

# **Axial Crushing of Aluminum Tubes**

## **Experimental Results and Finite Element Modeling**

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# Introduction

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- **Many Sandia-designed systems may be subjected to severe mechanical environments. Performance issues require analysis of system response under these conditions.**
- **System and component level finite element models are widely used to perform a substantial part of the analysis and to guide testing.**
- **Validation of FE modeling capabilities by comparison to experiment is an essential part of the process.**

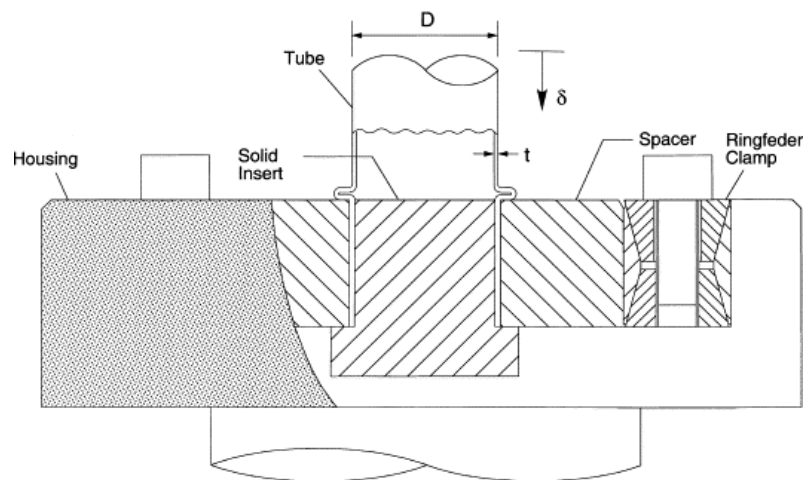
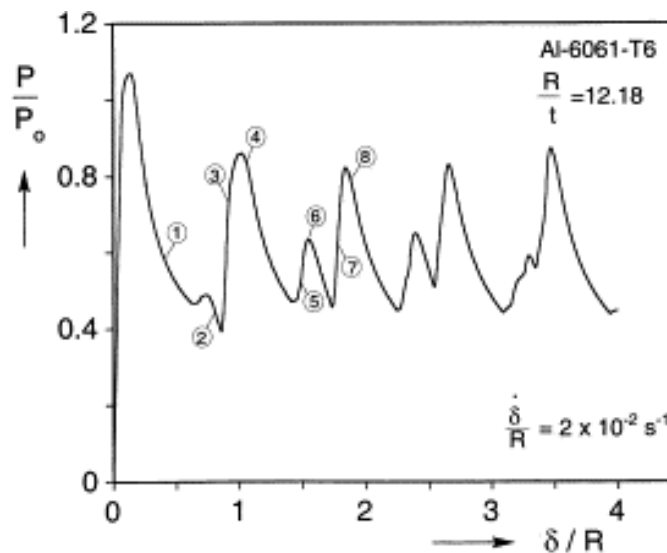
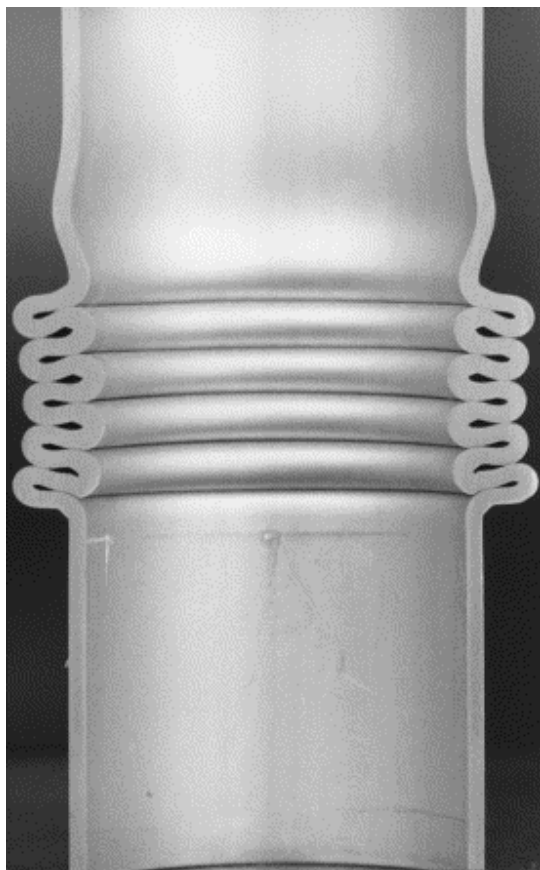


# Objectives

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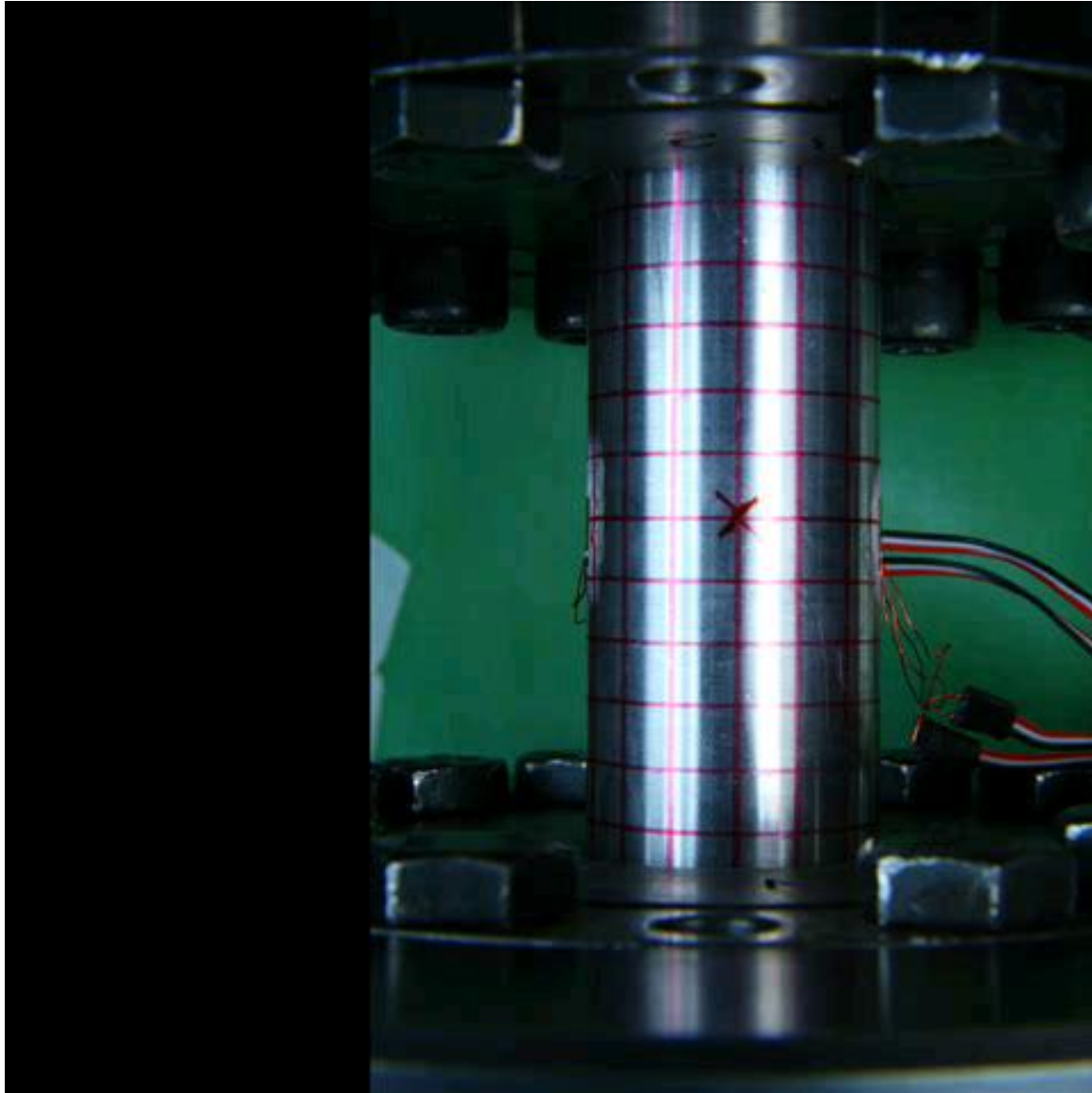
- **Demonstrate the performance of FE nonlinear structural models to simulate crushing and other large-deflection scenarios.**
- **Examples:**
  - **Crushing of tubular structures**
  - **Hydraulic collapse**
  - **Puncturing**
  - **Etc.**
- **This presentation addresses aluminum tubes crushed by quasi-static axial compression.**

