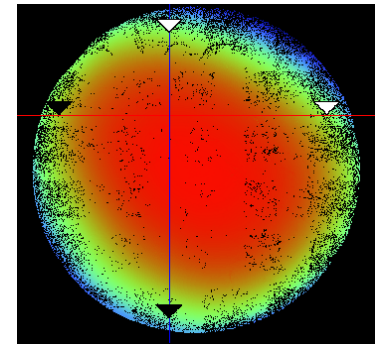
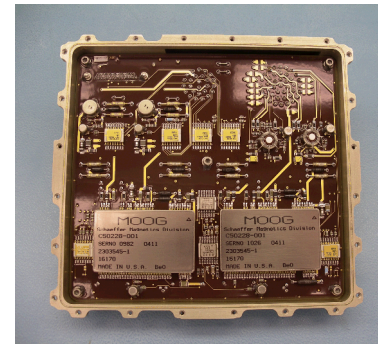


*Exceptional service in the national interest*



# Thermal Contact Conductance of Radiation-Aged Thermal Interface Materials for Space Applications

**Robert A. Sayer, Timothy P. Koehler, Scott M. Dalton,  
Thomas W. Grasser and Ronald L. Akau**

**Sandia National Laboratories**

**Albuquerque, NM, USA**

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# Thermal Contact Resistance

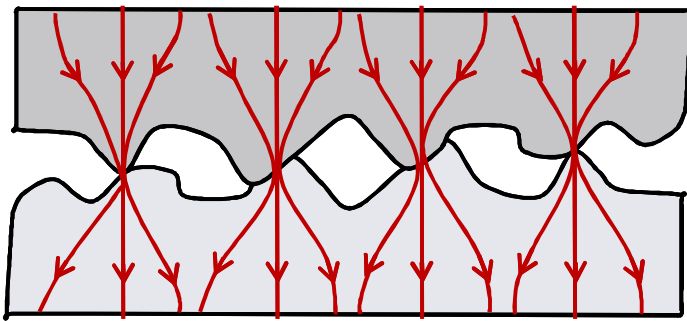
- For interfaces in contact, the real area of contact is typically 2 to 6 orders of magnitude less than the apparent area of contact

$$\frac{A_r}{A} = \frac{P}{H}$$

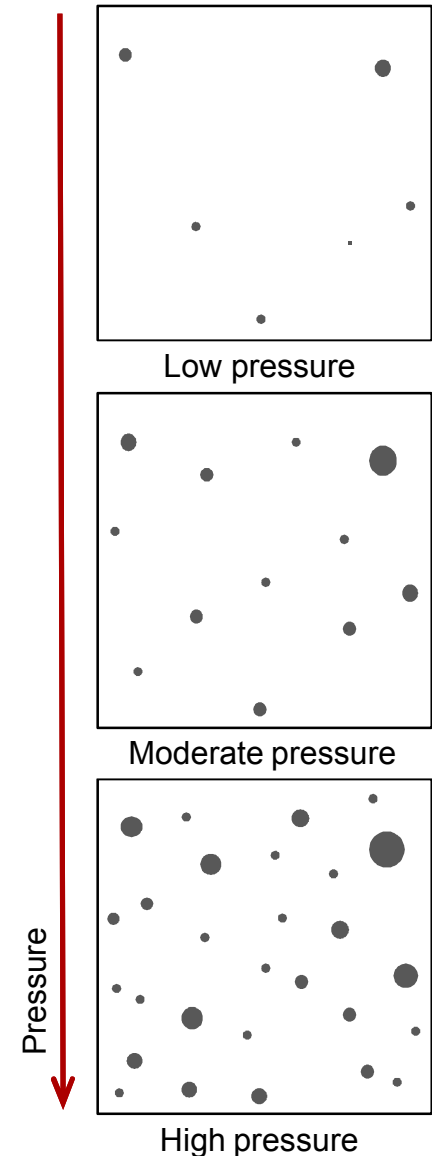
- In vacuum, thermal contact resistance (TCR) of a Gaussian surface is given by

$$R = 0.88 \frac{\sigma}{km} \left( \frac{H}{P} \right)^{-0.94} = aP^b$$

- For systems with multiple interfaces, TCR can consume a significant part of the thermal budget

