



# **Shock testing accelerometers with a Hopkinson pressure bar**

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SAND2011-4154C

## **2011 SEM Conference & Exposition on Experimental and Applied Mechanics**

June 16, 2011

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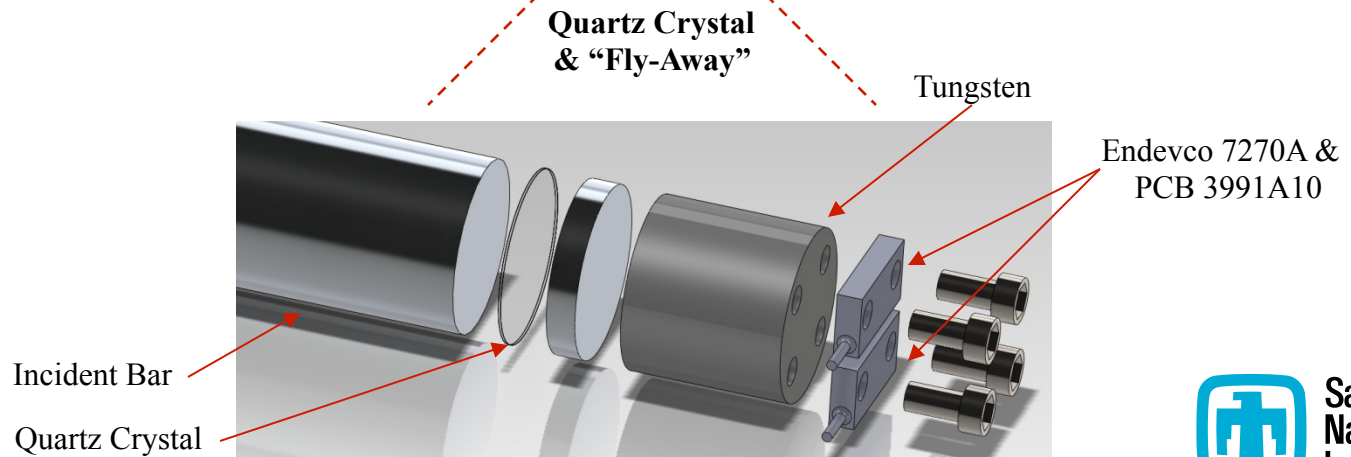
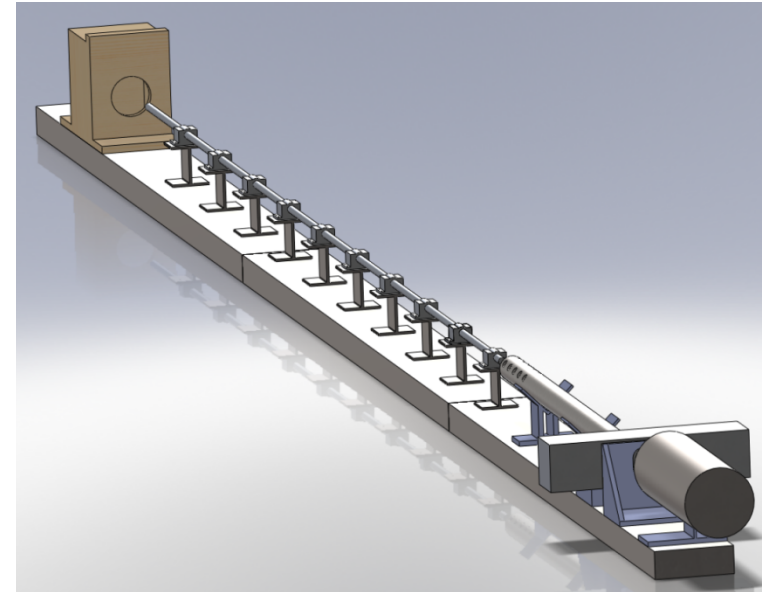
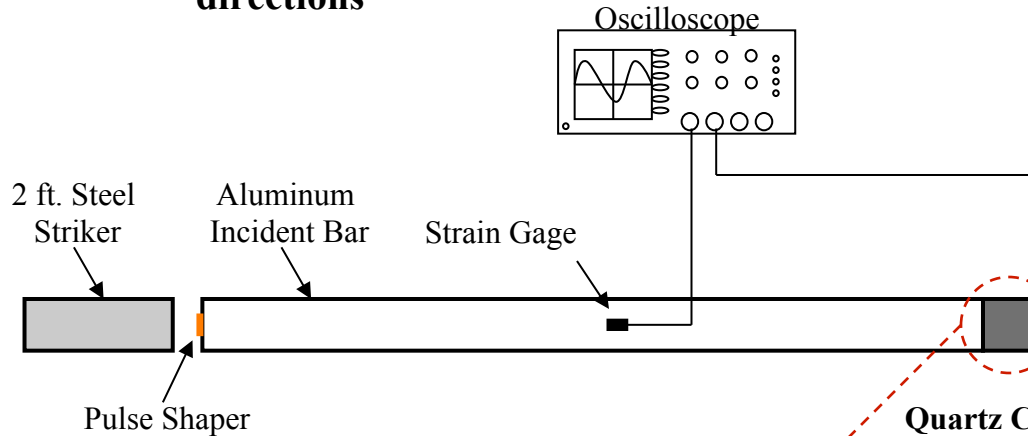
# Outline