# Axisymmetric Collapse (Bardi et al, 2003)

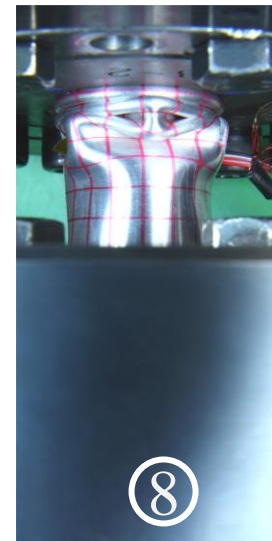
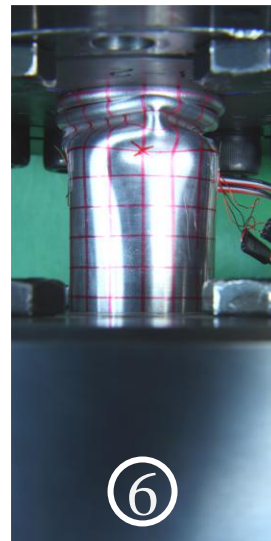
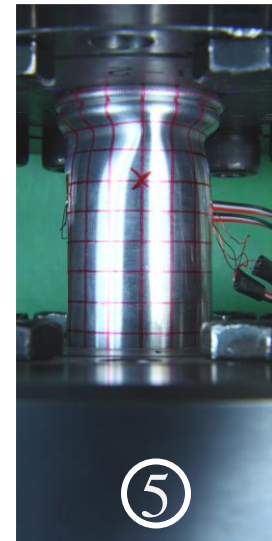
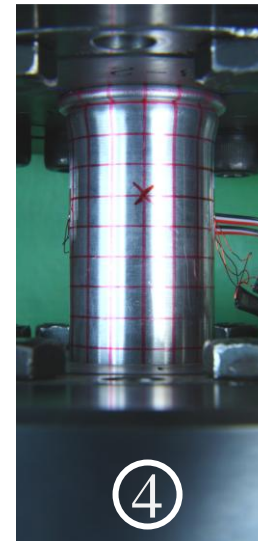
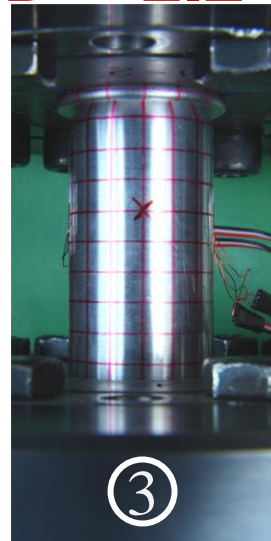
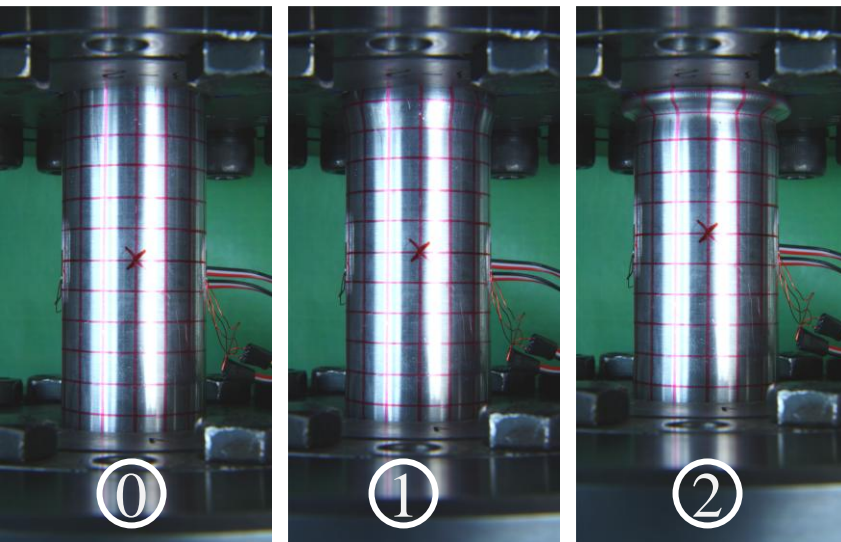
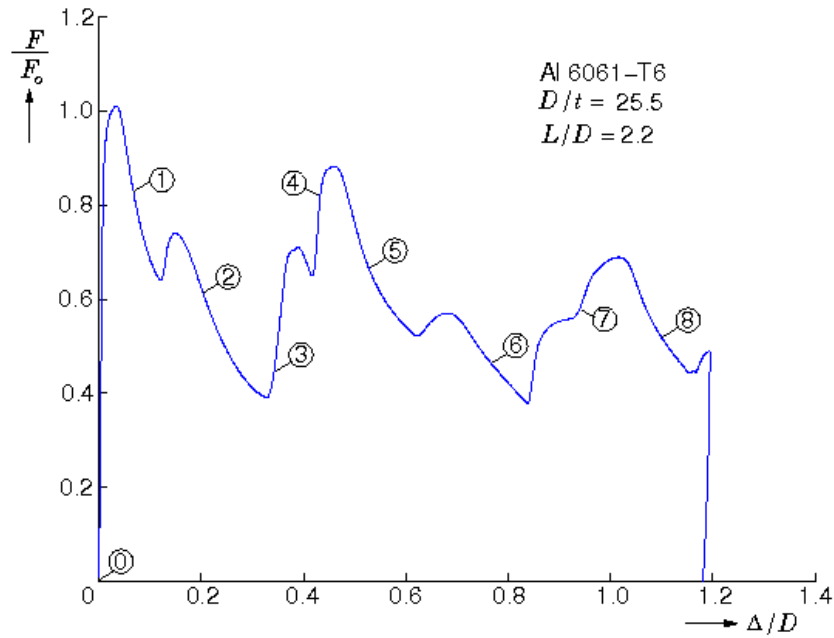


