



High Temperature Splitting Of Water And Carbon Dioxide Using Complex Oxides As A Route To Solar Fuels

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Energy security and climate change are intertwined



- To “stabilize” global CO₂ levels need > 10 TW of clean energy by 2050.
- US consumes 378 million gallons per day gasoline.
 - 0.58 TW annual average
 - Petroleum imports > 50%

- US land solar resource > 1800 TW.

Leading Petroleum Importers in 2003 (mbpd*)

United States	11.2
Japan	5.5
Germany	2.5
China	2.0

Leading Exporters

Persian Gulf	18.7
Russia	5.5
Norway	3.3
Venezuela	2.2

*millions of barrels per day

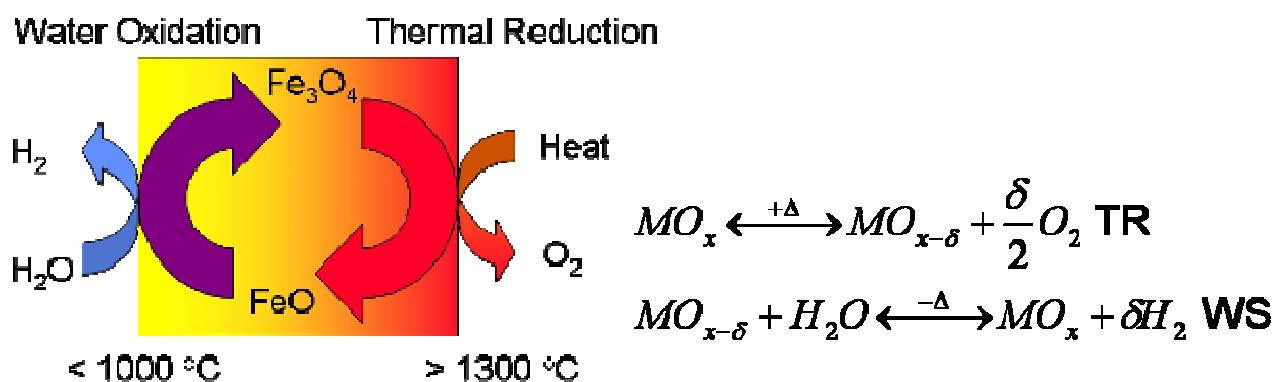
Roger Doyle, *Scientific American*, Sept. 2004.



Concentrated solar power and thermochemical cycles



“no bugs, no wires”... and no membranes

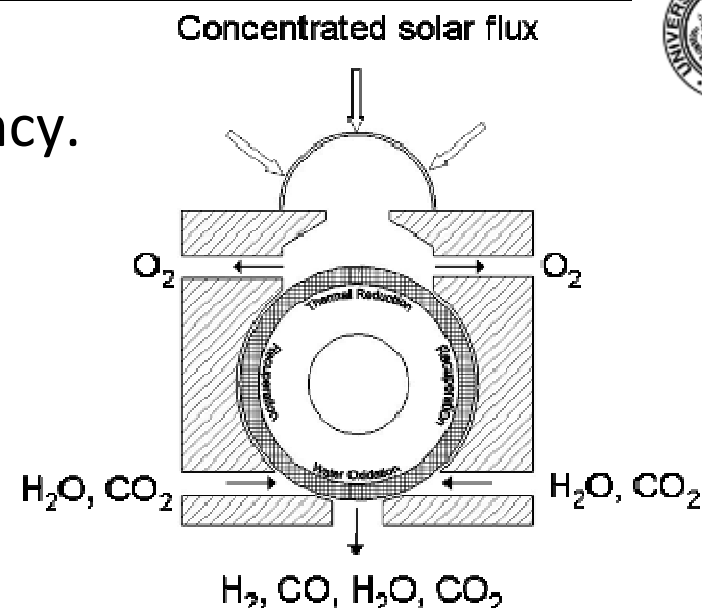


- Concentrate solar energy using conventional technology.
 - 1000 suns = 100 W/cm²
- Thermochemistry is a promising alternative to bio-fuels, PV-based electrolysis, photo-catalysis, or artificial photosynthesis.
 - Efficiency, simplicity, scalability
 - Dish Stirling engine currently holds world-record for peak efficiency (31.25% net solar-to-electric)

Key attributes of Sandia CR5 concept reactor

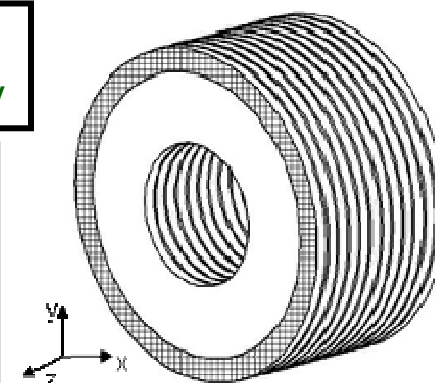
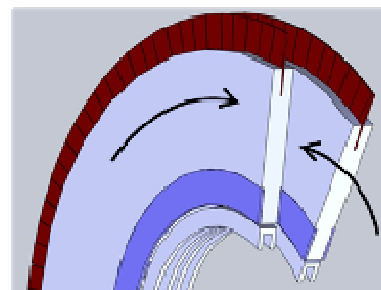


- Needed to achieve high efficiency.
 - Continuous operation on-sun.
 - Direct solar absorption.
 - Sensible energy recovery.
 - Minimal work input.
 - Intrinsic separation of products
 - H_2/CO from O_2



heat recuperation
key to high efficiency

Design challenge to effectively
balance incident solar flux, redox
kinetics, and heat recuperation to yield
an efficient thermochemical
conversion cycle

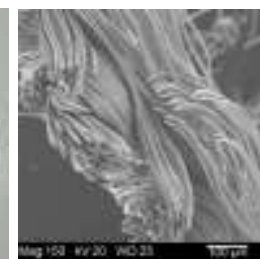
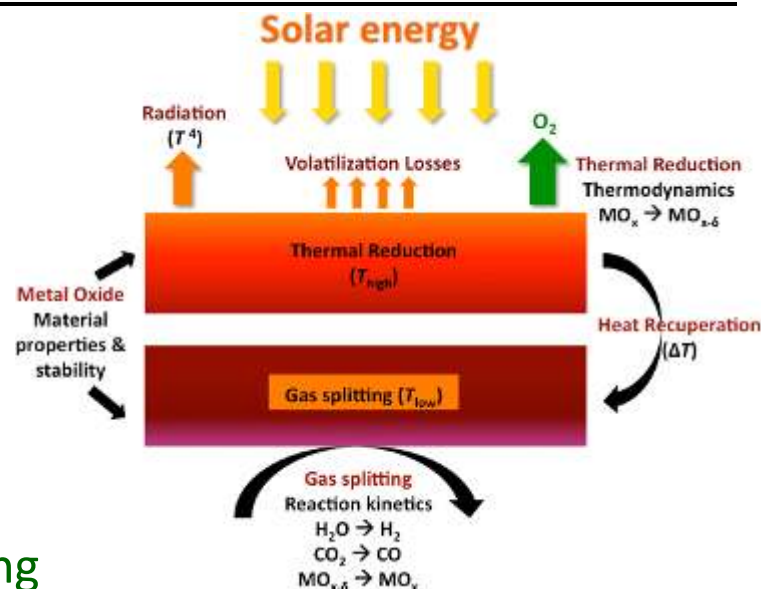


