

Axial Crushing of Aluminum Tubes

Experimental Results and Finite Element Modeling

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Albuquerque, NM**



Introduction

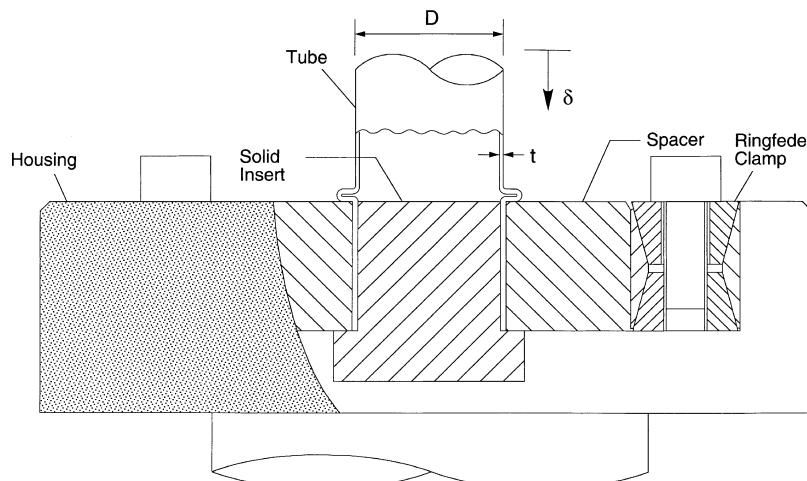
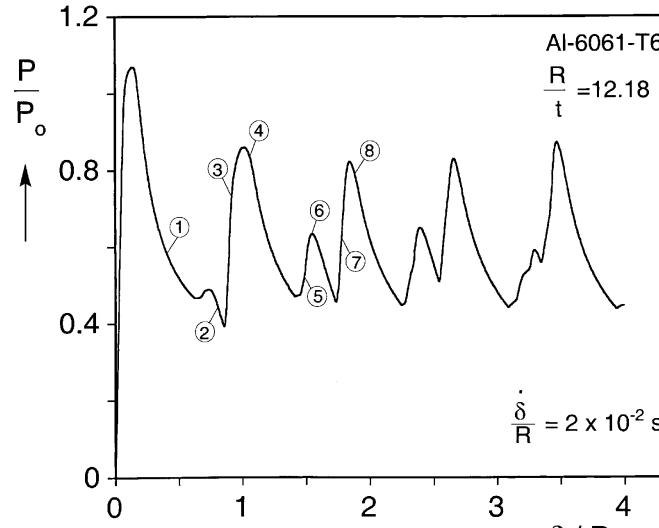
- Many Sandia-designed systems may be subjected to severe mechanical environments. Safety and security issues require analysis of system response under these conditions.
- System and component level finite element models are widely used to perform a substantial part of the analysis and to guide testing.
- Validation of FE modeling capabilities, by comparison to experiment is an essential part of the process.



Objectives

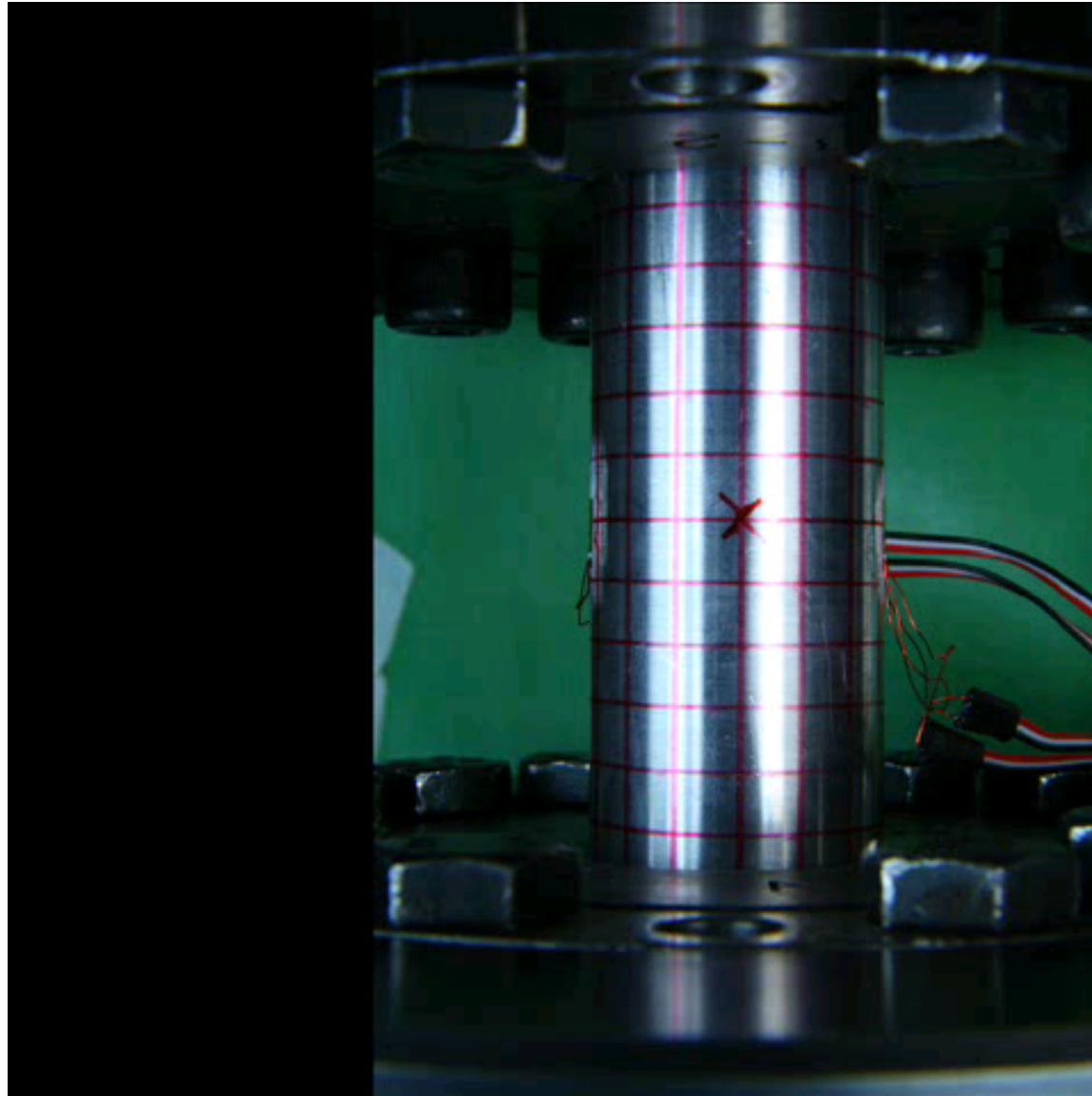
- Demonstrate the performance of FE nonlinear structural models to simulate crushing and other large-deflection scenarios.
- Examples:
 - Axial and lateral crushing of tubular structures
 - Hydraulic collapse
 - Puncturing
 - Etc.
- This presentation addresses aluminum tubes crushed by quasi-static axial compression.

Axisymmetric Collapse (Bardi et al, 2003)