**$L/D = 2.2$**

Al 6061-T6  
 $D/t = 25.5$   
 $L/D = 2.2$



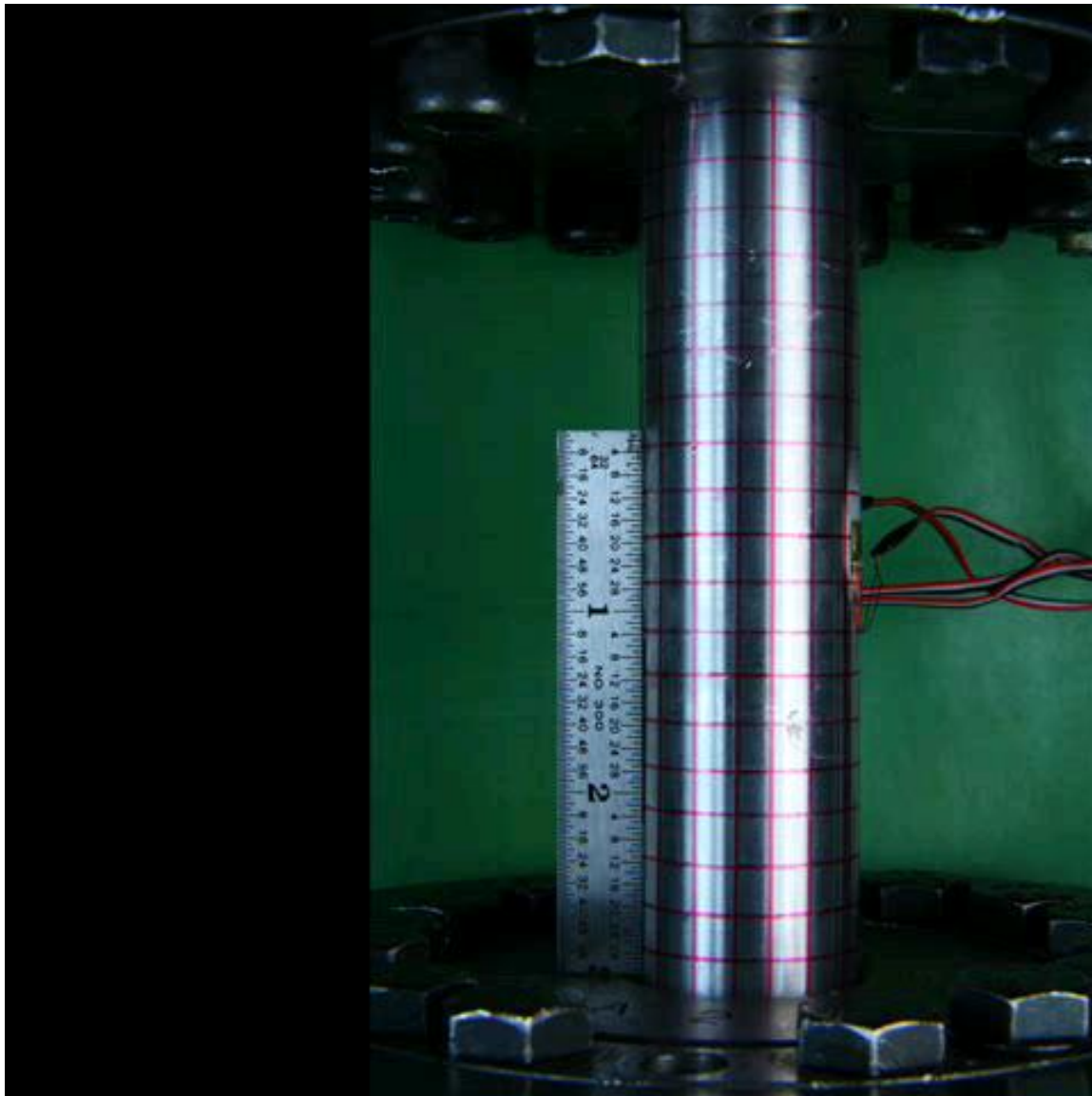
**$L/D = 2.2$**



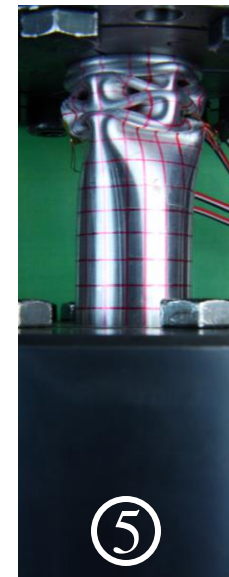
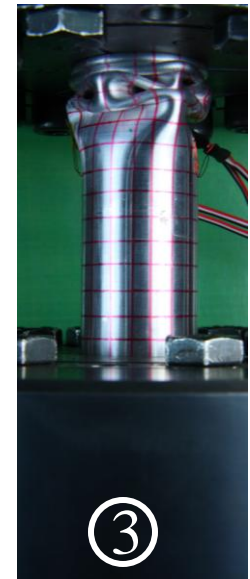
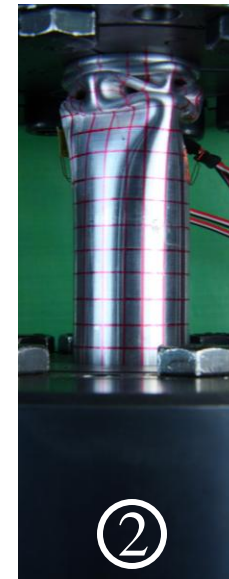
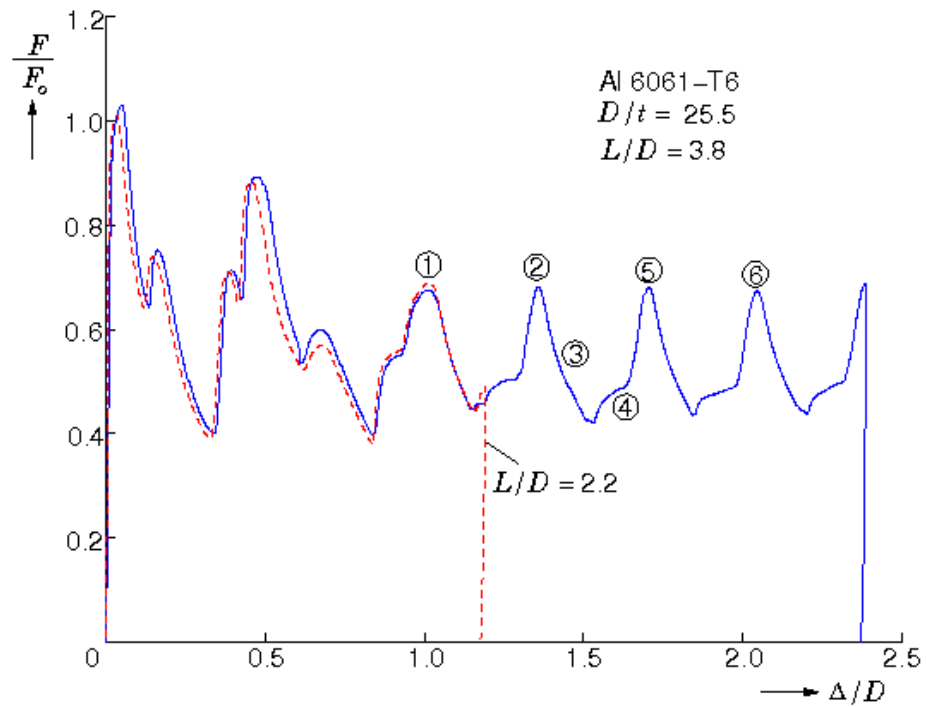


$L/D = 3.8$

Al 6061-T6  
 $D/t = 25.5$   
 $L/D = 3.8$

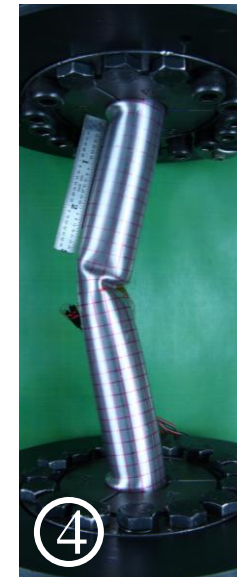
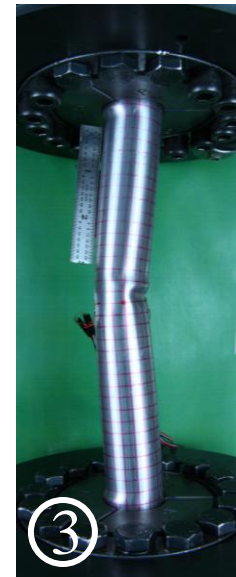
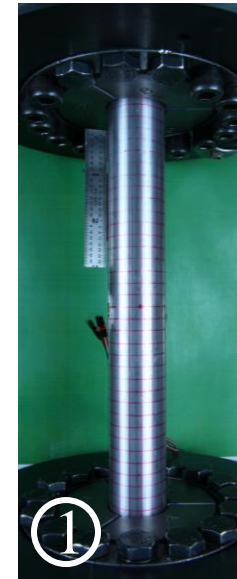
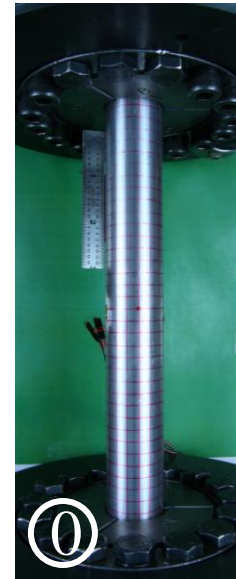
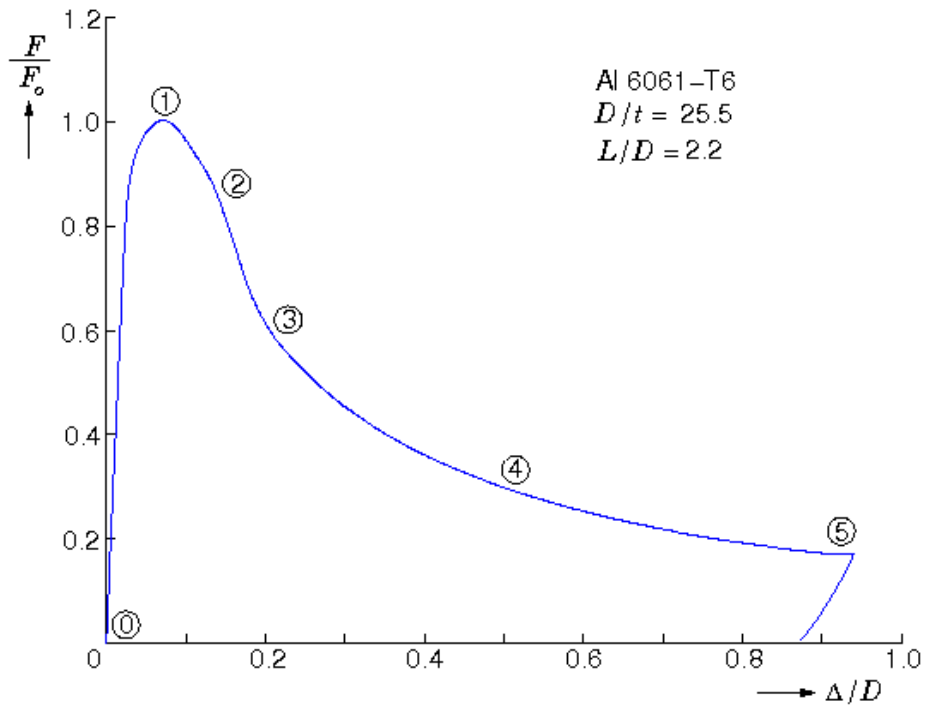


**$L/D = 3.8$**

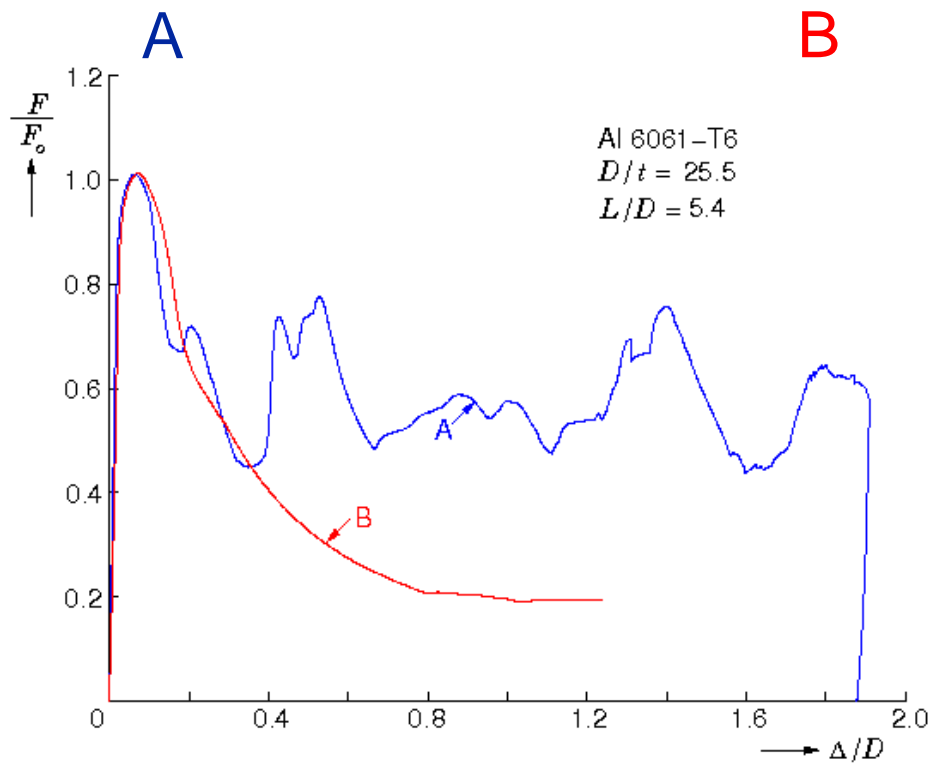
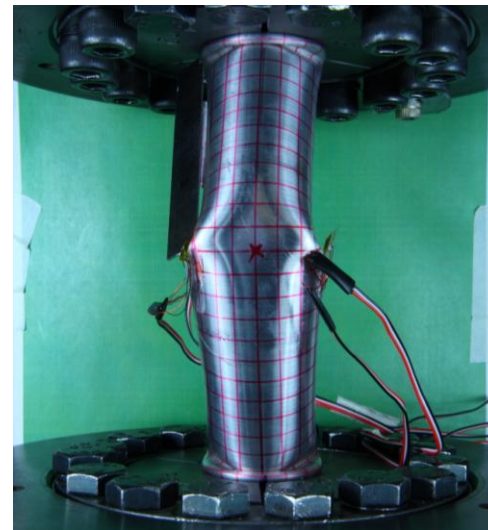