Counter-Rotating-Ring Receiver/Reactor/Recuperator (CR5)

Non-volatile metal oxide reactive structures



- Basic considerations.
 - Chemical composition
 - Macroscopic structure
 - Sunlight penetration
 - Gas transport
 - Microstructure
 - Reactive surface area
 - Structural stability and loading
- Understand complex behavior.
 - Surface/bulk reaction
 - Solid phase transport
 - Ionic species
 - Effects of dopants and supports
 - Reactivity/compatibility



Material systems currently under investigation

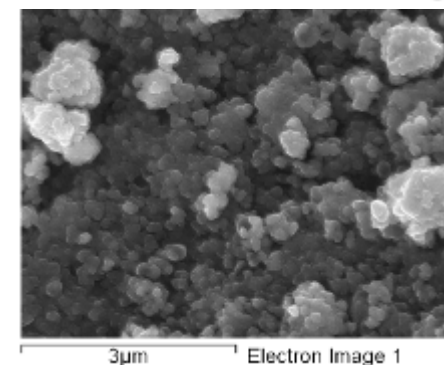
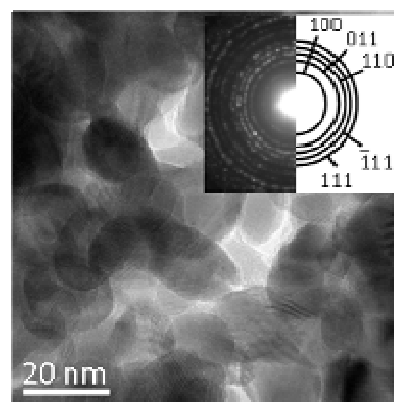
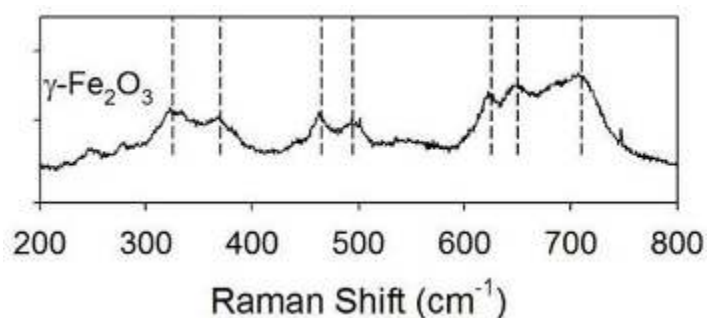


Fe_2O_3	CoFe_2O_4	$\text{MO}_x:\text{CeO}_{2-\delta}$	$\text{La}_{1-x}\text{Sr}_x\text{Cr}_{1-y}\text{Mn}_y\text{O}_{3-\delta}$	
YSZ m-ZrO_2	m-ZrO_2	10 mol% Mn, Ni, Co, Mo, & Fe	$\underline{\text{X}}$ 0.9	$\underline{\text{Y}}$ 0.5
CeO_2			0.8	
			0.7	
Al_2O_3	Al_2O_3		0.6	
			0.5	

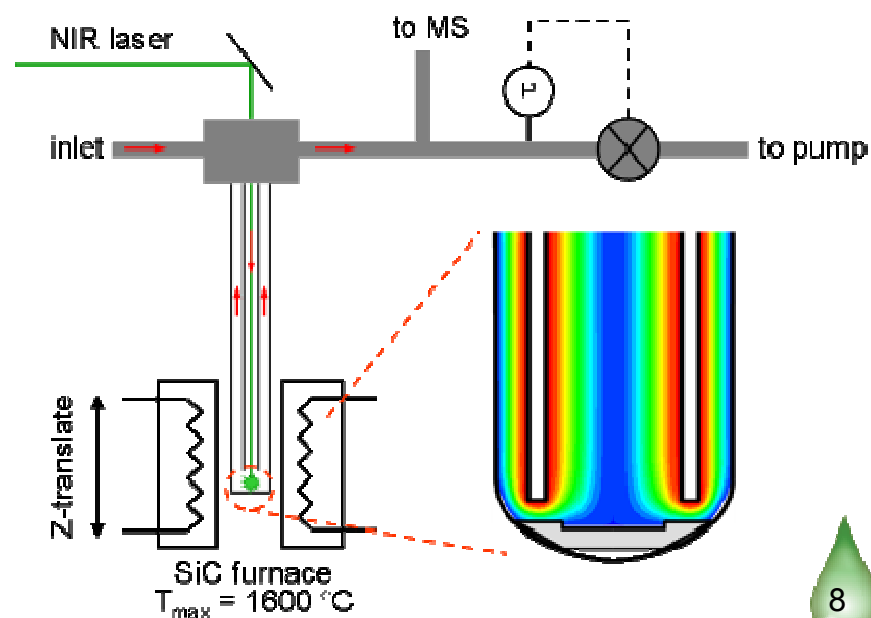
chemical and/or physical
modification required to
achieve performance
goals

- Redox cycle chemistries.
 - Chemical systems
 - $\text{M}^{+n}/\text{M}^{+(n+1)}$ redox couples
 - $\text{MO}_{n-\delta}$ non-stoichiometric oxides
 - CU “hercynite”
 - Supports
 - m-ZrO_2 , YSZ, CeO_2 , Al_2O_3

Experimental approach



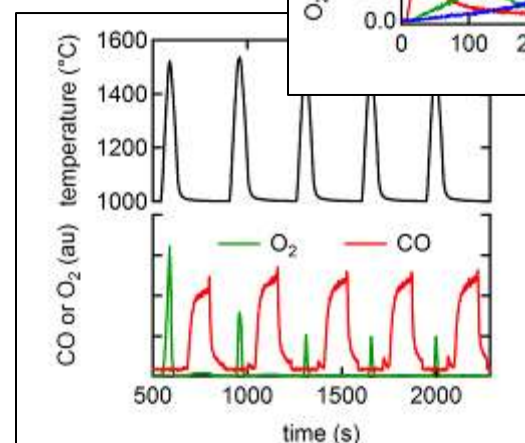
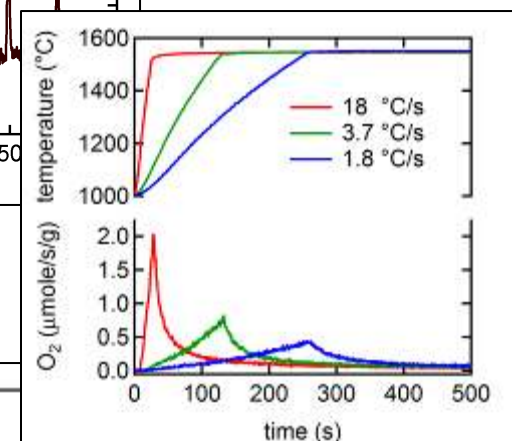
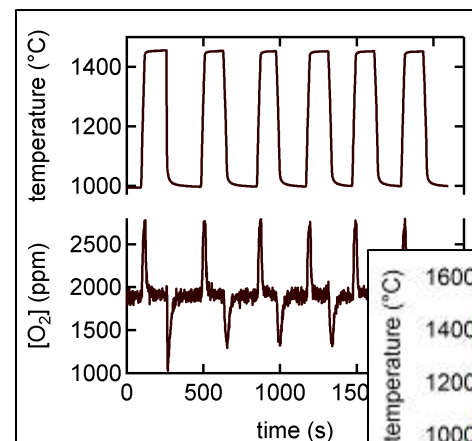
- Material properties.
 - BET surface area
 - SEM-EDX, TEM-EELS, XRD
- Surface analysis.
 - Surface Raman, XPS
- Kinetic measurements.
 - Stagnation flow reactor
 - 500 W CW NIR laser heating
 - Modulated beam mass spectrometer