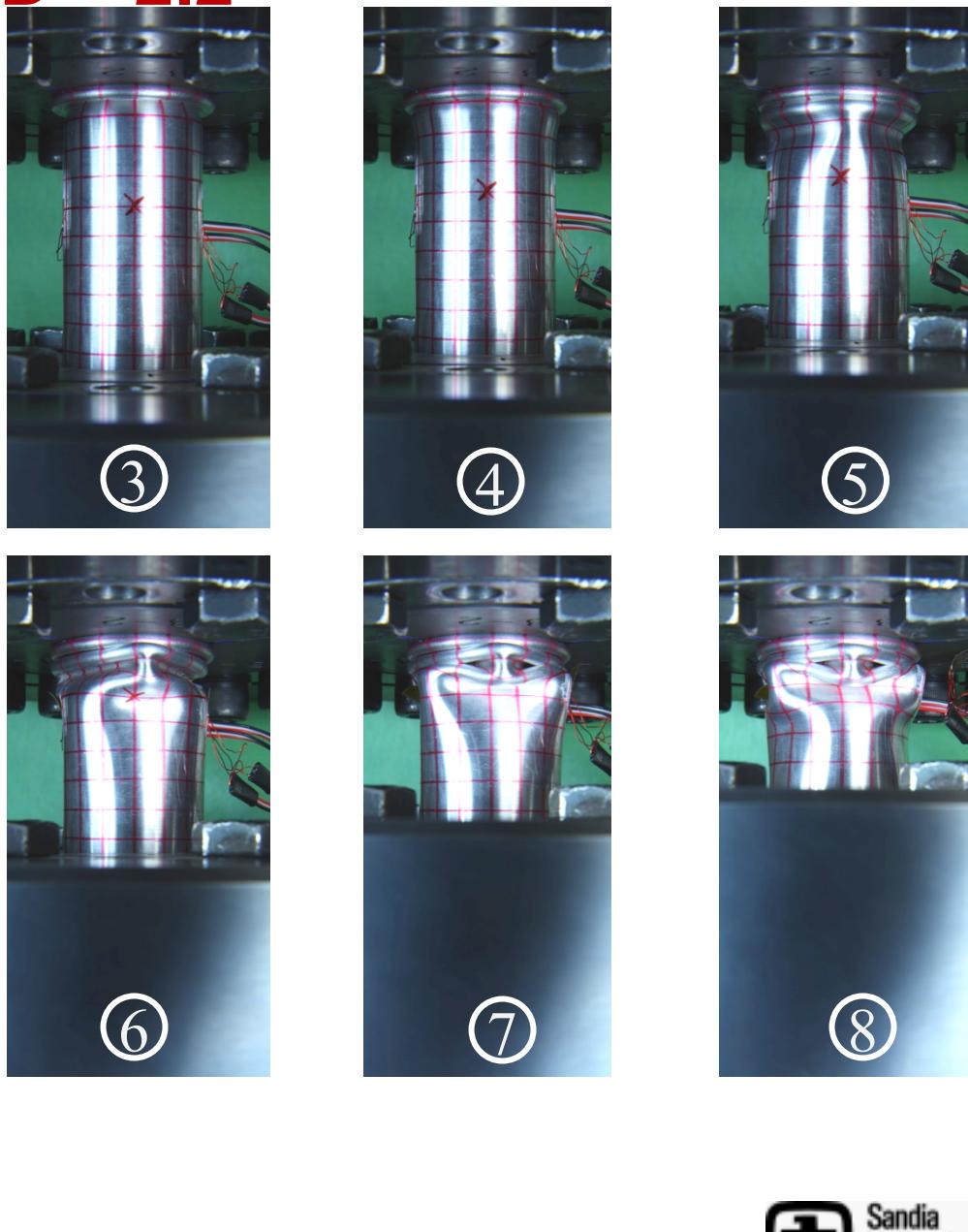
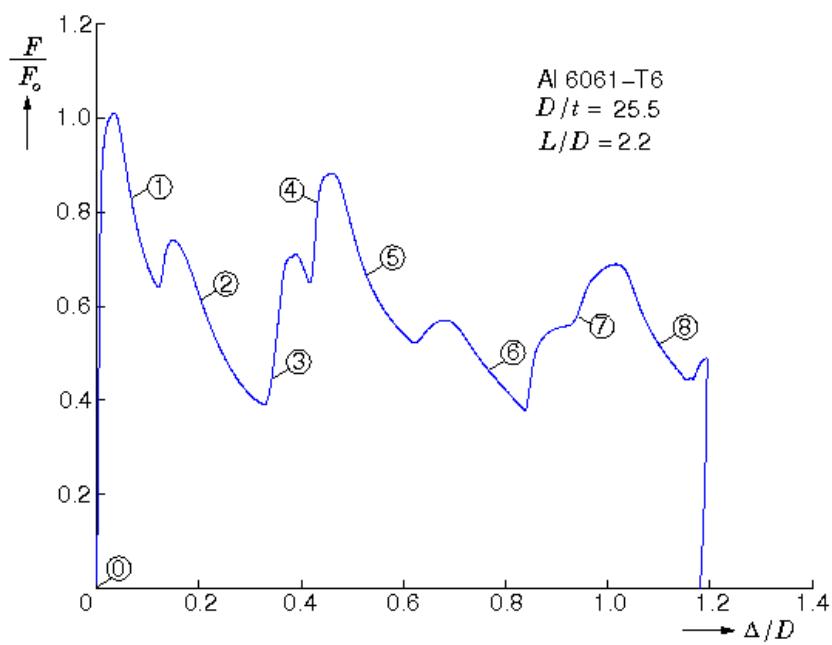


L/D = 2.2

AI 6061-T6
D/t = 25.5
L/D = 2.2



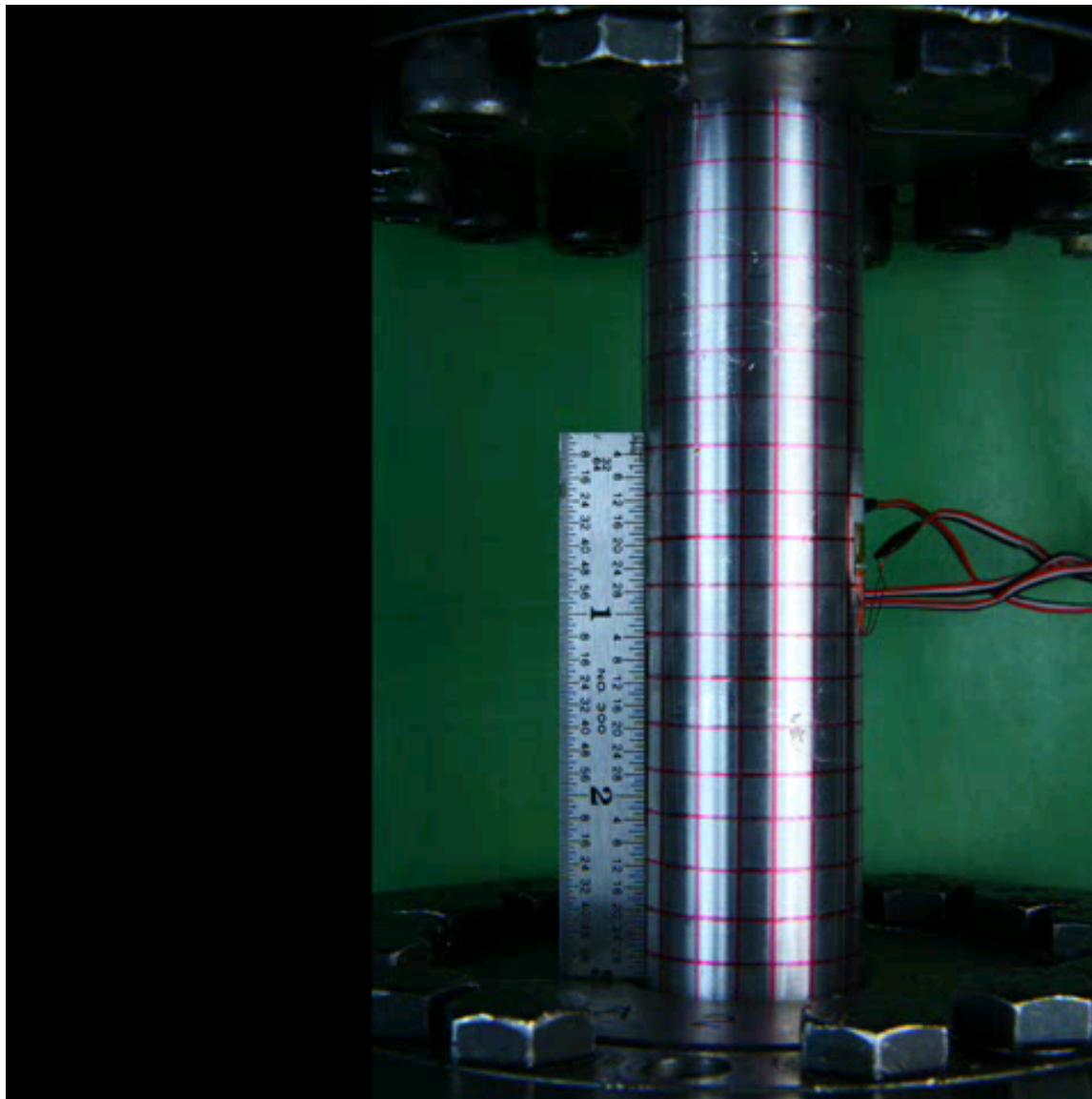
L/D = 2.2



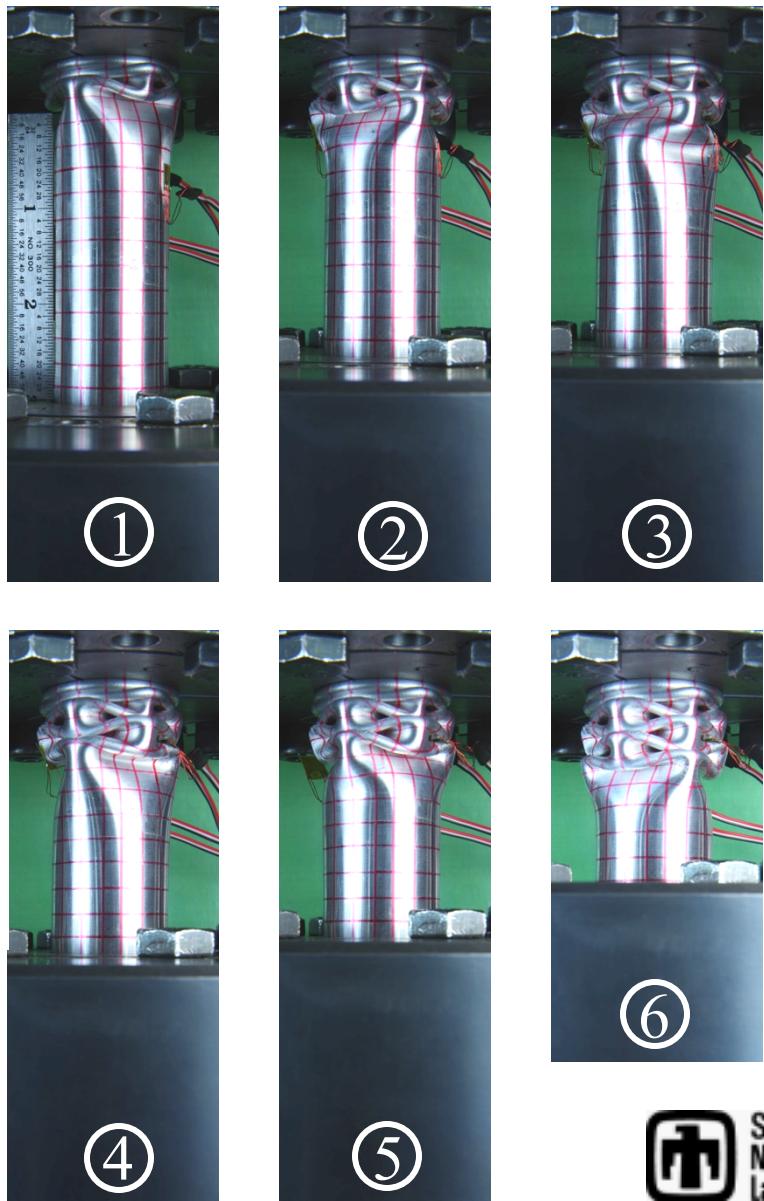
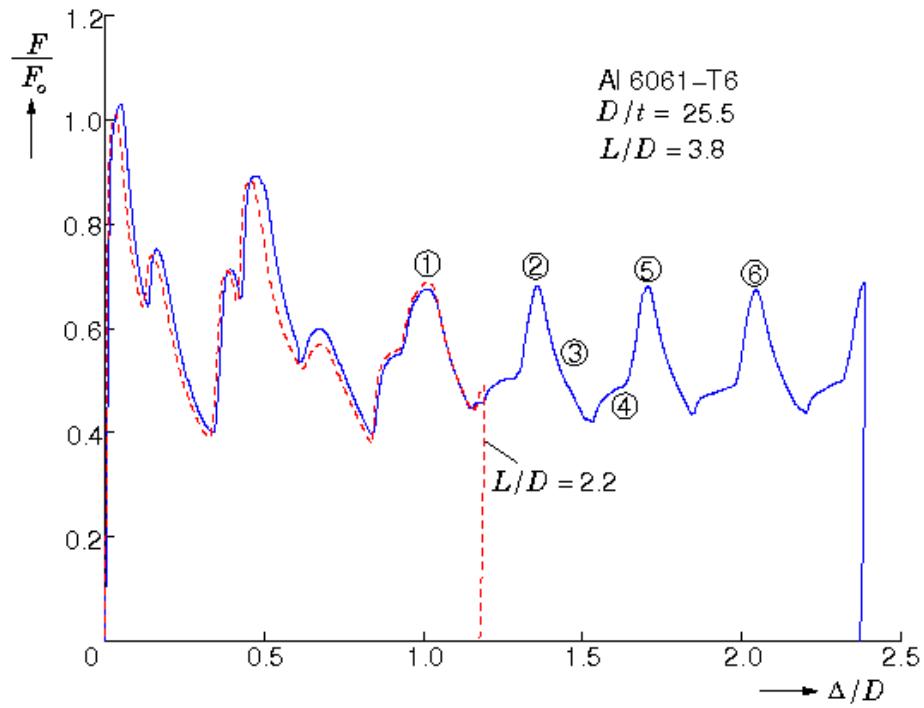


