

Summary of the Sandia Supercritical CO₂ Development Program

SAND2011-3659C

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SCO₂ Power Cycle Symposium

May 24-25, 2011

University of Colorado, at Boulder





Goals of Presentation

- DOE Gen-IV S-CO₂ Research Program Program
 - Major Research Areas
 - **Testing**
 - **Brayton and Compression Loop Descriptions**
 - **Compressor Performance Mapping**
 - **Breakeven Power Generation**
 - **Mixtures**
 - **Condensation Cycles**
 - **Thrust Bearing Heating**
 - Modeling
 - 10 MW_e Development and Demonstration Program Plans and Cost
 - Ability of Sandia S-CO₂ Brayton Loop to Reproduce Other Cycles



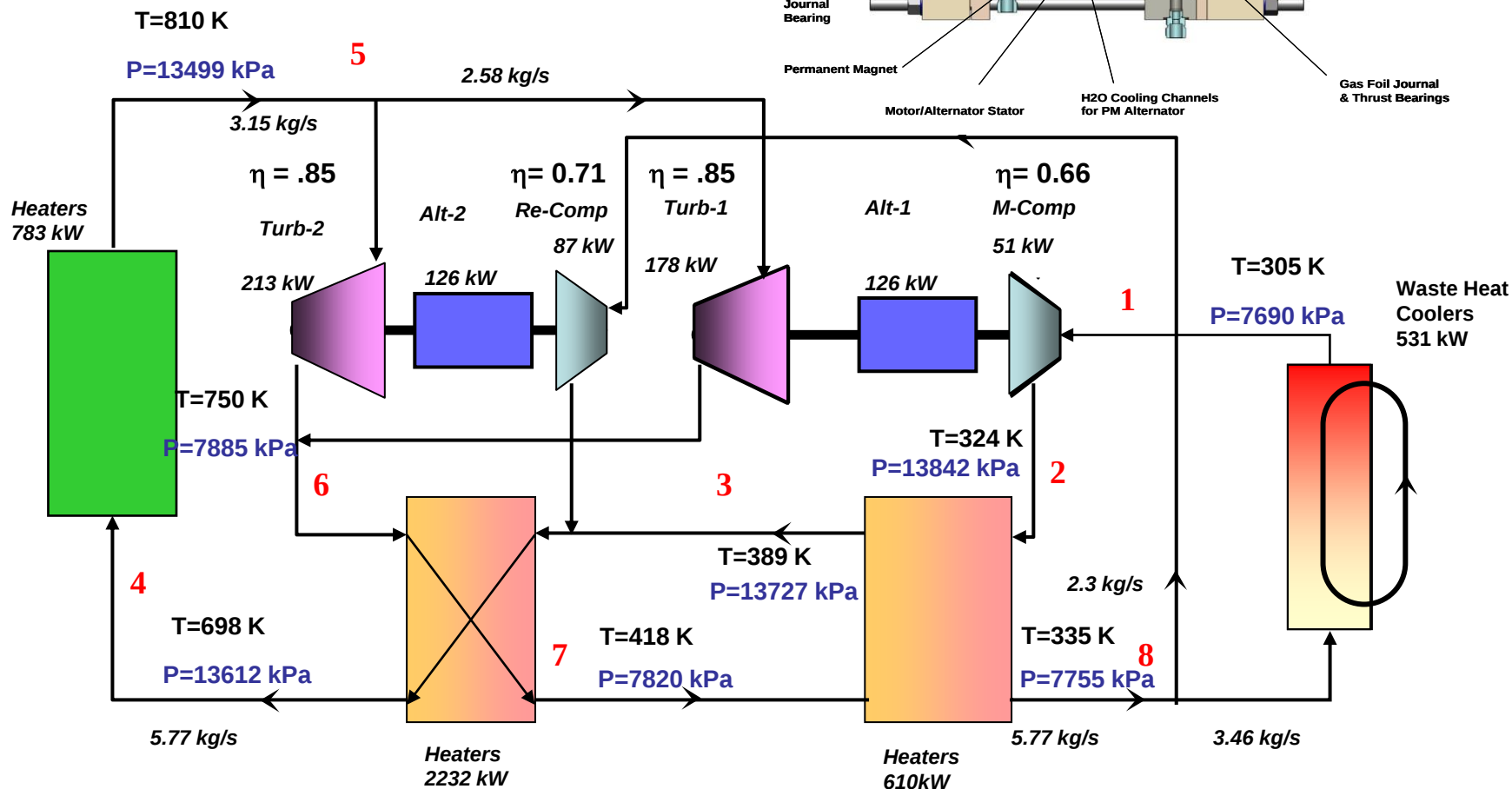
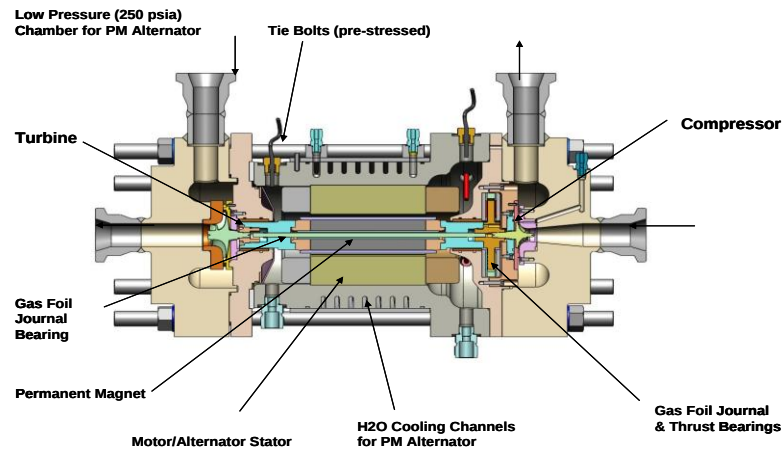


DOE Supercritical CO₂ Program Description



SNL/DOE Design Target for Proof-of-Principle Split-Flow Re-compression S-CO₂ Brayton Cycle

Modified Cycle to Enable Scaled
Turbomachinery Development with Lower Risk
Dual Shafts, Lower Pressure Ratio (1.8 versus 2.6)

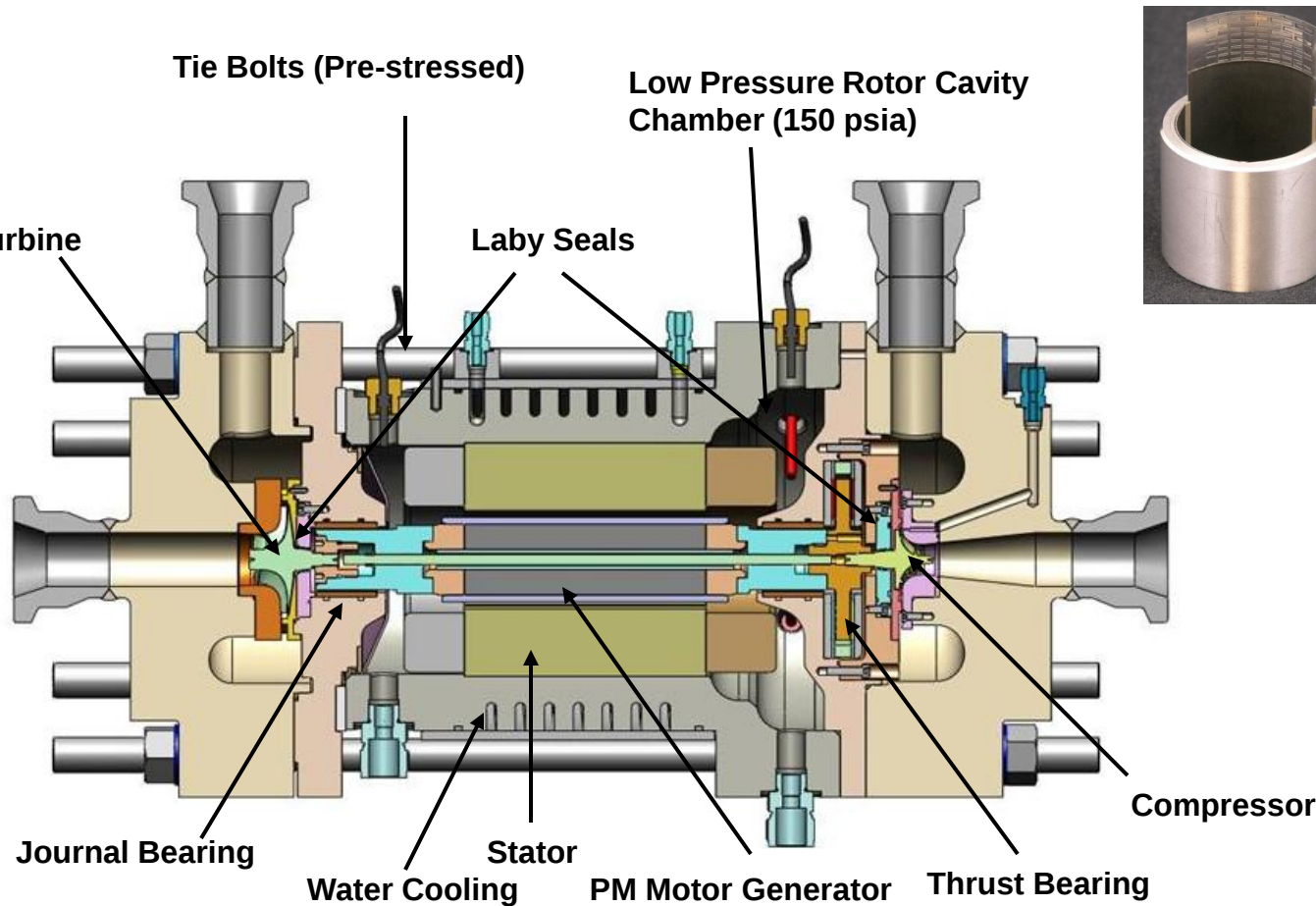




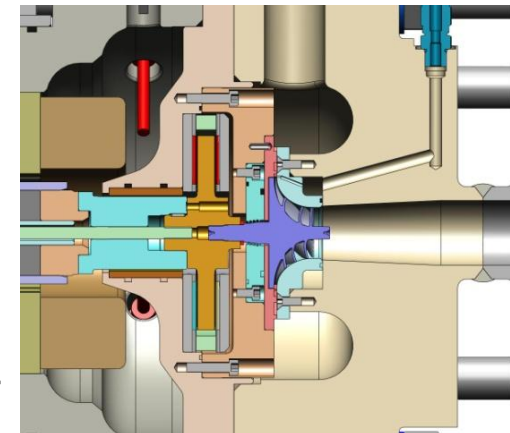
Key Technology

Turbo- Alternator Compressor Design with Gas Foil Bearings (~24" Long by 12" diameter)