Oxidation and reduction behavior



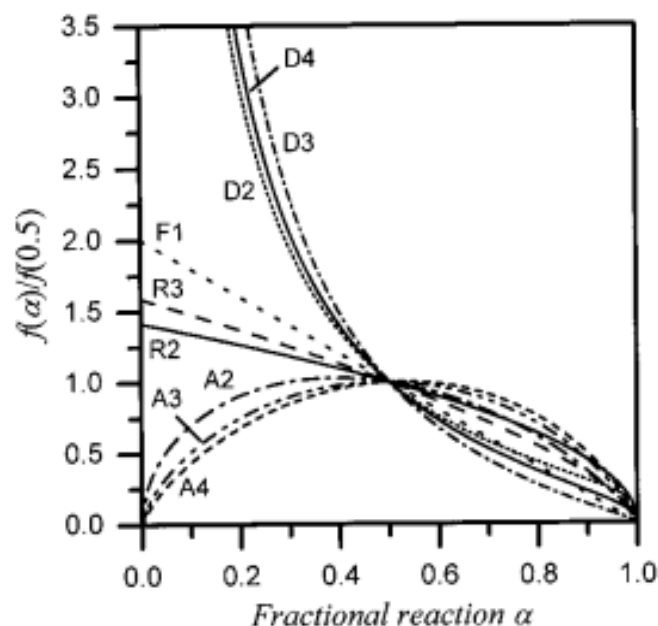
- Screen for O₂ uptake and release.
 - System viability
- Resolve thermal reduction behavior.
 - Variable heating rates
- Resolve gas splitting behavior.
 - Variable T, P, [OX]
- Analysis.
 - Rate limiting mechanisms
 - Kinetic models
 - Material stability
 - Cycle performance



Solid-state kinetic theory



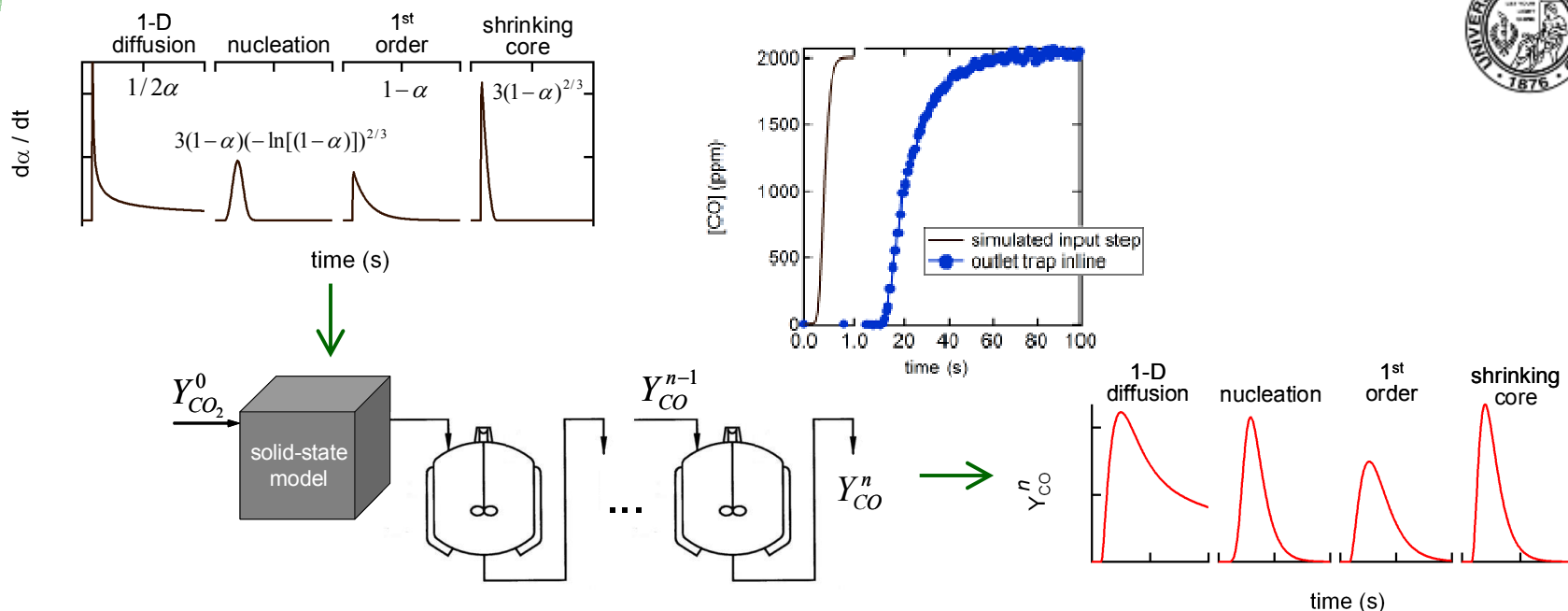
Khawam and Flanagan, *J. Phys. Chem. B*, **110**, 17315 (2006)



model	differential form $f(\alpha) = 1/k \, d\alpha/dt$	integral form $g(\alpha) = kt$
nucleation models		
power law (P2)	$2\alpha^{1/2}$	$\alpha^{1/2}$
power law (P3)	$3\alpha^{2/3}$	$\alpha^{1/3}$
power law (P4)	$4\alpha^{3/4}$	$\alpha^{1/4}$
Avrami–Erofev (A2)	$2(1-\alpha)[- \ln(1-\alpha)]^{1/2}$	$[- \ln(1-\alpha)]^{1/2}$
Avrami–Erofev (A3)	$3(1-\alpha)[- \ln(1-\alpha)]^{2/3}$	$[- \ln(1-\alpha)]^{1/3}$
Avrami–Erofev (A4)	$4(1-\alpha)[- \ln(1-\alpha)]^{3/4}$	$[- \ln(1-\alpha)]^{1/4}$
Prout–Tompkins (B1)	$\alpha(1-\alpha)$	$\ln[\alpha/(1-\alpha)] + c$
geometrical contraction models		
contracting area (R2)	$2(1-\alpha)^{1/2}$	$1 - (1-\alpha)^{1/2}$
contracting volume (R3)	$3(1-\alpha)^{2/3}$	$1 - (1-\alpha)^{1/3}$
diffusion models		
1-D diffusion (D1)	$1/(2\alpha)$	α^2
2-D diffusion (D2)	$-[1/\ln(1-\alpha)]$	$((1-\alpha)\ln(1-\alpha)) + \alpha$
3-D diffusion–Jander (D3)	$[3(1-\alpha)^{2/3}]/[2(1-(1-\alpha)^{1/3})]$	$(1-(1-\alpha)^{1/3})^2$
Ginstling–Brounshtein (D4)	$3/[2((1-\alpha)^{-1/3}-1)]$	$1-(2/3)\alpha-(1-\alpha)^{2/3}$
reaction-order models		
zero-order (F0/R1)	1	α
first-order (F1)	$(1-\alpha)$	$-\ln(1-\alpha)$
second-order (F2)	$(1-\alpha)^2$	$[1/(1-\alpha)] - 1$
third-order (F3)	$(1-\alpha)^3$	$(1/2)[(1-\alpha)^{-2} - 1]$

