

FINITE ELEMENT MODELING AND RAY TRACING OF PARABOLIC TROUGH COLLECTORS FOR EVALUATION OF OPTICAL INTERCEPT FACTORS WITH GRAVITY LOADING

Joshua M. Christian and Clifford K. Ho

**Concentrating Solar Technologies Department
Sandia National Laboratories
Albuquerque, NM 87185**

jmchris@sandia.gov





Overview

- **Introduction**
- **Finite Element Analysis**
- **Ray Tracing**
- **Conclusions and Future Work**

LS-2 Introduction

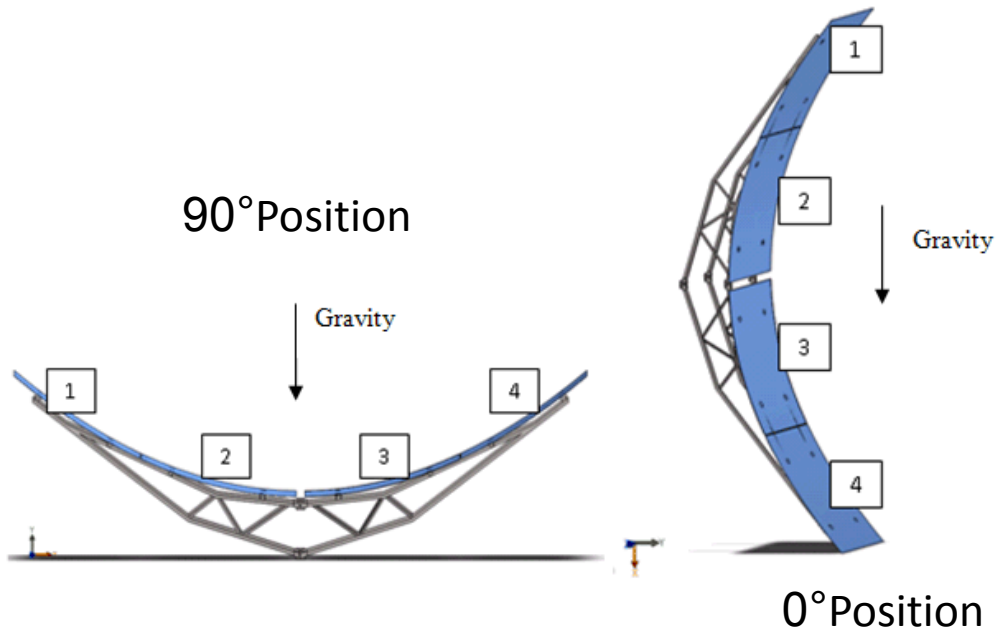


Photo courtesy of NSTTF photo database

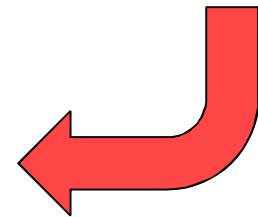
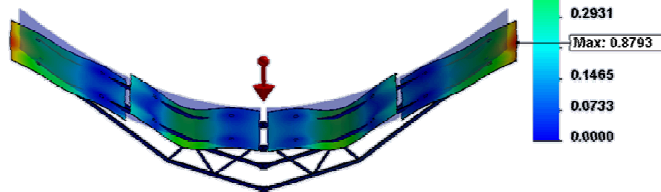
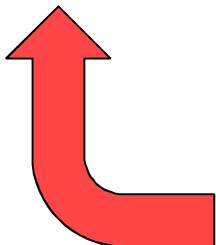
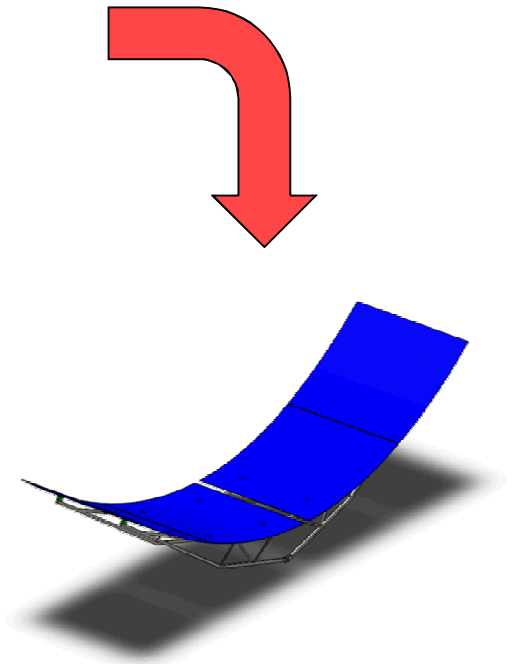
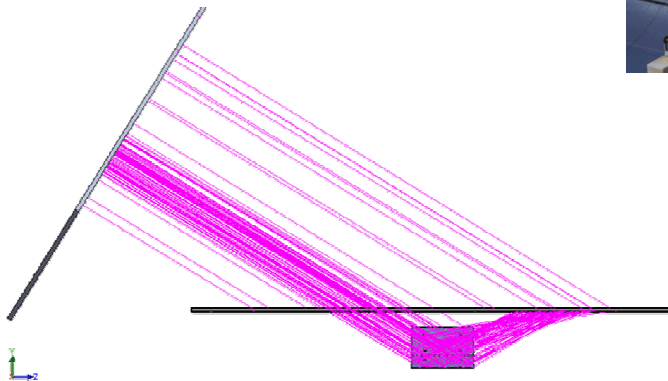
LS-2 parabolic trough (LUZ Industries)

