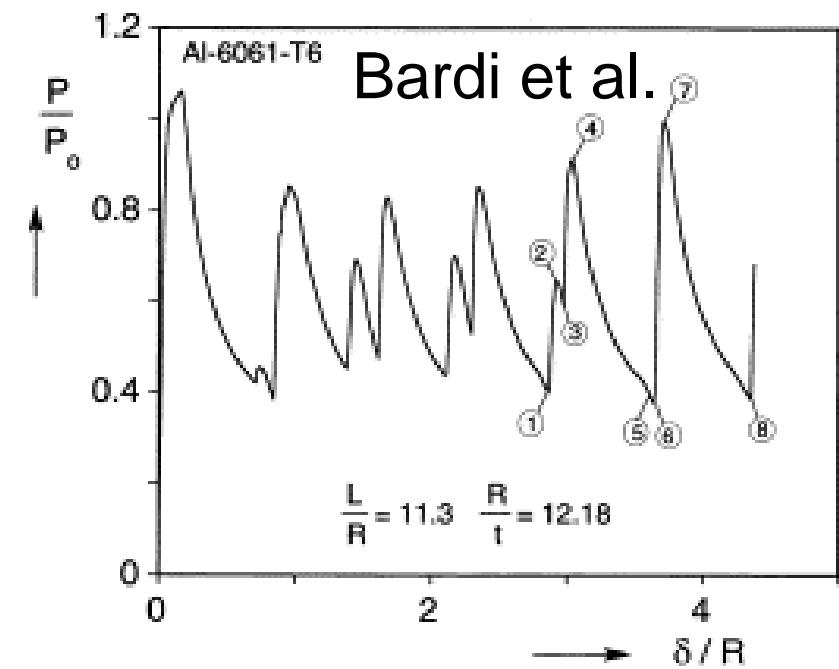
Boundary Effects



Fillet



Chamfer





Conclusions

- Shell model does a reasonable job in predicting the crushing response of the tubes.
- N=3 crushing mode seems to be a consequence of the three-segmented clamping fixture and of the applied clamping pressure.
- Shell contact thickness is a model feature that probably affects the numerical results.
- Crushing mode is influenced by the geometric details of the clamping fixture. Perhaps more generally, by the geometry of preceding folds.

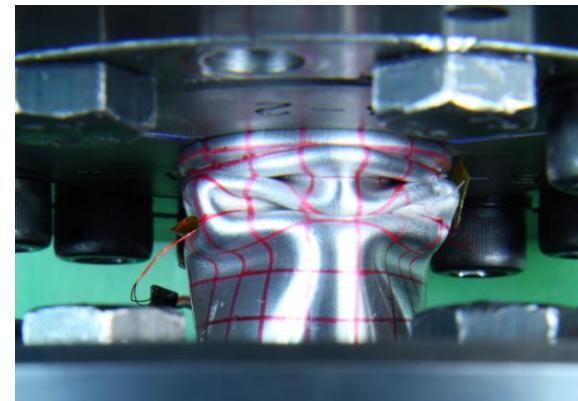
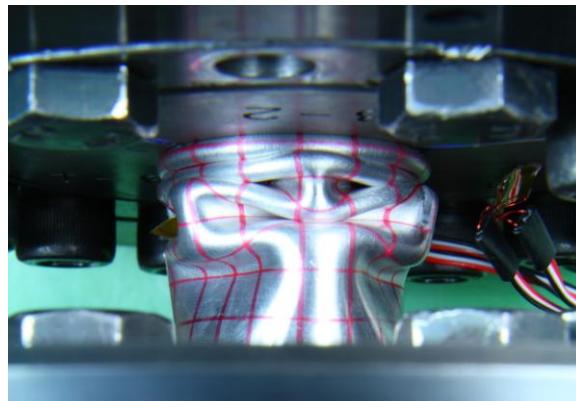


Parametric Study

Clamping Pressure (PSI)	Plug Size (inches)	Mesh (inches)	Result
1250	1.15	0.05	N=3
1250	1.147	0.05	N=2
1250	1.15	0.025	N=2
2500	1.15	0.05	N=3
2500	1.147	0.05	N=3
12500	1.15	0.05	N=3
12500	1.15	0.025	N=3
12500	1.147	0.05	N=3
6250	1.15	0.025	N=3