- Master Plot used to screen rate controlling mechanism(s).
 - Applied to any measure of the extent of reaction (α).
- Extract kinetic parameters from isoconversion analysis.
 - Model independent

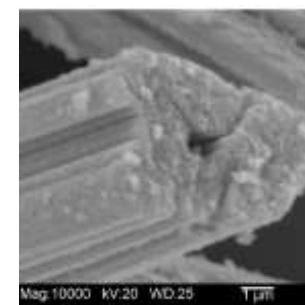
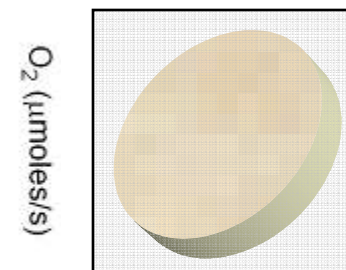
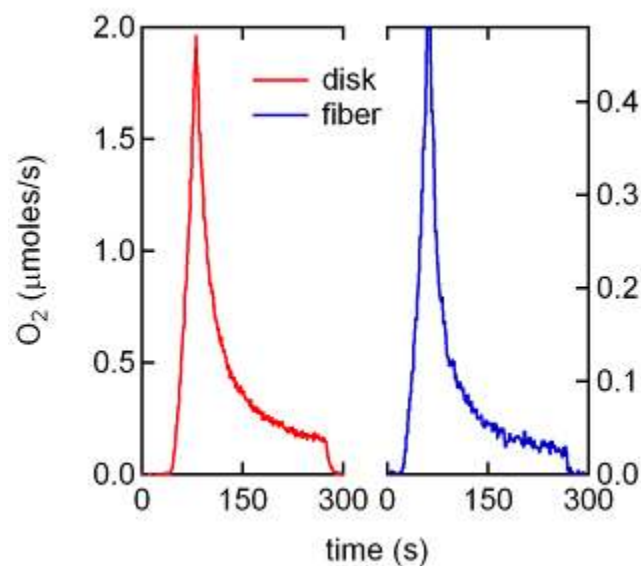
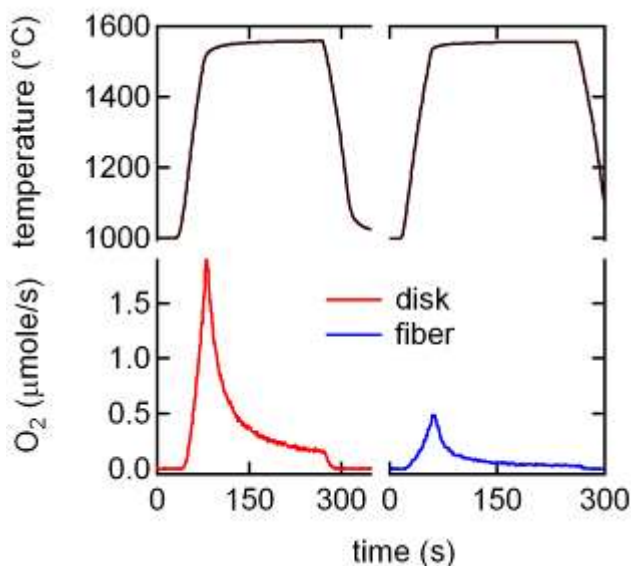
Model-based approach to evaluating kinetic behavior



- CSTR model accounts for dispersion and detector lag.
 - Deconvolute experimental effects from O_2 , H_2 , and CO signals
- Governing equations constitute a system of DAEs.
- Mathematica™ based optimization.
 - Least squares objective function
 - Stochastic algorithms search for best fit model and kinetic parameters
 - Differential Evolution, Simulated Annealing

Transition metal doped CeO_2

Thermal reduction of CeO_2 very rapid



- Disk 1000 μm thick.
- Fiber diameter $\sim 10 \mu\text{m}$.
- Solid-state dynamics at *these length scales and heating rates* do not limit reduction kinetics.
 - Thermal conduction, vacancy diffusion, surface chemistry

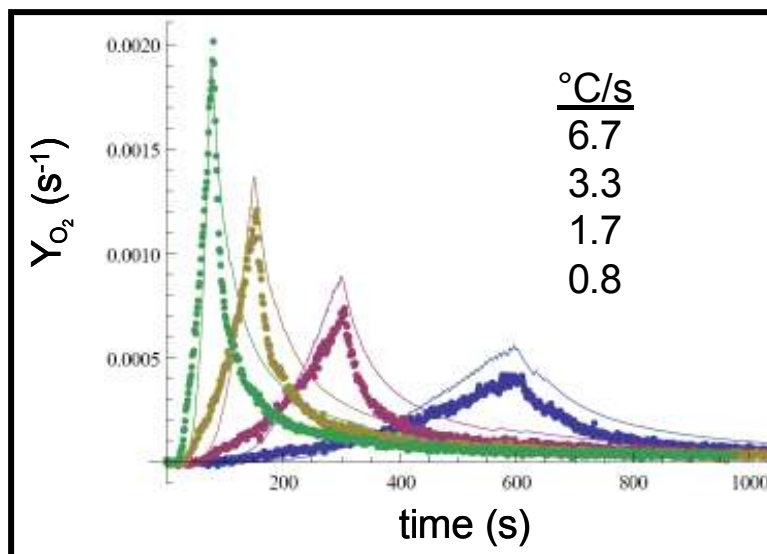
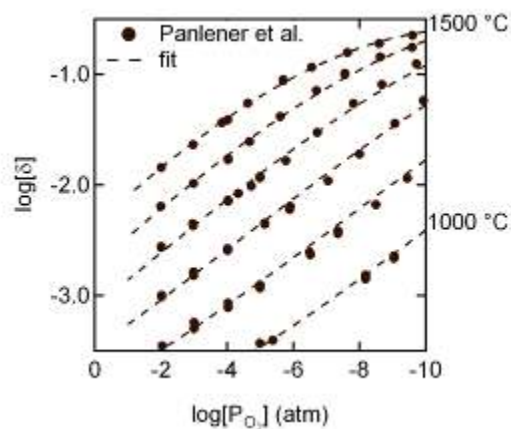
mass (mg)	mole O ($\times 10^{-6}$)	δ
960	220	0.039
207	48	0.039