# L/D = 7.0

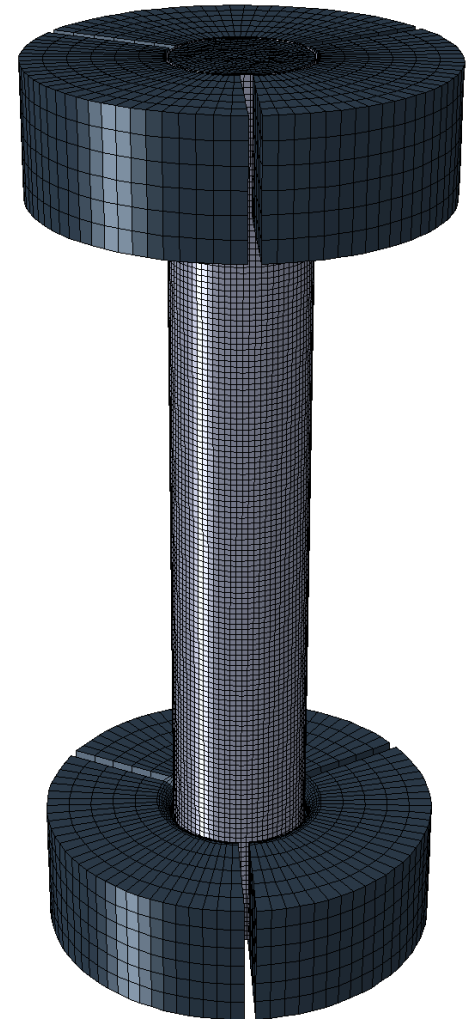


**$L/D = 5.4$**



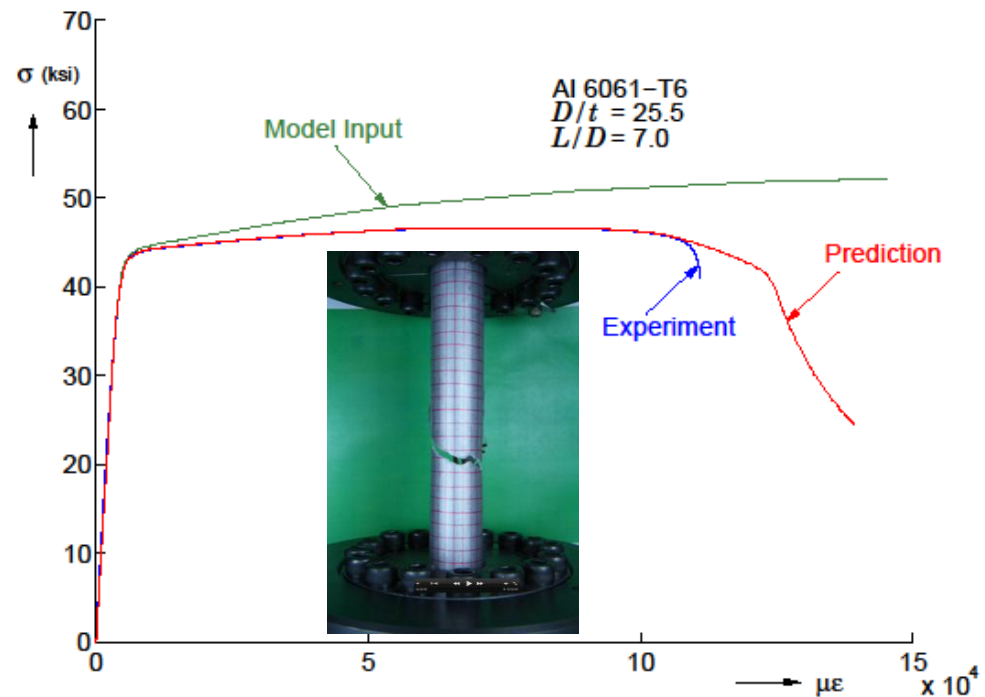
# Modeling Overview

- **Abaqus/Explicit**
- **Shell Elements on Tube**
  - Reduced Integration (S4R)
  - Relax Stiffness Hourglass Control
- **Rigid Fixtures**
- **Two Step Procedure**
  - Clamping Pressure on Fixtures
  - Displacement on End
- **Shell Contact Thickness**
  - Set by Contact Algorithm
  - $\leq 42\%$  of Element Edge Length



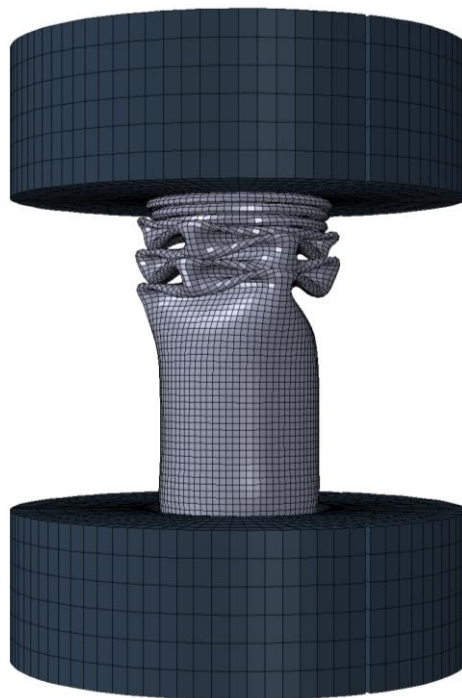
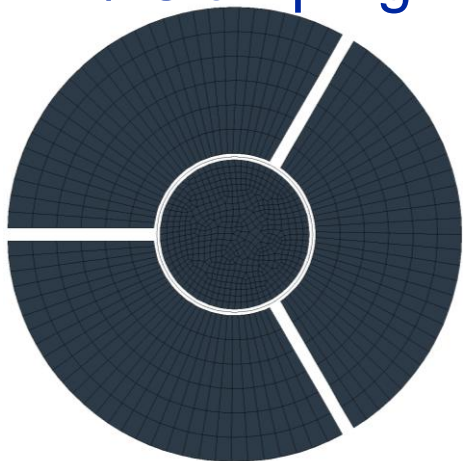
# Material Properties

- Tensile Test of Tube
  - Pulled a Section from Same Tube
- Material Model Input
  - Up to UTS from Test
  - Iteratively Determined from UTS till Near Failure

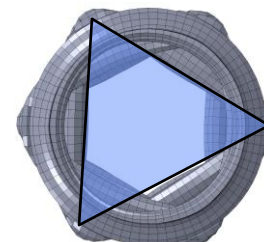


# Crushing Pattern

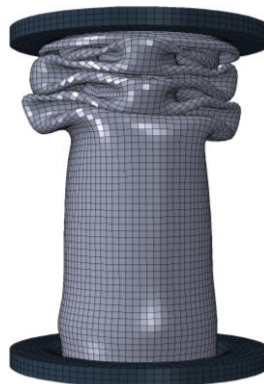
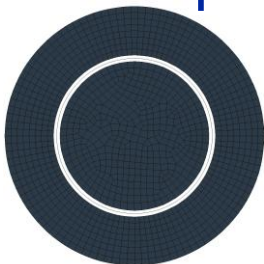
3 Piece Fixture  
w/ Clamping



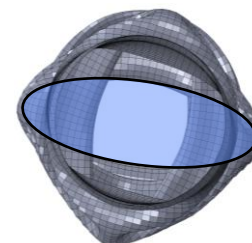
$N=3$



Continuous Fixture  
No Clamping



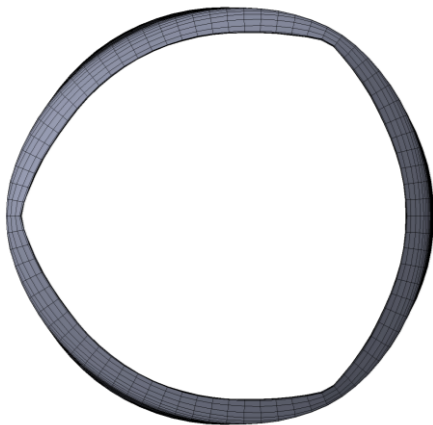
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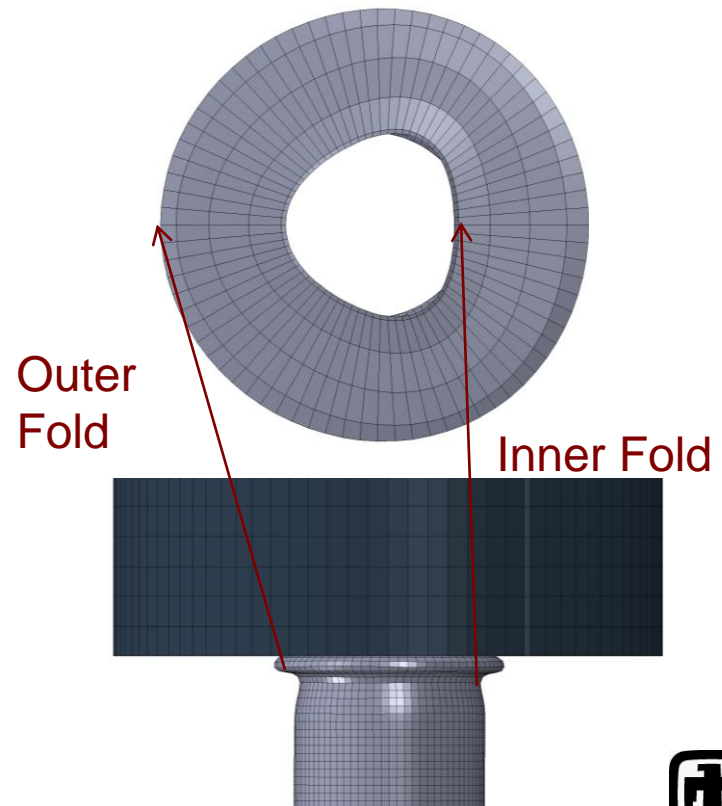