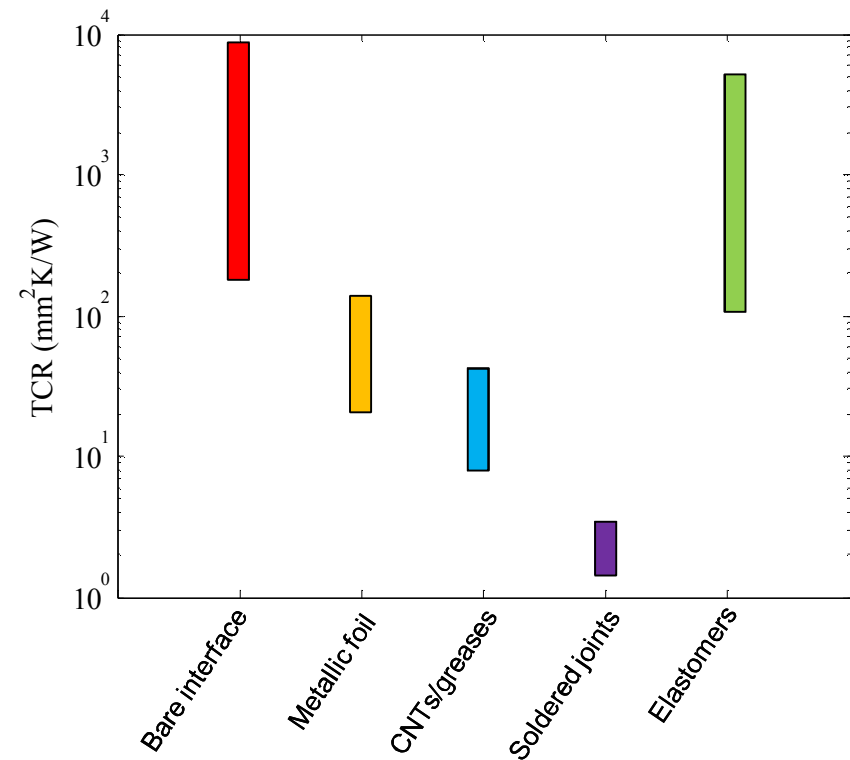
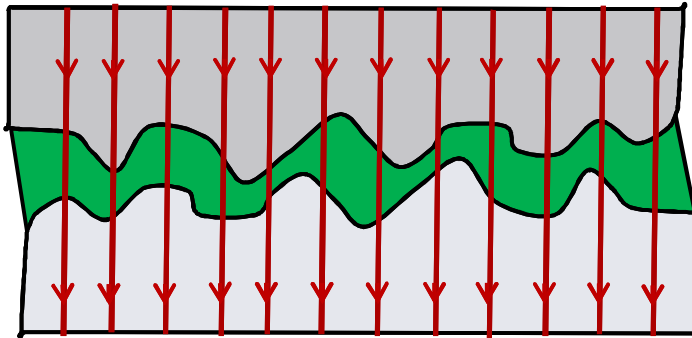


$A$	Apparent contact area
$A_r$	Real contact area
$a, b$	Constants
$H$	Hardness
$k$	Thermal conductivity
$m$	Asperity slope
$P$	Contact pressure
$R$	Contact resistance
$\sigma$	Surface roughness



# Thermal Interface Materials

- Thermal interface materials (TIMs) provide a means of decreasing TCR by filling the gaps between asperity contacts
  - Thermal greases
  - Metallic foils
  - Carbon nanotube (CNT) materials
  - Elastomeric materials



# TIMs in Satellite Systems

- Special considerations are required for TIMs used in satellites
  - Vacuum compatible
  - **Electrically insulating**
- Space systems are exposed to a wide array of radiation sources

- UV
- X-ray
- Charged particles

Absorbed and reflected by outer materials

- $\gamma$ -ray

Experience little attenuation  
Easily reach and pass through all components  
Doses as high as 10 Mrad /yr [1]

**Interactions with TIMs are important**

- Common TIMs

- ~~■ Thermal greases~~
- ~~■ Metallic foils~~
- ~~■ CNT materials~~
- Elastomeric materials

# TIMS used in this Study

Two different materials were investigated

- Cho-Therm 1671
  - Silicone elastomer filled with boron nitride particles
  - Reinforced with a fiberglass cloth
- ThermaCool R10404
  - Closed cell silicone sponge rubber

Cho-Therm

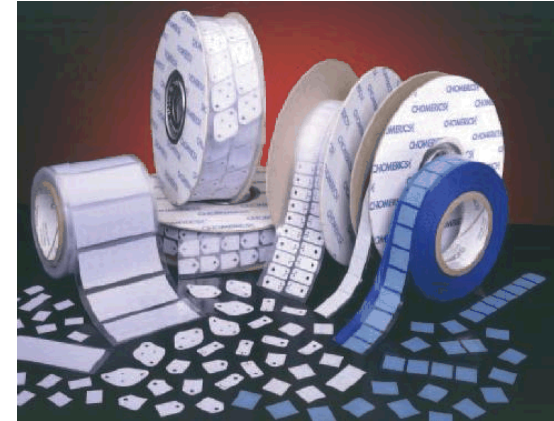


Image <http://products.robertmckeown.com>

ThermaCool

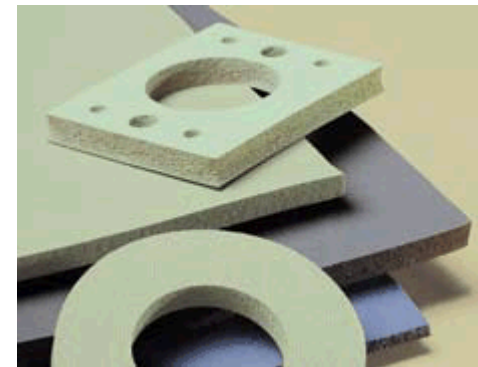


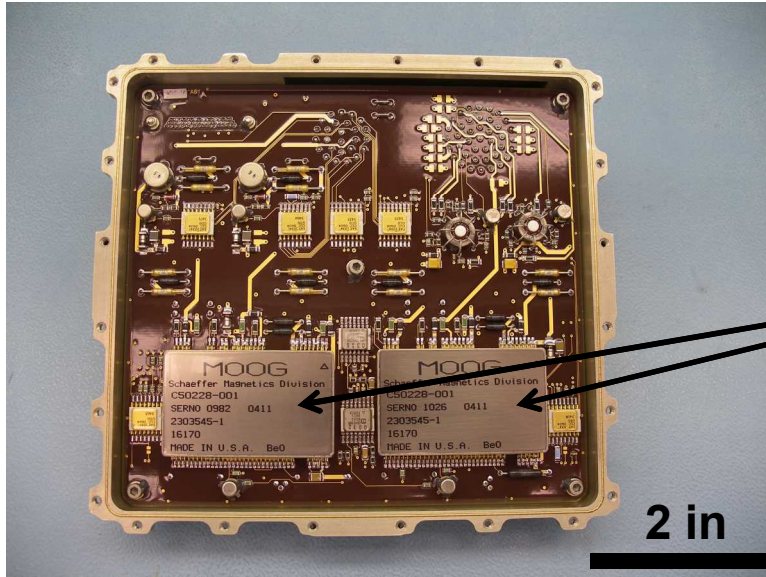
Image from ThermaCool R10404 Data Sheet,  
Saint-Gobain Performance Plastics