- Mirror aperture = 5 m
- Focal length = 1.49 m
- Five mirror columns on single module

Procedure



Photo courtesy of NSTTF photo database



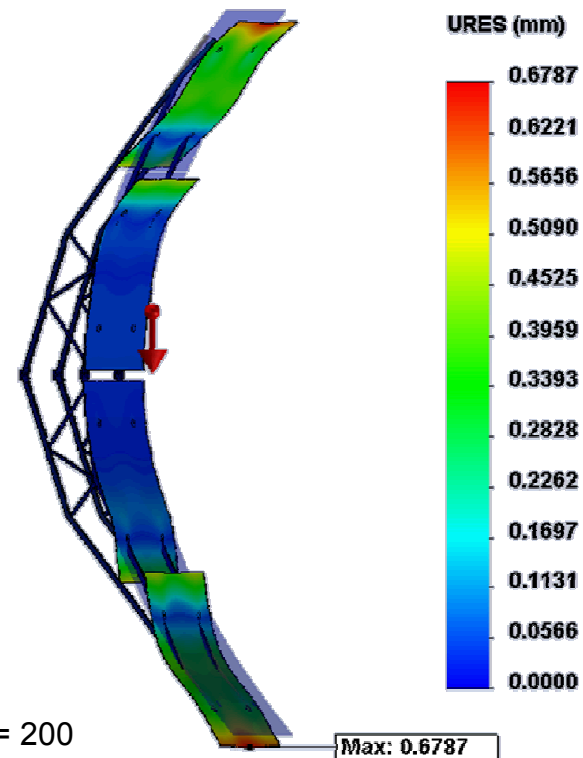
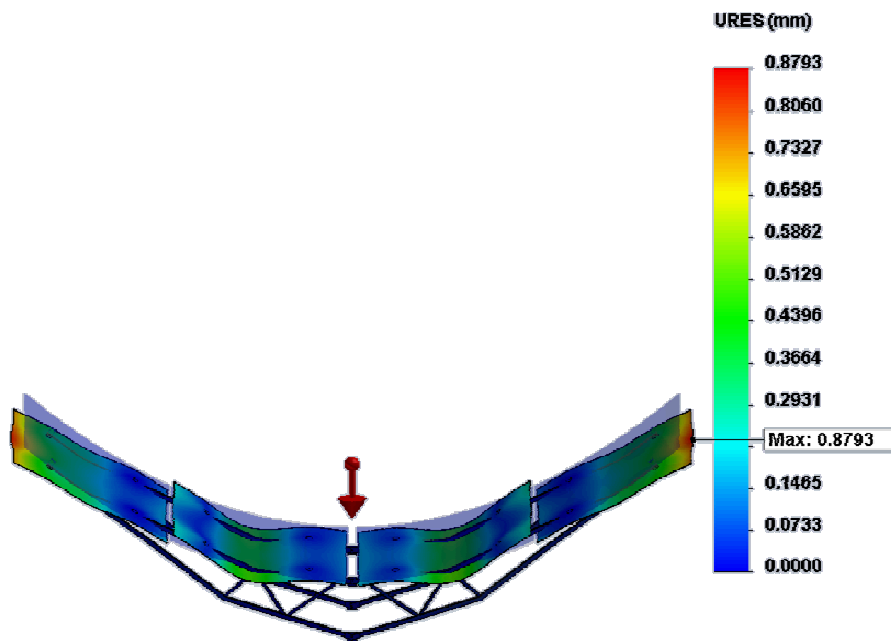


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LS-2 Analysis: Predicting Deformation

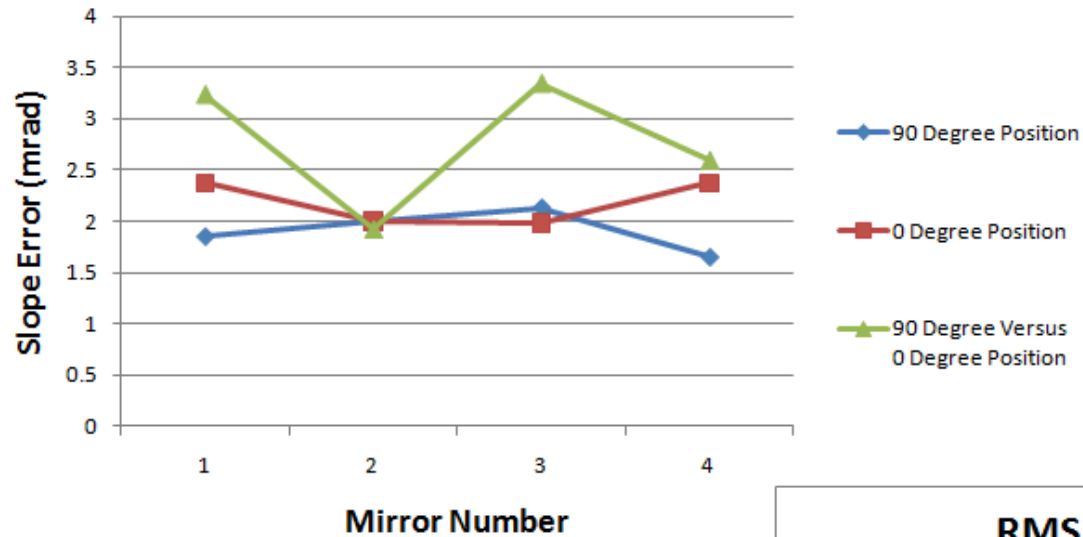
- 90 degree position
- 0 degree position
- Max displacement = 0.9 mm
- Max displacement = 0.7 mm



