



Shock testing accelerometers with a Hopkinson pressure bar

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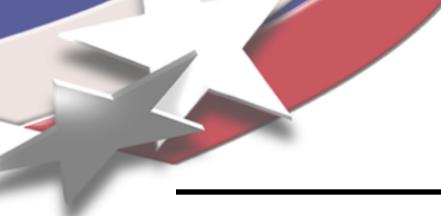
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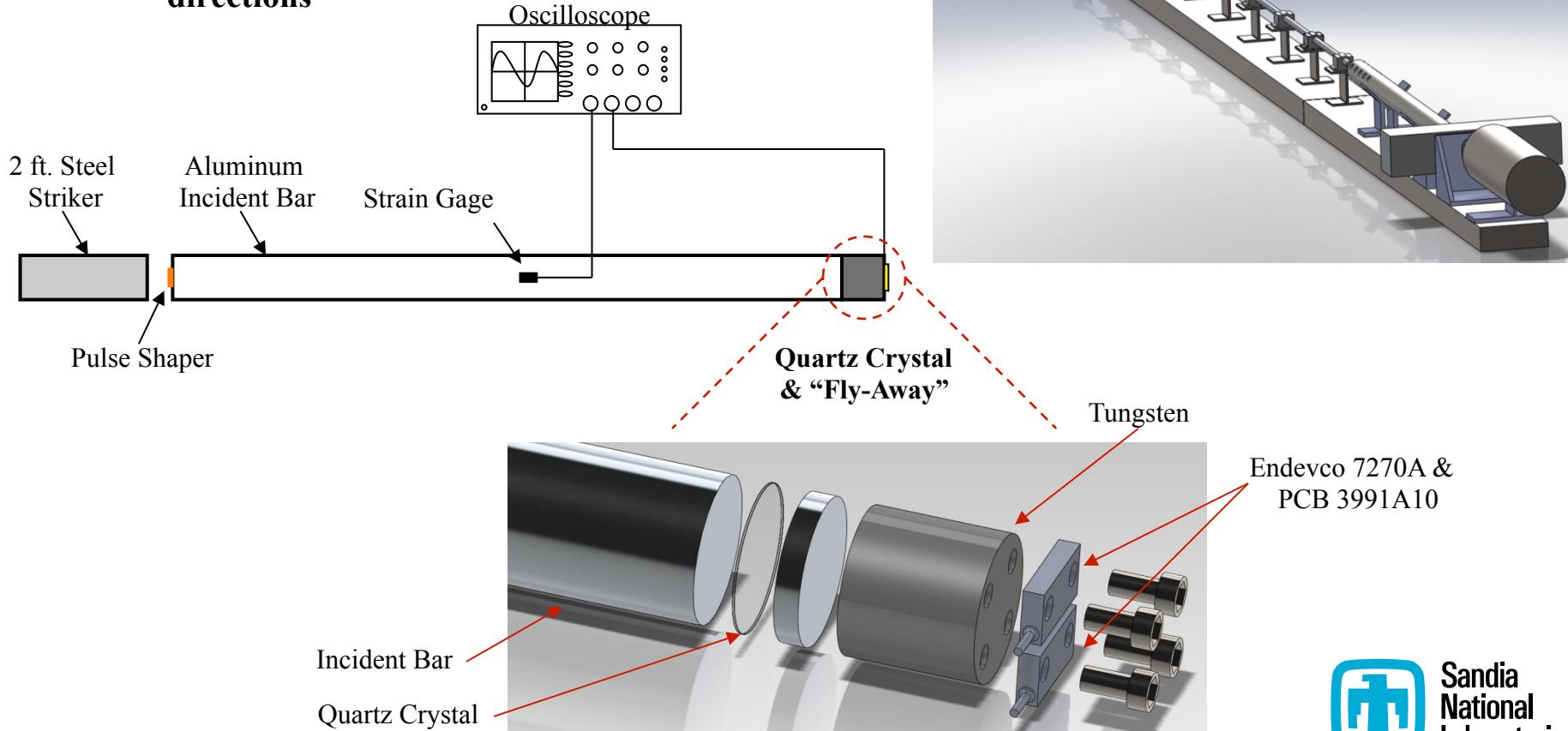
Outline

- **Overview of experimental apparatus**
- **Models utilized in design of experiments**
- **Model comparisons and results**