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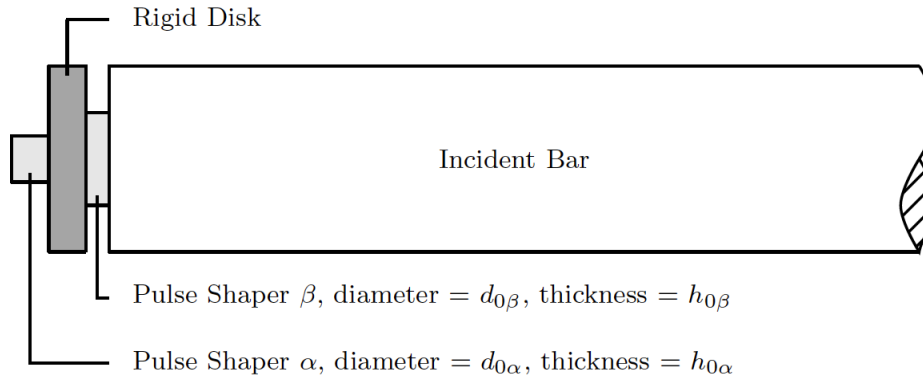
- **Overview of experimental apparatus**
- **Models utilized in design of experiments**
- **Model comparisons and results**

# Experimental Apparatus

- Utilize “fly-away” method of characterization
  - Controlled pulse shaping
  - Single pulse loading
  - Evaluation in axial and transverse directions



# Pulse Shaping



## Nonlinear ODE

$$\frac{h_{0\alpha}}{V} \dot{\varepsilon}_{\alpha}(t) = 1 - K \left( \frac{1}{\rho c} + \frac{1}{\rho_{st} c_{st}} \right) \frac{f[\varepsilon_{\alpha}(t)]}{1 - \varepsilon_{\alpha}(t)} - \frac{2K}{\rho_{st} c_{st}} \left\{ \frac{f[\varepsilon_{\alpha}(t - \tau)]}{1 - \varepsilon_{\alpha}(t - \tau)} + \frac{f[\varepsilon_{\alpha}(t - 2\tau)]}{1 - \varepsilon_{\alpha}(t - 2\tau)} + \dots + \frac{f[\varepsilon_{\alpha}(t - n\tau)]}{1 - \varepsilon_{\alpha}(t - n\tau)} \right\} - \frac{h_{0\beta}}{V} \dot{\varepsilon}_{\beta}(t),$$