Technology for Small Scale System



Gas-Foil Bearings



Patent Application is in Process for All major Features of this Design



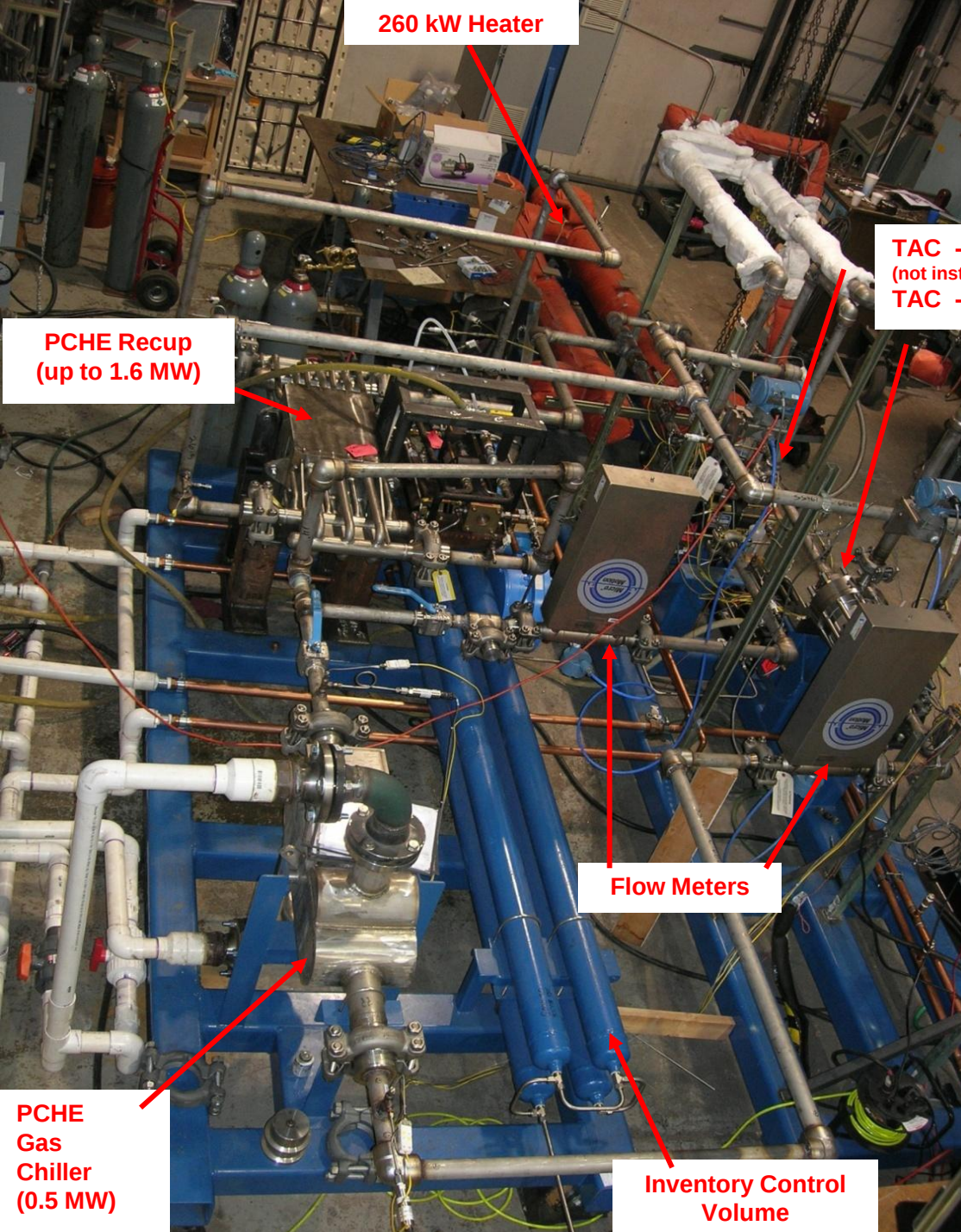
S-CO₂ Development Sequence



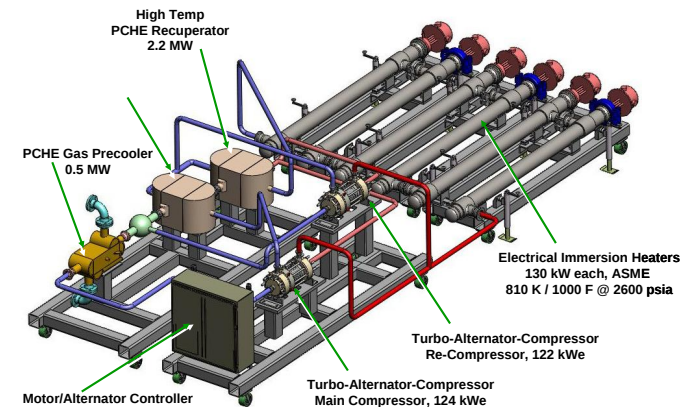
**Sandia Single
Compressor Loop**

**DOE Gen IV Split-Flow
Re-compression
Brayton Loop**



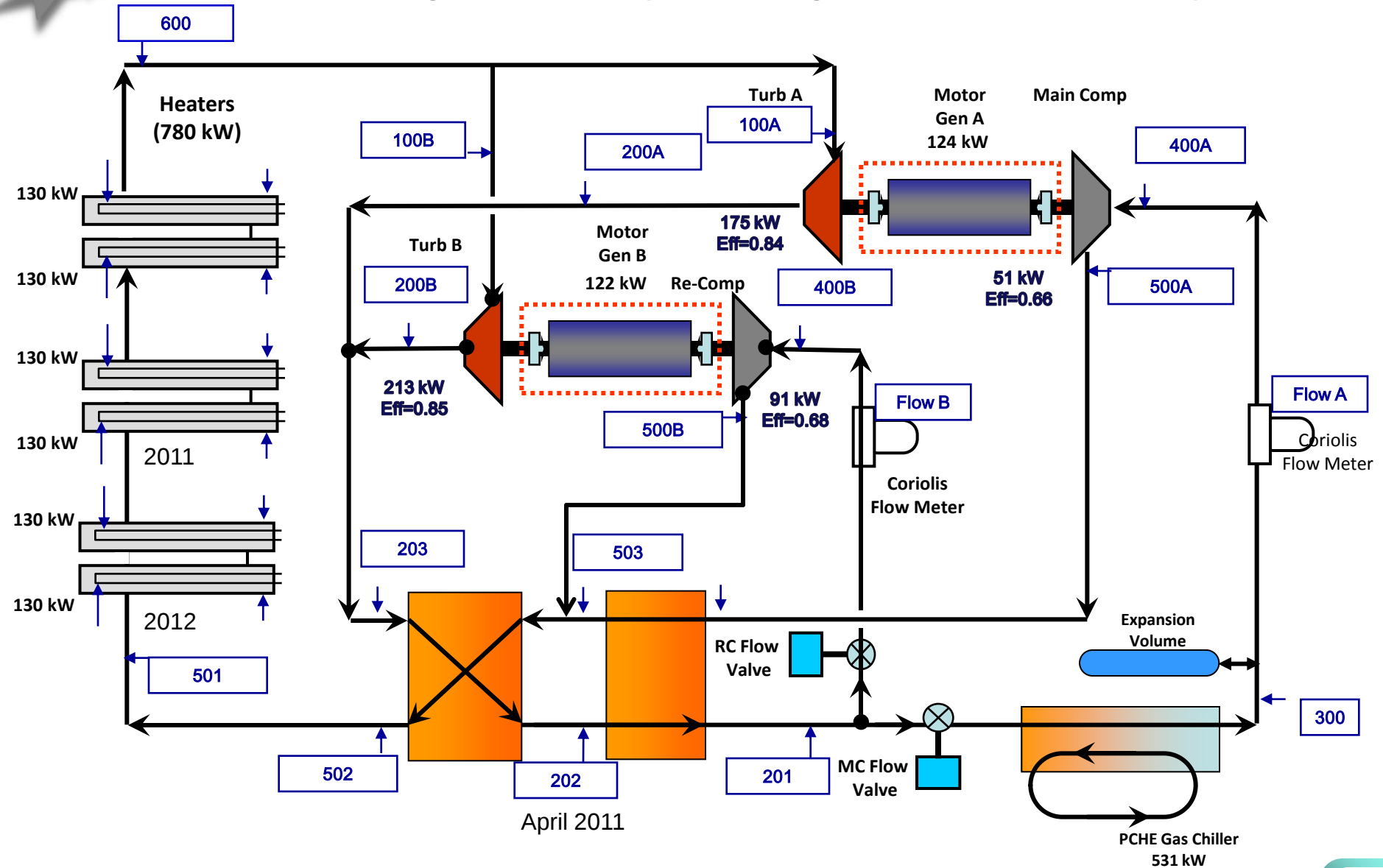


Supercritical S-CO₂ Brayton Cycle DOE-Gen IV



Supercritical CO₂ Brayton Loop

Final Design, Currently Existing, and Alternative Layouts





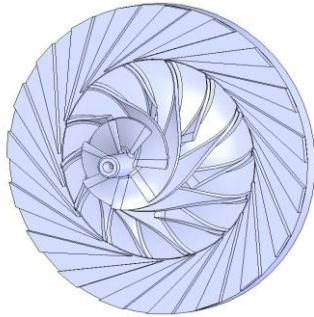
Mapping



Turbomachinery Wheels



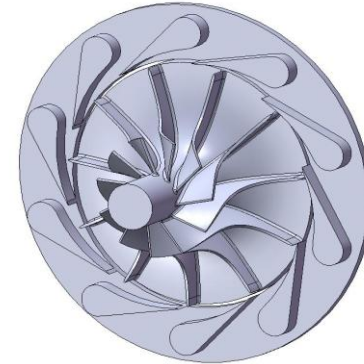
**Main
Compressor**



**Re-
Compressor**



**Turbine for
Re-Compressor**



**Turbine for
Main Compressor**



OD=37.3 mm
1.47"



OD=57.9 mm
2.27"



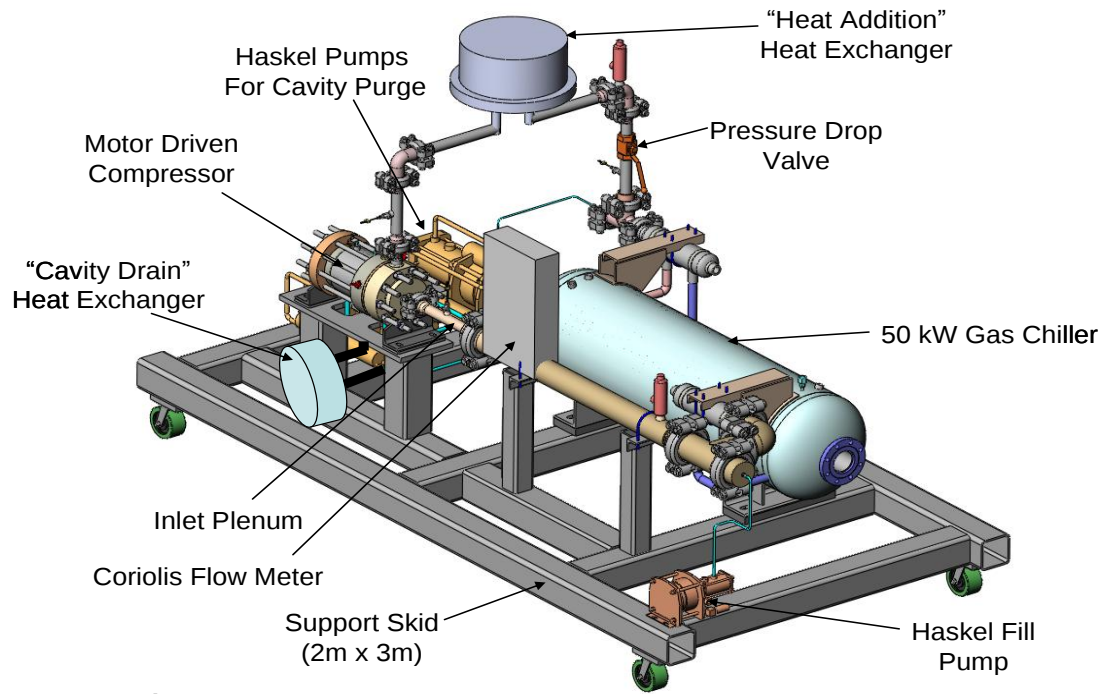
OD=68.3 mm
2.69"



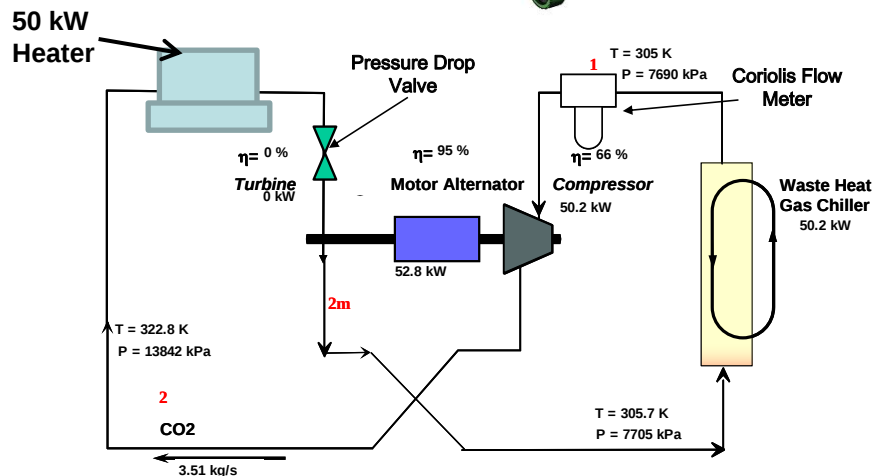
OD=68.1 mm
2.68"



Sandia S-CO₂ Compression Research Loop

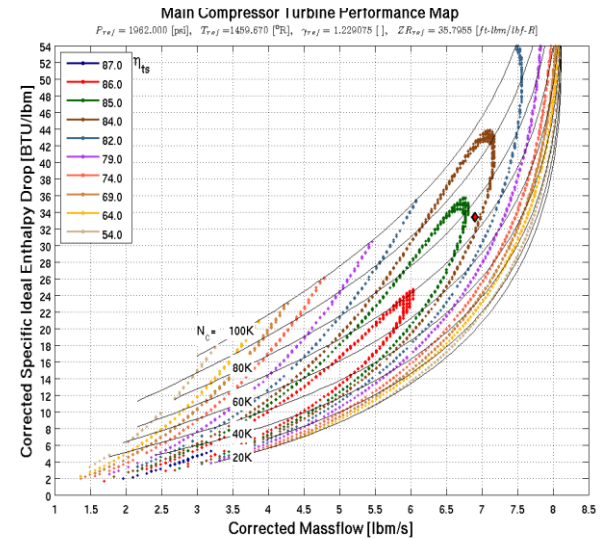
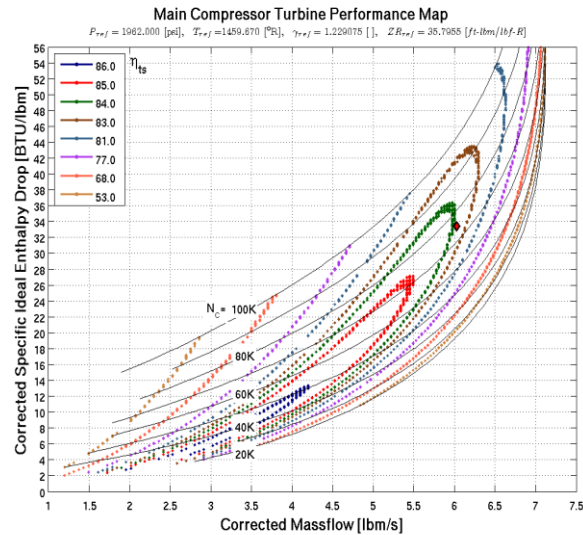
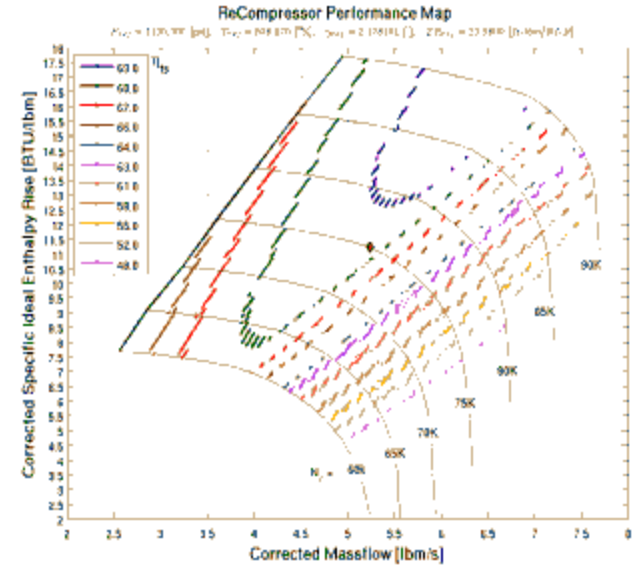
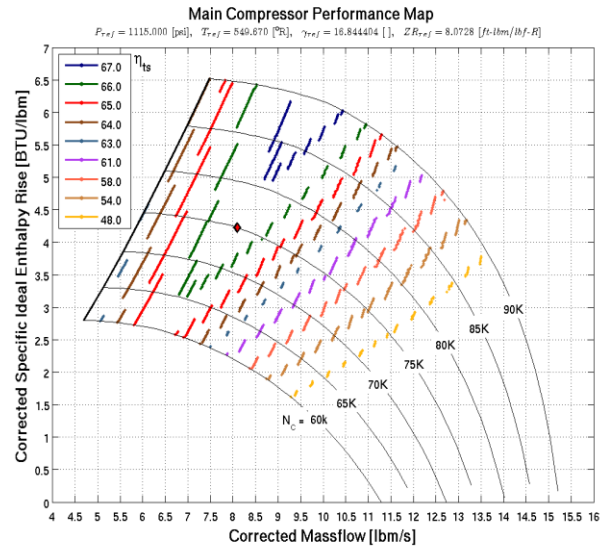
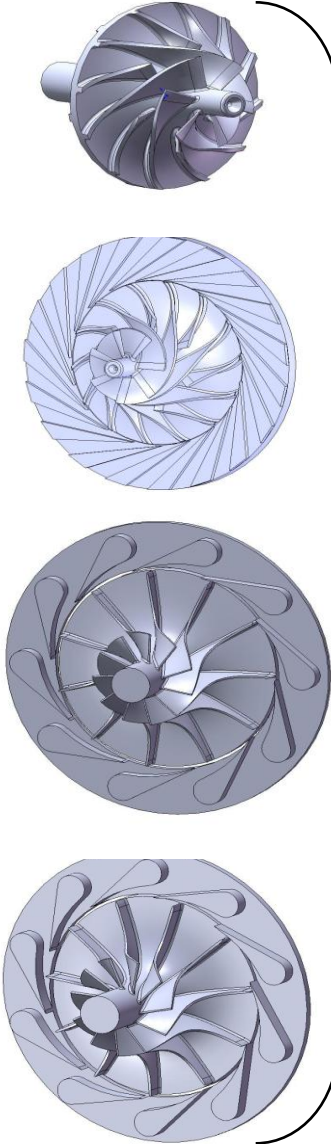


- Sandia S-CO₂ compression loop, consists of a compressor, heater, flow control valve, and chiller
- Instrumented with T,p sensors at 4 key state points, and a density meter at compressor inlet
- Used for mapping compressor performance near the critical point, bearings & seals R&D, windage tests, fluid mixtures and natura circlation