L/D = 3.8

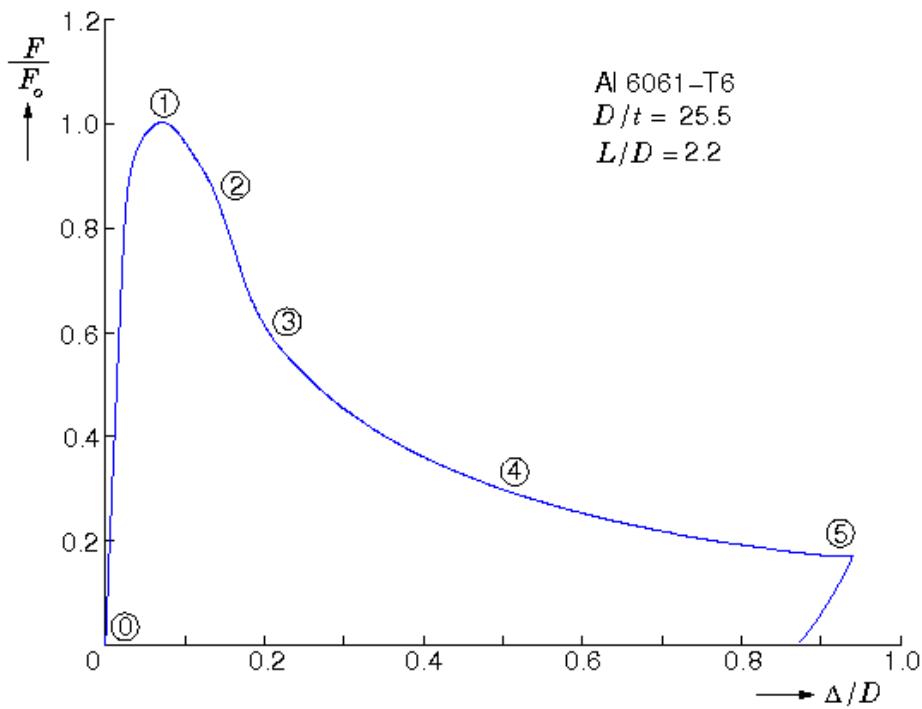
Al 6061-T6
D/t = 25.5
L/D = 3.8



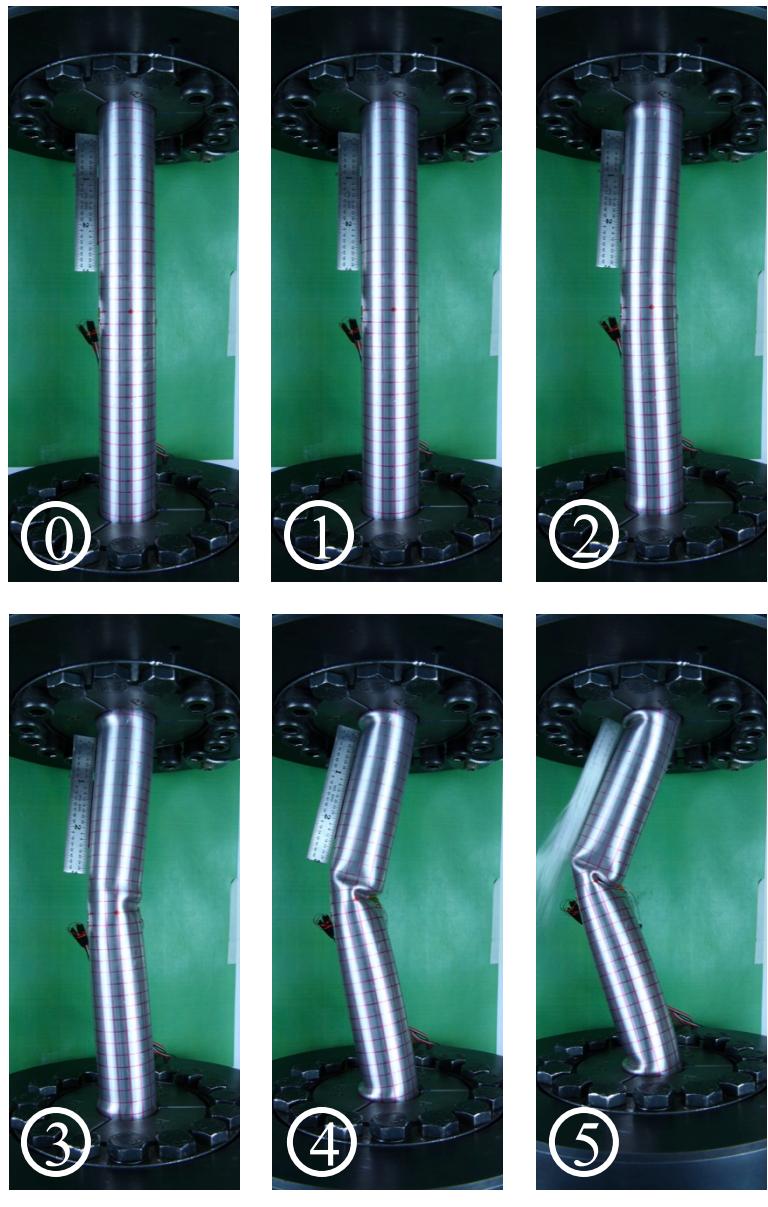
L/D = 3.8



L/D = 7.0



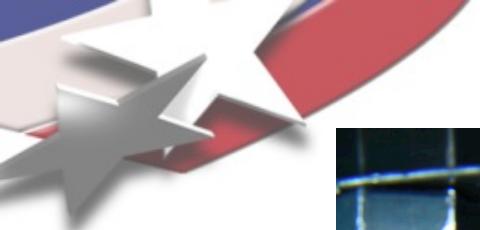
Al 6061-T6
 $D/t = 25.5$
 $L/D = 2.2$



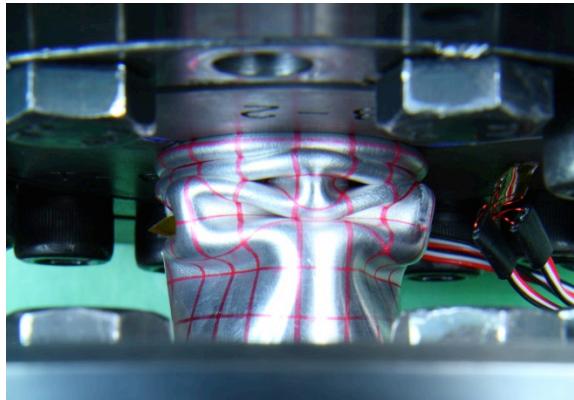
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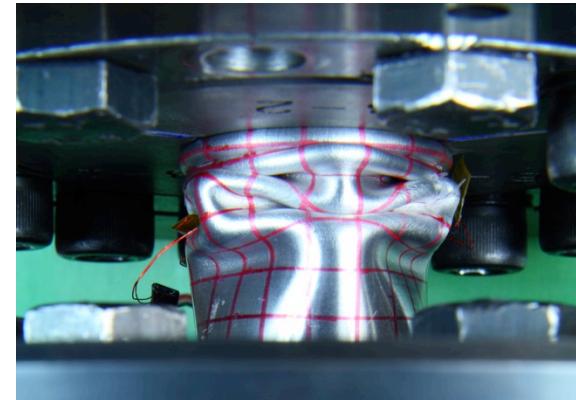
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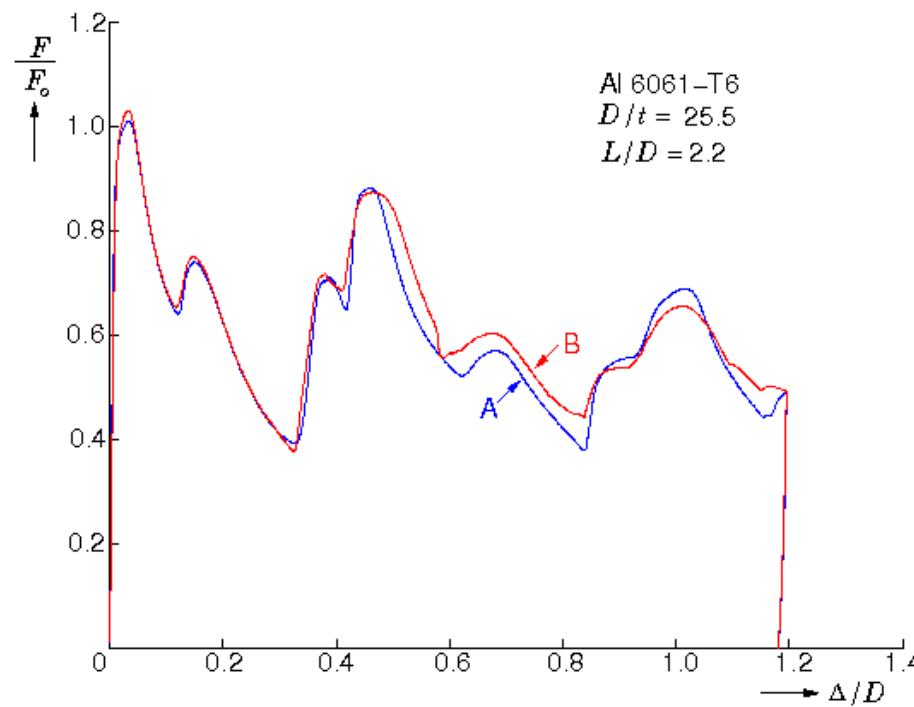
L/D = 2.2



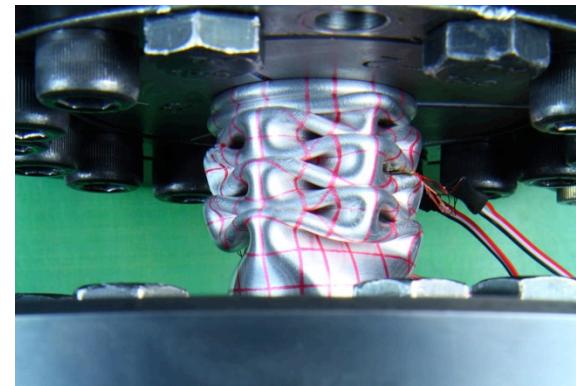
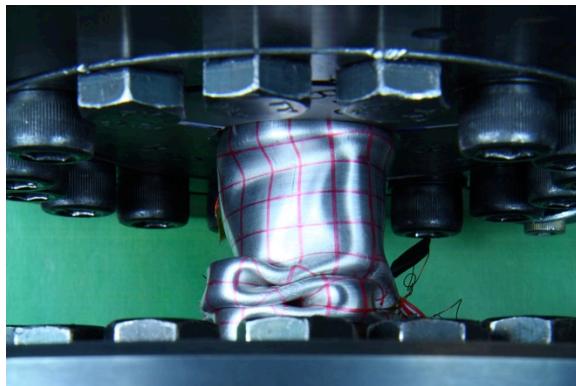
A



B

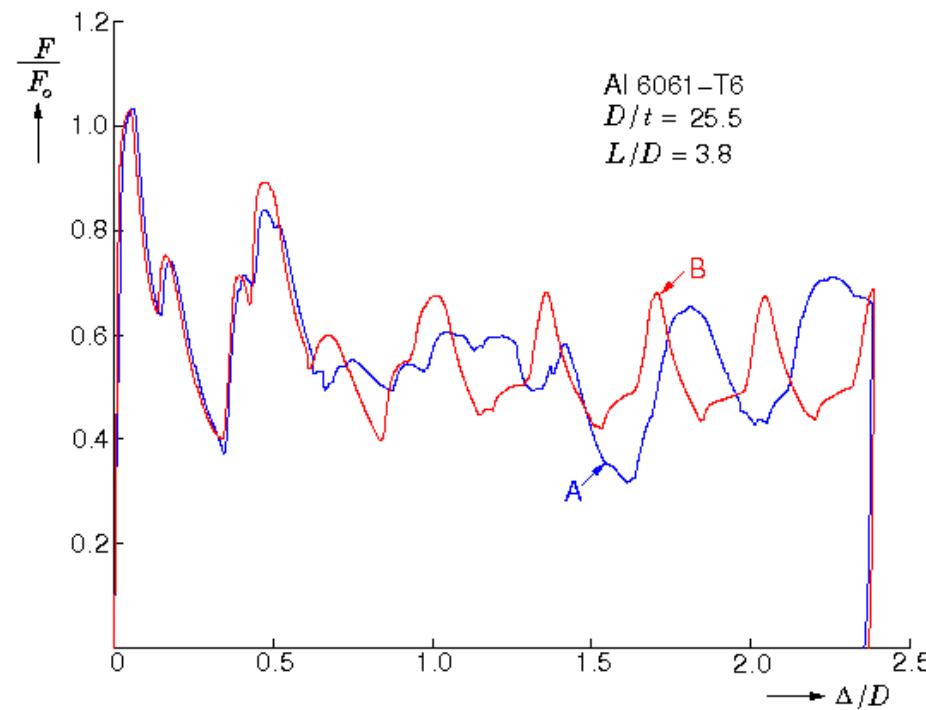