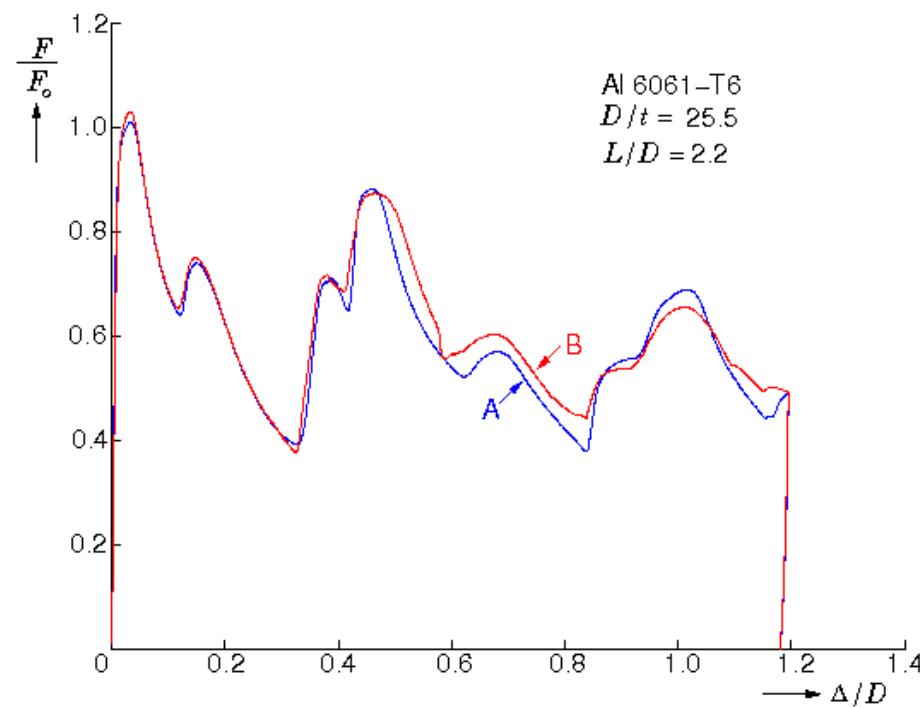


L/D = 2.2



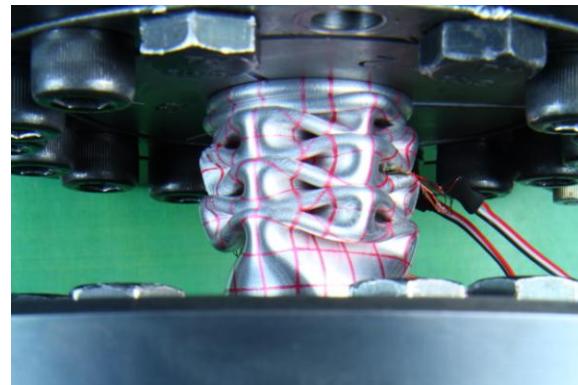
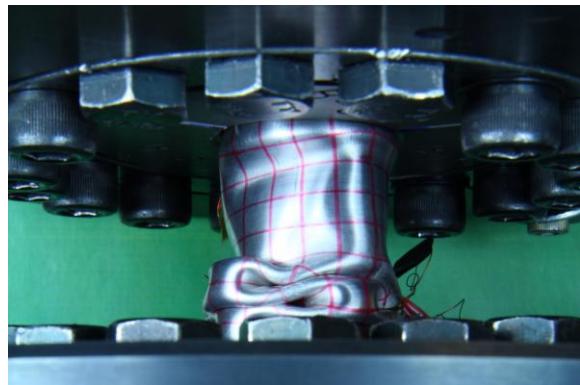
A