$$n\tau \leq t < (n+1)\tau,$$

$$K = \frac{\sigma_{0\alpha} a_{0\alpha}}{AV}$$

## Algebraic Constraint

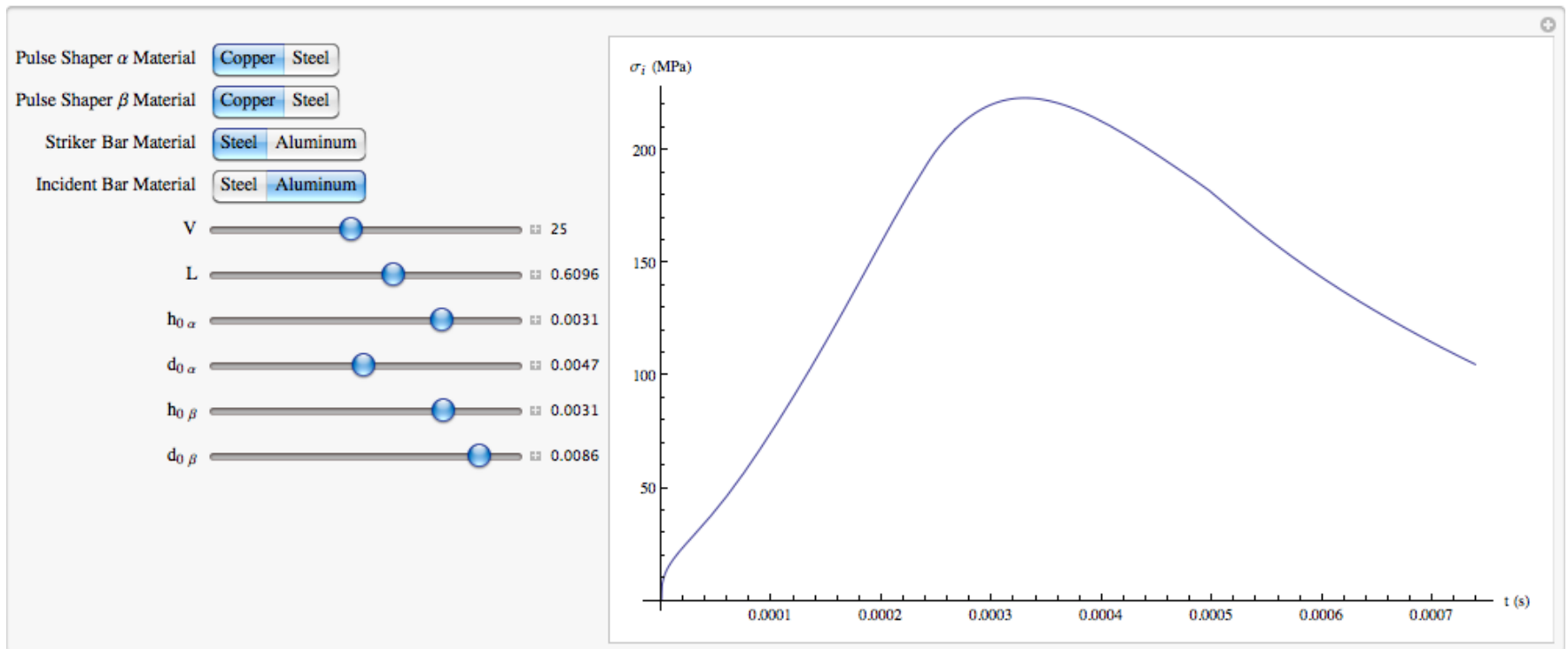
$$\frac{g[\varepsilon_{\beta}(t)]}{1 - \varepsilon_{\beta}(t)} = \frac{a_{0\alpha} \sigma_{0\alpha} f[\varepsilon_{\alpha}(t)]}{a_{0\beta} \sigma_{0\beta} (1 - \varepsilon_{\alpha})},$$

## Response functions

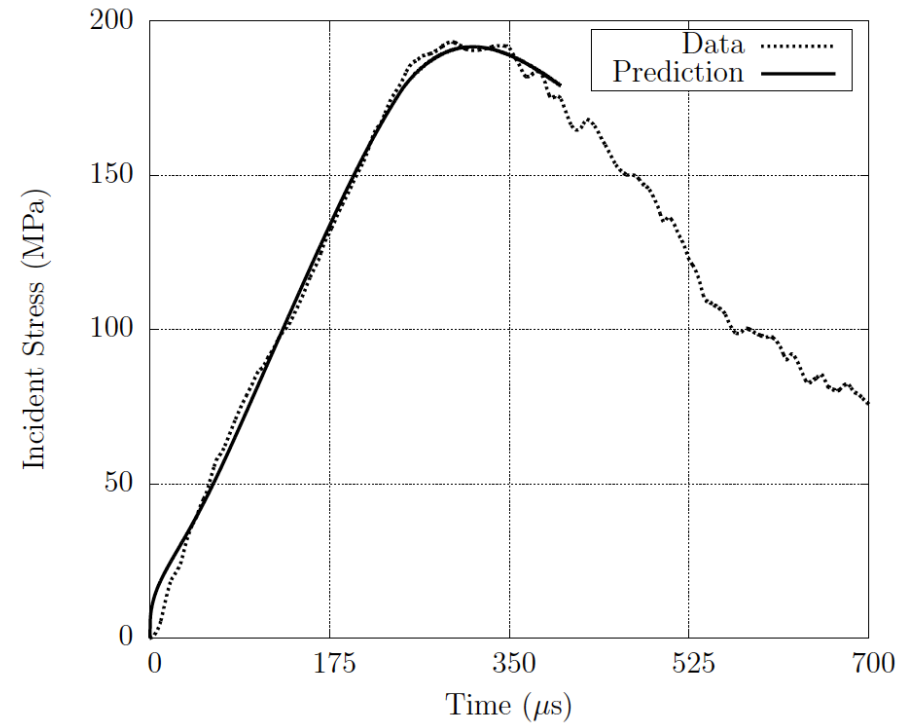
$$f[\varepsilon_{\alpha}(t)] = \frac{\varepsilon_{\alpha}(t)^n}{1 - \varepsilon_{\alpha}(t)^m}, \quad g[\varepsilon_{\beta}(t)] = \frac{\varepsilon_{\beta}(t)^k}{1 - \varepsilon_{\beta}(t)^j},$$

System of equations is solved with implicit time integration scheme to predict incident stress