L/D = 3.8



A

B





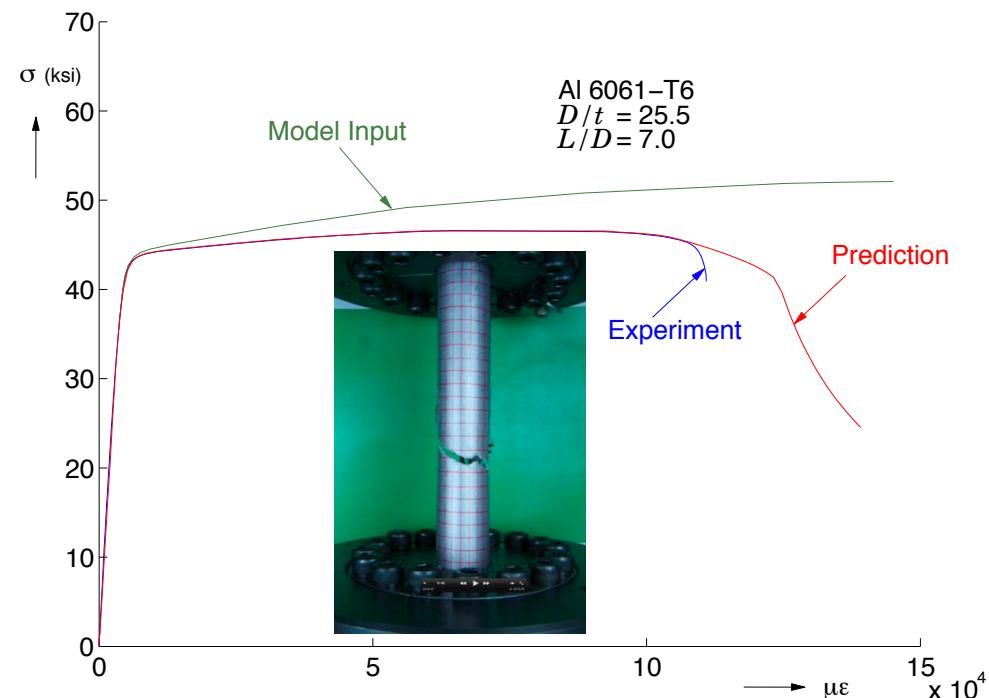
Modeling Overview

- Abaqus/Explicit
- Shell Elements on Tube
 - Reduced Integration (S4R)
 - Relax Stiffness Hourglass Control
- Rigid Fixtures
- Two Step Procedure
 - Clamping Pressure on Fixtures
 - Displacement on End
- Shell Contact Thickness
 - Set by Contact Algorithm
 - $\leq 42\%$ of Element Edge Length



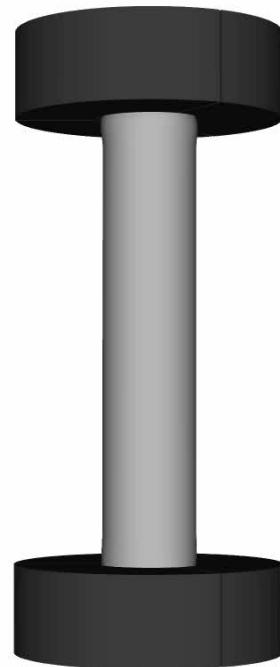
Material Properties

- **Tensile Test of Tube**
 - Pulled a Section from Same Tube
- **Material Model Input**
 - Up to UTS from Test
 - Iteratively Determined from UTS till Near Failure