Property	Cho-Therm	ThermaCool
Color	White	Light green
Thickness (mm)	0.4	3.2
Thermal conductivity (W/mK)	2.6	0.36-0.86*
Thermal resistance (mm <sup>2</sup> K/W)	150	3400-8600*
Hardness (Shore 'A')	90	13
Density (kg/m <sup>3</sup> )	1550	1105

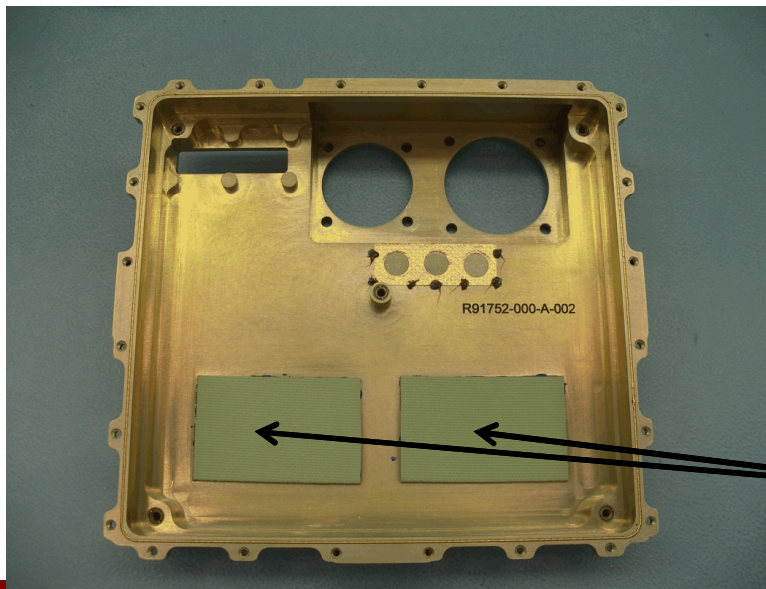
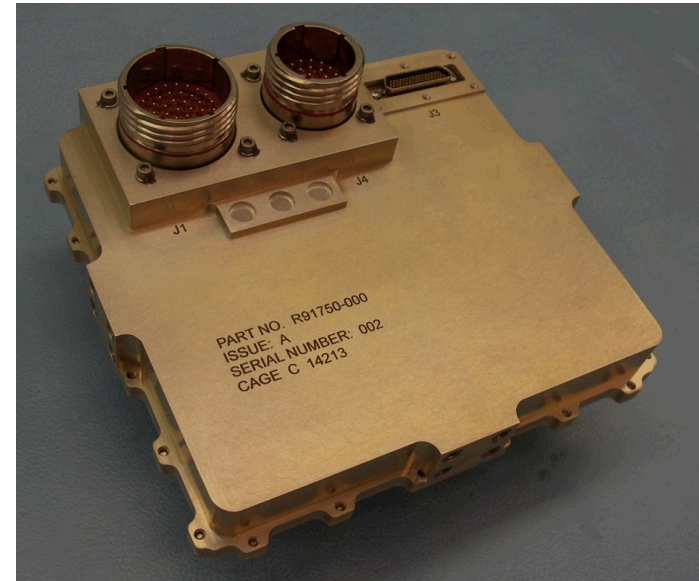
\*Highly sensitive to compression of the TIM