B



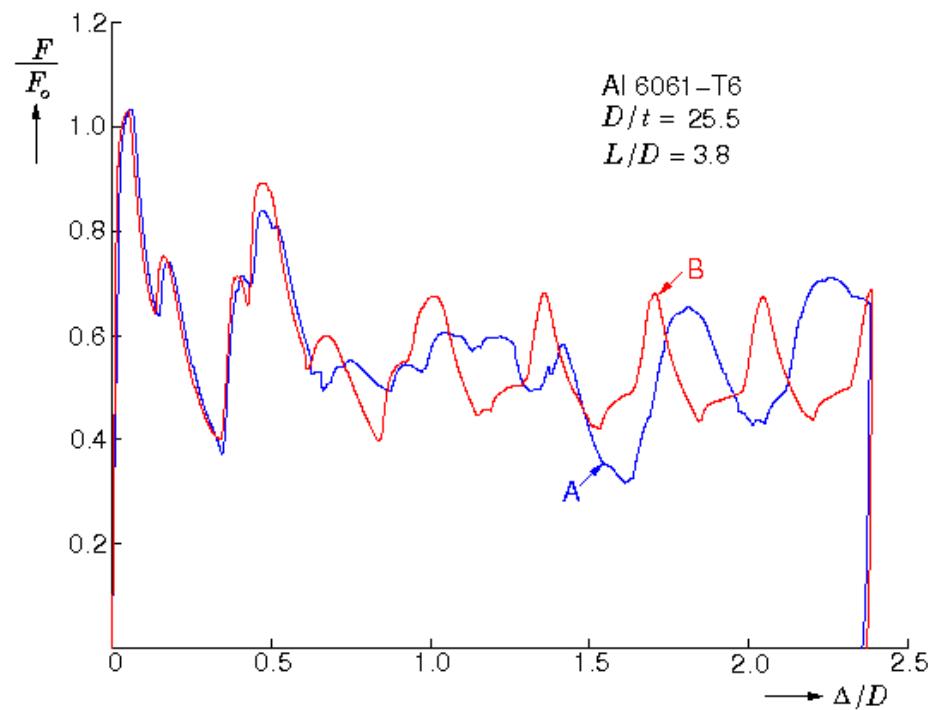


L/D = 3.8



A

B





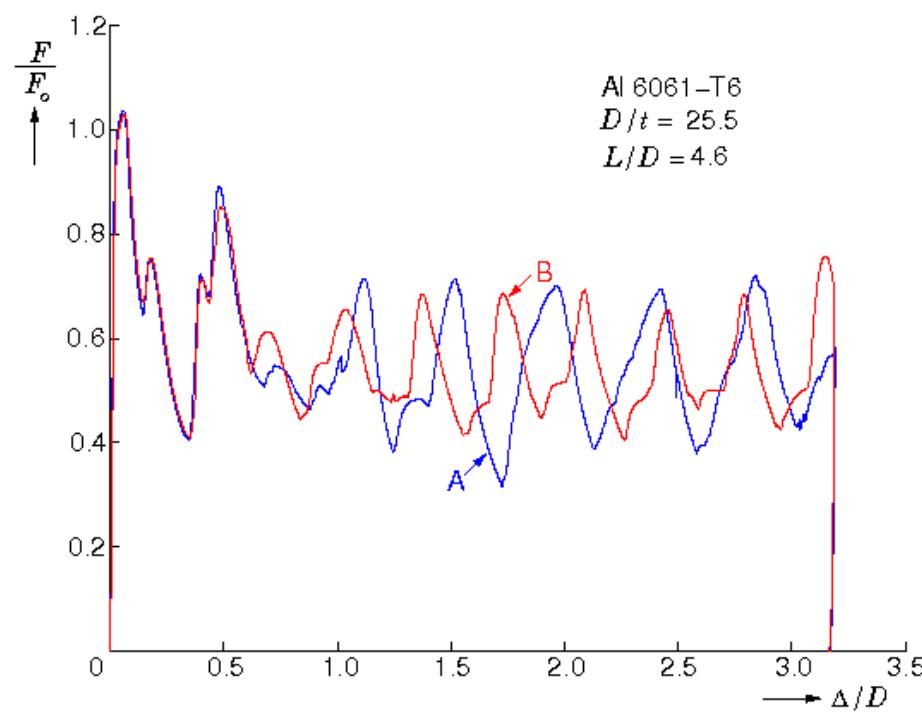
L/D = 4.6



A

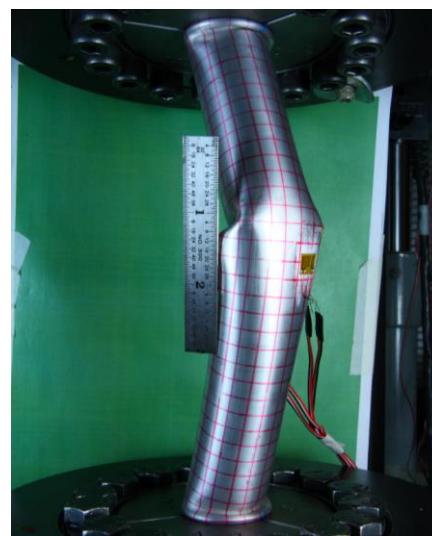


B





L/D = 7



A

B