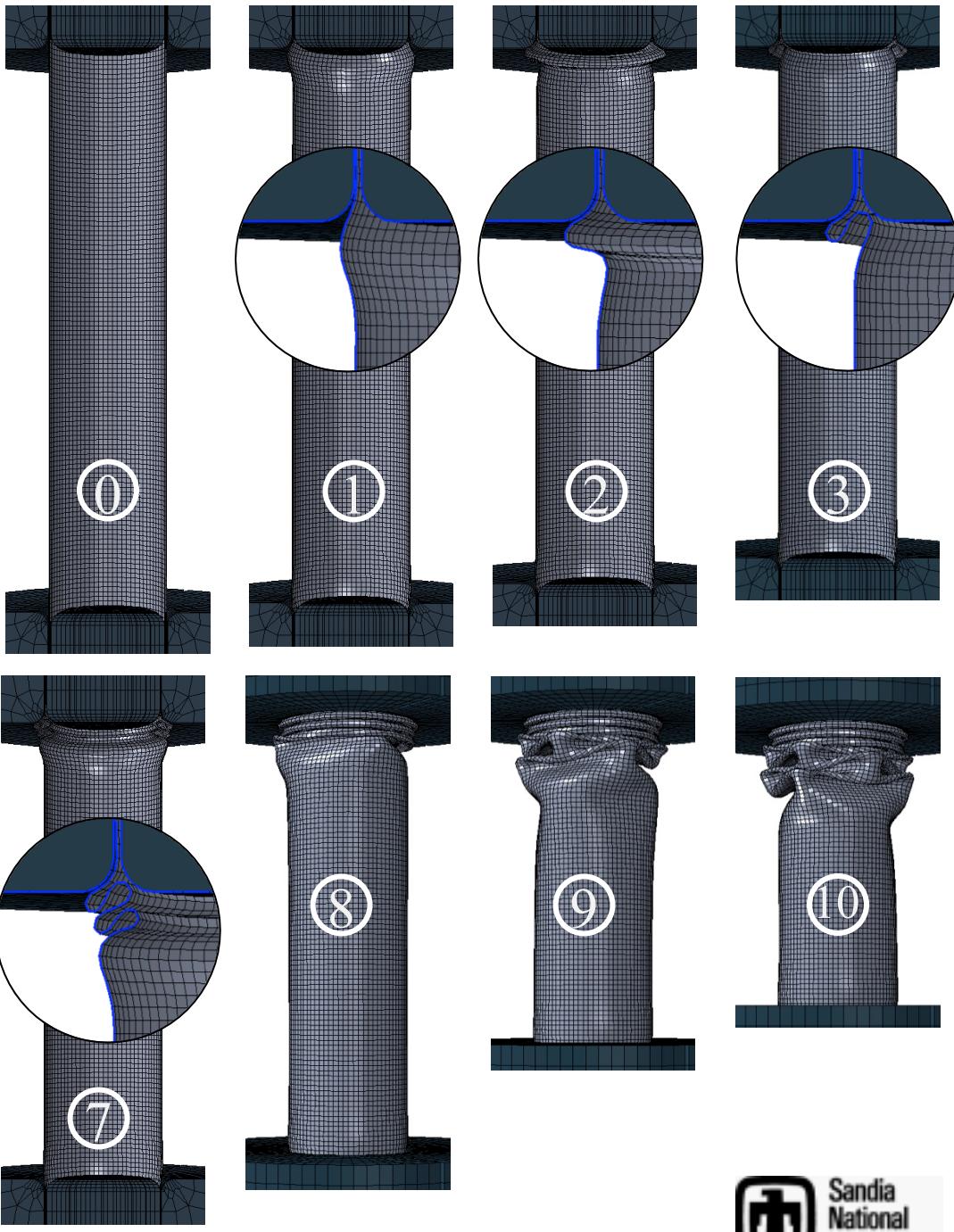
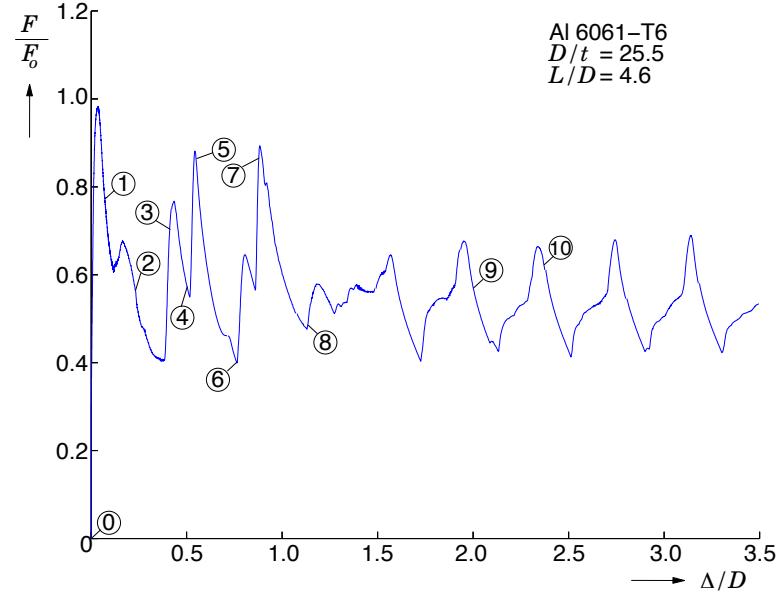


Crushing Prediction L/D=4.6



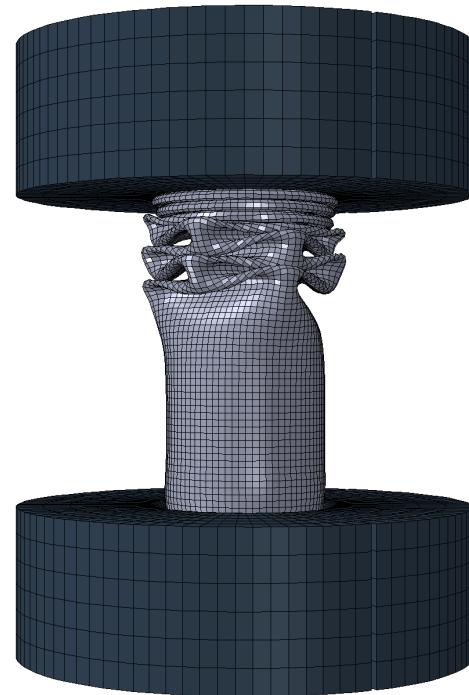
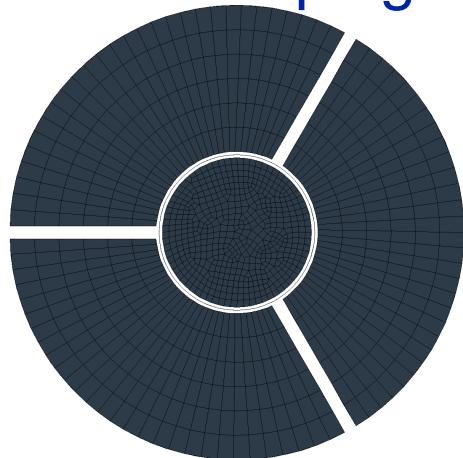
L/D = 4.6

Al 6061-T6
 $D/t = 25.5$
 $L/D = 4.6$

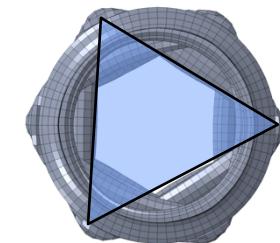


Crushing Pattern

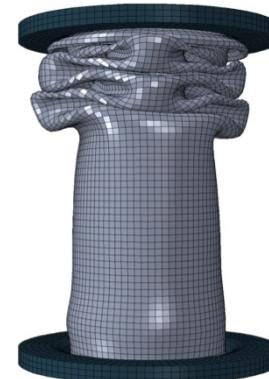
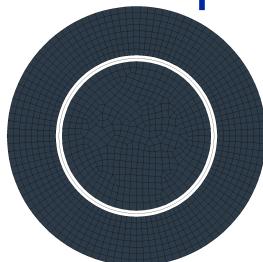
3 Piece Fixture
w/ Clamping



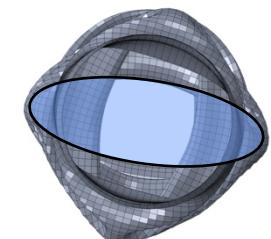
N=3



Continuous Fixture
No Clamping



N=2



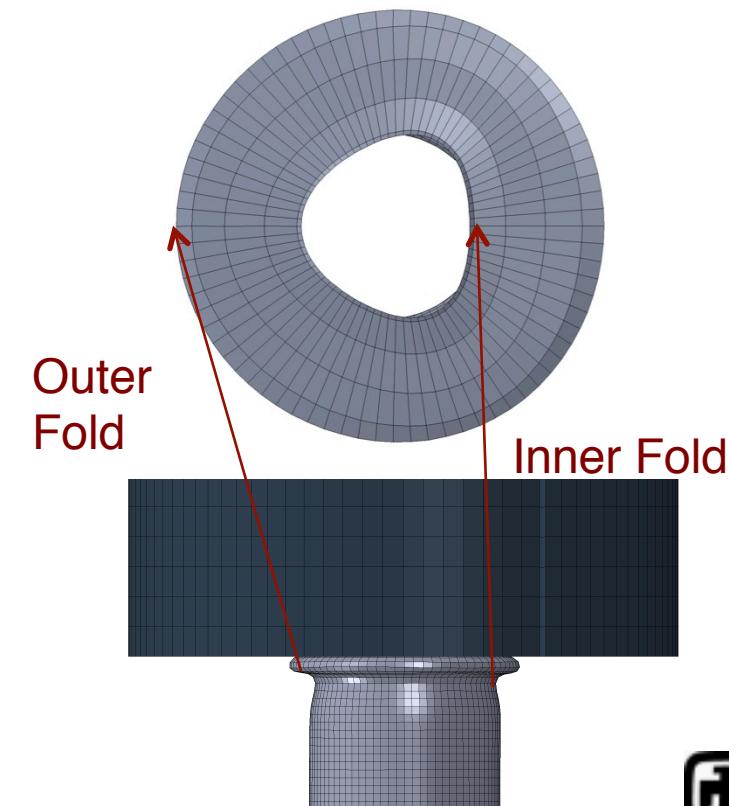


N = 3 Pattern

Tube End After
Clamping
(5x Displacement)