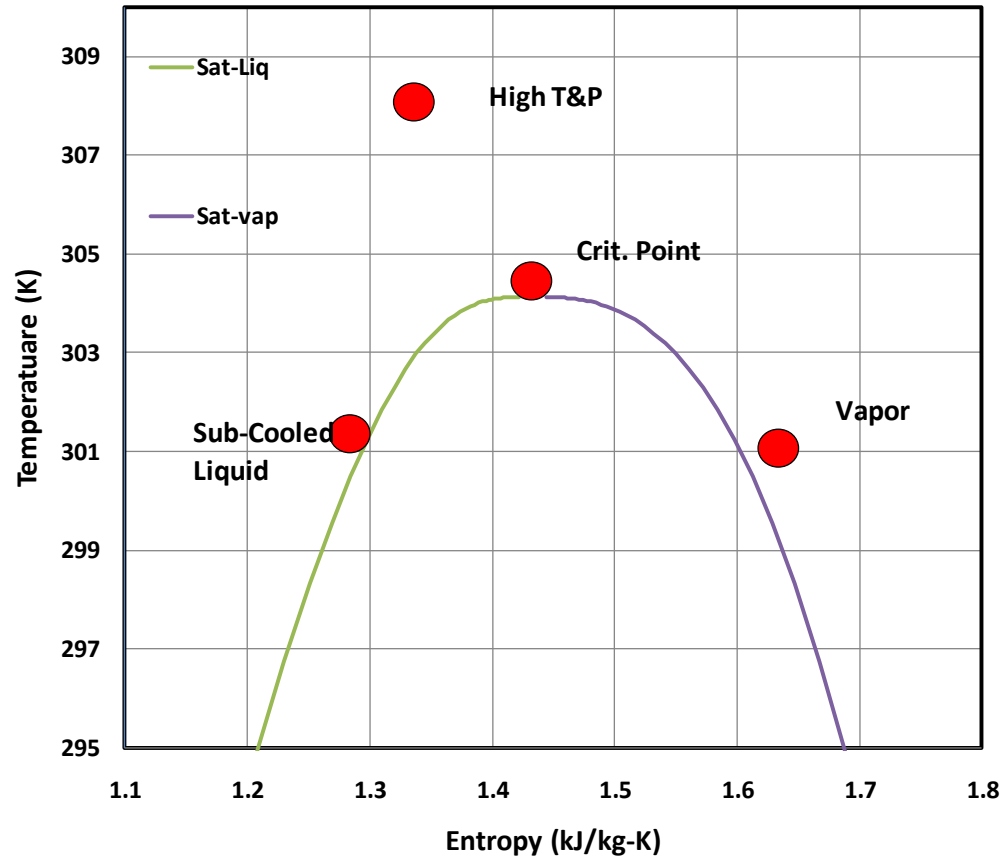


Performance Maps

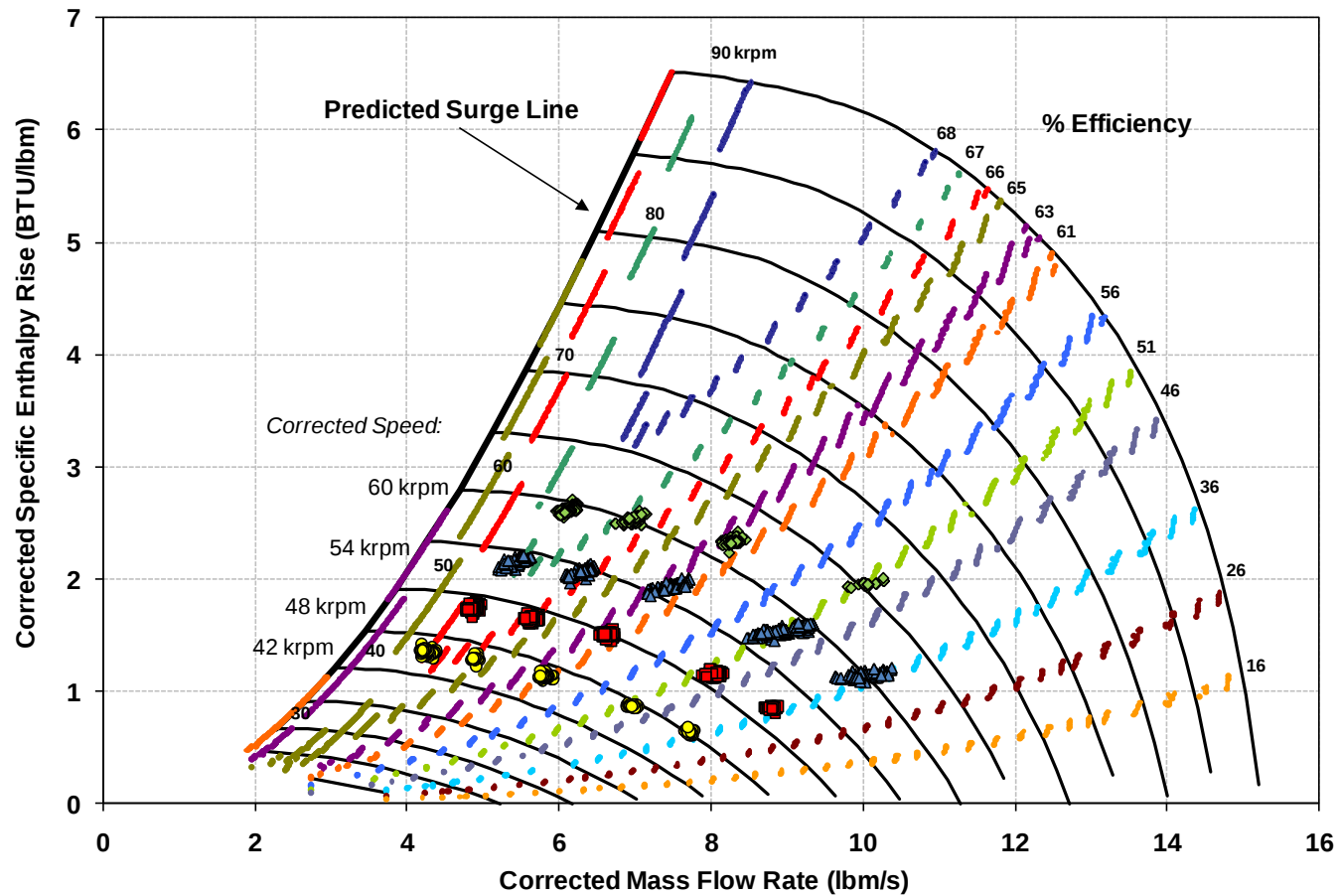
Barber-Nichols Model Predictions



Compressor Inlet Conditions for Map Measurements (50 krpm) Performed September 2010 at Sandia



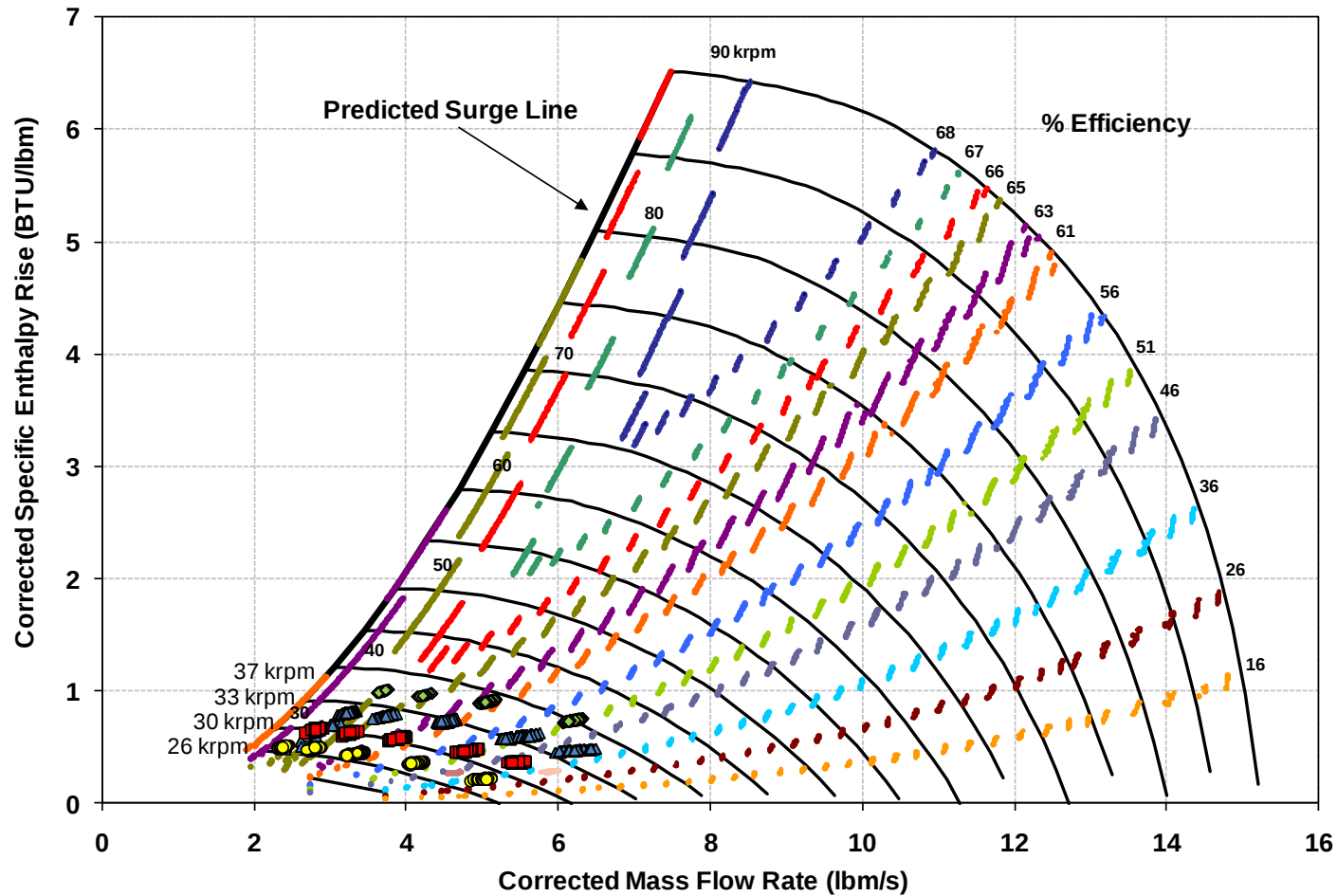
Supercritical CO₂ Main Compressor Map
(dH based on T and P calculated Real Time during Run)



For CO₂ liquid, compressor maps



Supercritical CO₂ Main Compressor Map
(dH based on T and P calculated Real Time during Run)



Vapor, compressor maps are near predictions for supercritical CO₂.



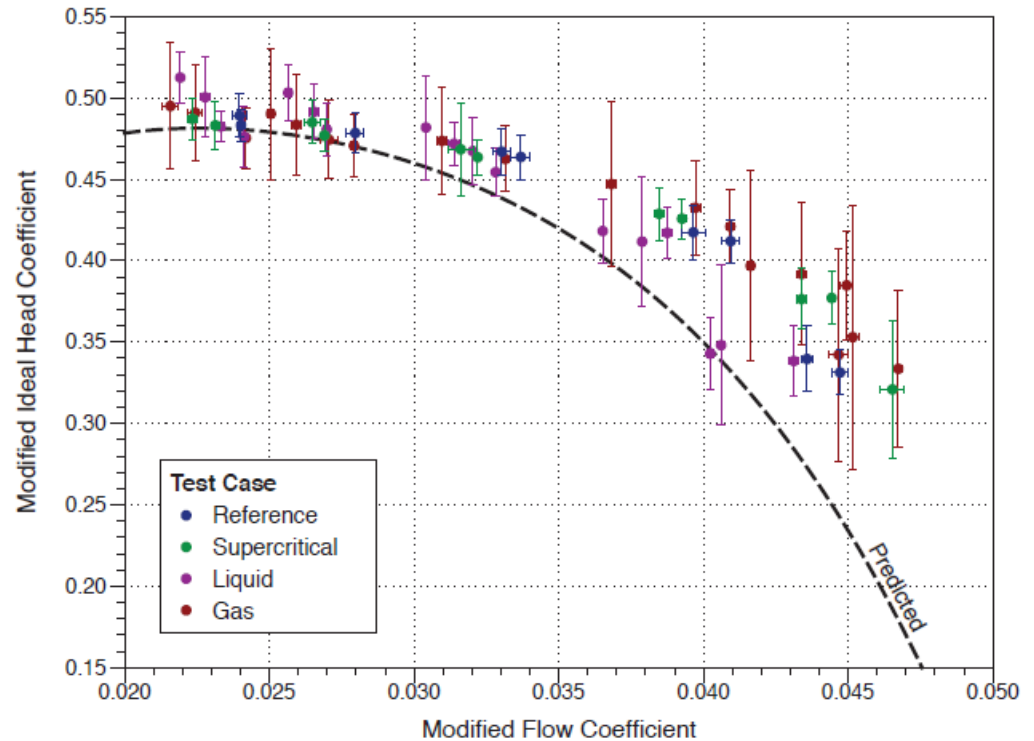
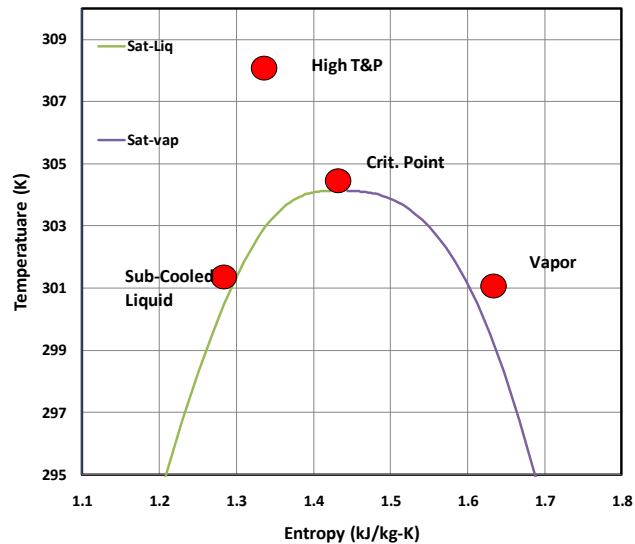