# Filter Wheel Controller (FWC) Board



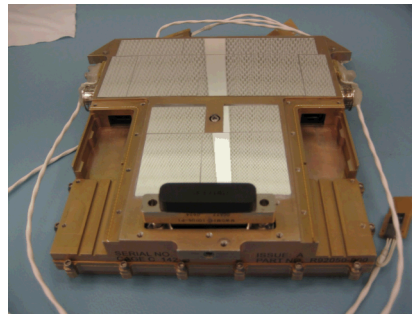
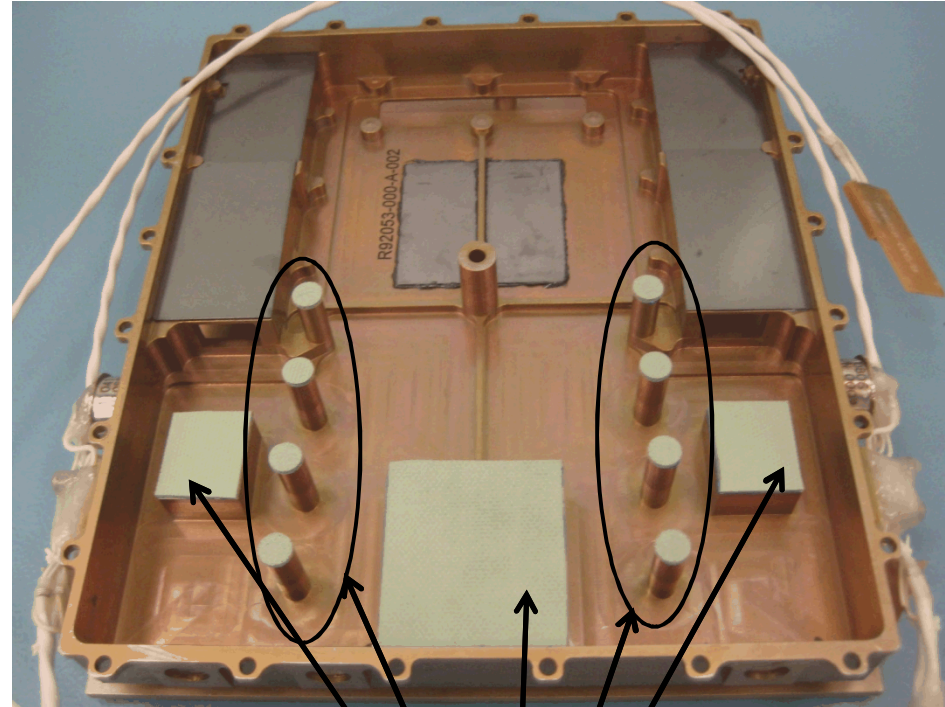
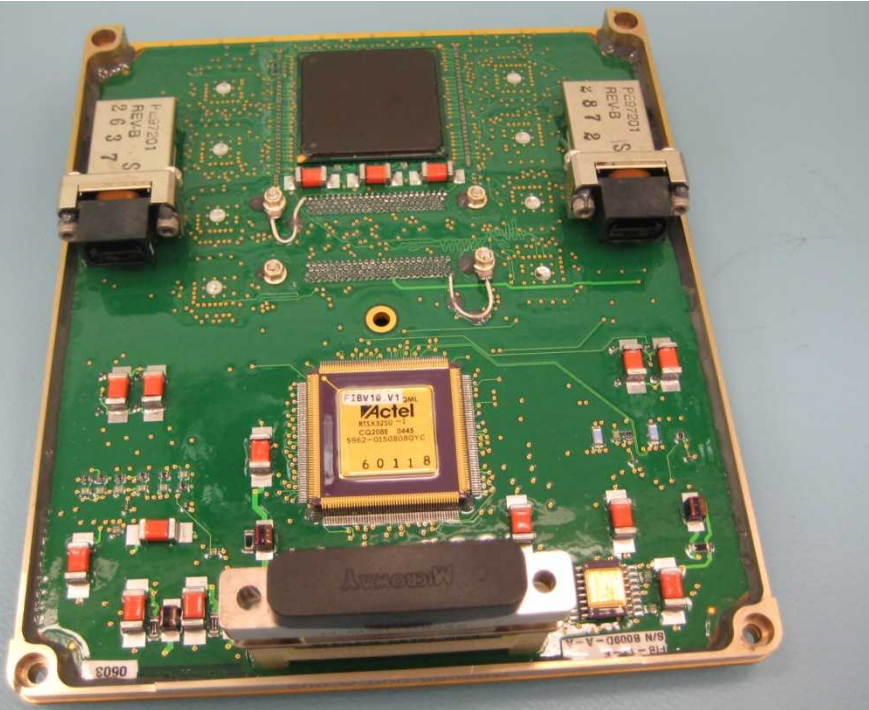
Power converters  
4 W dissipated



TIMs

# Fiber Interface Board (FIB)

5 W dissipated

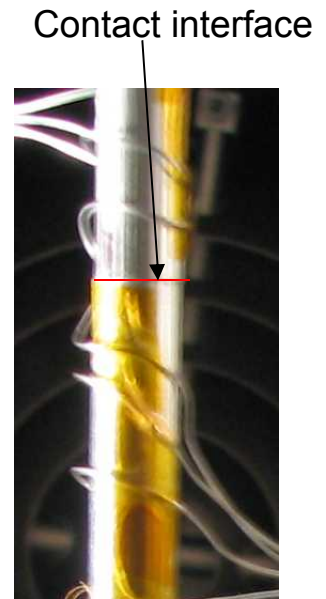


TIMs



# 1-D Steady State Experimental System Sandia National Laboratories

- Minimum chamber pressure:  $2 \times 10^{-6}$  torr
  - Can also look at N<sub>2</sub>, Ar, He, air and other gas environments up to 630 torr
- Maximum interface pressure: 10,000 psi
- Temperature range: 0 to 80 °C
- 12 thermocouples (6 per bar)