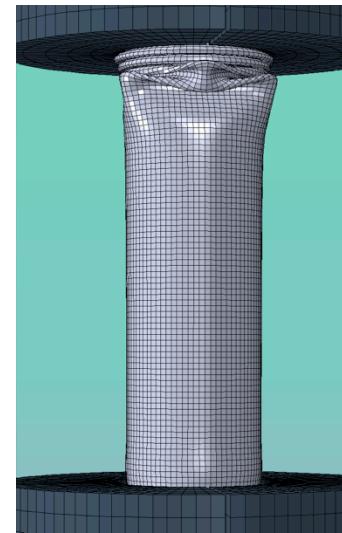
X-Section at First
Neck
(5x Displacement)



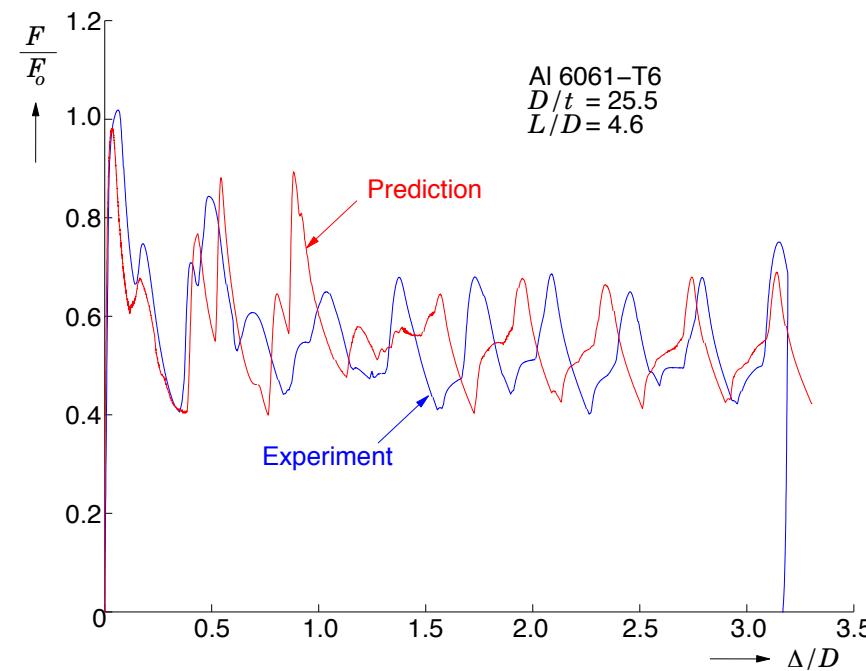
L/D = 4.6



Experiment

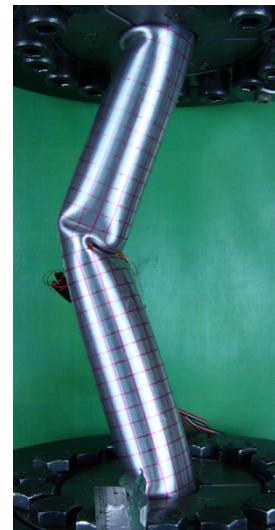


Prediction





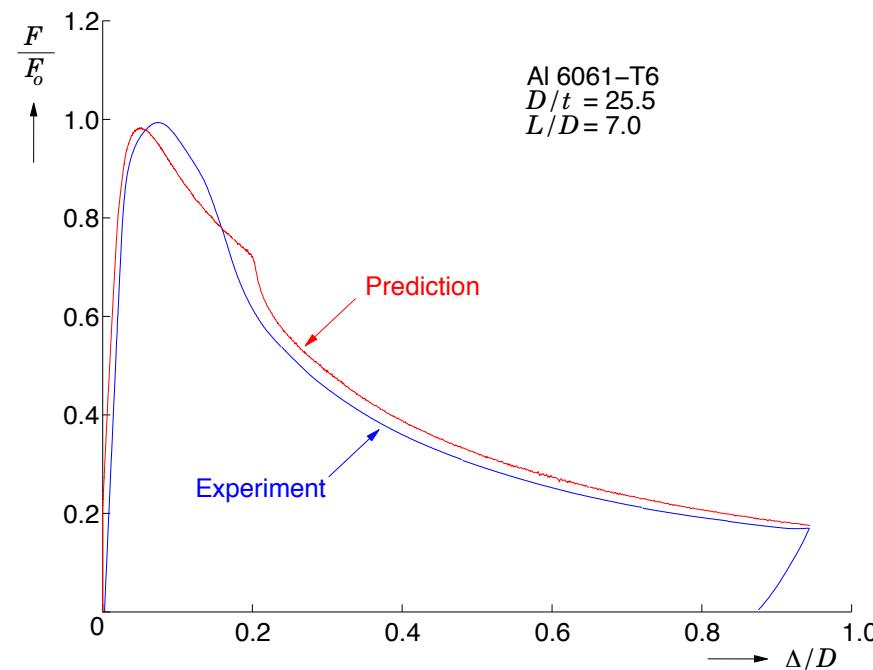
L/D = 7



Experiment



Prediction



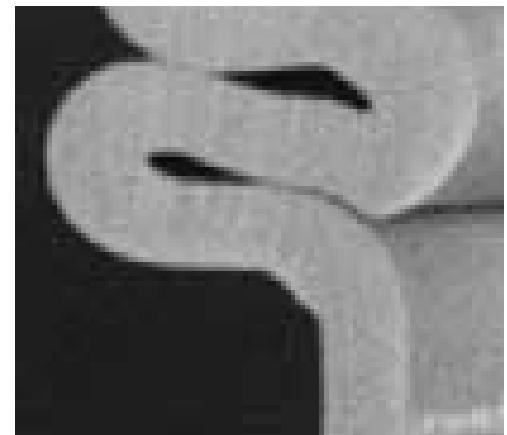
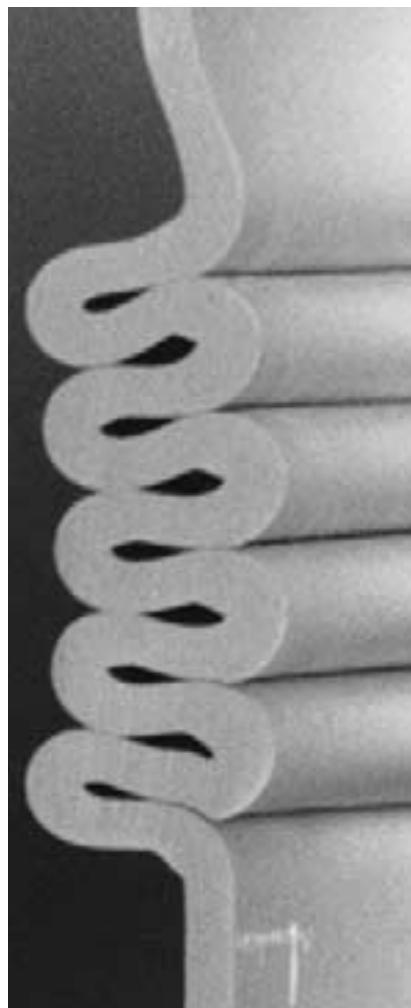
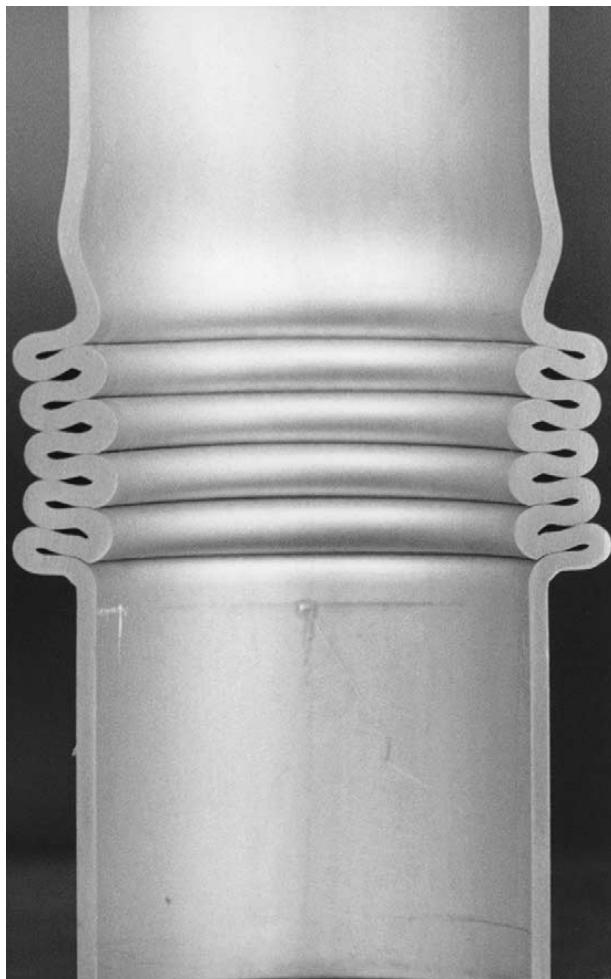


Summary of Results

L/D	Mode Experiment	Mode Prediction	$\lambda (\Delta/D)$ Experiment	$\lambda (\Delta/D)$ Prediction
2.2	N=3 / N=3	N=3	-	-
3.8	N=3 / N=3	N=3	0.352	0.388
4.6	N=3 / N=2-3	N=3	0.354	0.394
5.4	N=3 / Lateral	N=3	-	0.395
7.0	Lateral / Lateral	Lateral	-	-