Generalized Measured and Predicted Maps

Modified ideal head coefficient versus modified flow coefficient

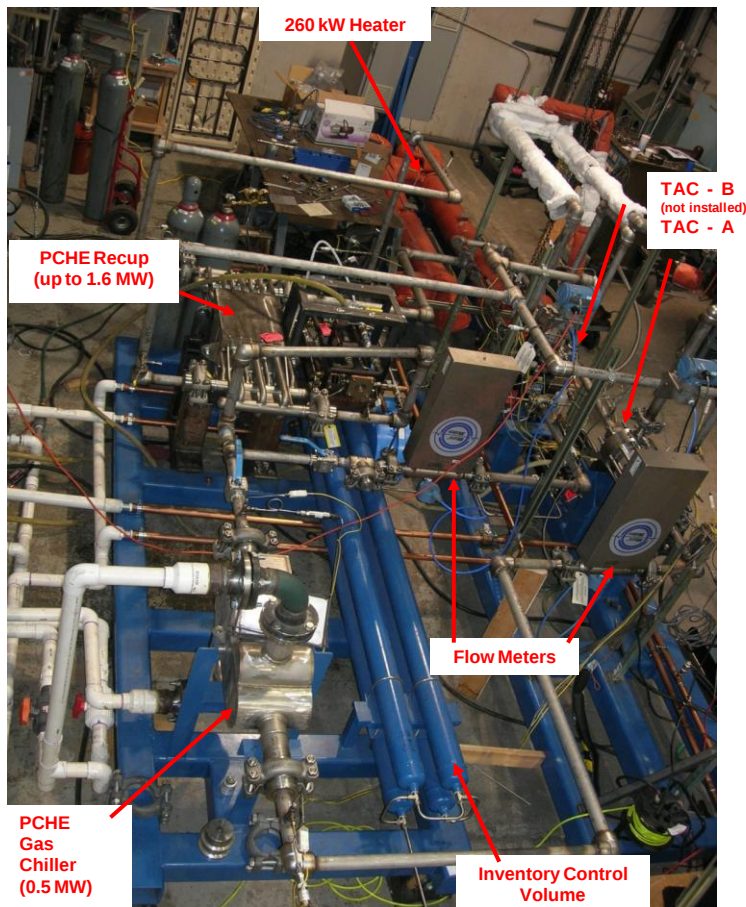
J. Dyreby (Univ. of Wisconsin Madison)

Similar Results by Bob Fuller (Barber-Nichols)