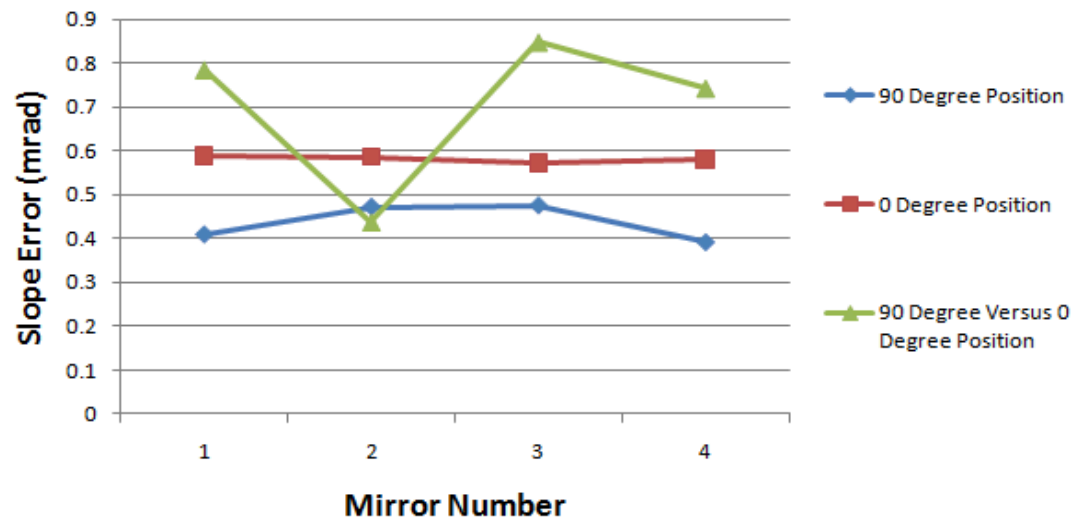
Displacement exaggeration scale = 200

Slope Errors

Maximum Slope Errors in Trough Positions



RMS Slope Errors in Trough Positions

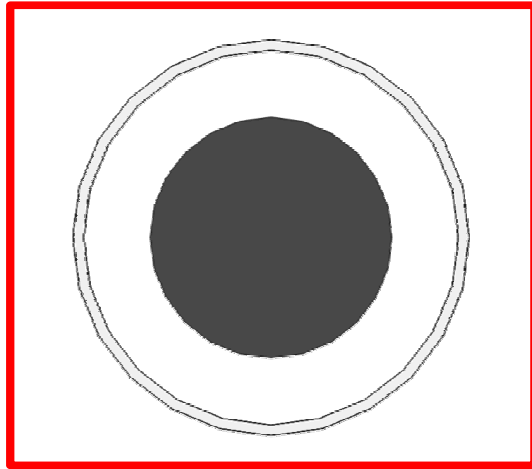




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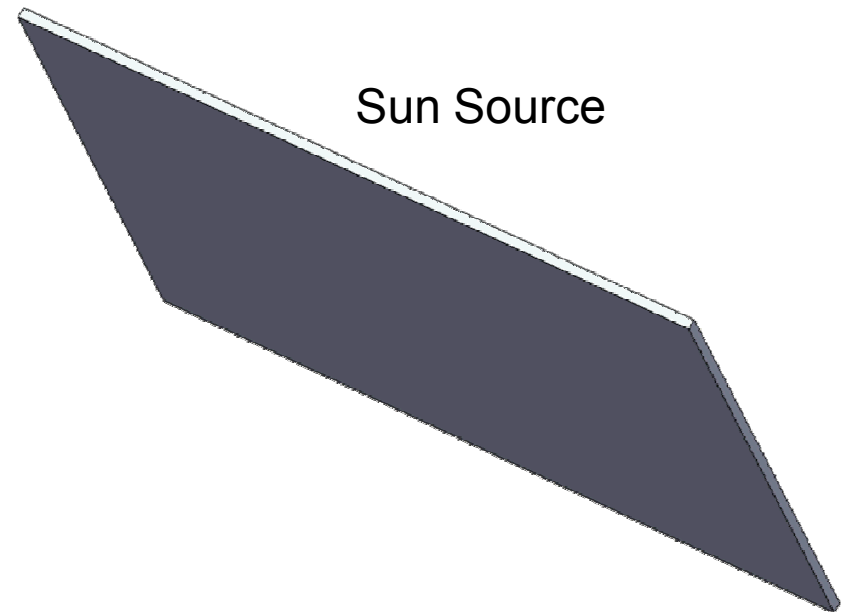
Ray Trace Modeling Components