Axisymmetry? Bardi et al



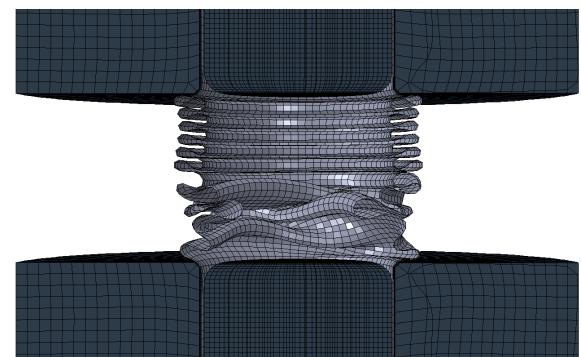
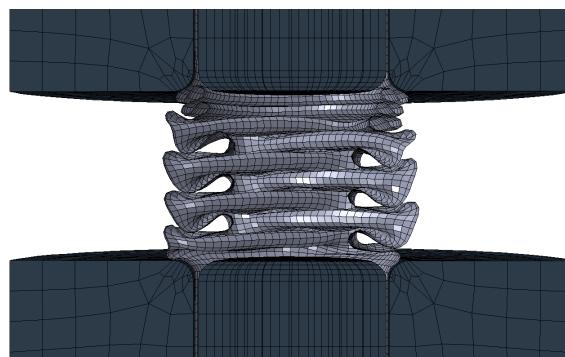
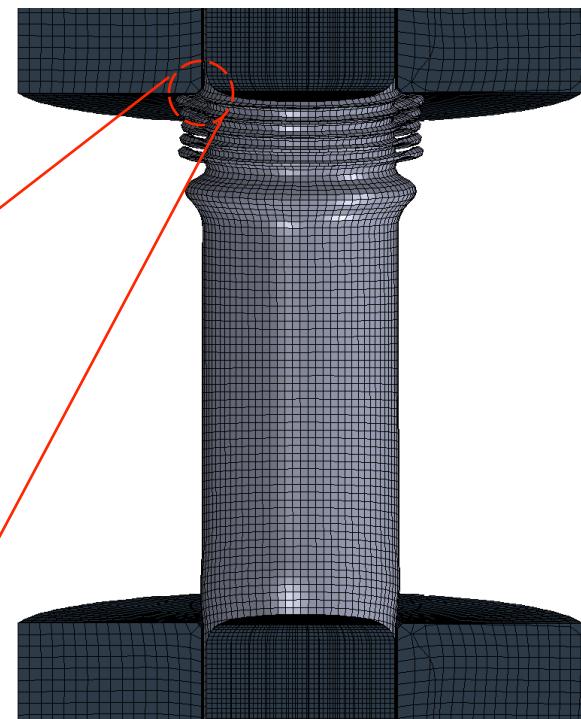


Boundary Effects

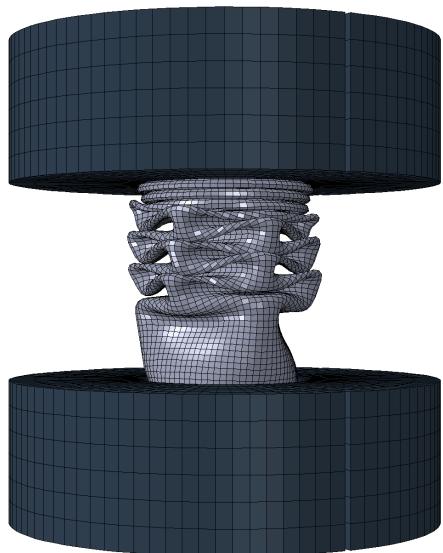
Fillet



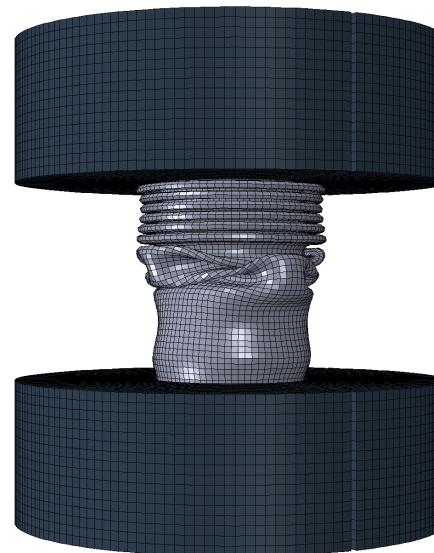
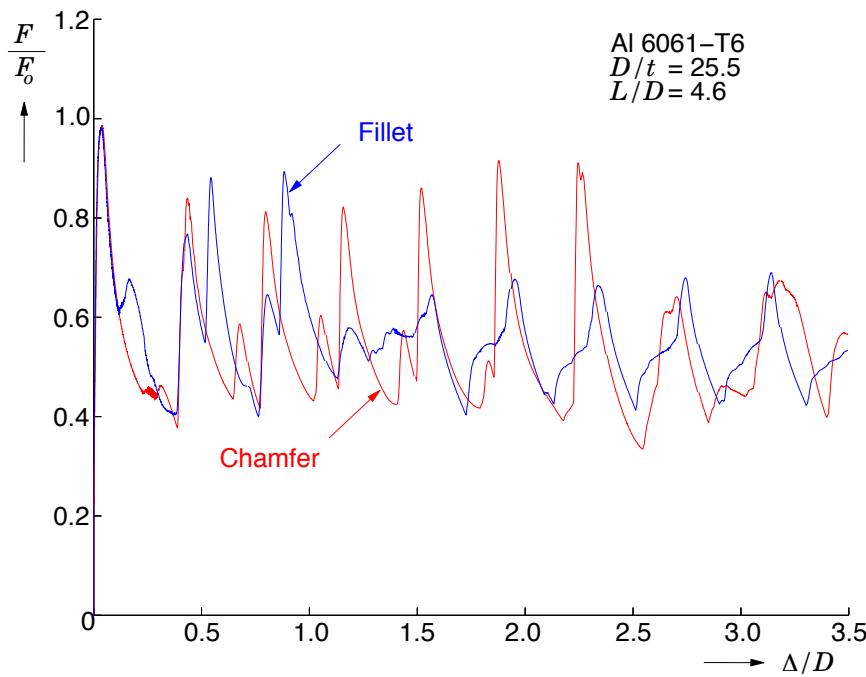
Chamfer



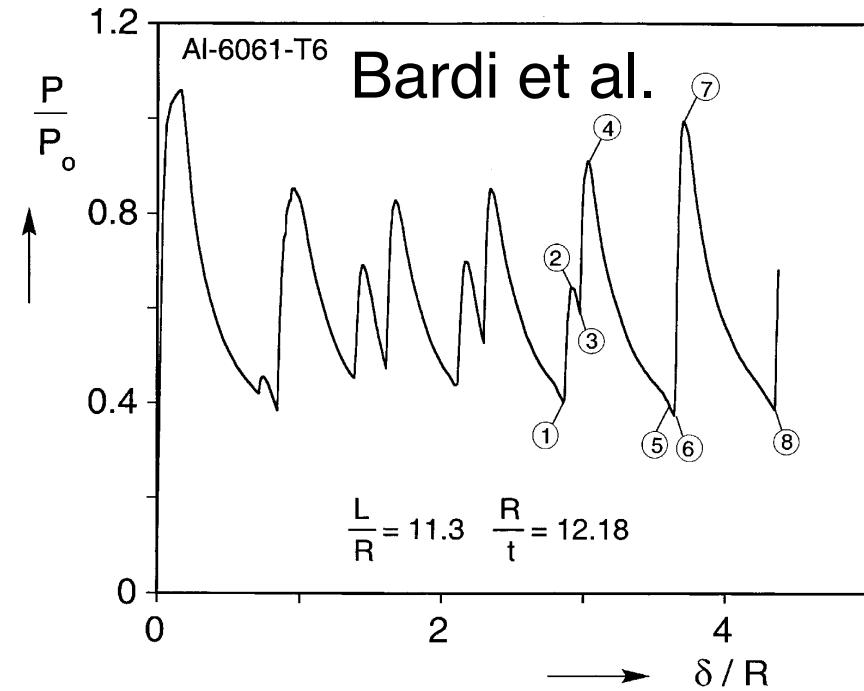
Boundary Effects



Fillet



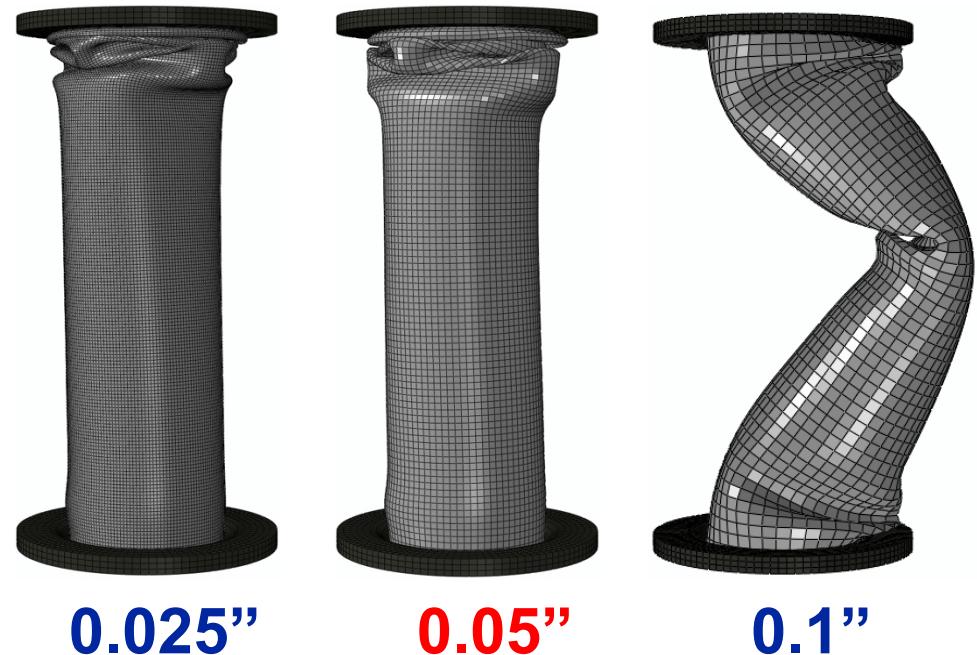
Chamfer





Sensitivity Investigations

- **Mesh Sensitivity**
 - 0.025, 0.05, 0.1 inch squares studied
- **Other Studies**
 - Clamping Pressure
 - Fixture Dimensions
- **Future Studies**
 - Hex-Based Meshes
 - Anisotropic Material