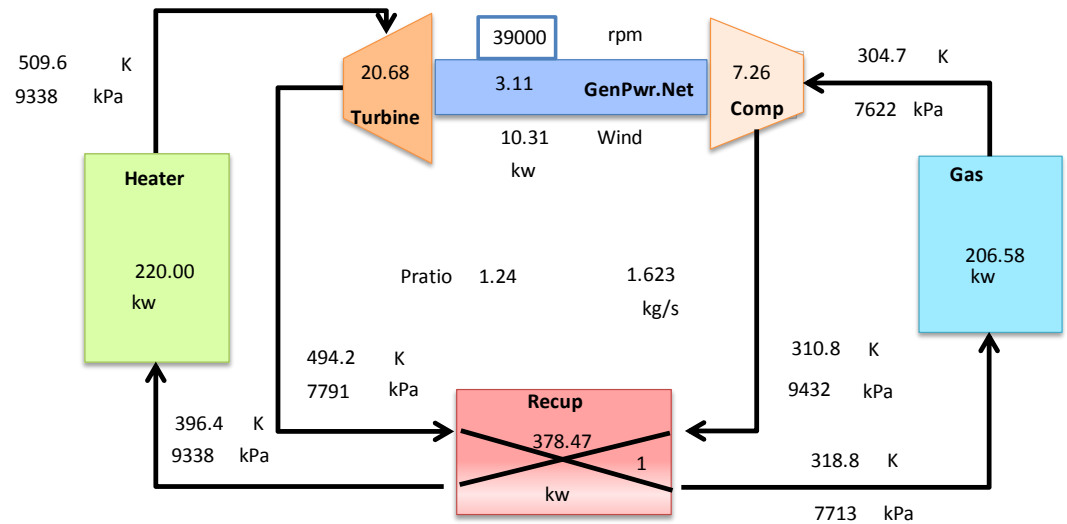




Break-Even Power Generation



TAC-A

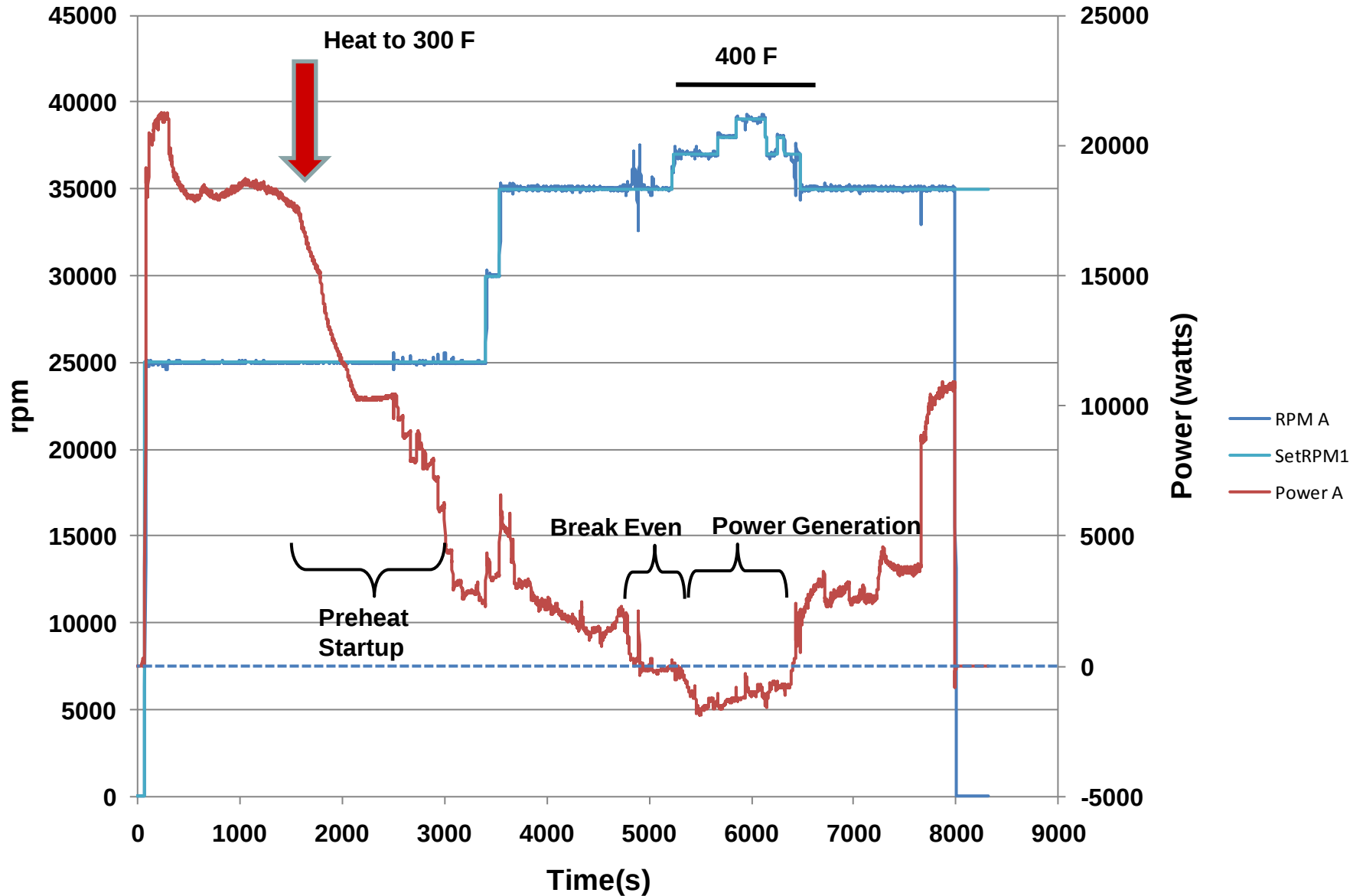


Off Design Cycle Analysis



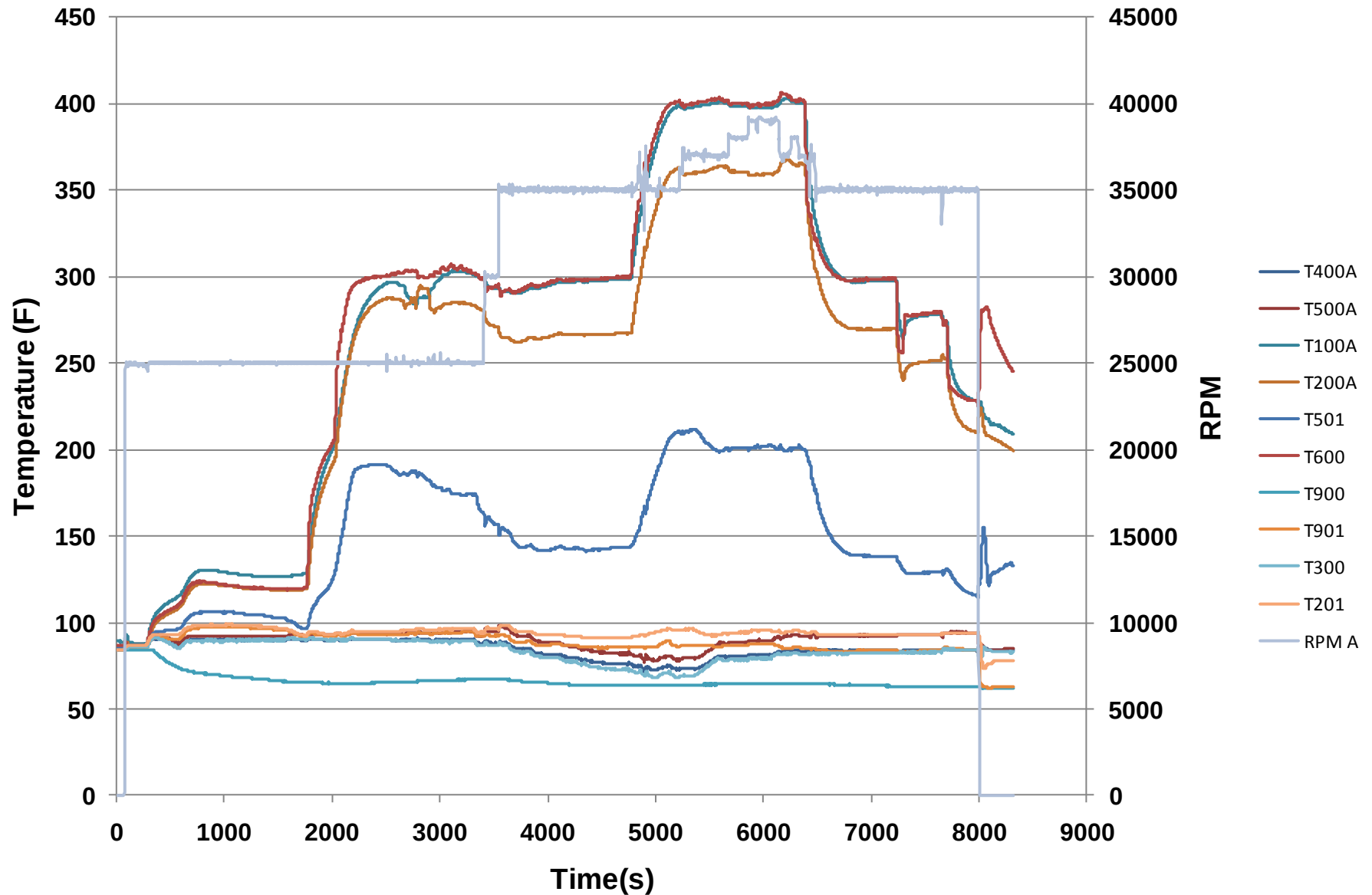
RPM and Motor/Alternator Power: TAC-A

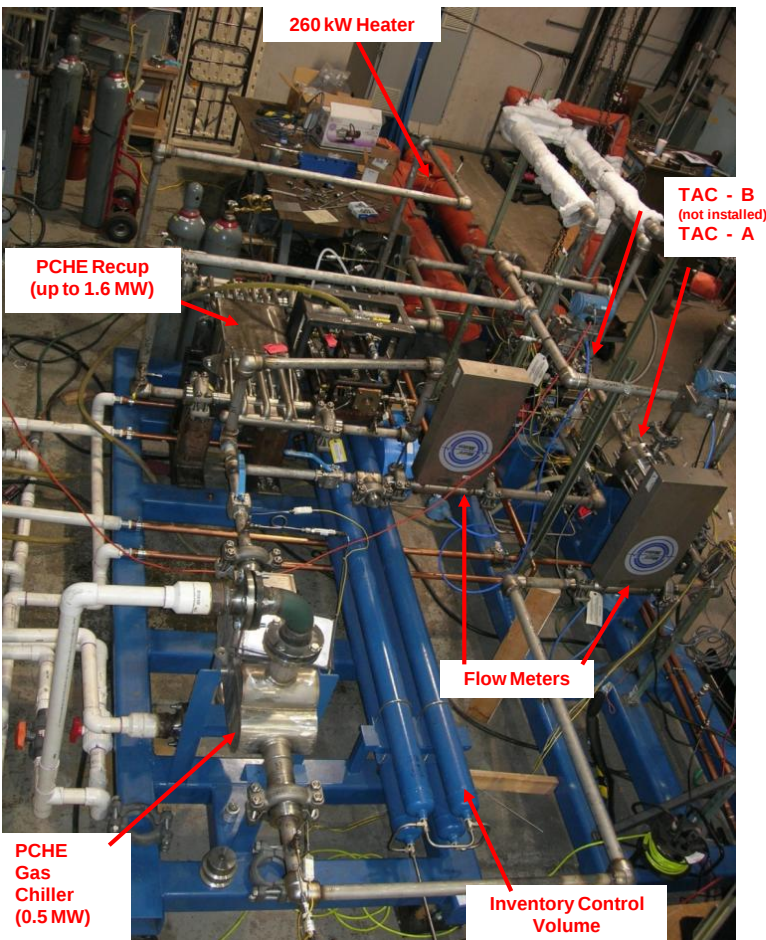
GenIV_101201_1041.csv



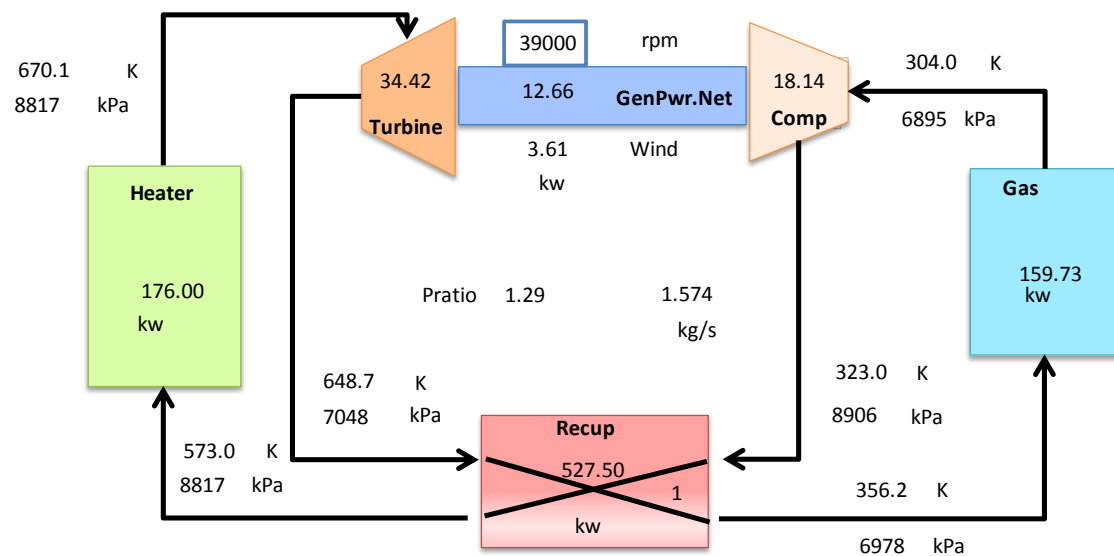
Compression Loop Temperatures: TAC-A

GenIV_101201_1041.csv





TAC-B

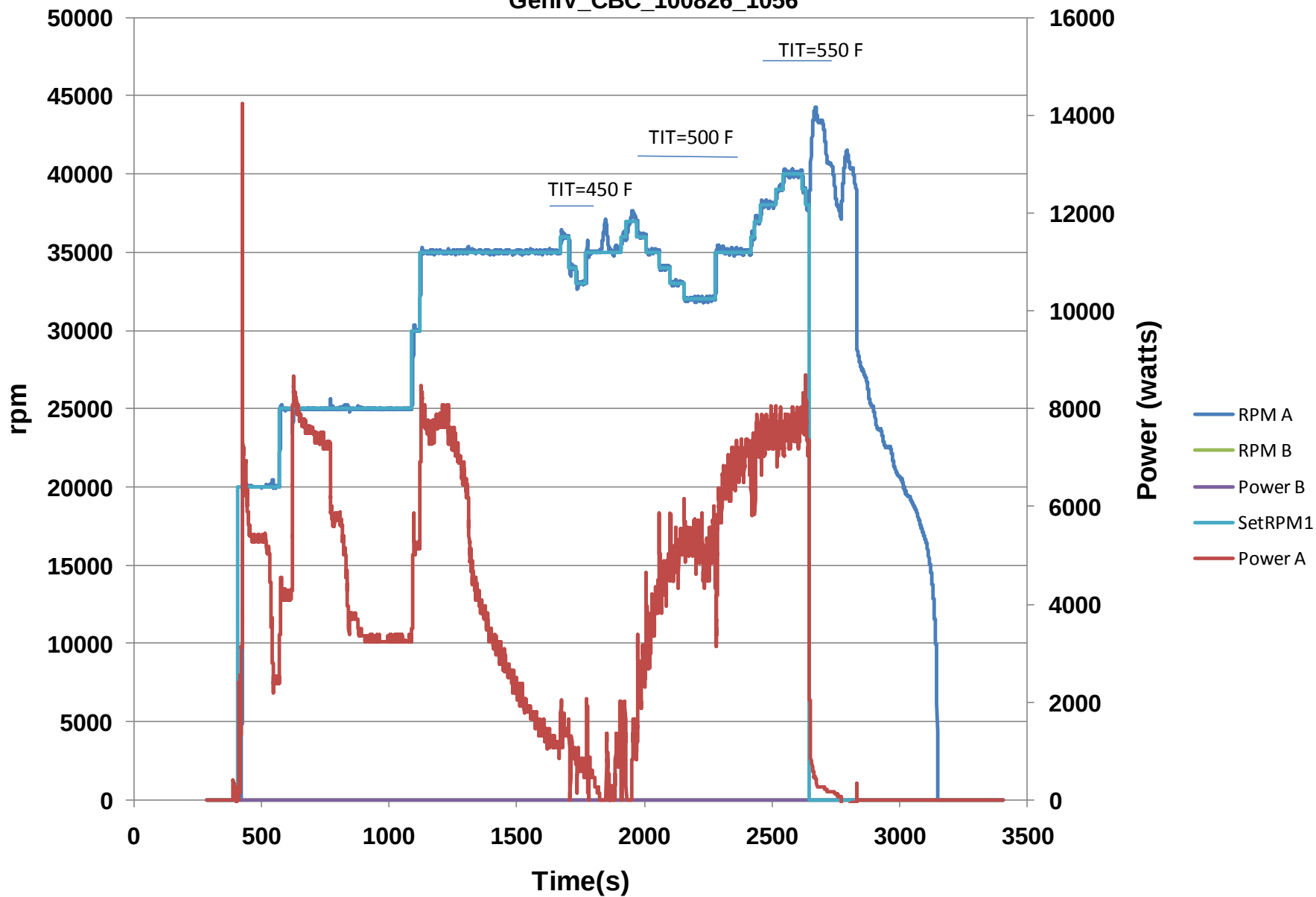


Off Design Cycle Analysis



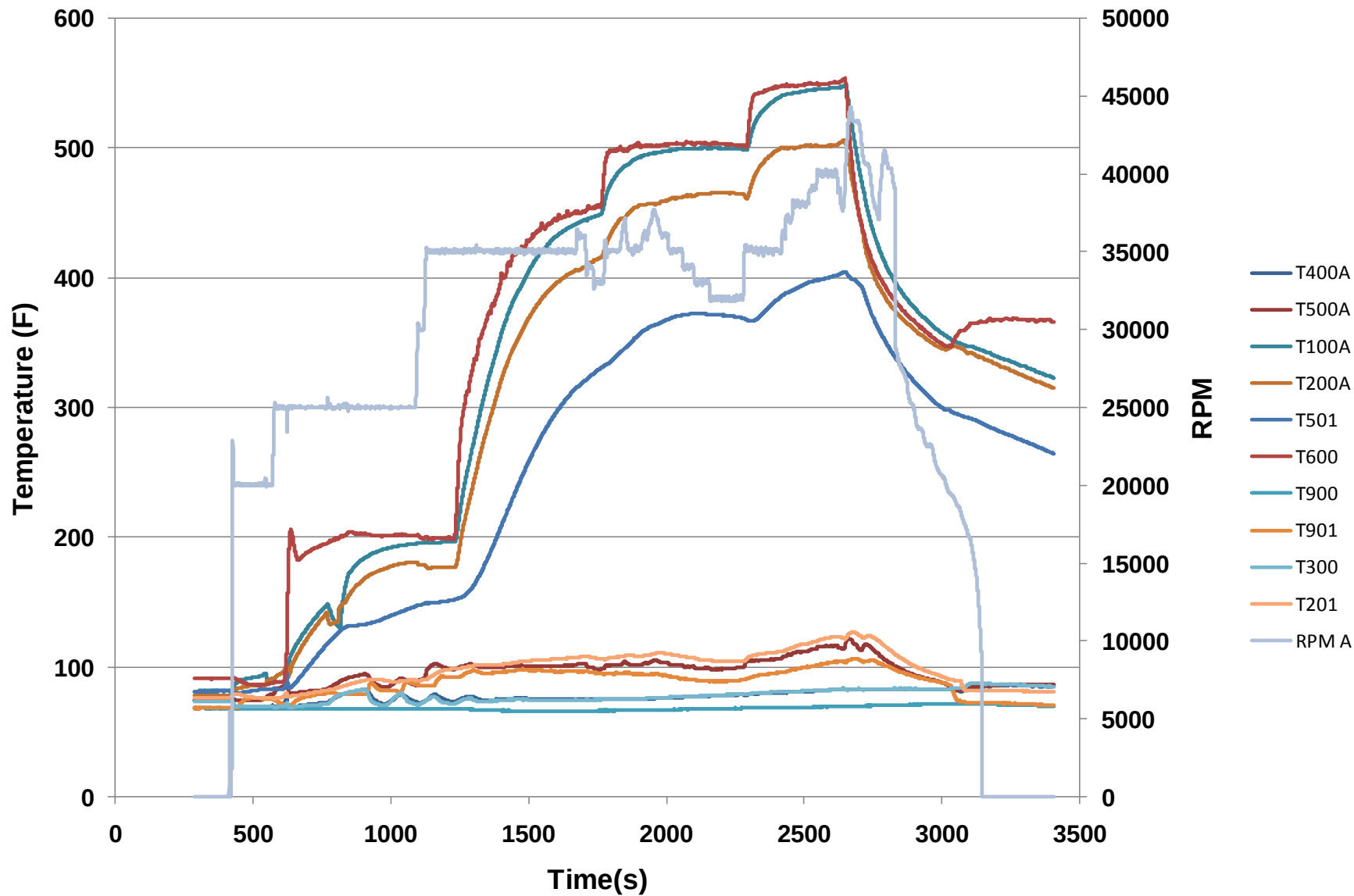
RPM and Motor/Alternator Power

GenIV_CBC_100826_1056



Compression Loop Temperatures

GenIV_CBC_100826_1056





Break-Even Power Production Summary and Conclusions

- Simple Recuperated Brayton configurations have just enough heater power to reach break-even conditions with 260 kW of heater power
- Too much flow in the re-compression Brayton cycle to make power in both TACs
- Break-even at 350/430 F Main-TAC-A and Re-TAC-B
 - Main-compressor: Peak Temperatures to 400 F, 3.2 kWe
 - Re-compressor: Peak Temperatures to 600 F, 8 kWe, ~ 6%
- Off design models predict these break-even performance parameters for power, rpm and TIT.
- Successful startup/preheat procedures implemented





Mixtures

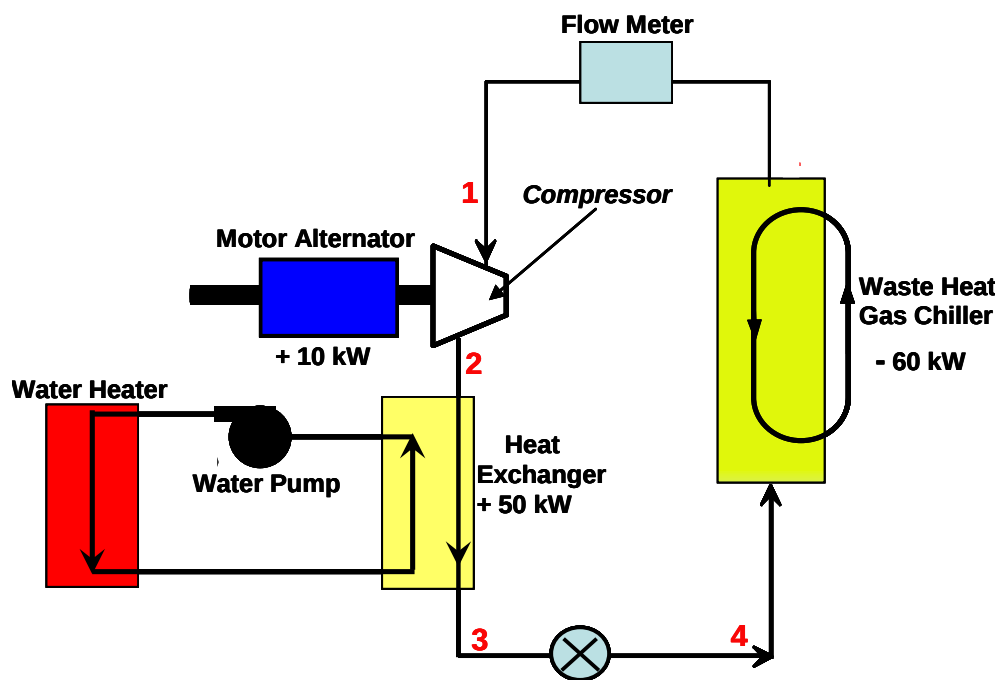


S-CO₂ Compression Loop Used to Measure Effects of Gas Mixtures: Motivation is Efficiency Improvements

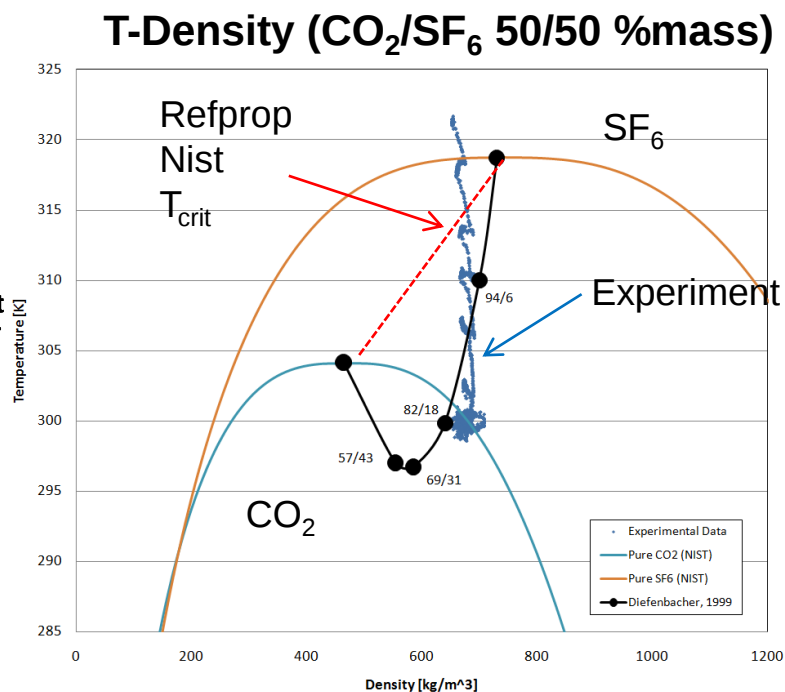
Measured (EOS: T_{crit} , P_{crit} , Compressor Maps)

Mixtures Tested

CO ₂	CO ₂ butane	CO ₂ Neon	CO ₂ /SF ₆	CO ₂ /SF ₆	CO ₂ /SF ₆	SF ₆
100%	8% molar n-butane	4% molar Neon	30/70 %mass SF ₆	40/60 %mass SF ₆	50/50 %mass SF ₆	100%



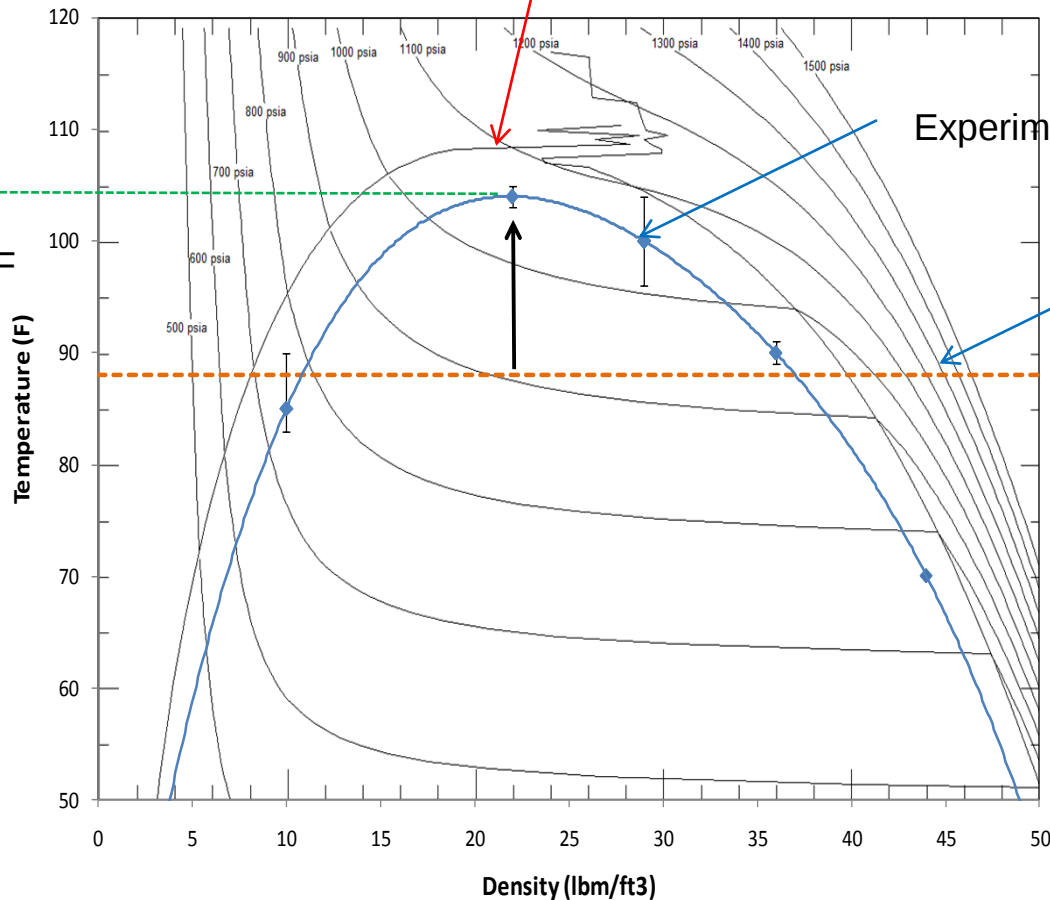
Compression Loop Schematic



CO₂-Butane Mixture

NIST Refprop CO₂ n-Butane 8% molar

Measured:
 T_{crit} CO₂ / 8%
Butane = 104 F



- 1) Gas Mixtures can be used to Increase or Decrease the Effective Critical Point.
- 2) Gas Brayton/Rankine cycles can increase the cycle efficiency with these mixtures compared to pure CO₂