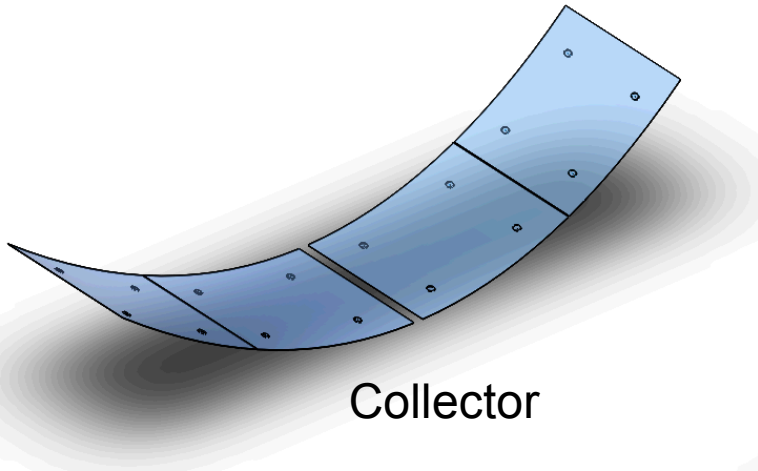
HCE with Envelope



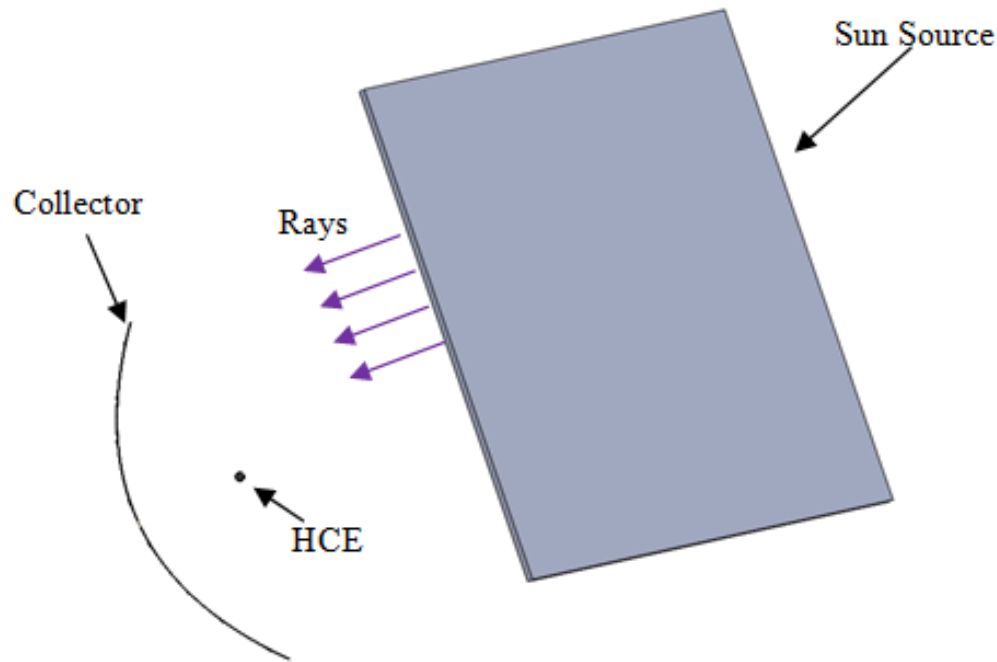
Sun Source



Collector



LS-2 Analysis: Optical Performance



HCE and Envelope

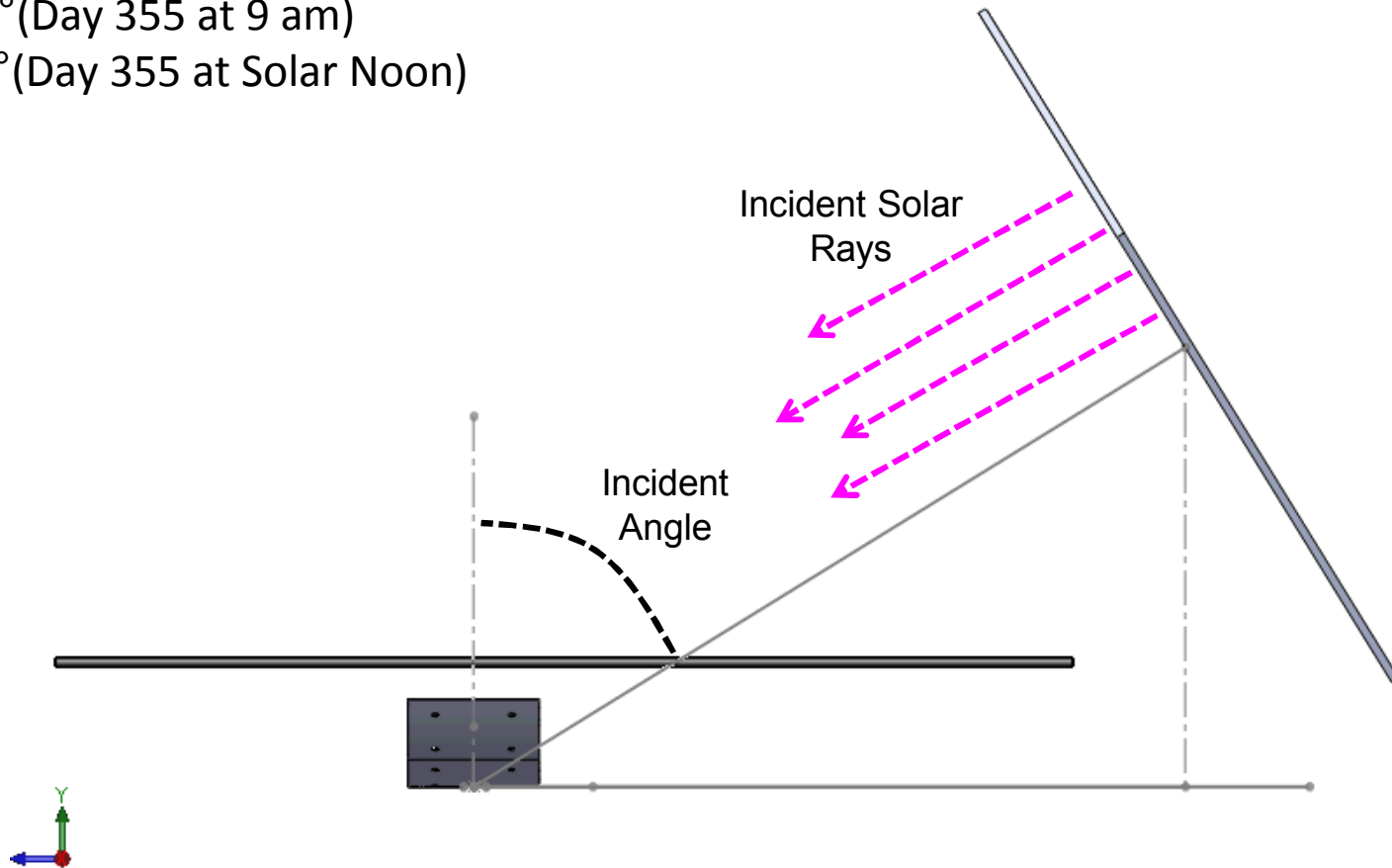
- Glass envelope medium: Schott N-BK7 ($\eta=1.5168$)
- Schott PTR-70
- HCE is 70mm