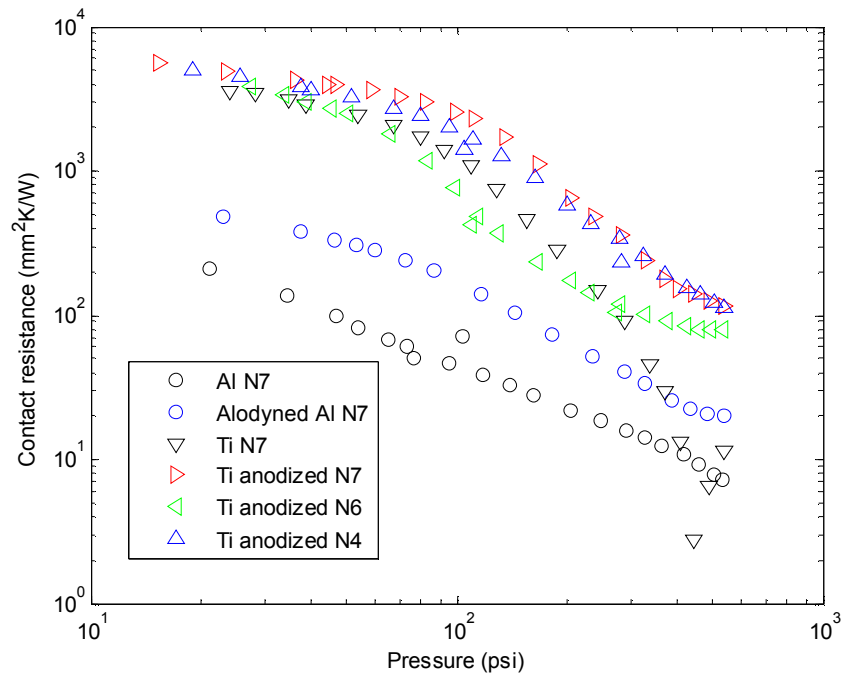


# Metallic Samples

- Common metals used in satellite systems were chosen

- Aluminum
- Alodined aluminum
- Titanium
- Anodized titanium

Sample	Material	Surface treatment	Surface finish	Sample name	R <sub>a</sub> (nm)	R <sub>q</sub> (nm)	R <sub>t</sub> (μm)	R <sub>sk</sub>	R <sub>ku</sub>
1	Aluminum	none	N7	Al_N7_N	119	162	2.5	-1.5	7.9
2	Aluminum	alodine	N7	Al_N7_T	271	440	3.9	19.0	-3.0
3	Titanium	none	N7	Ti_N7_N	168	219	1.1	4.6	-1.0
4	Titanium	anodize	N7	Ti_N7_T	582	750	3.8	3.7	-0.6
5	Titanium	anodize	N6	Ti_N6_T	643	822	2.5	3.9	-0.3
6	Titanium	anodize	N4	Ti_N4_T	540	692	2.5	3.7	-0.7

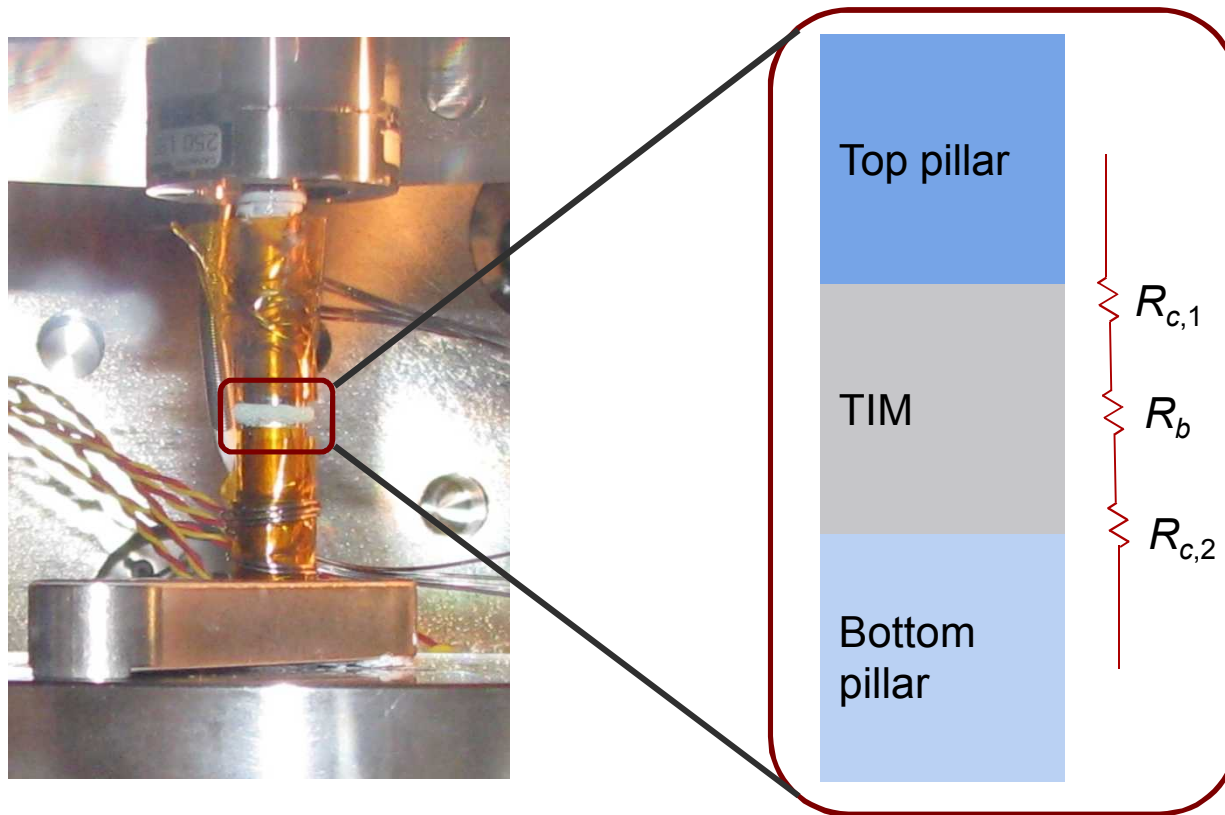


$$R = aP^b$$

Run #	Metal pillar	a	b
1	Al_N7_N	2.11E+04	-1.02
2	Al_N7_T	1.30E+05	-1.14
3	Ti_N7_N	2.12E+05	-0.86
4	Ti_N7_T	3.50E+04	-0.43
5	Ti_N6_T	1.41E+06	-1.22
6	Ti_N4_T	1.76E+05	-0.77
	All Ti samples	8.14E+04	-0.64