With a Low Temperature S-CO₂ Power Cycle

160 C Turbine Inlet Temperature With Dry Cooling (at 47 C)

Eff=18.1% with CO₂/Butane Mixture

Eff=14.5 % with pure CO₂

			CO2 + 10% Butane	CO2
Inlet Values	Variable Name	Units	Value	Value
Turbine Inlet T	T.5	K	433.15	433.15
Fractional Pressure drop	f.dp		0.0071	0.0071
Compressor Pressure Ratio	r.c		2.64	2.21
Compressor Inlet Pressure	p.1	kPa	8500	8500
Compressor Inlet Temperature	T.1	K	320	320
Mass flow rate	mdot	kg/s	50	50
Split flow frac thru chiller	f.split		0.8272	0.6074
Recup Approach Temp	dT.appr	K	4.00	4.00
Compressor Isentropic Eff		0.85 0.9	0.921954446	0.921954446
Re Comp Isen Efficiency		0.87 0.9	0.87	0.87
Turbine Isen Effic		0.9 0.93	0.965489385	0.965489385
Fraction of Carnot			0.691	0.555
Carnot Efficienc			0.261	0.261
Power				
Heat Transferred in HP leg of LT Recup		kW	6706.41	5234.17
Heat Transferred in LP leg of LT Recup		kW	6706.41	5234.17
Heat Trnsfrd in HP leg of HT recup		kW	0.00	0.00
Heat trnsfrd in LP leg of HT recup		kW	0.00	0.00
Rx Pwr	P.Rx	kW	7204.99	5493.44
Main Comp Pwr	P.Comp	kW	448.39	444.74
Maon Comp Pwr b	P.Comp.B	kW	550.24	300.62
ReComp Pwr	P.ReComp	kW	376.16	828.52
Turb Pwr	P.turb	kW	2675.32	2369.87
Chiller Heat Trnsfr	Q.Chill	kW	5904.46	4697.44
TAC Pwr	P.TAC	kW	1300.53	796.00
	P.TAC-chk	kW	1300.53	796.00
Eff Cycle			0.181	0.145

Substantial improvement in efficiency using S-CO₂ power cycle using CO₂ Butane Mixture



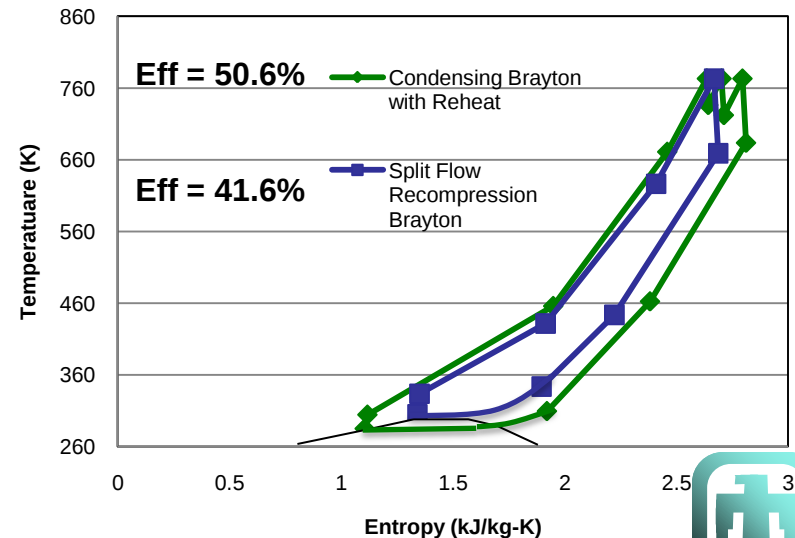
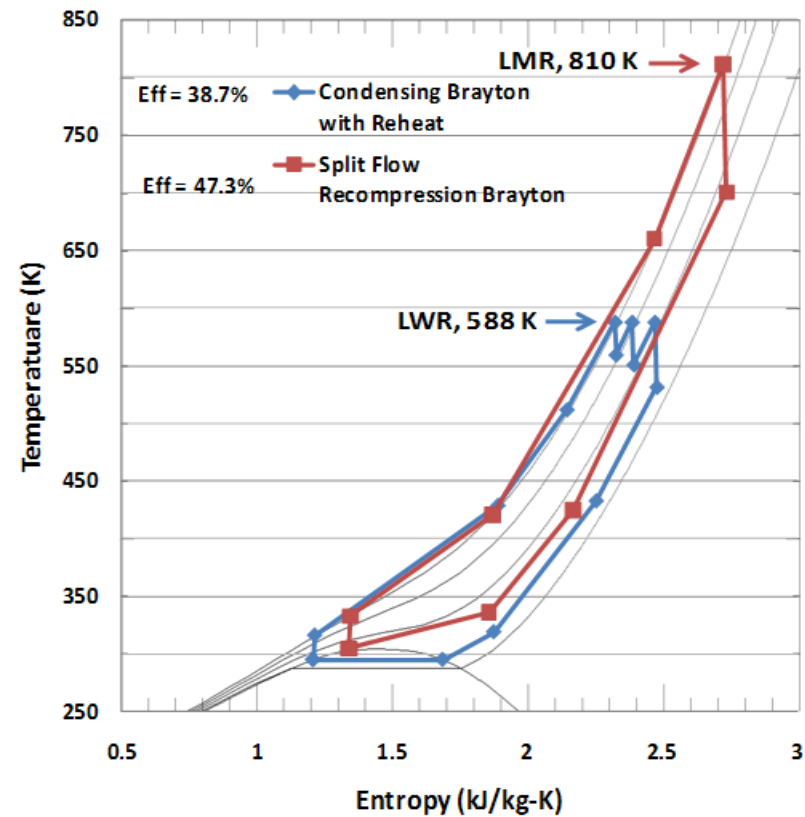
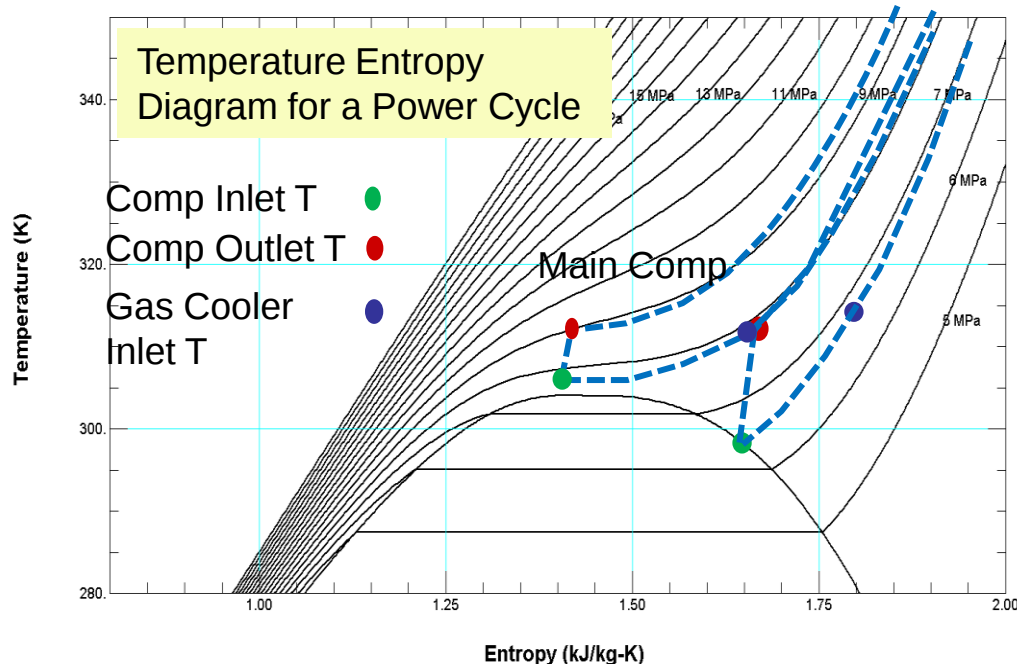


Condensation

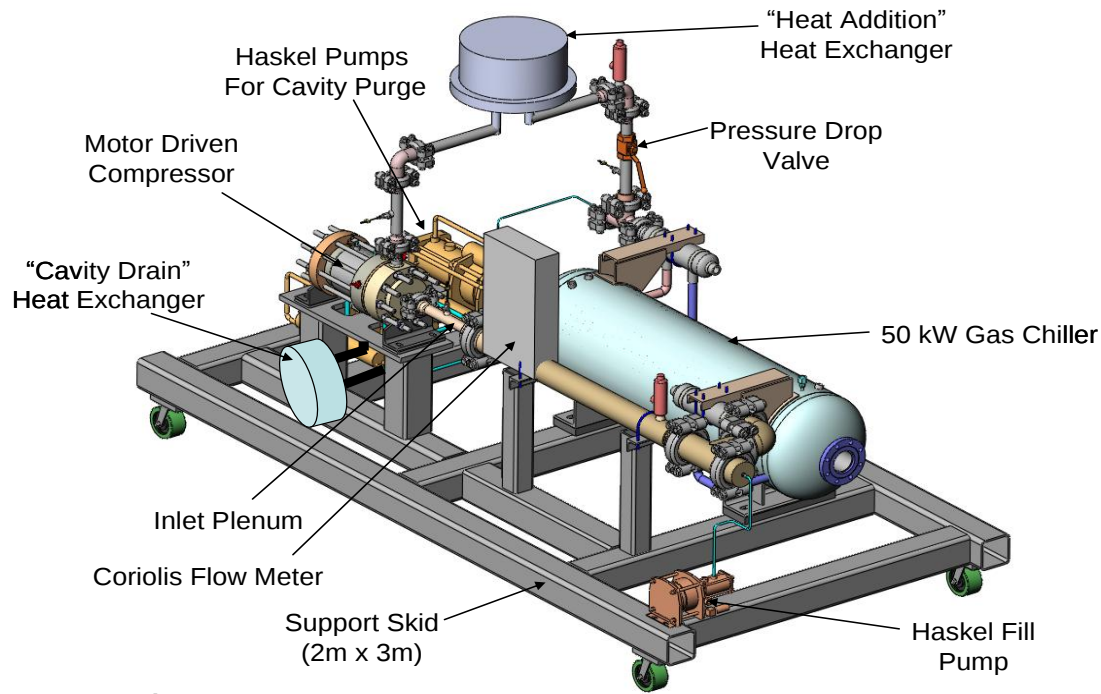


Condensation Motivation

- At Sandia, ongoing research into analysis of advanced S-CO₂ power cycles:
 - reheat, condensing, intercooling, etc.
- This will require compressor and chiller operation in a variety of new, unproven operating regimes
- Experimental tests have been performed to verify performance under these conditions



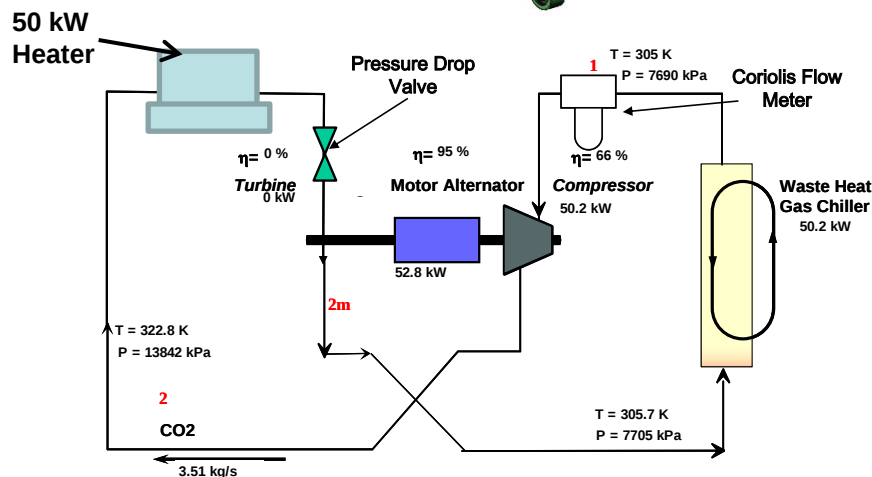
Test Equipment



- Tests used the Sandia S-CO₂ compression loop, which consists of a compressor, heater, flow control valve, and chiller.