Sun Source

- Sun cone angle $\sim 0.55^\circ$
- Direct normal irradiance (DNI) of 1000 W/m^2
- Initially emits 100,000 rays
- Scattering surface scatters each ray into 10 children rays

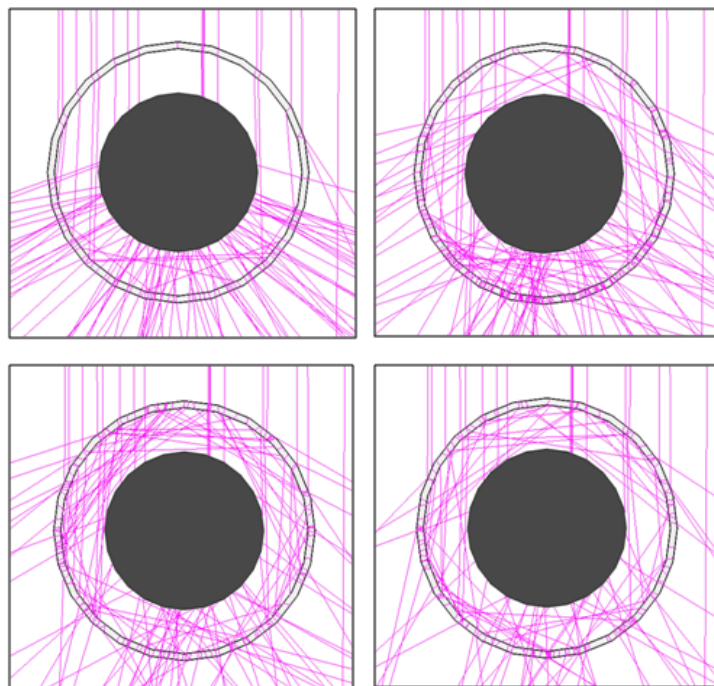
Solar Incident Angles

- 44.22° (Day 355 at 9 am)
- 58.32° (Day 355 at Solar Noon)