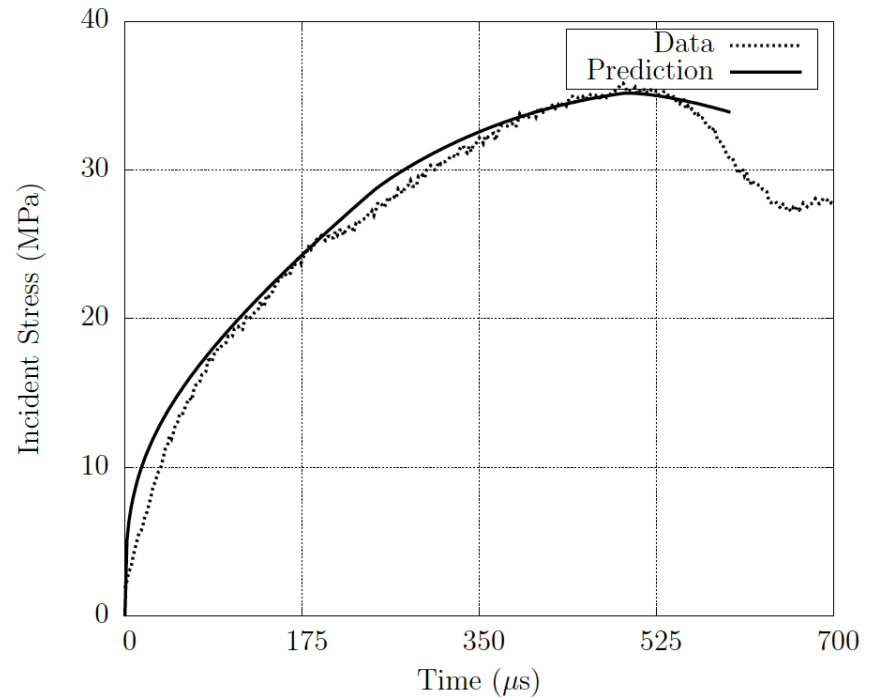
# Pulse Shaper Design Code



# Pulse Shaping Model Comparison



$$V \approx 20 \text{ m/s}$$



$$V \approx 7 \text{ m/s}$$

# Rigid Body Model

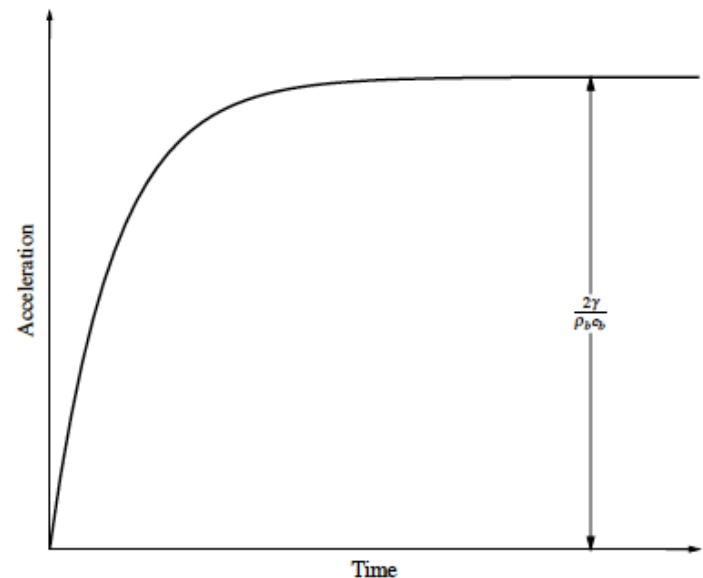
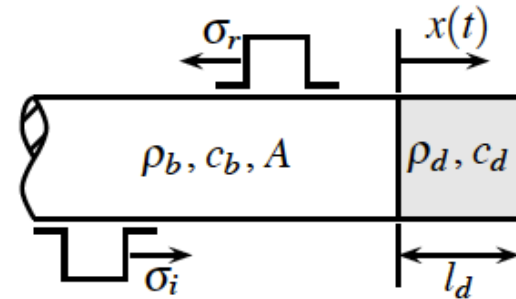
$$A(\sigma_r + \sigma_i) = A\rho_d l_d \ddot{x}(t) \quad (1)$$

$$\sigma_i - \sigma_r = \rho_b c_b \dot{x}(t) \quad (2)$$

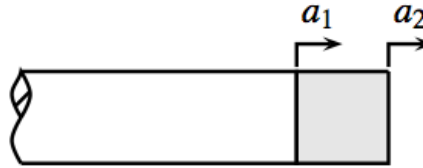
Combining (1) & (2) by eliminating  $\sigma_r$ , yields:

$$\rho_d l_d \ddot{x}(t) + \rho_b c_b \dot{x}(t) = 2\sigma_i \quad (3)$$

Let  $\sigma_i = \gamma t$ , where  $\gamma$  is a constant incident stress rate and solve (3).