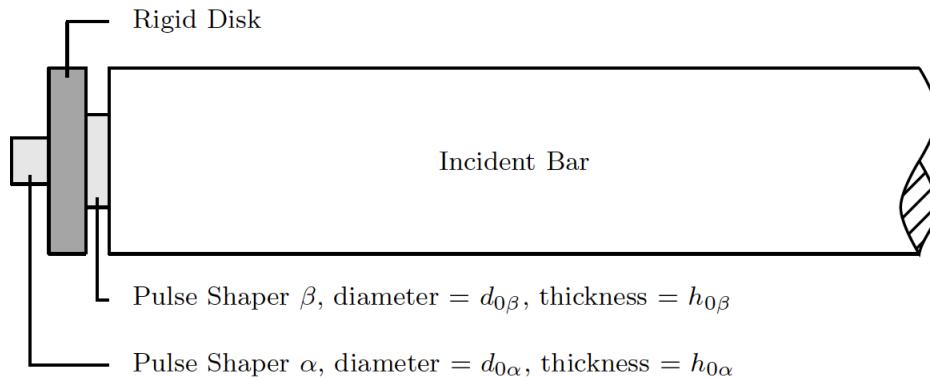


Experimental Apparatus

- Utilize “fly-away” method of characterization
 - Controlled pulse shaping
 - Single pulse loading
 - Evaluation in axial and transverse directions



Pulse Shaping



Nonlinear ODE

$$\frac{h_{0\alpha}}{V} \dot{\varepsilon}_\alpha(t) = 1 - K \left(\frac{1}{\rho c} + \frac{1}{\rho_{st} c_{st}} \right) \frac{f [\varepsilon_\alpha(t)]}{1 - \varepsilon_\alpha(t)} - \frac{2K}{\rho_{st} c_{st}} \left\{ \frac{f [\varepsilon_\alpha(t - \tau)]}{1 - \varepsilon_\alpha(t - \tau)} + \frac{f [\varepsilon_\alpha(t - 2\tau)]}{1 - \varepsilon_\alpha(t - 2\tau)} + \dots + \frac{f [\varepsilon_\alpha(t - n\tau)]}{1 - \varepsilon_\alpha(t - n\tau)} \right\} - \frac{h_{0\beta}}{V} \dot{\varepsilon}_\beta(t),$$

$$n\tau \leq t < (n+1)\tau,$$

$$K = \frac{\sigma_{0\alpha} a_{0\alpha}}{AV}$$

Algebraic Constraint

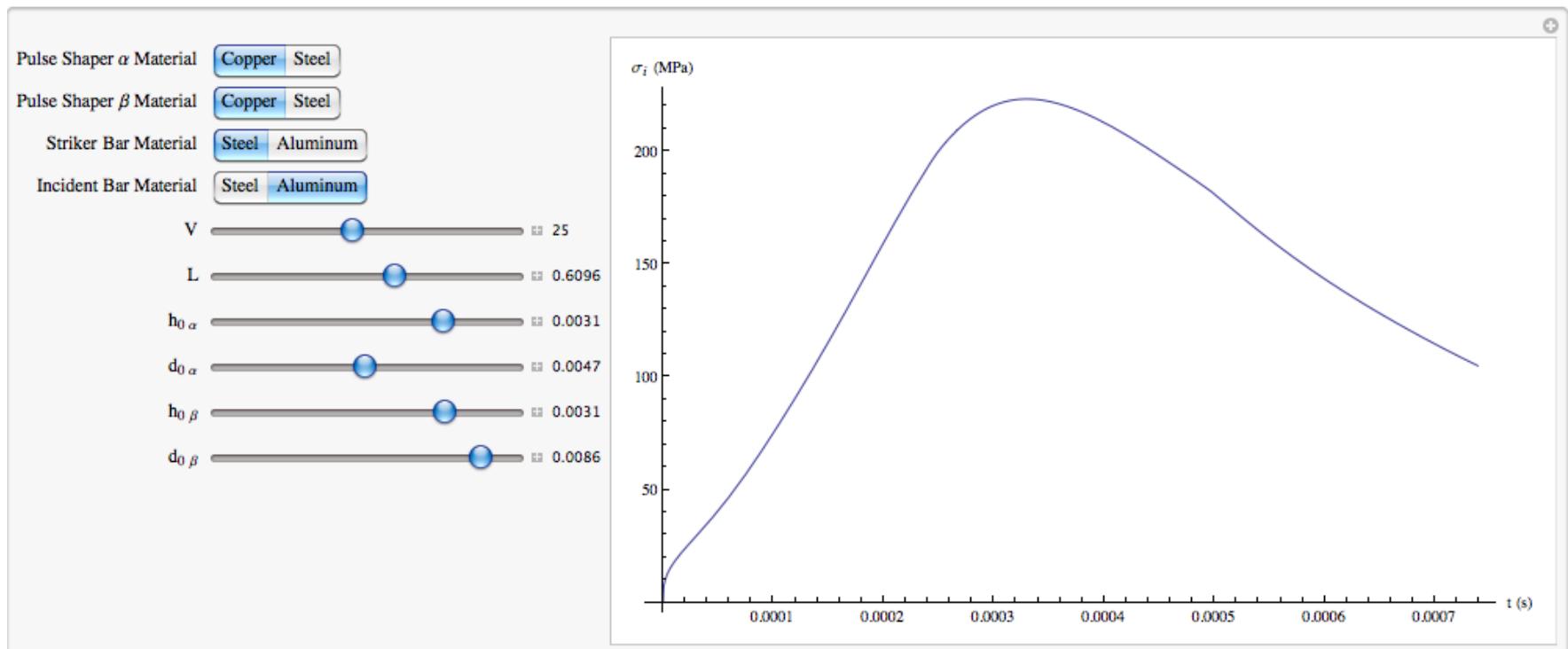
$$\frac{g [\varepsilon_\beta(t)]}{1 - \varepsilon_\beta(t)} = \frac{a_{0\alpha}}{a_{0\beta}} \frac{\sigma_{0\alpha} f [\varepsilon_\alpha(t)]}{\sigma_{0\beta} (1 - \varepsilon_\alpha)},$$