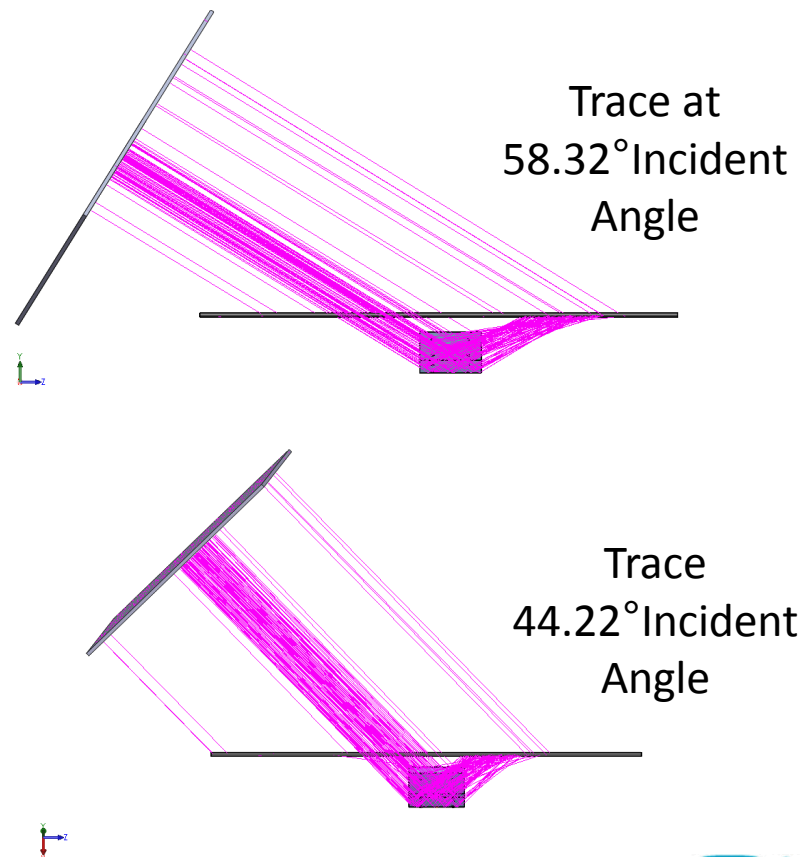


LS-2 Analysis: Optical Performance

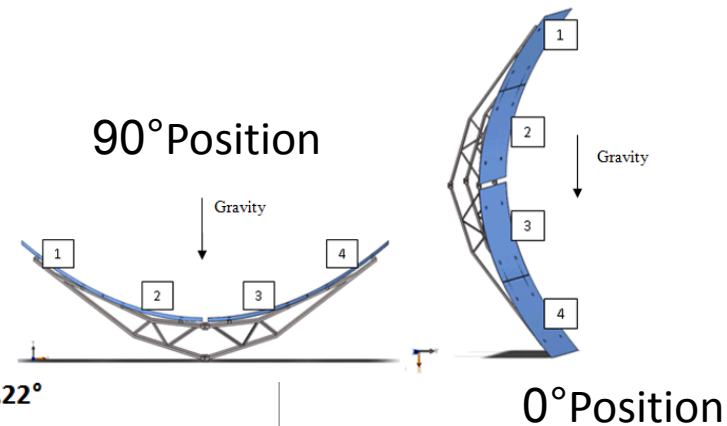
$$\text{Intercept Factor} = \frac{\text{Power from the collector hitting the receiver}}{\text{Total power from the collector}}$$



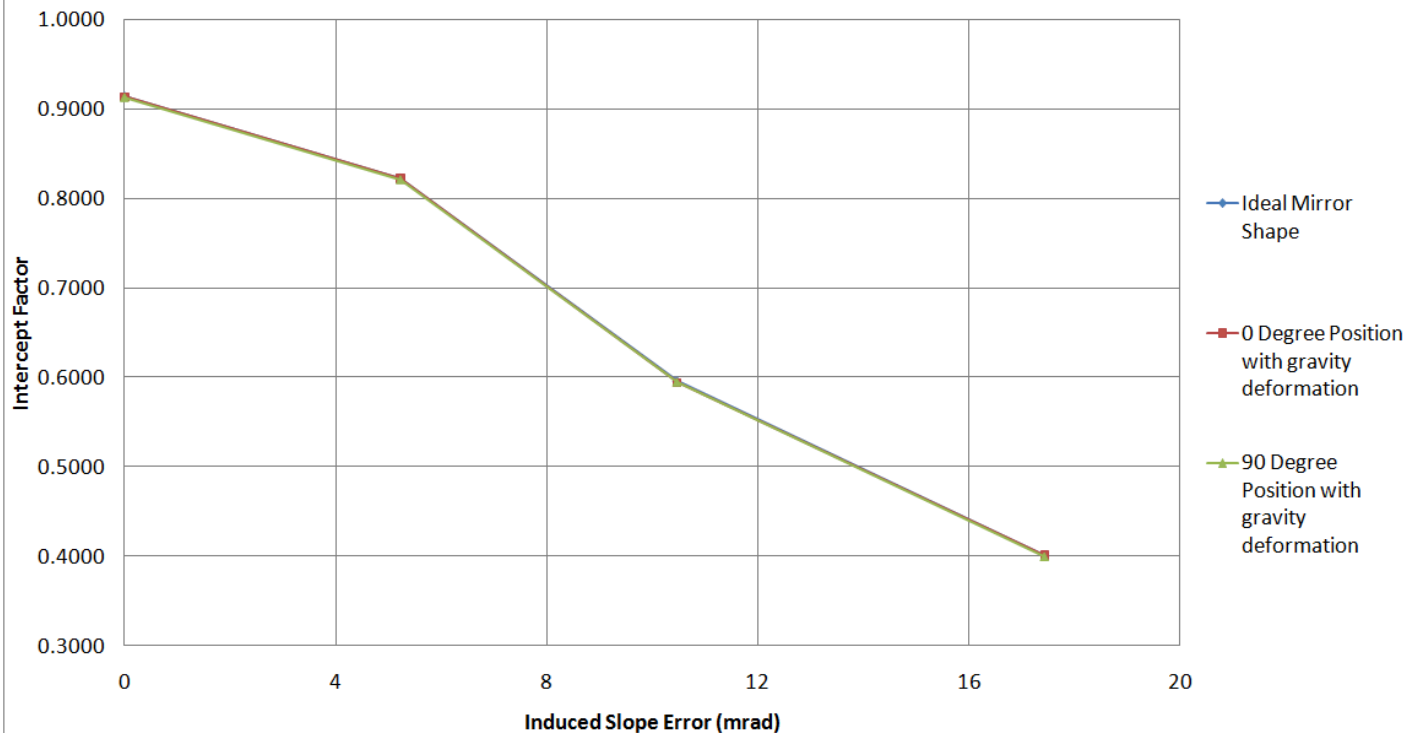
(Top Left) 0 mrad additional slope error;
(Top Right) 5.23 mrad additional slope error;
(Bottom Left) 10.47 mrad additional slope error;
(Bottom Right) 17.44 mrad additional slope error