# Wave analysis



$$a_1(t) = \begin{cases} \frac{2r}{\rho_b c_b (1+r)} \frac{d\sigma_i(t)}{dt} & 0 \leq t < 2t_0 \\ \frac{2r}{\rho_b c_b (1+r)} \left\{ \frac{d\sigma_i(t)}{dt} + \left[ 1 + \frac{1-r}{1+r} \right] \frac{d\sigma_i(t-2t_0)}{dt} \right\} & 2t_0 \leq t < 4t_0 \\ \vdots & \\ \frac{2r}{\rho_b c_b (1+r)} \left\{ \frac{d\sigma_i(t)}{dt} + \dots + \left[ \left( \frac{1-r}{1+r} \right)^{\frac{n-2}{2}} + \left( \frac{1-r}{1+r} \right)^{\frac{n}{2}} \right] \frac{d\sigma_i(t-nt_0)}{dt} \right\} & (n-2)t_0 \leq t < nt_0 \end{cases}$$

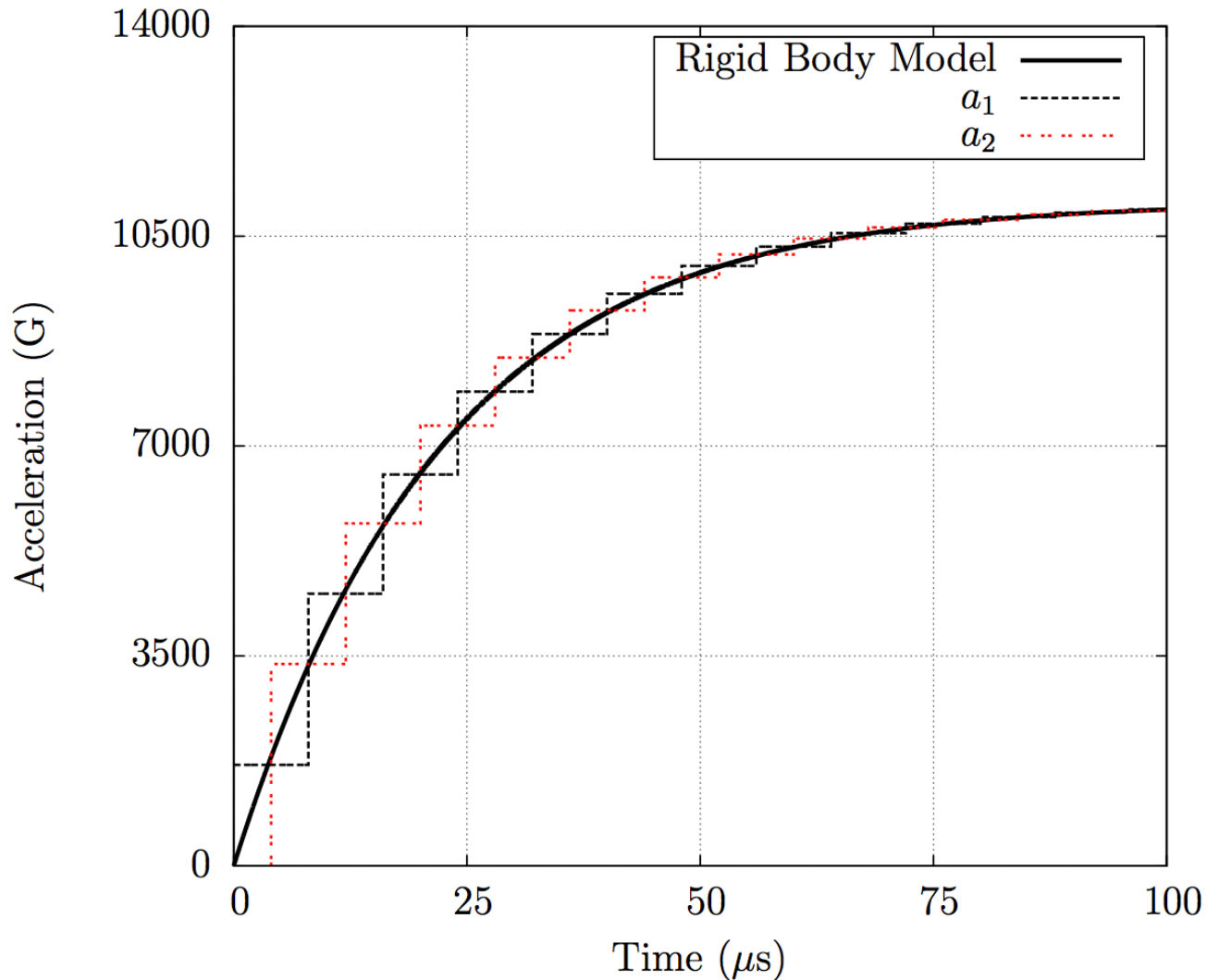
For even  $n$ , where  $t_0 = l_d/c_d$ ,  $r = \frac{\rho_b c_b}{\rho_d c_d}$

$$a_2(t) = \begin{cases} 0 & 0 \leq t < t_0 \\ \frac{4r}{\rho_b c_b (1+r)} \frac{d\sigma_i(t-t_0)}{dt} & t_0 \leq t < 3t_0 \\ \vdots & \\ \frac{4r}{\rho_b c_b (1+r)} \left\{ \frac{d\sigma_i(t-t_0)}{dt} + \dots + \left( \frac{1-r}{1+r} \right)^{\frac{n-1}{2}} \frac{d\sigma_i(t-nt_0)}{dt} \right\} & (n-2)t_0 \leq t < nt_0 \end{cases}$$