Response functions

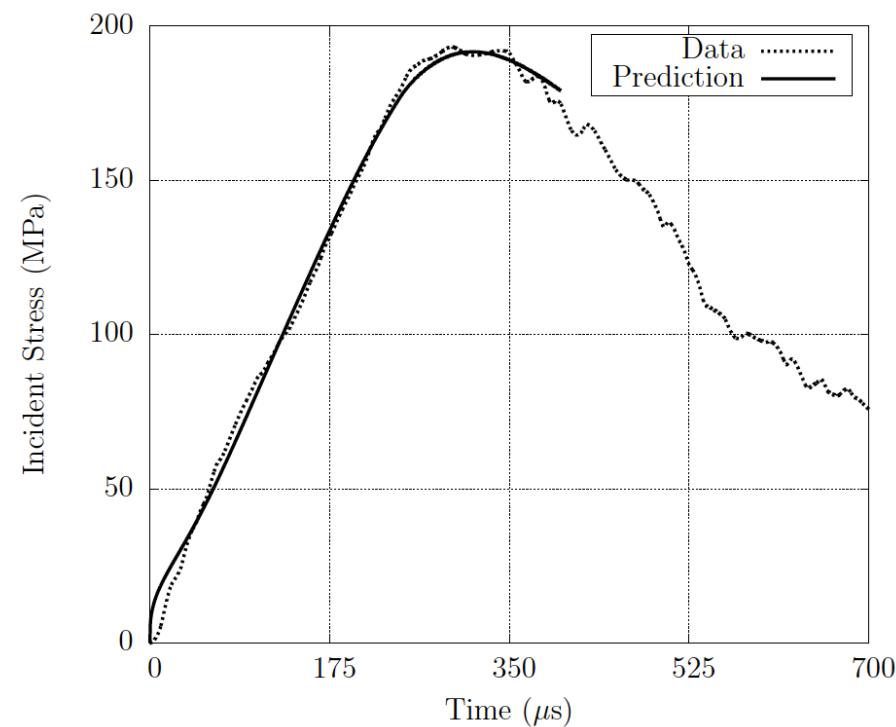
$$f [\varepsilon_\alpha(t)] = \frac{\varepsilon_\alpha(t)^n}{1 - \varepsilon_\alpha(t)^m}, \quad g [\varepsilon_\beta(t)] = \frac{\varepsilon_\beta(t)^k}{1 - \varepsilon_\beta(t)^j},$$

System of equations is solved with implicit time integration scheme to predict incident stress