# N = 3 Pattern

Tube End After  
Clamping  
(5x Displacement)



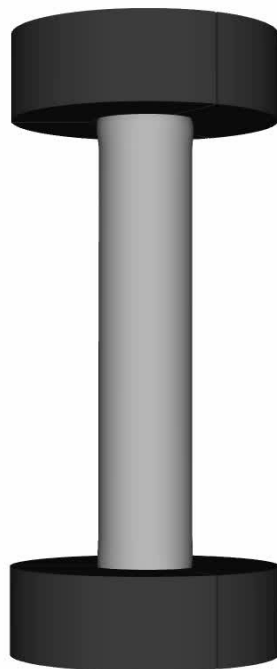
X-Section at First  
Neck  
(5x Displacement)



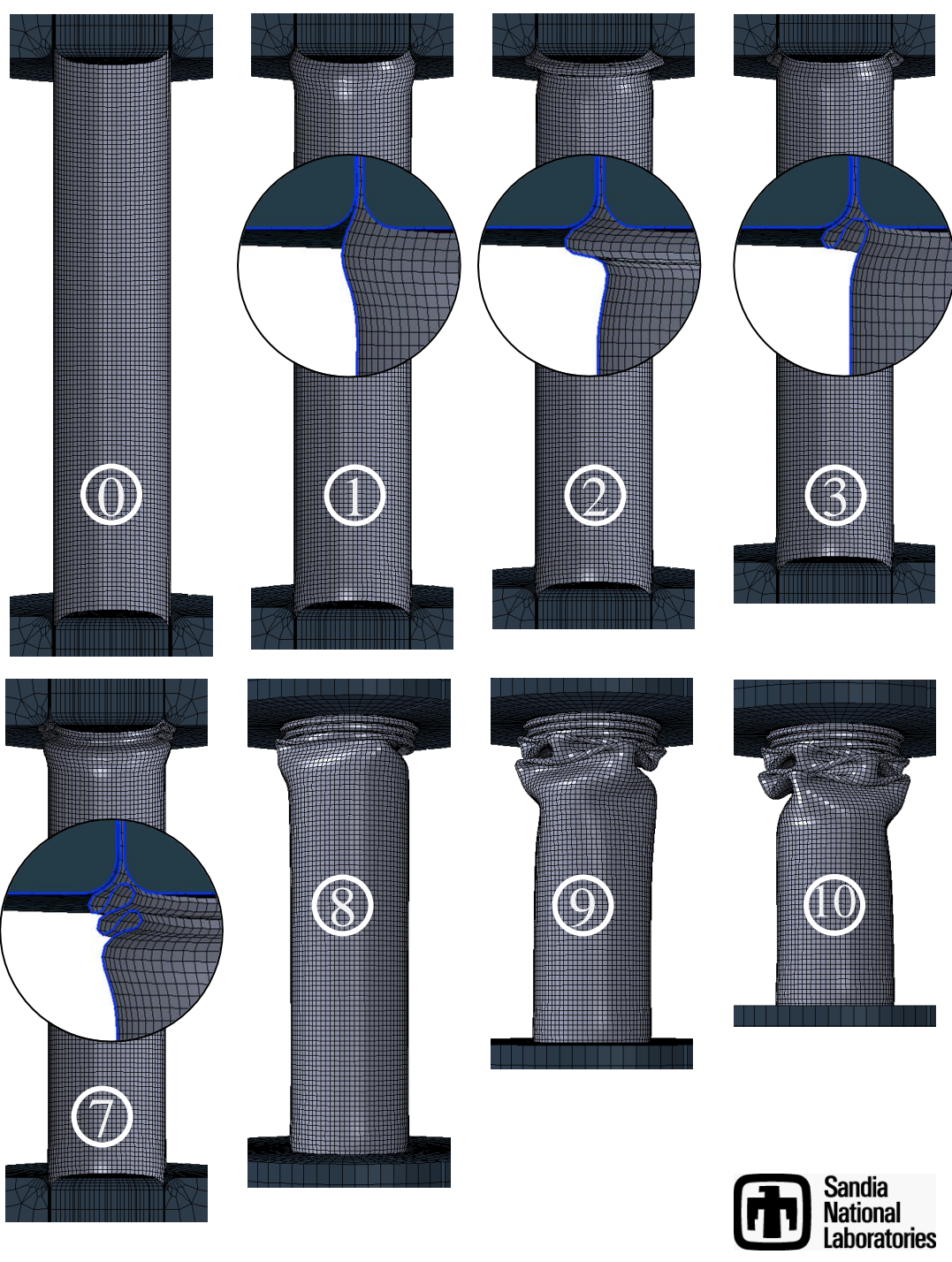
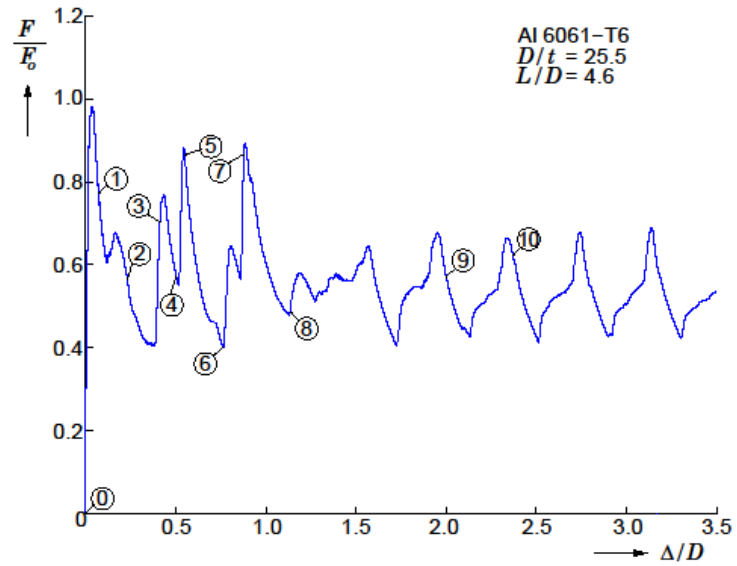


## Crushing Prediction $L/D=4.6$

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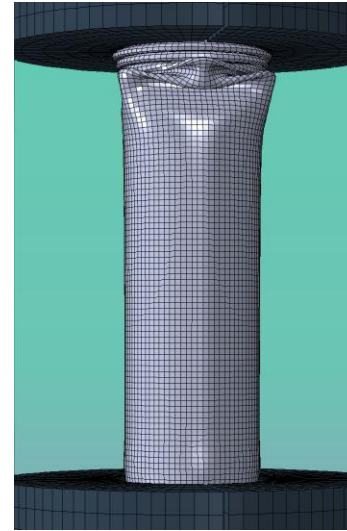
# $L/D = 4.6$



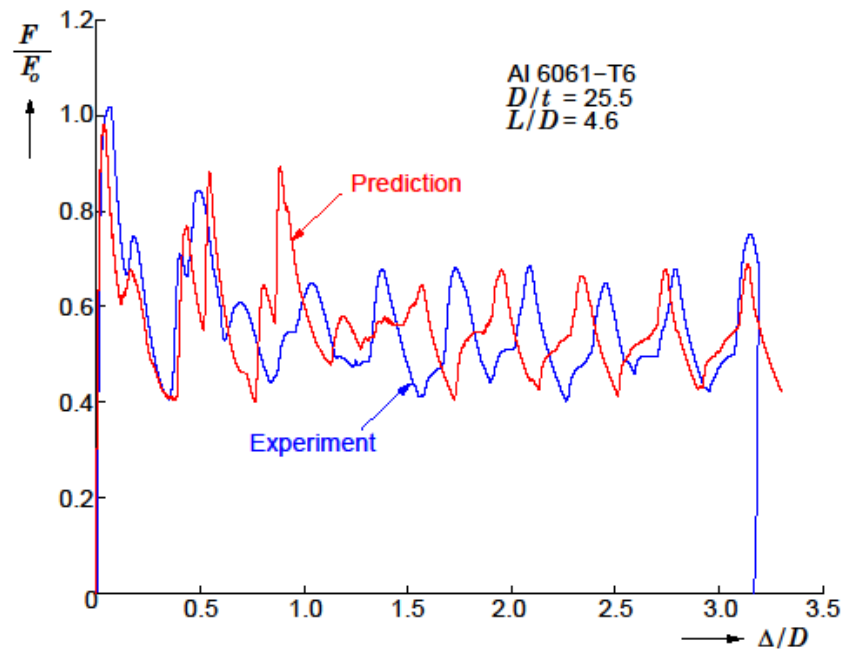
$L/D = 4.6$



Experiment

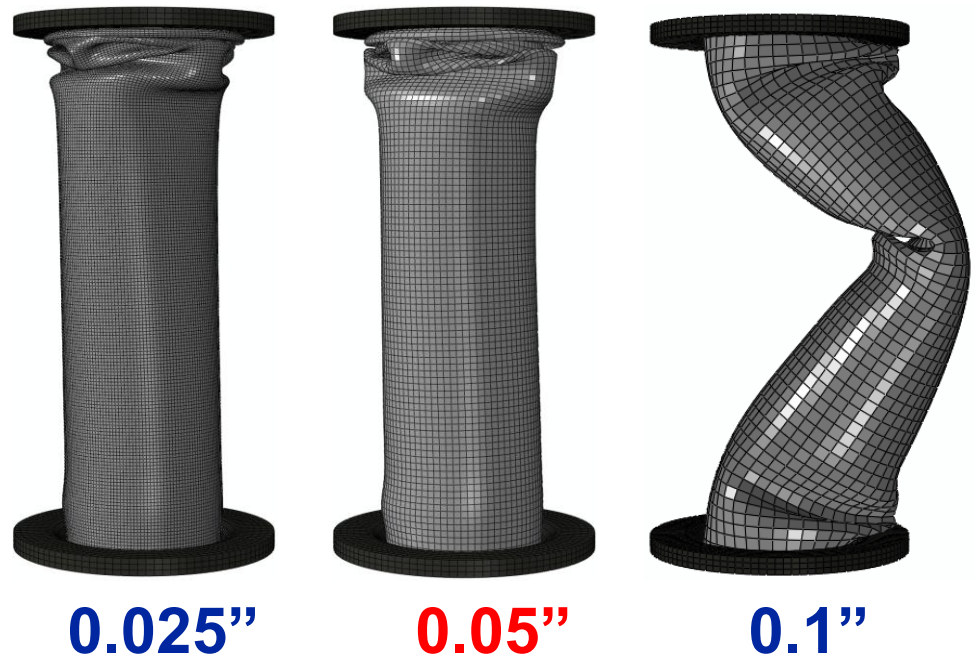


Prediction



# Sensitivity Investigations

- **Mesh Sensitivity**
  - 0.025, 0.05, 0.1 inch squares studied
- **Other Studies**
  - Clamping Pressure
  - Fixture Dimensions
- **Future Studies**
  - Hex-Based Meshes