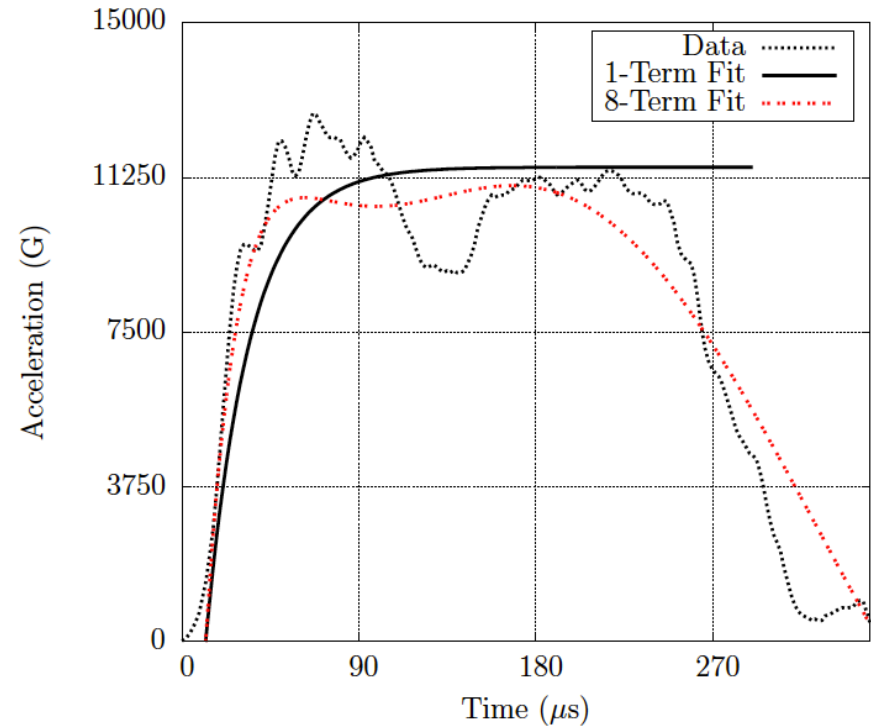
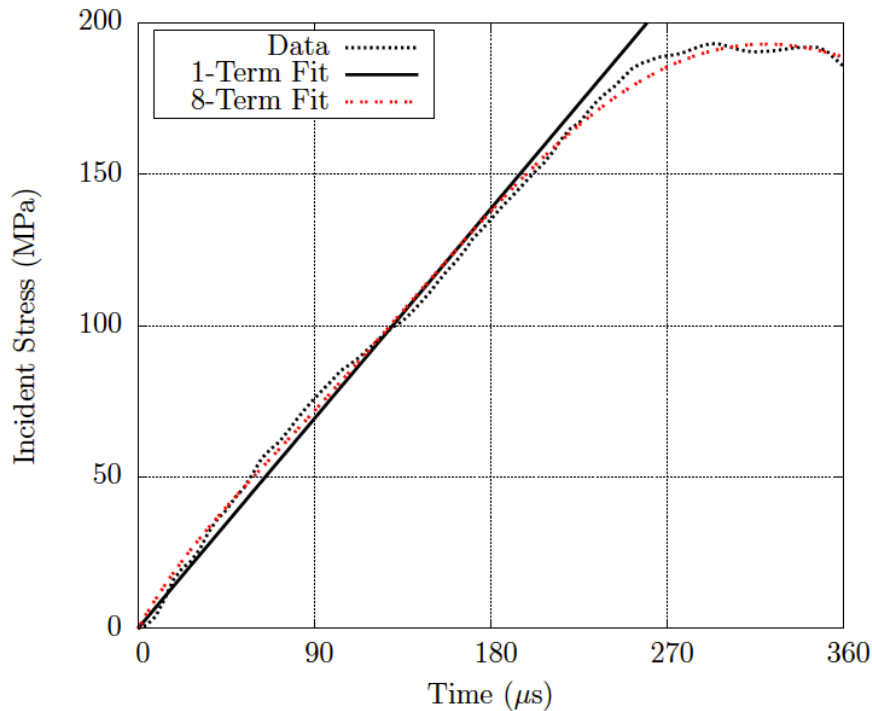
For odd  $n$ , where  $t_0 = l_d/c_d$ ,  $r = \frac{\rho_b c_b}{\rho_d c_d}$