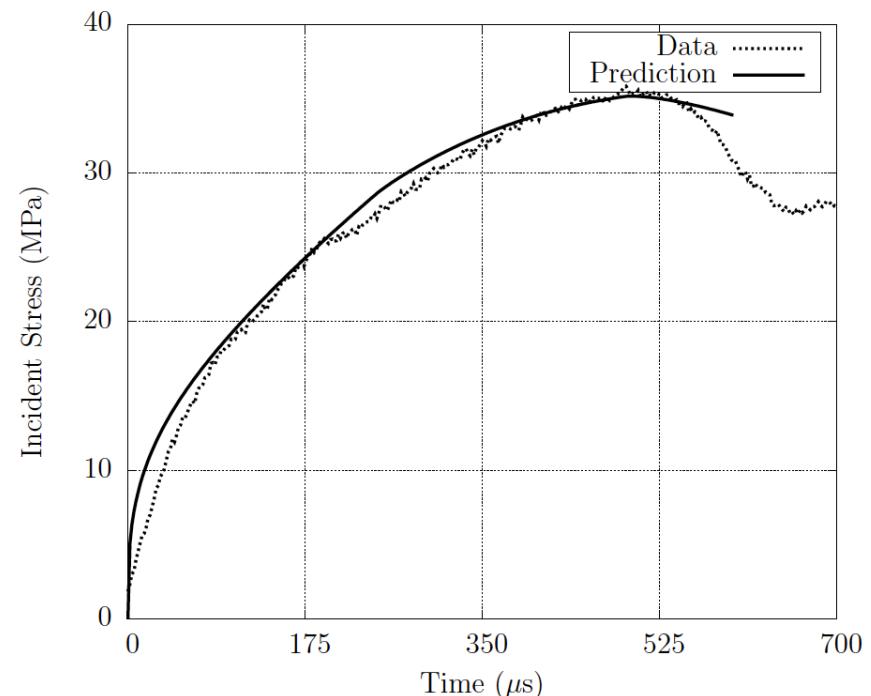
Pulse Shaper Design Code



Pulse Shaping Model Comparison



$$V \approx 20 \text{ m/s}$$



$$V \approx 7 \text{ m/s}$$

Rigid Body Model

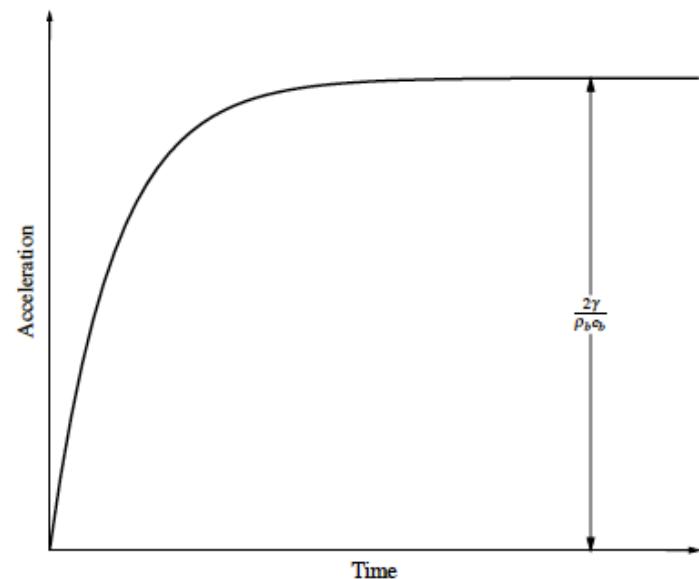
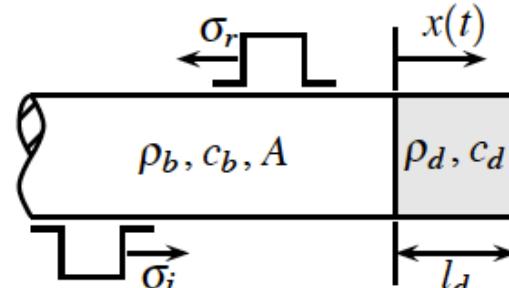
$$A(\sigma_r + \sigma_i) = A\rho_d l_d \ddot{x}(t) \quad (1)$$

$$\sigma_i - \sigma_r = \rho_b c_b \dot{x}(t) \quad (2)$$

Combining (1) & (2) by eliminating σ_r , yields:

$$\rho_d l_d \ddot{x}(t) + \rho_b c_b \dot{x}(t) = 2\sigma_i \quad (3)$$

Let $\sigma_i = \gamma t$, where γ is a constant incident stress rate and solve (3).