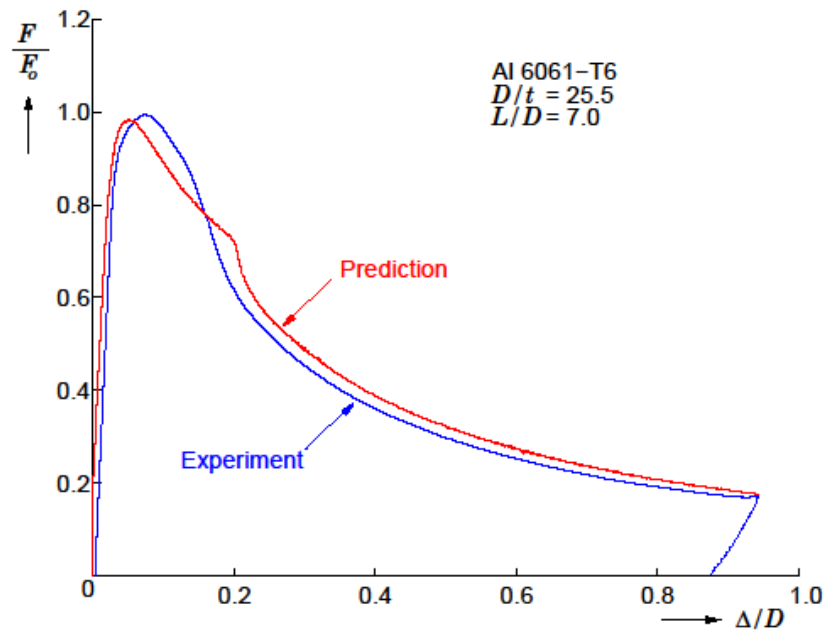
$$L/D = 7$$



Experiment



Prediction





## Summary of Results

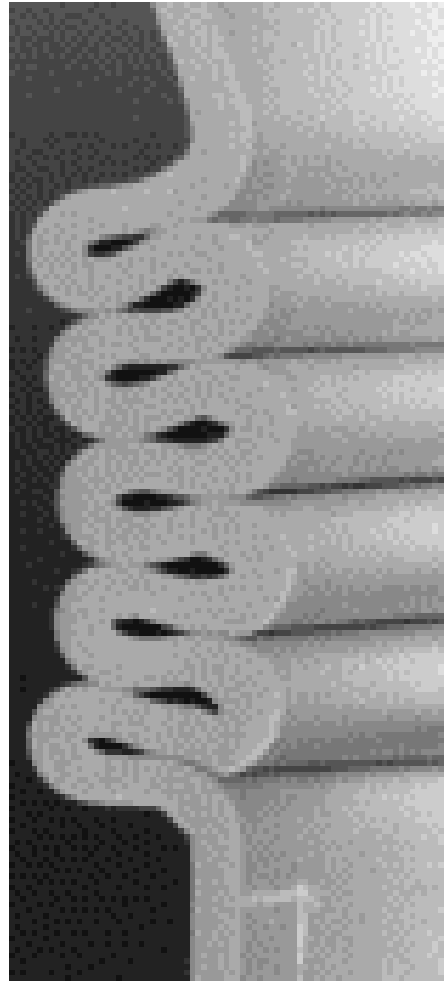
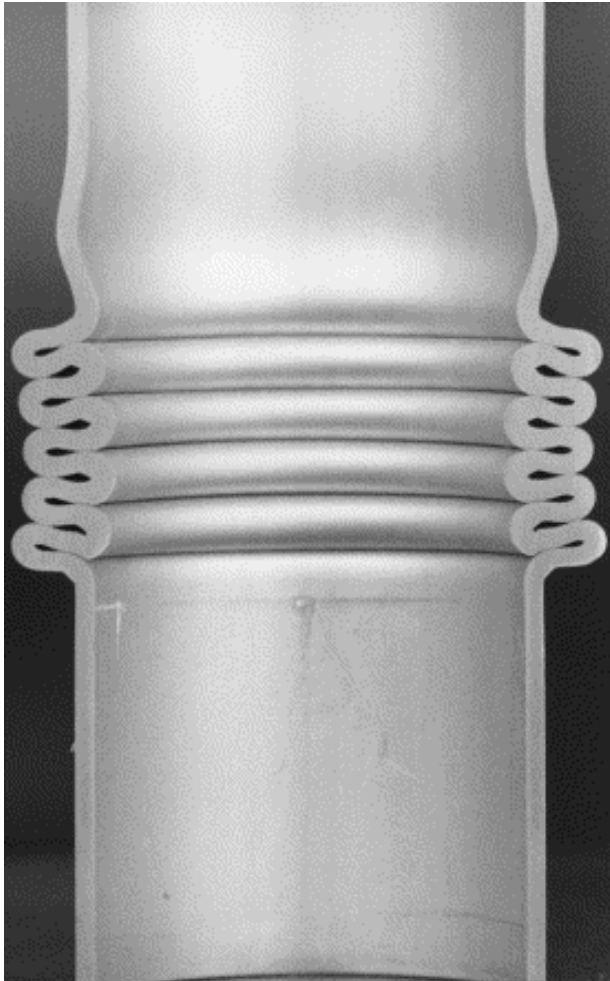
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$L/D$	Mode Experiment	Mode Prediction	$\lambda$ ( $\Delta/D$ ) Experiment	$\lambda$ ( $\Delta/D$ ) Prediction
2.2	N=3 / N=3	N=3	-	-
3.8	N=3 / N=2-3 (t)	N=3	0.352	0.388
4.6	N=3 / N=2-3 (t)	N=3	0.354	0.394
5.4	N=3 (t)/ Lateral	N=3	-	0.395
7.0	Lateral / Lateral	Lateral	-	-

# Axisymmetry?

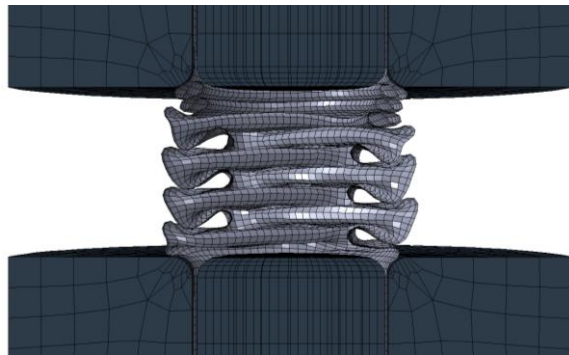
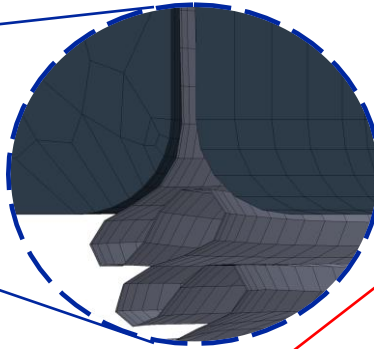
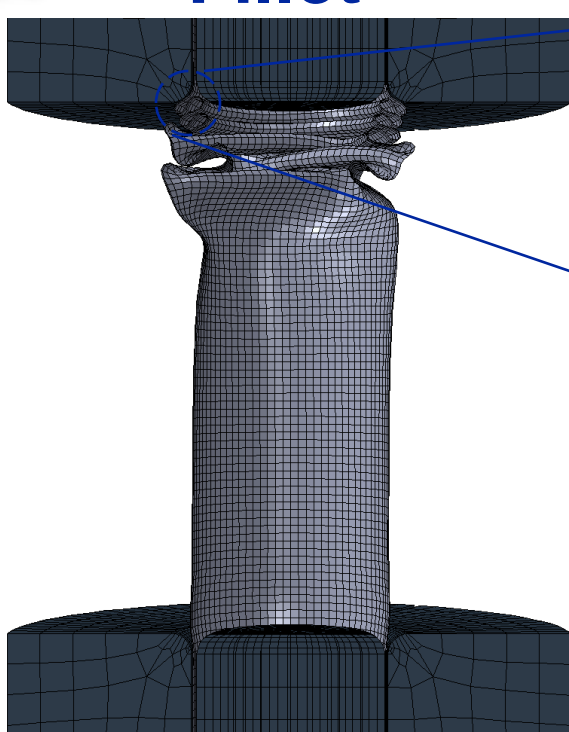
## Bardi et al