- Instrumented with T,p sensors at 4 key state points, and a density meter at compressor inlet

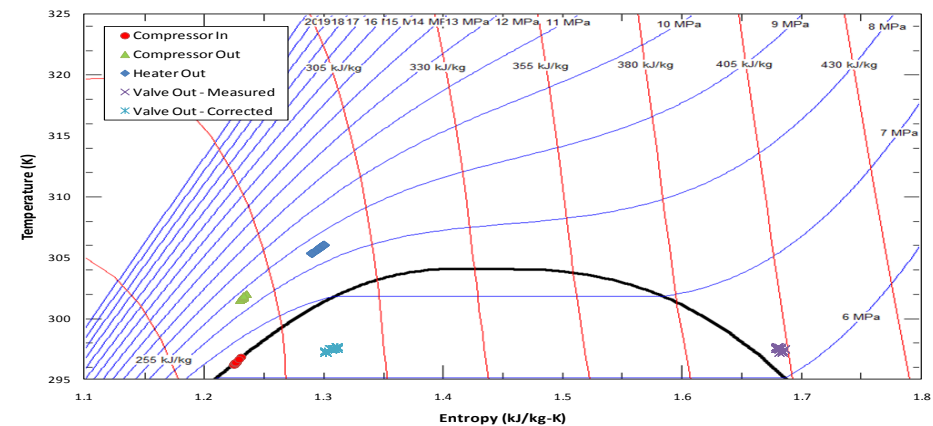
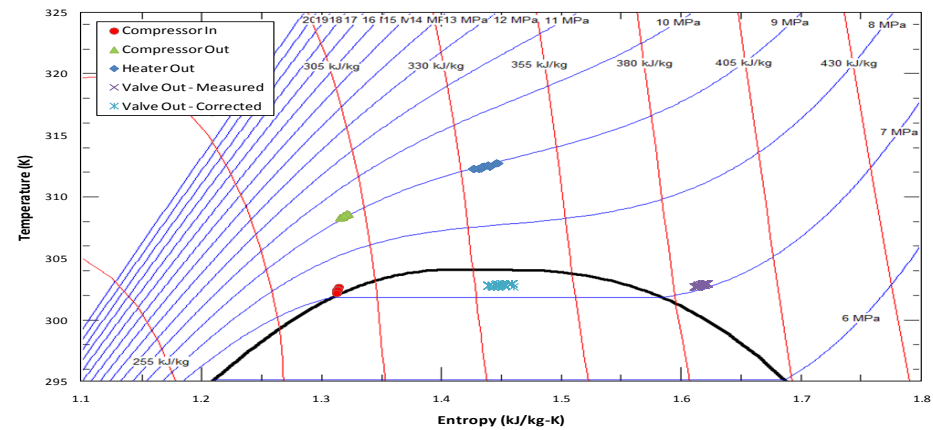
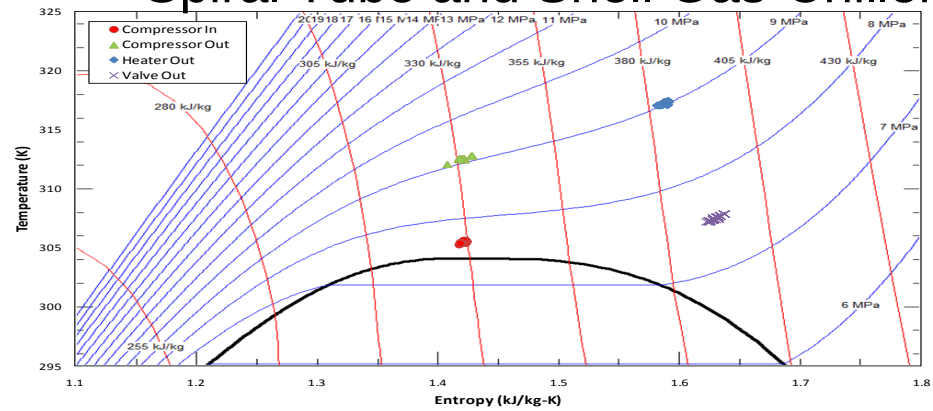
- Previously used for mapping compressor performance at the critical point, bearings & seals R&D, windage tests, etc.





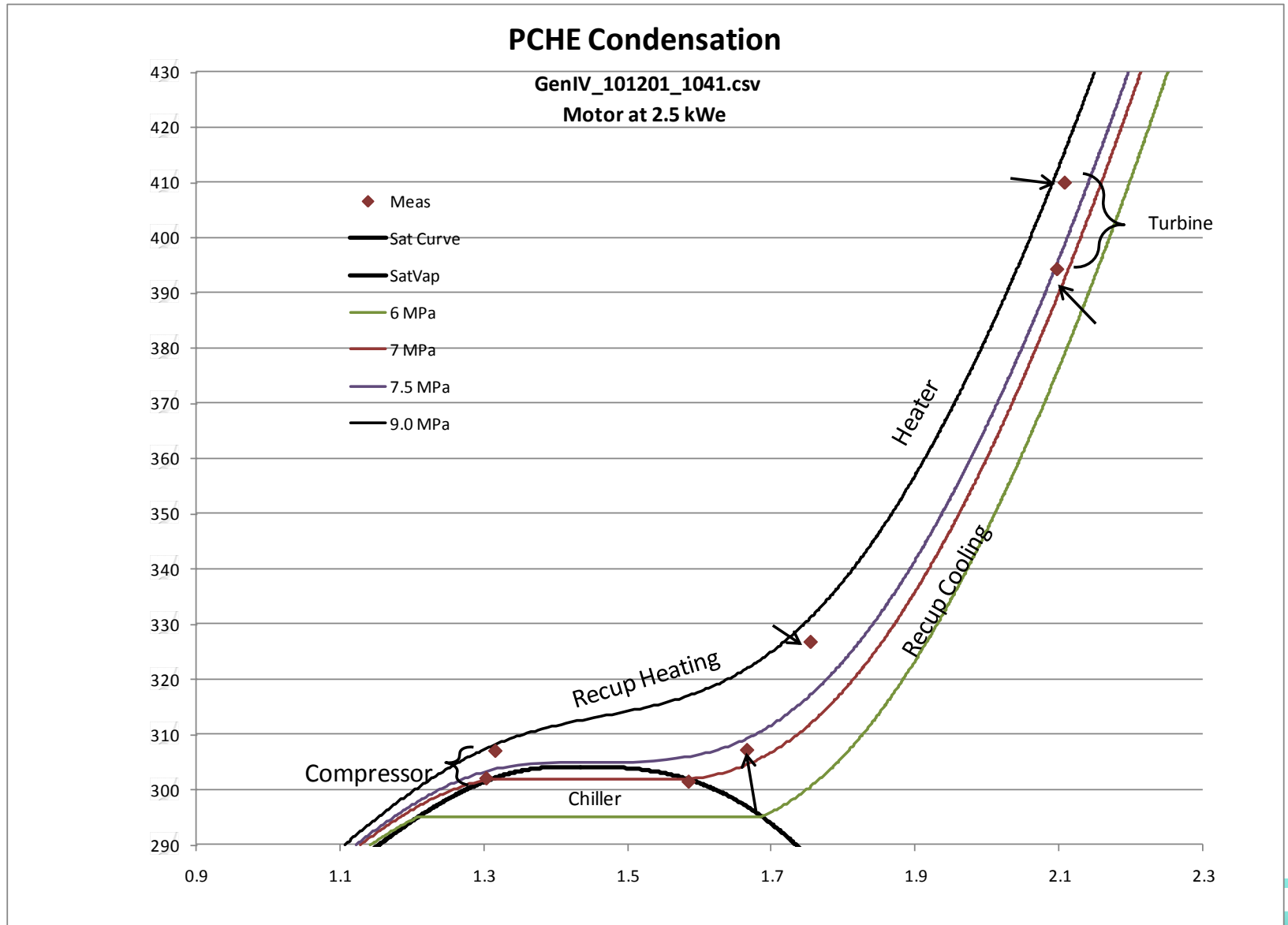
Condensation in Sandia Compression Loop

Spiral Tube and Shell Gas-Chiller



Condensation in Brayton Loop (TAC-A)

PCHE Gas-Chiller





Condensation Conclusions

- Both Tube and Shell and PCHE can be used to condense CO₂
- Significance: Brayton Cycle can improve cycle efficiency by using condensation when environmental conditions permit.
- S-CO₂ Power cycles are not constrained to operate only at the critical point
 - Appears so far that the compressor inlet can be positioned at different T,p to improve efficiency depending on environmental conditions (night, day, summer, winter, latitude).



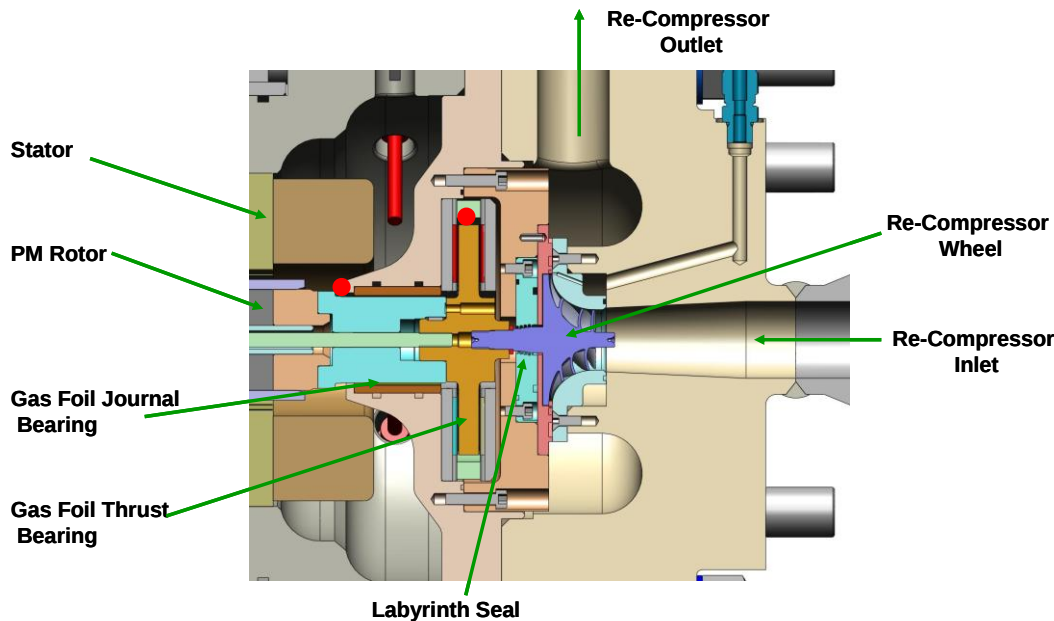


Gas-Foil Bearings



Gas Foil Bearings

$$Pwr = \pi C_d (Re) \rho r_{rotor}^4 \omega^3 L_r$$

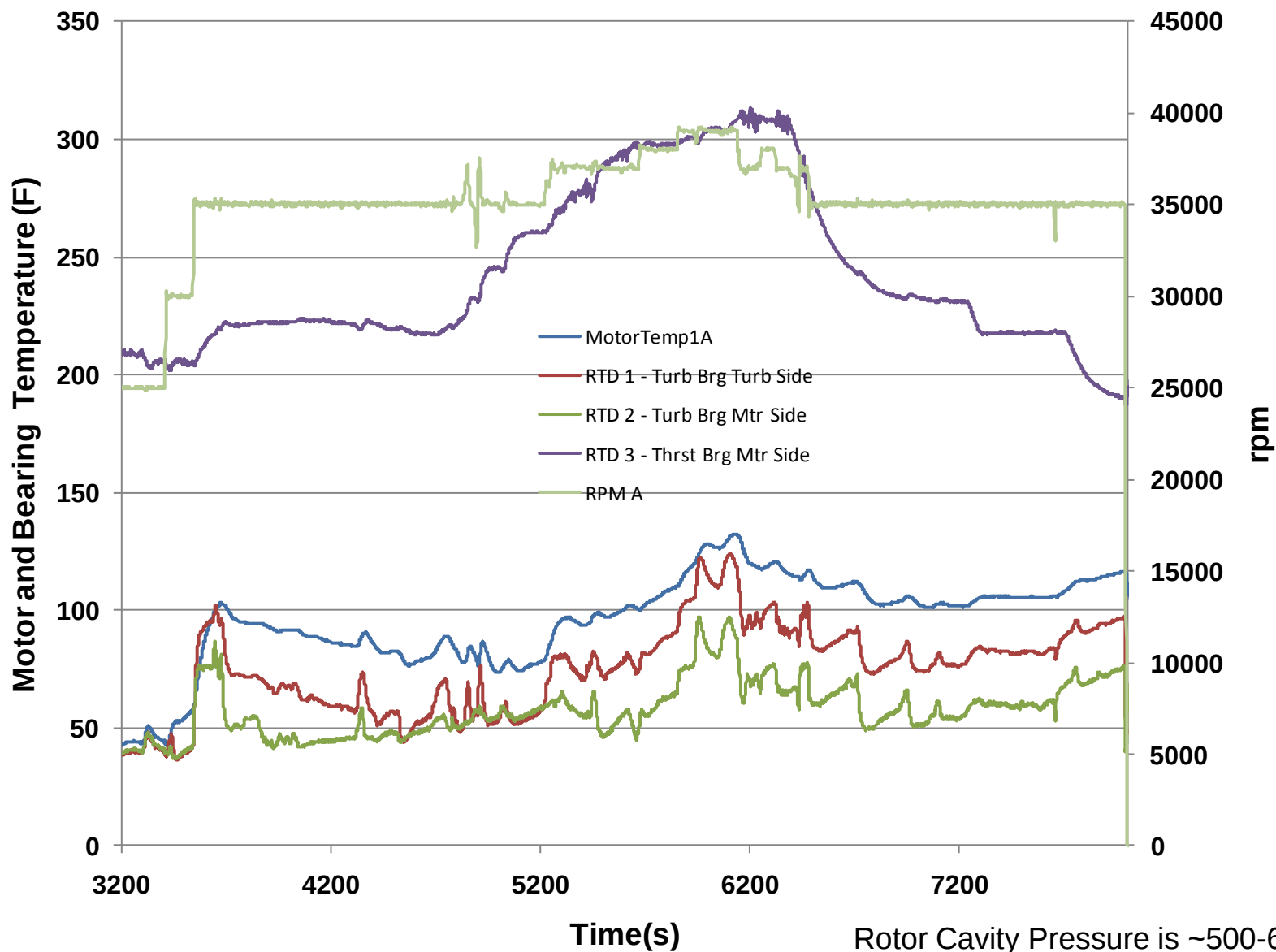


- At near supercritical pressures losses are large
- Strongly sensitive to radius and frequency
 - Penalizes small high speed systems
- Requires reduced rotor cavity pressure
- Model developed for Air and Steam
 - Not supercritical CO₂
 - Model is accurate for S-CO₂



Motor & Bearing Temperatures with RPM : TAC-A

GenIV_101201_1041.csv

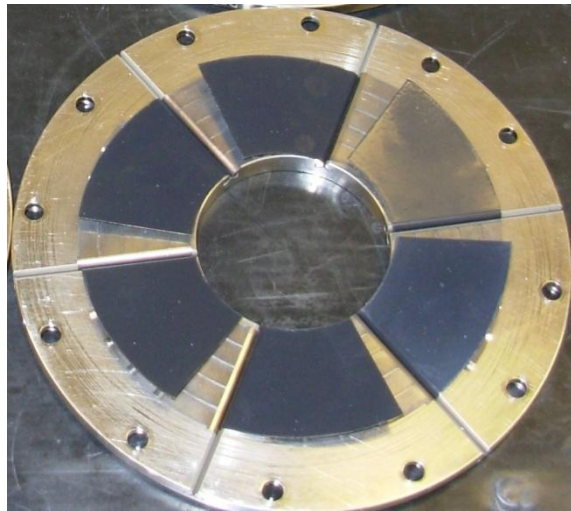




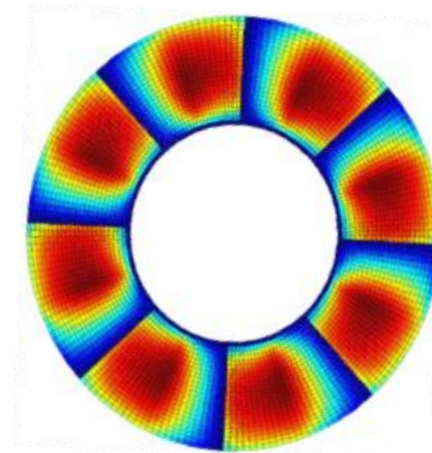
Gas Foil Bearings

Model for Gap Thickness, Power, Heating, Temperature
Tom Conboy

S-CO₂ Gas-Foil Thrust Bearing Pads



Reynolds Model for Pressure Under Pad



- Model is currently for laminar flow.
- Needs upgrade to turbulent to account for real gas
- Effects with high Reynolds numbers
due to high density, high velocity, low viscosity