Wave analysis



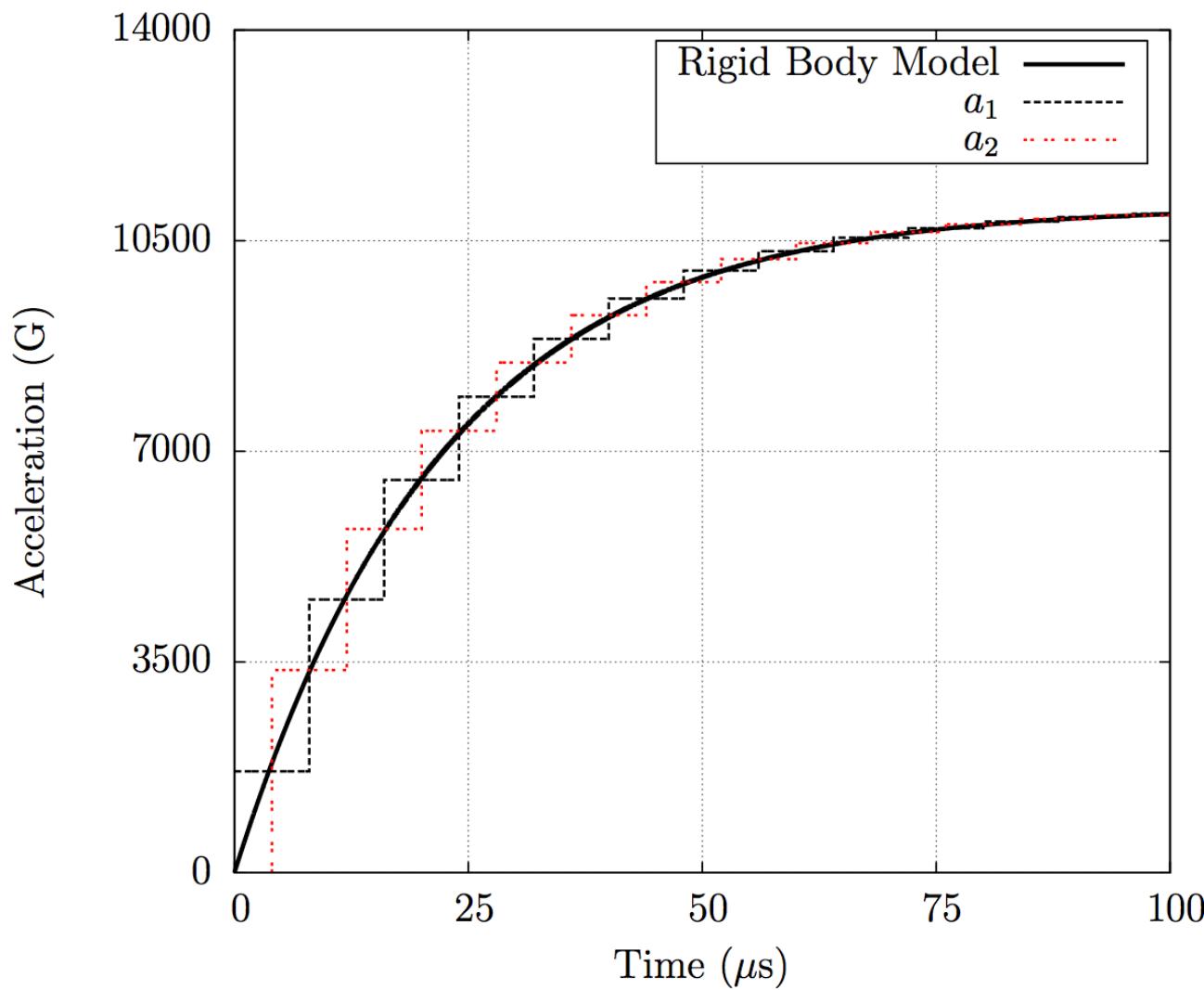
$$a_1(t) = \begin{cases} \frac{2r}{\rho_b c_b (1+r)} \frac{d\sigma_i(t)}{dt} & 0 \leq t < 2t_0 \\ \frac{2r}{\rho_b c_b (1+r)} \left\{ \frac{d\sigma_i(t)}{dt} + \left[1 + \frac{1-r}{1+r} \right] \frac{d\sigma_i(t-2t_0)}{dt} \right\} \\ \vdots \\ \frac{2r}{\rho_b c_b (1+r)} \left\{ \frac{d\sigma_i(t)}{dt} + \cdots + \left[\left(\frac{1-r}{1+r} \right)^{\frac{n-2}{2}} + \left(\frac{1-r}{1+r} \right)^{\frac{n}{2}} \right] \frac{d\sigma_i(t-nt_0)}{dt} \right\} & (n-2)t_0 \leq t < nt_0 \end{cases}$$