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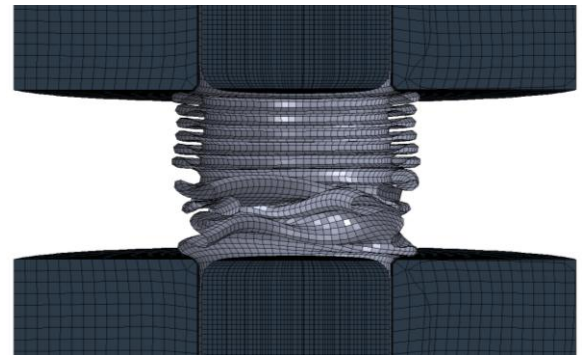
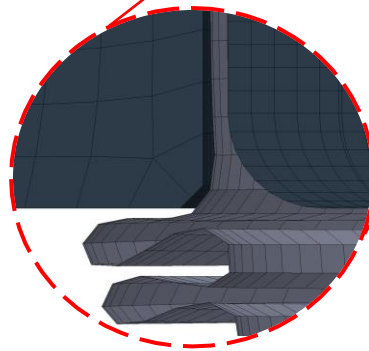
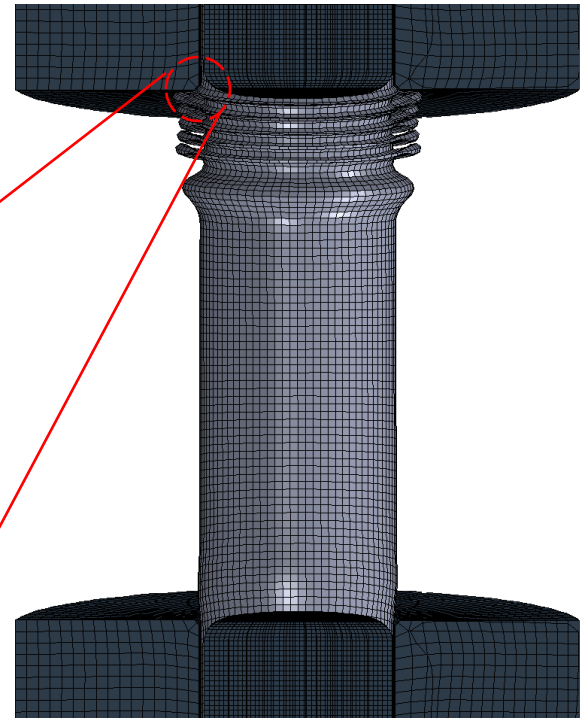


# Boundary Effects

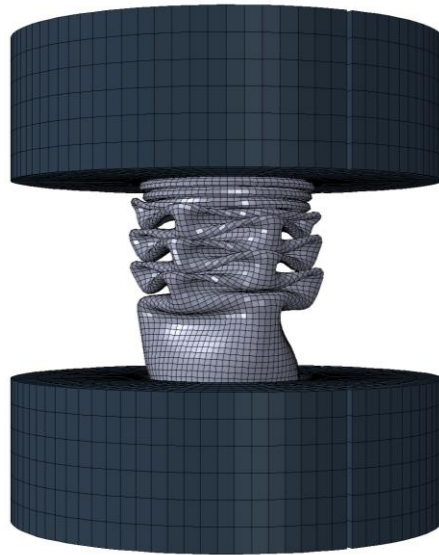
**Fillet**



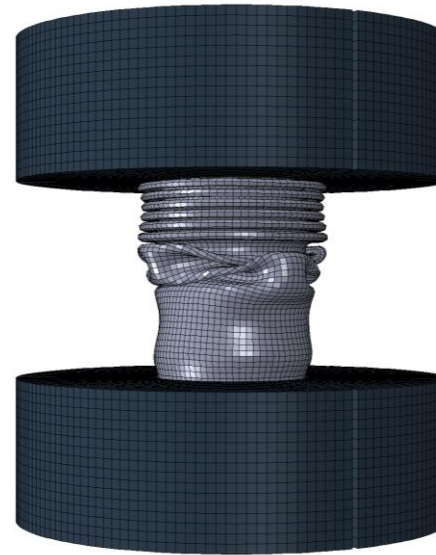
**Chamfer**



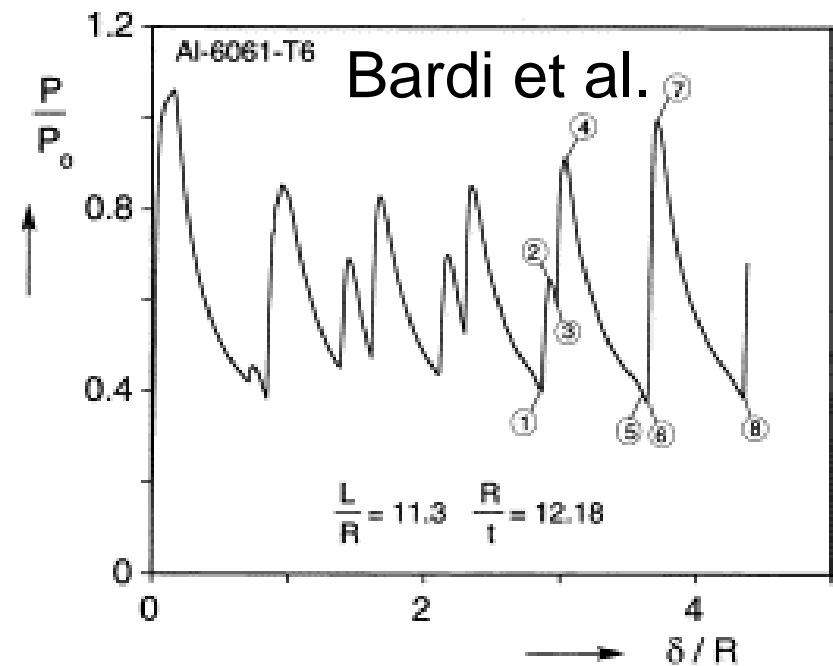
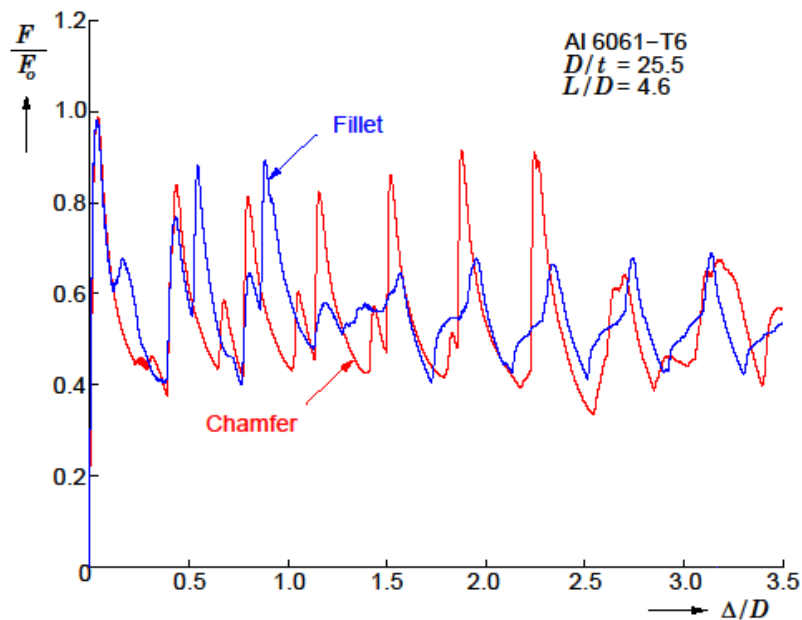
# Boundary Effects



Fillet



Chamfer







## Conclusions

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- Shell model does a reasonable job in predicting the crushing response of the tubes.
- $N=3$  crushing mode seems to be a consequence of the three-segmented clamping fixture and of the applied clamping pressure.
- Shell contact thickness is a model feature that probably affects the numerical results.
- Crushing mode is influenced by the geometric details of the clamping fixture. Perhaps more generally, by the geometry of preceding folds.

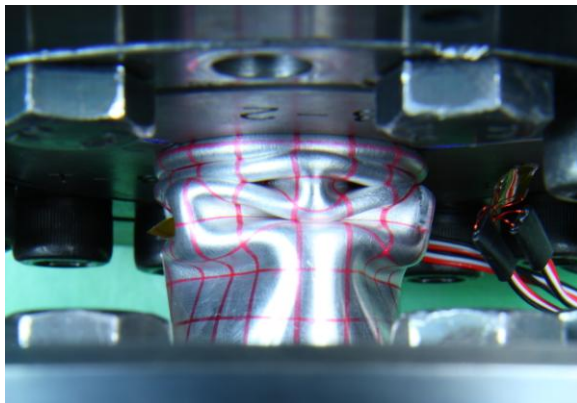


## Parametric Study

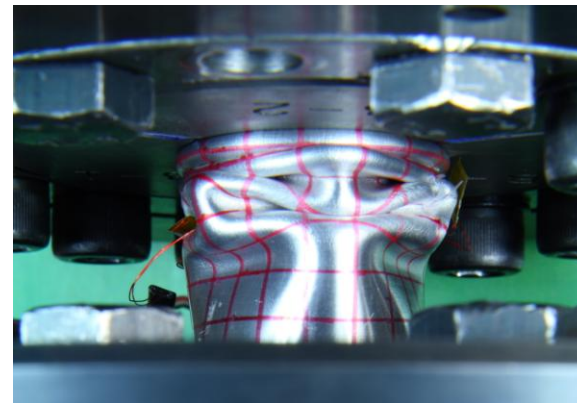
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Clamping Pressure (PSI)	Plug Size (inches)	Mesh (inches)	Result
1250	1.15	0.05	N=3
1250	1.147	0.05	N=2
1250	1.15	0.025	N=2
2500	1.15	0.05	N=3
2500	1.147	0.05	N=3
12500	1.15	0.05	N=3
12500	1.15	0.025	N=3
12500	1.147	0.05	N=3
6250	1.15	0.025	N=3