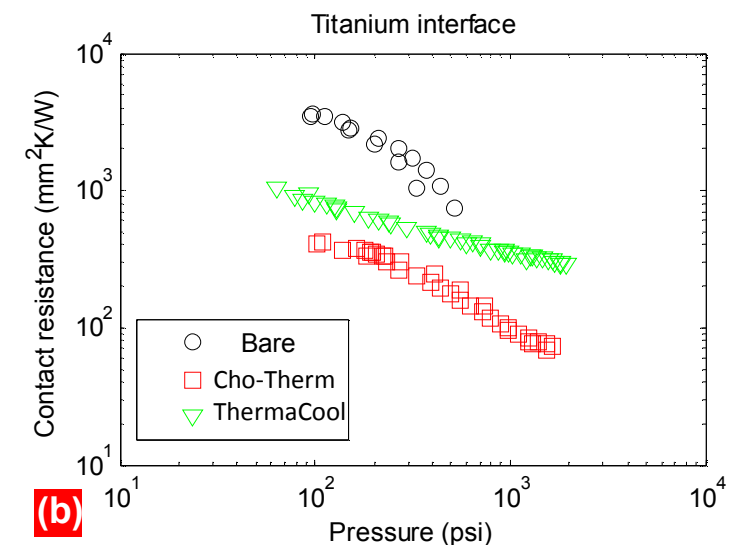
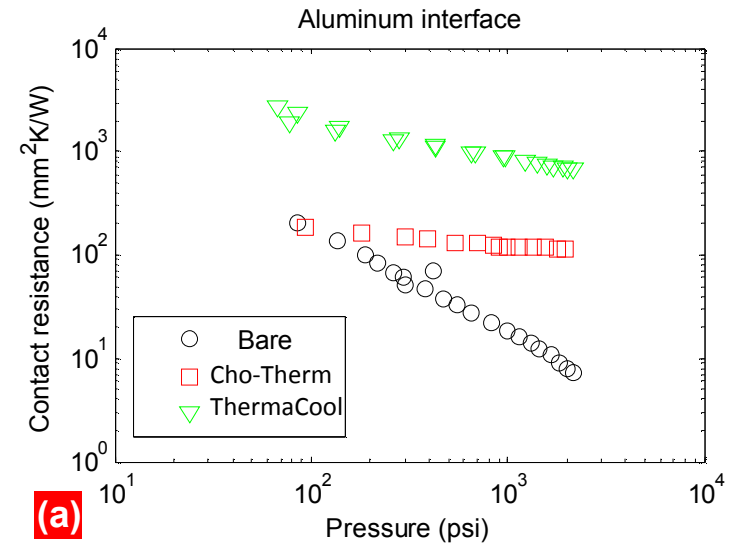
# Total Thermal Interface Resistance Sandia National Laboratories

- The total thermal resistance at the interface when a TIM is used is the sum of contact resistance between the TIM and each metallic pillar and the bulk resistance of the TIM



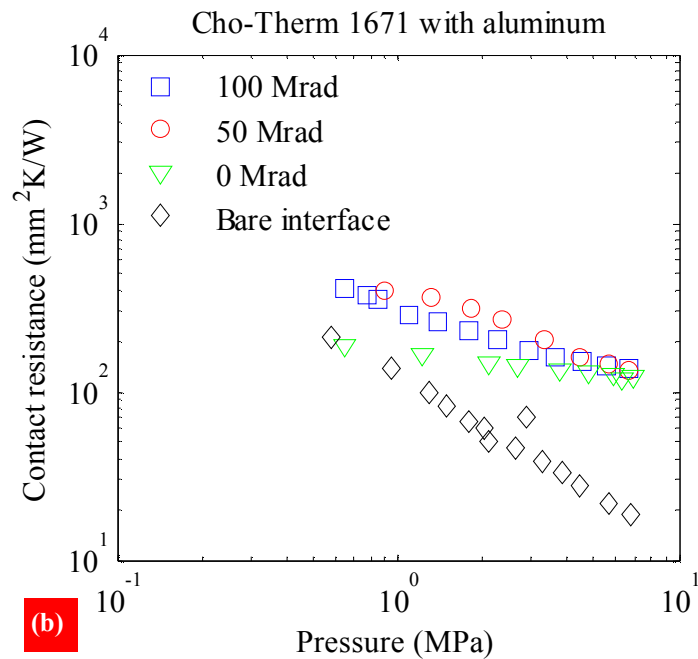
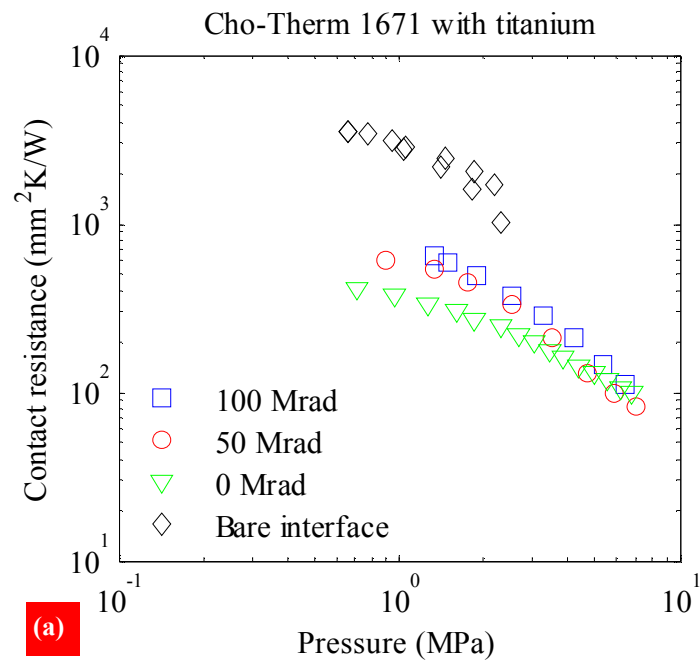
# Thermal Contact Resistance: TIMS