For even n , where $t_0 = l_d/c_d$, $r = \frac{\rho_b c_b}{\rho_d c_d}$

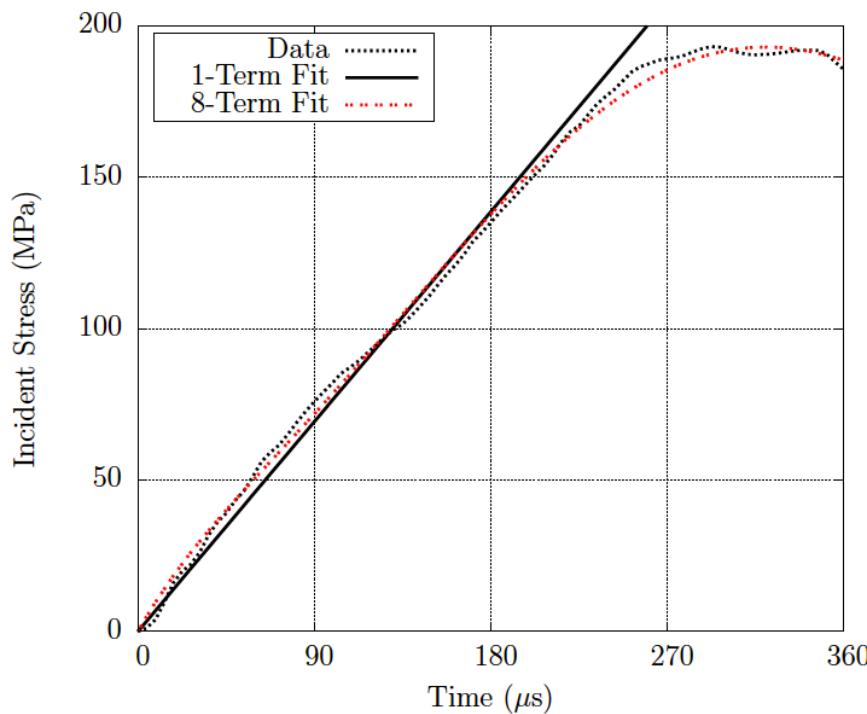
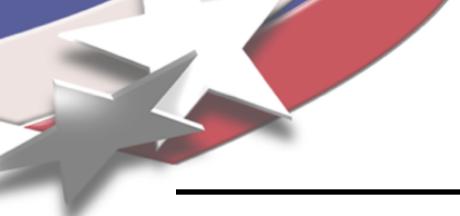
$$a_2(t) = \begin{cases} 0 & 0 \leq t < t_0 \\ \frac{4r}{\rho_b c_b (1+r)} \frac{d\sigma_i(t-t_0)}{dt} & t_0 \leq t < 3t_0 \\ \vdots \\ \frac{4r}{\rho_b c_b (1+r)} \left\{ \frac{d\sigma_i(t-t_0)}{dt} + \cdots + \left(\frac{1-r}{1+r} \right)^{\frac{n-1}{2}} \frac{d\sigma_i(t-nt_0)}{dt} \right\} & (n-2)t_0 \leq t < nt_0 \end{cases}$$