# Wave analysis of tungsten disk response to ramp loading



# Model for V = 7 m/s

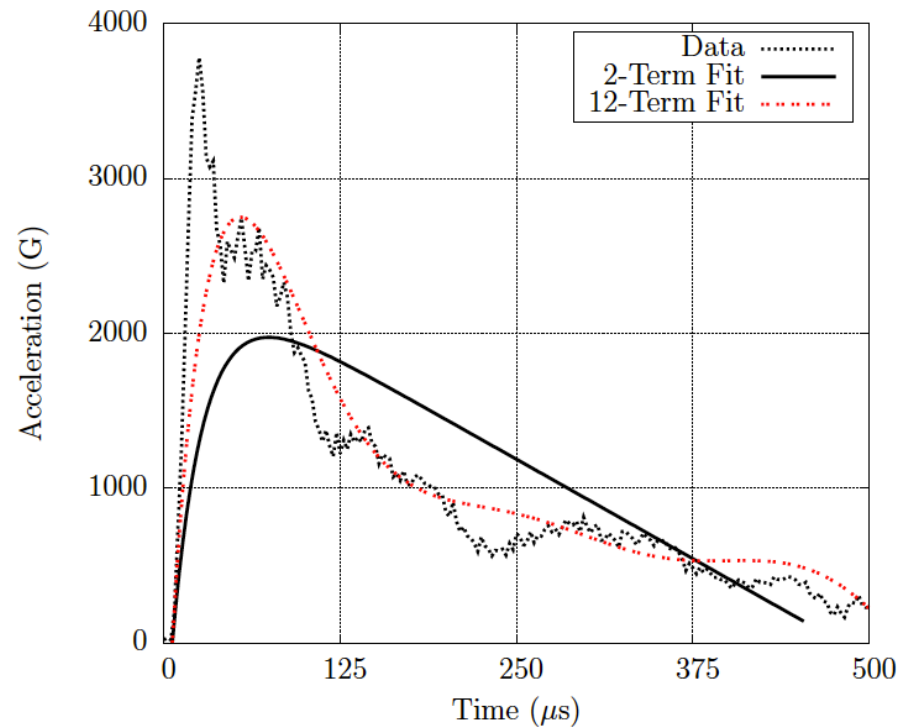
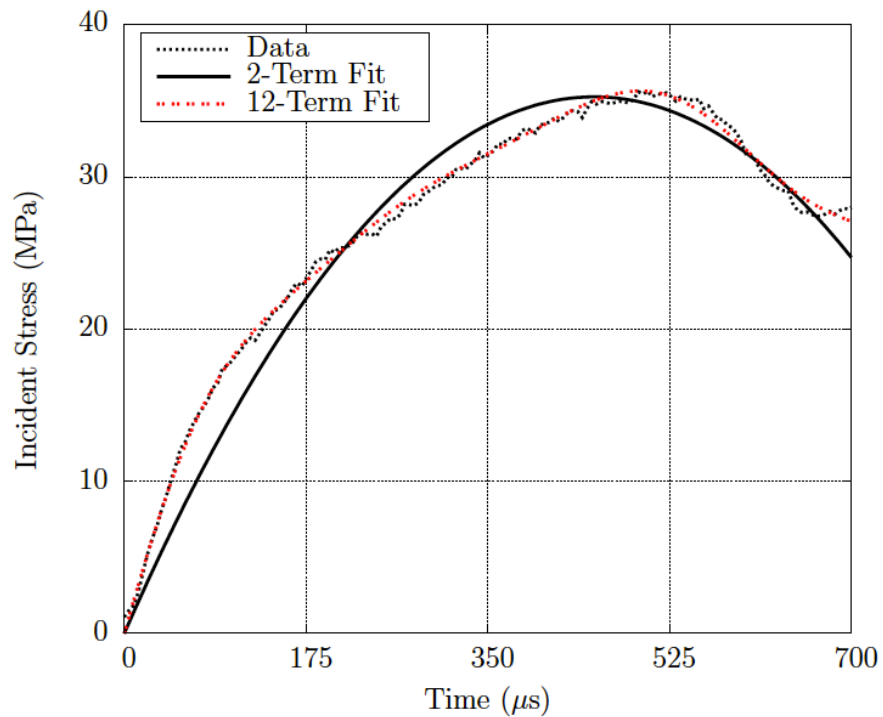