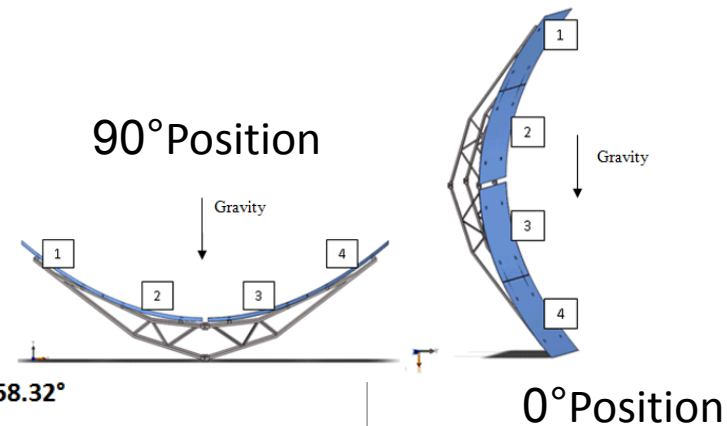
Intercept Factors at 44.22°



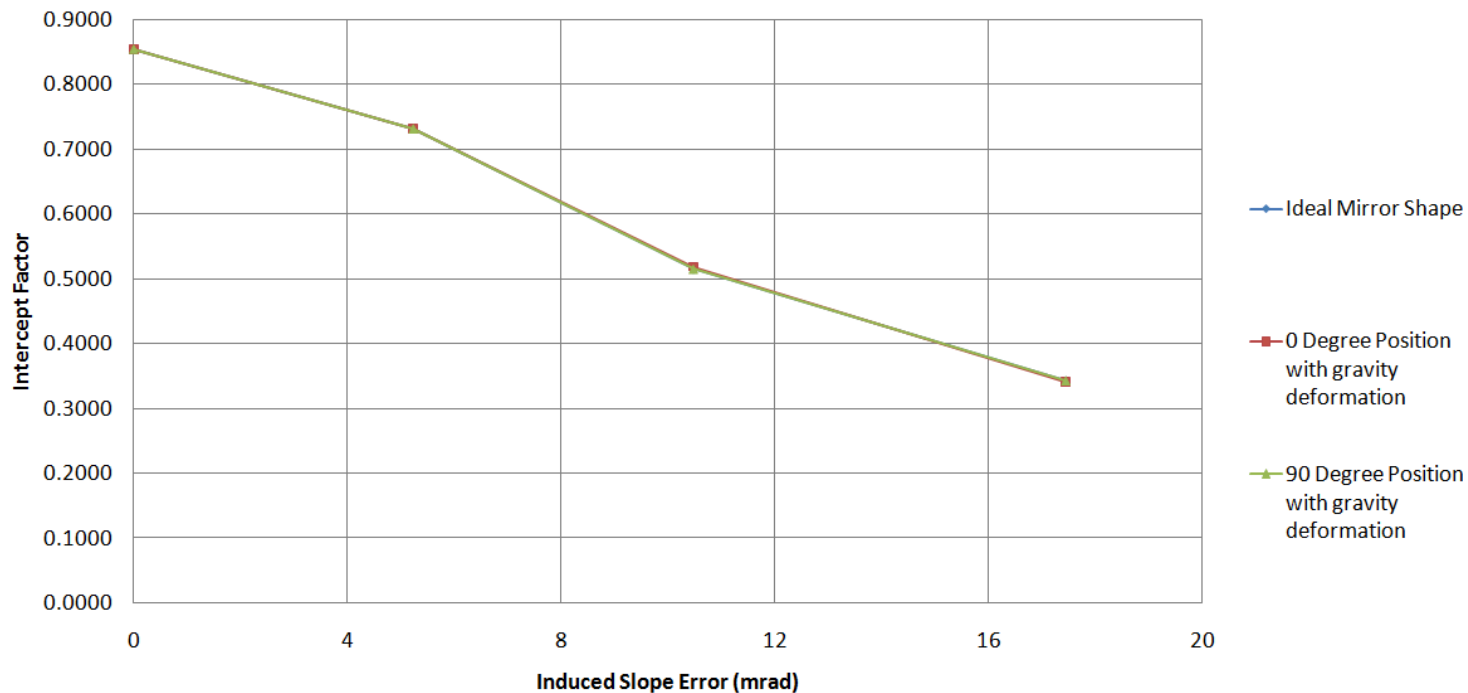
Induced RMS slope errors versus Intercept Factor for Incident Angle of 44.22°