For odd n , where $t_0 = l_d/c_d$, $r = \frac{\rho_b c_b}{\rho_d c_d}$

Wave analysis of tungsten disk response to ramp loading

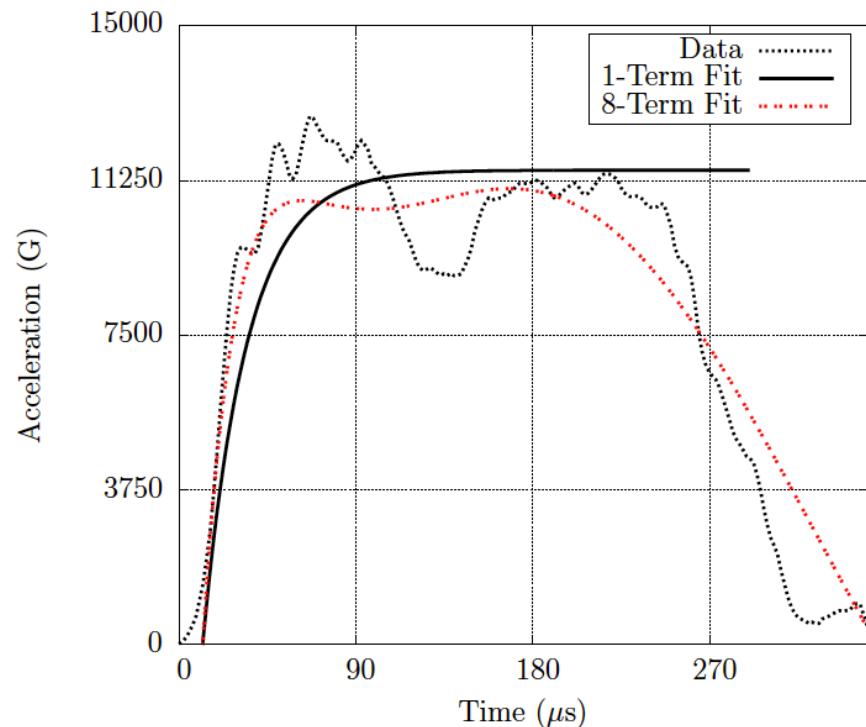


Model for $V = 7 \text{ m/s}$



$$\sigma_i = \gamma_1 t + \gamma_2 t^2 + \dots + \gamma_N t^N$$

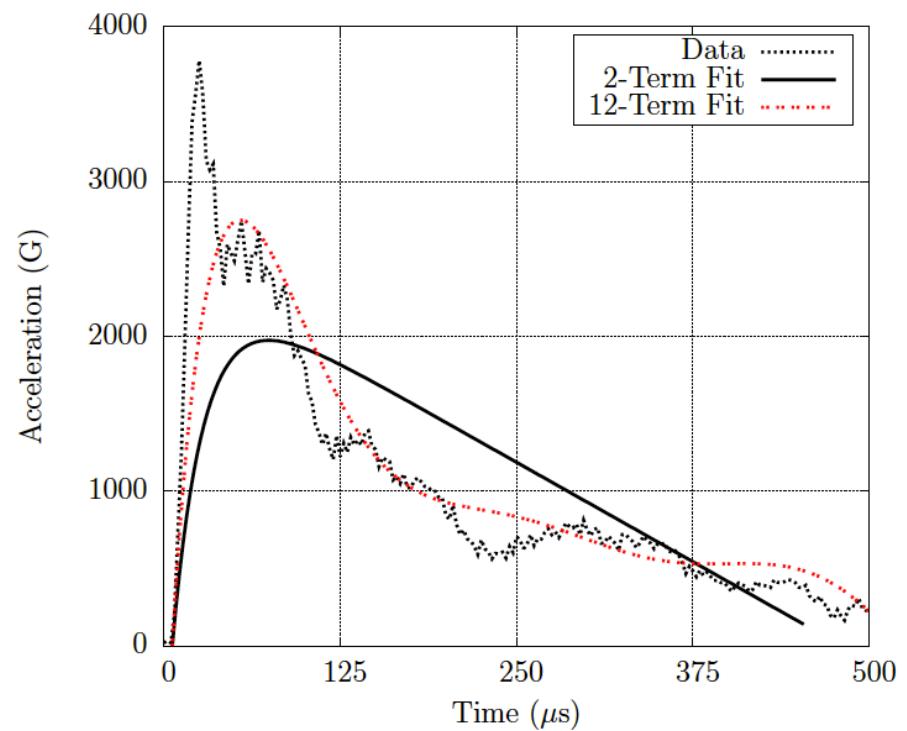
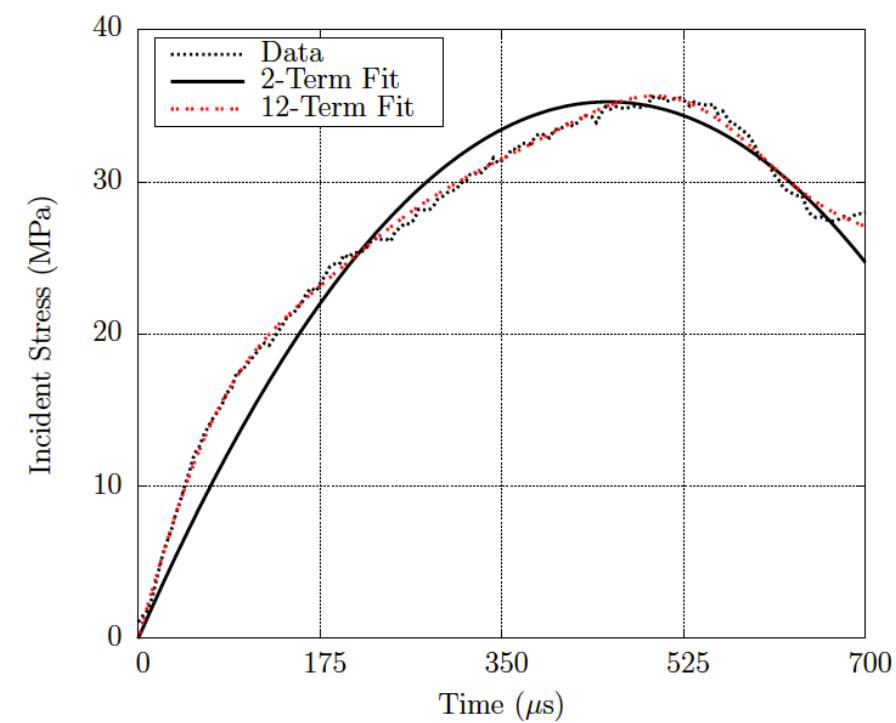
N-term model



$$a(t) = \sum_{n=1}^N \left[(-1)^{n-1} \frac{2n! \gamma_n}{\rho c \lambda^{n-1}} (1 - e^{-\lambda t}) \right] + \sum_{m=1}^N \sum_{n=1}^{m-1} \left[(-1)^{n+m-1} \frac{2m! \gamma_m}{n! \rho c \lambda^{m-n-1}} t^n \right]$$