Relatively simple kinetic model for CeO_2 reduction



$$\frac{d\delta}{dt} = k_1 \left(\frac{T}{T_1} \right)^{\beta_1} \exp[-E_1 / RT] \cdot (\delta_{eq} - \delta)^{m_1}$$

$$\delta_{eq} = f(\text{Log}[P_{O_2}], T)$$

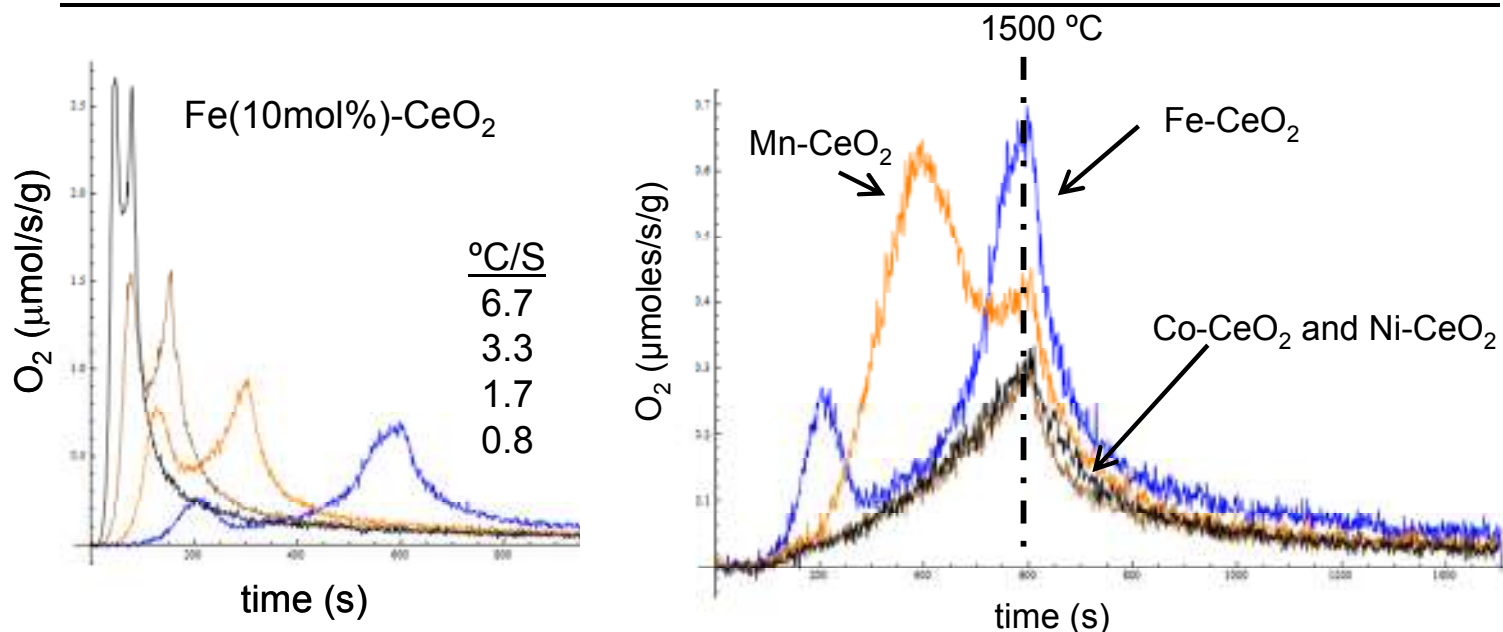


$$\delta = 0.048$$

- Incorporated into engineering models to predict CR5 performance

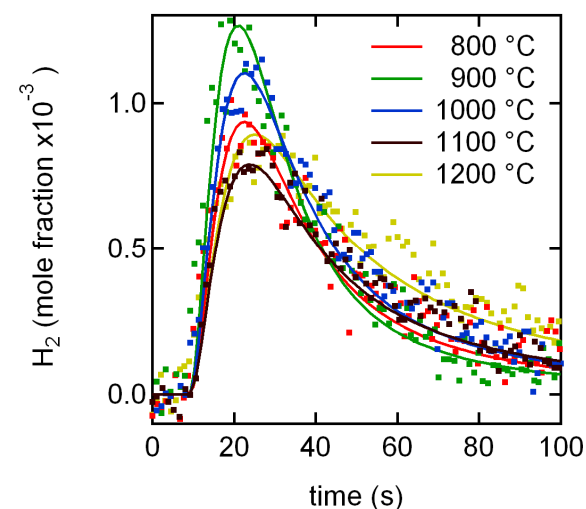
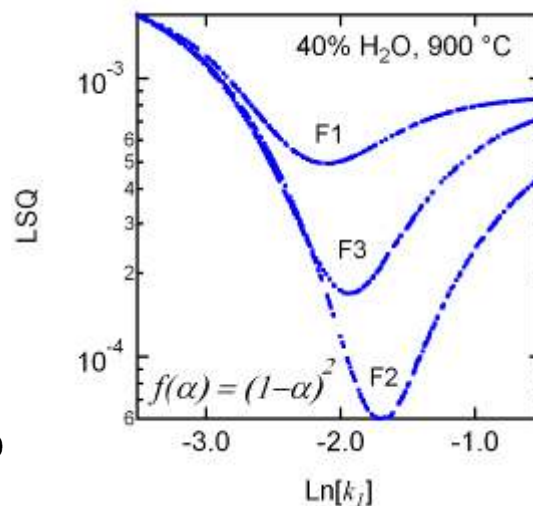
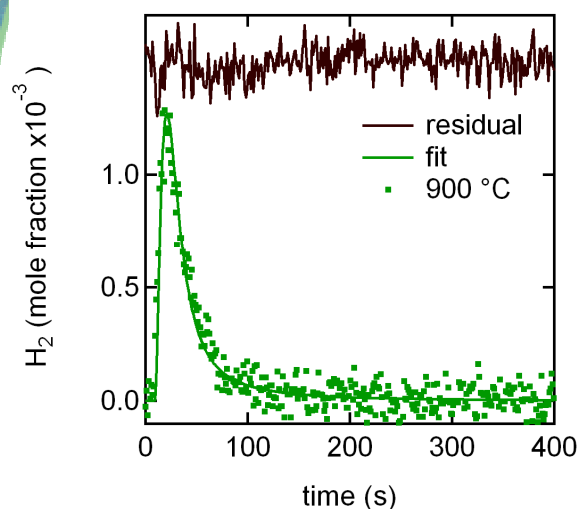
"mass"	"temp"	"[oxid]"	"total O2"
0.4129	1503.67	0	140.244
0.4129	1500.74	0	137.743
0.4129	1503.79	0	141.993
0.4129	1503.75	0	143.211

Reduction behavior of transition-metal doped CeO_2 powders



- Goal is to lower the thermal reduction temperature.
 - Destabilize the fluorite crystal structure
- O_2 evolution complex for Mn and Fe doped CeO_2 .
 - Compound formation and phase segregation possible
- Significantly more O_2 evolved per unit mass of material.
 - Mn and Fe variants at 10 mol% but O_2 capacity $> 2\times$