$$\sigma_i = \gamma_1 t + \gamma_2 t^2 + \dots + \gamma_N t^N$$

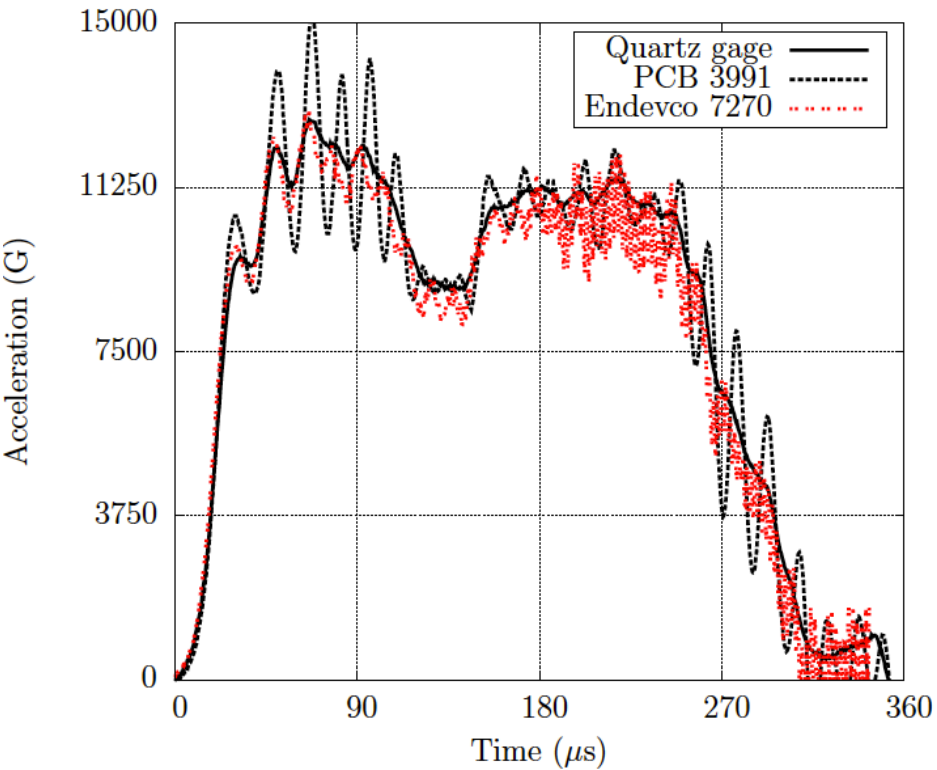
N-term model

$$a(t) = \sum_{n=1}^N \left[ (-1)^{n-1} \frac{2n! \gamma_n}{\rho c \lambda^{n-1}} (1 - e^{-\lambda t}) \right] + \sum_{m=1}^N \sum_{n=1}^{m-1} \left[ (-1)^{n+m-1} \frac{2m! \gamma_m}{n! \rho c \lambda^{m-n-1}} t^n \right]$$

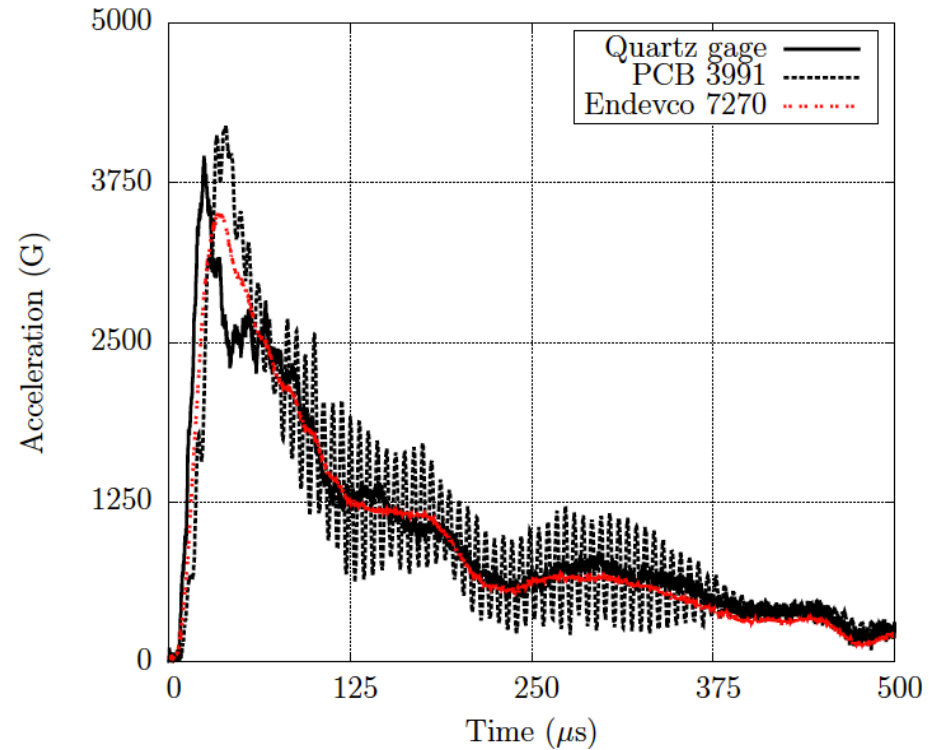
# Model for $V = 20$ m/s



# Acceleration Measurements



$$V \approx 20 \text{ m/s}$$



$$V \approx 7 \text{ m/s}$$



# Summary

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- **Presented pulse shaping techniques for extending loading duration of incident stress pulses**
- **Presented both rigid body and wave mechanics models for predicting the acceleration of the “fly-away” disk given an incident stress pulse**
- **Comparison of models to experimental measurements from quartz stress gage and two accelerometers are in good agreement.**