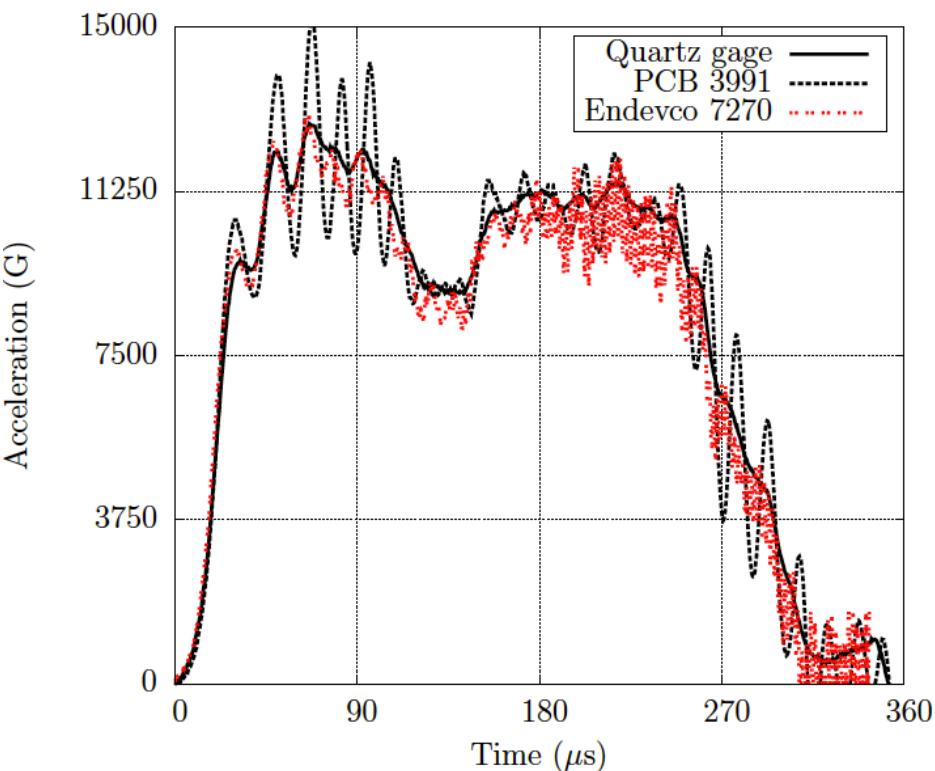


Model for $V = 20 \text{ m/s}$

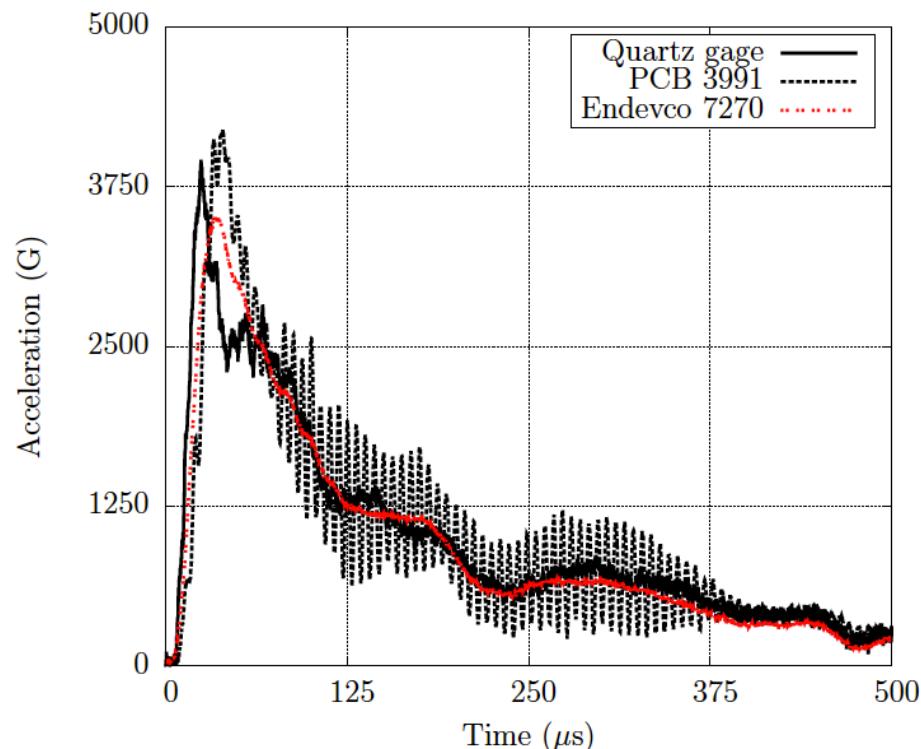




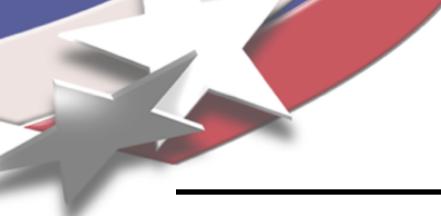
Acceleration Measurements



$$V \approx 20 \text{ m/s}$$



$$V \approx 7 \text{ m/s}$$



Summary

- Presented pulse shaping techniques for extending loading duration of incident stress pulses
- Presented both rigid body and wave mechanics models for predicting the acceleration of the “fly-away” disk given an incident stress pulse
- Comparison of models to experimental measurements from quartz stress gage and two accelerometers are in good agreement.