Conclusions

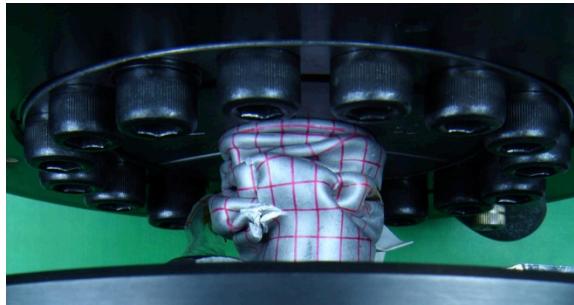
- Shell model does a reasonable job in predicting the crushing response of the tubes.
- N=3 crushing mode seems to be a consequence of the three-segmented clamping fixture and of the applied clamping pressure.
- Shell contact thickness is a model feature that probably affects the numerical results.
- Crushing mode is influenced by the geometric details of the clamping fixture. Perhaps more generally, by the geometry of preceding folds.



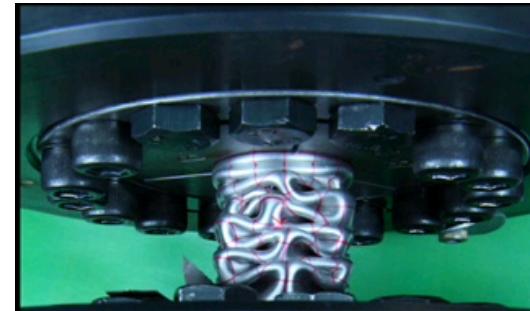
Backup Slides Below



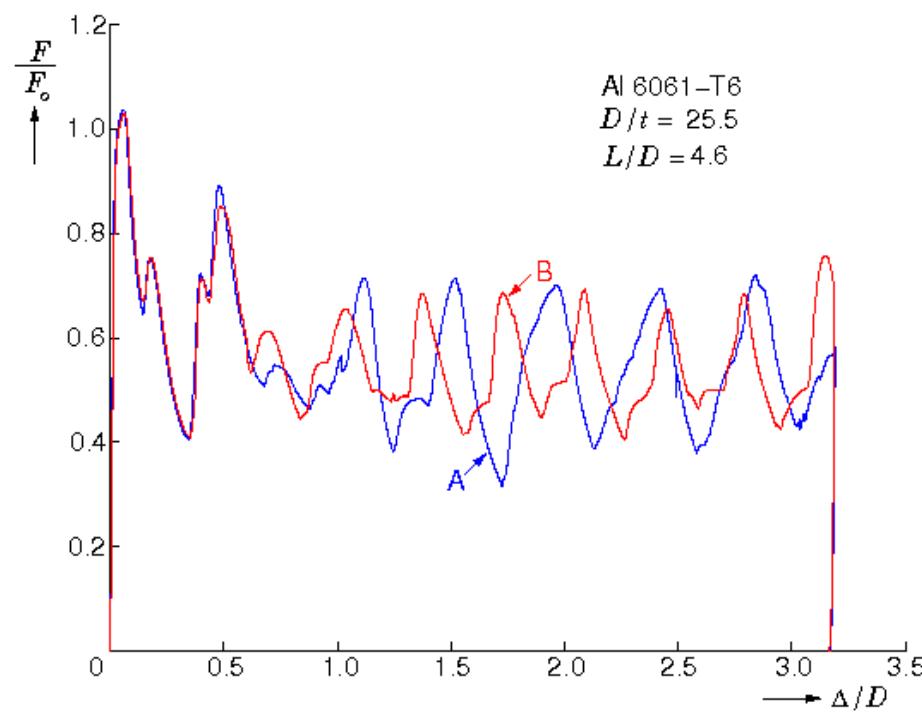
L/D = 4.6



A



B

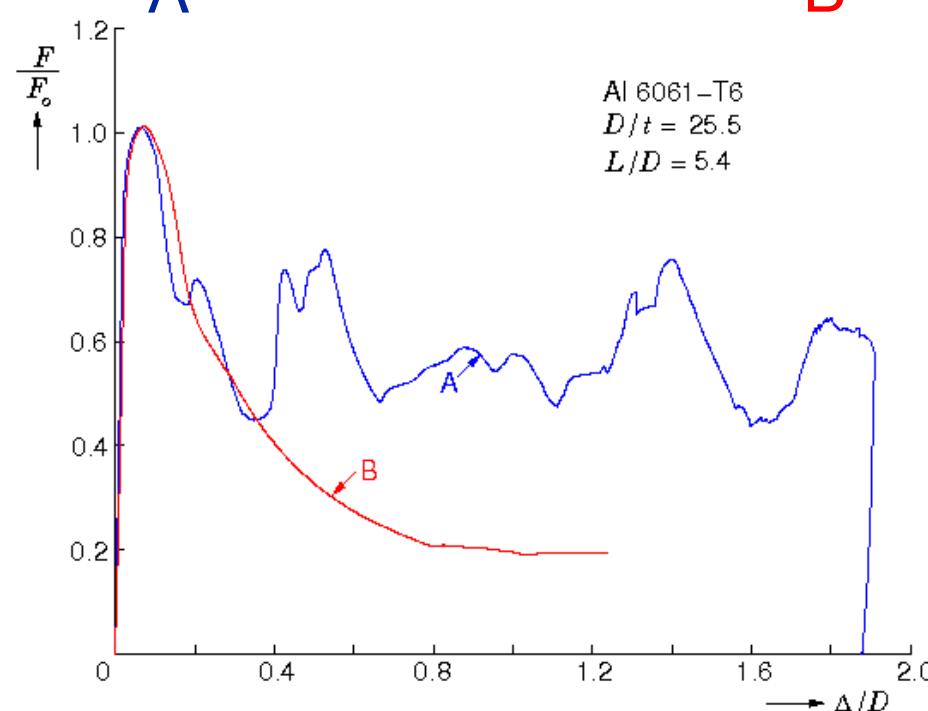


L/D = 5.4

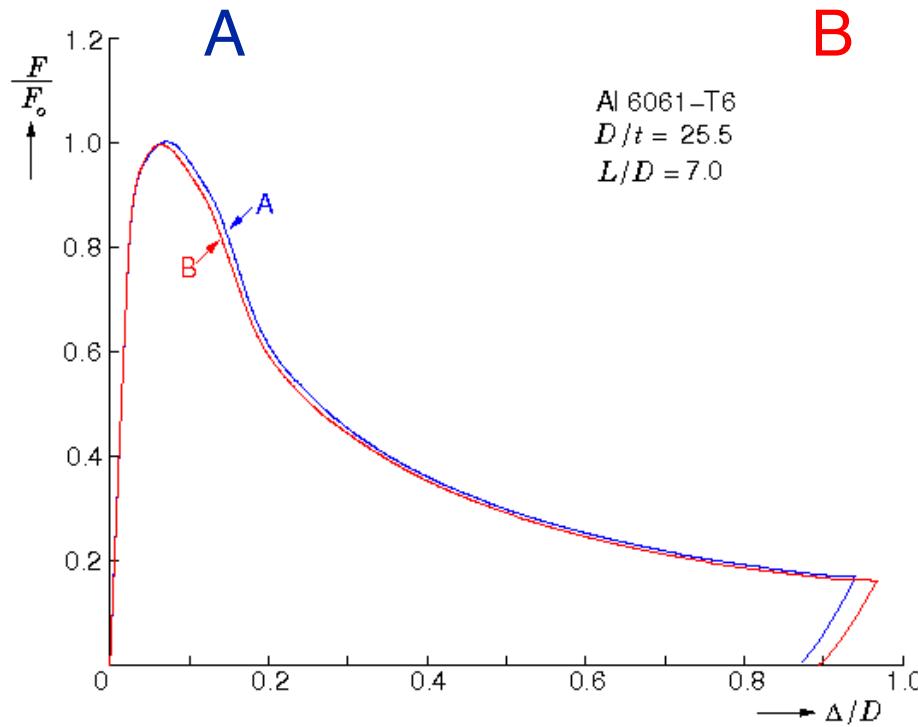


A

B



L/D = 7



Parametric Study

Clamping Pressure (PSI)	Plug Size (inches)	Mesh (inches)	Result
1250	1.15	0.05	N=3
1250	1.147	0.05	N=2
1250	1.15	0.025	N=2
2500	1.15	0.05	N=3
2500	1.147	0.05	N=3
12500	1.15	0.05	N=3
12500	1.15	0.025	N=3
12500	1.147	0.05	N=3
6250	1.15	0.025	N=3