H₂O oxidation of CeO₂ exhibits 2nd order behavior



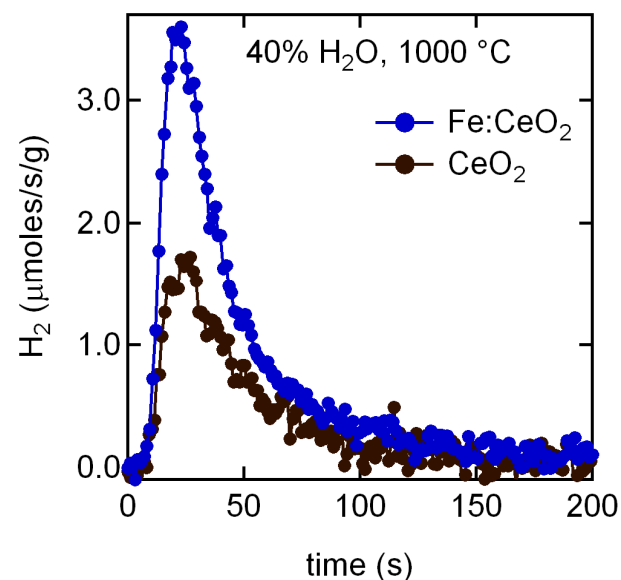
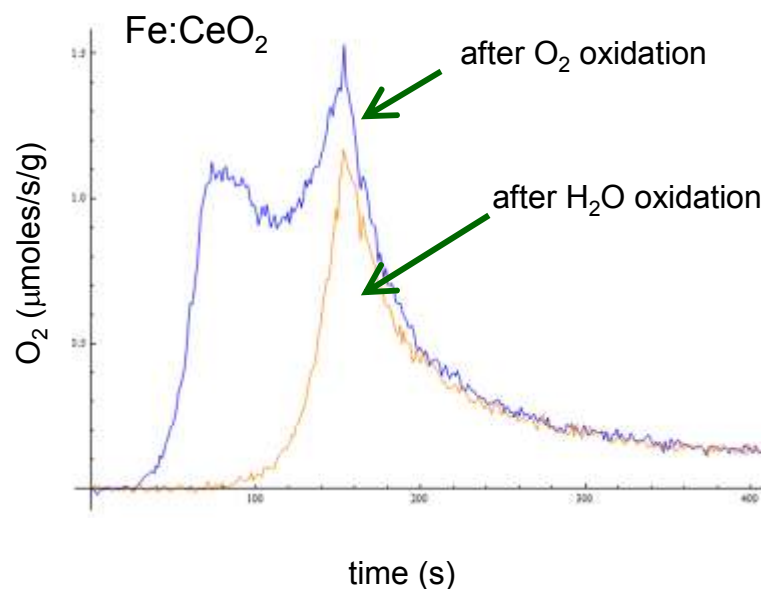
$$\frac{d\alpha_1}{dt} = k_1[Y_{CO_2}^0(t - t_{shift})] \cdot f(\alpha_1)$$

- H₂ production rate peaks at 900 °C.
- Well defined LSQ minimum for the F2 model over all T.

H₂O splitting on Fe-doped CeO₂

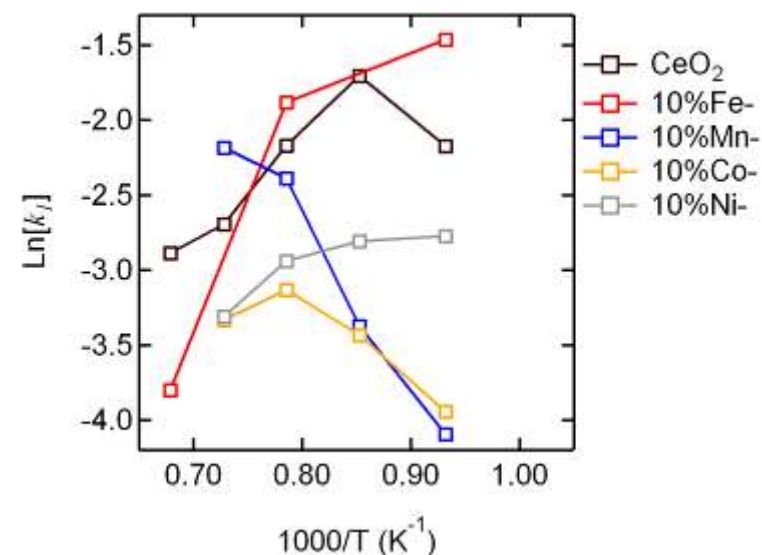
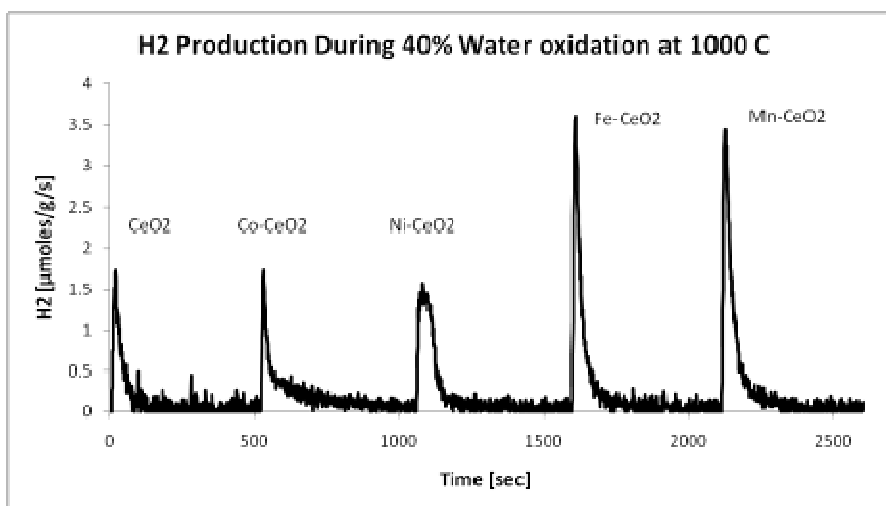


TR to 1500 °C @ 3.3 °C/s



- O₂ evolution post-H₂O oxidation reveals that active sites in doped system re-oxidize at different rates.
- Presence of 10mol% Fe increases net H₂ production.