- TCR increased when TIM was inserted between Al contacts
  - Al has a low TCR due to high  $k$  and low  $H$  values
- TCR decreased when TIM was inserted between Ti contacts
  - Ti has a high TCR due to low  $k$  and high  $H$  values
- Cho-Therm out performs ThermaCool due to its much small thickness
- TIMs minimize the effect that pressure has on TCR



# Radiation Aging: Cho-Therm

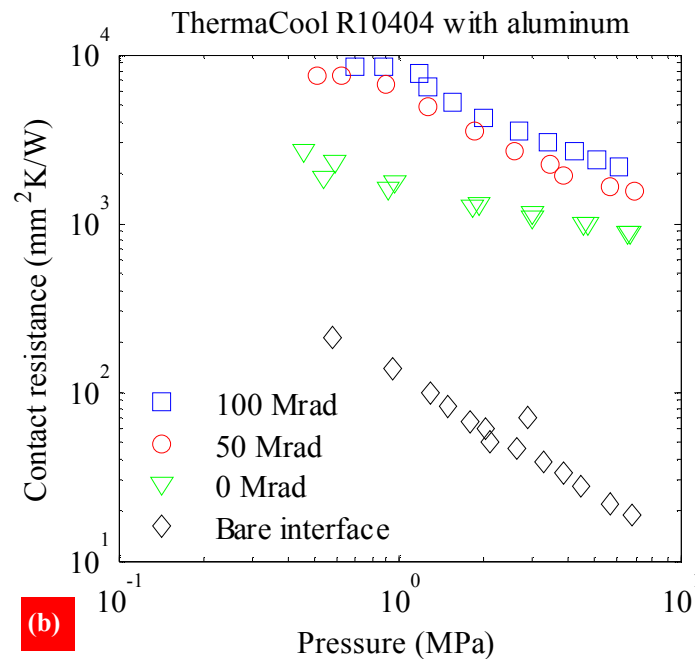
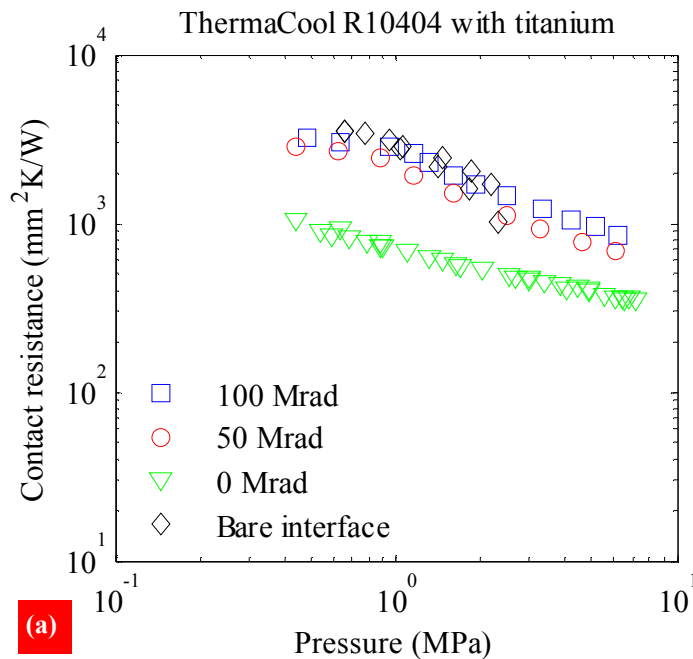
- Radiation aging increases the TCR
- Little difference between the 50 Mrad and 100 Mrad samples