$$\text{Re} = \frac{\rho v D}{u}$$





Natural Circulation Flow And Decay Heat Removal





Natural Circulation Summary

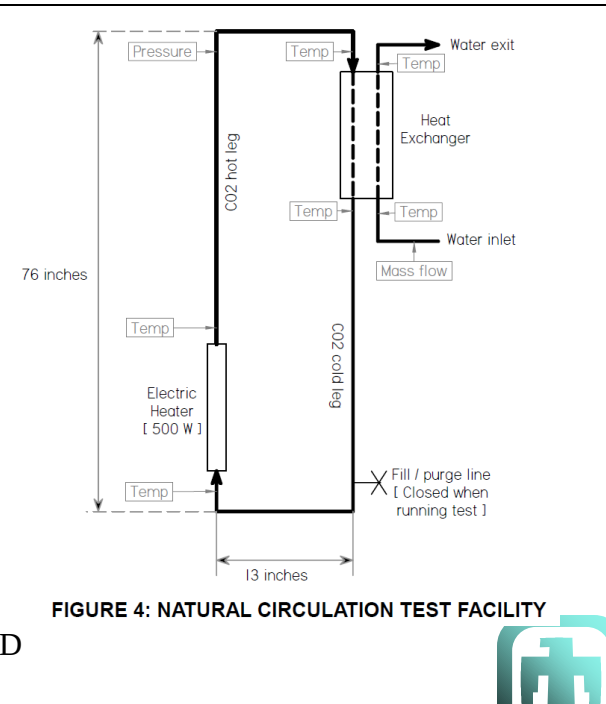
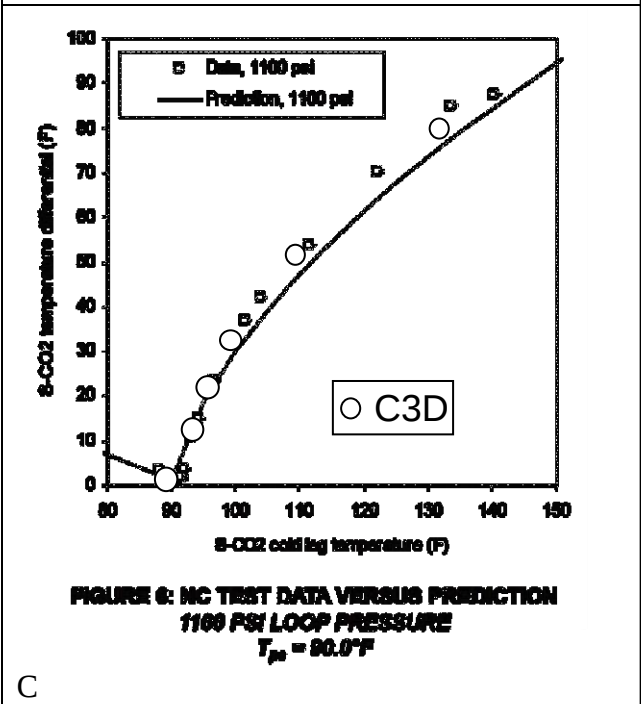
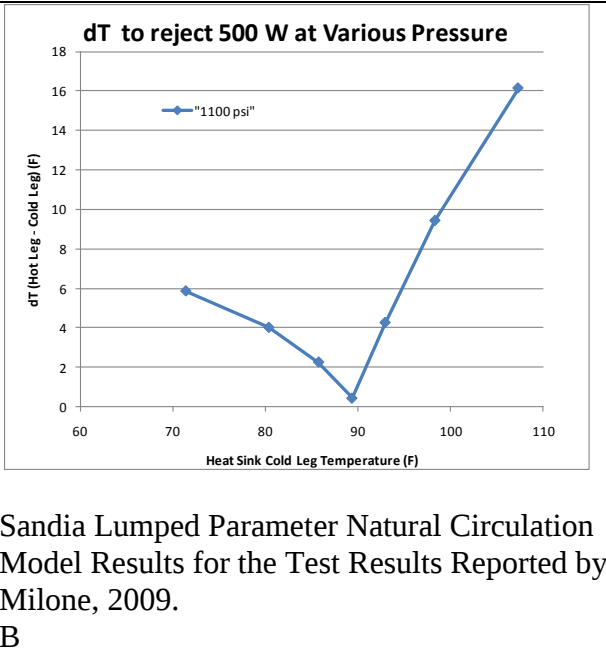
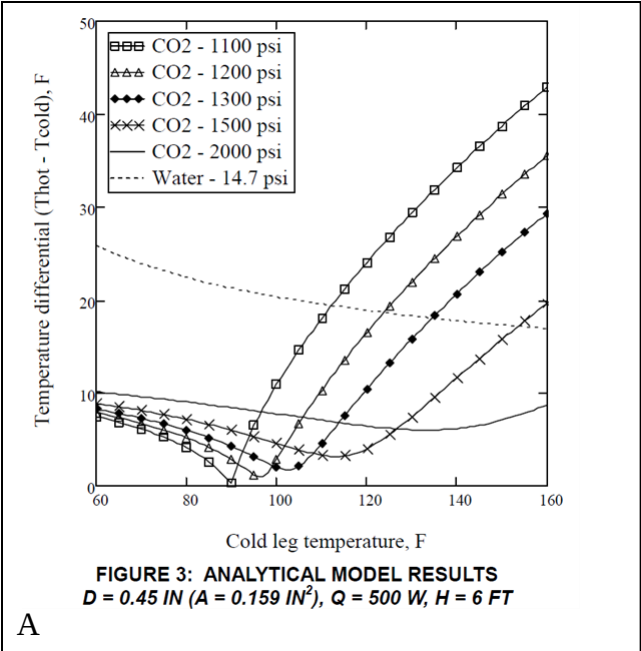
- **Powerful Natural Circulation Forces**
 - Large density changes with small temperature changes near critical point
- **Developed Simple Scoping Calculation Models in Excel**
 - Based on theory described by D. Milone
 - Validated against experiments in a 1/2" OD Loop 72" Tall
- **Modified Scoping Model to Apply it to**
 - Reactors, Heat Exchangers, Gas-Chiller
 - Evaluated Proposed SNL Experiment
- **Developed a 3 D CFD model by modifying a fire code C3D**
 - Implement Nist Calls
 - Modified Energy Equation to use Enthalpy
 - Verified against D. Milone Report
 - Explored Natural Circ in Rx, with HXs and with Gas Chiller



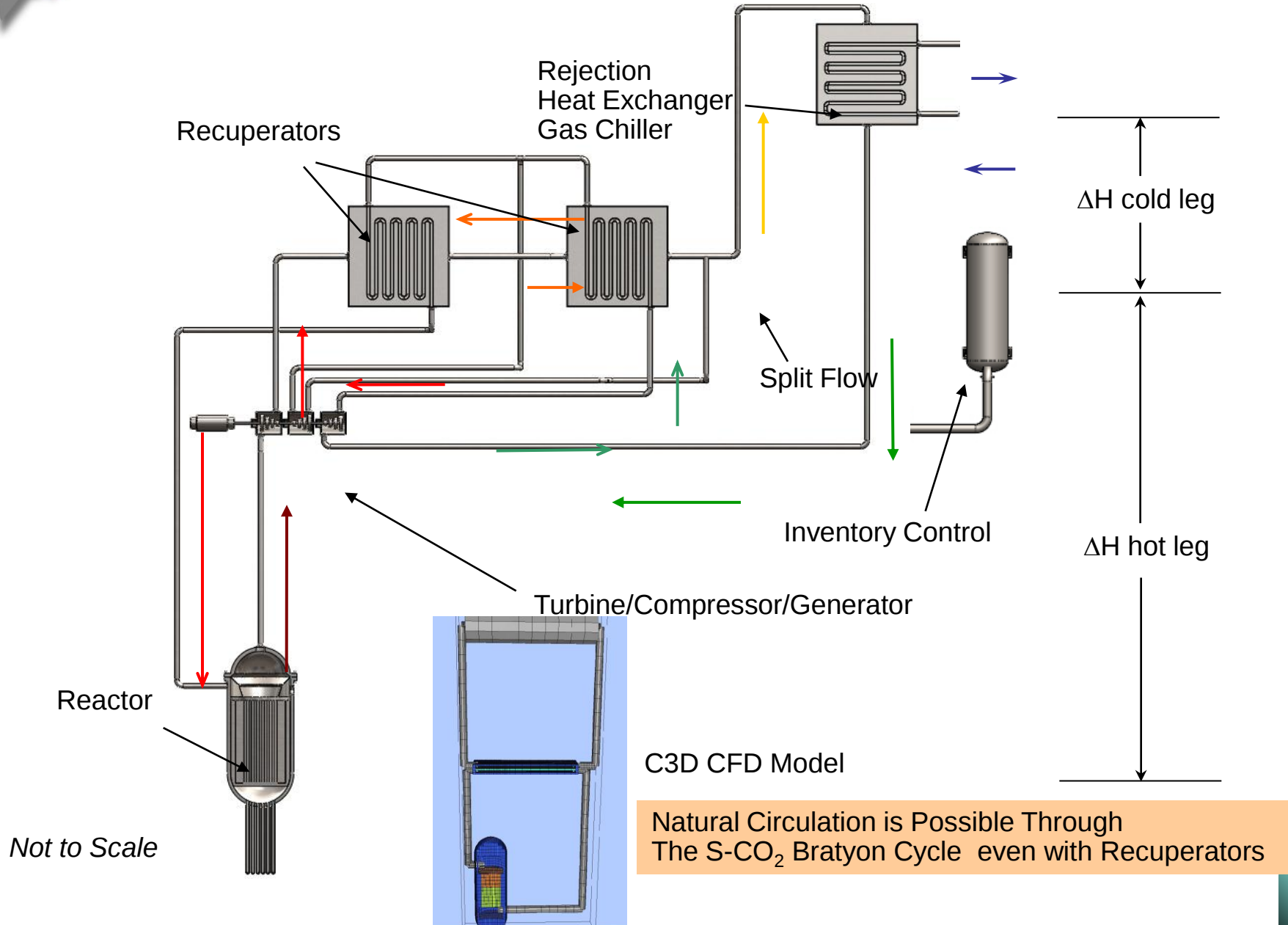


Natural Circulation in S-CO₂ Gas Cooled Fast Reactor (GCFR-CO₂)

- A) Experiment (Milone)
- B) Scoping Model
- C) C3D Model
- D) Geometry

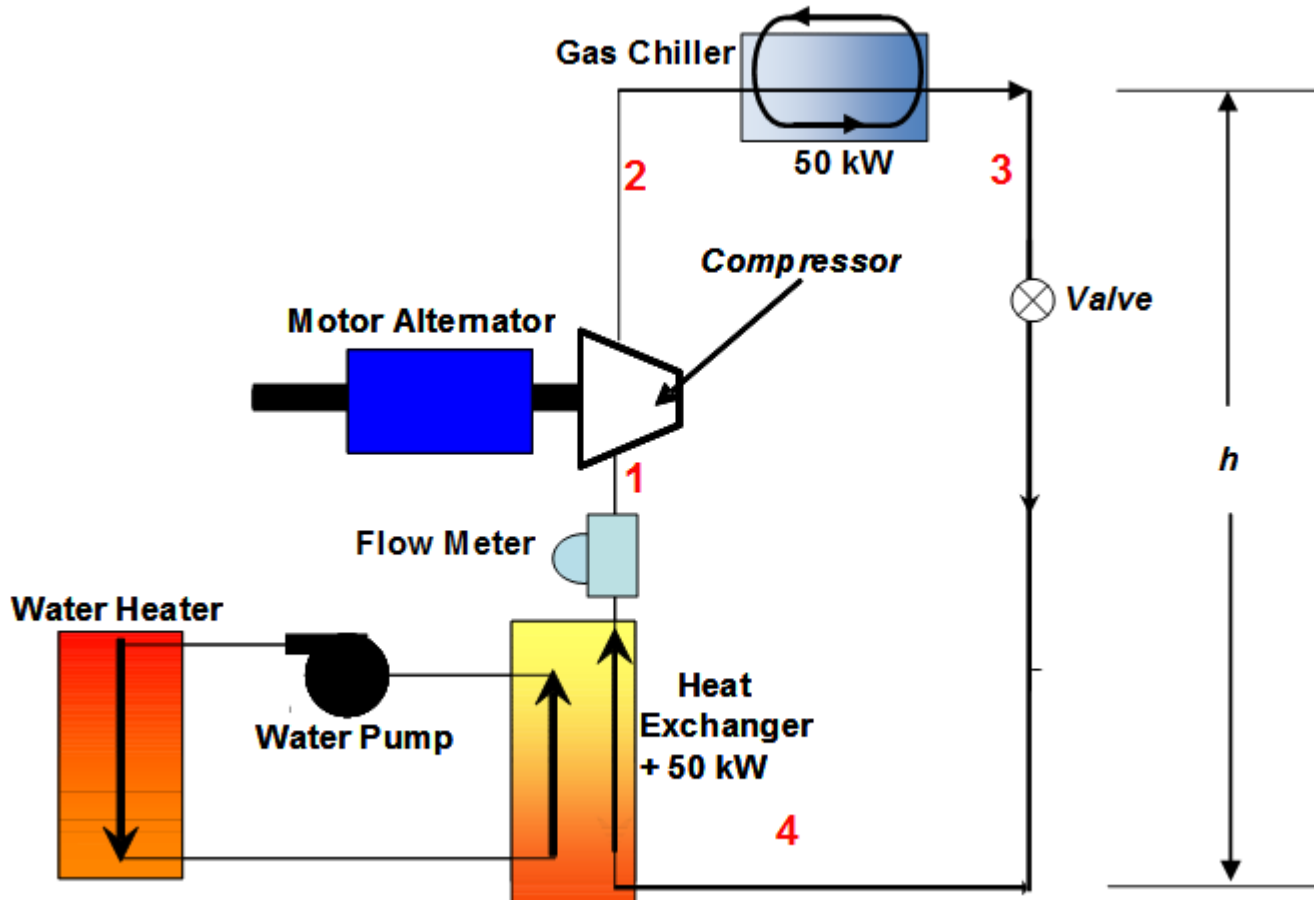


Natural Convection Flow in GFR-SCO2



S-CO₂ Natural Circulation Tests

are planned for Compression Research Loop



Need to Switch the location of the Cooling and Heating
Tests will provide measured data at high power levels 20-50 kW
in complicated Geometries





Conclusions

- S-CO₂ Power Conversion Systems
 - Smaller, Simpler, As/more Efficient Than Existing Gas or Steam Power Systems in the (500-525 C) temperature range
 - Better Materials Compatibility
 - Can be built with existing technologies
 - Models of System and Component Performance are Accurate
 - Growth Potential (performance exceeds existing technologies)
 - Higher Temperatures (750 C) >50% Efficiency
 - Smaller
 - Fluid Mixtures to modify supercritical properties to higher or lower temperatures
 - PCHE and Tube and Shell HXs can be operated in the condensing mode with no changes
 - Inter-cooling with higher pressure ratios (small size means easier to implement)
 - IC allows for Higher Pressure systems to increase efficiency
 - Re-heat is an effective way to increase efficiency
 - Higher Temperature Ability and Smaller Size
 - Cost competitive higher efficiency power systems for all heat sources
 - Advanced cycles may increase SMR efficiency to 38% for LWR and 50 % for LMRs with a simpler and smaller plant
 - Useful for all heat sources (Nuclear, Solar, Fossil, Geothermal)
 - Numerous early non-nuclear Products (Marine, Fossil, Solar)
 - Can improve the economics of nuclear systems
 - Dry Cooling is Possible