Dopants have a dramatic effect on H₂ production rates



- Peak temperature in volcano plot shifts.
- Effect on net hydrogen production varies.
- Trends not obvious.
 - All multivalent (2⁺– 4⁺, or 2⁺– 6⁺ for Mn)
 - All have effective ionic radii << Ce³⁺ and Ce⁴⁺

Fe and Mn enhance sintering of powders during redox

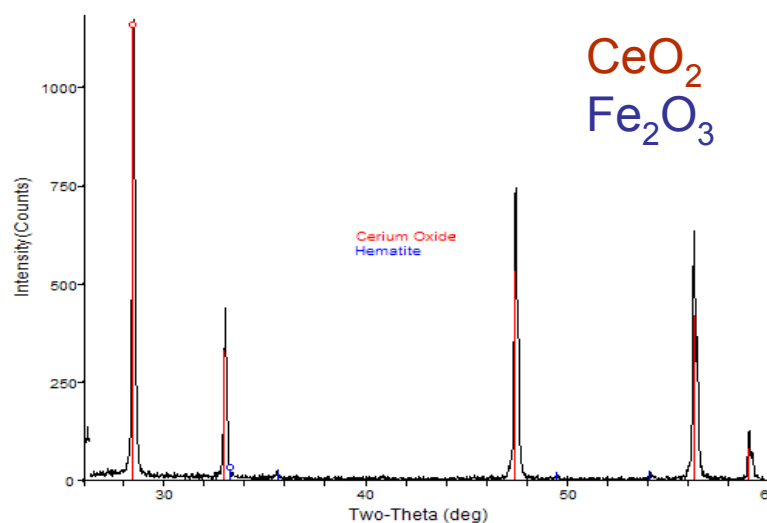


- Calcine in air @ 1400 °C for 36 hrs.
 - XRD patterns show little evidence of other phases
 - Material is a loose packed powder
- TR in He at 1500 °C followed by H₂O oxidation at 1000 °C.
 - Color darkens
 - Material sinters
 - Need to complete analysis
 - Composition and morphology
- Fe and Mn-doped ceria not likely a viable strategy despite greater redox capacity.
 - Slow kinetics on “low energy” O-site
 - Severe problems with sintering/reactivity with ceramics

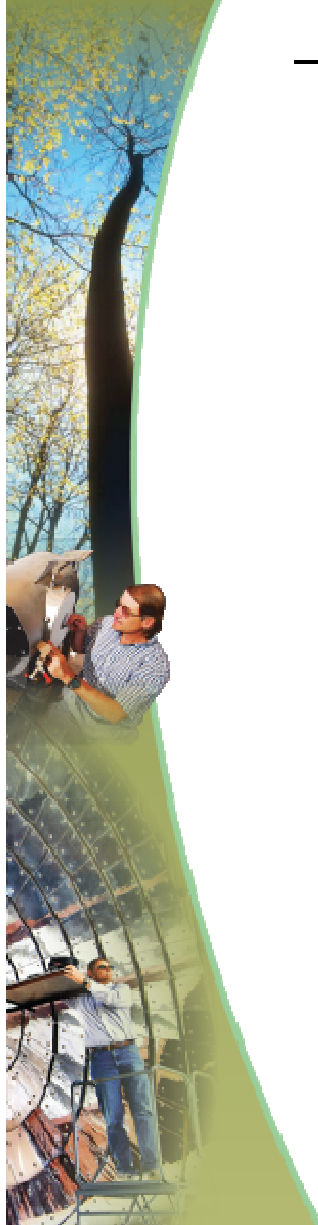
before



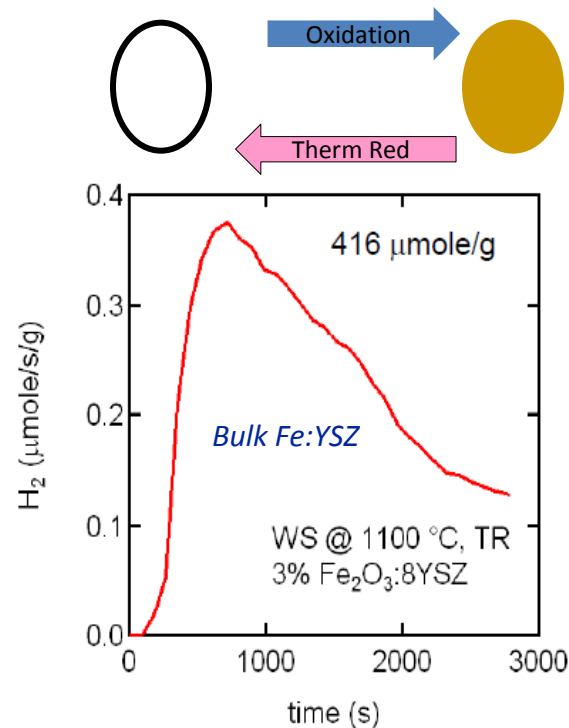
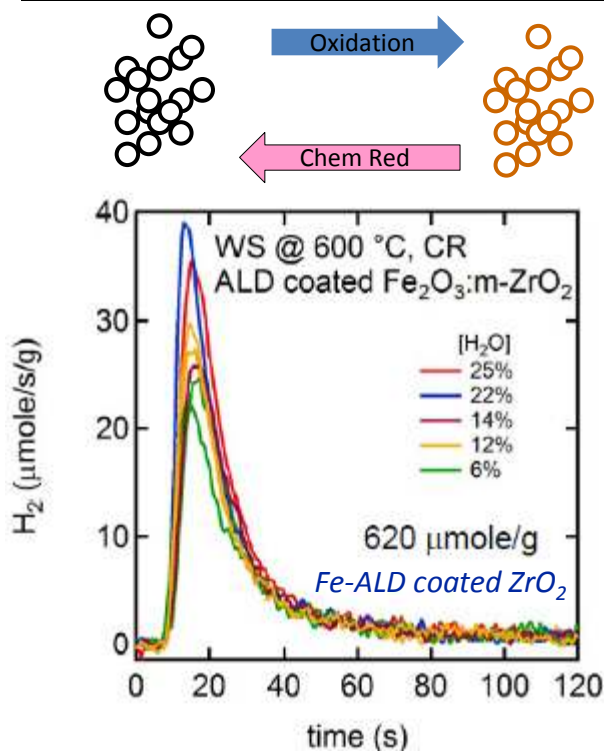
after