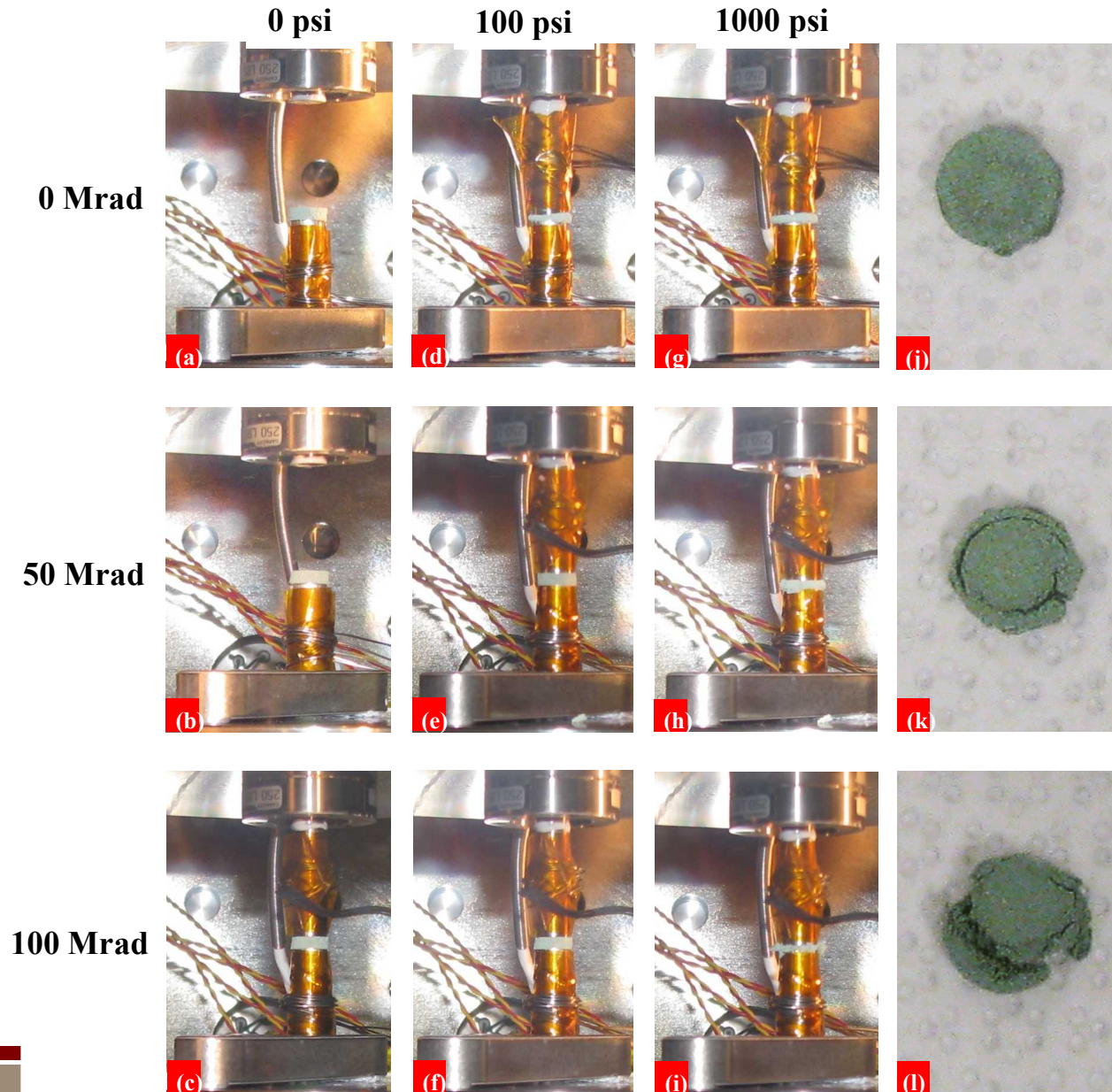


# Radiation Aging: ThermaCool

- Radiation aging increases the TCR
- Little difference between the 50 Mrad and 100 Mrad samples
- Much larger increase in TCR for the ThermaCool samples
- $\gamma$ -ray radiation makes the sample much stiffer, thus increasing the bulk resistance
- Radiation aged samples are pressure independent under 170 psi



# ThermaCool Compression



# Recommended TCR Values

- Values were found from a least squares fit to experimental data
- Typical pressure range is 200 to 300 psi.

$$R = aP^b$$

TIM	Dose (Mrad)	Aluminum			Titanium		
		<i>a</i>	<i>b</i>	<i>P</i> (psi)	<i>a</i>	<i>b</i>	<i>P</i> (psi)
Bare interface	0	1.61E+04	-0.98	80-990	1.34E+05	-0.78	90-340
Cho-Therm	0	4.13E+02	-0.18	90-1000	1.21E+04	-0.68	100-990
	50	7.97E+03	-0.59	130-960	1.28E+05	-1.05	130-1000
	100	3.54E+03	-0.49	90-960	2.46E+05	-1.11	190-930
ThermaCool	0	1.08E+04	-0.37	70-970	4.71E+03	-0.38	70-1000
	50	7.23E+03	0.00	70-170	2.65E+03	0.00	70-170
		1.73E+05	-0.70	170-1000	4.74E+04	-0.63	170-880
	100	8.23E+03	0.00	100-170	3.02E+03	0.00	70-170
		2.01E+05	-0.67	170-880	6.94E+04	-0.65	170-900

# Conclusions

- A capability for testing TCR satellite materials before and after  $\gamma$  radiation has been developed
- TCR of two commonly used electrically insulating thermal interface materials was investigated
  - The effectiveness of the TIM depends on the contacting materials between which it is placed
  - TCR increased when placed between Al
  - TCR decreased when placed between Ti
- A significant increase in TCR was observed when the samples were  $\gamma$  radiation aged
  - TIM effectiveness decreases over the mission life
- Sample brittleness increased with radiation aging
  - Could potentially lead to system contamination through flaking or cracking of the TIM

## Next Steps

- Investigate materials that are radiation-aged under compression
- Look into the effects of  $\gamma$  radiation on electrically conductive TIMs with superior thermal performance (CNTs and foils)



# Acknowledgments

- Sandia National Laboratories is a multi-program laboratory managed and operated by Sandia Corporation, a wholly owned subsidiary of Lockheed Martin Corporation, for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000.
- For technical review of this work:
  - Dan Guildenbecher(Sandia National Laboratories)
  - Travis Fisher (Sandia National Laboratories)