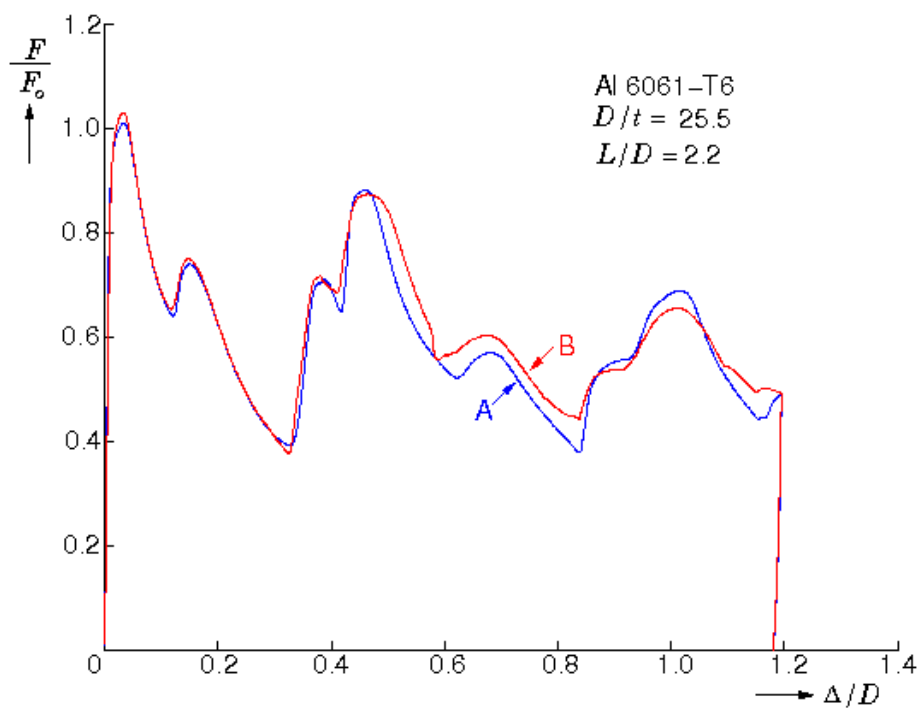
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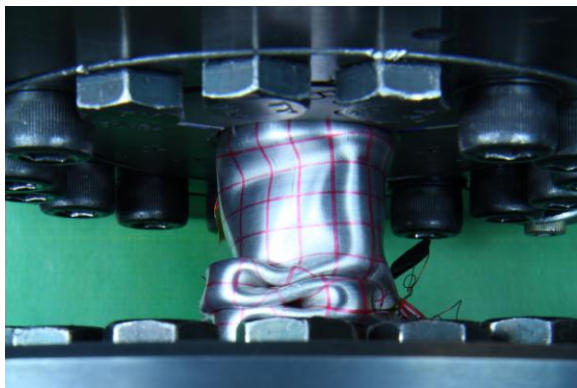
**A**



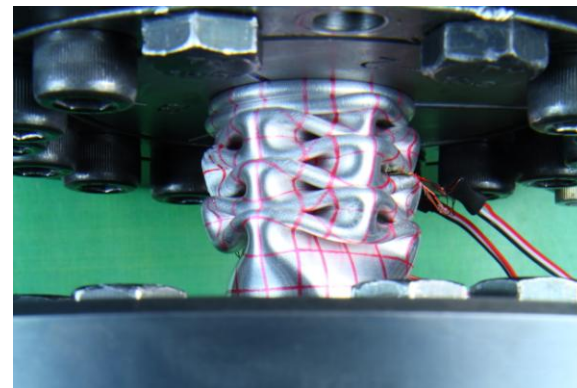
**B**



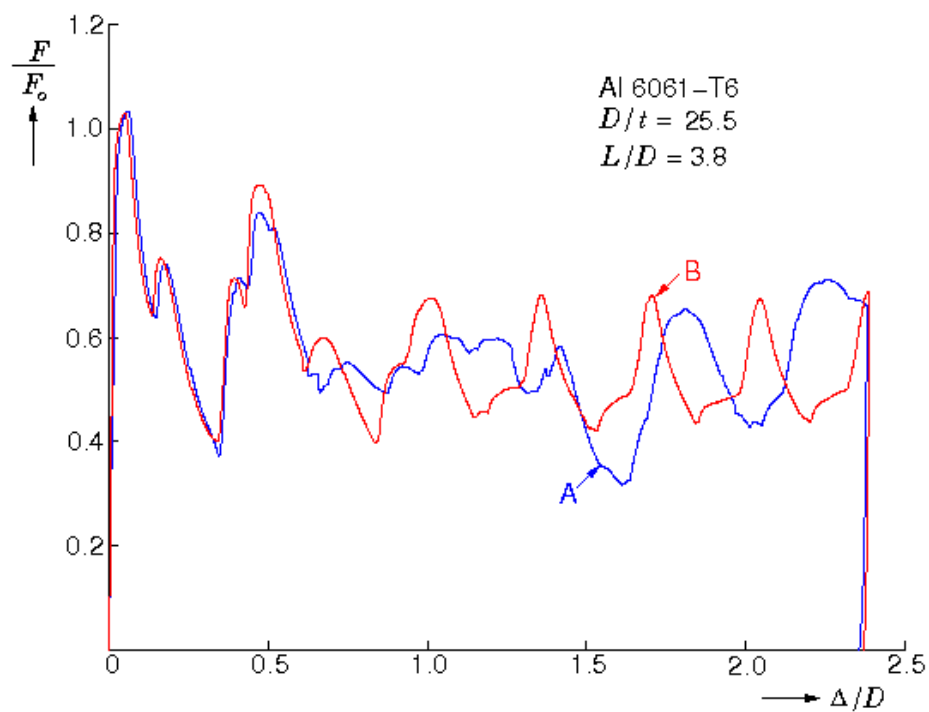
$L/D = 3.8$



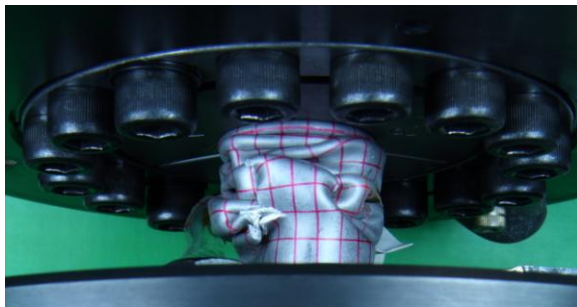
A



B



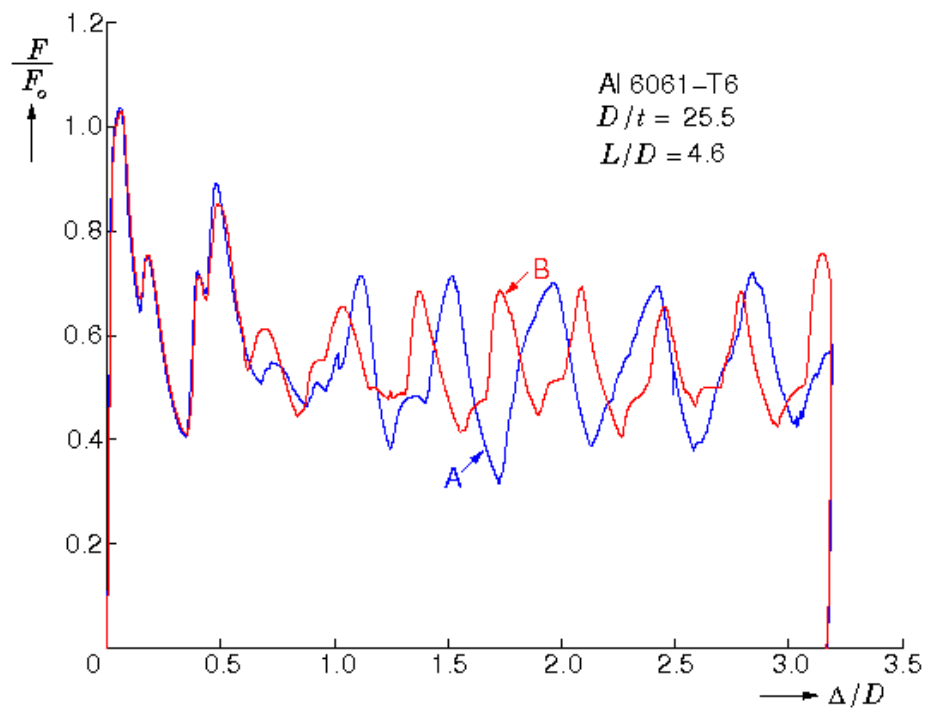
$L/D = 4.6$



A

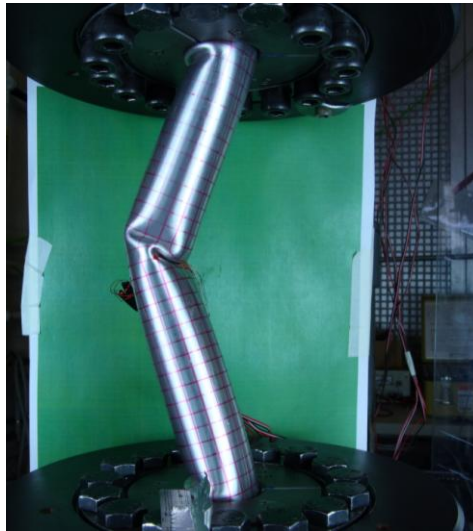


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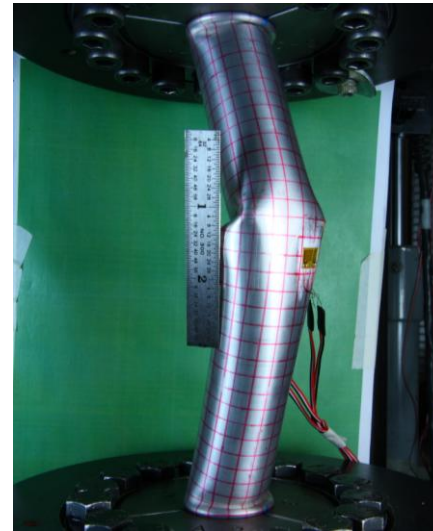




$$L/D = 7$$



A



B