Fe in YSZ



High surface area/small dimension structures desirable

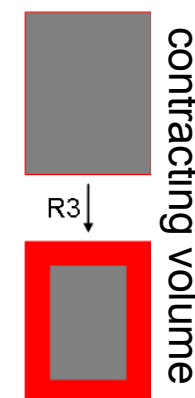
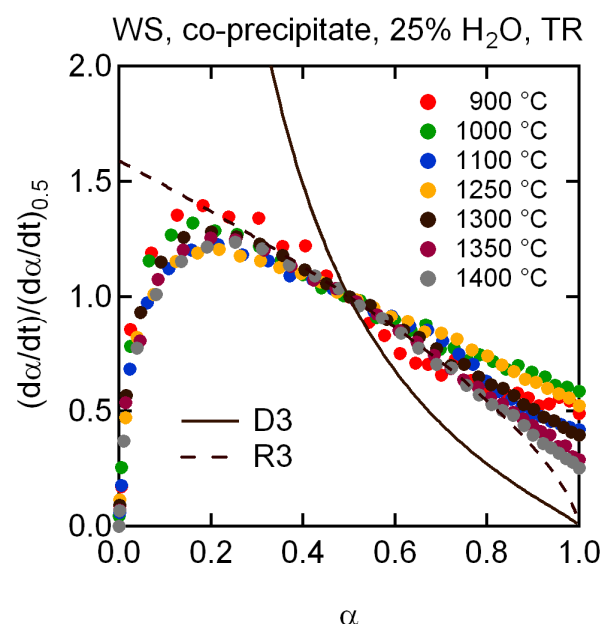
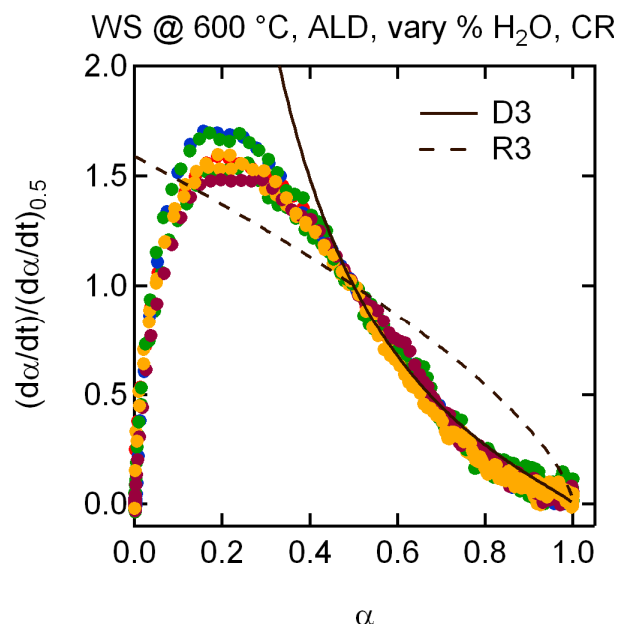
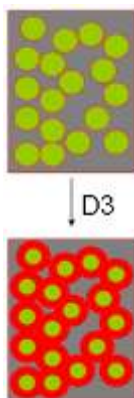


- Rates for water oxidation highly dependent on reactive structure.
 - Different manifestations of $\text{Fe}^{2+}/\text{Fe}^{3+}$ redox couple
 - ALD thin film peak H_2 production rate 100× faster than Fe dissolved in YSZ

Rate controlling mechanisms revealed through MP analysis

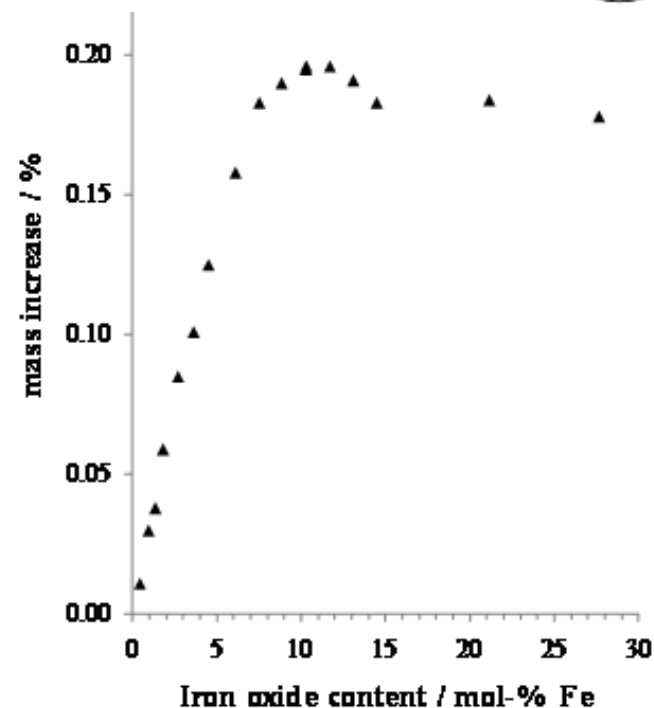
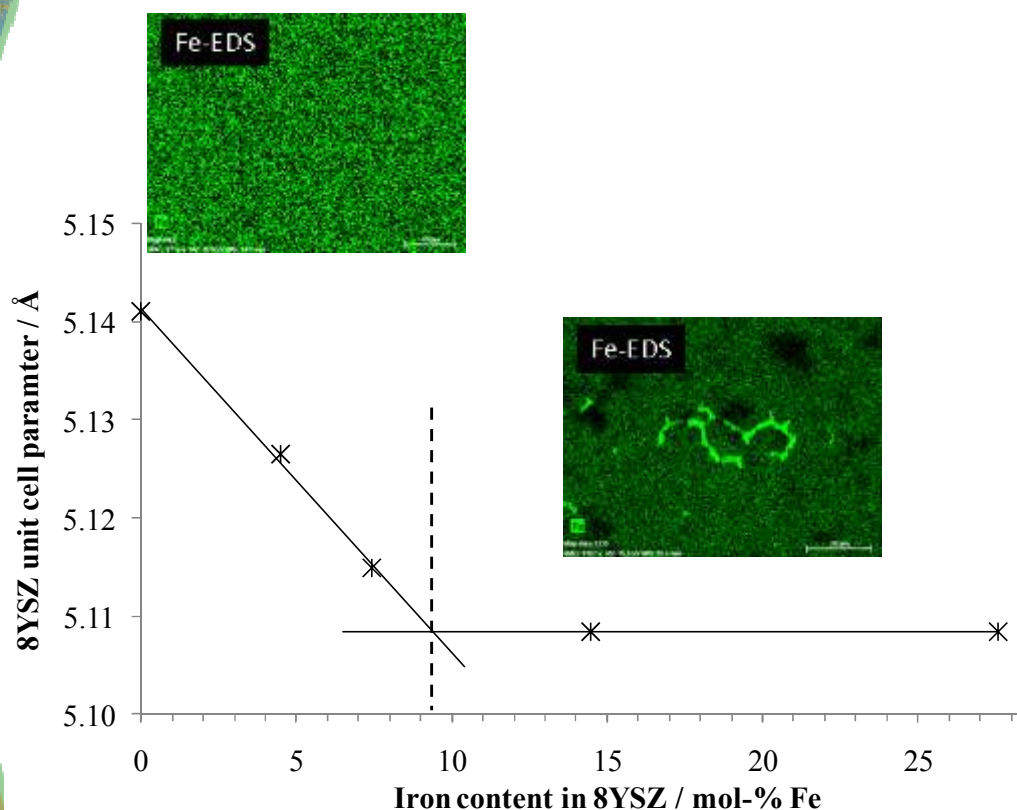


3-D diffusion



- Thin film structure results from ALD films.
 - Expect diffusion limited behavior (D3)
- Homogenous structure results from co-precipitate.
 - Uniform dispersion of Fe cation
 - Expect contracting volume behavior (R3)

Iron solubility in 8YSZ limits performance



- Ferrite cycle desirable due to greater redox capacity compared to ceria.
 - Higher efficiency if iron utilization can be improved

Summary



- Solid-state kinetic models show promise for describing oxidation and reduction behavior.
 - Redox models incorporated into CR5 simulation tools
- Cerium oxide cycle.
 - Facile reduction kinetics
 - Complex redox chemistry evident when doped with various transitional metals (especially Fe and Mn)
- Ferrite cycle.
 - More desirable than ceria if higher effective mass loading can be realized
 - Oxidation rates can be manipulated by choice of reactive structure
- Sandia remains committed to demonstrating greater than 2% net solar-to-fuel conversion efficiency in the CR5 testbed before the end of 2011.
 - 18 KW system with continuous CO production

Thank you for your attention.

Questions?