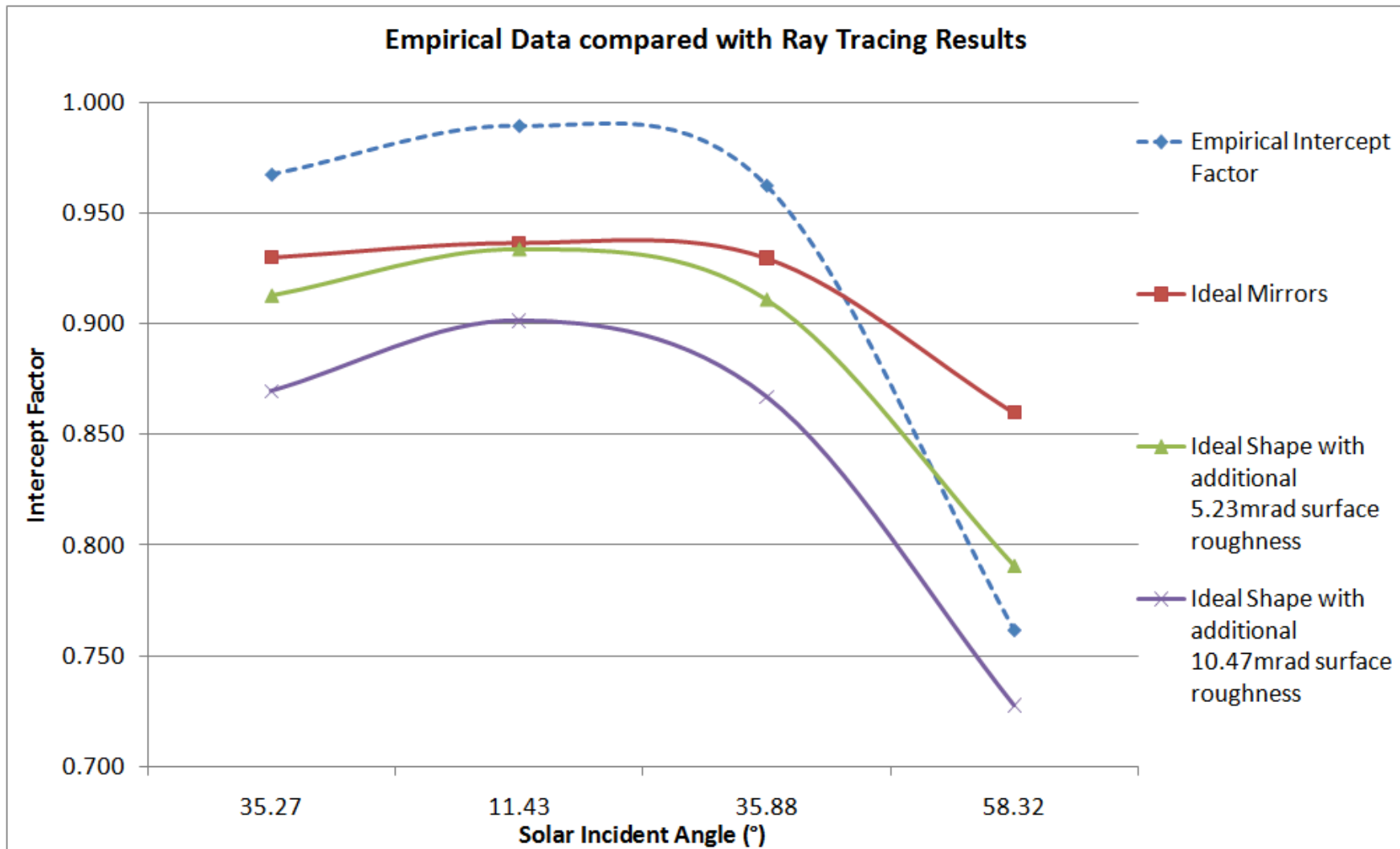
Intercept Factors at 58.32°



Induced RMS slope errors versus Intercept Factor for Incident Angle of 58.32°



Empirical Data Comparison





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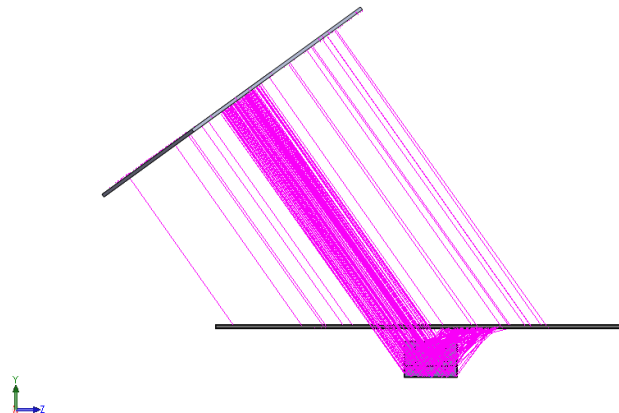


Conclusions

- **Ray tracing has been combined with FEA to evaluate the optical performance of a trough module under gravity loads**
- **Simulated intercept factors were not impacted significantly by gravity**
 - However, structural/gravity impacts of torque tube and pylons were not included
- **Reflectivity of the envelope is crucial in the ray-tracing process**

Future Work

- **Expand analysis to a full trough collector module**
- **Evaluate impacts of wind loading on optical performance**



Questions

